

Agenda

| Time (EST) | Topic | Speaker |
|-------------------|--|--|
| 11:00 - 11:02AM | Welcome/Housekeeping | Mr. Andrew Barto, NRC |
| 11:02 - 11:05AM | Workshop Theme and Intro | Dr. William Wieselquist |
| 11:05 - 11:15AM | HALEU Availability Program | Mr. William McCaughey, Director, Advanced Fuels Technologies, DOE-NE |
| 11:15 - 11:25AM | Project Background | Mr. Don Algama, DOE-NE |
| 11:25 - 11:35AM | Project Goals | Mr. Andrew Barto, NRC |
| 11:35AM - 12:35PM | Discussion of Considerations for HALEU-Based Fuel Cycle Validation Basis Assessment and Benchmark Prioritization, Including: <ul style="list-style-type: none"> • Current HALEU-Based Reactor Landscape and Transportation Packages • Current Nuclear Data Gaps (e.g. TSL Uncertainty) | Dr. William B.J. Marshall Dr. Iyad Al-Qasir Dr. Mathieu Dupont Dr. Lisa Fassino |
| 12:35 - 12:50PM | Open Discussion | Audience Questions |
| 12:50 - 1:20PM | Background on Validation Methods and the need for Application Models | Dr. William B.J. Marshall Mr. Alex Shaw |
| 1:20 - 1:50PM | Presentation of Recently Developed Criticality Safety Application Models | Dr. William B.J. Marshall Mr. Alex Shaw Dr. Veronica Karriem |
| 1:50 - 2:15 PM | Open Discussion | Audience Questions |
| 2:15 PM | Concluding Remarks | Dr. Will Wieselquist |
| | Adjourn | Ms. Lindsey Aloisi |

Workshop 1 Theme and Intro

- Demonstrate our strategy for prioritizing benchmarks
 1. Survey the field
 2. Prioritize a target application
 3. Develop an application model (today: **fresh fuel pebble transport**)
 4. Assess the validation basis
 5. Host a workshop
 6. Develop Experiment Support Opportunity (ESO) to address gaps in validation bases
 7. Rinse and repeat
- ESOs are the main vehicle for critical benchmark awards
- We are hungry for information
 - **Long lead-time on nuclear data and experiments!**
 - Existing measurements that could become benchmarks
 - From reactor designers: what are your intended transportation packages, front-end/back-end storage systems
- Any ideas where you may need additional nuclear data or benchmarks for safe, commercial-scale operations
- Feedback methods
 - Use the chat 😊
 - Respond to feedback form (following the workshop)
 - Email DNCSH@ornl.gov
- When to ask questions?
 - Feel free to ask questions in the chat, we may answer in the chat or hold it for the discussion period
 - During the discussion period, we would like attendees to raise their virtual hands to ask questions and we'll give some preference to those versus chat-based questions

HALEU Availability Program (HAP)

02/29/24

Energy Act of 2020; Sec. 2001 “Advanced Nuclear Fuel Availability” (42 U.S.C. 16281;
PL-116)
Section (A) and (C)(ii)

William McCaughey NE-42 Office Director

Authorities

- The Energy Act of 2020 authorizes the DOE to “support the availability of HA–LEU for civilian domestic research, development, demonstration, and commercial use.”
- Inflation Reduction Act in 2022 provided initial funding of \$700M divided into three areas.
 - \$500M to develop near-term and long-term sources of HALEU.
 - \$100M to develop criticality safety BM and support vendor transportation packages
 - \$100M for supporting activities.

HALEU Availability Program (HAP) Elements

Eleven Elements that Compose the Program

- Reclamation from EBR-II
- Downblending SRS & Y-12
- HALEU enrichment follow on operations at Piketon
- Enrichment in commercial quantities
- Post-enrichment deconversion
- The HALEU Consortium
- The HALEU Bank
- Physical storage
- Transportation
- NEPA
- DOE/NRC Criticality Safety for Commercial-Scale HALEU Fuel Cycle and Transportation (DNCSH) ← **This workshop**

HALEU Availability Program (HAP)

Goal

- Overall goal is to kick start the industry on the road to be self sufficient.

DOE/NRC Criticality Safety for Commercial-Scale HALEU Fuel Cycle and Transportation (DNCSH)

02/29/24

Energy Act of 2020; Sec. 2001 “Advanced Nuclear Fuel Availability” (42 U.S.C. 16281; PL-116)
Section (A) and (C)(ii)

Don Algama (DOE Fed. Manager)

Authorities

- The Energy Act of 2020 authorizes the DOE and NRC to collaborate to develop **criticality safety data**.
- Inflation Reduction Act in 2022 provided \$700M, of which **\$60M** is the cost estimate for this project.
- **HALEU fuel cycle** is the scope, except reactor operation step.
- **NRC** is primary customer.

Authorities: LWR Fuel Cycle Mapping

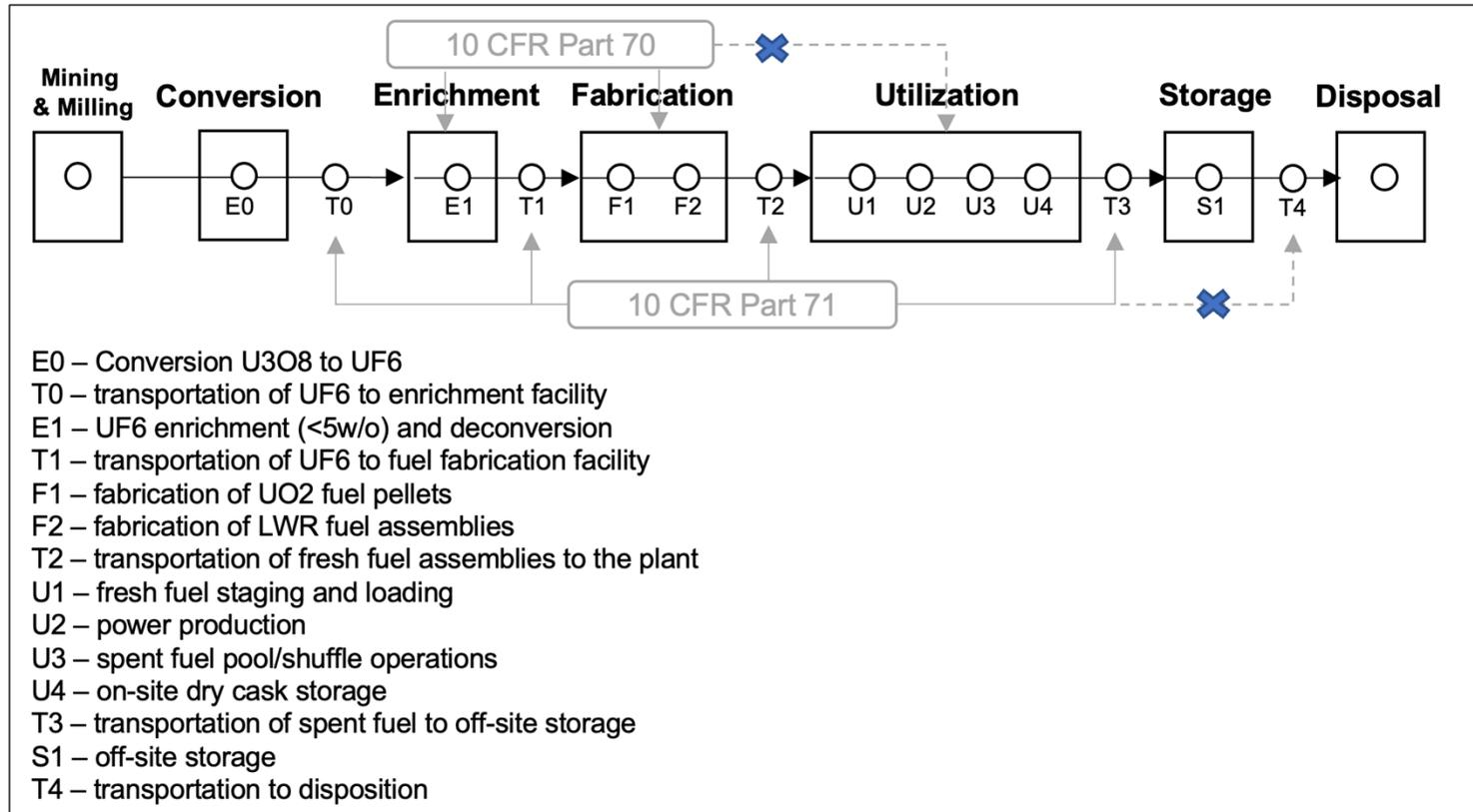
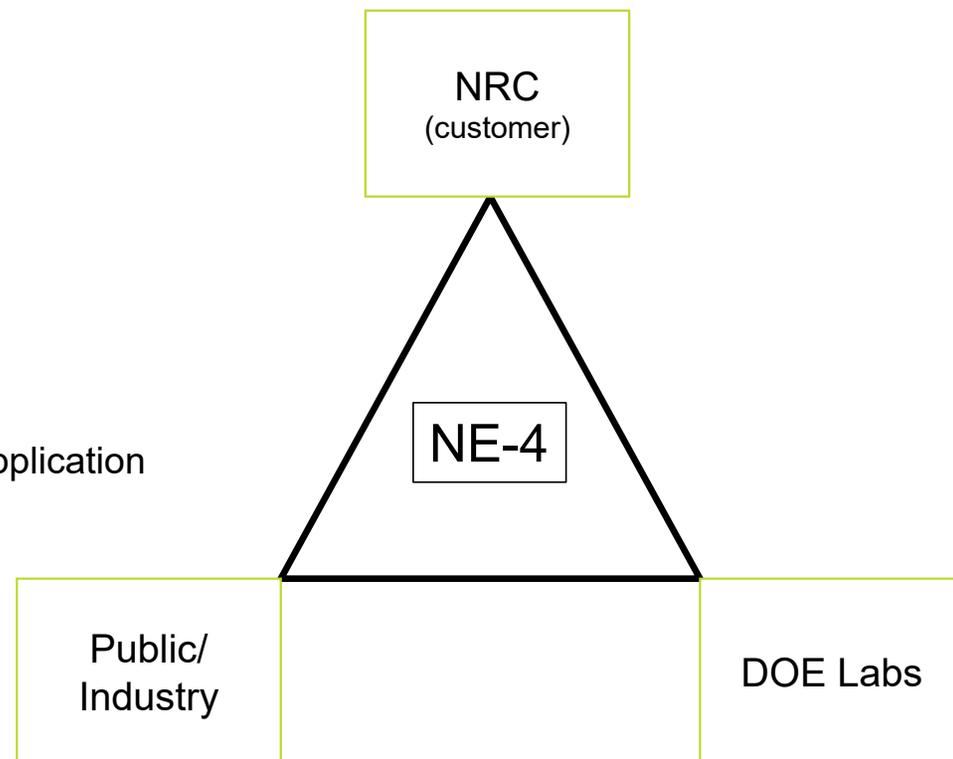


Illustration of a LWR fuel cycle based on ([ML21088A047](#)) annotated with NRC regulations of interest for this effort

Who and Approach

- Customer:
 - NRC
- Partners:
 - DOE offices (NE, NNSA/NCSP, OS/NP, etc.).
 - DOE labs and universities.
 - Funded experiment opportunities.
- Approach:
 1. Develop *working* HALEU fuel cycle analysis and application models (HTGR, SFR, MSR, HPR, etc.)
 2. Conduct public workshops.
 3. **Issue experiment opportunities.**
 4. **Review and responses.**
 5. Data collection, interpretation, processing and public reports.



DNCSH Organization Structure – Management Team

| Name | Project Role | Responsibilities Include |
|---------------------|--------------------------------------|--|
| William McCaughey | DOE Office Director | Coordinate throughout DOE Complex |
| Don Algama | DOE Fed Manager | Coordinate throughout DOE Complex |
| Mark Angil | DOE Advisor | Advisor and representative for DOE HALEU Consortium |
| Bob Rova | DOE Experiment Support Opportunities | Implementation |
| Andrew Barto | NRC Program Manager | Coordinate throughout NRC Complex |
| William Wieselquist | National Technical Director | Coordinate technical activities, approve and review tasks, assign top-level task leads. |
| Lindsey Aloisi | Project Manager | Collect status, update PMP, allocate and track spending, update PICS-NE, and manage plans. |

DNCSH Organization Structure – Technical Team Leads

| Responsibilities | Project Role | Name |
|-------------------------|---|---------------------|
| Engagement Area 1 | Management and Engagement | William Wieselquist |
| Engagement Area 2 | Quality Assurance | Travis Greene |
| Engagement Area 3 | Survey and Summaries | Walid Metwally |
| Engagement Area 4 | Facility Enhancements | Catherine Percher |
| Engagement Area 5 | Reference Application Model Development | Nathanael Hudson |
| Engagement Area 6 | Critical Benchmark Execution | Catherine Percher |
| Engagement Area 7 | Nuclear Data Enhancement | Iyad Al-Qasir |
| Engagement Area 8 | Simulation Methods Improvements | Rob Lefebvre |
| Engagement Area 9 | Validation Basis Improvement | Ugur Mertuyrek |

Success Metrics

- Tier 1 (easily quantifiable):
 - Publicly available experiments.
 - Publicly available application models (including enabling reports).
 - Publicly available methods and approaches.
- Tier 2 (difficult to quantify):
 - Number of applications using new data/methods.
 - Number of times NRC can use new data/methods in review.

Concluding Remarks

- NRC is primary customer and project will produce publicly available data.
- Unique opportunity that will have long lasting impact on the commercial industry.
- Project application area is 10CFR70 and 10CFR71.
- Coordinate high impact experiments via experiment support opportunities available to the public. More information to follow.
- Key success metric will be in the availability of public data and models

**WORKSHOP ON COLLABORATION BETWEEN DOE AND NRC
FOR DEVELOPMENT OF CRITICALITY SAFETY
BENCHMARKING DATA FOR HALEU FUEL CYCLE AND
TRANSPORTATION**

February 29, 2024

Drew Barto

Division of Fuel Management

Office of Nuclear Material Safety and Safeguards

U.S. Nuclear Regulatory Commission

OVERVIEW

- Background
- Regulations
- Code Validation
- Existing Transportation Packages
- DNCSH Outcomes

BACKGROUND

- Office of Nuclear Material Safety and Safeguards Division of Fuel Management (NMSS/DFM) within NRC is responsible for regulation of:
 - Fuel cycle facilities under 10 CFR Part 70
 - Radioactive material (including fissile material, e.g., HALEU) transportation package designs under 10 CFR Part 71
- Regulations include requirements to maintain criticality safety under all conditions

REGULATIONS

- 10 CFR 70.61 – Subcritical under normal and credible abnormal conditions
- 10 CFR 70.64 – Double contingency principle
- 10 CFR 70.24 – Criticality monitoring
- 10 CFR 71.55 - Single packages.
 - 10 CFR 71.55(b): subcritical considering water in-leakage
 - 10 CFR 71.55(d): subcritical under normal conditions of transport (NCT)
 - 10 CFR 71.55(e): subcritical under hypothetical accident conditions (HAC)
- 10 CFR 71.59 – Package arrays.
 - Subcritical under NCT and HAC
 - Limiting number of packages under NCT or HAC used to determine Criticality Safety Index (CSI) to control package accumulation on conveyance

CODE VALIDATION

ANS 8.1 - Nuclear Criticality Safety In Operations With Fissionable Materials Outside Reactors:

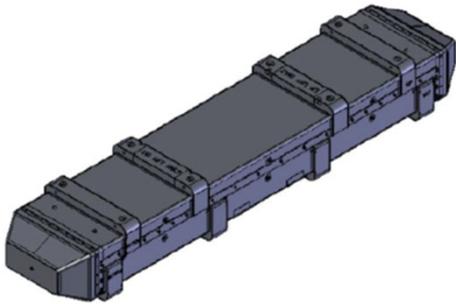
- Validation shall be performed by comparison to critical experiments, and the area of applicability for the validation should be established from this comparison
- Establish:
 - Applicability of experiments
 - Code bias and bias uncertainty
 - Trending analysis

CODE VALIDATION

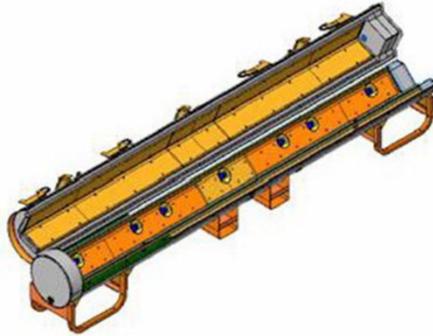
- ANS 8.24 - *Validation of Neutron Transport Methods for Nuclear Criticality Safety Calculations*
- NUREG/CR-6698 - *Guide for Validation of Nuclear Criticality Safety Computational Methodology*
- NUREG/CR-5661 - *Recommendations for Preparing the Criticality Safety Evaluation of Transportation Packages*
- NUREG/CR-6361 - *Criticality Benchmark Guide for Light-Water-Reactor Fuel in Transportation and Storage Packages*
- International Criticality Safety Benchmark Evaluation Project (ICSBEP):
 - Descriptions of over 5,000 laboratory critical experiments
 - Grouped by fissile media, physical form, and neutron energy where most fissions occur
 - Many experiments representative of <5% enriched UO₂ LWR fuel; less for enrichment range of 5-20%; much less for key systems of interest (e.g., TRISO, low moderation UF₆)

EXISTING HALEU PACKAGES

LWR Fresh Fuel:



MAP 12 and MAP 13 (71-9319)



Traveller (71-9380)

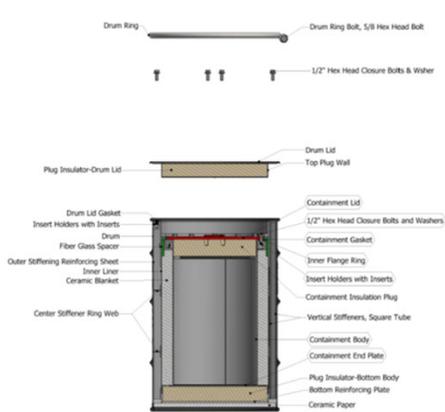


GNF RAJ-II (71-9309)

- **Certified to LEU+ range – up to 8.0% enrichment**
- **No issues with code validation**
 - Many applicable low enriched UO_2 experiments
 - Regulations require consideration of moderation by water – thermal uranium systems generally fairly easy to validate

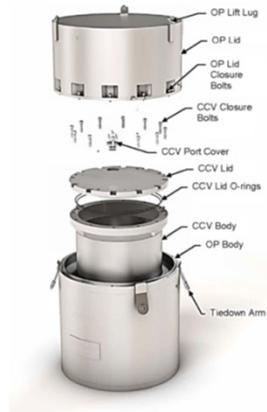
The critical benchmarks performed at SNL with 7% enriched fuel were instrumental in certifying these package designs.

EXISTING HALEU PACKAGES



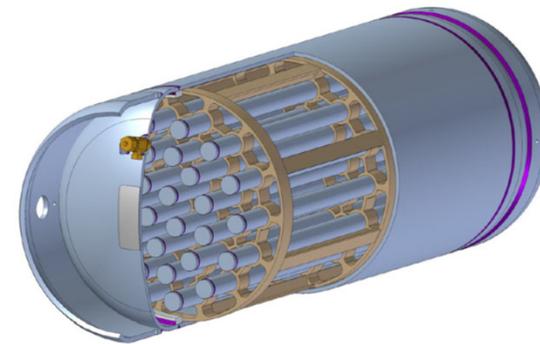
Versa Pac (71-9342)

- Varied uranium contents enriched up to 100%
- TRISO allowed
- Low mass of ^{235}U per package
- CSI 0.7 to 1.4



Optimus-L (71-9390)

- Up to 68 kg of 20% enriched TRISO compacts
- CSI = 0
- Gross weight ~9,200 lbs.



DN30-X (71-9388)

- UF_6 cylinder with internal criticality control system in overpack
- Up to 10% enriched UF_6 in 30B-10 cylinder; 20% enriched in 30B-20
- Up to 1,460 kg UF_6 in 30B-10, 1,271 kg in 30B-20 (standard 30B is 2,277 kg)
- CSI = 0.0

DNCSH OUTCOMES

- High-quality publicly available benchmark experiments, nuclear data, and evaluations applicable to wide range of HALEU systems where current data is lacking
- Will allow applicants and licensees more options for optimizing HALEU fuel cycle and transportation systems, with potentially:
 - Higher throughput fuel cycle processes
 - Higher capacity transportation package designs
 - Fewer RAIs related to code validation and criticality

Discussion of Considerations for HALEU- Based Fuel Cycle Validation Basis Assessment and Benchmark Prioritization

Lisa Fassino
Iyad Al-Qasir
Mathieu Dupont

DNCSH Workshop #1
February 29th, 2024, Germantown, MD

ORNL is managed by UT-Battelle LLC for the US Department of Energy

Outline

Introduction

Current HALEU-Based Reactor and Transportation Landscape

Lisa Fassino

Nuclear Data Gaps: Current Status of Thermal Scattering Laws for HALEU-Fueled Advanced Reactors

Iyad Al-Qasir

Review of Available Critical Experiment Benchmarks and Critical Experiment Facilities for HALEU Fuel Transport Validation

Mathieu Dupont

Introduction

Advanced reactors are driving a change in the nuclear power landscape

New analyses must identify where the current validation basis is and is not suitable for changing fuel cycle needs

**Larger variety of
fuel forms**

**Higher
Enrichment**

Higher Burnup

HALEU ARDP Designs and Transportation Packages

Lisa Fassino



HALEU in Advanced Reactor Designs

- **Goal:** scope the unique features of HALEU reactor fuel to determine needs for validation basis
 - **As a launching point:** begin with designs in the Advanced Reactor Demonstration Program (ARDP) using HALEU
 - Only 1 not planning to use HALEU (Holtec International's SMR-160)
 - 10 Designs, 9 with HALEU
 - **Far from an exhaustive list!** →



| Leads | Designs |
|---------------------------------|---------|
| TerraPower | Sodium |
| X-energy | Xe-100 |
| Kairos Power | KP-FHR |
| Westinghouse Nuclear | eVinci |
| Southern Company and TerraPower | MCFR |
| BWXT | BANR |
| ARC | ARC-100 |
| GA-EMS | FMR |
| MIT | HC-HTGR |

Many more...

The MARVEL microreactor by DOE

The Aurora powerhouse reactor by Oklo

The Hermes test reactor and Hermes 2 by Kairos Power

The Ultra Safe Nuclear Corporation (USNC) micro modular reactor (MMR)

The Lightbridge helically twisted HALEU fuel for current commercial reactors

The Project Pele microreactor by the US Department of Defense (DoD) and BWXT

The Demonstration Rocket for Agile Cislunar Operations (DRACO) by the Defense Advanced Research Projects Agency (DARPA) in collaboration with the National Aeronautics and Space Administration (NASA)

The Molten Salt Research Reactor (MSRR) by the Nuclear Energy eXperimental Testing Laboratory (NEXT Lab) at Abilene Christian University (ACU)

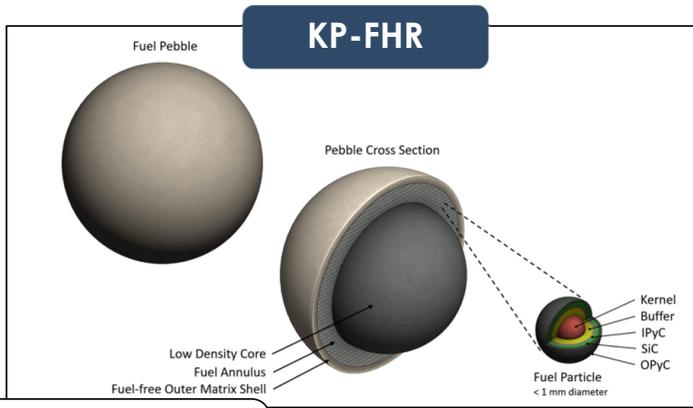
This is not an exhaustive list, either!

Let us know about public references for any additional fuel forms, storage, transportation at this email:
DNCSH@ornl.gov

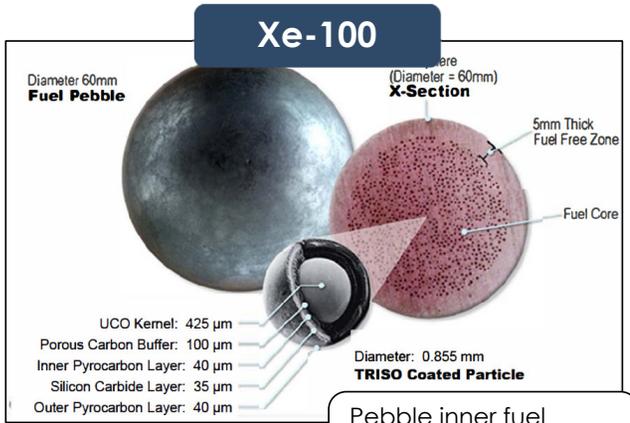
Summary of HALEU ARDP Characteristics

| Lead | Reactor Name | Reactor Type | Neutron Spectrum | Fuel Type | Power | Enrichment (wt% ²³⁵ U) | Moderator | Reflector | Coolant |
|---------------------------------|--------------|------------------------|------------------|--|----------|-----------------------------------|---------------------------|--|-------------------|
| TerraPower | Natrium | SFR | Fast | Sodium-bonded Metallic Alloy U-10Zr Pins (Type 1) | 345 MWe | 19.75 | N/A | — | Salt |
| X-energy | Xe-100 | Pebble Bed HTGR | Thermal | UCO TRISO Spherical Compacts | 80 MWe | 15.5 | Graphite | Graphite | Helium |
| Kairos Power | KP-FHR | Pebble Bed FHR | Thermal | UCO TRISO Annular Spherical Compacts with Low-Density Graphite Cores | 140 Mwe | 19.55 | Pyrolytic Graphite, FLiBe | Graphite | FLiBe |
| Westinghouse Nuclear | eVinci | Heat-pipe Microreactor | Thermal | UCO TRISO Cylindrical Compacts | 5 Mwe | 19.75 | Graphite | — | Sodium Heat Pipes |
| Southern Company and TerraPower | MCFR | MSR | Fast | Dissolved Uranium in Salt (NaCl-UCl ₃) | 800 MWe | HALEU | N/A | — | Salt |
| BWXT | BANR | HTGR | Thermal | UN TRISO in SiC, Carbon Matrix Compact, Additively Manufactured | 50 MWth | 19.75 (Baseline Design) | Graphite | — | Helium |
| ARC | ARC-100 | SFR | Fast | Sodium-bonded U-10Zr pins | 100 MWe | 20 Max.; 13.1 Avg. | N/A | Stainless Steel | Sodium |
| GA-EMS | FMR | GFR | Fast | UO ₂ Pellets | 44 MWe | 19.75 | N/A | Zr ₃ Si ₂ and Graphite | Helium |
| MIT | HC-HTGR | HTGR | Thermal | TRISO Compact | ~58 MWth | — | Graphite | — | Helium |

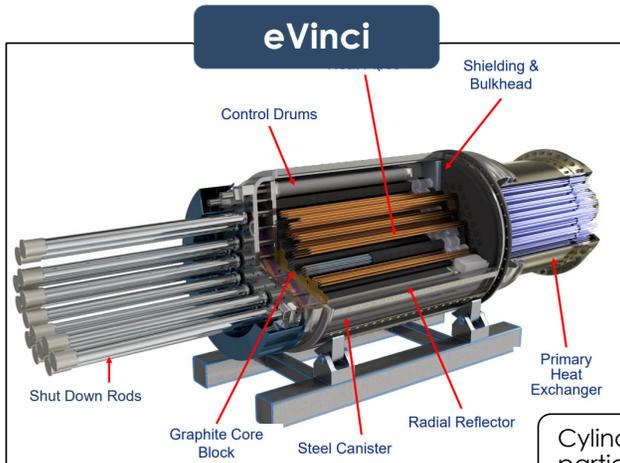
Fuel Forms Across ARDP Designs



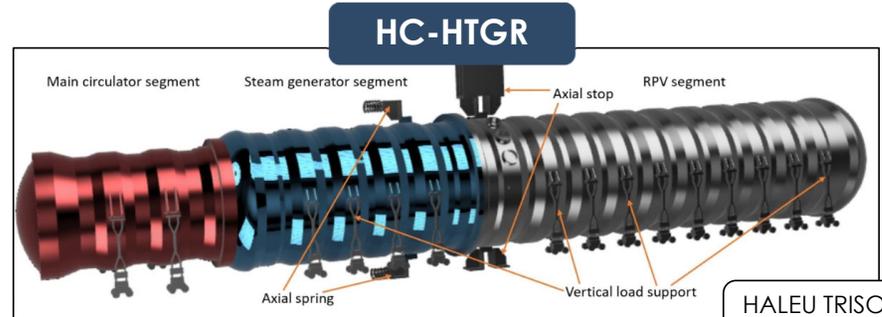
Pebble annular fuel region with UCO TRISO particles



Pebble inner fuel region with UCO TRISO particles

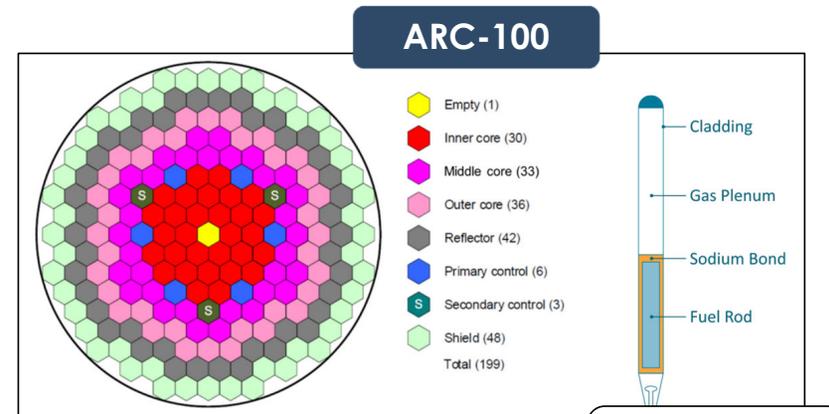
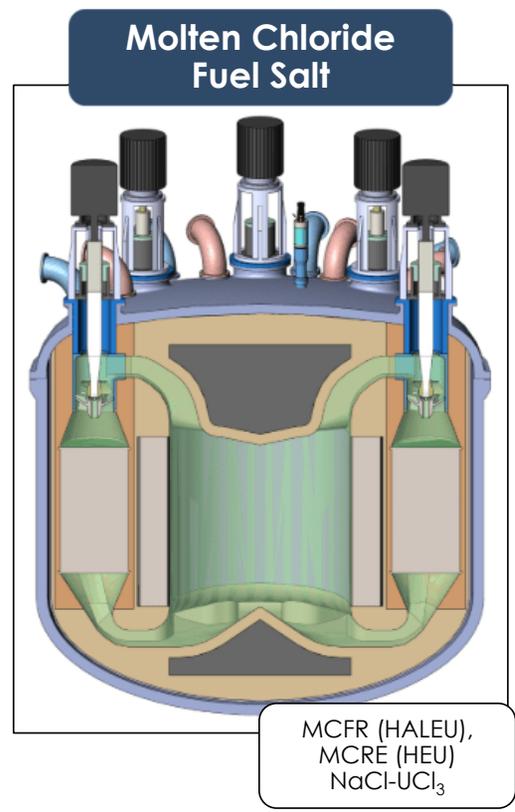
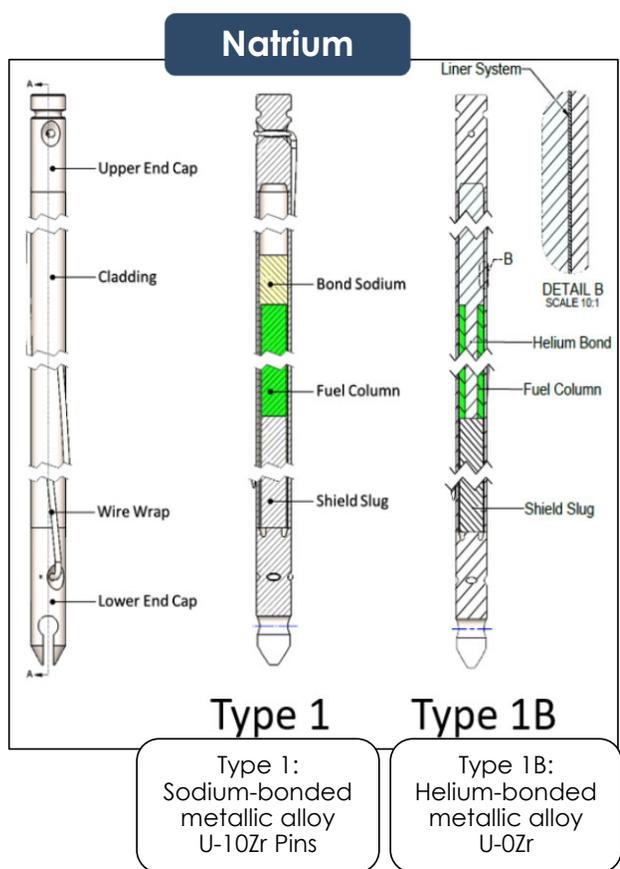


Cylindrical UCO TRISO particle compacts

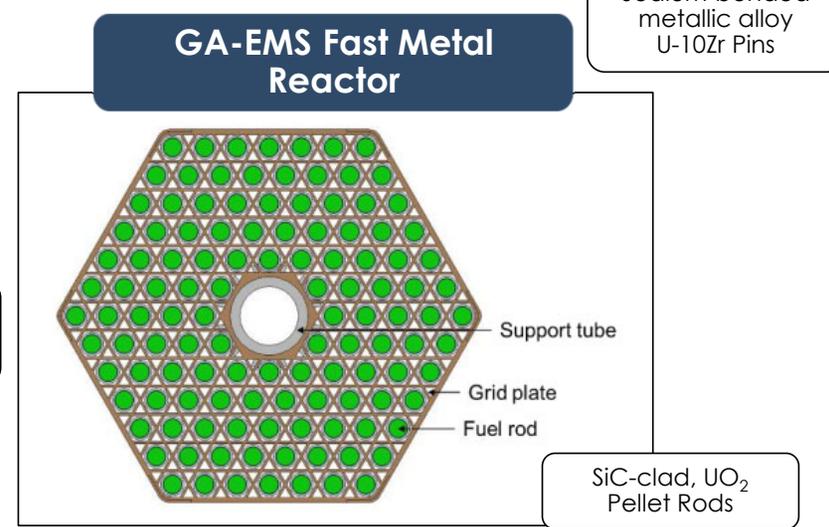


HALEU TRISO Particles Expected

Fuel Forms Across ARDP Designs

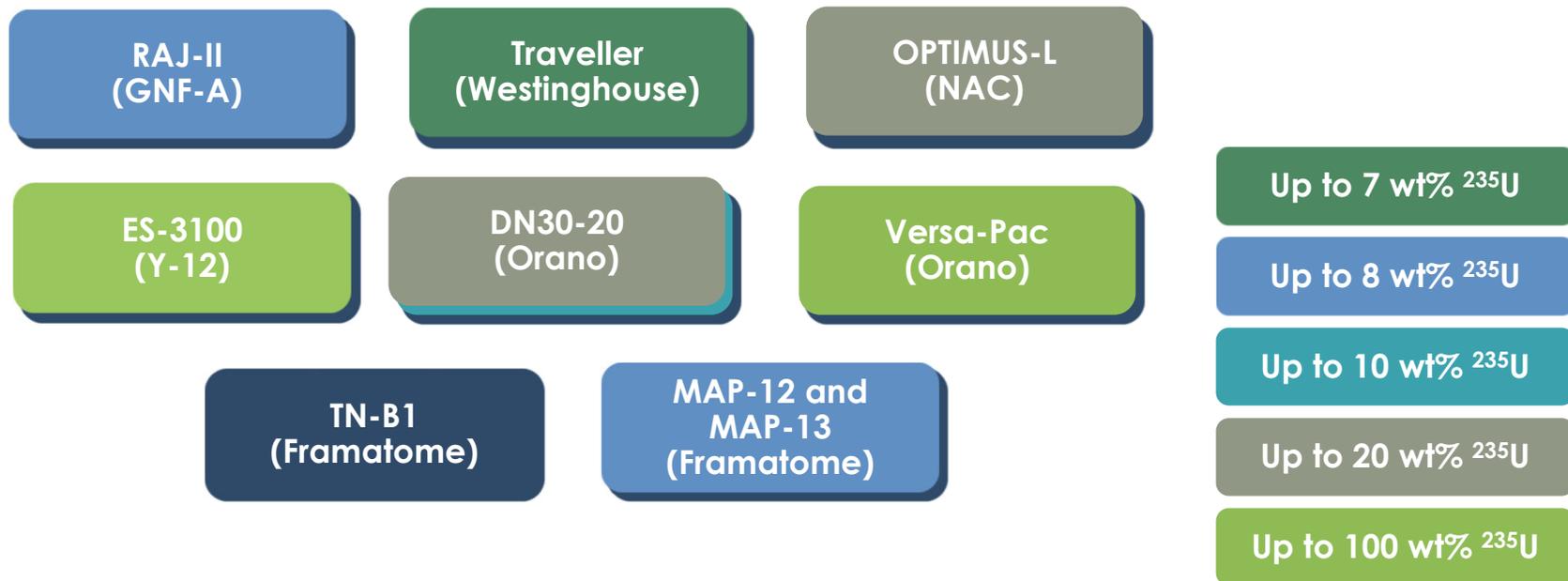


Sodium-bonded metallic alloy U-10Zr Pins



Transportation Packages

- NRC lists the following transportation packages as currently involved in increased enrichment licensing activities:



Summary of HALEU Transportation Package Details

| Transportation Package | Owner | Fuel Type | Approved Enrichment, wt% ²³⁵ U | Content Limits | Approximate Dimensions, m |
|------------------------|--------------|---|---|--|--|
| Traveller STD | Westinghouse | Fresh or Slightly Contaminated PWR UO ₂ Assemblies or Fuel Rods | Up to 6% for assemblies or up to 7% for fuel rods | One assembly or one container of loose rods | 5.0 x 0.7 x 1.0 (L x W x H) |
| Traveller XL | | | | | 5.7 x 0.7 x 1.0 (L x W x H) |
| MAP-12 | Framatome | Fresh uranium fuel assemblies | Up to 8% | Two assemblies | 5.3 x 1.1 x 0.8 (L x W x H) |
| MAP-13 | | | | | 5.6 x 1.1 x 0.8 (L x W x H) |
| TN-B1 | Framatome | Fresh UO ₂ PWR or BWR assemblies or UC fuel rods | Up to 5%, with request to extend to 8% | One assembly | 1.8 x 0.2 x 0.1 (inner L x W x H) 2.0 x 0.3 x 0.3 (outer L x W x H) |
| RAJ-II | GNF-A | BWR fuel assemblies; BWR, CANDU, or PWR rods | Up to 5% in UC; Up to 8% in UO ₂ . | Two assemblies | 1.8 x 0.2 x 0.1 (inner L x W x H) 2.0 x 0.3 x 0.3 (outer L x W x H) |
| OPTIMUS®-L | NAC | Certain waste materials; unirradiated TRISO cylindrical compacts | Up to 20% for cylindrical TRISO compacts | 68 kgU | 0.3 x 0.5 (inner D x H) 0.5 x 0.7 (outer D x H) |
| DN30-10 | Orano | UF ₆ | Up to 10% | 98 kg fissile material, 1460 kg UF ₆ | 0.8 x 2.1 (cylinder D x H) |
| DN30-20 | | | Up to 20% | 170 kg fissile material, 1271 kg UF ₆ | 1.2 x 2.4 (package D x H) |
| Versa-Pac 55 (VP-55) | Orano | Uranium oxides, metal, and other compounds; Uranyl nitrate crystals; TRISO fuel | Up to 100% | 610 g ²³⁵ U up to 5% 505 g ²³⁵ U up to 10% 445 g ²³⁵ U up to 20% 360 g ²³⁵ U up to 100% | 0.4 x 0.6 x 0.9 (ID x OD x H) |
| Versa-Pac 110 (VP-110) | | | | | 0.5 x 0.8 x 1.1 (ID x OD x H) |
| ES-3100 | Y-12 | Uranium oxides, metals, alloys, compounds, and uranyl nitrate crystals | Up to 100% | Up to 9.682 kg ²³⁵ U in oxides with 921 g carbon and CSI of 0.0; Up to 35.2 kg ²³⁵ U in metals/alloys | 1.1 x 0.5 (D x H) |

Conclusions

- Fresh HALEU fuel for LWRs (up to 8%) can be transported
- Fresh HALEU fuel for ARDP reactors does not have commercial-scale packages, except maybe DN-30X and ES3100 in some cases
- Details still needed for ARDP designs to assess transportation package suitability, e.g.
 - Fuel salt characteristics for MCFR
 - Fabrication, transportation, and storage processes/plans
 - Materials/components transported in reactor (e.g. for SMRs or MMRs)
- We can only plan for what we know!

Nuclear Data Gaps: Current Status of Thermal Scattering Laws for HALEU-Fueled Advanced Reactors

Iyad Al-Qasir



Outline

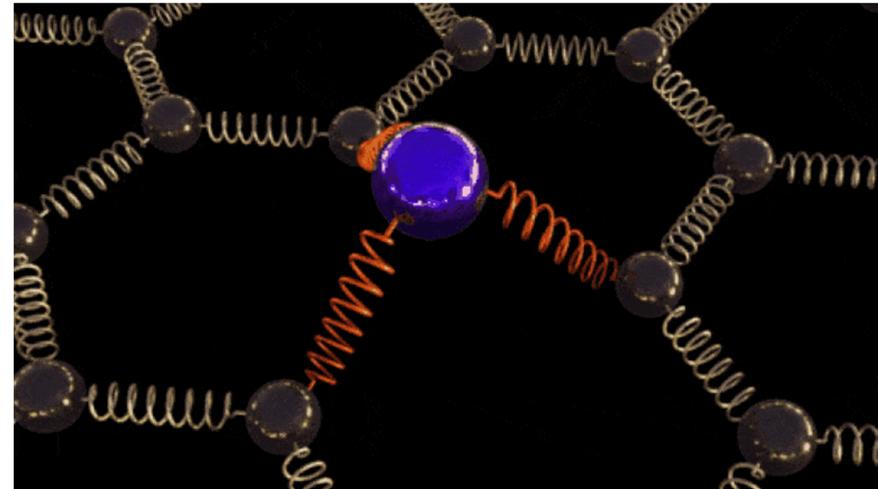
- Introduction
 - Importance of Nuclear Data
 - Thermal Neutrons
 - Neutron Moderation
- Status of Main Neutron Moderators
- Current Status Graphite TSL Sub-libraries
- Conclusions

Why Do We Need Nuclear Data?

- The effective design, operation, and eventual decommissioning of a nuclear power plant, along with licensing transportation packages for fresh or spent fuel, require extensive access to comprehensive nuclear data covering diverse radiation particles across a broad energy spectrum.
- The use of high-quality nuclear data in calculations is essential for accuracy, safety, reliability, optimization fuel performance, research, and **regulatory compliance** in various nuclear-related fields and applications.
- Nuclear data and uncertainty (aka covariance) plays a special role in similarity and validation basis assessment
- One specific category of relevant nuclear data is notably temperature-dependent and is referred to as the **thermal neutron scattering law (TSL)** or $S(\alpha, \beta)$.

Thermal Neutrons

- Thermal neutrons have wavelengths ($\sim\text{\AA}$) comparable to the separation distances of atoms in solids.
- Hence, the thermal motion of atoms or molecules in the scattering medium can no longer be ignored
- Thermal neutron scattering law (TSL) describes the neutron scattering intensity as a function of energy and momentum transfer between the thermal neutron and the scattering medium



ENDF/B-VIII.1 TSL Sub-Libraries

| Moderators | |
|--------------------------|---------------------------------------|
| H /Water/ICE | |
| 1 | H in H ₂ O (liquid) |
| 50 | O in H ₂ O (ice (Ih)) |
| 10 | H in H ₂ O (ice (Ih)) |
| 51 | O in D ₂ O (liquid) |
| 11 | D in D ₂ O (liquid) |
| 2 | para-Hydrogen |
| 3 | ortho-Hydrogen |
| 12 | para-Deuterium |
| 13 | ortho-Deuterium |
| Be compounds | |
| 26 | Be (metal) |
| 204 | Be+sd |
| 27 | Be in BeO |
| 46 | O in BeO |
| 28 | Be in Be ₂ C |
| 1021 | C in Be ₂ C |
| Graphite | |
| 30 | crystalline graphite |
| 301 | Graphite +sd |
| 31 | reactor-grade graphite (10% porosity) |
| 320 | reactor-grade graphite (20% porosity) |
| 32 | reactor-grade graphite (30% porosity) |
| Metallic Hydrides | |
| 5 | H in YH ₂ |
| 7 | H in ZrH |
| 3001 | Zr in ZrH ₂ |
| 3002 | H in ZrH ₂ |
| 3006 | Zr in ZrHx |
| 3007 | H in ZrHx |
| 3011 | Ca in CaH ₂ |
| 3013 | H1 in CaH ₂ |
| 3014 | H2 in CaH ₂ |
| 3031 | 7Li in 7LiH-mixed |
| 3032 | H in 7LiH-mixed |
| 3034 | 7Li in 7LiD-mixed |
| 3035 | D in 7LiD-mixed |
| 58 | Zr in ZrH |
| 55 | Y in YH ₂ |

| Fuel | |
|------|-----------------------------|
| 71 | N in UN |
| 72 | U in UN |
| 75 | U in UO ₂ |
| 45 | O in UO ₂ |
| 76 | U in UC |
| 71 | N in UN |
| 8000 | U-metal |
| 8010 | U-metal-10p |
| 8099 | U-metal-HEU |
| 8105 | U in UC-5p |
| 8110 | U in UC-10p |
| 8147 | U in UC-100P |
| 8148 | U in UC-HALEU |
| 8149 | U in UC-HEU |
| 8150 | C in UC |
| 8155 | C in UC-5p |
| 8160 | C in UC-10p |
| 8197 | C in UC-100P |
| 8198 | C in UC-HALEU |
| 8199 | C in UC-HEU |
| 8205 | U in UO ₂ -5p |
| 8210 | U in UO ₂ -10p |
| 8248 | U in UO ₂ -HALEU |
| 8249 | U in UO ₂ -HEU |
| 8255 | O in UO ₂ -5p |
| 8260 | O in UO ₂ -10p |
| 8297 | O in UO ₂ -100P |
| 8298 | O in UO ₂ -HALEU |
| 8299 | O in UO ₂ -HEU |
| 8305 | U in UN-5p |
| 8310 | U in UN-10p |
| 8347 | U in UN-100P |
| 8348 | U in UN-HALEU |
| 8349 | U in UN-HEU |
| 8355 | N in UN-5p |
| 8360 | N in UN-10p |
| 8397 | N in UN-100P |
| 8398 | N in UN-HALEU |
| 8399 | N in UN-HEU |
| 8540 | H in UH ₃ |

| Filters/Structural | |
|--------------------|--------------------------------------|
| 112 | Mg (metal) |
| 53 | Al (metal) |
| 56 | Fe (metal) |
| 59 | Si |
| 49 | beta-phase SiO ₂ |
| 3016 | Si in SiO ₂ -alpha |
| 3017 | O in SiO ₂ -alpha |
| 43 | Si in SiC |
| 44 | C in SiC |
| 1051 | C in CF ₂ |
| 1052 | F in CF ₂ |
| 3048 | H in HF |
| 3047 | F in HF |
| 1001 | Zr in ZrC |
| 1002 | C in ZrC |
| 3052 | Al in Al ₂ O ₃ |
| 3053 | O in Al ₂ O ₃ |

| FLiBe | |
|-------|-------------|
| 4001 | F in FLiBe |
| 4002 | Be in FLiBe |
| 4003 | Li in FLiBe |

Summary of HALEU ARDP Characteristics

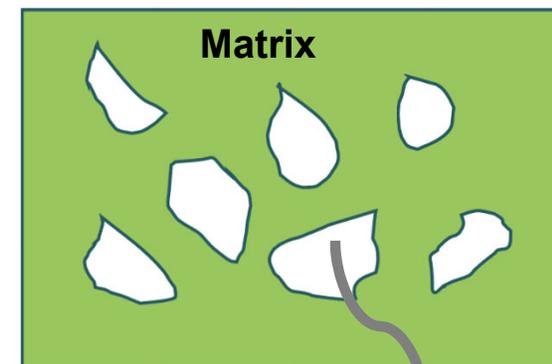
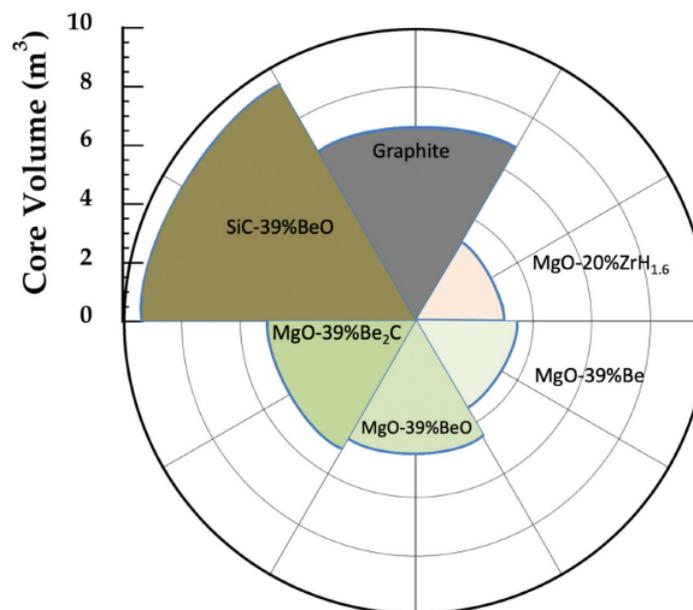
| Lead | Reactor Name | Reactor Type | Neutron Spectrum | Fuel Type | Power | Enrichment (wt% ²³⁵ U) | Moderator | Reflector | Coolant |
|---------------------------------|--------------|------------------------|------------------|--|----------|-----------------------------------|---------------------------|--|-------------------|
| TerraPower | Natrium | SFR | Fast | Sodium-bonded Metallic Alloy U-10Zr Pins | 345 MWe | 19.75 | N/A | — | Salt |
| X-energy | Xe-100 | Pebble Bed HTGR | Thermal | UCO TRISO Spherical Compacts | 80 MWe | 15.5 | Graphite | Graphite | Helium |
| Kairos Power | KP-FHR | Pebble Bed FHR | Thermal | UCO TRISO Annular Spherical Compacts with Low-Density Graphite Cores | 140 Mwe | 19.55 | Pyrolytic Graphite, FLiBe | Graphite | FLiBe |
| Westinghouse Nuclear | eVinci | Heat-pipe Microreactor | Thermal | UCO TRISO Cylindrical Compacts | 5 Mwe | 19.75 | Graphite | — | Sodium Heat Pipes |
| Southern Company and TerraPower | MCFR | MSR | Fast | Dissolved Uranium in Salt (NaCl-UCl ₃) | 800 MWe | HALEU | N/A | — | Salt |
| BWXT | BANR | HTGR | Thermal | UN TRISO in SiC, Carbon Matrix Compact, Additively Manufactured | 50 MWth | 19.75 (Baseline Design) | Graphite | — | Helium |
| ARC | ARC-100 | SFR | Fast | Sodium-bonded U-10Zr pins | 100 MWe | 20 Max.; 13.1 Avg. | N/A | Stainless Steel | Sodium |
| GA-EMS | FMR | GFR | Fast | UO ₂ Pellets | 44 MWe | 19.75 | N/A | Zr ₃ Si ₂ and Graphite | Helium |
| MIT | HC-HTGR | HTGR | Thermal | TRISO Compact | ~58 MWth | — | Graphite | — | Helium |

Neutron Moderation

- Typical core moderator and reflector materials consist of relatively simple compounds of a simple material type or simple composition (e.g, H_2O , D_2O , Be, BeO, Graphite, ZrH_2).
- Recently, compact thermal fission reactors are of increased interest due to their potential lower and controlled construction cost, enhanced safety, and portability to remote areas.
- They are also considered as a point-source for process industrial heat
- The compact nature of these cores requires good neutron economy

Example: Two Phase Composite Moderator

| | Entrained Phase | Matrix Phase |
|-----------------------|--|--------------|
| Scattering | High | Fair |
| Absorption | Low | Low |
| Thermal Conductivity | Fair | High |
| Radiation resistivity | Fair | Good |
| Mechanical Stability | Fair | Good |
| Examples | Graphite, Be, Be_4^{11}B , BeO, Be_2C , YH_{2-x} , ZrH_{2-x} | MgO, SiC |



Entrained Phase

Entrained Phase refers to a phase or component of a mixture that is carried along or transported by another medium or phase.

MgO-based composite moderators can exhibit considerably smaller critical volumes when compared to nuclear graphite

Be_2C : reacts with moisture to form $\text{Be}(\text{OH})_2$. However, as an entrained phase it will not

YH_{2-x} , ZrH_{2-x} : High dense matrix forms barriers that prevents hydrogen leakage

Neutron Moderators Status

| Material | Available TSL ENDF Files | Differential Measurement | Integral Measurements | Benchmark* Experiments. |
|---------------------------------------|--------------------------|--------------------------|-----------------------|-------------------------|
| Graphite | Yes | Yes | Yes | Yes |
| ZrH _{1.6} & ZrH ₂ | Yes | Yes | Yes | Yes |
| YH ₂ | Yes | Yes | Yes | No |
| Be metal | Yes | Yes | Yes | No |
| BeO | Yes | No | Yes | No |
| MgO | No** | No | Yes | No |
| Be ₂ C | Yes | No | No | No |
| FLiBe | Yes | No | No | No |
| SiC | Yes | No | No | No |
| Zr ₃ Si ₂ | No | No | No | No |

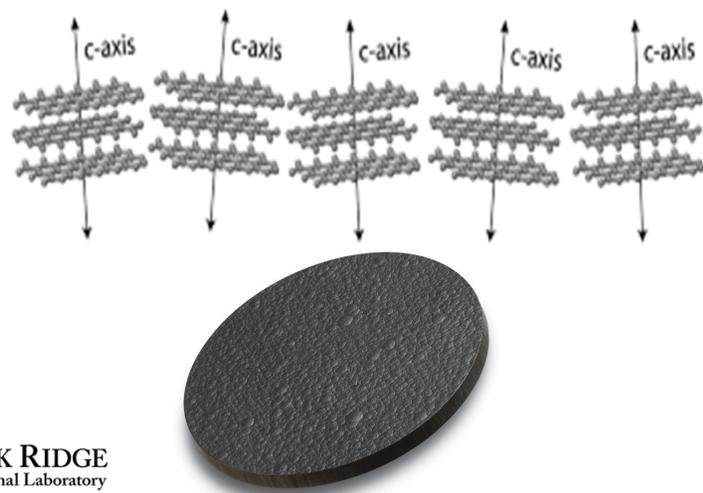
* These experiments involve fuel compositions ranging from 5 to 19.75 wt% enrichment with ²³⁵U and exhibit a neutron flux of < 0.625 eV

** The MgO TSL sub-library has been submitted to the Cross Section Evaluation Working Group (CSEWG) for approval and inclusion in the ENDF database; at this writing, approval is pending.

Current Status of Graphite TSL Sub-libraries

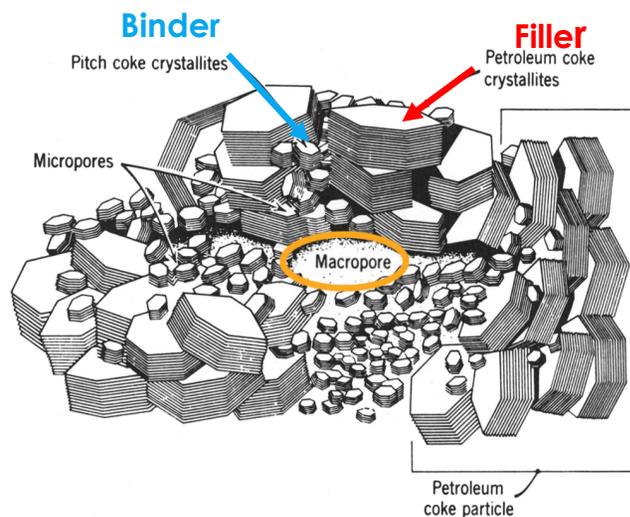
Graphite

- Crystalline Graphite
- Density $\sim 2.26 \text{ g/cm}^3$ (HOPG)
- Huge number of small nearly perfect **micro-crystallites** that have the same c-axis but with different orientations in x-y plane
- Very close to the Ideal, perfect or theoretical graphite.

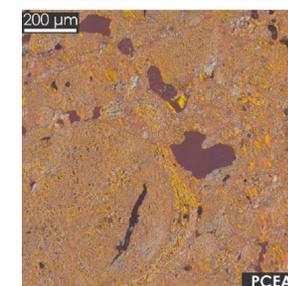
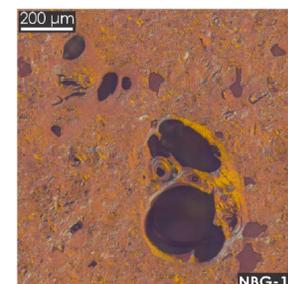


| | Graphite |
|-----|---------------------------------------|
| 30 | crystalline graphite |
| 301 | Graphite +sd |
| 31 | reactor-grade graphite (10% porosity) |
| 320 | reactor-grade graphite (20% porosity) |
| 32 | reactor-grade graphite (30% porosity) |

- Nuclear Graphite
- Density $(1.5\sim 1.90) \text{ g/cm}^3$
- Complex Microstructure- contains crystallite (filler and binder) & pores
- The size and shape of grains and pores vary from one graphite grade to another.



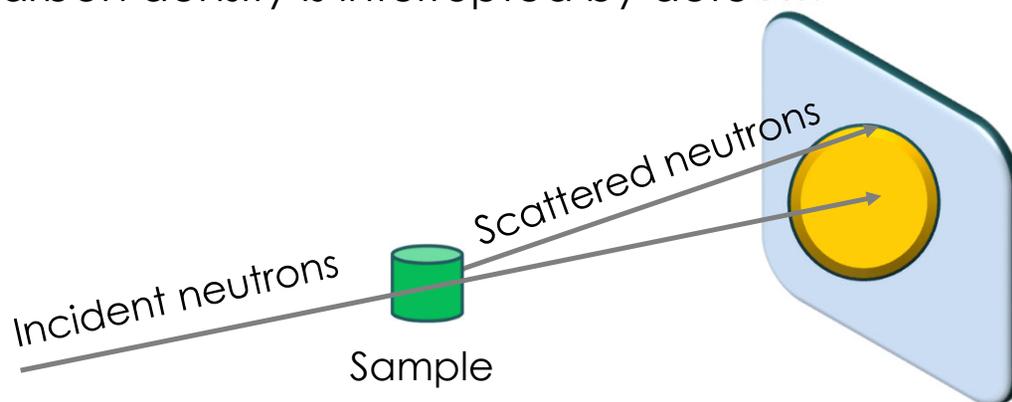
Contescu & Paul, ORNL/TM-2022/1839



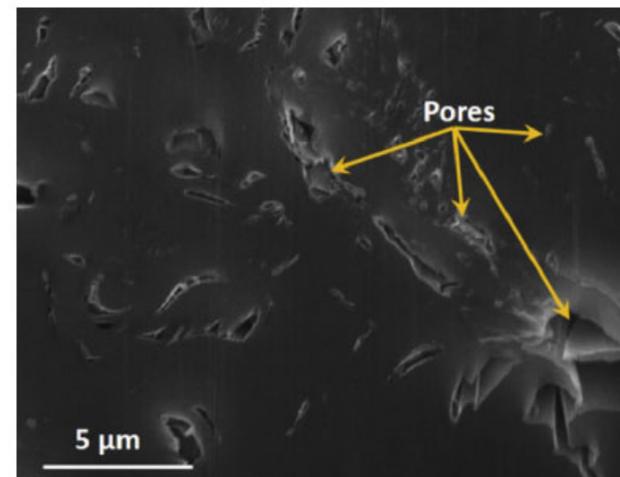
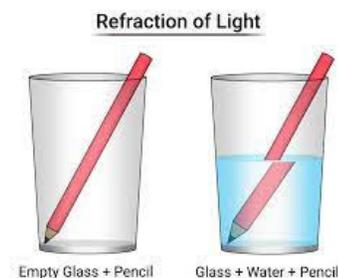
DNCSH WORKSHOP - I

Small Angle Neutron Scattering (SANS)

- SANS is an elastic scattering phenomenon where neutrons **diverges** from their incident beam by a small scattering angle (generally, $2\theta < 10$ deg), as it penetrates through a sample.
- In **nuclear graphite**, SANS occurs on cracks, voids, pores, etc., where the continuous distribution of carbon density is interrupted by defects.



Graphite: Inelastic + Elastic + SANS
Others : Inelastic + Elastic



Liu et al., *J. Nucl. Mater.* **493**, 246-54, (2017)

DNCSS WORKSHOP - 1

Thermal Scattering Law (TSL), $S(\alpha, \beta)$

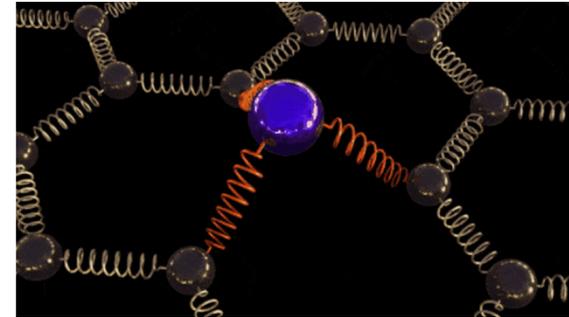
$$\frac{d^2\sigma}{dE' d\Omega} \cong \frac{\sigma_{coh} + \sigma_{incoh}}{4\pi k_B T} \sqrt{\frac{E'}{E}} e^{-\beta/2} \sum_{P=1}^P S_s(\alpha, \beta)$$

$$\Rightarrow S_s(\alpha, \beta) = \frac{1}{2\pi} \int_{-\infty}^{\infty} e^{i\beta\tau} e^{-\gamma^2(\tau)} d\tau$$

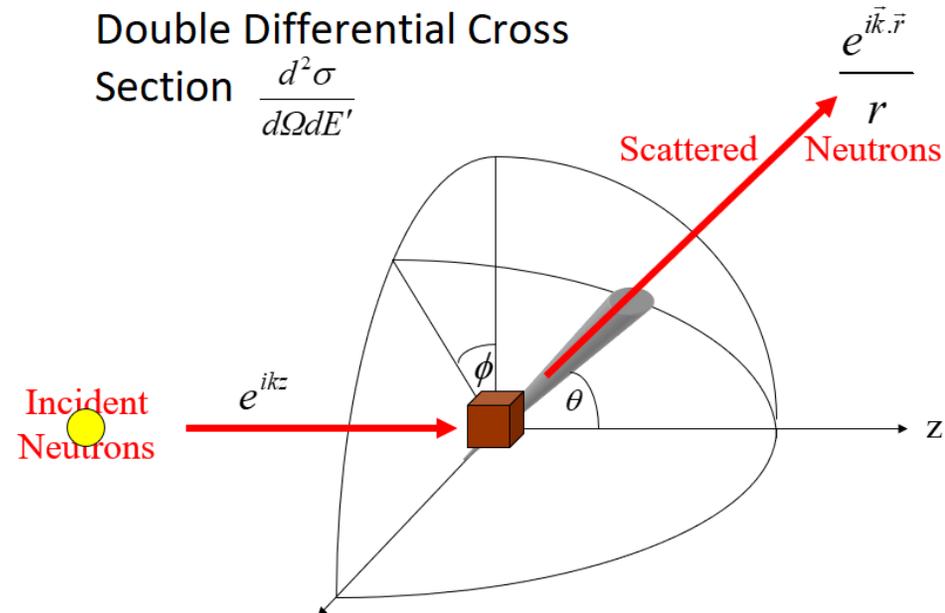
$$\gamma^2(\tau) = \alpha \int_{-\infty}^{\infty} \frac{\rho(\beta) [1 - e^{i\beta\tau}] e^{-\beta/2}}{2\beta \sinh(\beta/2)} d\beta$$

All we need to calculate the scattering law is the phonon density of states (PDOS), $\rho(\beta)$

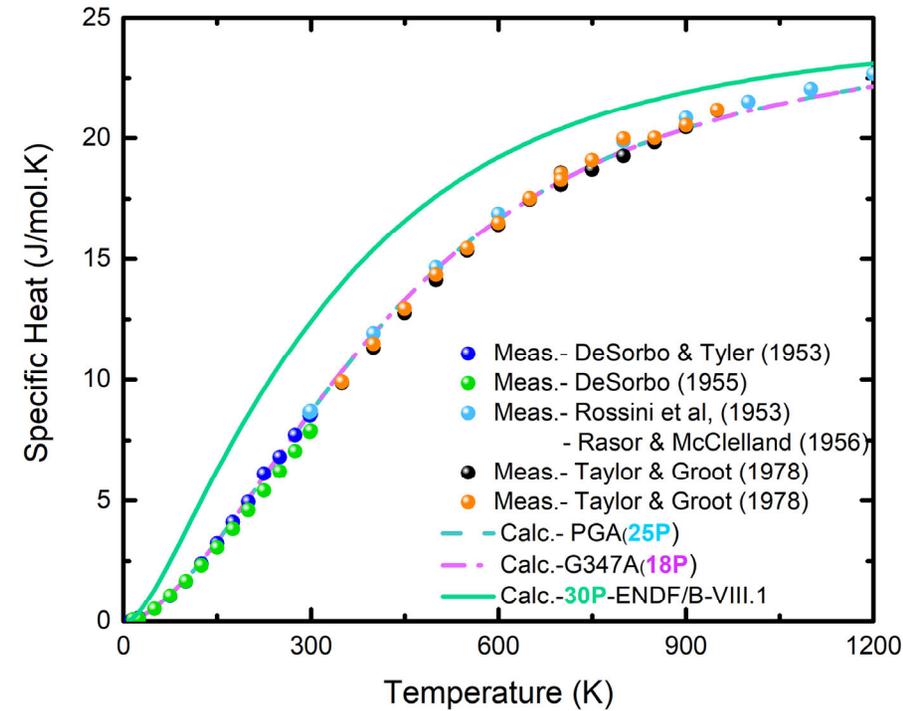
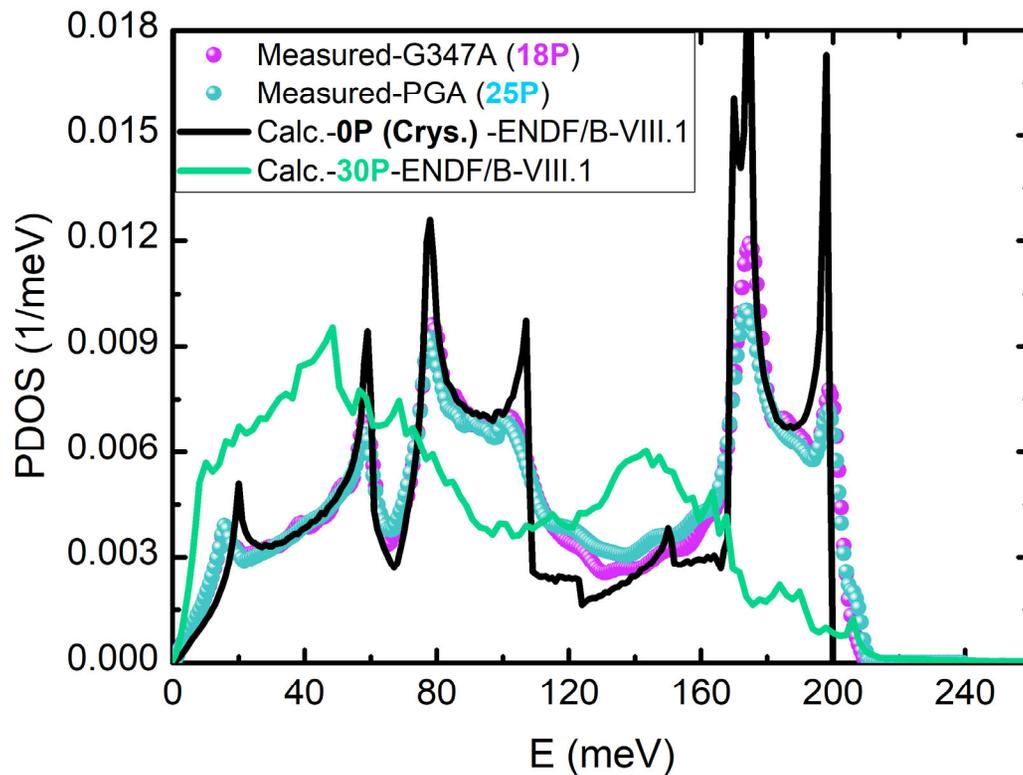
Energy Transfer
Momentum transfer



Double Differential Cross Section $\frac{d^2\sigma}{d\Omega dE'}$



ARCS Measurements of Phonon Density of States (PDOSs)



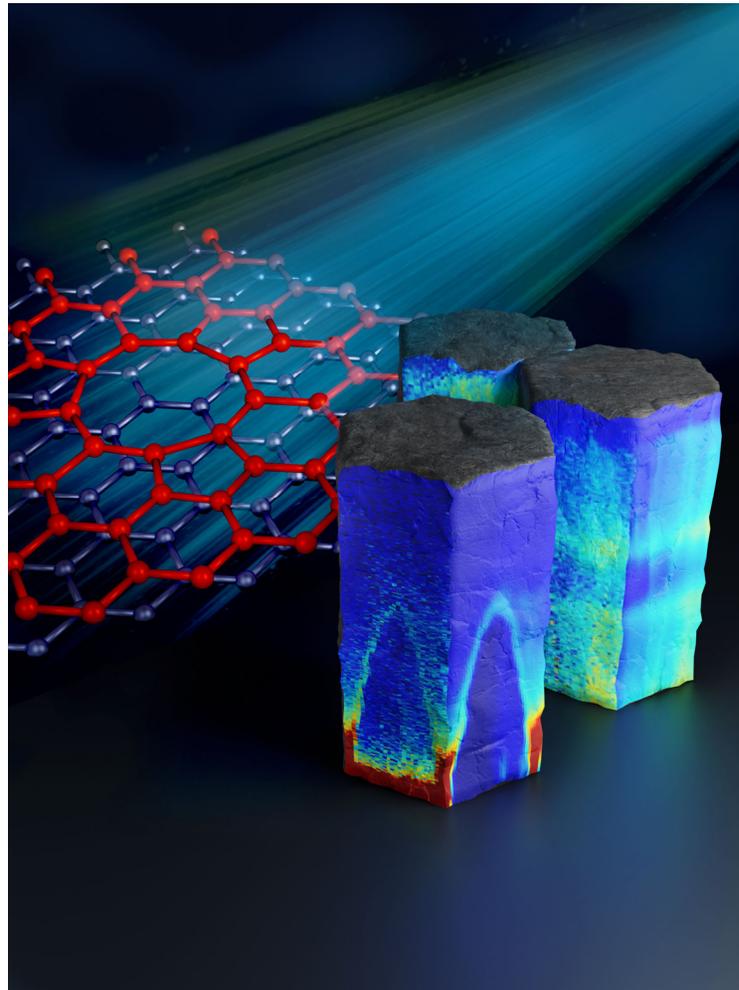
- ✓ Specific heat as well as $S(\alpha, \beta)$ are both functions of the PDOS, $\rho(\omega)$
- ✓ Different graphite grades, show similar measured PDOS & specific heat
- ✓ 30P-PDOS & Specific heat shows significant deviations from measured values

Conclusions

- Thermal moderators are not adequately covered across all necessary types of experiments
- High-fidelity nuclear graphite neutronics calculations require **inelastic+elastic+SANS** and pore size distribution
- A standardized approach for generating or preserving TSL 2D covariance data related does not exist—currently investigating relevance for criticality safety

| Material | Available TSL ENDF Files | Differential Measurement | Integral Measurements | Benchmark Experiments |
|---------------------------------------|--------------------------|--------------------------|-----------------------|-----------------------|
| Graphite | Yes | Yes | Yes | Yes |
| ZrH _{1.6} & ZrH ₂ | Yes | Yes | Yes | Yes |
| YH ₂ | Yes | Yes | Yes | No |
| Be metal | Yes | Yes | Yes | No |
| BeO | Yes | No | Yes | No |
| MgO | No | No | Yes | No |
| Be ₂ C | Yes | No | No | No |
| FLiBe | Yes | No | No | No |
| SiC | Yes | No | No | No |
| Zr ₃ Si ₂ | No | No | No | No |

Thank you



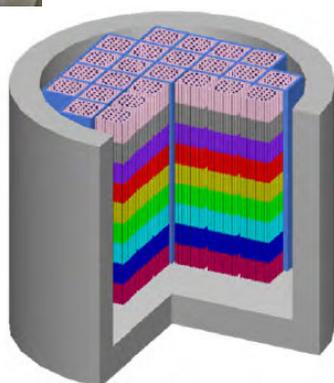
Review of Available Critical Experiment Benchmarks and Critical Experiment Facilities for HALEU Fuel Transport Validation

Mathieu Dupont

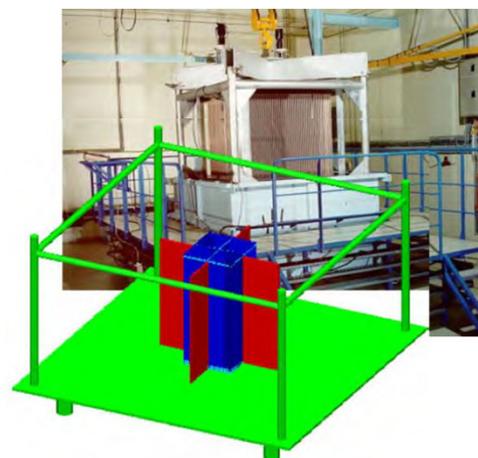


Introduction to HALEU fuel validation

- Computational validation [1]: determine the bias and bias uncertainty between calculations and observations
- Criticality safety: Compare k_{eff} values of critical experiment benchmarks and application models



Application



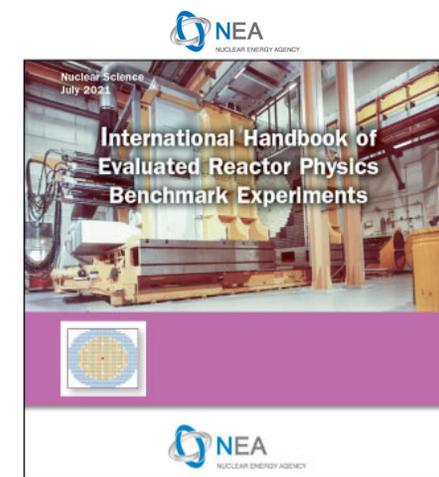
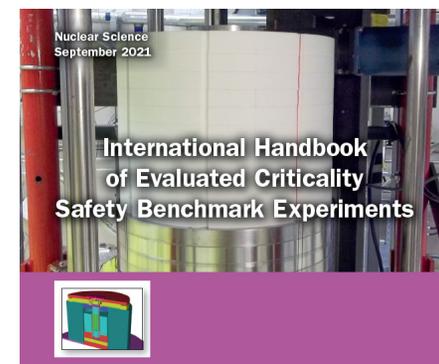
Critical Experiment

Introduction to HALEU fuel validation

- What we need: Critical experiment benchmark as similar as possible to the application to be validated
 - Fuel enrichment: HALEU 5-20 wt% ^{235}U , most advanced reactors are close to 20 wt% ^{235}U
 - Moderator/reflector material: graphite, FLiBe
 - Neutron energy spectrum: thermal and fast
 - Structural materials: wide range
 - Fuel form: Uranium compacts, TRISO particle-like, fuel salt, metal
- What do we have?

Review of available critical experiments for HALEU validation

- Two best sources from Nuclear Energy Agency (NEA):
 - International Criticality Safety Benchmark Evaluation Project (ICSBEP) [2]: wide range of critical experiments, focus on the light water reactor validation
 - International Reactor Physics Benchmark Evaluation Project (IRPhEP) [3]: focus on reactor physics experiments, some critical configurations available
- The handbooks provide thousands of benchmark experiments from dozens of countries with an assessment of data integrity, quantification of experimental uncertainties, and thorough technical review with established deployment process



Review of available critical experiments for HALEU validation

- Experiments potentially relevant for HALEU validation from the handbooks
- Experiments quality and correlation
- Upcoming experiments
- Conclusions and recommendations

Review of available critical experiments for HALEU validation

- **Experiments potentially relevant for HALEU validation from the handbooks**
- Experiments quality and correlation
- Upcoming experiments
- Conclusions and recommendations

Review of available critical experiments for HALEU validation

In ICSBEP handbook:

| Characteristic of Interest for HALEU Fuel Validation | Number of Evaluations | Number of Experiments |
|--|-----------------------|-----------------------|
| ^{235}U enrichment 5 to 21 wt% | 74 | 431 |
| ^{235}U enrichment 5 to 9 wt% | 26 | 247 |
| ^{235}U enrichment 9 to 21 wt% | 48 | 184 |
| ^{235}U enrichment 18 to 21 wt% | 13 | 36 |
| ^{235}U enrichment 9 to 21 wt% and uranium metal | 13 | 29 |
| ^{235}U enrichment 9 to 21 wt% and UF_4 | 2 | 6 |
| ^{235}U enrichment 9 to 21 wt% and UO_2 in TRISO particles | 1 | 5 |
| UF_4 - UF_6 any enrichment | 10 | 110 |
| Uranium metal of any enrichment | 195 | 799 |
| Uranium salts any enrichment | 0 | 0 |

Review of available critical experiments for HALEU validation

In IRPhE handbook:

| Characteristic of interest for HALEU Fuel Validation | Number of evaluations | Number of Experiments |
|--|-----------------------|-----------------------|
| Potentially relevant to HALEU fuel forms | 15 | 54 |
| Uranium salt any enrichment | 1 | 1 |
| UO ₂ in TRISO and BISO particles | 7 | 27 |
| ²³⁵ U enrichment 18 to 21 wt% and uranium metal or graphite moderator | 4 | 7 |

Review of available critical experiments for HALEU validation

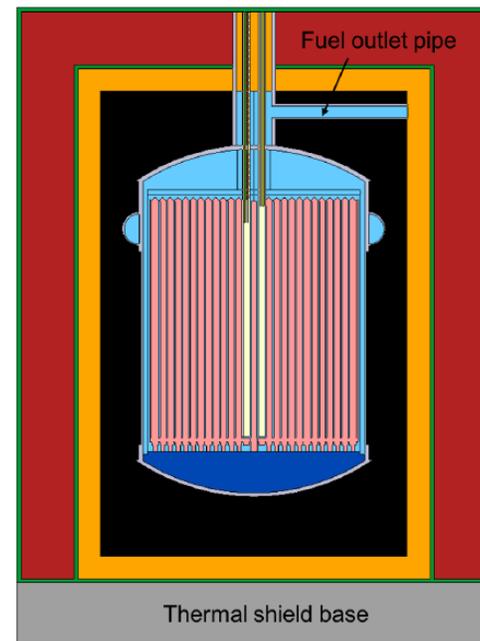
- Experiments potentially relevant for HALEU validation from the handbooks
- **Experiments quality and correlation**
- Upcoming experiments
- Conclusions and recommendations

Review of available critical experiments for HALEU validation

- Good validation suite:
 - As high as possible number of applicable critical experiments
 - As low as possible experimental uncertainty
 - As high as possible variety of experimental facilities to reduce experimental correlations [4]
- What is the current status on quality and correlation of HALEU validation critical experiments?

Review of available critical experiments for HALEU validation

- Experimental uncertainty:
 - ICSBEP: Mostly good, some outliers IEU-COMP-THERM-009-001 with an experimental uncertainty of 600 pcm and IEU-COMP-MIXED-002-008 with a Calculated/Expected ratio of 1.044
 - IRPhEP: Mostly high uncertainty, for example Molten Salt Reactor Experiment (MSRE) has an experimental uncertainty of 420 pcm on k_{eff} and a k_{eff} C/E ratio of 1.0215: known deficiencies exist



MSRE benchmark model core [5]

Review of available critical experiments for HALEU validation

- Additional review of the quality of critical experiments may be needed, such efforts already exist:
 - ORNL Verified, Archived Library of Inputs and Data (VALID) [6]: peer-reviewed criticality benchmarks sensitivity data files
 - WPNCS subgroup 8 (SG-8) [7]; “Preservation of Expert Knowledge and Judgement Applied to Criticality Benchmarks”



VALID [8]

Initial Efforts Organizing WPNCS SG-8: Preservation of Expert Knowledge and Judgement Applied to Criticality Benchmarks

William Wieselquist,¹ John D. Bess,² Douglas Bowen,¹ Isabelle Duhamel,³ Ian Hill,⁴ Nicolas Leclaire,³ William B. J. Marshall,¹ Catherine Percher,⁵ Ellen Marie Saylor,¹ Shuichi Tsuda⁴

¹Oak Ridge National Laboratory (ORNL), Oak Ridge, TN, USA, wieselquiswa@ornl.gov

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⁴OECD Nuclear Energy Agency (NEA), Boulogne-Billancourt, France

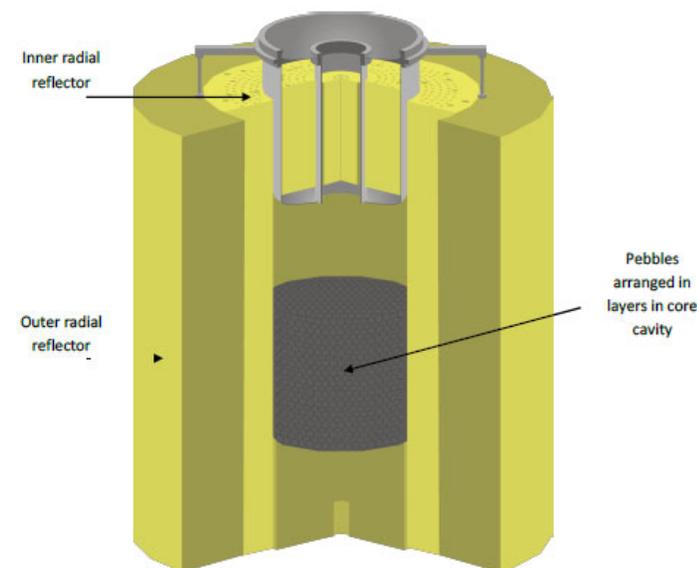
⁵Lawrence Livermore National Laboratory (LLNL), Livermore, CA, USA

<https://dx.doi.org/10.13182/T123-32977>

WPNCSSG-8 [7]

Review of available critical experiments for HALEU validation

- Experimental correlations:
 - From both ICSBEP and IRPhEP handbooks, 616 experiments in 104 evaluations were identified
 - Many come from the same facilities: experimental correlations exist
 - Example: PROTEUS-GCR



**Generic
HTR-PROTEUS configuration [9]**

Review of available critical experiments for HALEU validation

- Experimental correlations:
 - 11 PROTEUS-GCR experiments from 4 evaluations come from the same PROTEUS facility operated at the Paul Scherrer Institute (PSI) in Switzerland
 - All have around 300–400 pcm experimental uncertainty, from the same ^{235}U isotopic content, resulting in 250–300 pcm keff
 - Correlation within and between the evaluations, so the resulting computational bias for all the experiments and evaluations from the same facility will be similar

- **Critical experiments from different facilities are recommended**

Review of available critical experiments for HALEU validation

- Experiments potentially relevant for HALEU validation from the handbooks
- Experiments quality and correlation
- **Upcoming experiments**
- Conclusions and recommendations

Upcoming experiments potentially relevant for HALEU validation [10]

| Experiment | Characteristic of Interest for HALEU Fuel Validation | Facility/ Organization / country | Status | Potential issues |
|---|---|---|---------------------------------------|--|
| AGN-201M Reactor Benchmark [11] | 19.5 wt% microspheres coated with graphite | University of New Mexico, USA | Expected benchmark completion in 2025 | Lack of characterization of the fuel plates |
| IPEN/MB01 reactor conversion to 19.75 wt% metallic plates fuel [12] | 19.75 wt% U_3Si_2 -Al metal fuel | IPEN, Brazil | Experiments ongoing | Evaluation plans not officially announced |
| The Deimos Experiment [13] | 19.9 wt% TRISO particles in cylindrical graphite compacts | Los Alamos National Laboratory/NCERC, USA | Experiments ongoing | Evaluation plans not officially announced |
| MARVEL Reactor [14] | 19.75 wt% TRIGA uranium zirconium hydride metal fuel | Idaho National Laboratory, USA | Under construction | Goal is to demonstrate microreactor technologies, not critical benchmark |
| ROSE Critical Facility [15] | 21 wt% UO_2 rods | Joint Institute for Power and Nuclear Research, Belarus | Experiments performed and evaluated | Evaluation not in ICSBEP format |

Review of available critical experiments for HALEU validation

- Experiments potentially relevant for HALEU validation from the handbooks
- Experiments quality and correlation
- Upcoming experiments
- **Conclusions and recommendations**

Conclusions and recommendations

1. High number of critical experiments are available in the HALEU fuel enrichment range
2. High number of critical experiments are available in the thermal, intermediate and fast neutron spectra
3. A low number of experiments with TRISO particle-based fuels or similar, with questionable uncertainty, and only one experiment in development (DEIMOS)
4. Only one Uranium salt critical experiment benchmark is available, with very high uncertainty and C/E ratio (MSRE), and the only one in development not planned to be a benchmark (MCRE [16])
5. No critical experiments with depleted HALEU fuel exist for the back-end validation
6. Experimental correlations could be reduced by performing experiments in new facilities
7. Quality of evaluations can be ensured (low uncertainty) by performing experiments in already trusted facilities with potential new equipment

Review of available critical experiments facilities for HALEU validation

- Where to perform new critical experiments?
 - Established critical experiment facilities
 - University research reactors
 - Other facilities

Lists are non-exhaustive, from analysis of the handbooks and recent NEA efforts [17] [18]

Review of available critical experiments facilities for HALEU validation

Most promising facilities:

| Facility, Organization | Location, Status | Advantages | Disadvantages |
|--|-----------------------------|--|---|
| NCERC, Los Alamos National Laboratory [19] | USA, Operational | TRISO experiment ongoing, broad staff experience designing critical experiments and ICSBEP/IRPhE evaluation | Hazard category 2 facility, no water allowed, time and money consuming, low availability |
| SPRF/CX, Sandia National Laboratories [20] | USA, Operational | Room to install new critical machines, broad staff experience designing critical experiments and ICSBEP/IRPhE evaluation, existing fuel rods enriched around 7% | Facility in air force base, no critical experiment machine for new HALEU fuel, low availability |
| ZED-2, Chalk River, Canadian Nuclear Laboratories [21] | Canada, Operational | HALEU fuel research ongoing, staff experience designing critical experiments and ICSBEP/IRPhE evaluation, announced facility availability for international collaborations | Procure HALEU fuel could be a challenge |
| New STACY, Japan Atomic Energy Agency [22] | Japan, Operational Mid 2024 | Staff experience designing critical experiments and ICSBEP/IRPhE evaluation, announced facility availability for international collaborations | Not yet operational, so delays could occur |
| IPEN/MB01, Instituto de Pesquisas Energéticas e Nucleares [23] | Brazil, Operational | Broad staff experience designing critical experiments and ICSBEP/IRPhE evaluation, new core with metallic rods within HALEU enrichment range | No communicated plans for international collaboration |

Review of available critical experiments facilities for HALEU validation

University-led facilities:

| Facility, Organization | Location, Status | Advantages | Disadvantages |
|---|---------------------------------|---|---|
| Reactor Critical Facility, Rensselaer Polytechnic Institute [24] | USA, Operational | Flexible reactor, critical experiments experience | No experiments are in a ICSBEP or IRPhE evaluation |
| Illinois Microreactor Demonstration Project, University of Illinois Urbana [25] | USA, Licensing stage, not built | Use of TRISO-like fuel | Not built yet, no flexibility once built, potentially not suitable for benchmarking |
| Molten Salt Nuclear Reactor Research, Abilene Christian University [26] | USA, Licensing stage, not built | Use of Uranium salt fuel | Not built yet, no flexibility once built, potentially not suitable for benchmarking |
| Missouri S&T Reactor, Missouri University of Science and Technology [27] | USA, Operational | Use of 19.75 wt% Uranium silicide fuel | No critical benchmarking experience |
| Kyoto University Critical Assembly, Kyoto University [28] | Japan, Core upgrade in progress | Modern upgrade | Not built yet, potential loss of flexibility and capabilities once built |

Review of available critical experiments facilities for HALEU validation

- Other notable facilities:

- VENUS [29], operated by SCL CEN at Mol, Belgium
- LR-0 [30], operated by the Nuclear Research Institute Řež plc at Husinec, Czech Republic
- RSV Tapiro [31], operated by the Italian National Agency for New Technologies, Energy and Sustainable Economic Development (ENEA), located in Rome, Italy
- CROCUS [32], operated by Polytechnique Federale (EPFL) in Lausanne, Switzerland
- UTR [28], located at the Kindai University in Japan
- DOME and LOTUS testbeds [33], located at Idaho National Laboratory (MCRE), USA
- Nextgen MURR [34], operated by University of Missouri, USA
- Other university research reactors such as TRIGA reactors

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Questions ?

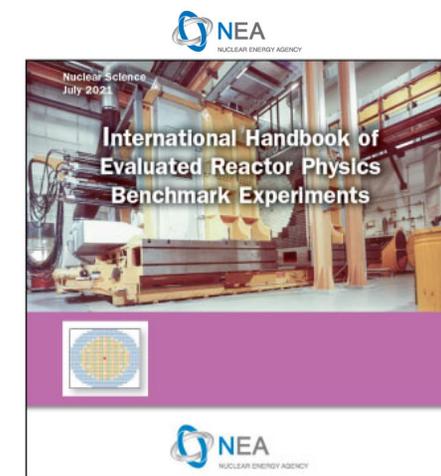
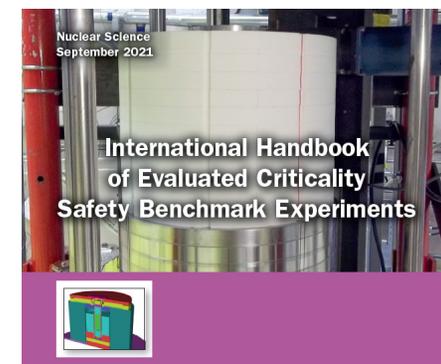
Review of available critical experiments for HALEU validation

- Comments on ICSBEP and IRPhE handbooks available critical experiments:
 - High number of critical experiments in the HALEU fuel enrichment range, neutron spectrum
 - Only one evaluation and 5 cases with TRISO fuel at 20.91 wt% ^{235}U (IEU-COMP-THERM-008)
 - No Uranium salts experiments in ICSBEP handbook, only one in IRPhE handbook
 - More critical experiments related to advanced reactors in IRPhE handbook, but potentially more uncertainty because criticality is not the main focus

Review of available critical experiments for HALEU validation

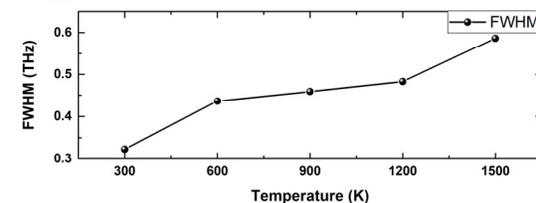
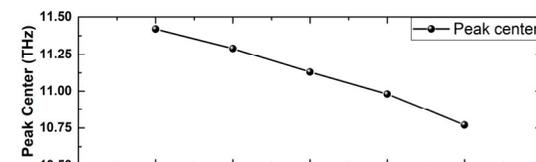
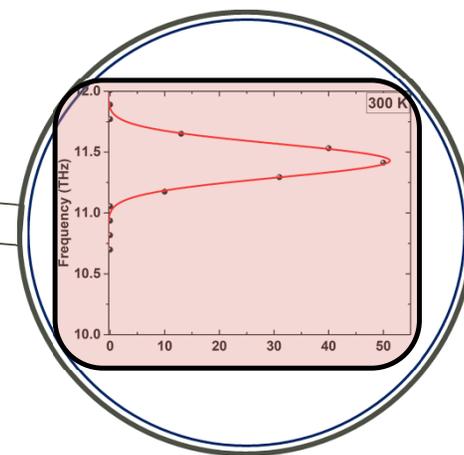
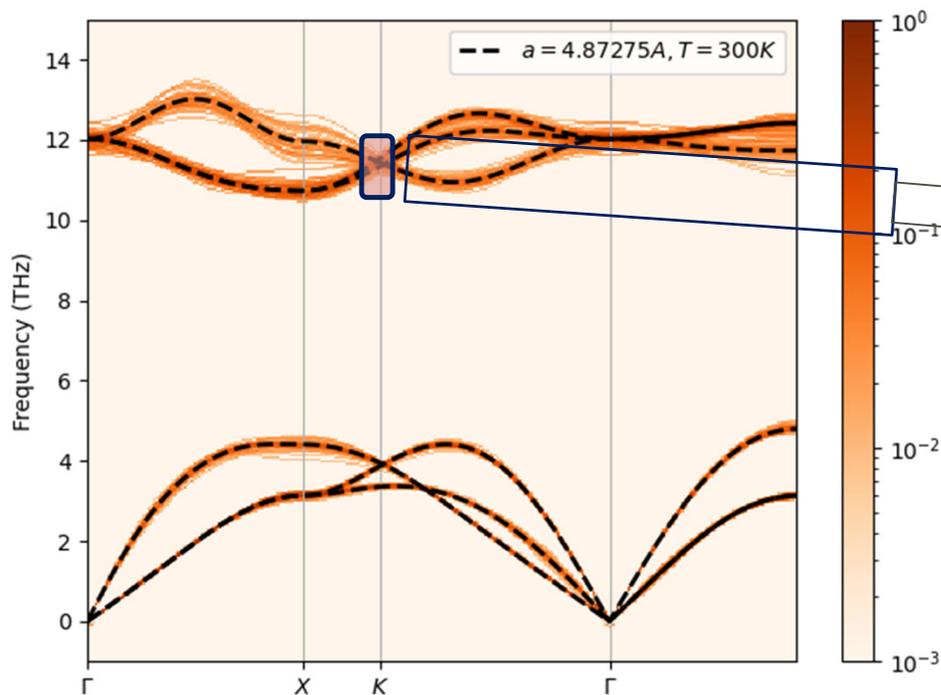
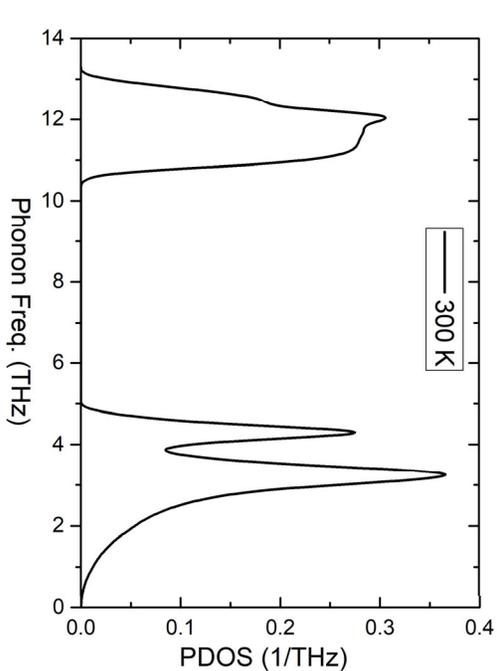
- ICSBEP Handbook 2021:
 - 26 contributing countries
 - Over 80,000 pages
 - More than 5000 approved benchmarks

- IRPhE Handbook 2021:
 - 25 contributing countries
 - 57 reactor facilities
 - 165 approved benchmarks



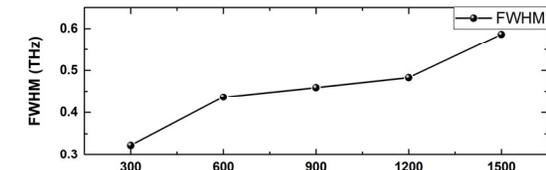
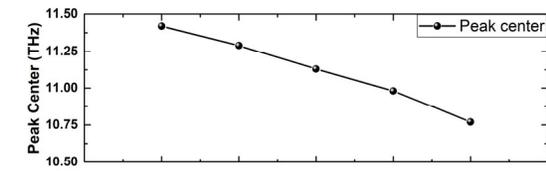
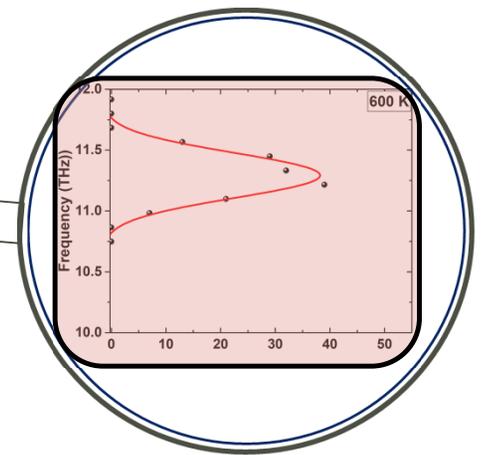
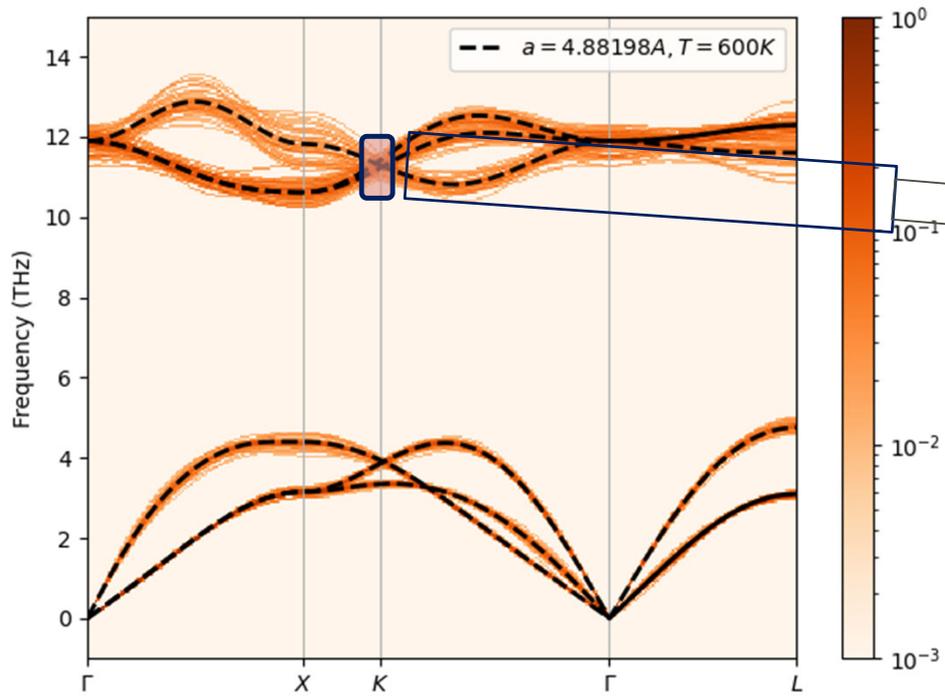
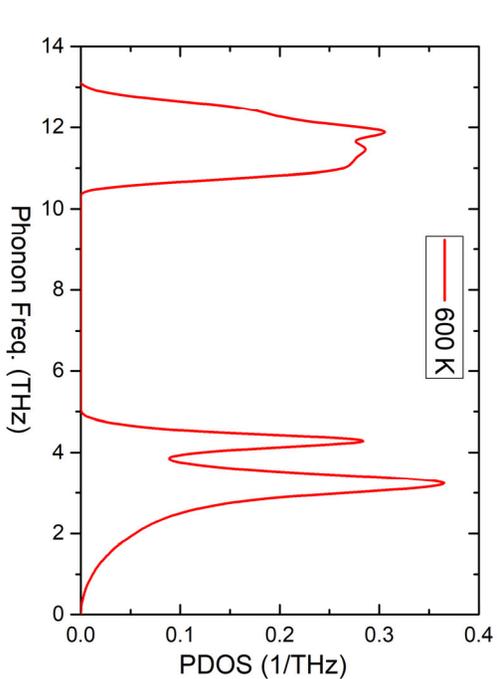
Phonon Calculations at High Temperatures

T = 300 K



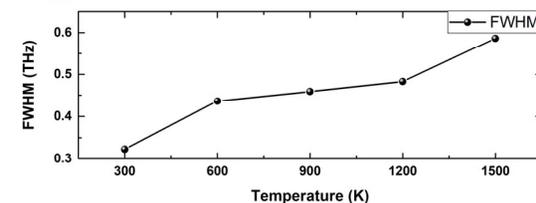
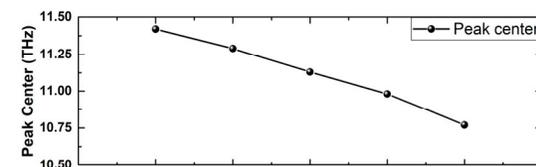
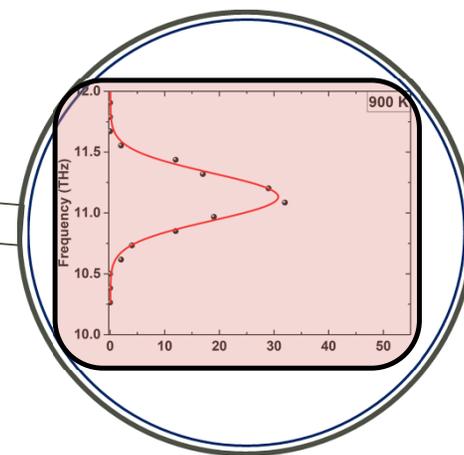
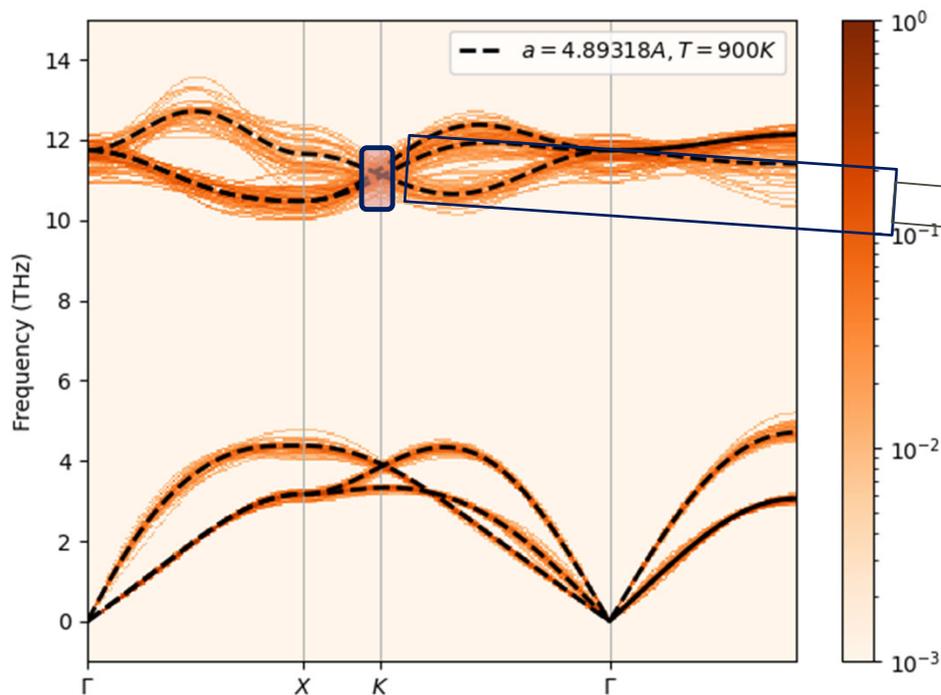
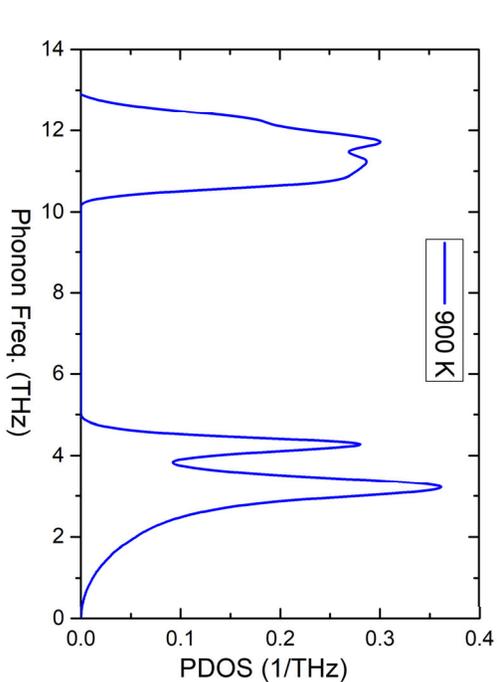
Phonon Calculations at High Temperatures

T = 600 K

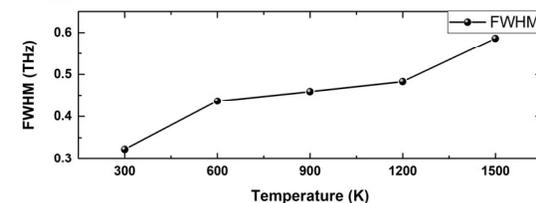
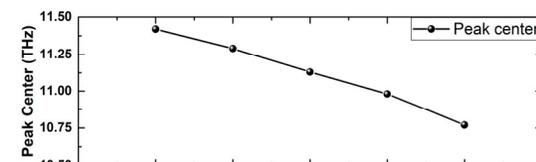
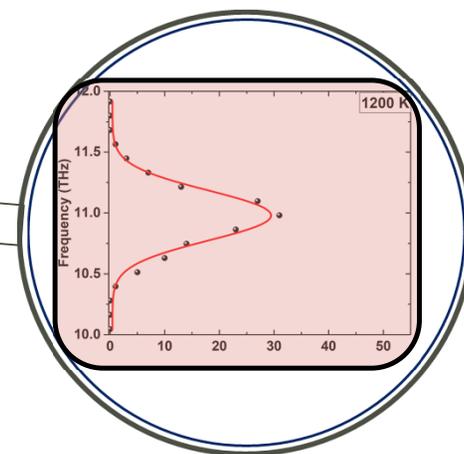
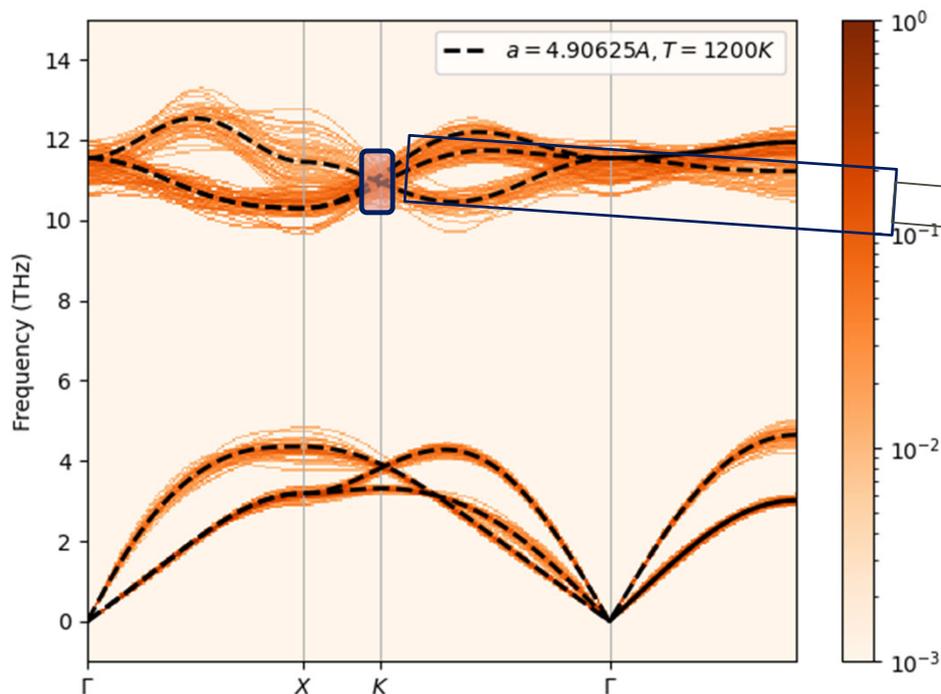
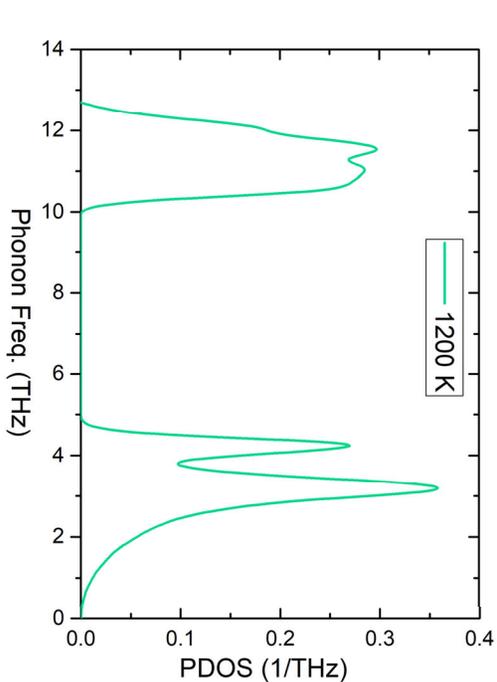


Phonon Calculations at High Temperatures

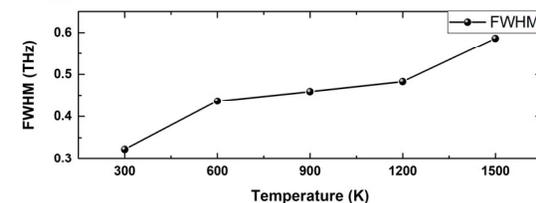
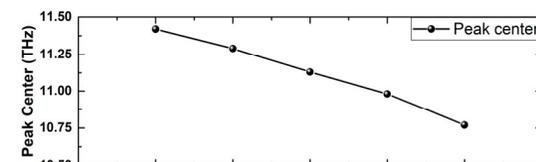
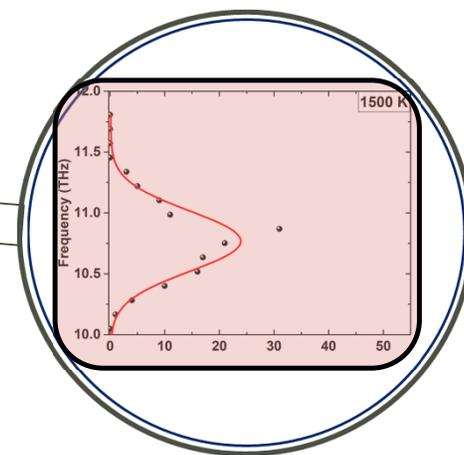
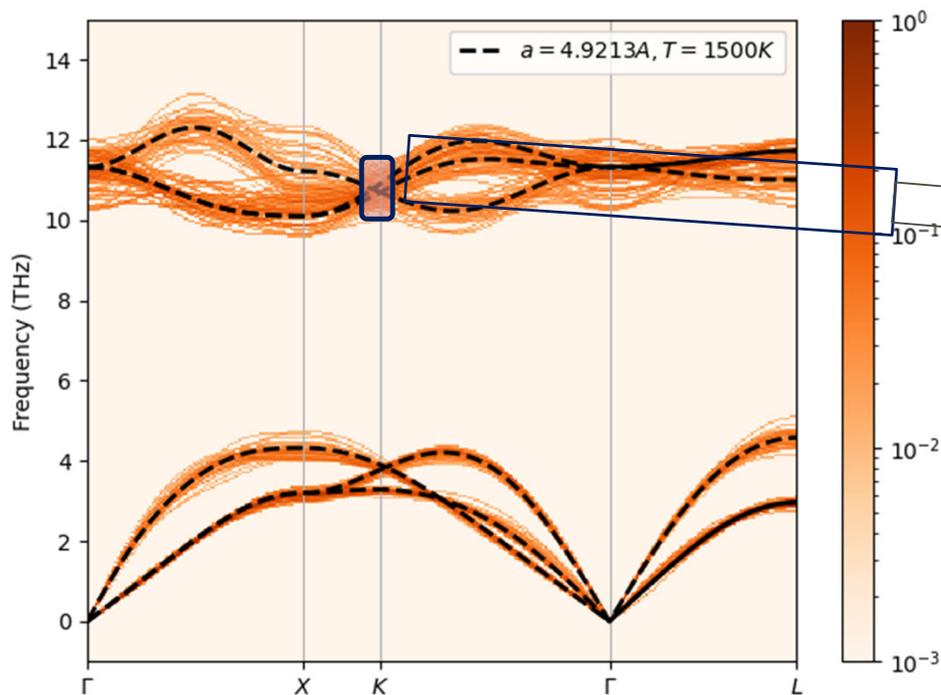
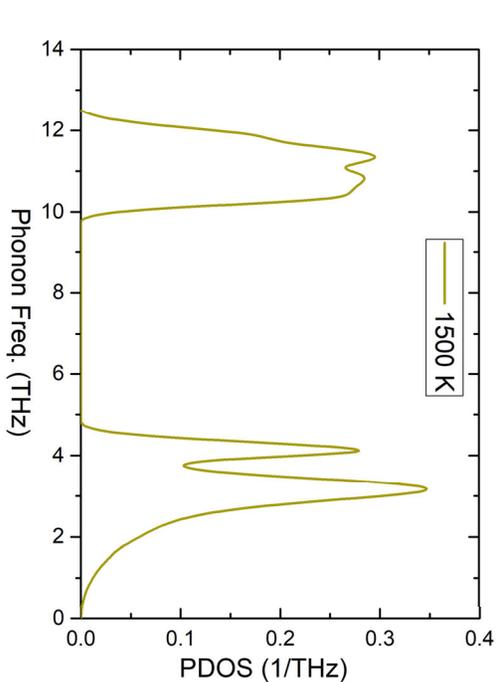
T = 900 K



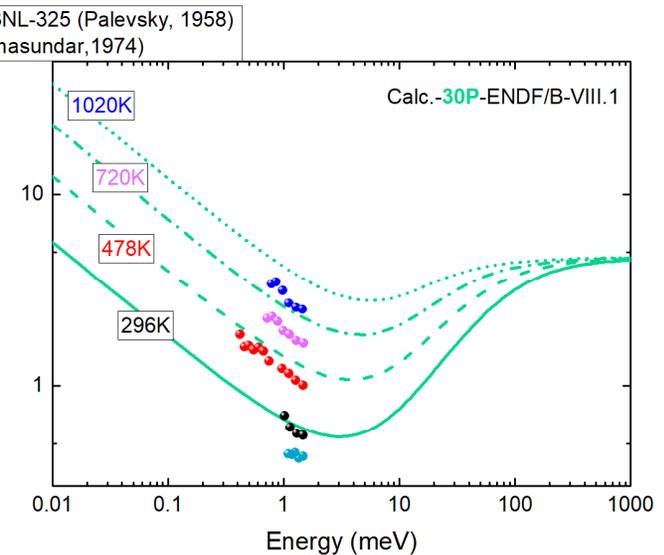
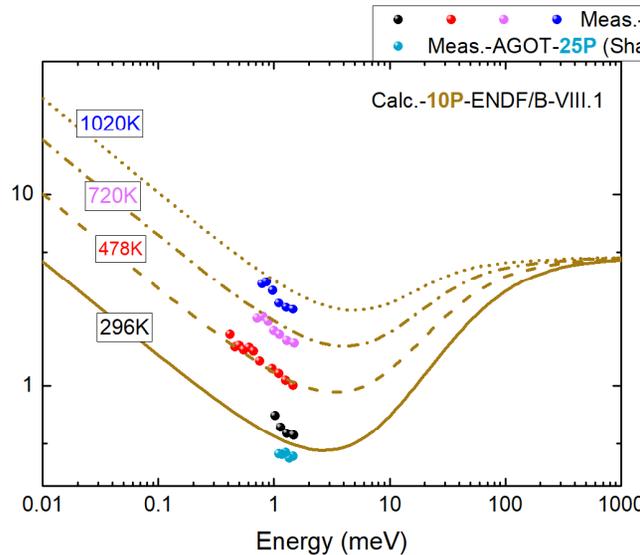
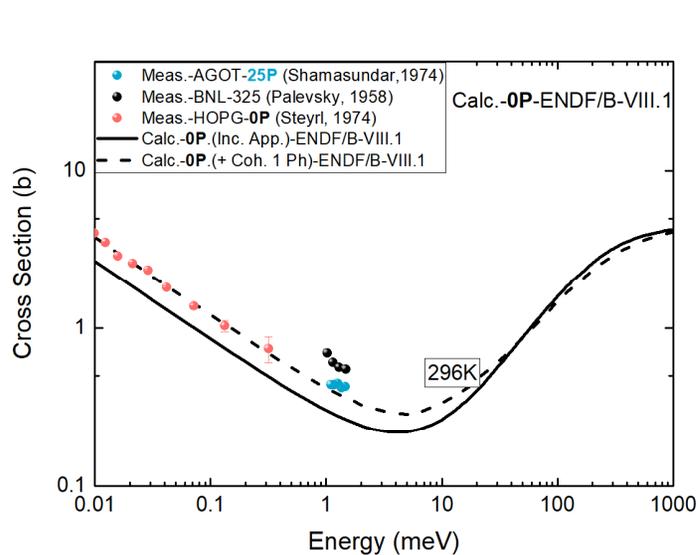
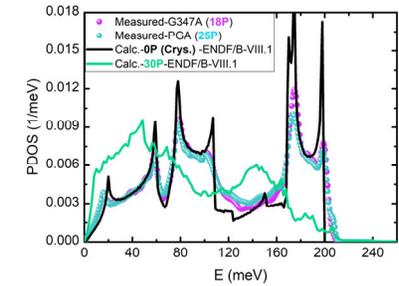
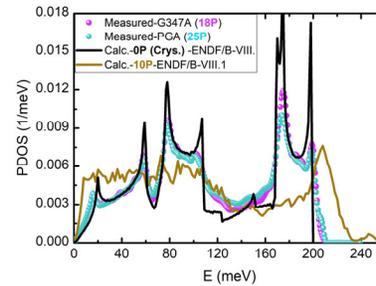
Phonon Calculations at High Temperatures $T = 1200 \text{ K}$



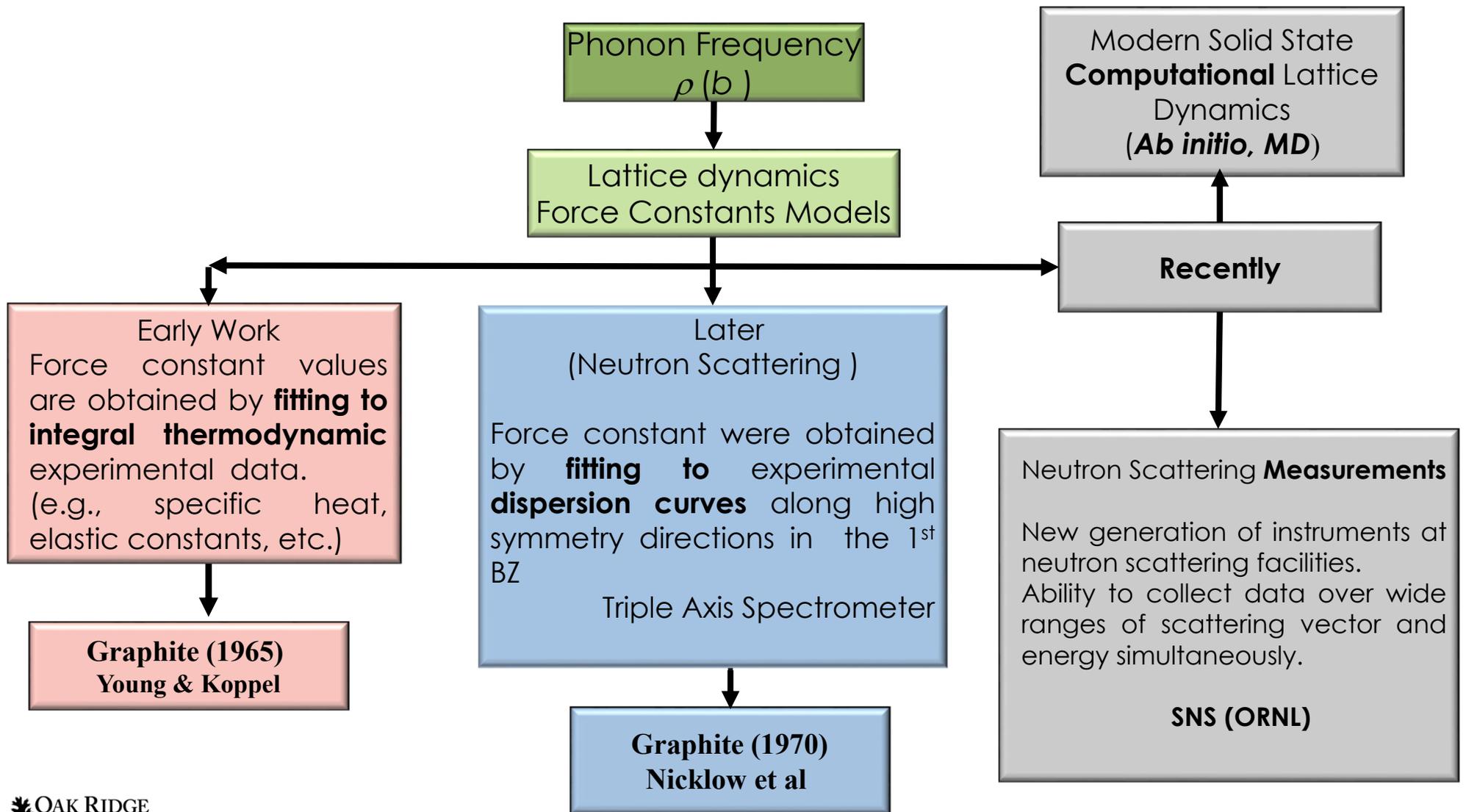
Phonon Calculations at High Temperatures $T = 1500 \text{ K}$



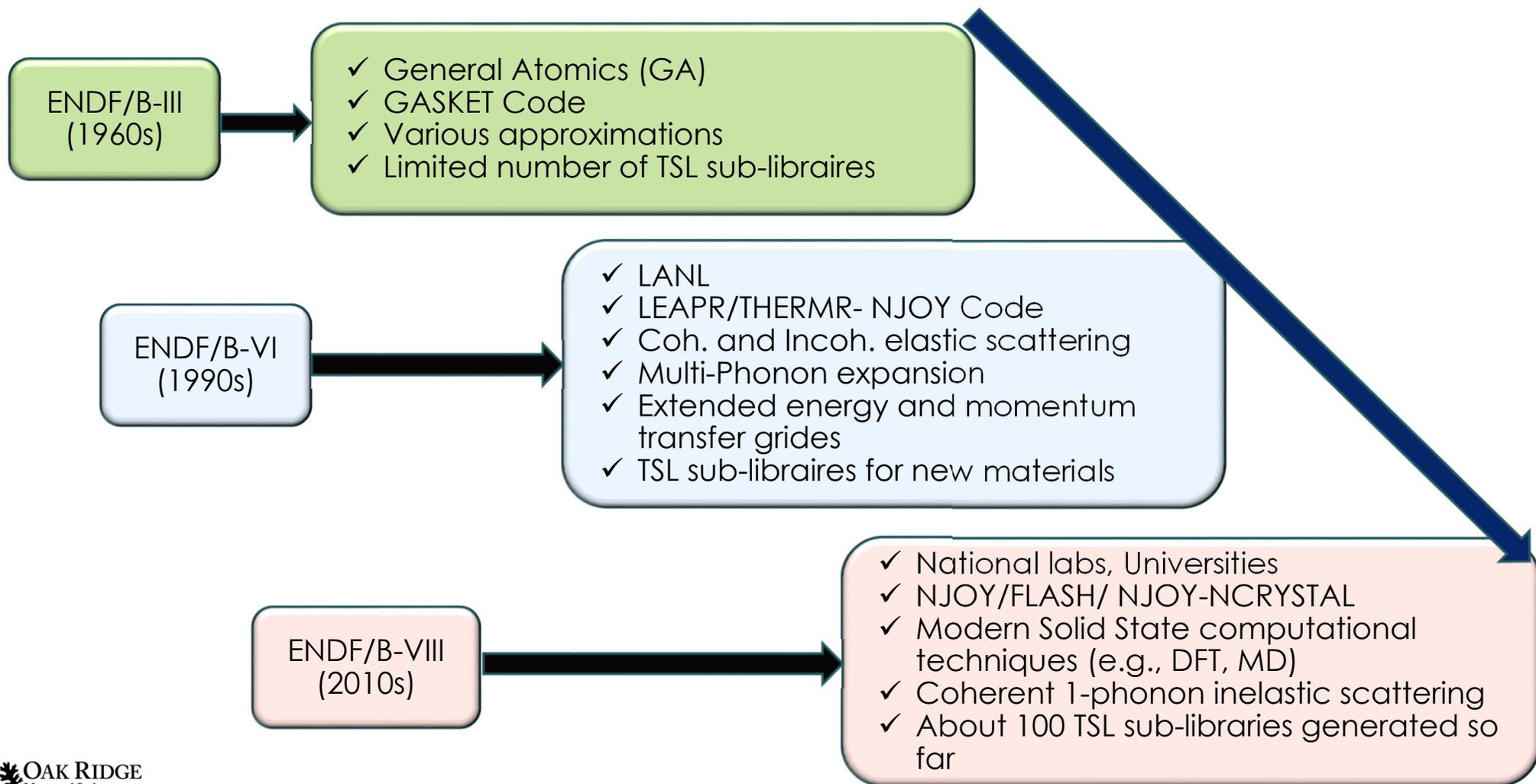
Inelastic Scattering XS



- ✓ As the temperature increases, both the 10P & 20P ENDF/B-VIII.1 cross sections overestimate the measured cross sections of Palevsky.
- ✓ The higher the temperature, the higher overestimation. This is due to the phono excess in the low energy part of the PDOSs

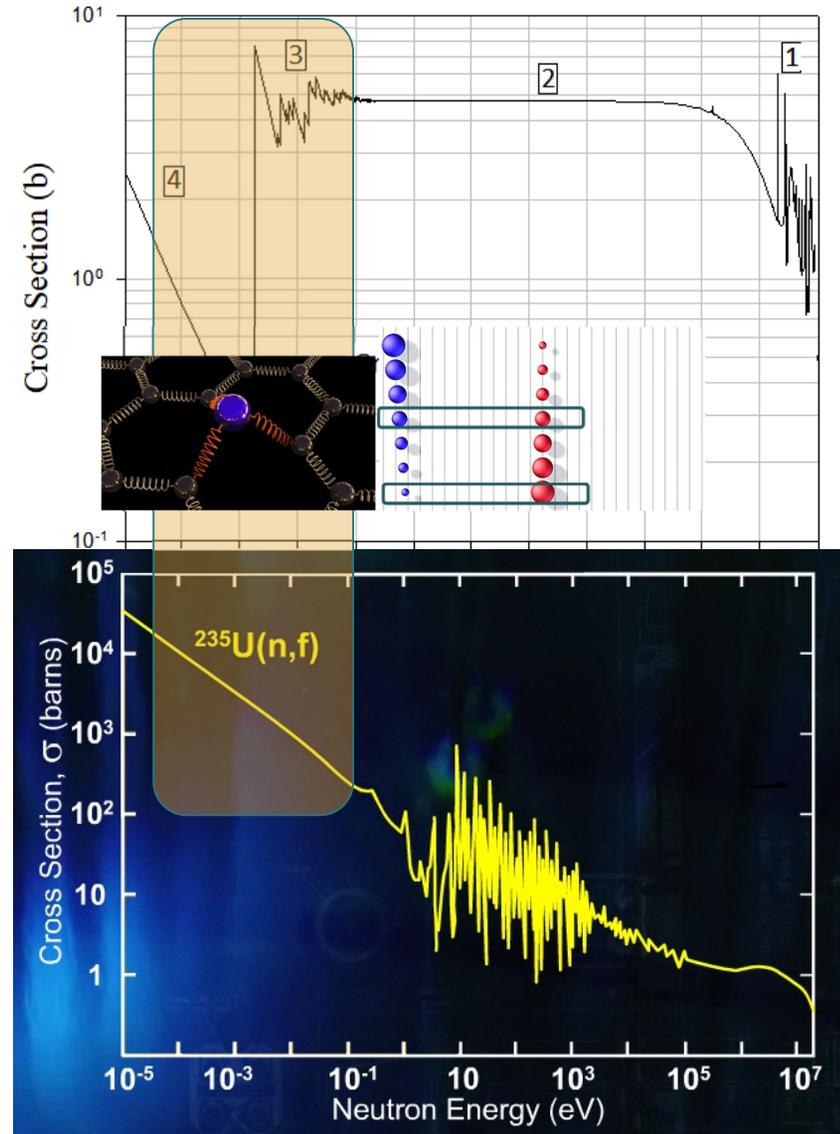
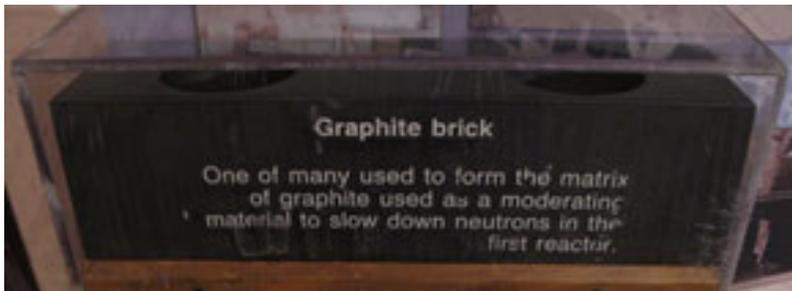


TSL Sub-Libraries Evolution



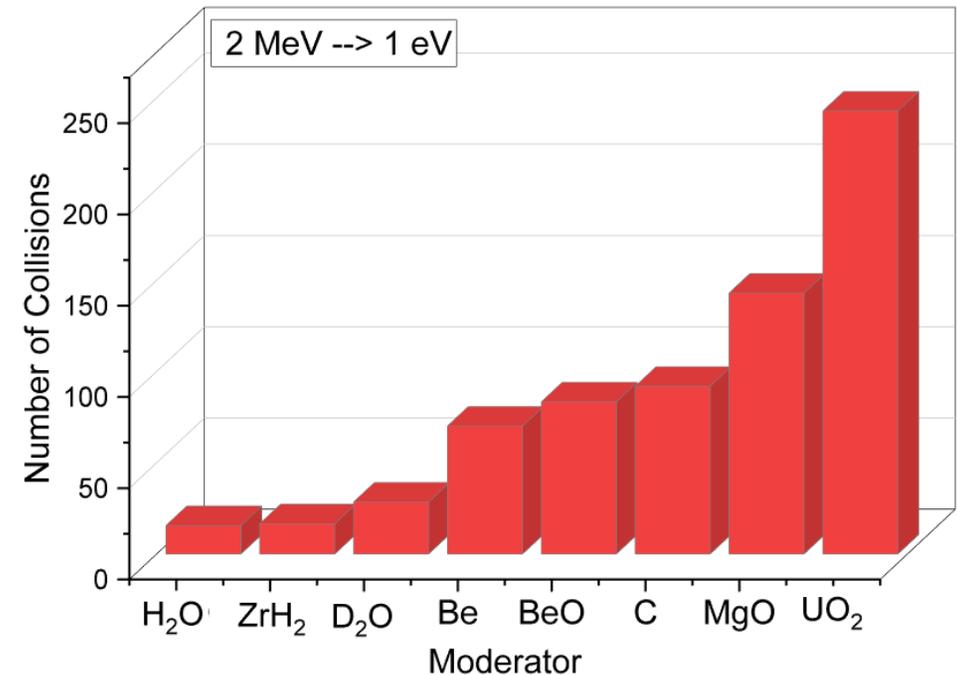
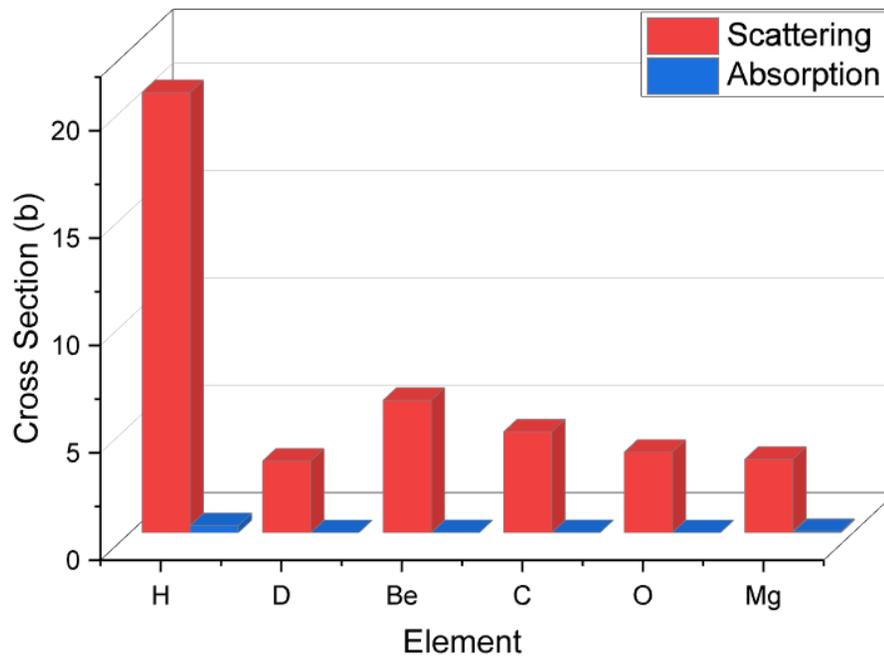
Neutron Moderation

- *Slowing Down: Region 2*
- *Thermalization* { *Region 3* *Elastic Scattering*
 { *Region 4* *Inelastic Scattering*
- High Purity (low boron content)
- High Thermal Conductivity
- High Strength
- Good stability under irradiation
- High oxidation Resistivity
- Low anisotropy
- Low Cost

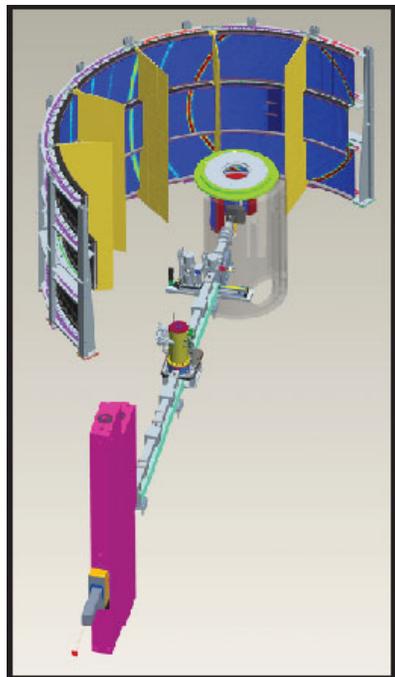


Neutron Moderation

- High scattering cross section
- Low Atomic Mass Number

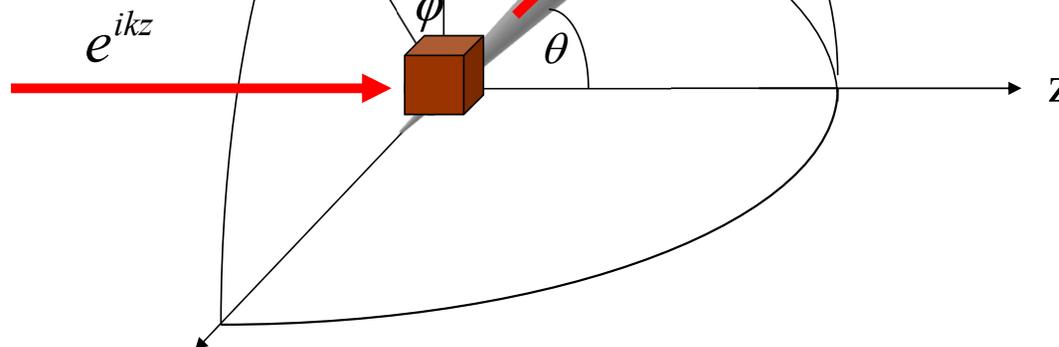


Double Differential Cross Section



ARCS/ORNL

Incident
Neutrons



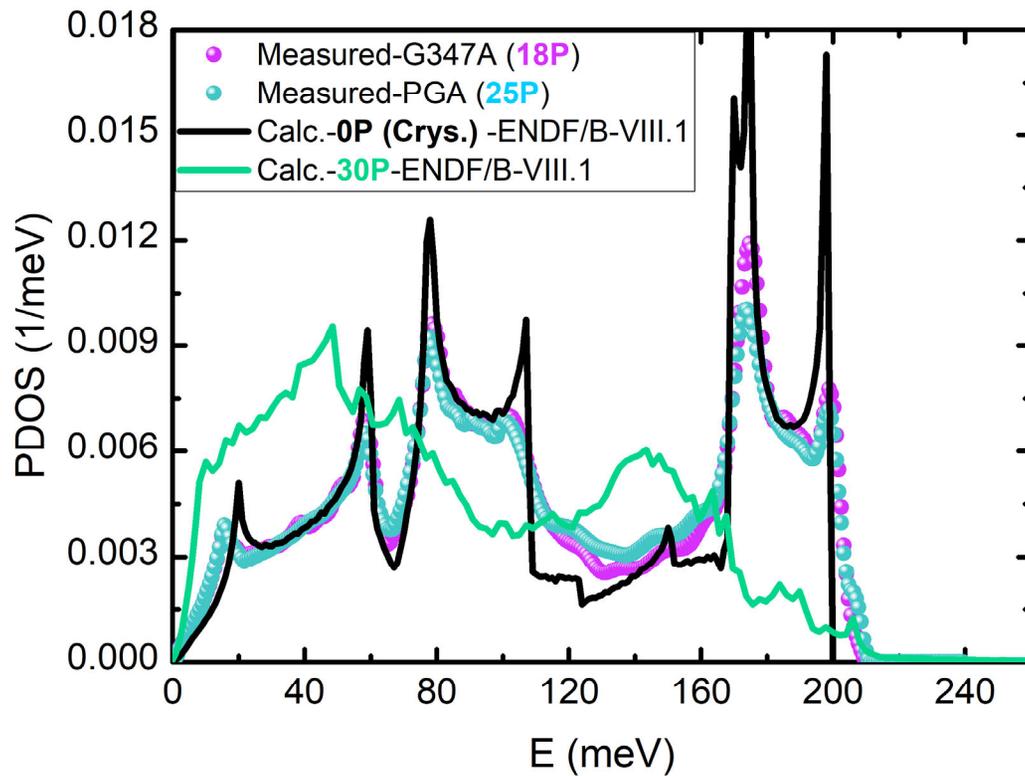
$$\frac{d^2\sigma}{d\Omega dE'} = \left(\text{Number of neutrons scattered into } d\Omega \text{ per second with final energy between } E' \text{ and } E' + dE' \right) / \Phi d\Omega dE'$$

TSL Sensitivity and Uncertainty

- Established formats and procedures exist for representing covariances in various types of ENDF reaction data.
- Transport codes, like SCALE, calculate sensitivity to 1D scattering, but they do not directly address TSL. Covariance data are accessible for all neutron files, but not for the 2D TSL.
- Presently, no published ENDF evaluations include covariance data for TSL or its corresponding scattering cross sections.
- Additionally, there is a lack of a standardized approach for generating or preserving covariance data related to TSLs.
- Ongoing initiatives such as the Global Nuclear Data System (GNDS) and the Working Party on International Nuclear Data Evaluation Cooperation (WPEC), subgroup 42/44/48, actively explore thermal scattering covariances.
- Recent efforts have focused on evaluating covariances in thermal neutron scattering for moderators like H₂O, D₂O, and graphite^{1,2,3}.

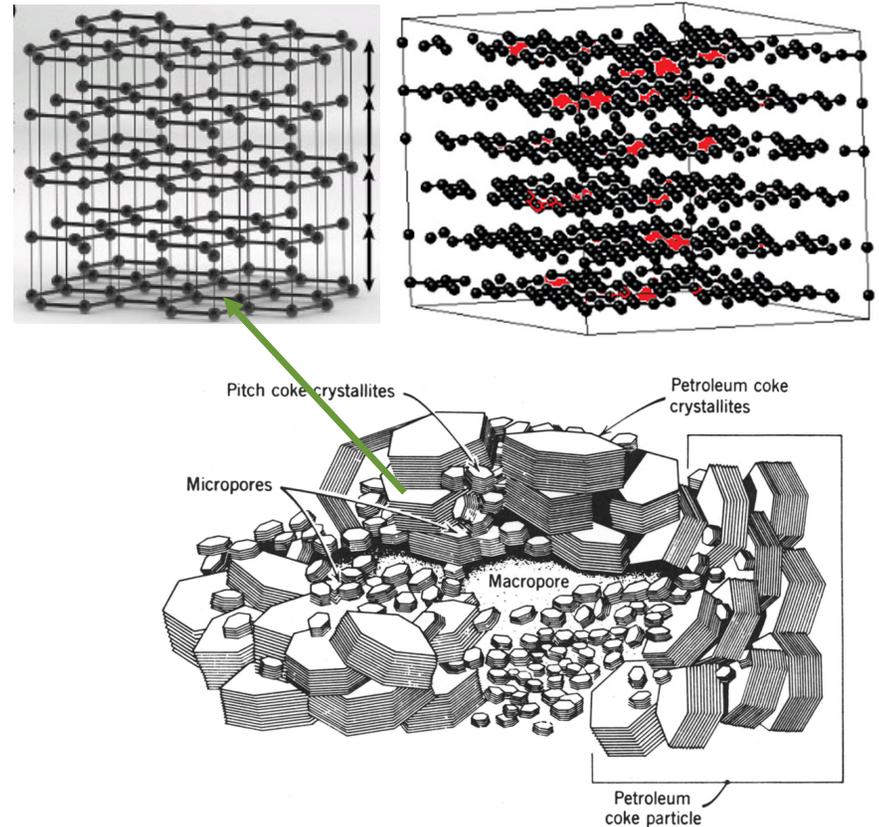
1. C. W. CHAPMAN et al., "Methodology for Generating Covariance Data of Thermal Neutron Scattering Cross Sections," *Nucl. Sci. Eng.* **195**, 13 (2021).
2. J. P. SCOTTA et al., "Generation of the ¹H in H₂O Neutron Thermal Scattering Law Covariance Matrix of the CAB Model," *EPJ Nucl. Sci. Technol.* **4**, 32 (2018).
3. J. C. HOLMES et al., "A Phonon-Based Covariance Methodology for ENDF S(α , β) and Thermal Neutron Inelastic Scattering Cross Sections," *Nucl. Sci. Eng.* **184**, 84 (2016).

MD Porosity modeling??



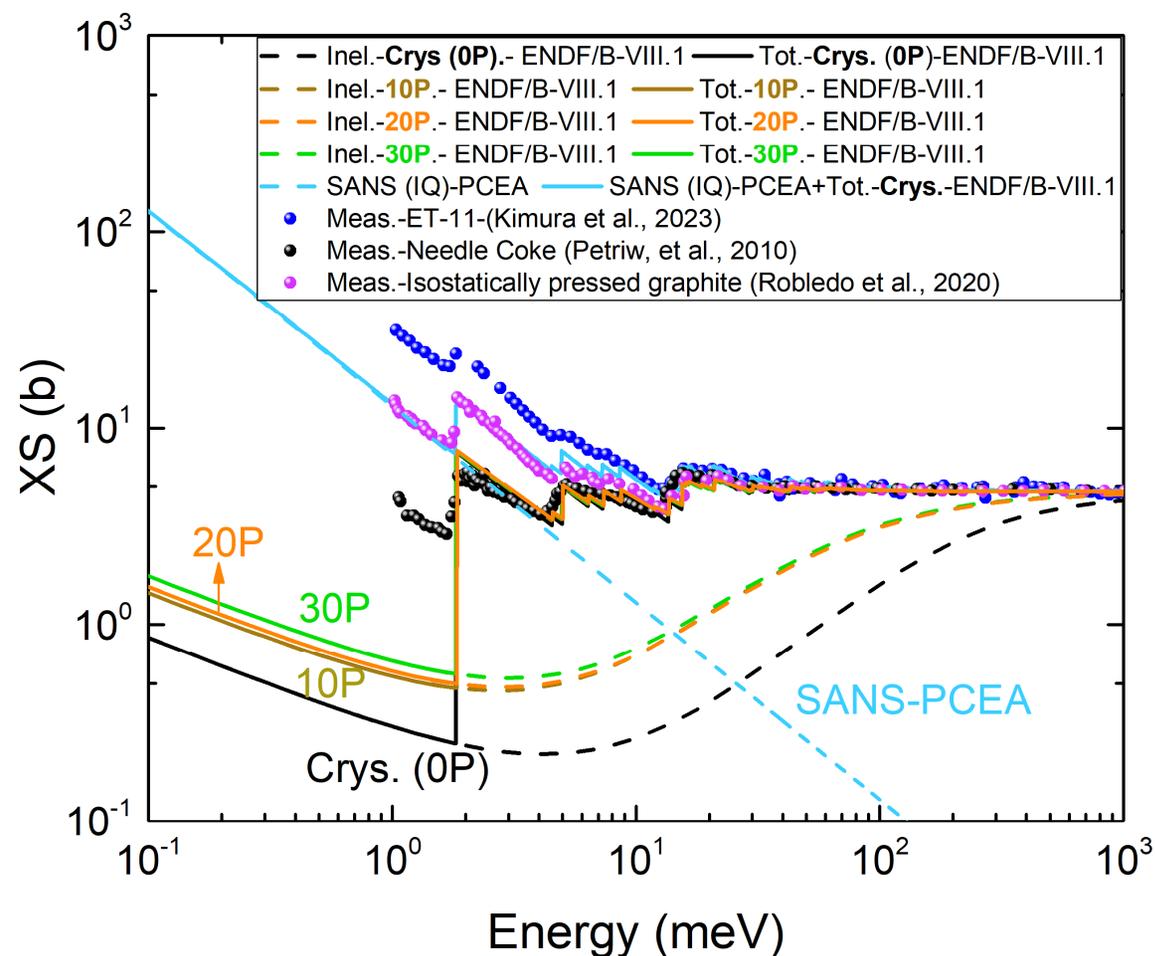
Perfect Graphite SC

Defected graphite SC
Randomly removed atoms



Small Angle Neutron Scattering (SANS)

- Different nuclear graphite types show different cross section due to SANS
- SANS is much higher than inelastic scattering cross section

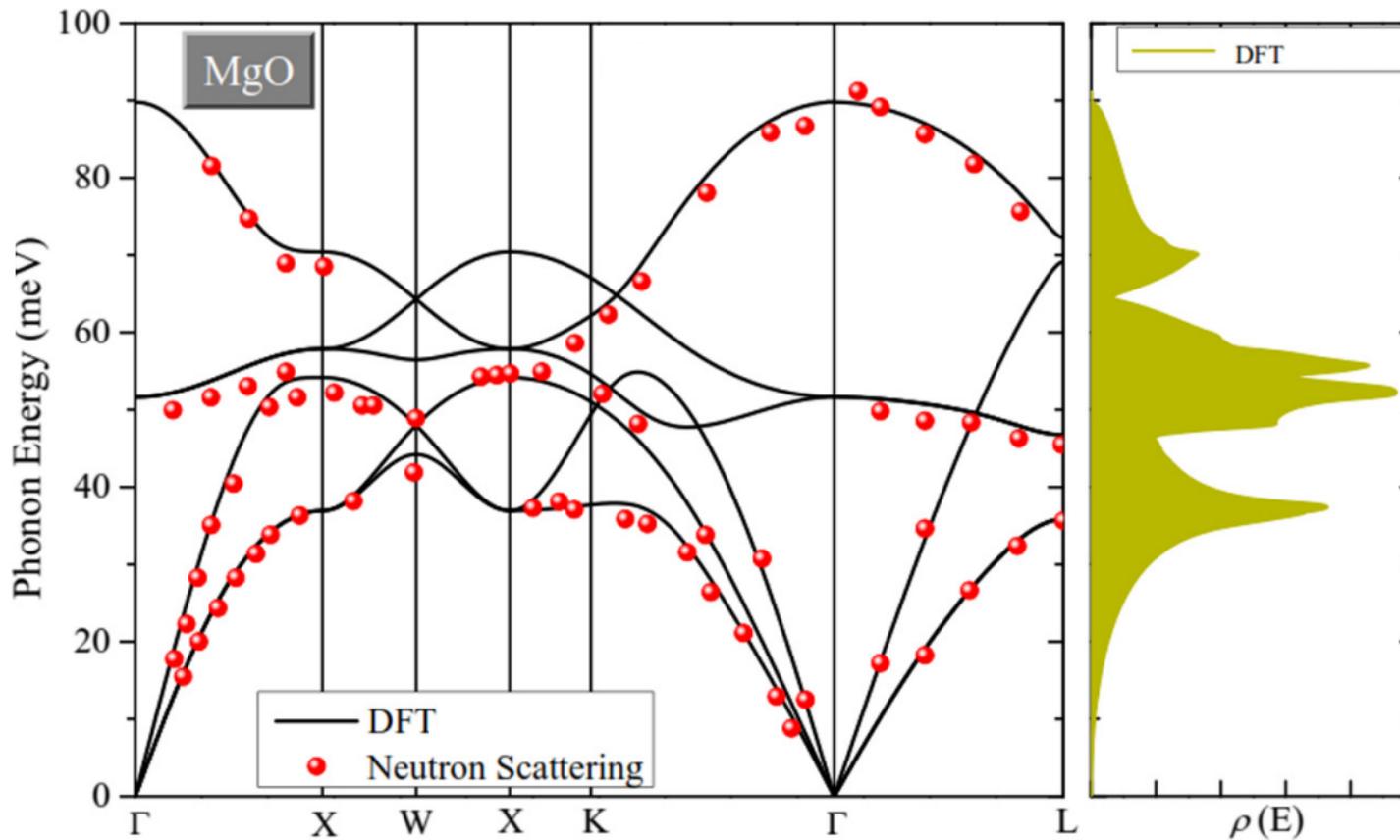


Gaps/ Nuclear Graphite

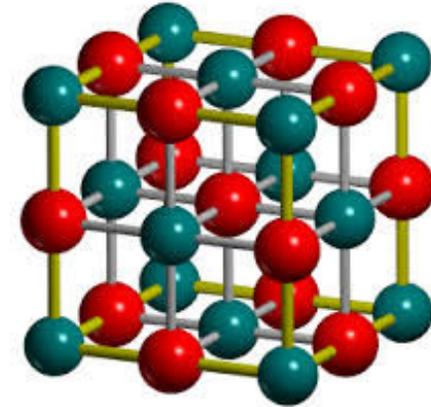
- The following **measurements** are need for different types of nuclear grade graphite
 - 1- Temperature-dependent inelastic neutron scattering cross section
 - 2- Small angle neutron scattering
 - 3- Temperature-dependent benchmarking
- The behavior of atomic vibrations at high temperatures (anharmonicity effects)need to be calculated.

Current Status of MgO TSL Sub-library

MgO Phonon Calculations



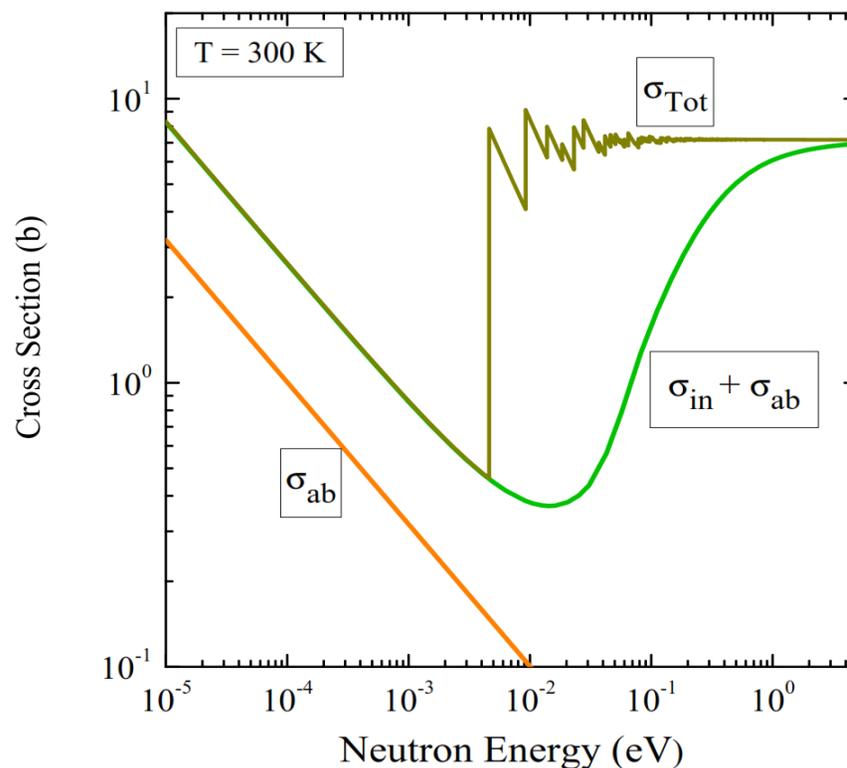
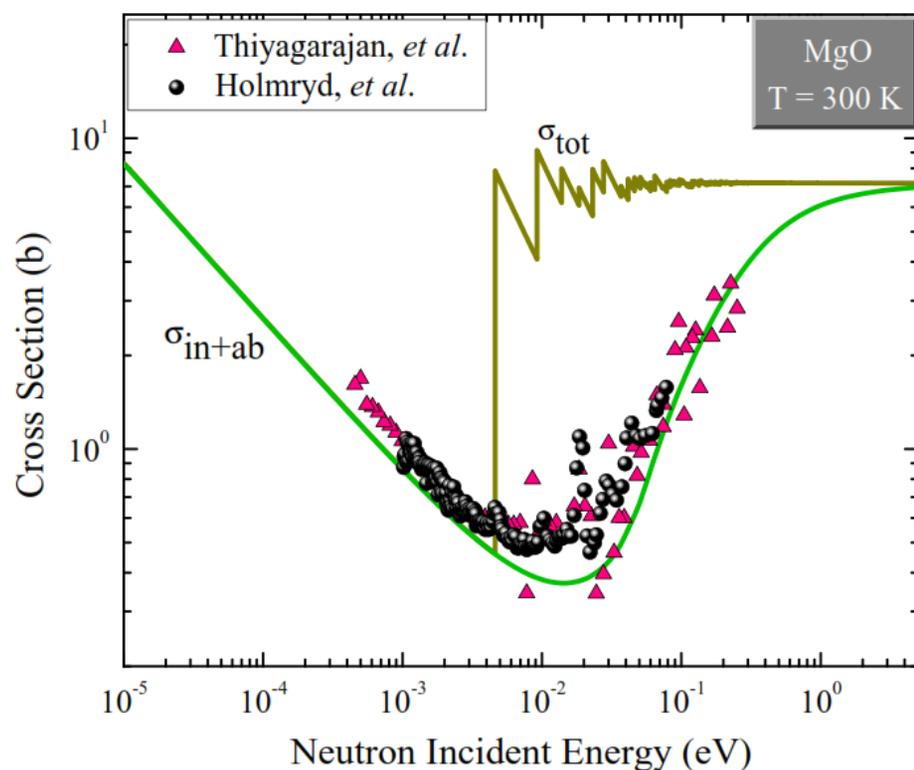
MgO Unit Cell
Rock Salt Structure



- ✓ ABINIT code
- ✓ LDA-PW
- ✓ Norm Conserving PP
- ✓ Ecut = 40 Ha
- ✓ 8 x8x8 k-mesh
- ✓ 4x4x4 -q mesh

Al-Qasir *et al.*, Thermal neutron scattering cross sections of beryllium and magnesium oxides, *Annals of Nuclear Energy* **87**, 242 (2016)

MgO Inelastic and Elastic Scattering Cross Section**



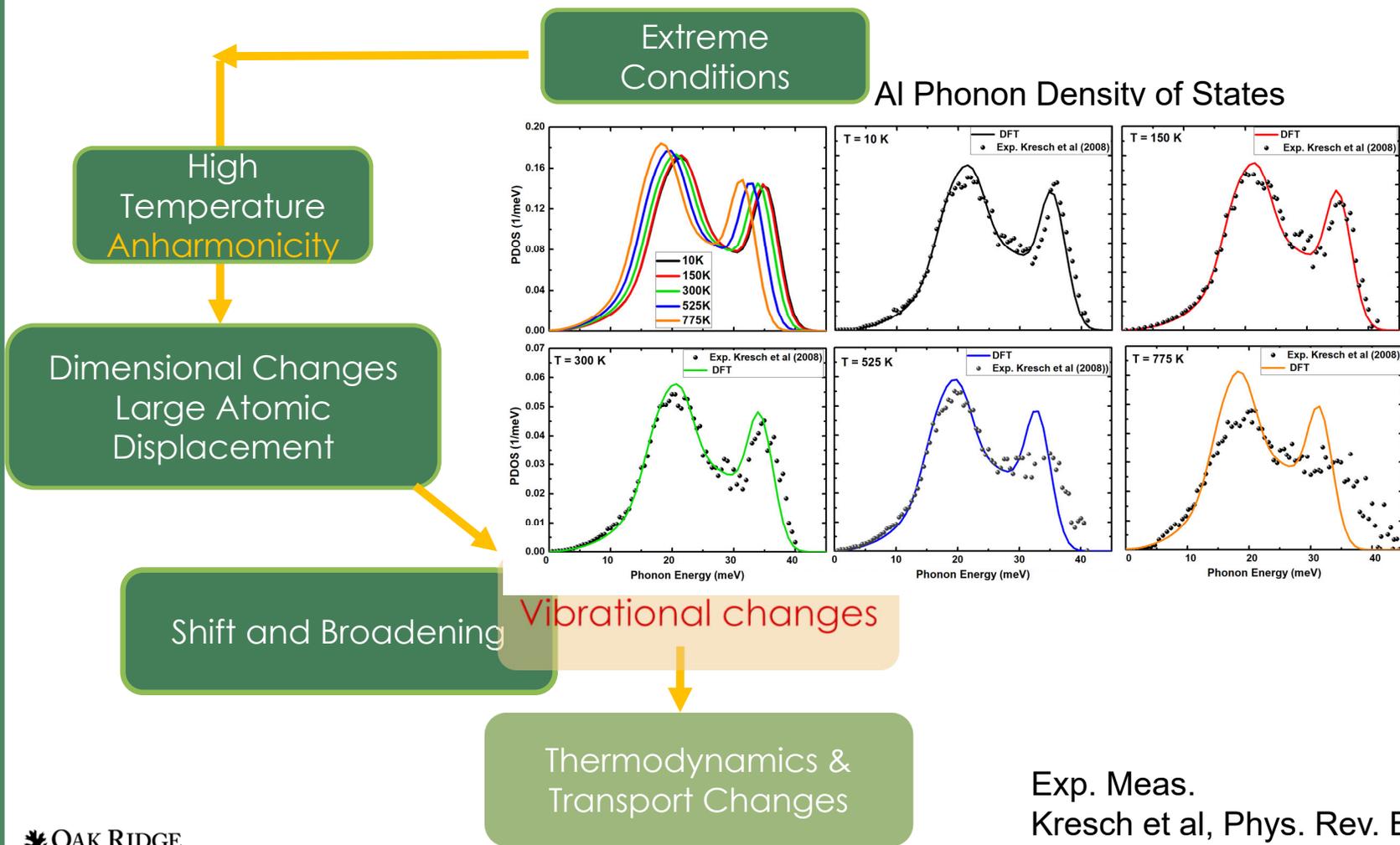
** The MgO TSL sub-library has been submitted to the Cross Section Evaluation Working Group (CSEWG) for approval and inclusion in the ENDF database; approval is pending.

Al-Qasir *et al.*, Thermal neutron scattering cross sections of beryllium and magnesium oxides, *Annals of Nuclear Energy* **87**, 242 (2016)

Gaps/MgO

- Temperature-dependent inelastic neutron scattering cross measurements of high pure MgO are required
- The behavior of atomic vibrations at high temperatures (anharmonicity effects)need to be calculated.

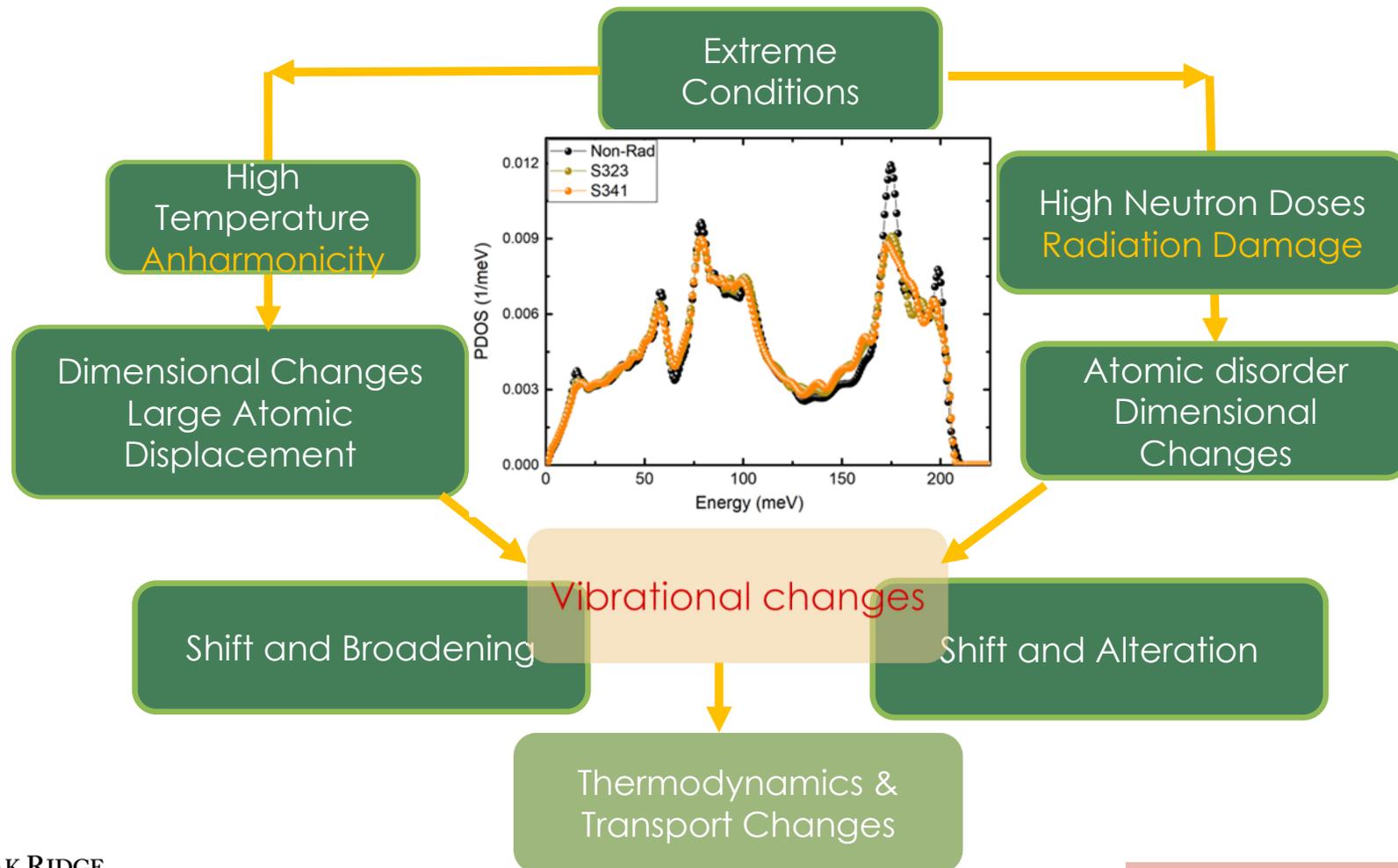
Nuclear Materials in Reactor Core (High Temperature)



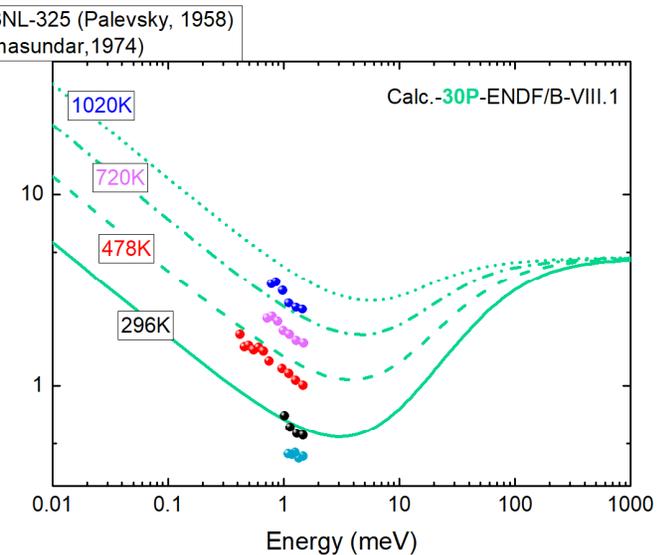
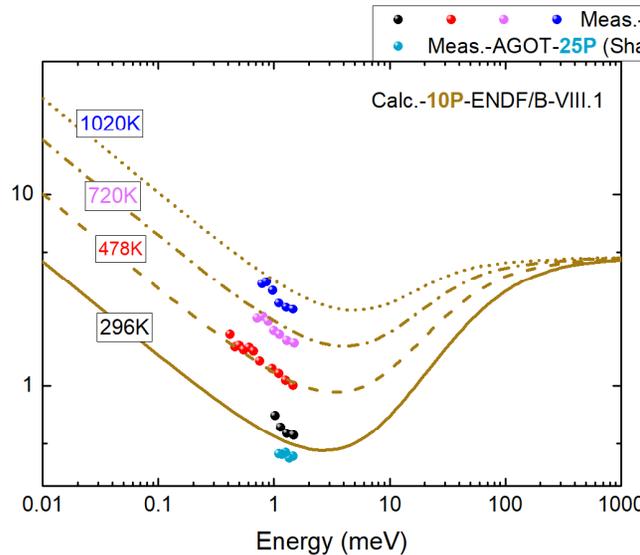
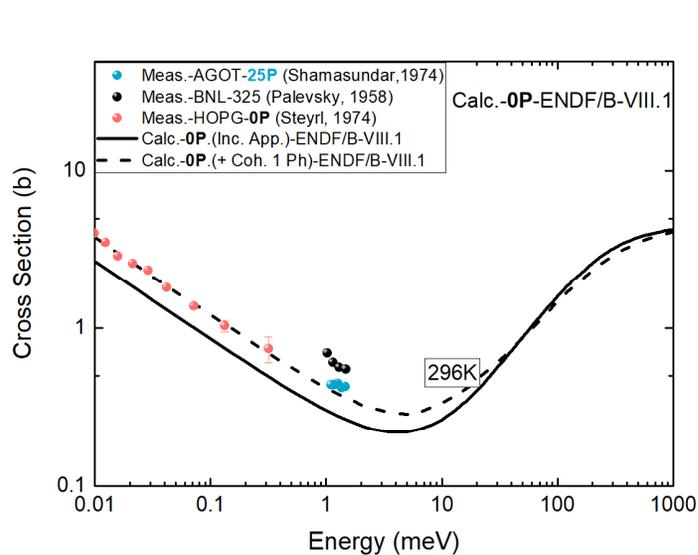
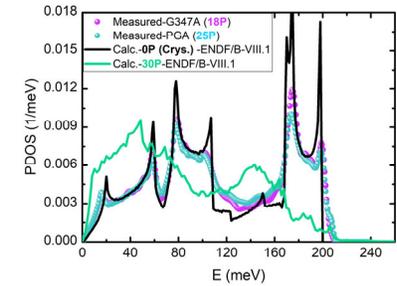
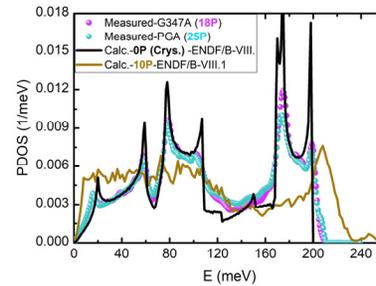
Exp. Meas.
Kresch et al, Phys. Rev. B **77**, 024301 (2008)

DNCSH WORKSHOP - 1

Nuclear Graphite in Reactor Core (High Doses of Radiation)



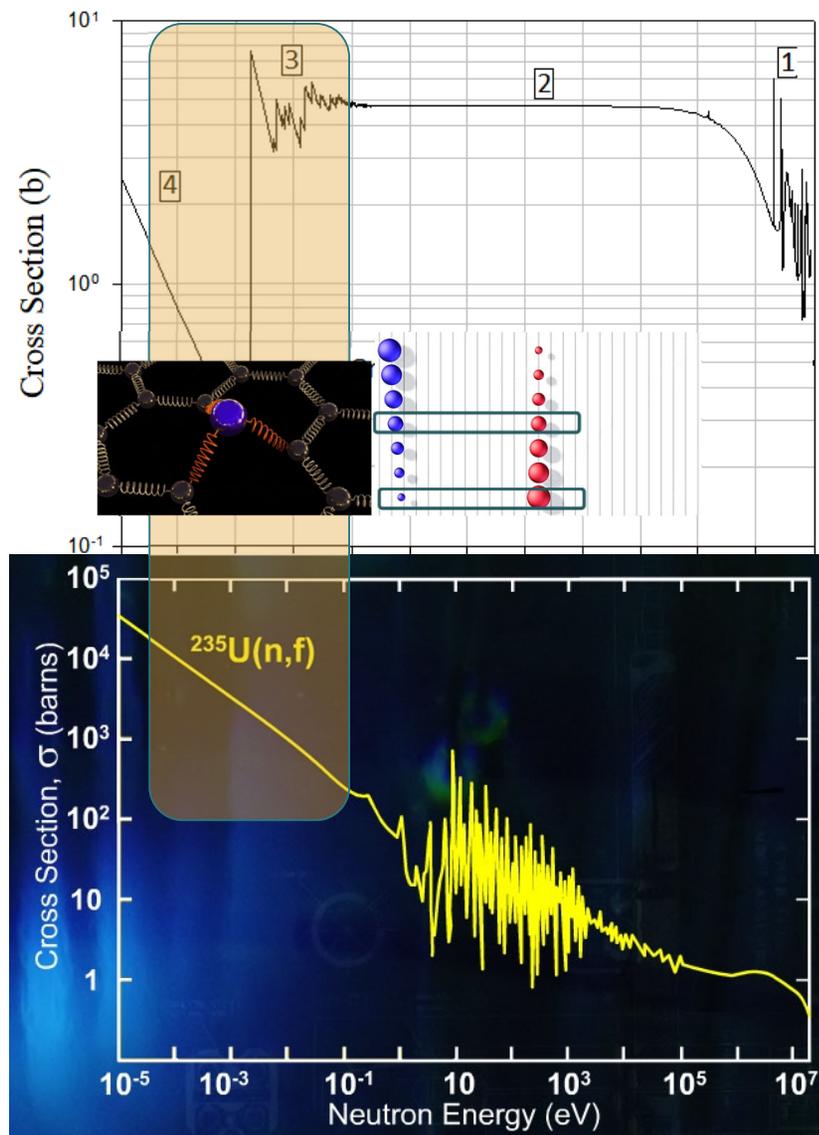
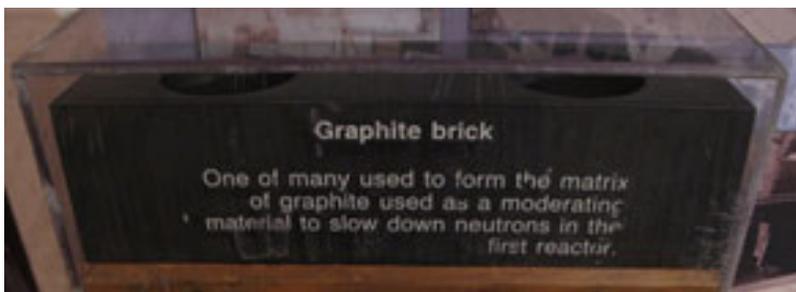
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- ✓ The higher the temperature, the higher overestimation. This is due to the phono excess in the low energy part of the PDOSs

Neutron Moderation

- *Slowing Down: Region 2*
- *Thermalization*
 - { *Region 3* *Elastic Scattering*
 - { *Region 4* *Inelastic Scattering*
- High Purity (low boron content)
- High Thermal Conductivity
- High Strength
- Good stability under irradiation
- High oxidation Resistivity
- Low anisotropy
- Low Cost



Nuclear Criticality Safety Validation & Similarity Assessment

B.J. Marshall

DNCSH Workshop
Germantown, MD
February 29, 2024

ORNL is managed by UT-Battelle LLC for the US Department of Energy

Outline

- Verification and validation
- Validation overview
- Brief introduction to sensitivity coefficients
- Sensitivity/uncertainty basis for similarity assessment
- Uncertainty propagation and correlation coefficients
- Similarity assessment via integral index c_k
- Summary

Verification and validation

- “All models are wrong, some models are useful.”
 - George E.P. Box, FRS
- There are two separate yet equally important processes to confirm the usefulness of a model:
 - Verification: Was the intended model implemented?
 - Validation: Does that model accurately predict real world measurements of the phenomena being modeled?
- This talk focuses on validation because in the United States each organization is responsible for its own validation

Validation overview

- Validation is necessary to understand how calculated model results apply to the real world
- Criticality safety validation is required to be performed by comparison to measured critical benchmark experiments
- Experiments must be neutronicallly similar to the safety application or applications being evaluated
- A large number of independent experiments should be used to determine the *bias* and *bias uncertainty* for the computational method being used

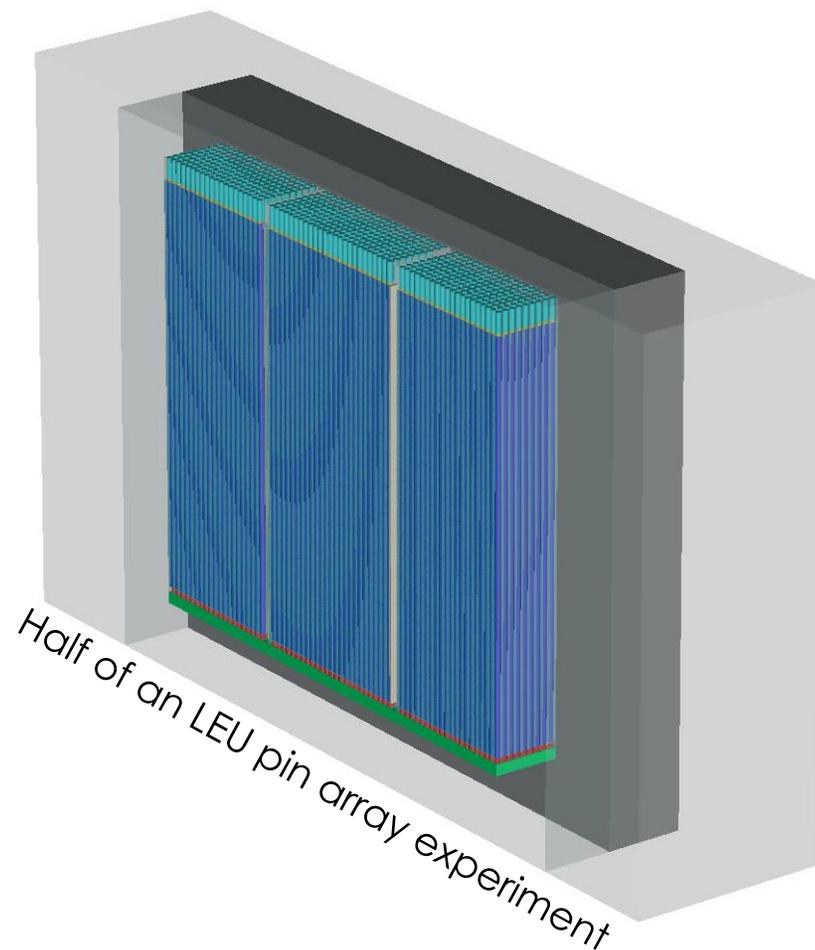
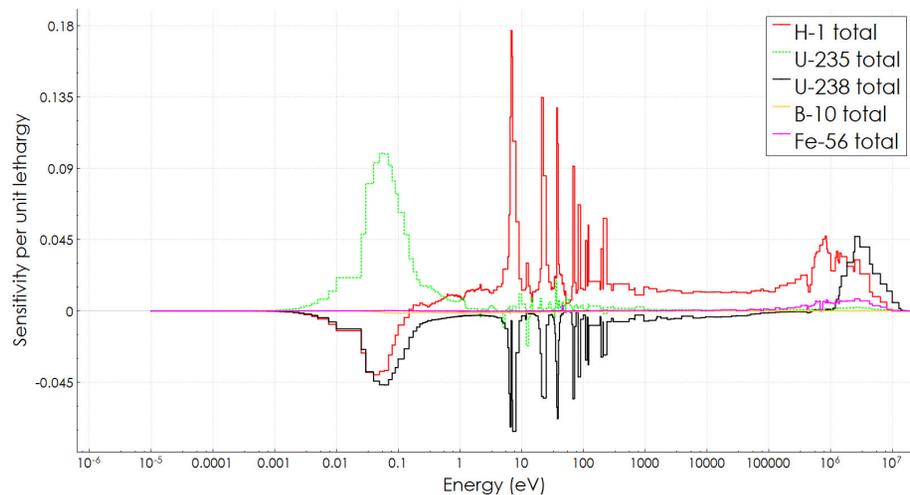
Introduction to sensitivity coefficients

- Sensitivity coefficients represent the expected change in k_{eff} due to a change in nuclear data
- The sensitivity coefficients are dimensionless ratios
- What would happen to the system k_{eff} if some piece of data were changed by some amount?

$$S_{k,\Sigma} = \frac{\frac{\partial k}{k}}{\frac{\partial \Sigma}{\Sigma}} \longleftrightarrow \Delta k_{\text{eff}} = (S_{k,\Sigma}) \left(\frac{\delta \Sigma}{\Sigma} \right)$$

k_{eff} sensitivities for a critical experiment

| Nuclide | Material | Sensitivity |
|---------|-----------|-------------|
| H-1 | Moderator | 0.240 |
| U-235 | Fuel | 0.242 |
| U-238 | Fuel | -0.140 |
| B-10 | Absorber | -0.010 |
| Fe-56 | Reflector | 0.020 |



S/U basis for similarity assessment

- Principle: bias is caused by errors in nuclear data, which are bounded by their uncertainties
- Systems will have similar computational biases if they have similar sensitivities to the same nuclear data errors
- System sensitivity combined with nuclear data uncertainties estimate potential for bias in each system
- Comparison examines nuclide-, reaction-, and energy-dependent data

Propagation of nuclear data uncertainties

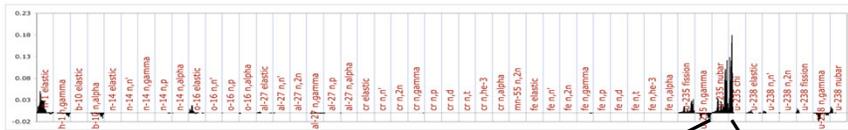
- Nuclear data uncertainty (i.e., covariances) can be propagated to quantify the data-induced uncertainty in k_{eff}

$$\sigma_k^2 = SC_{aa}S^T$$

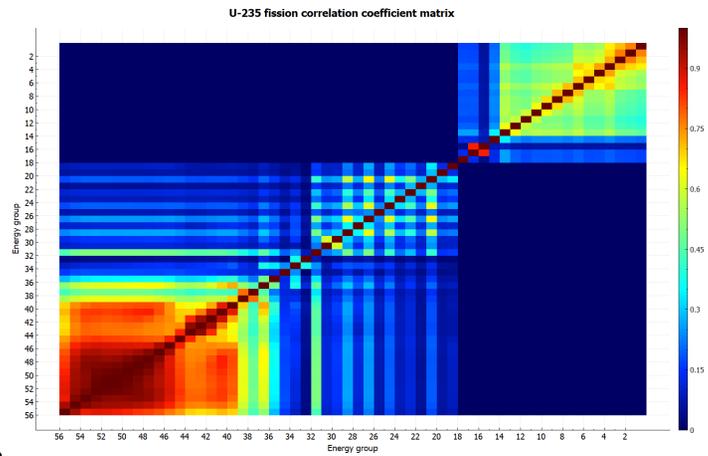
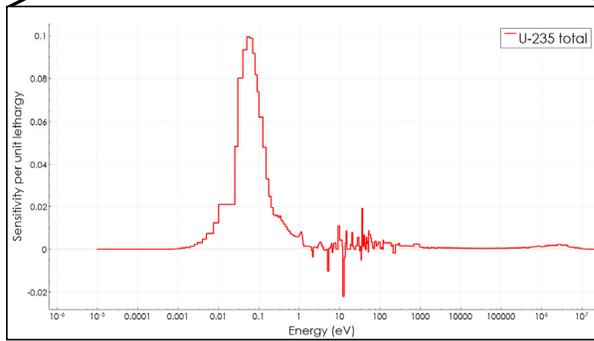
- Where:
 - S is a matrix of all energy-dependent sensitivity data for all systems considered (S^T is transpose)
 - C_{aa} is a matrix containing energy-dependent covariance information evaluated for all nuclear data

Uncertainty propagation: single system uncertainty

- Uncertainty in k_{eff} of a single system



$$S \left(\frac{\partial k}{\partial \Sigma} \right) \frac{k}{\Sigma}$$



$$C_{\alpha\alpha} \left(\frac{d\Sigma}{\Sigma} \right)^2$$

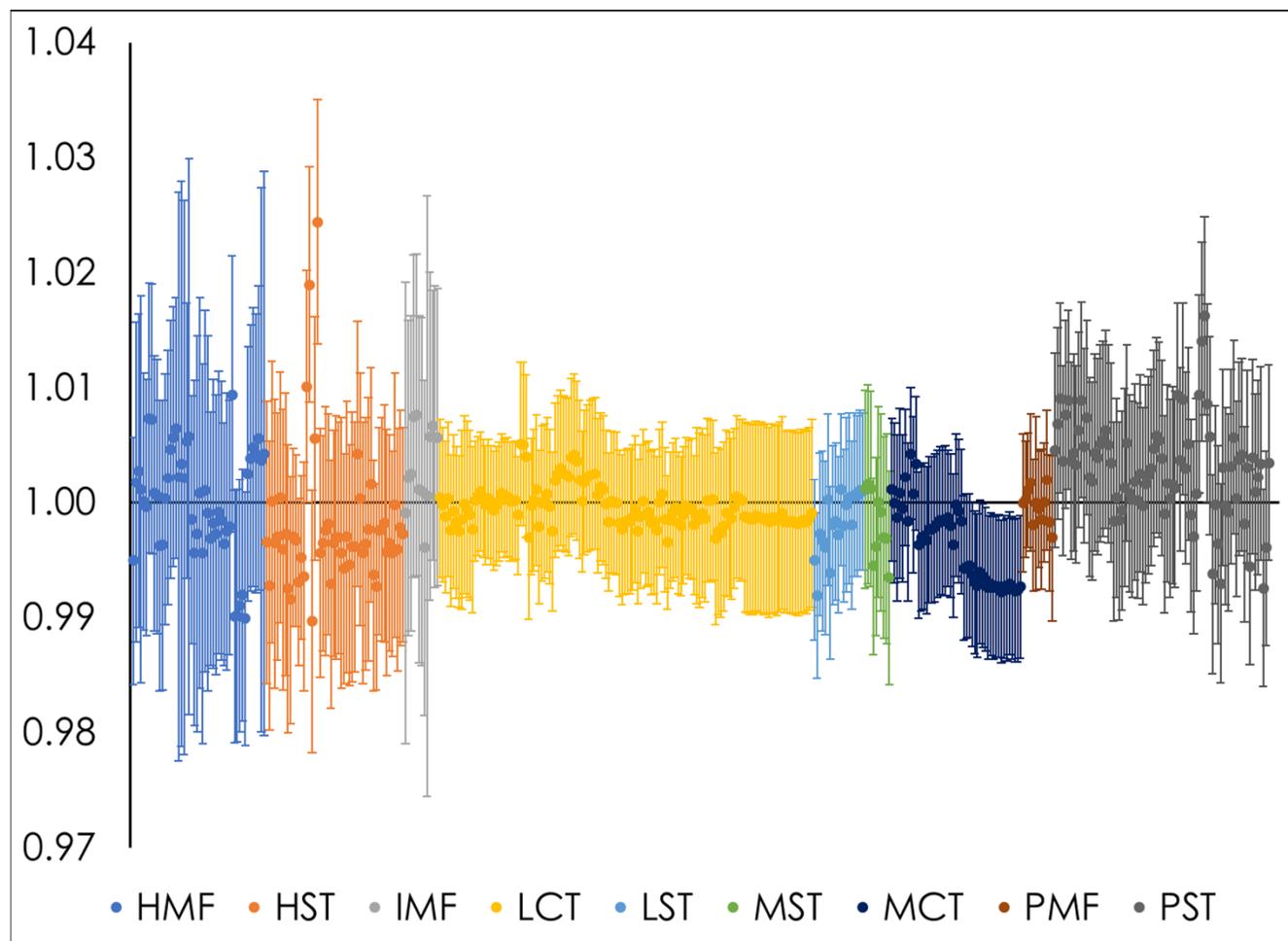
| | |
|----|----------------|
| 1 | f elastic |
| 2 | f gamma |
| 3 | b-10 elastic |
| 4 | b-10 gamma |
| 5 | n-alpha |
| 6 | n-14 elastic |
| 7 | n-14 n' |
| 8 | n-14 n, gamma |
| 9 | n-14 n, p |
| 10 | n-14 n, alpha |
| 11 | o-16 elastic |
| 12 | o-16 n' |
| 13 | o-16 n, p |
| 14 | o-16 n, alpha |
| 15 | al-27 elastic |
| 16 | al-27 n' |
| 17 | al-27 n, z, n |
| 18 | al-27 n, gamma |
| 19 | al-27 n, p |
| 20 | al-27 n, alpha |
| 21 | cr elastic |
| 22 | cr n' |
| 23 | cr n, z, n |
| 24 | cr n, gamma |
| 25 | cr n, p |
| 26 | cr n, d |
| 27 | cr n, t |
| 28 | cr n, he-3 |
| 29 | cr n, alpha |
| 30 | mn-55 n, z, n |
| 31 | fe elastic |
| 32 | fe n' |
| 33 | fe n, z, n |
| 34 | fe n, gamma |
| 35 | fe n, p |
| 36 | fe n, d |
| 37 | fe n, t |
| 38 | fe n, he-3 |
| 39 | fe n, alpha |
| 40 | u-235 fission |
| 41 | u-235 n, gamma |
| 42 | u-235 nubar |
| 43 | u-235 n, z, n |
| 44 | u-235 n, gamma |
| 45 | u-235 n, p |
| 46 | u-235 n, alpha |
| 47 | u-238 elastic |
| 48 | u-238 n' |
| 49 | u-238 n, z, n |
| 50 | u-238 fission |
| 51 | u-238 n, gamma |
| 52 | u-238 nubar |

$$= \sigma^2 C_{kk} \left(\frac{dk}{k} \right)^2$$

$$S^T \left(\frac{\partial k}{\partial \Sigma} \right) \frac{k}{\Sigma}$$

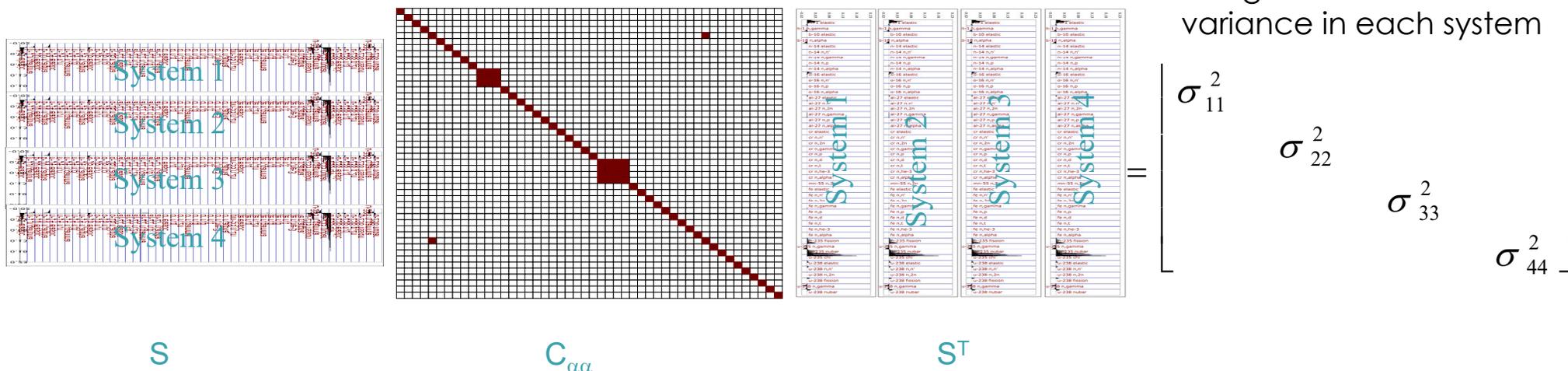
Uncertainties for critical benchmarks experiments

- Results from SCALE 6.2.2 Validation Report (ORNL/TM-2018/884)
- ~96.5% of C/E values within 1σ of unity
- **Uncertainty bounds bias!**



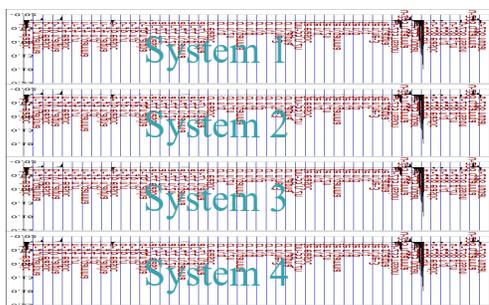
Uncertainty propagation: multiple system uncertainties

- Suppose we have sensitivity information for multiple systems:

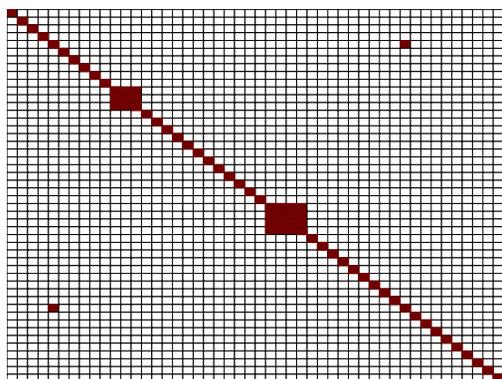


Uncertainty propagation: multiple systems covariances

- Suppose we have sensitivity information for multiple systems:



S



$C_{\alpha\alpha}$



ST

$$= \begin{bmatrix} \sigma_{12}^2 & \sigma_{13}^2 & \sigma_{14}^2 \\ \sigma_{21}^2 & \sigma_{23}^2 & \sigma_{24}^2 \\ \sigma_{31}^2 & \sigma_{32}^2 & \sigma_{34}^2 \\ \sigma_{41}^2 & \sigma_{42}^2 & \sigma_{43}^2 \end{bmatrix}$$

Off-diagonal elements are covariance between two systems

Correlation coefficient (c_k) for System 1 and System 4

- Integral index c_k based on definition of Pearson correlation coefficient

$$c_{kk} = \begin{bmatrix} \sigma_{11}^2 & \sigma_{12}^2 & \sigma_{13}^2 & \sigma_{14}^2 \\ \sigma_{21}^2 & \sigma_{22}^2 & \sigma_{23}^2 & \sigma_{24}^2 \\ \sigma_{31}^2 & \sigma_{32}^2 & \sigma_{33}^2 & \sigma_{34}^2 \\ \sigma_{41}^2 & \sigma_{42}^2 & \sigma_{43}^2 & \sigma_{44}^2 \end{bmatrix}$$


$$c_k = \frac{\sigma_{41}^2}{\sqrt{\sigma_{11}^2} \sqrt{\sigma_{44}^2}}$$

Integral index c_k

- c_k is an integral index used to assess similarity
 - Uncertainty weighted comparison of sensitivity profiles between an application and a critical benchmark experiment
 - Measure of data-induced uncertainty shared by systems and thus a measure of the shared bias
 - Correlation coefficient, so normalized from -1.0 to +1.0
 - All caveats about use of linear correlation coefficients apply
- Current guidance:
 - c_k of 0.9 or higher indicates a highly similar system
 - c_k between 0.8 and 0.9 are “marginally” similar

Summary

- S/U-based parameters should be useful in identifying similar benchmark systems
 - Basis for similarity is both sensitivity information and nuclear data uncertainties
 - c_k can be used to filter benchmarks used in any validation approach
 - c_k values can be used in trending analyses to determine subcritical limits
- ORNL recommends c_k values greater than 0.8 for inclusion in validation

Recent ORNL-Developed Models

B.J. Marshall, Veronica Karriem, Alex Shaw

DNCSH Workshop
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Outline

- TRISO pebbles in notional high-volume package
 - Model development
 - Similarity assessment
- SFR fuel in ES-3100
 - Container and fuel description
 - k_{eff} results
 - Similarity assessment
- Summary

PBMR-type and Kairos-type TRISO Pebbles in Notional High-Volume Package

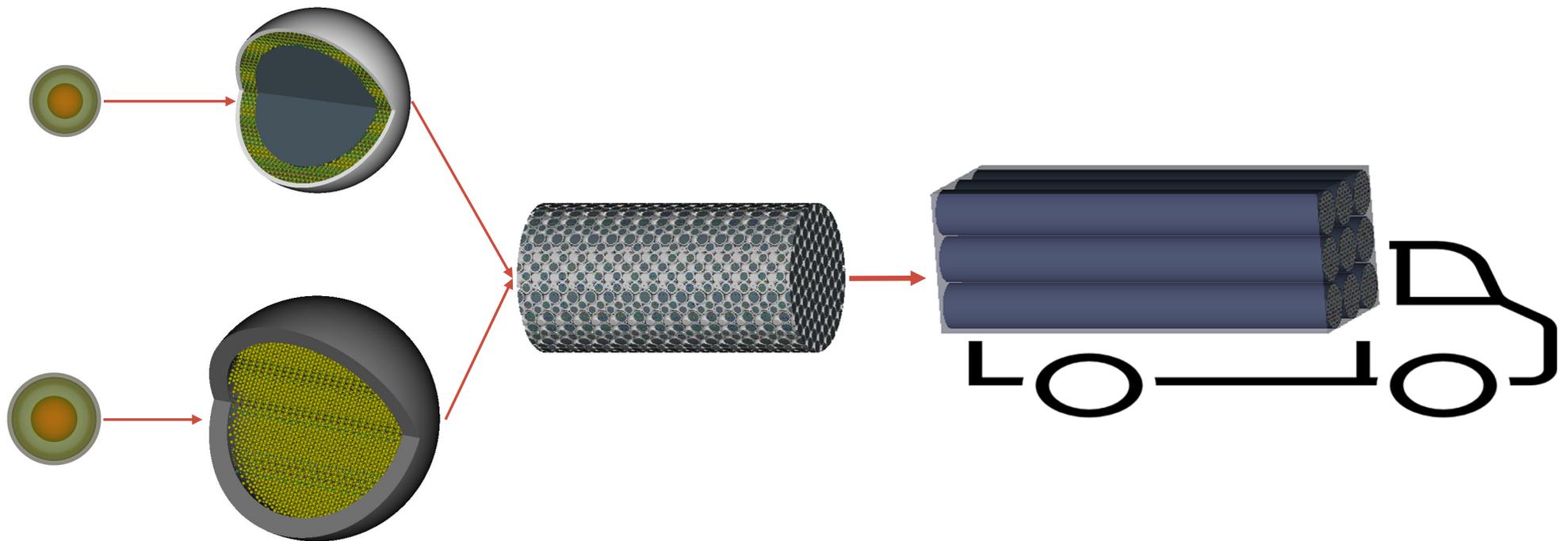
“Pebble Tanker”



Goals for “Pebble Tanker” design

- Create notional, high-volume transportation package for TRISO pebbles: PBMR-type pebble and Kairos-type pebble
- Concept is an array of metal tubes filled with pebbles inside a “dry van” semi trailer
- Size and spacing of tubes meets a k_{eff} limit of 0.94 to generate a representative system
- No analysis outside of k_{eff} dry/flooded and sensitivity coefficients calculations for both conditions

The “pebble tanker” concept



- Kairos-type pebble (top): 4×4 array of 22 cm radius tubes
- PBMR-type pebble (bottom): 3×3 array of 28 cm radius tubes

Pebble tanker model specifications

| Parameter | PBMR-type pebble | Kairos-type pebble |
|--------------------------|----------------------------|----------------------------|
| Volume fraction (grain) | 50.4 % | 36.8 % |
| U mass/pebble | 9.50 g | 5.93 g |
| Total mass/pebble | 204.1 g | 54.37 g |
| Tube array size | 3×3 | 4×4 |
| Pebbles/tube | ~12,000 | ~25,700 |
| Enrichment | 19.75 wt% ²³⁵ U | 19.95 wt% ²³⁵ U |
| k_{eff} dry | 0.44260 ± 0.00020 | 0.44993 ± 0.00020 |
| k_{eff} flooded | 0.94012 ± 0.00020 | 0.93144 ± 0.00020 |

Similarity assessment

- TSUNAMI-3D used to calculate sensitivity coefficients for flooded arrays
- c_k calculated for each tanker compared to 3936 experiments
- PBMR-type application has 285 experiments with $c_k > 0.9$
- Kairos-type application has 85 experiments with $c_k > 0.9$
- Sufficient experiments to perform validation
- Applicable experiments are largely solutions with enrichments ranging from 4.31 to 93 wt% ^{235}U

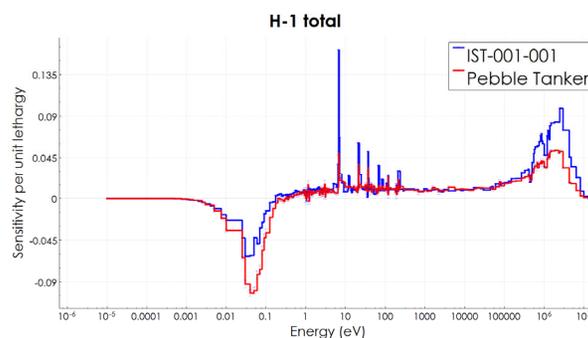
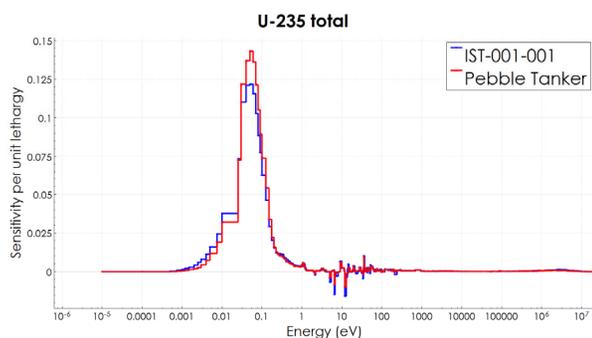
Similarity assessment details

Uncertainty contributions for flooded PBMR-type tanker model (pcm)

| Nuclide | Uncertainty | Running | Percentage |
|------------------|-------------|---------|------------|
| ²³⁵ U | 678 | 678 | 88.2 |
| ¹ H | 263 | 727 | 94.6 |
| ⁵⁶ Fe | 187 | 751 | 97.7 |
| graphite | 142 | 764 | 99.5 |
| ¹⁶ O | 69 | 767 | 99.9 |
| Total | | 768 | 100 |

c_k contribution for flooded PBMR-type tanker model and IEU-SOL-THERM-001-001

| Nuclide | c _k contribution | Running Total |
|------------------|-----------------------------|---------------|
| ²³⁵ U | 0.8029 | 0.8029 |
| ¹ H | 0.0855 | 0.8884 |
| ⁵⁶ Fe | 0.0652 | 0.9536 |
| graphite | 0.0112 | 0.9648 |
| ¹⁶ O | 0.0087 | 0.9735 |
| Total | | 0.9774 |



SFR Fuel in ES-3100



ES-3100

- 30 gal. drum with inner containment vessel (CV) for fissile material
 - Drum: Appx. 110 cm tall, 25 cm radius
 - CV: Appx. 80 cm tall, 6.5 cm radius
- Designed for transport of HEU metal and oxides, research reactor fuel
- Steel CV and casing
- Kaolite (concrete+vermiculite) fill

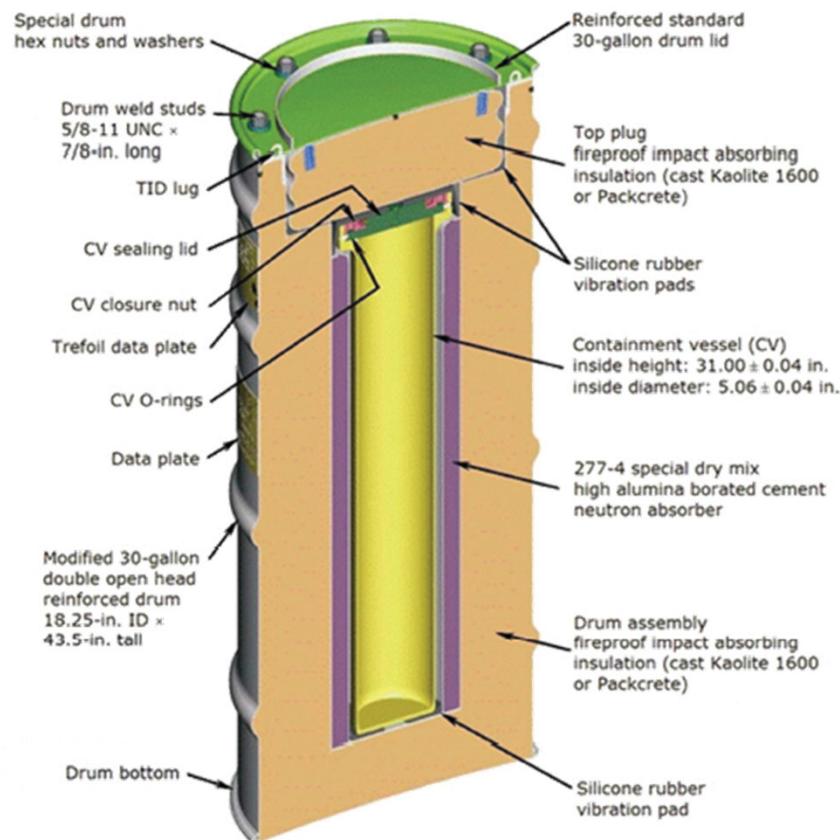


Figure from CoC 9315 Rev. 19 (USA/9315/B(U)F-96)

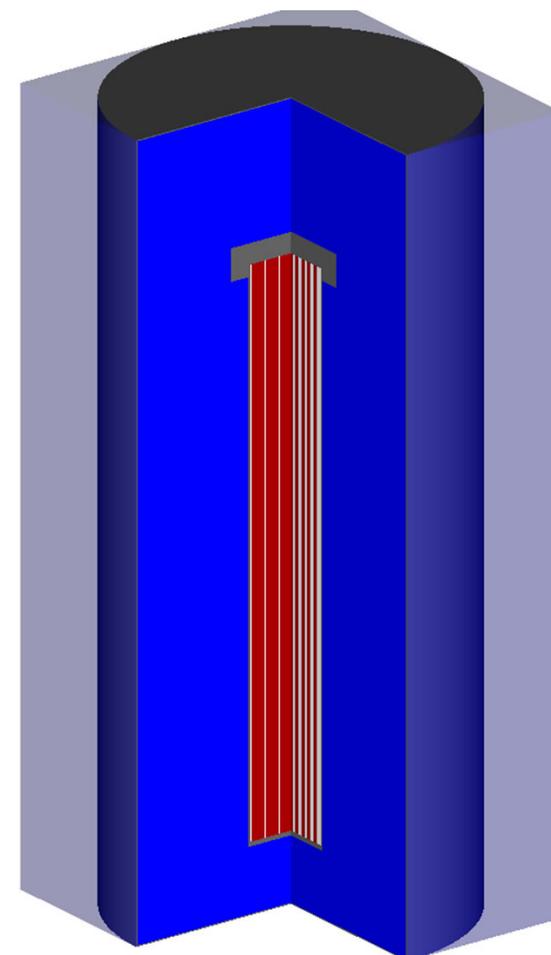
SFR Fuel Summary

- SFR fuel is expected to consist of stacked metal slugs or full-length rods
 - Example SFRs: EBR-I, EBR-II, FFTF, Fermi 1
- ORNL/TM-2022/2758 used ABTR (advanced burner test reactor) as a representative SFR design
 - Simplified composition to U/Zr alloy metallic fuel (20 wt% ^{235}U)
- ABTR uses 60 fuel assemblies for 250 MWth
- Each fuel assembly has 217 fuel slugs/rods

k_{eff} results

- 217 slugs modeled inside a single ES-3100
 - Enough fuel for a single assembly
- Modeled an infinite array of packages
 - Water flooded
 - Dry with kaolite fill
 - Polyethylene bounding of water or kaolite

| Case | k_{eff} | σ |
|---------------|------------------|----------|
| Dry | 0.62301 | 0.00010 |
| Water flooded | 0.69196 | 0.00010 |
| Polyethylene | 0.70079 | 0.00010 |



Model Development and Similarity Assessments

Similarity assessment

- TSUNAMI-3D used to calculate sensitivity coefficients for water- and polyethylene-filled ES-3100 package arrays
- c_k calculated for each package compared to a set of 4011 experiments

| Model | $0.8 < c_k < 0.9$ | $0.9 < c_k$ |
|-------|-------------------|-------------|
| Water | 41 | 1 |
| Poly | 85 | 2 |

- Sufficient experiments for validation
- Further analysis needed for gap assessment

Summary



Summary

- Notional high-volume package model developed
 - Similar experiments identified for flooded case
 - No glaring data gaps for this system
 - ^{56}Fe may be a useful target given its uncertainty contribution
- ES-3100 model with simplified SFR fuel developed
 - Similar experiments identified for flooded case
 - Additional work needed to determine if gaps exist
- Additional work needed for MSR fuel forms

Summary of Workshop 1

- Demonstrate our strategy for prioritizing benchmarks
 1. Survey the field
 2. Prioritize a target application
 3. Develop an application model (today: **fresh fuel pebble transport**)
 4. Assess the validation basis
 5. Host a workshop
 6. Develop Experiment Support Opportunity (ESO) to address gaps in validation bases
 7. Rinse and repeat
- ESOs are the main vehicle for critical benchmark awards
- We are hungry for information
 - **Long lead-time on nuclear data and experiments!**
 - Existing measurements that could become benchmarks
 - From reactor designers: what are your intended transportation packages, front-end/back-end storage systems
 - Any ideas where you may need additional nuclear data or benchmarks for safe, commercial-scale operations
- Feedback methods
 - Use the chat ☺
 - **Respond to feedback form (following the workshop)**
 - **Email DNCSH@ornl.gov**
- What next?
 - Prepare short workshop summary document and send to participants
 - Prepare ESO #1
 - April 1 2024 **Announce**
 - June 7, 2024 **Award**

Final Notes:

- Thank you for coming!
- A feedback summary will be coming to your email box. Please fill it out to provide us the needed information to make the workshop's summary report and future workshops better.
- In addition, information about the upcoming ESO will be coming to your email on or about April 1.
- Questions? Have technical information to share?

Email us at DNCSH@ornl.gov