

CORE OPERATING LIMITS REPORT (COLR)

FOR

BRAIDWOOD UNIT 2 CYCLE 23

EXELON TRACKING ID:

COLR BRAIDWOOD 2 REVISION 14

CORE OPERATING LIMITS REPORT (COLR) for BRAIDWOOD UNIT 2 CYCLE 23

1.0 CORE OPERATING LIMITS REPORT

This Core Operating Limits Report (COLR) for Braidwood Station Unit 2 Cycle 23 has been prepared in accordance with the requirements of Technical Specification 5.6.5 (ITS).

The Technical Specification Safety Limits and Limiting Conditions for Operation (LCOs) affected by this report are listed below:

SL	2.1.1	Reactor Core Safety Limits (SLs)
LCO	3.1.1	SHUTDOWN MARGIN (SDM)
LCO	3.1.3	Moderator Temperature Coefficient (MTC)
LCO	3.1.4	Rod Group Alignment Limits
LCO	3.1.5	Shutdown Bank Insertion Limits
LCO	3.1.6	Control Bank Insertion Limits
LCO	3.1.8	PHYSICS TESTS Exceptions – MODE 2
LCO	3.2.1	Heat Flux Hot Channel Factor ($F_Q(Z)$)
LCO	3.2.2	Nuclear Enthalpy Rise Hot Channel Factor ($F_{N\Delta H}$)
LCO	3.2.3	AXIAL FLUX DIFFERENCE (AFD)
LCO	3.2.5	Departure from Nucleate Boiling Ratio (DNBR)
LCO	3.3.1	Reactor Trip System (RTS) Instrumentation
LCO	3.3.9	Boron Dilution Protection System (BDPS)
LCO	3.4.1	Reactor Coolant System (RCS) Pressure, Temperature, and Flow Departure from Nucleate Boiling (DNB) Limits
LCO	3.9.1	Boron Concentration

The portions of the Technical Requirements Manual (TRM) affected by this report are listed below:

TRM TLCO 3.1.b	Boration Flow Paths – Operating
TRM TLCO 3.1.d	Charging Pumps – Operating
TRM TLCO 3.1.f	Borated Water Sources – Operating
TRM TLCO 3.1.g	Position Indication System – Shutdown
TRM TLCO 3.1.h	Shutdown Margin (SDM) – MODE 1 and MODE 2 with $k_{eff} \geq 1.0$
TRM TLCO 3.1.i	Shutdown Margin (SDM) – MODE 5
TRM TLCO 3.1.j	Shutdown and Control Rods
TRM TLCO 3.1.k	Position Indication System – Shutdown (Special Test Exception)

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2.0 OPERATING LIMITS

The cycle-specific parameter limits for the specifications listed in Section 1.0 are presented in the following subsections. These limits are applicable for the entire cycle unless otherwise identified. These limits have been developed using the NRC-approved methodologies specified in Technical Specification 5.6.5.

2.1 Reactor Core Safety Limits (SLs) (SL 2.1.1)

2.1.1 In MODES 1 and 2, the combination of Thermal Power, Reactor Coolant System (RCS) highest loop average temperature, and pressurizer pressure shall not exceed the limits specified in Figure 2.1.1.

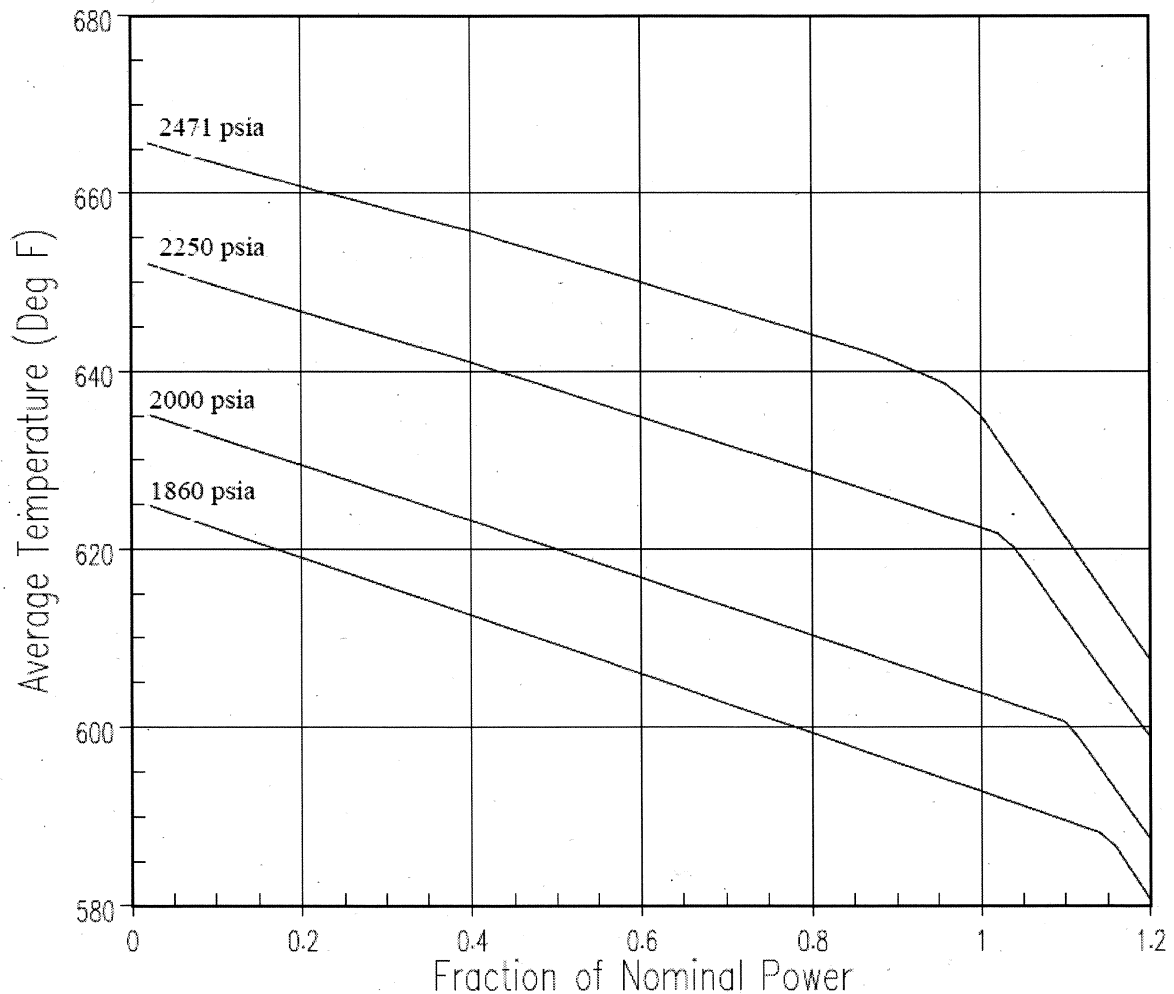


Figure 2.1.1: Reactor Core Limits

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2.2 SHUTDOWN MARGIN (SDM)

The SDM limit for MODES 1, 2, 3, and 4 is:

2.2.1 The SDM shall be greater than or equal to 1.3% $\Delta k/k$ (LCOs 3.1.1, 3.1.4, 3.1.5, 3.1.6, 3.1.8, 3.3.9; TRM TLCOs 3.1.b, 3.1.d, 3.1.f, 3.1.h, and 3.1.j).

The SDM limit for MODE 5 is:

2.2.2 SDM shall be greater than or equal to 1.3% $\Delta k/k$ (LCO 3.1.1, LCO 3.3.9; TRM TLCOs 3.1.i and 3.1.j).

2.3 Moderator Temperature Coefficient (MTC) (LCO 3.1.3)

The Moderator Temperature Coefficient (MTC) limits are:

2.3.1 The BOL/ARO/HZP-MTC upper limit shall be $+2.314 \times 10^{-5} \Delta k/k/^{\circ}F$.

2.3.2 The EOL/ARO/HFP-MTC lower limit shall be $-4.6 \times 10^{-4} \Delta k/k/^{\circ}F$.

2.3.3 The EOL/ARO/HFP-MTC Surveillance limit at 300 ppm shall be $-3.7 \times 10^{-4} \Delta k/k/^{\circ}F$.

2.3.4 The EOL/ARO/HFP-MTC Surveillance limit at 60 ppm shall be $-4.3 \times 10^{-4} \Delta k/k/^{\circ}F$.

where: BOL stands for Beginning of Cycle Life
ARO stands for All Rods Out
HZP stands for Hot Zero Thermal Power
EOL stands for End of Cycle Life
HFP stands for Hot Full Thermal Power

2.4 Shutdown Bank Insertion Limits (LCO 3.1.5)

2.4.1 All shutdown banks shall be fully withdrawn to at least 224 steps.

2.5 Control Bank Insertion Limits (LCO 3.1.6)

2.5.1 The control banks, with Bank A greater than or equal to 224 steps, shall be limited in physical insertion as shown in Figure 2.5.1.

2.5.2 Each control bank shall be considered fully withdrawn from the core at greater than or equal to 224 steps.

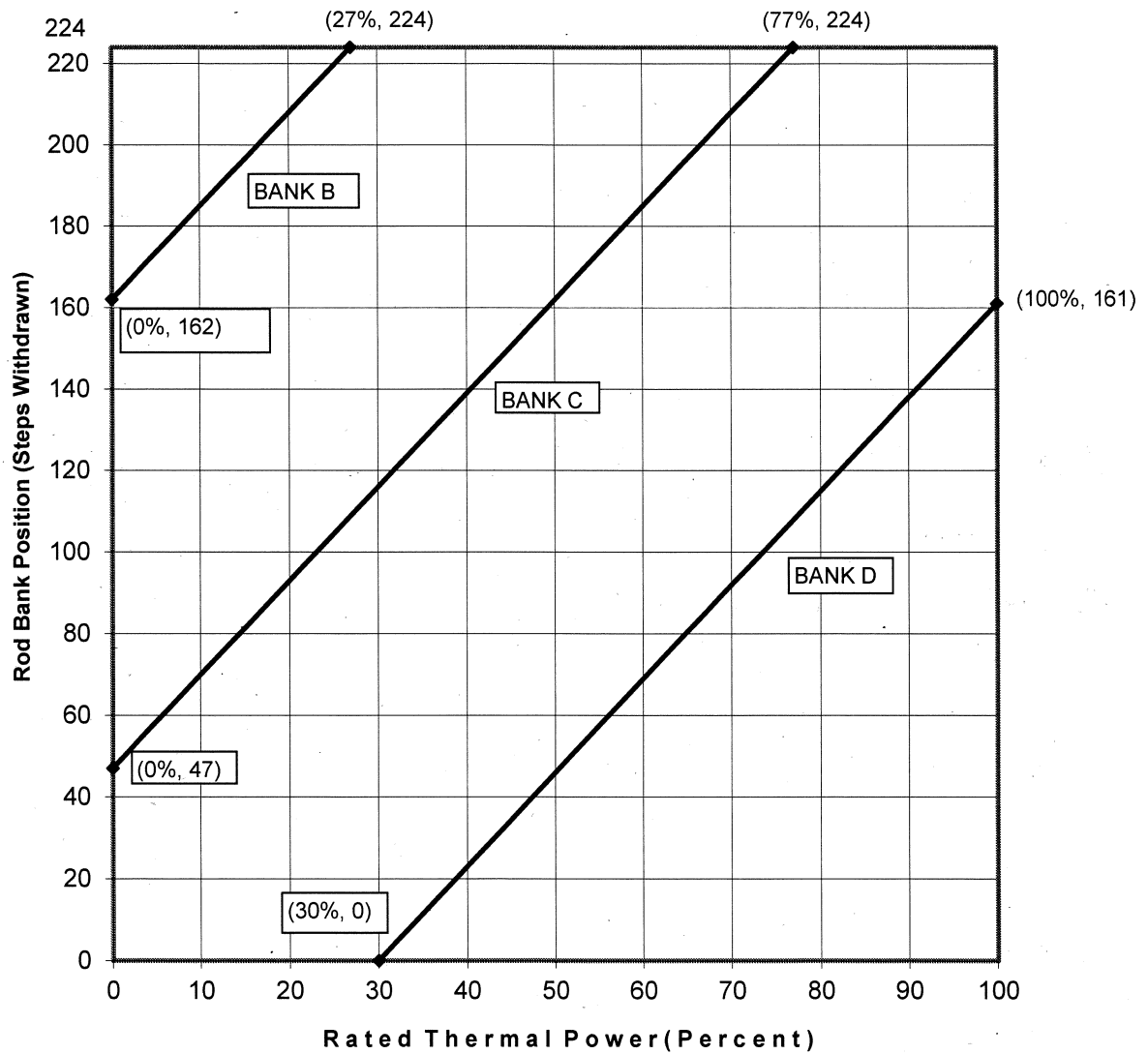
2.5.3 The control banks shall be operated in sequence by withdrawal of Bank A, Bank B, Bank C and Bank D. The control banks shall be sequenced in reverse order upon insertion.

2.5.4 Each control bank not fully withdrawn from the core shall be operated with the following overlap limits as a function of park position:

Park Position (step)	Overlap Limit (step)
225	110

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Figure 2.5.1:
Control Bank Insertion Limits Versus Percent Rated Thermal Power



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2.6 Heat Flux Hot Channel Factor ($F_Q(Z)$) (LCO 3.2.1)

2.6.1 Total Peaking Factor:

$$F_Q(Z) \leq \frac{F_Q^{RTP}}{0.5} \times K(Z) \quad \text{for } P \leq 0.5$$

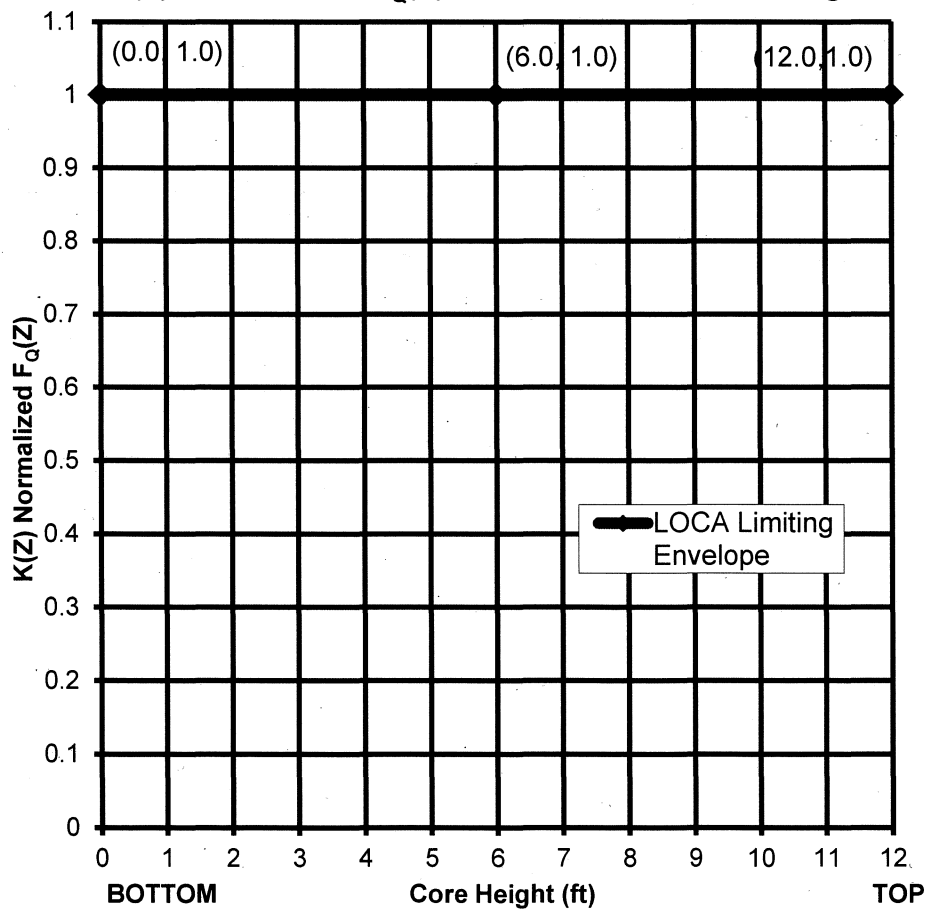
$$F_Q(Z) \leq \frac{F_Q^{RTP}}{P} \times K(Z) \quad \text{for } P > 0.5$$

where: P = the ratio of THERMAL POWER to RATED THERMAL POWER

$$F_Q^{RTP} = 2.60$$

$K(Z)$ is provided in Figure 2.6.1.

Figure 2.6.1:
 $K(Z)$ - Normalized $F_Q(Z)$ as a Function of Core Height



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2.6.2 W(Z) Values:

- a) When the Power Distribution Monitoring System (PDMS) is OPERABLE, $W(Z) = 1.00000$ for all axial points.
- b) When PDMS is inoperable, $W(Z)$ is provided as:
 - 1) Table 2.6.2.a are the normal operation $W(Z)$ values that correspond to the NORMAL AXIAL FLUX DIFFERENCE (AFD) Acceptable Operation Limits provided in Figure 2.8.1.a. The Normal AFD Acceptable Operation Limits may be invoked at any time and must be used with the corresponding $W(Z)$ values.
 - 2) Table 2.6.2.b are the Expanded normal operation $W(Z)$ values that correspond to the EXPANDED AXIAL FLUX DIFFERENCE (AFD) Acceptable Operation Limits provided in Figure 2.8.1.b. The Expanded AFD Acceptable Operation Limits may be invoked at any time and must be used with the corresponding $W(Z)$ values.

Table 2.6.2.c shows the $F_Q^C(z)$ penalty factors that are greater than 2% per the allowable surveillance frequency. These values shall be used to increase the $F_Q^W(z)$ as per Surveillance Requirement 3.2.1.2. A 2% penalty factor shall be used at all cycle burnups that are outside the range of Table 2.6.2.c.

2.6.3 Uncertainty:

The uncertainty, U_{FQ} , to be applied to the Heat Flux Hot Channel Factor $F_Q(Z)$ shall be calculated by the following formula

$$U_{FQ} = U_{qu} \bullet U_e$$

where:

- U_{qu} = Base F_Q measurement uncertainty = 1.05 when PDMS is inoperable
(U_{qu} is defined by PDMS and cannot be less than 1.05 when OPERABLE.)
 U_e = Engineering uncertainty factor = 1.03

2.6.4 PDMS Alarms:

$F_Q(Z)$ Warning Setpoint = 2% $F_Q(Z)$ Margin
 $F_Q(Z)$ Alarm Setpoint = 0% $F_Q(Z)$ Margin

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Table 2.6.2.a

W(Z) versus Core Height for Normal AFD Acceptable Operation Limits in Figure 2.8.1.a
(Top and Bottom 8% Excluded per Braidwood SR 3.2.1.2 Bases)

Height (feet)	150 MWD/MTU	3000 MWD/MTU	14000 MWD/MTU	20000 MWD/MTU
0.00 (core bottom)	1.2598	1.3645	1.2469	1.1953
0.20	1.2525	1.3544	1.2404	1.1863
0.40	1.2522	1.3507	1.2426	1.1875
0.60	1.2559	1.3508	1.2497	1.1946
0.80	1.2639	1.3539	1.2626	1.2090
1.00	1.2621	1.3462	1.2657	1.2139
1.20	1.2514	1.3306	1.2589	1.2080
1.40	1.2366	1.3108	1.2483	1.1984
1.60	1.2212	1.2898	1.2377	1.1892
1.80	1.2064	1.2673	1.2261	1.1797
2.00	1.1929	1.2433	1.2132	1.1690
2.20	1.1784	1.2183	1.1993	1.1575
2.40	1.1637	1.1934	1.1850	1.1458
2.60	1.1492	1.1690	1.1707	1.1343
2.80	1.1340	1.1445	1.1558	1.1218
3.00	1.1234	1.1254	1.1443	1.1168
3.20	1.1199	1.1163	1.1397	1.1185
3.40	1.1185	1.1151	1.1391	1.1277
3.60	1.1167	1.1149	1.1400	1.1387
3.80	1.1138	1.1145	1.1434	1.1494
4.00	1.1137	1.1135	1.1482	1.1598
4.20	1.1164	1.1122	1.1520	1.1694
4.40	1.1180	1.1106	1.1552	1.1781
4.60	1.1193	1.1094	1.1576	1.1855
4.80	1.1201	1.1092	1.1591	1.1913
5.00	1.1203	1.1094	1.1595	1.1964
5.20	1.1198	1.1096	1.1588	1.2014
5.40	1.1195	1.1091	1.1568	1.2050
5.60	1.1233	1.1091	1.1533	1.2064
5.80	1.1281	1.1124	1.1530	1.2113
6.00	1.1345	1.1177	1.1571	1.2215
6.20	1.1449	1.1223	1.1681	1.2329
6.40	1.1574	1.1258	1.1775	1.2418
6.60	1.1690	1.1304	1.1868	1.2496
6.80	1.1802	1.1373	1.1947	1.2552
7.00	1.1904	1.1470	1.2005	1.2579
7.20	1.1988	1.1578	1.2042	1.2580
7.40	1.2055	1.1669	1.2058	1.2553
7.60	1.2101	1.1746	1.2052	1.2498
7.80	1.2128	1.1791	1.2024	1.2418
8.00	1.2124	1.1861	1.1968	1.2303
8.20	1.2113	1.1987	1.1907	1.2179
8.40	1.2151	1.2099	1.1888	1.2105
8.60	1.2178	1.2240	1.1863	1.2077
8.80	1.2222	1.2403	1.1890	1.2101
9.00	1.2365	1.2641	1.1985	1.2210
9.20	1.2619	1.2955	1.2116	1.2309
9.40	1.2876	1.3213	1.2264	1.2355
9.60	1.3082	1.3472	1.2366	1.2535
9.80	1.3286	1.3700	1.2459	1.2763
10.00	1.3447	1.3893	1.2583	1.2956
10.20	1.3563	1.4094	1.2713	1.3132
10.40	1.3807	1.4303	1.2819	1.3279
10.60	1.4039	1.4482	1.2897	1.3397
10.80	1.4268	1.4696	1.2968	1.3485
11.00	1.4465	1.4929	1.2992	1.3530
11.20	1.4459	1.5010	1.2915	1.3493
11.40	1.3953	1.4617	1.2726	1.3291
11.60	1.3522	1.4154	1.2451	1.3008
11.80	1.3473	1.4086	1.2201	1.2752
12.00 (core top)	1.3404	1.3905	1.1852	1.2394

Note: W(Z) values at 20000 MWD/MTU may be applied to cycle burnups greater than 20000 MWD/MTU to prevent W(Z) function extrapolation

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Table 2.6.2.b				
W(Z) versus Core Height for Expanded AFD Acceptable Operation Limits in Figure 2.8.1.b (Top and Bottom 8% Excluded per Braidwood SR 3.2.1.2 Bases)				
Height (feet)	150 MWD/MTU	3000 MWD/MTU	14000 MWD/MTU	20000 MWD/MTU
0.00 (core bottom)	1.3730	1.4662	1.3080	1.3155
0.20	1.3640	1.4549	1.3008	1.3048
0.40	1.3635	1.4501	1.3025	1.3049
0.60	1.3652	1.4493	1.3094	1.3114
0.80	1.3724	1.4514	1.3221	1.3255
1.00	1.3687	1.4417	1.3245	1.3289
1.20	1.3557	1.4238	1.3167	1.3208
1.40	1.3382	1.4012	1.3049	1.3085
1.60	1.3201	1.3772	1.2928	1.2964
1.80	1.3005	1.3513	1.2797	1.2835
2.00	1.2794	1.3235	1.2650	1.2692
2.20	1.2572	1.2946	1.2494	1.2537
2.40	1.2347	1.2654	1.2329	1.2375
2.60	1.2132	1.2367	1.2157	1.2209
2.80	1.1971	1.2064	1.2066	1.2048
3.00	1.1840	1.1872	1.2024	1.1850
3.20	1.1754	1.1798	1.1974	1.1762
3.40	1.1722	1.1738	1.1926	1.1827
3.60	1.1685	1.1690	1.1874	1.1904
3.80	1.1639	1.1633	1.1805	1.1971
4.00	1.1598	1.1591	1.1780	1.2036
4.20	1.1566	1.1564	1.1782	1.2089
4.40	1.1531	1.1526	1.1774	1.2131
4.60	1.1490	1.1481	1.1759	1.2158
4.80	1.1441	1.1430	1.1733	1.2165
5.00	1.1387	1.1370	1.1695	1.2171
5.20	1.1324	1.1304	1.1647	1.2173
5.40	1.1255	1.1230	1.1594	1.2155
5.60	1.1232	1.1145	1.1559	1.2171
5.80	1.1286	1.1132	1.1588	1.2259
6.00	1.1359	1.1178	1.1704	1.2396
6.20	1.1476	1.1223	1.1832	1.2530
6.40	1.1617	1.1257	1.1936	1.2633
6.60	1.1745	1.1320	1.2019	1.2706
6.80	1.1857	1.1397	1.2080	1.2750
7.00	1.1965	1.1484	1.2118	1.2762
7.20	1.2059	1.1579	1.2131	1.2743
7.40	1.2135	1.1664	1.2120	1.2693
7.60	1.2190	1.1739	1.2086	1.2614
7.80	1.2226	1.1788	1.2013	1.2488
8.00	1.2231	1.1861	1.1958	1.2382
8.20	1.2227	1.1982	1.1950	1.2325
8.40	1.2273	1.2095	1.1929	1.2247
8.60	1.2337	1.2235	1.1936	1.2235
8.80	1.2421	1.2405	1.1997	1.2231
9.00	1.2586	1.2650	1.2120	1.2204
9.20	1.2848	1.2963	1.2263	1.2195
9.40	1.3047	1.3220	1.2359	1.2276
9.60	1.3250	1.3479	1.2454	1.2328
9.80	1.3399	1.3705	1.2518	1.2463
10.00	1.3582	1.3897	1.2555	1.2668
10.20	1.3890	1.4097	1.2601	1.2830
10.40	1.4177	1.4305	1.2641	1.2971
10.60	1.4436	1.4480	1.2676	1.3091
10.80	1.4651	1.4690	1.2747	1.3195
11.00	1.4815	1.4921	1.2806	1.3236
11.20	1.4807	1.5000	1.2774	1.3164
11.40	1.4279	1.4605	1.2615	1.2968
11.60	1.3836	1.4141	1.2363	1.2689
11.80	1.3787	1.4071	1.2129	1.2441
12.00 (core top)	1.3720	1.3887	1.1801	1.2093

Note: W(Z) values at 20000 MWD/MTU may be applied to cycle burnups greater than 20000 MWD/MTU to prevent W(Z) function extrapolation

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Table 2.6.2.c Penalty Factors in Excess of 2%	
Cycle Burnup (MWD/MTU)	Penalty Factor $F^c_q(z)$
0	1.0200
150	1.0800
371	1.0810
593	1.0800
844	1.0770
1257	1.0585
1478	1.0455
1921	1.0325
2142	1.0310
3028	1.0200
5905	1.0200
6549	1.0310
6791	1.0290
7253	1.0260
7676	1.0200
8340	1.0200
8562	1.0265
9150	1.0281
10333	1.0255
10997	1.0200

Notes:

Linear interpolation is adequate for intermediate cycle burnups.

All cycle burnups outside the range of Table 2.6.2.c shall use a 2% penalty factor for compliance with the 3.2.1.2 Surveillance Requirements.

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2.7 Nuclear Enthalpy Rise Hot Channel Factor ($F_{\Delta H}^N$) (LCO 3.2.2)

2.7.1 $F_{\Delta H}^N \leq F_{\Delta H}^{RTP} [1.0 + PF_{\Delta H}(1.0 - P)]$

where: P = the ratio of THERMAL POWER to RATED THERMAL POWER (RTP)

$F_{\Delta H}^{RTP} = 1.70$

$PF_{\Delta H} = 0.3$

2.7.2 Uncertainty:

The uncertainty, $U_{F\Delta H}$, to be applied to the Nuclear Enthalpy Rise Hot Channel Factor $F_{\Delta H}^N$ shall be calculated by the following formula:

$U_{F\Delta H} = U_{F\Delta Hm}$

where:

$U_{F\Delta Hm} = \text{Base } F_{\Delta H}^N \text{ measurement uncertainty} = 1.04 \text{ when PDMS is inoperable}$
($U_{F\Delta Hm}$ is defined by PDMS and cannot be less than 1.04 when OPERABLE.)

2.7.3 PDMS Alarms:

$F_{\Delta H}^N$ Warning Setpoint = 2% $F_{\Delta H}^N$ Margin

$F_{\Delta H}^N$ Alarm Setpoint = 0% $F_{\Delta H}^N$ Margin

2.8 AXIAL FLUX DIFFERENCE (AFD) (LCO 3.2.3)

2.8.1 The AXIAL FLUX DIFFERENCE (AFD) Acceptable Operation Limits are provided in the Figures described below.

- a) Figure 2.8.1.a is the Normal AFD Acceptable Operation Limits associated with the W(Z) values in Table 2.6.2.a. Prior to changing to Figure 2.8.1.a, confirm that the plant is within the specified AFD envelope.
- b) Figure 2.8.1.b is the Expanded AFD Acceptable Operation Limits associated with the W(Z) values in Table 2.6.2.b.

2.9 Departure from Nucleate Boiling Ratio (DNBR) (LCO 3.2.5)

2.9.1 $DNBR_{APSL} \geq 1.563$

The Axial Power Shape Limiting DNBR ($DNBR_{APSL}$) is applicable with THERMAL POWER $\geq 50\%$ RTP when PDMS is OPERABLE.

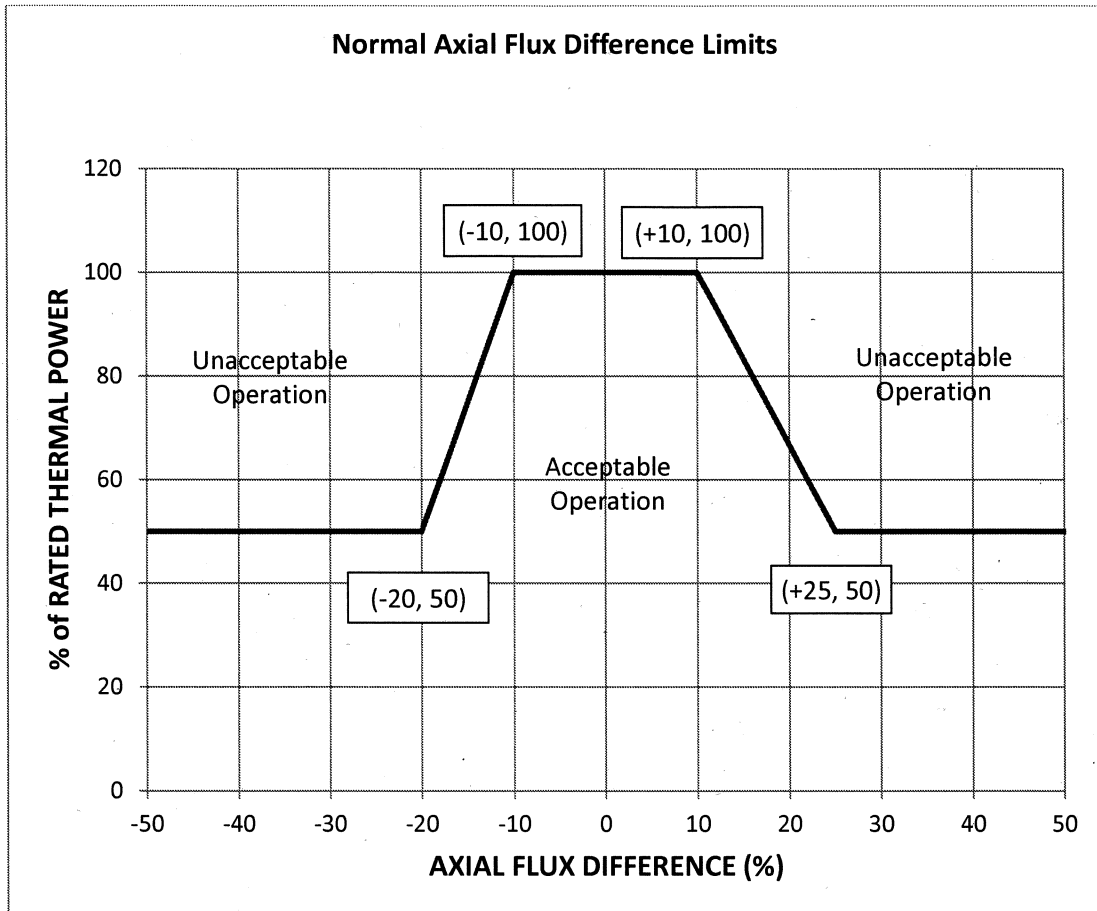
2.9.2 PDMS Alarms:

DNBR Warning Setpoint = 2% DNBR Margin

DNBR Alarm Setpoint = 0% DNBR Margin

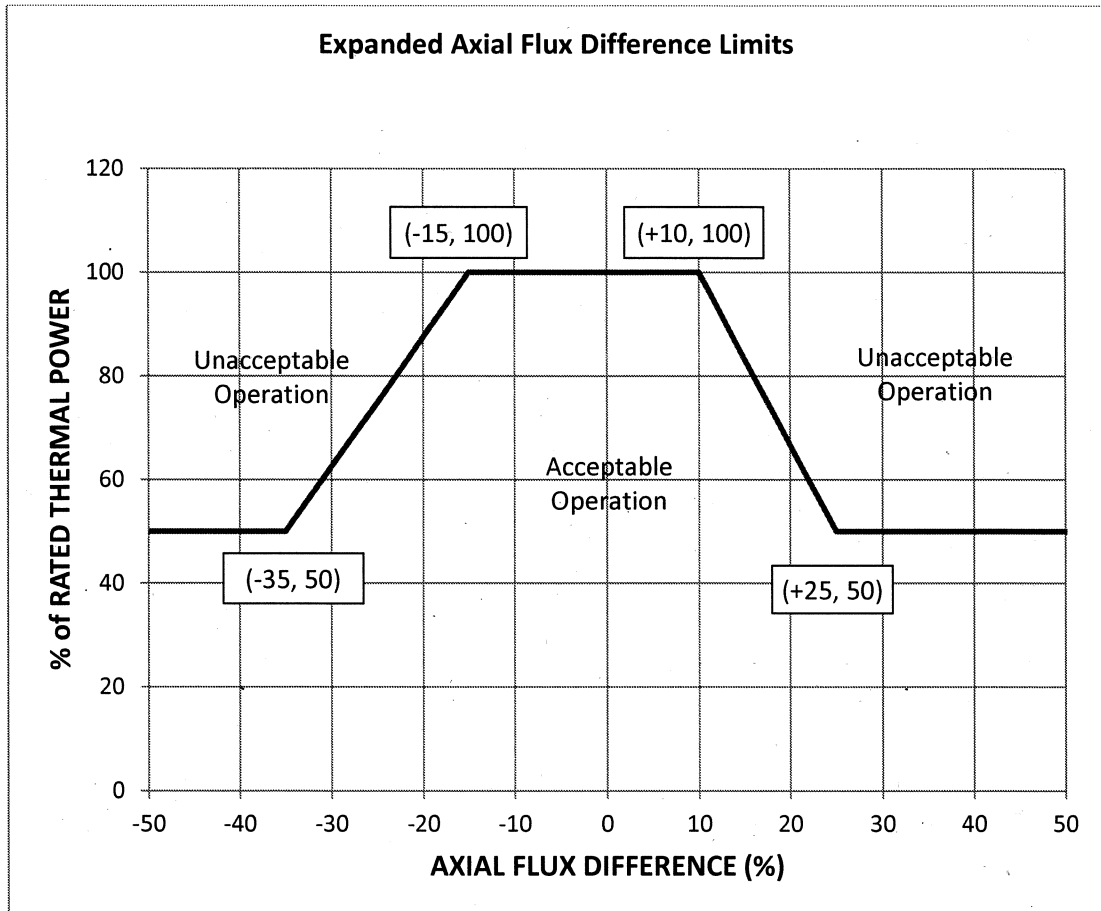
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Figure 2.8.1.a:
Normal Axial Flux Difference Limits
as a Function of Rated Thermal Power



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Figure 2.8.1.b:
Expanded Axial Flux Difference Limits
as a Function of Rated Thermal Power



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2.10 Reactor Trip System (RTS) Instrumentation (LCO 3.3.1) - Overtemperature ΔT Setpoint Parameter Values

- 2.10.1 The Overtemperature ΔT reactor trip setpoint K_1 shall be equal to 1.325.
- 2.10.2 The Overtemperature ΔT reactor trip setpoint T_{avg} coefficient K_2 shall be equal to 0.0297 / $^{\circ}F$.
- 2.10.3 The Overtemperature ΔT reactor trip setpoint pressure coefficient K_3 shall be equal to 0.00135 / psi.
- 2.10.4 The nominal T_{avg} at RTP (indicated) T' shall be less than or equal to 583.5 $^{\circ}F$.
- 2.10.5 The nominal RCS operating pressure (indicated) P' shall be equal to 2235 psig.
- 2.10.6 The measured reactor vessel ΔT lead/lag time constant τ_1 shall be equal to 8 sec.
- 2.10.7 The measured reactor vessel ΔT lead/lag time constant τ_2 shall be equal to 3 sec.
- 2.10.8 The measured reactor vessel ΔT lag time constant τ_3 shall be less than or equal to 2 sec.
- 2.10.9 The measured reactor vessel average temperature lead/lag time constant τ_4 shall be equal to 33 sec.
- 2.10.10 The measured reactor vessel average temperature lead/lag time constant τ_5 shall be equal to 4 sec.
- 2.10.11 The measured reactor vessel average temperature lag time constant τ_6 shall be less than or equal to 2 sec.
- 2.10.12 The $f_1(\Delta I)$ "positive" breakpoint shall be +10% ΔI .
- 2.10.13 The $f_1(\Delta I)$ "negative" breakpoint shall be -18% ΔI .
- 2.10.14 The $f_1(\Delta I)$ "positive" slope shall be +3.47% / % ΔI .
- 2.10.15 The $f_1(\Delta I)$ "negative" slope shall be -2.61% / % ΔI .

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2.11 Reactor Trip System (RTS) Instrumentation (LCO 3.3.1) - Overpower ΔT Setpoint Parameter Values

- 2.11.1 The Overpower ΔT reactor trip setpoint K_4 shall be equal to 1.072.
- 2.11.2 The Overpower ΔT reactor trip setpoint T_{avg} rate/lag coefficient K_5 shall be equal to 0.02 / °F for increasing T_{avg} .
- 2.11.3 The Overpower ΔT reactor trip setpoint T_{avg} rate/lag coefficient K_5 shall be equal to 0 / °F for decreasing T_{avg} .
- 2.11.4 The Overpower ΔT reactor trip setpoint T_{avg} heatup coefficient K_6 shall be equal to 0.00245 / °F when $T > T''$.
- 2.11.5 The Overpower ΔT reactor trip setpoint T_{avg} heatup coefficient K_6 shall be equal to 0 / °F when $T \leq T''$.
- 2.11.6 The nominal T_{avg} at RTP (indicated) T'' shall be less than or equal to 583.5 °F.
- 2.11.7 The measured reactor vessel ΔT lead/lag time constant τ_1 shall be equal to 8 sec.
- 2.11.8 The measured reactor vessel ΔT lead/lag time constant τ_2 shall be equal to 3 sec.
- 2.11.9 The measured reactor vessel ΔT lag time constant τ_3 shall be less than or equal to 2 sec.
- 2.11.10 The measured reactor vessel average temperature lag time constant τ_6 shall be less than or equal to 2 sec.
- 2.11.11 The measured reactor vessel average temperature rate/lag time constant τ_7 shall be equal to 10 sec.
- 2.11.12 The $f_2(\Delta I)$ "positive" breakpoint shall be 0 for all ΔI .
- 2.11.13 The $f_2(\Delta I)$ "negative" breakpoint shall be 0 for all ΔI .
- 2.11.14 The $f_2(\Delta I)$ "positive" slope shall be 0 for all ΔI .
- 2.11.15 The $f_2(\Delta I)$ "negative" slope shall be 0 for all ΔI .

CORE OPERATING LIMITS REPORT (COLR) for BRAIDWOOD UNIT 2 CYCLE 23

2.12 Reactor Coolant System (RCS) Pressure, Temperature, and Flow Departure from Nucleate Boiling (DNB) Limits (LCO 3.4.1)

2.12.1 The pressurizer pressure shall be greater than or equal to 2209 psig.

2.12.2 The RCS average temperature (T_{avg}) shall be less than or equal to 588.6 °F.

2.12.3 The RCS total flow rate shall be greater than or equal to 386,000 gpm.

2.13 Boron Concentration

2.13.1 The refueling boron concentration shall be greater than or equal to the applicable value given in the Table below (LCO 3.9.1). The reported "prior to initial criticality" value also bounds the end-of-cycle requirements for the previous cycle.

2.13.2 To maintain $k_{eff} \leq 0.987$ with all shutdown and control rods fully withdrawn in MODES 3, 4, or 5 (TRM TLCO 3.1.g Required Action B.2 and TRM TLCO 3.1.k.2), the Reactor Coolant System boron concentration shall be greater than or equal to the applicable values given in the Table below.

COLR Section	Conditions	Boron Concentration (ppm)
2.13.1	a) prior to initial criticality	1755
	b) for cycle burnups ≥ 0 MWD/MTU and < 16000 MWD/MTU	1889
	c) for cycle burnups $\geq 16,000$ MWD/MTU	1464
2.13.2	a) prior to initial criticality	1858
	b) for cycle burnups ≥ 0 MWD/MTU and < 16000 MWD/MTU	2123
	c) for cycle burnups ≥ 16000 MWD/MTU	1605