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October 6, 2021

ATTN: Document Control Desk  
Director, Spent Fuel Project Office  
Office of Nuclear Material Safety and Safeguards  
U.S. Nuclear Regulatory Commission  
Washington, DC 20555-0001

Subject: RESPONSE TO REQUEST FOR ADDITIONAL INFORMATION FOR  
REVISION 25 OF THE TRUPACT-II SHIPPING PACKAGE APPLICATION,  
DOCKET NO. 71-9218, AND REVISION 8 OF THE HalfPACT SHIPPING  
PACKAGE APPLICATION, DOCKET NO. 71-9279  
(EPIDS L-2021-LLA-0033 AND L-2021-LLA-0034)

References; 1. Letter from T. E. Sellmer to Document Control Desk dated February 23,  
2021, subject: Revision 25 of the TRUPACT-II Shipping Package  
Application, Docket No. 71-9218, and Revision 8 of the HalfPACT  
Shipping Package Application, Docket No. 71-9279  
2. Letter from T. E. Sellmer to Document Control Desk dated June 24, 2021,  
subject: Amendment to Revision 25 of the TRUPACT-II Shipping  
Package Application, Docket No. 71-9218, and Revision 8 of the  
HalfPACT Shipping Package Application, Docket No. 71-9279 (EPIDS  
L-2021-LLA-0033 AND L-2021-LLA-0034)  
3. Letter from N. Garcia Santos to T. E. Sellmer dated August 11, 2021,  
subject: Application for the Model Nos. TRUPACT-II and HALFPACT  
Transport Packages – Request for Additional Information (EPIDS L-2021-  
LLA-0033 AND L-2021-LLA-0034)

Dear Sir or Madam:

Nuclear Waste Partnership LLC, on behalf of the U.S. Department of Energy (DOE), hereby submits an amendment to Revision 25 of the application for a Certificate of Compliance (CoC) for the TRUPACT-II Packaging, U.S. Nuclear Regulatory Commission (NRC) Docket No. 71-9218, and Revision 8 to the application for a CoC for the HalfPACT Packaging, NRC Docket No. 71-9279 (References 1 and 2). This amendment is in response to the Request for Additional Information (Reference 3) and consists of the following documents:

- TRUPACT-II Safety Analysis Report (SAR), Revision 25
- HalfPACT SAR, Revision 8
- Contact-Handled Transuranic Waste Authorized Methods for Payload Control (CH-TRAMPAC), Revision 6
- CH-TRU Payload Appendices, Revision 5.
- HPT-REP-0001, Revision 1
- SCA-CAL-0005, Revision 0

Individual responses to the RAI are provided in Attachment A. All technical changes added in response to the RAI are indicated by right-bars in the margin of the documents ("|") and are summarized in Attachment B. Right-bars in the margin of the documents ("|") indicating technical changes made to the documents in the original submittal and amendment of this application also have been retained. Revised report HPT-REP-0001 R1 and new calculation SCA-CAL-0005 R0 are provided as discussed in the Attachment A RAI responses.

This submission contains files, one or more of which contains hyperlinks to other files or to Internet websites. These hyperlinks are either inoperable or are not essential to the use of the filing. Any material referenced by hyperlinks to Internet websites that was essential for use of this filing has been submitted as part of the filing. Any material referenced by a hyperlink to another file that was essential for the use of this filing has either been included by reference or submitted as part of this filing.

To facilitate implementation, it is requested that the current package CoCs be valid for use one year from the date of issuance of the revised CoCs.

If you have any questions regarding this submittal, please contact Scott Burns of my staff at (575) 706-7920.

Sincerely,

**TODD SELLMER**  
(Affiliate)

Digitally signed by TODD  
SELLMER (Affiliate)  
Date: 2021.10.06 07:32:33 -06'00'

T. E. Sellmer, Manager  
Packaging and Information Systems

TES:clm

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L. F. Gelder, SRRC  
N. Santos Garcia, USNRC  
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The following table summarizes the components of this submittal. No deviations occur from the NRC-prescribed PDF formatting for the submitted files. Please contact Ms. C. L. Morrison at (505) 350-3693 or [cindy.morrison@wipp.ws](mailto:cindy.morrison@wipp.ws) to resolve any discrepancies in this submittal.

<b>File Name</b>	<b>File Size (MB)</b>	<b>Release Level</b>	<b>Submittal Type</b>
001 Transmittal Letter – October 2021.pdf	1.2	Publicly Available	EIE
002 TRUPACT-II SAR R25 – October 2021.pdf	38.5	Publicly Available	EIE
003 HalfPACT SAR R8 – October 2021.pdf	40.3	Publicly Available	EIE
004 CH-TRAMPAC R6 – October 2021.pdf	6.2	Publicly Available	EIE
005 CH-TRU Payload Appendices R5 – October 2021.pdf	50.8	Publicly Available	EIE
006 HPT-REP-0001 R1	86.8	Publicly Available	EIE
007 SCA-CAL-0005 R0	15.1	Publicly Available	EIE

**Responses to NRC Request for Additional Information (RAI) on Revision 25 of the TRUPACT-II Safety Analysis Report (SAR), Revision 8 of the HalfPACT SAR, Revision 6 of the Contact-Handled Transuranic Waste Authorized Methods for Payload Control (CH-TRAMPAC), and Revision 5 of the CH-TRU Payload Appendices**

**STRUCTURAL EVALUATION (St)**

RAI-St-1 Pertaining to SC-30G2, SC-30G3, SC-55G1, and SC-55G2, the application states that the SC-30G1 was previously approved based on 4-foot (4-ft) drop tests for normal conditions of transport (NCT) and 30-foot (30-ft) drop tests for hypothetical accident condition (HAC). Provide the following information:

- a. Clarify whether the 4-ft drop test was conducted on the SC-55G1 version under NCT. If tests were performed, provide the test results. If the 4-ft drop test was not performed, demonstrate that the SC-55G1 shielded canister meets the 4-ft drop NCT requirement (e.g., show that the 4-ft drop test performed on other shielded canister bounds the SC-55G1 shielded canister or perform the test and provide the results).

The report HPT-REP-0001, "Regulatory Hypothetical accident Condition Type B testing for the HalfPACT Shielded Container Payload," Revision 0, page 2, states that 4-ft drop tests were performed for all four new versions of the shielded canisters. On page 2, the report states that the 4-ft drop test and the 30-ft drop test were conducted for the SC-30G3 and the SC-55G1 versions of the canisters for HAC, but other sections of the report (e.g., page 30) do not state that a 4-ft drop test was conducted. Similarly, the report CH-TRU on page 4.9-5 does not state that a 4-ft drop test was conducted for SC55G1.

- b. Clarify whether the SC-30G2 was only tested for the 4-ft drop test. Justify why the 4-ft drop tests are an adequate means to demonstrate acceptability of the HAC 30-ft drop tests for the package with the new contents.

It appears that in the discussion in the report HPT-REP-0001, Section 7.1.4, "SC-30G2 and SC-55G2 Evaluation," states that the 4-ft drop test was credited to demonstrate acceptable performance of the 30-ft drop test for HAC. However, on Section 5.1.1, "SC-30G2 Payload Assembly vs. SC-55G1 Payload Assembly," it appears to state that no testing was performed on the SC-30G2 shielded canister.

- c. Clarify what is intended by the term "informally" in the report HPT-REP-0001 excerpt. If the term "informally" means that the accelerometer was not calibrated or otherwise qualified for testing, then justify why the comparison of the test results is valid.

## ATTACHMENT A – Responses to RAI

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In the report, HPT-REP-0001 Section 7.1.1, “SC-30G3 Impact Acceleration Comparison,” the applicant stated that “the SC-30G3 will be used for direct comparison of 30-ft protected versus 4-ft unprotected bottom and side drops. Informally [bolded for emphasis], an information only uniaxial accelerometer was installed on SC-30G3 18TU-04 (the test unit used for Type B HAC drop testing).”

Revision 8 of the application for the HalfPACT package references report CH-TRU, “Payload Appendices”, Revision 5, and the CH-TRU report references Report HPT-REP-0001. In these reports, the applicant discusses the methodology to qualify the shielded canisters included as part of the amendment request. The applicant refers in various instances to a 4-ft drop test performed for NCT (e.g., Type A tests) that is used to support the qualification of canisters. The applicant also discusses the 30-ft drop tests for HAC (e.g., Type B package tests).

The staff needs this information to determine compliance with the requirements in Title 10 of the Code of Federal Regulations Section 71.71(c) [10 CFR 71.71(c)] and 10 CFR 71.73(c).

### **Response:**

Drop test report HPT-REP-0001, Rev. 0, submitted on February 23, 2021 as attachment 008 used to develop the RAIs has been revised to Rev. 1. The responses below where referenced (RAI-St-1 and RAI-Sh-8) are based on the updated HPT-REP-0001, Rev. 1, attached in the RAI response submittal.

As discussed in Section 1.2 of drop test report HPT-REP-0001, Rev. 1, both DOT-7A Type A 4-foot drop tests and Type B HAC 30-foot drop tests were performed for the previously approved SC-30G1. The DOT-7A Type A 4-foot free drop tests were performed to meet the requirements of 49 CFR §173.465(c). For clarification, these are 4-foot drops of bare (unprotected) shielded containers that are not inside a HalfPACT package with its protective internal dunnage, and not the requisite NCT 3-foot package drops that are performed on the TRUPACT-II and HalfPACT packages per 10 CFR §71.71(c).

- a. DOT-7A Type A 4-foot bare (unprotected) free drop tests were performed on all four shielded container designs to meet the requirements of 49 CFR §173.465(c). The HPT-REP-0001 example text (pages 2 and 30) cited by RAI-St-1(a) pertains to the HAC Type B 30-foot package drops. The bare (unprotected) DOT-7A Type A 4-foot drop test results for the SC-55G1 are presented in Section 6.1.2 of HPT-REP-0001, Rev. 1.
- b. The SC-30G2 and SC-55G2 were only tested for the bare (unprotected) DOT-7A Type A 4-foot drops. HAC Type B 30-foot drop tests were only performed for the SC-30G3 and SC-55G1 designs because the SC-30G3 and SC-55G1 payload assemblies, and associated packaging dunnage components, are more damaging to the ICV structure than the SC-55G2

and SC-30G2 designs, respectively. Justification for performing the HAC Type B 30-foot drop tests for these bounding designs is provided in Section 5.1 of HPT-REP-0001. For convenience, Table 1 summarizes the tested configurations for the four shielded container designs, and has been added to Section 1.2 of HPT-REP-0001, Rev. 1, for clarity.

**Table 1** – Summary of Shielded Container Type A and Type B Testing

Drop Test	Shielded Container Test Unit 18-TUXX <sup>1</sup>			
	SC-30G2	SC-30G3	SC-55G1	SC-55G2
Type A – 4' CG Over Corner	01	03	06	09
Type A – 4' Flat Bottom End	01	03	—	09
Type A – 4' Near-Vertical Lid	02	05	06	10
Type A – 4' Flat Side	02	05	—	10
Type B – 30' Flat Bottom End	—	04	07 & 08	—
Type B – 30' Flat Side	—	04	07 & 08	—

1. "XX" defines the test unit number, e.g., 18-TU01, 18-TU02, etc.

The basis for acceptance of the SC-30G2 and SC-55G2 designs is that physical damage to shielded containers caused by the DOT-7A Type A 4-foot bare drop tests is worse than physical damage to shielded containers caused by HAC Type B 30-foot protected (by foam-filled dunnage) drop tests within the HalfPACT package assembly. Comparison of physical damage to the tested shielded containers from the original SC-30G1 tests as well from the new SC-30G3 and SC-55G1 tests validate this assertion. Therefore, demonstrating that the SC-30G2 and SC-55G2 designs successfully passed the bounding DOT-7A Type A 4-foot drop tests of bare shielded containers ensures that they would also pass the HAC Type B 30-foot drop tests of protected shielded containers within the HalfPACT package. The HAC Type B 30-foot drops demonstrated that the foam-filled dunnage within the bounding payload assembly configurations protected the ICV from internal damage due to the shielded containers.

- c. The term "informally" was intended to denote the use of a currently uncertified accelerometer (i.e., the accelerometer's certification was expired, and certifying agencies were not available last summer due to COVID-19 closures). The data collected from the use of the uniaxial accelerometer is not the basis for regulatory compliance. The accelerometer data provides additional evidence that corroborates the documented post-test inspections confirming there was no loss of confinement of fluorescein dye from the payloads and the visual comparison of physical damage to shielded containers subject to bare DOT-7A Type A 4-foot drops and those subject to dunnage-protected HAC 30-foot drops. Section 7.0 of HPT-REP-0001, Rev. 1, has been revised to clarify the use of this information. Accelerometer data supports

what was observed from drop testing, i.e., that bare 4-foot drops were more damaging to the shielded containers than dunnage-protected 30-foot drops.

### SHIELDING EVALUATION (Sh)

RAI-Sh-1 Clarify, with justifications, how the uncertainties in the source intensity, source term geometric distribution, and the density correction factors (DFCs) were considered in the calculations of the dose rates and revise the allowable contents as necessary to meet the dose rate limits.

Sections 5.5.6, 5.5.7, 5.5.8, and 5.5.9 of Revision 25 of the TRUPACT-II application provide information on the allowable source intensity, source term geometric distribution, and the DFCs. However, it is not clear whether the uncertainties in these parameters have been considered in determining the maximum allowable activity for each of the containers with the targeted dose rate limit.

The staff needs this information to determine compliance with the requirements in 10 CFR 71.47.

#### **Response:**

All calculations used to determine activity limits and density correction factors (DCF) are based on an adjusted dose rate ( $D_a$ ) that is equal to the Monte Carlo N-Particle (MCNP) calculated dose rate ( $D_c$ ) plus the tally error ( $E$ ), i.e., one standard deviation, as follows:

$$D_a = D_c(1 + E)$$

To account for uncertainties in the payload activity assay evaluation, Section 3.3.1.1 of the *Contact-Handled Transuranic Waste Authorized Methods for Payload Control* (CH-TRAMPAC) includes the following requirement:

“Each payload shall be acceptable for shipment only if the determined activity plus the error (i.e., one standard deviation) meets the specific limit as determined by the procedure provided in Section 5.5.10 of the TRUPACT-II SAR.”

With reference to Section 5.5.10 of the TRUPACT-II SAR, the default payload configuration from a shielding standpoint conservatively assumes a point source. If, however, a waste form can be shown to meet the requirements for “distributed throughout” from NUREG-1608, then the activity limits for the distributed source model, in conjunction with the appropriate DCF for gamma-emitting radionuclides, may be used; neutron bearing wastes do not utilize a DCF for distributed source models. Uncertainties in the calculated DCFs were considered by conservatively implementing a DCF curve-fit utilizing the minimum DCFs calculated over a range of gamma energies as a function of

source density that utilizes zirconium as a conservative basis for self-shielding material in the distributed source region.

To account for other uncertainties in source intensity and/or source term geometric distribution, Section 5.5.10 of the TRUPACT-II SAR and correspondingly Section 3.3.2.1 of the CH-TRAMPAC apply a 10% administrative margin to the calculated activity limit, where the combined sum of partial fractions for the gamma and neutron source terms present in the package must be less than or equal to 0.9.

RAI-Sh-2 Provide the maximum size of the solid-large objects, for each of the categories of the contents as specified in “Contact-Handled Transuranic Waste Authorized

Methods for Payload Control” (CH-TRAMPAC) (ADAMS Accession No. ML21054A054) Revision 6, (ADAMS Accession No. ML21054A054) and clarify which shielding analyses supports the large objects.

CH-TRAMPAC, Revision 6, Table 2.9-49, Table 2.9-53, Table 2.9-57, and Table 2.9-61 identifies three forms of authorized contents for the SC-30G2, SC-55G1, and SC-55G1 containers. The three forms include the following:

1. solids, any particle size (e.g., fine powder or inorganic particulates),
2. large particle size (e.g., sand, concrete, or debris), and
3. large objects (e.g., metal cans containing waste).

However, it is not clear how to distinguish what constitutes a large object and particle of any size. Also, it is not clear how these definitions of the sizes of the particles or objects are related to the shielding models of distributed or concentrated sources in the package.

The staff needs this information to determine compliance with the requirements in 10 CFR 71.33(b)(3), 10 CFR 71.47, and 10 CFR 71.51.

### **Response:**

Table 2.9-41, Table 2.9-49, Table 2.9-53, Table 2.9-57, and Table 2.9-61 of the CH-TRAMPAC identify material content forms authorized for transport within each of the five shielded container designs (i.e., the currently licensed SC-30G1, and the new SC-30G2, SC-30G3, SC-55G1, and SC-55G2, respectively). Each waste form must be accordingly loaded within a 30-gallon or 55-gallon waste drum.

The term “particle size” is used comparatively in CH-TRAMPAC Section 2.9 to broadly differentiate physical forms as powder/particulate (as present in sludge or solidified waste) or debris; it is not quantitative. The first waste form, “solids, any particle size,” generically refers to relatively uniform solid waste material such as fine powders, ash, oxides, and cements. The second



waste form, “large particle size,” generically refers to non-uniform waste material such as sands, concrete, and random-sized debris. Finally, the third waste form, “large objects,” generically refers to waste material packed within inner metal containers, and may be as large as the 30-gallon or 55-gallon waste drum’s cavity allows. However, as shown in the subsequent paragraph, the precise waste form is generally unimportant from a shielding evaluation standpoint.

Material content forms from Section 2.9 of CH-TRAMPAC are not used in the determination of source term distribution or related in any way to shielding model inputs.

With reference to Section 5.5.10 of the TRUPACT-II SAR, the default payload configuration from a shielding standpoint conservatively assumes a point source; thus, the physical waste form becomes unimportant because source self-shielding is not relevant for gamma-emitting radionuclides, and the container materials of construction make them essentially transparent to neutron-emitting radionuclides. If a payload of containers can be shown to meet the requirements for “distributed throughout” from NUREG-1608, then the activity limits for the distributed source model, in conjunction with the appropriate density correction factor (DCF) for gamma-emitting radionuclides, may be used.

RAI-Sh-3 Explain why the density correction factors (DCFs) for SC-30G3 and SC-55G1 are identical.

The application shows that the equations for the self-shielding factor DCFs of the SC-30G3 and SC-55G1 are identical. Specifically, the application presents these polynomial equations as:

$$DCF_{SC-30G3} = 0.0051 \cdot p^3 - 0.0987 \cdot p^2 + 0.8030 \cdot p + 0.2342,$$

$$DCF_{SC-55G1} = 0.0051 \cdot p^3 - 0.0987 \cdot p^2 + 0.8030 \cdot p + 0.2342$$

However, it is not clear why they behave the same since these two containers have different shielding designs and source term limits as shown in Tables 5.5-18 to 5.5-21.

The staff needs this information to determine compliance with the requirements of 10 CFR 71.47 and 10 CFR 71.51.

### **Response:**

As identified by RAI-Sh-3, the DCF equation for the SC-55G1 was incorrect in the application. Section 5.5.8 of the TRUPACT-II SAR has been revised to present the following corrected DCF equation for the SC-55G1.

$$DCF_{SC-55G1} = 0.0024 \cdot p^3 - 0.0668 \cdot p^2 + 0.7557 \cdot p + 0.2630$$

## ATTACHMENT A – Responses to RAI

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RAI-Sh-4 Add the steps listed in Section 5.5.10 to the Chapter 7 of the safety analysis report (SAR) as part of the instructions for determining the allowable contents.

Section 5.5.10, “Determination of Acceptable Activity,” of the TRUPACT-II SAR provides a list of the steps for determining the allowable quantity of the wastes based on their radioactive characteristics. These steps/instructions form the basis for determining the maximum allowable contents and should be part of the loading instructions.

The staff needs this information to determine compliance with the requirements in 10 CFR 71.33(b)(1), 10 CFR 71.43(f), 10 CFR 71.47, 10 CFR 71.51, and 10 CFR 71.87(a).

### **Response:**

The TRUPACT-II and HalfPACT Certificates of Compliance as well as Section 7.1.4 of the TRUPACT-II and HalfPACT SARs specify the use of the *Contact-Handled Transuranic Waste Authorized Methods for Payload Control* (CH-TRAMPAC) for determining allowable contents. Section 3.3.1.1 of the CH-TRAMPAC includes the following requirement:

“Each payload shall be acceptable for shipment only if the determined activity plus the error (i.e., one standard deviation) meets the specific limit as determined by the procedure provided in Section 5.5.10 of the TRUPACT-II SAR.”

Chapter 7 of the TRUPACT-II and HalfPACT SARs – the procedural instructions for operational loading of a payload assembly into a packaging – specifies that a payload configuration has been properly prepared per the requirements of CH-TRAMPAC. Prior to assembling a payload for loading into a package, Section 6.2.2 of CH-TRAMPAC requires a Transportation Certification Official to comply with Section 3.3 of CH-TRAMPAC. As discussed above, Section 3.3.1.1 of CH-TRAMPAC requires compliance determination as described in Section 5.5.10 of the TRUPACT-II SAR. Therefore, the steps listed in Section 5.5.10 of the TRUPACT-II SAR are included in Chapter 7 of the SARs because Chapter 7 requires compliance with CH-TRAMPAC.

RAI-Sh-5 Demonstrate there are no significant secondary gammas or neutrons from the package or provide control measures to ensure that there will be no significant (n, gamma) or (gamma, n) reactions in the TRU wastes.

Page 5.3-27 of the TRUPACT-II application states the following:

“Combined photon/neutron mode evaluations were not employed for the neutron analyses as multiple test runs demonstrated that the gamma dose rate due to the interaction of neutrons in the shielding materials contributes a statistically insignificant (<1%) change in the dose rate as compared to the neutron dose rate.”

However, it is not clear what the multiple runs were referred to. If the term “run” is related to the MCNP model calculation, the secondary gammas or neutrons in the TRU contents would not be captured in the analyses because the definition of the material in the sample MCNP input, as provided in the application, for the content does not include the TRU isotopes as defined in the Department of Energy’s Environmental Impact Statements (DOE 2016). The (n, gamma) and (gamma, n) reactions in the TRU wastes are well understood physical phenomena (McNair, 2019). The MCNP models can only capture the secondary gamma and neutrons when the material compositions for the TRU contents are explicitly defined in the material cards.

The staff needs this information to determine compliance with the requirements in 10 CFR 71.47 and 10 CFR 71.51.

### References:

1. Department of Energy, “Final Environmental Impact Statement for the Disposal of Greater-Than-Class C (GTCC) Low-Level Radioactive Waste and GTCC-Like Waste (DOE/EIS-0375),” Department of Energy, January 2016.
2. Carson R McNair, “Characterization techniques for TRU waste from the Analytical Laboratory Hot Cells at Idaho National Laboratory,” Idaho National Laboratory, March 2019.

### **Response:**

As correctly stated in RAI-Sh-5, the determination that secondary gamma production from neutrons is statistically insignificant relates only to neutron interaction with the materials of construction for the shielded containers proper. It is asserted that any dose rate increases due to secondary gamma production from neutron interaction with waste material contents is concurrently associated with a more dominant effect of neutron attenuation due to self-shielding (which is not credited for neutrons in either concentrated or distributed waste form activity limits). This assertion was again tested and affirmed via a supplemental series of calculations described below.

To increase neutron capture and corresponding secondary gamma production, the entire shielded container payload cavity was filled with polyethylene with a density of 0.94 g/cc. The SC-30G3 and SC-55G1, which are associated with the greatest and least gamma shielding, respectively, were modeled to encompass the four new shielded container designs.

Two MCNP analyses were run for the SC-30G3 and for the SC-55G1, i.e., NCT and HAC with a concentrated  $^{252}\text{Cf}$  neutron source. With the exception of placing polyethylene in the payload cavities and adding photon measurement for the tally regions, the MCNP models are identical to those used to develop Tables 5.4-13 (SC-30G3) and 5.4-14 (SC-55G1) of the TRUPACT-II SAR. For

## ATTACHMENT A – Responses to RAI

completeness, the MCNP output files for the four runs are provided in Attachment RAI-Sh-5, and summarized below in Tables 2 and 3 below.

Self-shielding plays a major role in reducing dose rates such that the activity limits calculated in Tables 2 and 3 are significantly greater than the activity limits determined in Tables 5.4-13 and 5.4-14 of the TRUPACT-II SAR for the SC-30G3 and SC-55G1, respectively. Thus, the presence of a material within the shielded container's payload cavity that could stimulate secondary gamma production also serves to provide self-shielding for the neutron source. In summary, accounting for waste material from a neutron to secondary gamma production perspective results in far less restrictive activity limits than what is presented in the SAR.

**Table 2 – SC-30G3 NCT & HAC Activity Limits with a Polyethylene Payload**

Particle Type	Source Strength (par/s/Ci)	Calculated Dose Rate (mrem/hr / par/s)	Tally Error	Adjusted Dose Rate (mrem/hr / par/s)	Percent of Total Dose Rate	Allowable Dose Rate (mrem/hr)	Allowable Activity (n/s)	Activity Limit (Ci)
<b>NCT - HalfPACT Package Side Surface</b>								
Neutron	3.8322E+09	5.68E-09	0.8%	5.73E-09	95.6%	191.2	3.34E+10	8.716
Gamma	7.3991E+10	2.62E-10	0.9%	2.64E-10	4.4%	8.8	—	—
Total	—	—	—	5.99E-09	100.0%	200.0	—	—
<b>NCT - 2 Meters from HalfPACT Package Side Surface</b>								
Neutron	3.8322E+09	7.15E-10	1.0%	7.22E-10	95.8%	9.6	1.33E+10	3.471
Gamma	7.3991E+10	3.12E-11	1.0%	3.15E-11	4.2%	0.4	—	—
Total	—	—	—	7.54E-10	100.0%	10.0	—	—
<b>HAC - 1 Meter from HalfPACT Package Side Surface</b>								
Neutron	3.8322E+09	5.55E-07	0.2%	5.56E-07	99.4%	994.2	1.79E+09	<b>0.467</b>
Gamma	7.3991E+10	3.24E-09	0.6%	3.26E-09	0.6%	5.8	—	—
Total	—	—	—	5.59E-07	100.0%	1,000.0	—	—

**Table 3 – SC-55G1 NCT & HAC Activity Limits with a Polyethylene Payload**

Particle Type	Source Strength (par/s/Ci)	Calculated Dose Rate (mrem/hr / par/s)	Tally Error	Adjusted Dose Rate (mrem/hr / par/s)	Percent of Total Dose Rate	Allowable Dose Rate (mrem/hr)	Allowable Activity (n/s)	Activity Limit (Ci)
<b>NCT - HalfPACT Package Side Surface</b>								
Neutron	3.8322E+09	5.75E-09	0.8%	5.80E-09	76.8%	153.6	2.65E+10	6.915
Gamma	7.3991E+10	1.75E-09	0.2%	1.75E-09	23.2%	46.4	—	—
Total	—	—	—	7.55E-09	100.0%	200.0	—	—
<b>NCT - 2 Meters from HalfPACT Package Side Surface</b>								
Neutron	3.8322E+09	5.14E-10	1.2%	5.20E-10	73.4%	7.3	1.41E+10	3.679
Gamma	7.3991E+10	1.87E-10	0.3%	1.88E-10	26.6%	2.7	—	—
Total	—	—	—	7.08E-10	100.0%	10.0	—	—
<b>HAC - 1 Meter from HalfPACT Package Side Surface</b>								
Neutron	3.8322E+09	3.83E-07	0.3%	3.84E-07	98.6%	986.4	2.57E+09	<b>0.671</b>
Gamma	7.3991E+10	5.28E-09	0.4%	5.30E-09	1.4%	13.6	—	—
Total	—	—	—	3.89E-07	100.0%	1,000.0	—	—

RAI-Sh-6 Clarify whether the uncertainties associated with the source term calculation and the statistical uncertainty associated with the dose rate calculation have been included in the final dose rates. If they are not, include the uncertainties associated with these calculations and demonstrate that the package meets the regulatory requirements.

The applicant used computer code SOURCES-4A to calculate the specific activity of each of the nuclides provided in the document CH-TRAMPAC. However, it is not clear what are the uncertainties, if any, associated with the source term calculations of the transuranic wastes using the SOURCES-4A computer code. The uncertainties of the source term calculations should include, as a minimum, how the transuranic wastes were produced, i.e., irradiation parameters, such as fluxes and spectra, cooling time, and the uncertainties of these parameters.

The applicant developed a scheme to calculate the allowable activity for the SC-30G1 and the four new containers. The scheme determines the maximum allowable contents by dividing the targeted dose rate by the calculated dose rate per curie of each nuclide in the wastes. Table 5.1-8 to Table 5.1-11 of Revision 25 of the TRUPACT-II application provide the targeted maximum dose rates for the Half-PACT packaging system containing the payloads for the four new containers (SC-30G2, SC-30G3, SC-55G1, and SC-55G2) and Table 5.1-7 provides the revised neutron dose rate for neutron sources for the SC-30G1 container. The dose rates in these tables show that the maximum dose rate is less than one percent (e.g., 9.99 mrem/hr vs. 10 mrem/hr for the SC-30G2 container) within the regulatory limits of 10 CFR 71.47, which is 10 mrem/hr. In addition, the data provided in Table 5.4-12, Table 5.4-13, Table 5.4-14, and Table 5.4-15 show that the statistical errors of the Monte Carlo method used in the shielding analyses are in 0.1% to 0.3% for packages under NCT. Based on the MCNP manual, the error associated tally of MCNP calculation is a percentage of the mean value, thus,  $0.3\% \times 9.99 = 0.02997$ . Considering the statistical error, the actual dose rate could be as high as  $9.99 + 0.02997 = 10.01997$  mrem/hr, which exceeds the regulatory dose rate limit of 10 mrem/hr.

The staff needs this information to determine compliance with the requirements in 10 CFR 71.47.

### **Response:**

The response to RAI-Sh-1 addresses uncertainties associated with source term calculation and the statistical uncertainty associated with the dose rate calculations that are used to determine activity limits.

Per Section 5.2.2 of the TRUPACT-II SAR, the SOURCES-4A computer code was used to generate the neutron source energy spectrum that was used for neutron shielding calculations, and not the specific activities of radionuclides; specific activities are taken from Table 3.1-2 of the CH-TRAMPAC.

## ATTACHMENT A – Responses to RAI

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As stated earlier, all MCNP shielding calculation results that are used to determine activity limits and density correction factors are based on an adjusted dose rate ( $D_a$ ) that is equal to the calculated dose rate ( $D_c$ ) plus the tally error ( $E$ ), i.e., one standard deviation, as follows:

$$D_a = D_c(1 + E)$$

Thus, the tally error is already taken into account for developing the activity limits and is not additive to the dose rates provided in Tables 5.1-8 through 5.1-11 of the TRUPACT-II SAR.

RAI-Sh-7 Justify the assumption for maximizing the distance to the detector for the shielding model for the package under NCT.

On page 5.3-1, the first paragraph the TRUPACT-II SAR states the following:

“NCT assumptions maximize the distance from the source(s) to the nearest detector whereas HAC assumptions minimize the distance from the source(s) to the nearest detector.”

The staff understands the assumption for modeling of the package under HAC. However, it does not understand why the applicant tried to maximize the distance between the source and the detector in the NCT model. This assumption may not be conservative even if the source is homogeneously distributed in the waste.

The staff needs this information to determine compliance with the requirements in 10 CFR 71.47.

### **Response:**

To maximize the distance from the source to the shielded container's surface in all radial directions, the source is located at the shielded container's axial centerline. Given the nature of CH-TRU waste, the expected distribution of waste is such that the average source activity occurs near the center of the payload container. Any potential deviation from its center is captured within the 10% administrative margin that is used to restrict activity limits.

A response to a similar RAI was provided in March 2013 (Letter from T.E. Sellmer to Document Control Desk, dated March 27, 2013, subject: Response to Second Request for Additional Information for Revision 23 of the TRUPACT-II Shipping Package Application, Docket No. 71-9218, TAC No. L24643, and Revision 6 of the HalfPACT Shipping Package Application, Docket NO. 71-9279, TAC NO. L24642). Since the same approved methodology is being implemented for the four new shielded container designs, the previous RAI 5.1 response is still valid.

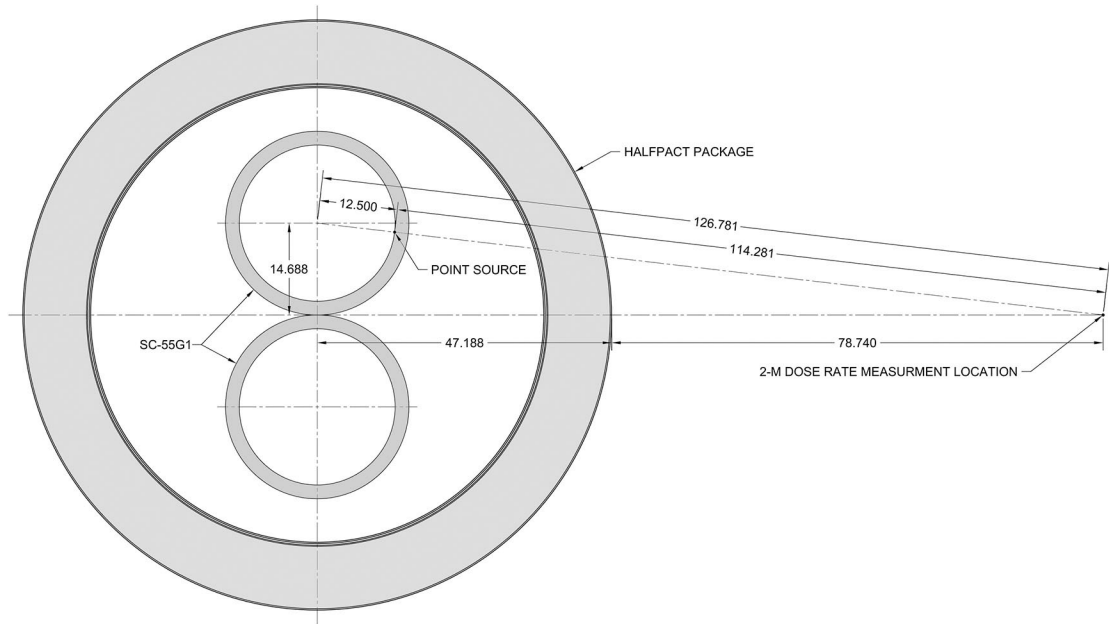
The calculated allowable activity is administratively reduced 10% to address the potential for reconfiguration of source material within shielded containers

under NCT where the combined sum of partial fractions for gamma and neutron source terms are required to be less than or equal to 0.9. As shown below, potential reconfiguration of the source material in the shielded containers under NCT is highly improbable and will not cause a significant change in the limiting package dose rate values. Other potential sources of dose rate increase under NCT are not applicable for shielded containers due to test results indicating no damage to the payload container under those conditions.

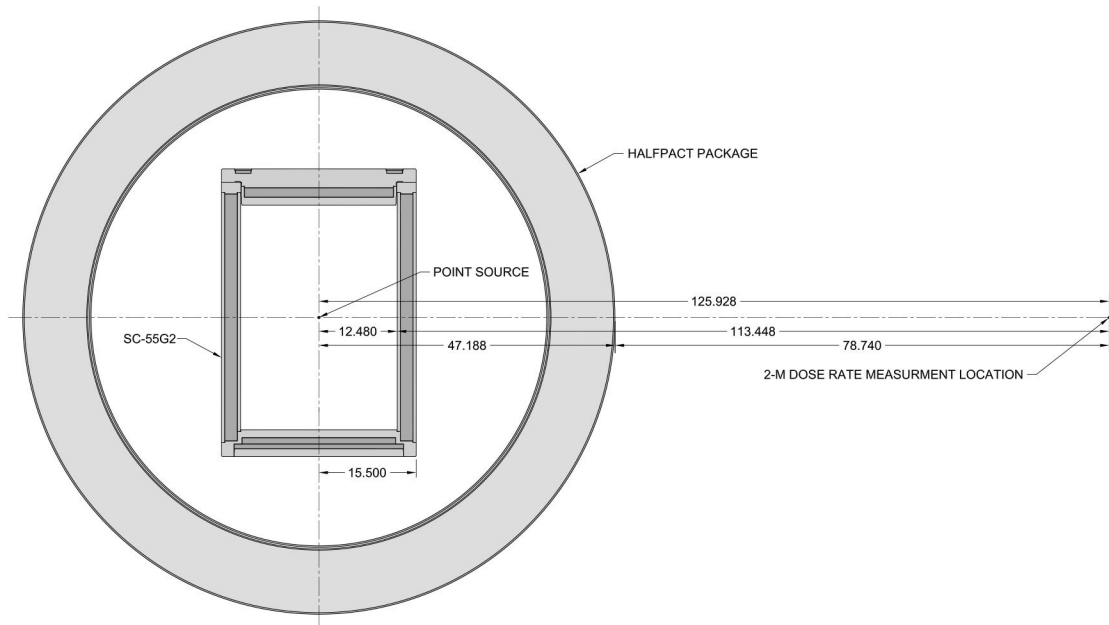
DOE TRU waste packaging guidance and site-specific waste acceptance criteria direct the preparation of CH-TRU waste payload containers to ensure safe and compliant ALARA payload container dose rates during characterization activities, intra-site transport operations, generator site storage, Type B package loading and transport processes, and WIPP repository disposal sequences. By definition, a CH-TRU waste payload container surface dose rate cannot exceed 200 mrem/hr. The CH-TRAMPAC and the WIPP Land Withdrawal Act (Public Law 102-579) impose this payload container surface dose rate requirement. The absence of CH-TRU payload containers exceeding the payload container surface dose rate requirement when surveyed after receipt at WIPP is a strong indicator that dose rate changes during handling and shipment, even at the payload container level, are insignificant. This indicator is important because any change in the payload container surface dose rate translates into a much smaller corresponding change in the limiting 2-meter package dose rate.

Using distance attenuation for the SC-55G1 configuration as an example, where the dose rate is directly proportional to the inverse square of the distance, the limiting dose rate of 10 mrem/hr at a distance 2 meters from the HalfPACT package surface containing two SC-55G1s with initially centered point sources that are unrealistically moved the full radial distance to the SC-55G1's inner shell surface would only increase to  $(126.781/114.281)^2 \times 10 = 12.3$  mrem/hr (see Figure 1). Similarly, the limiting dose rate of 10 mrem/hr at a distance 2 meters from the HalfPACT package surface containing one SC-55G2 with an initially centered point source that is unrealistically moved the full radial distance to the SC-55G2's inner shell surface would only increase to  $(125.928/113.448)^2 \times 10 = 12.3$  mrem/hr (see Figure 2).

Any substantial concentration of sources resulting from movement during transport would be readily observable during receipt inspection of the package, and none has been noted in thousands of CH-TRU waste shipments within the TRUPACT-II and HalfPACT packages.



**FIGURE 1** – HalfPACT Package with Two SC-55G1s; Shifted Point Source



**FIGURE 2** – HalfPACT Package with One SC-55G2; Shifted Point Source

Regardless, the occurrence of shielded containers having initially centered sources with full source reconfiguration to the worst possible location under NCT is not considered a credible scenario. Given the nature of CH-TRU waste, the expected distribution of waste is such that the average source activity occurs near the center of the payload container. Any potential deviation from its center is captured within the 10% administrative margin that is used to restrict activity limits.



RAI-Sh-8 Either demonstrate that lead slump does not occur or provide an analysis of the effect of lead slump on the dose rate at one meter for the damaged package.

In the document titled “CH-TRU Payload Appendices,” Revision 5, the applicant stated in the application that no lead slump occurred by examining the lead layer of the testing unit. However, staff does not find the justification for not evaluating lead slump in the application. The staff notes that lead slump under impact is an unavoidable natural phenomenon and will occur in accordance with the basic physics (G. C. Mok, 1989, Tan, et al, 2017) unless the package is designed such that the shielded containers inside the overpack do not experience any significant impact (g-load) under the drop tests required in 10 CFR 71.73(c)(1), which states the following:

“Free Drop. A free drop of the specimen through a distance of 9 m (30 ft) onto a flat, essentially unyielding, horizontal surface, striking the surface in a position for which maximum damage is expected.”

The staff notes that Figure 4.10-18 – SC-55G2 18TU-10 Cut AM-AN Near Mid-Span shows visible deformation of the lead layer in the middle section of the test unit. The staff also notes that the picture in Figure 7-20 of the document, with document identification number “HPT-REP-0001,” seems to show a void gap at the top end of the lead shield after drop test. These gaps are probable evidence that there will be a loss of lead shield resulting from lead slump. In fact, the gap created by lead slump can be calculated by the differential contraction of the lead layer and the steel shells. If there is not sufficient data to prove lead slump will never occur for this package under HAC, a shielding analysis should be provided assuming there is lead slump under HAC, as predicted using the method in the “Cask Designers Guide” (ORNL, 1970) document. The analysis should also account for any void between the top of the lead shielding and the outer cask top flange resulting from package fabrication. Using analyses for a few radionuclide contents (e.g., Co-60), the applicant may demonstrate that the dose rates for the puncture HAC configuration bound those for the lead slump configuration. In addition, the publication from Sandia National Laboratory, “Dose Estimates in a Loss of Lead Shielding Truck Accident,” clearly indicate that lead slump is a credible condition for transportation package under HAC.

The staff needs this information to determine compliance with the requirements in 10 CFR 71.51.

### References:

1. Lawrence Livermore National Laboratory. G. C. Mok, et al., “The Analysis of Lead Slump Effects in Shipping Casks for Radioactive Materials,” March 1989.

2. Tan, Z., Bernal, S.A., and Provis, J.L., “Reproducible mini-slump test procedure for measuring the yield stress of cementitious pastes,” *Mater Struct* Vol. 50, PP 235, 2017.
3. Oak Ridge National Laboratory. “Cask Designers Guide, A Guide for the Design, Fabrication, and Operation of Shipping Casks for Nuclear Applications,” February 1970.
4. Matthew L. Dennis, Ruth F. Weiner, Douglas M. Osborn, and Terence J. Heames, “Dose estimates in a loss of lead shielding truck accident,” Sandia National Laboratory, August 2009.

### **Response:**

With reference to Figure 7-43 in drop test report HPT-REP-0001, Rev. 1 (Figure 4.10-18 in CH-TRU Payload Appendices), the last paragraph of Section 7.1.3.2 clarifies that the visible deformation at mid-length of SC-55G2 18TU-10 occurred because of a side drop strike on the test rigging’s lifting shackle, not because of lead slump. Therefore, the damage shown in Figure 7-43 at mid-length and Figure 7-34 (not Figure 7-20) at the upper flange end are unrelated.

Axial voids at the ends of the sidewall lead column are shown in HPT-REP-0001, Rev. 1, Figures 6-51 and 6-53 for SC-30G3 18TU-04 that was used for 30-foot HAC drop testing in two orientations (a flat end drop and a flat side drop); Figures 7-18, 7-20, and 7-23 for SC-30G2 18TU-02 that was used for 4-foot Type A drop testing in two orientations (a 10° near-vertical top-down drop and horizontal side drop); and Figure 7-34 for SC-55G2 18TU-09 that was used for bare (unprotected) 4-foot Type A drop testing in two orientations (a center-of-gravity over bottom corner drop and a bottom-down vertical end drop). All axial voids are identified as “cold-shuts” that occurred during the lead pour process. The reasons for this conclusion are summarized below:

1. SC-30G3 18TU-04: The axial void depicted in Figures 6-51 and 6-53 only occurred at the upper step; no void occurred at the lower step. If lead slump had occurred, a void would have been present at both upper and lower steps.
2. SC-30G2 18TU-02: The axial void depicted in Figures 7-18, 7-20, and 7-23 occurred on the second SC-30G2 test unit that was subjected to a 10° near-vertical top-down drop and horizontal side drop. In comparison, SC-30G2 18TU-01 that was subjected to a flat end drop and center-of-gravity-over-corner drop showed no axial void at either end (see Figures 7-13 through 7-16). If lead slump had occurred, SC-30G2 18TU-01 would have exhibited an axial void greater than that observed in SC-30G2 18TU-02.

3. SC-55G2 18TU-09: The axial void depicted in Figure 7-34 occurred on the first SC-55G2 test unit that was subjected to a center-of-gravity over bottom corner drop followed by a flat end drop. The flat end drop should have produced an axisymmetric axial void, yet Figure 7-36 at a cut position 180° from the void shown in Figure 7-34 shows no evidence of lead movement.

Considering all test units, both Type B and Type A, the maximum measured axial void that occurred due to “cold-shuts” was 0.318 inches observed in SC-55G2 18TU-09. To address the effect of axial voids, the SC-30G2, SC-30G3, and SC-55G2 shielding models were modified to include an identical axial gap at both ends of the sidewall lead column; stepped ends included the gap at both steps. This evaluation is included in SCA-CAL-0005, *Effect of Axial Gaps in the SC-30G2, SC30G3, and SC-55G2 Lead Sidewalls* and the results are summarized in new Section 5.4.5, *Evaluation for Axial Gaps in the Sidewall Lead*, of the TRUPACT-II SAR. These models were evaluated for both NCT and HAC.

This evaluation demonstrated that axial gaps as great as 1/2-inch at either the upper or lower end of the sidewall lead column result in a maximum NCT dose rate increase of only 1.01× and a maximum HAC dose rate increase of 1.17×, both associated with the SC-30G2 design (see Table 5.4-16 of the TRUPACT-II SAR). Table 5.4-12 of the TRUPACT-II SAR for the SC-30G2 shows that the HAC activity limit is 9.73× greater than the NCT activity limit. Similarly, Tables 5-4-13 and 5.4-15 of the TRUPACT-II SAR show HAC and NCT activity limit ratios of 3.35× and 4.10× for the SC-30G3 and SC-55G2 designs, respectively. Therefore, the reported increases in HAC dose rates due to 1/2-inch axial gaps are inconsequential because the NCT 2-meter dose rate bounds the activity limits for all shielded container designs.

RAI-Sh-9 Show that the MCNP gamma shielding analysis model for the HalfPACT containing the SC-30G3 container properly converged.

The applicant provided the input file for the MCNP model for the HalfPACT containing the SC-30G3 container. The input model indicates that the applicant set a cut-off computing time of 1200 minutes. However, it is not clear how this cut-off time was determined and whether it can assure a proper convergence of the calculations. One method of showing convergence is providing an output file for the package under NCT. Also, clarify whether the calculations were made on a multiprocessor computer cluster or single processor. For the CTME card, the MCNP 6.2 user’s manual (LA-UR-17-29981, Los Alamos National Laboratory, 2017) explicitly points out that it is highly recommended that the NPS card (Section 3.3.7.1.1) should be used to limit the run time for multiprocessor cluster computers.

The staff needs this information to determine compliance with the requirements in 10 CFR 71.47 and 10 CFR 71.51(a)(2).

### **Response:**

While convergence may be used to terminate MCNP calculations for a criticality analysis, it is not applicable for a shielding analysis. A shielding evaluation relies on the results of MCNP's ten statistical checks for determining a problem's validity. A user's model can attain a solution from MCNP that can pass all ten statistical checks, yet have a high tally error (i.e., statistical uncertainty) because a low number of particle histories were evaluated. To reduce the tally error, the user must run a greater number of particle histories, but doing so increases the probability that one or more poorly-behaved particles will cause one or more of the ten statistical checks to fail.

An MCNP run is terminated based on one of two possible methods: 1) controlling computer processor time using the CTME card, or 2) controlling total quantity of particles using the NPS card. Because LANL never corrected MCNP when multi-threading was implemented, computer processor time is semi-arbitrary when running a multi-threading evaluation; hence, the reason the NPS card is recommended, but not required, for use in that situation. Regardless of the method employed to perform an MCNP evaluation and determine the run's cut-off point, however, it is still the responsibility of the user to evaluate results carefully to determine whether sufficient particles have been evaluated to produce an accurate solution.

Although the CTME card was employed for all runs, and all runs were performed using a multi-threading computer, the evaluation goal was to run for sufficient time (i.e., number of particles) to achieve a tally error under one percent. For the SC-30G3 example given, time was increased to 1,200 minutes using a trial-and-error process until the  $\leq 1\%$  tally error goal was achieved. As such, running with the NPS card would not have changed the reported results because the value on the NPS card would have been increased until the same answer with the same tally error goal was achieved.

RAI-Sh-10 Confirm that pre-shipment radiation survey is not relied upon for demonstrating that the package design will meet the regulatory requirement of 10 CFR 71.51(a)(1) and revise the SAR as necessary.

On page 5.3-1, the first paragraph the TRUPACT-II SAR states:

"Any significant deviation from the NCT configuration assumption is precluded through the use of pre-shipment radiological surveys of the package to validate that the source(s) are reasonably distributed within the package."

This statement seems to indicate that assurance of compliance with the regulatory requirement of 10 CFR 71.51(a)(1), "..., no significant increase in external surface radiation levels, and no substantial reduction in the effectiveness of the packaging;.." relies on pre-shipment dose rate measurement. It is not clear how this pre-shipment measurement can assure that the package meets the regulatory requirements of no significant increase

in external surface radiation levels even before a shipment has been made. A pre-shipment dose rate measurement can only assure that the package is fabricated and loaded as designed. It cannot tell any information on the potential source terms reconfiguration or relocation under NCT. Only design analysis can provide such an assurance.

In addition, as explained in Regulatory Issue Summary 2013-04, “Content Specification and Shielding Evaluations for Type B Transportation Packages,” pre-shipment dose rate measurement is a requirement of 10 CFR 71.87, “Routine determinations.” Per 10 CFR 71.35(a), an application for a CoC must include a demonstration that the package satisfies the standards in Subpart E which includes requirements in 10 CFR 71.51.

The staff needs this information to determine compliance with the requirements in 10 CFR 71.35 and 10 CFR 71.51.

**Response:**

For clarity, Section 5.3.1 of the TRUPACT-II SAR has been revised to delete the last two sentences.

Assurance that the NCT regulatory requirement of 10 CFR §71.51(a)(1) has been met is accomplished via the shielding analyses presented in Chapter 5 of the TRUPACT-II SAR. The responses to RAI-Sh-1 and RAI-Sh-6 address uncertainties in the payload activity assay evaluation. The 10% administrative margin that is applied to the calculated activity limit, where the combined sum of partial fractions for the gamma and neutron source terms present in the package must be less than or equal to 0.9, accounts for all other uncertainties.

## Attachment RAI-Sh-5 – MCNP Output Files

1. SC-30G3 NCT Model with  $^{252}\text{Cf}$  – Polyethylene with Secondary Gammas

Code Name &amp; Version = MCNP\_6.20, 6.2.0



```

+-----+
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```

```

1mcnp version 6 ld=02/20/18 08/29/21 09:02:49
*****
i=NCT_HP_SC-30G3_252cf_0.i name=NCT_HP_SC-30G3_252cf_0. tasks 24

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probid = 08/29/21 09:02:49

warning. universe map (print table 128) disabled.

comment. Physics models disabled.

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2- c
3- c Universe Fill Boundary
4- c
5- 1 0 -107 108 -109 fill=1 $Shielded Container
6- imp:n=1 imp:p=1 trcl=1
7- c
8- c Payload Cell $Material Density 100%
9- c
10- 2 1 -0.9400 -1 2 -3 $Payload
11- imp:n=1 imp:p=1 u=1
12- c
13- c Shielded Container Cells $Material Density 100%
14- c
15- 3 2 -7.8526 -11 12 -13 -14 $Lower Flange Steel
16- ((11 :13 :-15 :-16)
17- (11 :16 :-17 :-18)
18- (11 :18 :-19 :-20)
19- (11 :20 :-21 :-22)
20- (-12 :26 :27)
21- (23 :24 :-27))
22- imp:n=1 imp:p=1 u=1
23- 4 3 -11.3500 -23 -24 25 $Lower Flange Upper Lead
24- imp:n=1 imp:p=1 u=1
25- 5 3 -11.3500 -26 -27 28 $Lower Flange Lower Lead
26- imp:n=1 imp:p=1 u=1
27- 6 2 -7.8526 (12 -26 -31): $Lower Flange Base Steel
28- (-29 31 -32)
29- imp:n=1 imp:p=1 u=1
30- 7 2 -7.8526 16 33 -34 -45 $Inner Shell Steel
31- imp:n=1 imp:p=1 u=1
32- 8 3 -11.3500 (-16 17 18 -35): $Sidewall Lead
33- (16 34 -35 -40):
34- (-18 19 20 -35):

```

## ATTACHMENT A – Responses to RAI

35-				(34 40 -43 -45)	
36-				imp:n=1 imp:p=1 u=1	
37-	9	2	-7.8526	22 36 -37 -45	\$Outer Shell Steel
38-				imp:n=1 imp:p=1 u=1	
39-	10	2	-7.8526	((38 -39 -41 45):	\$Upper Flange Steel
40-				(40 43 -44 -45))	
41-				((-38 :41 :42))	
42-				imp:n=1 imp:p=1 u=1	
43-	11	2	-7.8526	-49 50 -51 -52	\$Lid Steel
44-				((39 :41 :-50 :-80)	
45-				(-41 :63 :-64 :65)	
46-				(-50 :51 :-65 :83)	
47-				(51 :-57 :58 :-59)	
48-				(-53 :54 :-55 :59))	
49-				imp:n=1 imp:p=1 u=1	
50-	12	2	-7.8526	-50 -80 82 83	\$Lid Ring Steel
51-				(80 :-81 :-83 :-84)	
52-				imp:n=1 imp:p=1 u=1	
53-	13	2	-7.8526	-81 86 -87 -89	\$Lid Base Steel
54-				(81 :-83 :87 :-88)	
55-				imp:n=1 imp:p=1 u=1	
56-	14	3	-11.3500	-50 -82 85	\$Lid Plate Lead
57-				imp:n=1 imp:p=1 u=1	
58-	15	3	-11.3500	53 -54 55 -56	\$Lid Ring Lead
59-				imp:n=1 imp:p=1 u=1	
60-	16	2	-7.8526	59 60 -61 -62	\$Lid Ring Cover Plate Steel
61-				imp:n=1 imp:p=1 u=1	
62-	c				
63-	c			Cavity (Void) Cells	
64-	c				
65-	17	1	-0.9400	((13 -33 -86):	\$Payload Cavity
66-				(-13 15 16 -33):	
67-				(-33 86 89):	
68-				(-33 81 84 -89):	
69-				(-33 -45 80 -84):	
70-				(-38 42 45 80):	
71-				(-41 -42 80))	
72-				(1 :-2 :3)	
73-				imp:n=1 imp:p=1 u=1	
74-	18	0		-23 -25 27	\$Lower Flange Upper Lead
75-				imp:n=1 imp:p=1 u=1	
76-	19	0		(-26 -28 29 31):	\$ Axial Cavity
77-				(-28 -29 32)	\$Lower Flange Lower Lead
78-				imp:n=1 imp:p=1 u=1	
79-	20	0		(-20 21 22 -36):	\$sidewall Lead Outer Radial Gap
80-				(20 35 -36 -40):	
81-				(-36 40 44 -45)	
82-				imp:n=1 imp:p=1 u=1	
83-	21	0		41 -63 64 -65	\$Lid Gasket Recess Cavity
84-				imp:n=1 imp:p=1 u=1	
85-	22	0		53 -54 56 -59	\$Lid Lead Ring Axial Cavity
86-				imp:n=1 imp:p=1 u=1	
87-	23	0		(-82 83 -87 88):	\$Lid Lead Plate Axial Cavity
88-				(-82 -85 87)	
89-				imp:n=1 imp:p=1 u=1	
90-	24	0		((11 :-12 :14 :22)	\$Exterior Void
91-				(-22 :37 :45)	
92-				(-45 :49 :51 :52)):	
93-				((12 -29 -30):	
94-				(-51 57 -58 62):	
95-				(57 59 -60 -62):	
96-				(-58 59 61 -62))	
97-				imp:n=1 imp:p=1 u=1	
98-	c				
99-	c			HalfPACT Package Cells	\$Material Density 100%
100-	c				
101-	201	4	-8.0128	(201 -202 204 -205):	\$HalfPACT ICV/OCV Steel Structure
102-				(-202 203 -204):	
103-				(-202 205 -206)	
104-				imp:n=1 imp:p=1	
105-	202	5	-0.1322	(202 203 -206 -211):	\$HalfPACT OCA Polyurethane Foam
106-				(-203 -211 214):	
107-				(206 -211 -215)	
108-				imp:n=1 imp:p=1	
109-	203	4	-8.0128	(211 -212 214 -215):	\$HalfPACT OCA Steel Structure
110-				(-212 213 -214):	
111-				(-212 215 -216)	
112-				imp:n=1 imp:p=1	
113-	c				
114-	c			HalfPACT Package Void Cells	
115-	c				

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116-	204	0	-201 204 -205	\$HalfPACT ICV Interior Void
117-			#1	
118-			imp:n=1 imp:p=1	
119-	205	0	((-999 212 213 -216):	\$HalfPACT OCA Exterior Void
120-			(-999 -213):	
121-			(-999 216))	
122-			(-301 :302:-305 :306)	
123-			(-303 :304:-305 :306)	
124-			imp:n=1 imp:p=1	
125-	c			
126-	c		HalfPACT Package Surface and 2-meter Tally Cells	
127-	c			
128-	301	0	301 -302 305 -306	\$Package Side Middle @ Surface
129-			imp:n=1 imp:p=1	
130-	302	0	303 -304 305 -306	\$Package Side Middle @ 2-meters
131-			imp:n=1 imp:p=1	
132-	c			
133-	c		World Cell	
134-	c			
135-	999	0	999	
136-			imp:n=0 imp:p=0	
137-				
138-	c			
139-	c		Payload Surfaces	
140-	c			
141-	1	cz	1.27000	\$Radius
142-	2	pz	51.07305	\$Plane, Bottom
143-	3	pz	53.61305	\$Plane, Top
144-	c			
145-	c		Shielded Container Lower Flange Surfaces	
146-	c			
147-	11	cz	35.56000	\$Radius, Outer
148-	12	pz	0.00000	\$Plane, Lower Flange Bottom
149-	13	pz	14.60500	\$Plane, Lower Flange Top
150-	14	kz	-35.24250 1.00000 1	\$Chamfer, Bottom Outer Corner
151-	15	cz	25.79370	\$Radius, Inner Shell Step
152-	16	pz	13.97000	\$Plane, Inner Shell Step
153-	17	cz	27.19070	\$Radius, Inner Lead Step
154-	18	kz	10.47452 192.3724 -1	\$Cone, Inner Lead Step Vertex
155-	19	cz	31.43250	\$Radius, Outer Lead Step
156-	20	pz	5.08000	\$Plane, Outer Lead Step
157-	21	cz	34.23920	\$Radius, Outer Shell Step
158-	22	pz	4.44500	\$Plane, Outer Shell Step
159-	23	cz	25.40000	\$Radius, Upper Lead Plate Recess
160-	24	pz	10.18540	\$Plane, Upper Lead Plate Recess
161-	25	pz	5.74040	\$Plane, Upper Lead Plate Bottom
162-	26	cz	29.21000	\$Radius, Lower Lead Plate Recess
163-	27	pz	5.71500	\$Plane, Lower Lead Plate Recess
164-	28	pz	3.81000	\$Plane, Lower Lead Plate Bottom
165-	29	cz	29.07030	\$Radius, Base Plate
166-	30	pz	0.00000	\$Plane, Base Plate Bottom
167-	31	pz	2.54000	\$Plane, Base Plate Weld Elevation
168-	32	pz	3.81000	\$Plane, Base Plate Top
169-	c			
170-	c		Shielded Container Sidewall Inner Shell Surfaces	
171-	c			
172-	33	cz	25.92070	\$Radius, Inner
173-	34	cz	27.19070	\$Radius, Outer
174-	c			
175-	c		Shielded Container Sidewall Lead Shell Surface	
176-	c			
177-	35	cz	34.17570	\$Radius, Outer
178-	c			
179-	c		Shielded Container Sidewall Outer Shell Surfaces	
180-	c			
181-	36	cz	34.29000	\$Radius, Inner
182-	37	cz	35.56000	\$Radius, Outer
183-	c			
184-	c		Shielded Container Upper Flange Surfaces	
185-	c			
186-	38	cz	25.72385	\$Radius, Inner
187-	39	cz	35.56000	\$Radius, Outer
188-	40	pz	97.15500	\$Plane, Upper Flange Bottom
189-	41	pz	101.91750	\$Plane, Upper Flange Top
190-	42	kz	30.60680 0.13247 1	\$Chamfer, Top Inner Corner
191-	43	cz	27.24150	\$Radius, Inner Shell Step
192-	44	cz	34.23920	\$Radius, Outer Shell Step
193-	45	pz	97.79000	\$Plane, Shell Step Top
194-	c			
195-	c		Shielded Container Lid Surfaces	
196-	c			



## ATTACHMENT A – Responses to RAI

197-	49	cz	35.56000			\$Radius, Lid Outer
198-	50	pz	100.34270			\$Plane, Lid Bottom
199-	51	pz	107.32770			\$Plane, Lid Top
200-	52	kz	142.57020	1.00000	-1	\$Chamfer, Top Outside Corner
201-	53	cz	22.54250			\$Radius, Lead Ring Recess Inner
202-	54	cz	29.84500			\$Radius, Lead Ring Recess Outer
203-	55	pz	104.91470			\$Plane, Lead Ring Recess Bottom
204-	56	pz	106.81970			\$Plane, Lead Ring Top
205-	57	cz	22.22500			\$Radius, Lead Ring Cover Recess Inner
206-	58	cz	30.16250			\$Radius, Lead Ring Cover Recess Outer
207-	59	pz	106.84510			\$Plane, Lead Ring Cover Recess Bottom
208-	60	cz	22.27580			\$Radius, Lead Ring Cover Inner
209-	61	cz	30.11170			\$Radius, Lead Ring Cover Outer
210-	62	pz	107.29976			\$Plane, Lead Ring Cover Top
211-	63	cz	28.57500			\$Radius, Gasket Recess Outer
212-	64	cz	26.33980			\$Radius, Gasket Recess Inner
213-	65	pz	102.23500			\$Plane, Gasket Recess Top
214-	c					
215-	c					Shielded Container Lid Ring Surfaces
216-	c					
217-	80	cz	25.66035			\$Radius, Outer Upper
218-	81	cz	25.52700			\$Radius, Outer Lower
219-	82	cz	24.13000			\$Radius, Inner
220-	83	pz	93.28150			\$Plane, Bottom
221-	84	kz	26.24737	0.13247	1	\$Cone, Outer Radius Transition
222-	85	pz	94.62770			\$Plane, Lead Plate Bottom
223-	c					
224-	c					Shielded Container Lid Base Surfaces
225-	c					
226-	86	pz	90.08110			\$Plane, Bottom
227-	87	pz	94.52610			\$Plane, Top
228-	88	cz	24.06650			\$Radius, Lid Ring Step
229-	89	kz	20.58124	0.13247	1	\$Chamfer, Bottom Outside Corner
230-	c					
231-	c					Shielded Container Universe Fill Boundary Surfaces
232-	c					
233-	107	cz	35.56001			\$Radius, Fill Boundary
234-	108	pz	-0.00001			\$Plane, Fill Boundary Bottom
235-	109	pz	107.32771			\$Plane, Fill Boundary Top
236-	c					
237-	c					HalfPACT Package ICV/OCV Surfaces
238-	c					
239-	201	cz	92.23375			\$Radius, Shell Inner
240-	202	cz	93.34500			\$Radius, Shell Outer
241-	203	pz	22.86000			\$Plane, Lower Head Bottom
242-	204	pz	24.13000			\$Plane, Lower Head Top
243-	205	pz	198.12000			\$Plane, Upper Head Bottom
244-	206	pz	199.39000			\$Plane, Upper Head Top
245-	c					
246-	c					HalfPACT Package OCA Surfaces
247-	c					
248-	211	cz	118.74500			\$Radius, Shell Inner
249-	212	cz	119.38000			\$Radius, Shell Outer
250-	213	pz	0.00000			\$Plane, Lower Head Bottom
251-	214	pz	0.63500			\$Plane, Lower Head Top
252-	215	pz	229.23500			\$Plane, Upper Head Bottom
253-	216	pz	229.87000			\$Plane, Upper Head Top
254-	c					
255-	c					HalfPACT Package Tally Surfaces
256-	c					
257-	301	cz	119.38000			\$Radius, Inner (at Surface)
258-	302	cz	119.48000			\$Radius, Outer (at Surface)
259-	303	cz	319.38000			\$Radius, Inner (at 2.000-Meters)
260-	304	cz	319.48000			\$Radius, Outer (at 2.001-Meters)
261-	305	pz	108.58500			\$Plane, Bottom Elevation
262-	306	pz	113.66500			\$Plane, Top Elevation
263-	c					
264-	c					World Surface (Problem Boundary)
265-	c					
266-	999	sz	114.93500		400	
267-						
268-	c					
269-	c					Physics Cards
270-	c					
271-	mode n	p				
comment.	photonuclear	physics may be needed (phys:p).				
272-	c					
273-	c					Material Cards
274-	c					
275-	m1	1001.84C	-0.143704			\$Payload (Polyethylene)
276-		1002.84C	-0.000033			6000.84C -0.856263

# ATTACHMENT A – Responses to RAI

```

277-      plib = 84P
278-      C
279-      m2  26054.84C -0.058450      $Carbon Steel
280-      26056.84C -0.917540      26057.84C -0.021190      26058.84C -0.002820
281-      plib = 84P
282-      C
283-      m3  82204.84C -0.014000      $Lead
284-      82206.84C -0.241000      82207.84C -0.221000      82208.84C -0.524000
285-      plib = 84P
286-      C
287-      m4  14028.84C -0.009222      $Stainless Steel (ASTM A240, Type 304)
288-      14029.84C -0.000469      14030.84C -0.000309      24050.84C -0.008256
289-      24052.84C -0.159199      24053.84C -0.018052      24054.84C -0.004494
290-      25055.84C -0.020000      26054.84C -0.039746      26056.84C -0.623927
291-      26057.84C -0.014409      26058.84C -0.001918      28058.84C -0.068077
292-      28060.84C -0.026223      28061.84C -0.001140      28062.84C -0.003635
293-      28064.84C -0.000926
294-      plib = 84P
295-      C
296-      m5  1001.84C -0.069992      $Urethane Foam
297-      1002.84C -0.000008      6000.84C -0.600000      7014.84C -0.079709
298-      7015.84C -0.000291      8016.84C -0.239417      8017.84C -0.000091
299-      14028.84C -0.009222      14029.84C -0.000469      14030.84C -0.000309
300-      plib = 84P
301-      C
302-      C Specify Universe Transformations
303-      C
304-      *tr1      -53.66386      0.00000      111.12500
305-      -90      90      0      90      0      90      0      90      -90
306-      C
307-      C Specify Explicit Analysis for Weight Windows Evaluation
308-      C
309-      cut:n      2j      0
310-      cut:p      2j      0
311-      C
312-      C Source Cards
313-      C
314-      sdef par=1 axs=1 0 0 erg=d1 pos=d2 rad=d3 ext=d4
315-      sc1 Concentrated 252Cf Neutron Source
316-      si1      L      0.100000      0.500000      1.000000      2.000000      3.000000
317-      4.000000      6.000000      8.000000      10.000000      15.000000
318-      sp1      0.00E+00      1.80E+11      2.71E+11      5.36E+11      4.10E+11
319-      2.73E+11      2.66E+11      8.53E+10      2.44E+10      8.36E+09
320-      si2      L      -1.32080      0.00000      111.12500
321-      sp2      1
322-      si3      0.00000      1.27000
323-      sp3      -21      1
324-      si4      -1.27000      1.27000
325-      sp4      -21      0      0
326-      C
327-      C Package Tally Cards
328-      C
329-      f4:n 301
330-      fc4 Package Surface Neutron Dose Rate (mrem/hr) @ Z = 111.12500
331-      sd4 381.20362
332-      f14:n 302
333-      fc14 2-M from Package Surface Neutron Dose Rate (mrem/hr) @ Z = 111.12500
334-      sd14 1019.57524
335-      f24:p 301
336-      fc24 Package Surface Gamma Dose Rate (mrem/hr) @ Z = 111.12500
337-      sd24 381.20362
338-      f34:p 302
339-      fc34 2-M from Package Surface Gamma Dose Rate (mrem/hr) @ Z = 111.12500
340-      sd34 1019.57524
341-      C
342-      C ANSI/ANS-6.1.1-1977 Neutron Flux-to-Dose Rate Factor Cards
343-      C
344-      de0      2.50E-08      1.00E-07      1.00E-06      1.00E-05      1.00E-04      $Energy (Mev)
345-      1.00E-03      1.00E-02      1.00E-01      5.00E-01      1.00E+00
346-      2.50E+00      5.00E+00      7.00E+00      1.00E+01      1.40E+01
347-      2.00E+01
348-      df0      3.67E-03      3.67E-03      4.46E-03      4.54E-03      4.18E-03      $Factor (mrem/hr)
349-      3.76E-03      3.56E-03      2.17E-02      9.26E-02      1.32E-01
350-      1.25E-01      1.56E-01      1.47E-01      1.47E-01      2.08E-01
351-      2.27E-01
352-      C
353-      C ANSI/ANS-6.1.1-1977 Gamma Flux-to-Dose Rate Factor Cards
354-      C
355-      de24      0.01      0.03      0.05      0.07      0.10      $Energy (Mev)
356-      0.15      0.20      0.25      0.30      0.35
357-      0.40      0.45      0.50      0.55      0.60

```

# ATTACHMENT A – Responses to RAI

```

358-          0.65    0.70    0.80    1.00    1.40
359-          1.80    2.20    2.60    2.80    3.25
360-          3.75    4.25    4.75    5.00    5.25
361-          5.75    6.25    6.75    7.50    9.00
362-          11.00   13.00   15.00
363-   df24  3.96E-03  5.82E-04  2.90E-04  2.58E-04  2.83E-04  $Factor (mrem/hr)
364-        3.79E-04  5.01E-04  6.31E-04  7.59E-04  8.78E-04
365-        9.85E-04  1.08E-03  1.17E-03  1.27E-03  1.36E-03
366-        1.44E-03  1.52E-03  1.68E-03  1.98E-03  2.51E-03
367-        2.99E-03  3.42E-03  3.82E-03  4.01E-03  4.41E-03
368-        4.83E-03  5.23E-03  5.60E-03  5.80E-03  6.01E-03
369-        6.37E-03  6.74E-03  7.11E-03  7.66E-03  8.77E-03
370-        1.03E-02  1.18E-02  1.33E-02
371-   de34    0.01    0.03    0.05    0.07    0.10  $Energy (Mev)
372-        0.15    0.20    0.25    0.30    0.35
373-        0.40    0.45    0.50    0.55    0.60
374-        0.65    0.70    0.80    1.00    1.40
375-        1.80    2.20    2.60    2.80    3.25
376-        3.75    4.25    4.75    5.00    5.25
377-        5.75    6.25    6.75    7.50    9.00
378-        11.00   13.00   15.00
379-   df34  3.96E-03  5.82E-04  2.90E-04  2.58E-04  2.83E-04  $Factor (mrem/hr)
380-        3.79E-04  5.01E-04  6.31E-04  7.59E-04  8.78E-04
381-        9.85E-04  1.08E-03  1.17E-03  1.27E-03  1.36E-03
382-        1.44E-03  1.52E-03  1.68E-03  1.98E-03  2.51E-03
383-        2.99E-03  3.42E-03  3.82E-03  4.01E-03  4.41E-03
384-        4.83E-03  5.23E-03  5.60E-03  5.80E-03  6.01E-03
385-        6.37E-03  6.74E-03  7.11E-03  7.66E-03  8.77E-03
386-        1.03E-02  1.18E-02  1.33E-02
387-   c
388-   c Runtime and Print Cards
389-   c
390-   prdmp      j      j      1      2
391-   ctme      1200

```

```

*****
* Random Number Generator = 1 *
* Random Number Seed = 19073486328125 *
* Random Number Multiplier = 19073486328125 *
* Random Number Adder = 0 *
* Random Number Bits Used = 48 *
* Random Number Stride = 152917 *
*****

```

comment. total nubar used if fissionable isotopes are present.

```

surface 11 and surface 37 are the same. 37 will be deleted.
surface 11 and surface 39 are the same. 39 will be deleted.
surface 11 and surface 49 are the same. 49 will be deleted.
surface 12 and surface 30 are the same. 30 will be deleted.
surface 12 and surface 213 are the same. 213 will be deleted.
surface 17 and surface 34 are the same. 34 will be deleted.
surface 21 and surface 44 are the same. 44 will be deleted.
surface 28 and surface 32 are the same. 32 will be deleted.
surface 212 and surface 301 are the same. 301 will be deleted.

```

comment. 9 surfaces were deleted for being the same as others.

warning. 1 materials had unnormalized fractions. print table 40.

warning. 1 cells appear to consist of more than one piece.  
1cells

print table 60

cell	mat	atom density	gram density	volume	mass	pieces	neutron importance	photon importance	photon wt generation
1	1	0.00000E+00	0.00000E+00	4.26369E+05	0.00000E+00	1	1.0000E+00	1.0000E+00	-1.000E+00
2	2	1.21080E-01	9.40000E-01	1.28704E+01	1.20981E+01	1	1.0000E+00	1.0000E+00	-1.000E+00
3	3	8.46854E-02	7.85260E+00	2.01423E+04	1.58169E+05	1	1.0000E+00	1.0000E+00	-1.000E+00
4	4	3.29855E-02	1.13500E+01	9.00926E+03	1.02255E+05	1	1.0000E+00	1.0000E+00	-1.000E+00
5	5	3.29855E-02	1.13500E+01	5.10632E+03	5.79567E+04	1	1.0000E+00	1.0000E+00	-1.000E+00
6	6	8.46854E-02	7.85260E+00	1.01802E+04	7.99407E+04	1	1.0000E+00	1.0000E+00	-1.000E+00

# ATTACHMENT A – Responses to RAI

7	7	2	8.46854E-02	7.85260E+00	1.77619E+04	1.39477E+05	1	1.0000E+00	1.0000E+00	-1.000E+00
8	8	3	3.29855E-02	1.13500E+01	1.21436E+05	1.37829E+06	1	1.0000E+00	1.0000E+00	-1.000E+00
9	9	2	8.46854E-02	7.85260E+00	2.60142E+04	2.04279E+05	1	1.0000E+00	1.0000E+00	-1.000E+00
10	10	2	8.46854E-02	7.85260E+00	8.66283E+03	6.80257E+04	1	1.0000E+00	1.0000E+00	-1.000E+00
11	11	2	8.46854E-02	7.85260E+00	2.16660E+04	1.70134E+05	1	1.0000E+00	1.0000E+00	-1.000E+00
12	12	2	8.46854E-02	7.85260E+00	1.61985E+03	1.27201E+04	1	1.0000E+00	1.0000E+00	-1.000E+00
13	13	2	8.46854E-02	7.85260E+00	8.80459E+03	6.91389E+04	1	1.0000E+00	1.0000E+00	-1.000E+00
14	14	3	3.29855E-02	1.13500E+01	1.04540E+04	1.18652E+05	1	1.0000E+00	1.0000E+00	-1.000E+00
15	15	3	3.29855E-02	1.13500E+01	2.28952E+03	2.59860E+04	1	1.0000E+00	1.0000E+00	-1.000E+00
16	16	2	8.46854E-02	7.85260E+00	5.86345E+02	4.60433E+03	1	1.0000E+00	1.0000E+00	-1.000E+00
17	17	1	1.21080E-01	9.40000E-01	1.59844E+05	1.50253E+05	1	1.0000E+00	1.0000E+00	-1.000E+00
18	18	0	0.00000E+00	0.00000E+00	5.14815E+01	0.00000E+00	1	1.0000E+00	1.0000E+00	-1.000E+00
19	19	0	0.00000E+00	0.00000E+00	3.24842E+01	0.00000E+00	1	1.0000E+00	1.0000E+00	-1.000E+00
20	20	0	0.00000E+00	0.00000E+00	2.27755E+03	0.00000E+00	1	1.0000E+00	1.0000E+00	-1.000E+00
21	21	0	0.00000E+00	0.00000E+00	1.22433E+02	0.00000E+00	1	1.0000E+00	1.0000E+00	-1.000E+00
22	22	0	0.00000E+00	0.00000E+00	3.05269E+01	0.00000E+00	1	1.0000E+00	1.0000E+00	-1.000E+00
23	23	0	0.00000E+00	0.00000E+00	1.97815E+02	0.00000E+00	1	1.0000E+00	1.0000E+00	-1.000E+00
24	24	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0	1.0000E+00	1.0000E+00	-1.000E+00
25	201	4	8.80954E-02	8.01280E+00	1.82252E+05	1.46035E+06	1	1.0000E+00	1.0000E+00	-1.000E+00
26	202	5	1.11868E-02	1.32200E-01	5.29418E+06	6.99890E+05	1	1.0000E+00	1.0000E+00	-1.000E+00
27	203	4	8.80954E-02	8.01280E+00	1.65455E+05	1.32576E+06	1	1.0000E+00	1.0000E+00	-1.000E+00
28	204	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0	1.0000E+00	1.0000E+00	-1.000E+00
29	205	0	0.00000E+00	0.00000E+00	2.57789E+08	0.00000E+00	2	1.0000E+00	1.0000E+00	-1.000E+00
30	301	0	0.00000E+00	0.00000E+00	3.81204E+02	0.00000E+00	1	1.0000E+00	1.0000E+00	-1.000E+00
31	302	0	0.00000E+00	0.00000E+00	1.01958E+03	0.00000E+00	1	1.0000E+00	1.0000E+00	-1.000E+00
32	999	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0	0.0000E+00	0.0000E+00	-1.000E+00

total 2.64285E+08 6.22590E+06

minimum source weight = 1.0000E+00 maximum source weight = 1.0000E+00

comment. threading will be used when possible in portions of mcnp6.

comment. threading will be used for n/p/e table physics.

comment. threading will generally not be used for model physics.

3 warning messages so far.

1cross-section tables print table 100

XSDIR used: C:\MCNP\MCPN\_DATA\xsdir\_mcnp6.2

table	length						
tables from file xdata/endl71x/H/1001.714nc							
1001.84c	15325	H1 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53)	mat 125	12/17/12			
		Energy range: 1.00000E-11 to 2.00000E+01 Mev.					
		particle-production data for deuterons being expunged from 1001.84c					
		temperature = 2.1543E-07 adjusted to 2.5300E-08					
tables from file xdata/endl71x/H/1002.714nc							
1002.84c	7283	H2 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53)	mat 128	12/17/12			
		Energy range: 1.00000E-11 to 1.50000E+02 Mev.					
		particle-production data for protons being expunged from 1002.84c					
		particle-production data for tritons being expunged from 1002.84c					
		temperature = 2.1543E-07 adjusted to 2.5300E-08					
tables from file xdata/endl71x/C/6000.714nc							
6000.84c	55343	C0 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53)	mat 600	12/20/12			
		Energy range: 1.00000E-11 to 1.50000E+02 Mev.					
		particle-production data for protons being expunged from 6000.84c					
		particle-production data for deuterons being expunged from 6000.84c					
		particle-production data for alphas being expunged from 6000.84c					
		temperature = 2.1543E-07 adjusted to 2.5300E-08					
tables from file xdata/endl71x/N/7014.714nc							
7014.84c	102640	N14 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53)	mat 725	12/16/12			
		Energy range: 1.00000E-11 to 1.50000E+02 Mev.					
		particle-production data for protons being expunged from 7014.84c					
		particle-production data for deuterons being expunged from 7014.84c					
		particle-production data for alphas being expunged from 7014.84c					
		temperature = 2.1543E-07 adjusted to 2.5300E-08					
tables from file xdata/endl71x/N/7015.714nc							
7015.84c	28412	N15 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53)	mat 728	12/16/12			
		Energy range: 1.00000E-11 to 2.00000E+01 Mev.					
		temperature = 2.1543E-07 adjusted to 2.5300E-08					

## ATTACHMENT A – Responses to RAI

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tables from file xdata/endl71x/0/8016.714nc

8016.84c	264772	016 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 1.50000E+02 Mev. particle-production data for protons being expunged from 8016.84c particle-production data for deuterons being expunged from 8016.84c particle-production data for tritons being expunged from 8016.84c particle-production data for alphas being expunged from 8016.84c temperature = 2.1543E-07 adjusted to 2.5300E-08	mat 825	12/13/12
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tables from file xdata/endl71x/0/8017.714nc

8017.84c	4921	017 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 2.00000E+01 Mev. temperature = 2.1543E-07 adjusted to 2.5300E-08	mat 828	12/13/12
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warning. 8017.84c lacks gamma-ray production cross sections.

tables from file xdata/endl71x/Si/14028.714nc

14028.84c	169896	Si28 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 1.50000E+02 Mev. particle-production data for protons being expunged from 14028.84c particle-production data for deuterons being expunged from 14028.84c particle-production data for tritons being expunged from 14028.84c particle-production data for alphas being expunged from 14028.84c temperature = 2.1543E-07 adjusted to 2.5300E-08	mat1425	12/14/12
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tables from file xdata/endl71x/Si/14029.714nc

14029.84c	158834	Si29 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 1.50000E+02 Mev. particle-production data for protons being expunged from 14029.84c particle-production data for deuterons being expunged from 14029.84c particle-production data for tritons being expunged from 14029.84c particle-production data for alphas being expunged from 14029.84c temperature = 2.1543E-07 adjusted to 2.5300E-08	mat1428	12/14/12
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tables from file xdata/endl71x/Si/14030.714nc

14030.84c	130018	Si30 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 1.50000E+02 Mev. particle-production data for protons being expunged from 14030.84c particle-production data for deuterons being expunged from 14030.84c particle-production data for tritons being expunged from 14030.84c particle-production data for alphas being expunged from 14030.84c temperature = 2.1543E-07 adjusted to 2.5300E-08	mat1431	12/16/12
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tables from file xdata/endl71x/Cr/24050.714nc

24050.84c	291186	Cr50 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 1.50000E+02 Mev. particle-production data for protons being expunged from 24050.84c particle-production data for deuterons being expunged from 24050.84c particle-production data for tritons being expunged from 24050.84c particle-production data for alphas being expunged from 24050.84c temperature = 2.1543E-07 adjusted to 2.5300E-08	mat2425	12/13/12
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tables from file xdata/endl71x/Cr/24052.714nc

24052.84c	310582	Cr52 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 1.50000E+02 Mev. particle-production data for protons being expunged from 24052.84c particle-production data for deuterons being expunged from 24052.84c particle-production data for tritons being expunged from 24052.84c particle-production data for alphas being expunged from 24052.84c temperature = 2.1543E-07 adjusted to 2.5300E-08	mat2431	12/13/12
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tables from file xdata/endl71x/Cr/24053.714nc

24053.84c	254692	Cr53 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 1.50000E+02 Mev. particle-production data for protons being expunged from 24053.84c particle-production data for deuterons being expunged from 24053.84c particle-production data for tritons being expunged from 24053.84c particle-production data for alphas being expunged from 24053.84c temperature = 2.1543E-07 adjusted to 2.5300E-08	mat2434	12/13/12
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tables from file xdata/endl71x/Cr/24054.714nc

## ATTACHMENT A – Responses to RAI

24054.84c	190185	Cr54 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 1.50000E+02 Mev. particle-production data for protons being expunged from 24054.84c particle-production data for deuterons being expunged from 24054.84c particle-production data for tritons being expunged from 24054.84c particle-production data for alphas being expunged from 24054.84c temperature = 2.1543E-07 adjusted to 2.5300E-08  tables from file xdata/endl71x/Mn/25055.714nc	mat2437	12/13/12
25055.84c	455909	Mn55 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 6.00000E+01 Mev. particle-production data for protons being expunged from 25055.84c particle-production data for deuterons being expunged from 25055.84c particle-production data for tritons being expunged from 25055.84c particle-production data for helions being expunged from 25055.84c particle-production data for alphas being expunged from 25055.84c probability tables used from 1.2500E-01 to 1.0000E+00 mev. temperature = 2.1543E-07 adjusted to 2.5300E-08  tables from file xdata/endl71x/Fe/26054.714nc	mat2525	12/18/12
26054.84c	217705	Fe54 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 1.50000E+02 Mev. particle-production data for protons being expunged from 26054.84c particle-production data for deuterons being expunged from 26054.84c particle-production data for tritons being expunged from 26054.84c particle-production data for alphas being expunged from 26054.84c temperature = 2.1543E-07 adjusted to 2.5300E-08  tables from file xdata/endl71x/Fe/26056.714nc	mat2625	12/22/12
26056.84c	352429	Fe56 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 1.50000E+02 Mev. particle-production data for protons being expunged from 26056.84c particle-production data for deuterons being expunged from 26056.84c particle-production data for tritons being expunged from 26056.84c particle-production data for alphas being expunged from 26056.84c temperature = 2.1543E-07 adjusted to 2.5300E-08  tables from file xdata/endl71x/Fe/26057.714nc	mat2631	12/22/12
26057.84c	241212	Fe57 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 1.50000E+02 Mev. particle-production data for protons being expunged from 26057.84c particle-production data for deuterons being expunged from 26057.84c particle-production data for tritons being expunged from 26057.84c particle-production data for alphas being expunged from 26057.84c temperature = 2.1543E-07 adjusted to 2.5300E-08  tables from file xdata/endl71x/Fe/26058.714nc	mat2634	12/22/12
26058.84c	135502	Fe58 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 2.00000E+01 Mev. particle-production data for protons being expunged from 26058.84c particle-production data for alphas being expunged from 26058.84c temperature = 2.1543E-07 adjusted to 2.5300E-08  tables from file xdata/endl71x/Ni/28058.714nc	mat2637	12/22/12
28058.84c	420627	Ni58 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 1.50000E+02 Mev. particle-production data for protons being expunged from 28058.84c particle-production data for deuterons being expunged from 28058.84c particle-production data for tritons being expunged from 28058.84c particle-production data for alphas being expunged from 28058.84c temperature = 2.1543E-07 adjusted to 2.5300E-08  tables from file xdata/endl71x/Ni/28060.714nc	mat2825	12/15/12
28060.84c	344192	Ni60 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 1.50000E+02 Mev. particle-production data for protons being expunged from 28060.84c particle-production data for deuterons being expunged from 28060.84c particle-production data for tritons being expunged from 28060.84c particle-production data for alphas being expunged from 28060.84c temperature = 2.1543E-07 adjusted to 2.5300E-08  tables from file xdata/endl71x/Ni/28061.714nc	mat2831	12/17/12
28061.84c	190713	Ni61 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53)	mat2834	12/13/12

## ATTACHMENT A – Responses to RAI

Energy range: 1.00000E-11 to 1.50000E+02 Mev.  
 particle-production data for protons being expunged from 28061.84c  
 particle-production data for deuterons being expunged from 28061.84c  
 particle-production data for tritons being expunged from 28061.84c  
 particle-production data for alphas being expunged from 28061.84c  
 temperature = 2.1543E-07 adjusted to 2.5300E-08

tables from file xdata/endl71x/Ni/28062.714nc

28062.84c	169202	Ni62 ENDF71x (j1conlin) Ref. see j1conlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 1.50000E+02 Mev. particle-production data for protons being expunged from 28062.84c particle-production data for deuterons being expunged from 28062.84c particle-production data for tritons being expunged from 28062.84c particle-production data for alphas being expunged from 28062.84c probability tables used from 6.0000E-01 to 1.0000E+00 mev. temperature = 2.1543E-07 adjusted to 2.5300E-08	mat2837	12/17/12
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tables from file xdata/endl71x/Ni/28064.714nc

28064.84c	152759	Ni64 ENDF71x (j1conlin) Ref. see j1conlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 1.50000E+02 Mev. particle-production data for protons being expunged from 28064.84c particle-production data for deuterons being expunged from 28064.84c particle-production data for tritons being expunged from 28064.84c particle-production data for alphas being expunged from 28064.84c temperature = 2.1543E-07 adjusted to 2.5300E-08	mat2843	12/17/12
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tables from file xdata/endl71x/Pb/82204.714nc

82204.84c	392627	Pb204 ENDF71x (j1conlin) Ref. see j1conlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 2.00000E+02 Mev. particle-production data for protons being expunged from 82204.84c particle-production data for deuterons being expunged from 82204.84c particle-production data for tritons being expunged from 82204.84c particle-production data for helions being expunged from 82204.84c particle-production data for alphas being expunged from 82204.84c temperature = 2.1543E-07 adjusted to 2.5300E-08	mat8225	12/22/12
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tables from file xdata/endl71x/Pb/82206.714nc

82206.84c	801388	Pb206 ENDF71x (j1conlin) Ref. see j1conlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 2.00000E+02 Mev. particle-production data for protons being expunged from 82206.84c particle-production data for deuterons being expunged from 82206.84c particle-production data for tritons being expunged from 82206.84c particle-production data for helions being expunged from 82206.84c particle-production data for alphas being expunged from 82206.84c temperature = 2.1543E-07 adjusted to 2.5300E-08	mat8231	12/22/12
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tables from file xdata/endl71x/Pb/82207.714nc

82207.84c	353707	Pb207 ENDF71x (j1conlin) Ref. see j1conlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 2.00000E+02 Mev. particle-production data for protons being expunged from 82207.84c particle-production data for deuterons being expunged from 82207.84c particle-production data for tritons being expunged from 82207.84c particle-production data for helions being expunged from 82207.84c particle-production data for alphas being expunged from 82207.84c temperature = 2.1543E-07 adjusted to 2.5300E-08	mat8234	12/22/12
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tables from file xdata/endl71x/Pb/82208.714nc

82208.84c	317905	Pb208 ENDF71x (j1conlin) Ref. see j1conlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 1.50000E+02 Mev. particle-production data for protons being expunged from 82208.84c particle-production data for deuterons being expunged from 82208.84c particle-production data for tritons being expunged from 82208.84c particle-production data for alphas being expunged from 82208.84c temperature = 2.1543E-07 adjusted to 2.5300E-08	mat8237	12/22/12
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tables from file xdata/mcplib84

1000.84p	1974	Update of MCPLIB04 Photon Compton Broadening Data For MCNP5 see LA-UR- Energy range: 1.00000E-03 to 1.00000E+05 Mev.	12-00018	01/03/12
6000.84p	3228	Update of MCPLIB04 Photon Compton Broadening Data For MCNP5 see LA-UR- Energy range: 1.00000E-03 to 1.00000E+05 Mev.	12-00018	01/03/12
7000.84p	3270	Update of MCPLIB04 Photon Compton Broadening Data For MCNP5 see LA-UR- Energy range: 1.00000E-03 to 1.00000E+05 Mev.	12-00018	01/03/12
8000.84p	3348	Update of MCPLIB04 Photon Compton Broadening Data For MCNP5 see LA-UR- Energy range: 1.00000E-03 to 1.00000E+05 Mev.	12-00018	01/03/12

## ATTACHMENT A – Responses to RAI

14000.84p	4868	Update of MCPLIB04 Photon Compton Broadening Data For MCNP5 see LA-UR- Energy range: 1.00000E-03 to 1.00000E+05 Mev.	12-00018	01/03/12
24000.84p	5758	Update of MCPLIB04 Photon Compton Broadening Data For MCNP5 see LA-UR- Energy range: 1.00000E-03 to 1.00000E+05 Mev.	12-00018	01/03/12
25000.84p	5674	Update of MCPLIB04 Photon Compton Broadening Data For MCNP5 see LA-UR- Energy range: 1.00000E-03 to 1.00000E+05 Mev.	12-00018	01/03/12
26000.84p	5794	Update of MCPLIB04 Photon Compton Broadening Data For MCNP5 see LA-UR- Energy range: 1.00000E-03 to 1.00000E+05 Mev.	12-00018	01/03/12
28000.84p	5902	Update of MCPLIB04 Photon Compton Broadening Data For MCNP5 see LA-UR- Energy range: 1.00000E-03 to 1.00000E+05 Mev.	12-00018	01/03/12
82000.84p	10086	Update of MCPLIB04 Photon Compton Broadening Data For MCNP5 see LA-UR- Energy range: 1.00000E-03 to 1.00000E+05 Mev.	12-00018	01/03/12

total 6579868

comment. 28 cross sections modified by free gas thermal treatment.

maximum photon energy set to 100.0 mev (maximum electron energy)

tables from file xdata/el03

1000.03e	2329		6/6/98
6000.03e	2333	Energy range: 1.00000E-03 to 1.00000E+03 Mev.	6/6/98
7000.03e	2333	Energy range: 1.00000E-03 to 1.00000E+03 Mev.	6/6/98
8000.03e	2333	Energy range: 1.00000E-03 to 1.00000E+03 Mev.	6/6/98
14000.03e	2339	Energy range: 1.00000E-03 to 1.00000E+03 Mev.	6/6/98
24000.03e	2345	Energy range: 1.00000E-03 to 1.00000E+03 Mev.	6/6/98
25000.03e	2345	Energy range: 1.00000E-03 to 1.00000E+03 Mev.	6/6/98
26000.03e	2345	Energy range: 1.00000E-03 to 1.00000E+03 Mev.	6/6/98
28000.03e	2347	Energy range: 1.00000E-03 to 1.00000E+03 Mev.	6/6/98
82000.03e	2373	Energy range: 1.00000E-03 to 1.00000E+03 Mev.	6/6/98

1particles and energy limits

print table 101

particle type	particle cutoff energy	maximum particle energy	smallest table maximum	largest table maximum	always use table below	always use model above
1 n neutron	0.0000E+00	1.0000E+36	2.0000E+01	2.0000E+02	1.0000E+36	1.0000E+36
2 p photon	1.0000E-03	1.0000E+02	1.0000E+05	1.0000E+05	1.0000E+36	1.0000E+36
3 e electron	1.0000E-03	1.0000E+02	1.0000E+02	1.0000E+02	1.0000E+36	1.0000E+36

warning. material 2 has been set to a conductor.

warning. material 3 has been set to a conductor.

warning. material 4 has been set to a conductor.

comment. setting up hash-based fast table search for xsec tables

=====> Set up arrays for hash-based fast table search for xsec data

number of hash bins = 8192  
min hash table energy = 1.00000E-11  
max hash table energy = 2.00000E+02

nuclide	ne	emin	emax	ave_bins	min_bins	max_bins
1001.84c	590	1.00000E-11	2.00000E+01	0.1	0.0	1.0
1002.84c	583	1.00000E-11	1.50000E+02	0.1	0.0	2.0
6000.84c	1328	1.00000E-11	1.50000E+02	0.2	0.0	9.0
7014.84c	1826	1.00000E-11	1.50000E+02	0.2	0.0	20.0
7015.84c	939	1.00000E-11	2.00000E+01	0.1	0.0	6.0
8016.84c	2961	1.00000E-11	1.50000E+02	0.4	0.0	30.0
8017.84c	620	1.00000E-11	2.00000E+01	0.1	0.0	2.0
14028.84c	8019	1.00000E-11	1.50000E+02	1.0	0.0	115.0
14029.84c	4979	1.00000E-11	1.50000E+02	0.6	0.0	85.0
14030.84c	6089	1.00000E-11	1.50000E+02	0.7	0.0	89.0
24050.84c	29758	1.00000E-11	1.50000E+02	3.6	0.0	176.0
24052.84c	30705	1.00000E-11	1.50000E+02	3.7	0.0	214.0
24053.84c	21659	1.00000E-11	1.50000E+02	2.6	0.0	114.0



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24054.84c	14261	1.00000E-11	1.50000E+02	1.7	0.0	155.0
25055.84c	11703	1.00000E-11	6.00000E+01	1.4	0.0	87.0
26054.84c	18775	1.00000E-11	1.50000E+02	2.3	0.0	156.0
26056.84c	26742	1.00000E-11	1.50000E+02	3.3	0.0	164.0
26057.84c	15731	1.00000E-11	1.50000E+02	1.9	0.0	175.0
26058.84c	10972	1.00000E-11	2.00000E+01	1.3	0.0	106.0
28058.84c	43443	1.00000E-11	1.50000E+02	5.3	0.0	285.0
28060.84c	33910	1.00000E-11	1.50000E+02	4.1	0.0	177.0
28061.84c	11091	1.00000E-11	1.50000E+02	1.4	0.0	96.0
28062.84c	11345	1.00000E-11	1.50000E+02	1.4	0.0	134.0
28064.84c	10310	1.00000E-11	1.50000E+02	1.3	0.0	276.0
82204.84c	11175	1.00000E-11	2.00000E+02	1.4	0.0	108.0
82206.84c	33882	1.00000E-11	2.00000E+02	4.1	0.0	256.0
82207.84c	11334	1.00000E-11	2.00000E+02	1.4	0.0	111.0
82208.84c	7220	1.00000E-11	1.50000E+02	0.9	0.0	112.0

\*\*\*\*\*

dump no. 1 on file NCT\_HP\_SC-30G3\_252Cf\_0.r nps = 0 coll = 0 ctm = 0.00  
nrn = 0

7 warning messages so far.  
1problem summary

run terminated when it had used 1200 minutes of computer time.

+ 08/29/21 09:52:54

====> 205.55 M histories/hr (based on wall-clock time in mcrun)

title HP/SC-30G3 with a Concentrated 252Cf Neutron Source - NCT probid = 08/29/21 09:02:49

neutron creation	tracks	weight (per source particle)	energy	neutron loss	tracks	weight (per source particle)	energy
source	171447570	1.0000E+00	3.1175E+00	escape	2218146	1.2938E-02	1.7473E-02
nucl. interaction	0	0.	0.	energy cutoff	0	0.	0.
particle decay	0	0.	0.	time cutoff	0	0.	0.
weight window	0	0.	0.	weight window	0	0.	0.
cell importance	0	0.	0.	cell importance	0	0.	0.
weight cutoff	0	0.	0.	weight cutoff	0	0.	0.
e or t importance	0	0.	0.	e or t importance	0	0.	0.
dxtran	0	0.	0.	dxtran	0	0.	0.
forced collisions	0	0.	0.	forced collisions	0	0.	0.
exp. transform	0	0.	0.	exp. transform	0	0.	0.
upscattering	0	0.	1.2297E-06	downscattering	0	0.	3.0708E+00
photonuclear	0	0.	0.	capture	169294122	9.8744E-01	2.5583E-02
(n,xn)	129394	7.5471E-04	1.0222E-03	loss to (n,xn)	64696	3.7735E-04	4.6355E-03
prompt fission	0	0.	0.	loss to fission	0	0.	0.
delayed fission	0	0.	0.	nucl. interaction	0	0.	0.
prompt photofis	0	0.	0.	particle decay	0	0.	0.
tabular boundary	0	0.	0.	tabular boundary	0	0.	0.
tabular sampling	0	0.	0.	elastic scatter	0	0.	0.
total	171576964	1.0008E+00	3.1185E+00	total	171576964	1.0008E+00	3.1185E+00

number of neutrons banked	64698	average time of (shakes)	cutoffs
neutron tracks per source particle	1.0008E+00	escape	tco 1.0000E+33
neutron collisions per source particle	1.2235E+02	capture	eco 0.0000E+00
total neutron collisions	20975978939	capture or escape	wc1 0.0000E+00
net multiplication	1.0004E+00 0.0000	any termination	wc2 0.0000E+00

photon creation	tracks	weight (per source particle)	energy	photon loss	tracks	weight (per source particle)	energy
source	0	0.	0.	escape	2628755	1.5987E-02	2.8402E-02
nucl. interaction	0	0.	0.	energy cutoff	11	6.8289E-08	2.4878E-04
particle decay	0	0.	0.	time cutoff	0	0.	0.
weight window	0	0.	0.	weight window	0	0.	0.
cell importance	0	0.	0.	cell importance	0	0.	0.
weight cutoff	0	0.	0.	weight cutoff	0	0.	0.
e or t importance	0	0.	0.	e or t importance	0	0.	0.
dxtran	0	0.	0.	dxtran	0	0.	0.
forced collisions	0	0.	0.	forced collisions	0	0.	0.
exp. transform	0	0.	0.	exp. transform	0	0.	0.
from neutrons	177752852	1.0395E+00	2.4178E+00	compton scatter	0	0.	1.9557E+00
bremsstrahlung	200339191	1.1722E+00	6.8769E-02	capture	564406502	3.3013E+00	4.2040E-01
p-annihilation	22175546	1.2986E-01	6.6359E-02	pair production	11087773	6.4929E-02	1.9237E-01
photonuclear	0	0.	0.	photonuclear abs	0	0.	0.

# ATTACHMENT A – Responses to RAI

electron x-rays	0	0.	0.	loss to photofis	0	0.	0.
compton fluores	0	0.	0.				
muon capt fluores	0	0.	0.				
1st fluorescence	153987535	9.0089E-01	4.2572E-02				
2nd fluorescence	23867917	1.3965E-01	1.5735E-03				
cerenkov	0	0.	0.				
(gamma,xgamma)	0	0.	0.				
tabular sampling	0	0.	0.				
prompt photofis	0	0.	0.				
total	578123041	3.3822E+00	2.5971E+00	total	578123041	3.3822E+00	2.5971E+00

number of photons banked	424135495	average time of (shakes)	cutoffs		
photon tracks per source particle	3.3720E+00	escape	2.9777E+04	tco	1.0000E+33
photon collisions per source particle	1.0689E+01	capture	1.1985E+04	eco	1.0000E-03
total photon collisions	1832625563	capture or escape	1.2070E+04	wc1	0.0000E+00
		any termination	1.2169E+04	wc2	0.0000E+00

computer time so far in this run	1201.19 minutes	maximum number ever in bank	36
computer time in mcrun	1200.92 minutes	bank overflows to backup file	0
source particles per minute	1.4276E+05		
random numbers generated	420792660560	most random numbers used was	44705 in history 41959132

range of sampled source weights = 1.0000E+00 to 1.0000E+00

number of histories processed by each thread									
7111511	7128881	7129558	7163609	7171458	7169343	7132174	7127869	7152665	7134414
7151424	7161679	7187632	7133190	7167871	7170197	7167598	7152356	7153966	7099399
7140547	7113408	7067195	7159626						

1neutron activity in each cell

print table 126

cell	tracks entering	population	collisions	collisions * weight (per history)	number weighted energy	flux weighted energy	average track weight (relative)	average track mfp (cm)
1	1	0	0	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
2	2	198133649	171447340	160035752	9.3344E-01	2.2084E-03	2.3253E+00	3.0950E+00
3	3	434888	213847	1319064	7.6937E-03	8.0301E-04	1.0050E+00	4.2307E+00
4	4	145243	77873	292410	1.7055E-03	2.4369E-03	1.0701E+00	4.2895E+00
5	5	127385	67644	118004	6.8828E-04	2.8420E-03	9.4328E-01	4.3012E+00
6	6	101097	72199	276431	1.6123E-03	2.8107E-03	8.6943E-01	4.9968E+00
7	7	14769462	7314174	22951209	1.3387E-01	2.2312E-04	8.0674E-01	2.7209E+00
8	8	8607744	5274740	34178538	1.9935E-01	3.3188E-04	8.8166E-01	3.7758E+00
9	9	4725019	3556812	5755947	3.3573E-02	6.2911E-04	1.0707E+00	3.7016E+00
10	10	94390	61268	249834	1.4572E-03	2.2166E-03	7.0206E-01	4.9979E+00
11	11	152941	95232	549418	3.2046E-03	2.9508E-03	7.4214E-01	5.3276E+00
12	12	66353	38500	72463	4.2265E-04	2.3313E-03	8.4294E-01	4.7190E+00
13	13	305339	164633	994059	5.7980E-03	6.3864E-04	1.0600E+00	3.9470E+00
14	14	138863	72349	345998	2.0181E-03	2.5808E-03	1.0088E+00	4.2553E+00
15	15	33030	24369	27468	1.6021E-04	1.6313E-03	6.0280E-01	4.0499E+00
16	16	27497	22717	11833	6.9018E-05	9.3338E-04	5.4818E-01	4.5738E+00
17	17	202892850	171421599	20716256087	1.2083E+02	6.9990E-05	4.4758E-01	9.5472E-01
18	18	107976	54555	0	0.0000E+00	2.6158E-03	9.8994E-01	0.0000E+00
19	19	6859	5547	0	0.0000E+00	3.4267E-03	7.3205E-01	0.0000E+00
20	20	5669593	3553671	0	0.0000E+00	4.3367E-04	9.4065E-01	0.0000E+00
21	21	12801	9535	0	0.0000E+00	4.9722E-03	6.8307E-01	0.0000E+00
22	22	24214	18552	0	0.0000E+00	1.1603E-03	5.7148E-01	0.0000E+00
23	23	153514	69573	0	0.0000E+00	2.3613E-03	1.1061E+00	0.0000E+00
24	24	3616573	3023203	0	0.0000E+00	5.7887E-04	5.0208E-01	0.0000E+00
25	201	6085358	3024714	7308145	4.2626E-02	6.0129E-04	7.8211E-01	2.6453E+00
26	202	4351129	2800586	23399829	1.3648E-01	3.4088E-04	6.9574E-01	1.5881E+01
27	203	2812747	2428292	1836450	1.0711E-02	6.7767E-04	9.4032E-01	2.6264E+00
28	204	5021934	3024251	0	0.0000E+00	7.3924E-04	1.0096E+00	0.0000E+00
29	205	2236980	2218146	0	0.0000E+00	1.1779E-03	1.2852E+00	0.0000E+00
30	301	39100	39100	0	0.0000E+00	9.8804E-04	1.0633E+00	0.0000E+00
31	302	18393	18393	0	0.0000E+00	9.9483E-04	1.1731E+00	0.0000E+00
total	460912921	380213414	20975978939	1.2235E+02				

1photon activity in each cell

print table 126

cell	tracks entering	population	collisions	collisions * weight (per history)	number weighted energy	flux weighted energy	average track weight (relative)	average track mfp (cm)
1	1	0	0	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
2	2	2948644	3779326	436308	2.5450E-03	1.8669E+00	1.8669E+00	1.9081E+01
3	3	12905043	15687878	43060382	2.5137E-01	9.9250E-01	9.9250E-01	1.8220E+00
4	4	2470775	6829420	12709919	7.4270E-02	1.3924E+00	1.3924E+00	1.3409E+00
5	5	301646	718601	1194220	7.0099E-03	1.4225E+00	1.4225E+00	1.3624E+00
6	6	114796	194468	491318	2.9061E-03	1.1693E+00	1.1693E+00	1.9379E+00
7	7	150210736	161269954	240405104	1.4034E+00	1.1485E+00	1.1485E+00	1.9332E+00
8	8	82746569	270845782	513589535	3.0050E+00	1.4961E+00	1.4961E+00	1.3986E+00

# ATTACHMENT A – Responses to RAI

9	9	2590123	4498478	5157380	3.0484E-02	1.6210E+00	1.6210E+00	1.0121E+00	2.2182E+00
10	10	253385	353901	976300	5.7272E-03	1.0730E+00	1.0730E+00	1.0053E+00	1.8871E+00
11	11	229226	374990	1132686	6.6857E-03	1.0969E+00	1.0969E+00	1.0111E+00	1.8614E+00
12	12	609477	652299	1081364	6.3154E-03	9.9201E-01	9.9201E-01	1.0013E+00	1.8524E+00
13	13	12130203	14776858	39342827	2.2963E-01	9.8369E-01	9.8369E-01	1.0007E+00	1.8094E+00
14	14	2322841	6581530	12432876	7.2665E-02	1.3941E+00	1.3941E+00	1.0018E+00	1.3411E+00
15	15	36295	83125	138042	8.2038E-04	1.5113E+00	1.5113E+00	1.0173E+00	1.2340E+00
16	16	13805	16067	9353	5.7268E-05	1.5651E+00	1.5651E+00	1.0452E+00	2.0634E+00
17	17	27644010	189516876	947524648	5.5282E+00	9.9928E-01	9.9928E-01	1.0003E+00	1.3126E+01
18	18	203293	198688	0	0.0000E+00	1.4293E+00	1.4293E+00	1.0041E+00	0.0000E+00
19	19	8177	7448	0	0.0000E+00	1.1690E+00	1.1690E+00	1.0081E+00	0.0000E+00
20	20	3304874	2966609	0	0.0000E+00	1.6304E+00	1.6304E+00	1.0115E+00	0.0000E+00
21	21	32724	29352	0	0.0000E+00	1.0027E+00	1.0027E+00	1.0039E+00	0.0000E+00
22	22	11691	10893	0	0.0000E+00	1.5821E+00	1.5821E+00	1.0419E+00	0.0000E+00
23	23	2513390	2379166	0	0.0000E+00	1.0778E+00	1.0778E+00	1.0010E+00	0.0000E+00
24	24	2791707	2689575	0	0.0000E+00	1.5598E+00	1.5598E+00	1.0599E+00	0.0000E+00
25	201	4047942	5056171	7983354	4.8988E-02	1.6275E+00	1.6275E+00	1.0511E+00	2.0098E+00
26	202	3583293	3320205	1885027	1.1510E-02	1.4544E+00	1.4544E+00	1.0475E+00	1.1616E+02
27	203	3180937	3651603	3074920	1.8850E-02	1.5817E+00	1.5817E+00	1.0496E+00	1.9935E+00
28	204	3731514	3231746	0	0.0000E+00	1.5592E+00	1.5592E+00	1.0327E+00	0.0000E+00
29	205	2649542	2628755	0	0.0000E+00	1.7605E+00	1.7605E+00	1.0441E+00	0.0000E+00
30	301	45822	45822	0	0.0000E+00	1.7723E+00	1.7723E+00	1.0478E+00	0.0000E+00
31	302	20332	20332	0	0.0000E+00	1.7486E+00	1.7486E+00	1.0471E+00	0.0000E+00

total 323652812 702415918 1832625563 1.0706E+01  
 Summary of photons produced in neutron collisions in the tabular range

production by cell of photons created with energies above local photon energy cutoffs

cell	number of photons	weight per source neut	energy per source neut	avg photon energy	mev/gm per source neut	weight/neut collision	energy/neut collision
1	1	0	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
2	2	913424	5.32772E-03	1.61699E-02	3.03505E+00	5.70762E-03	1.73229E-02
3	3	204043	1.21350E-03	3.92881E-03	3.23759E+00	1.57727E-01	5.10654E-01
4	4	22626	1.46897E-04	1.79979E-04	1.22521E+00	8.61293E-02	1.05526E-01
5	5	7603	4.91958E-05	6.00596E-05	1.22083E+00	7.14764E-02	8.72604E-02
6	6	25875	1.54650E-04	3.74729E-04	2.42308E+00	9.59168E-02	2.32414E-01
7	7	4842344	2.85857E-02	1.13600E-01	3.97403E+00	2.13537E-01	8.48605E-01
8	8	2401312	1.53410E-02	2.11210E-02	1.37677E+00	7.69541E-02	1.05948E-01
9	9	1043625	6.17422E-03	2.08328E-02	3.37416E+00	1.83906E-01	6.20529E-01
10	10	19830	1.18263E-04	3.12908E-04	2.64585E+00	8.11578E-02	2.14732E-01
11	11	43556	2.60141E-04	6.29503E-04	2.41985E+00	8.11778E-02	1.96438E-01
12	12	6699	4.01448E-05	9.98461E-05	2.48715E+00	7.84950E-09	9.49827E-02
13	13	170500	1.01332E-03	3.41471E-03	3.36982E+00	4.93891E-08	1.74770E-01
14	14	24881	1.61778E-04	2.02119E-04	1.24936E+00	8.01637E-02	1.00153E-01
15	15	962	6.17579E-06	7.41154E-06	1.20010E+00	2.85212E-10	4.62608E-02
16	16	1047	6.20955E-06	2.17363E-05	3.50047E+00	4.72085E-09	8.99697E-02
17	17	166604224	9.71750E-01	2.20504E+00	2.26914E+00	1.46755E-05	8.04220E-03
18	18	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
19	19	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
20	20	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
21	21	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
22	22	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
23	23	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
24	24	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
25	201	1043192	6.80803E-03	2.41630E-02	3.54919E+00	1.65460E-08	1.59715E-01
26	202	97096	5.66338E-04	1.45003E-03	2.56036E+00	2.07179E-09	4.14949E-03
27	203	280002	1.82082E-03	6.22352E-03	3.41798E+00	4.69431E-09	1.69988E-01
28	204	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
29	205	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
30	301	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
31	302	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
32	999	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
total	177752841	1.03954E+00	2.41783E+00	2.32586E+00			

Energy distribution of photons produced in neutron collisions in the tabular range

all sampled photons from neutron collisions in the tabular range, without regard to energy cutoffs

energy interval	number of photons	number frequency	cum number distribution	weight of photons	weight frequency	cum weight distribution
20.000	6	3.37547E-08	3.37547E-08	4.00680E-08	3.85438E-08	3.85438E-08
15.000	45	2.53160E-07	2.86915E-07	2.74434E-07	2.63994E-07	3.02538E-07
10.000	2187	1.23036E-05	1.25905E-05	1.50398E-05	1.44677E-05	1.47702E-05
9.000	118890	6.68850E-04	6.81441E-04	7.12815E-04	6.85699E-04	7.00470E-04
8.000	100988	5.68137E-04	1.24958E-03	6.87854E-04	6.61688E-04	1.36216E-03
7.000	1840912	1.03566E-02	1.16062E-02	1.07971E-02	1.03864E-02	1.17485E-02
6.000	429486	2.41620E-03	1.40224E-02	2.60062E-03	2.50169E-03	1.42502E-02
5.000	439717	2.47375E-03	1.64961E-02	2.66847E-03	2.56696E-03	1.68172E-02

## ATTACHMENT A – Responses to RAI

4.000	4067251	2.28815E-02	3.93776E-02	2.38383E-02	2.29315E-02	3.97487E-02
3.000	831880	4.67998E-03	4.40576E-02	5.01769E-03	4.82681E-03	4.45755E-02
2.000	164447507	9.25147E-01	9.69205E-01	9.59503E-01	9.23003E-01	9.67579E-01
1.000	1923435	1.08208E-02	9.80025E-01	1.17020E-02	1.12568E-02	9.78836E-01
0.500	2600383	1.46292E-02	9.94655E-01	1.61286E-02	1.55151E-02	9.94351E-01
0.100	830449	4.67193E-03	9.99327E-01	5.09152E-03	4.89784E-03	9.99248E-01
0.010	100569	5.65780E-04	9.99892E-01	6.60859E-04	6.35720E-04	9.99884E-01
0.000	19147	1.07717E-04	1.00000E+00	1.20422E-04	1.15842E-04	1.00000E+00

<----- energy interval containing the global photon energy cutoff, 1.000E-03 Mev

total	177752852	1.00000E+00	1.03954E+00	1.00000E+00
-------	-----------	-------------	-------------	-------------

warning. 11 photons from neutron collisions were created below a local photon energy cutoff and were not followed.

```

1tally      4      nps = 171447570
+           Package Surface Neutron Dose Rate (mrem/hr) @ Z = 111.12500
           tally type 4      track length estimate of particle flux.
           particle(s): neutrons
           this tally is modified by dose function DE4 and DF4.

           volumes
             cell:      301
                   3.81204E+02

cell 301
           5.68309E-09 0.0082
  
```

=====

results of 10 statistical checks for the estimated answer for the tally fluctuation chart (tfc) bin of tally 4

tfc bin	--mean--	-----relative error-----			----variance of the variance----			--figure of merit--		-pdf-
behavior	behavior	value	decrease	decrease rate	value	decrease	decrease rate	value	behavior	slope
desired	random	<0.10	yes	1/sqrt(nps)	<0.10	yes	1/nps	constant	random	>3.00
observed	random	0.01	yes	yes	0.00	yes	yes	constant	random	6.23
passed?	yes	yes	yes	yes	yes	yes	yes	yes	yes	yes

=====

this tally meets the statistical criteria used to form confidence intervals: check the tally fluctuation chart to verify.  
the results in other bins associated with this tally may not meet these statistical criteria.

----- estimated confidence intervals: -----

estimated asymmetric confidence interval(1,2,3 sigma): 5.6373E-09 to 5.7301E-09; 5.5909E-09 to 5.7766E-09; 5.5444E-09 to 5.8230E-09  
estimated symmetric confidence interval(1,2,3 sigma): 5.6367E-09 to 5.7295E-09; 5.5902E-09 to 5.7759E-09; 5.5438E-09 to 5.8224E-09

1analysis of the results in the tally fluctuation chart bin (tfc) for tally 4 with nps = 171447570 print table 160

normed average tally per history = 5.68309E-09	unnormed average tally per history = 2.16642E-06
estimated tally relative error = 0.0082	estimated variance of the variance = 0.0017
relative error from zero tallies = 0.0051	relative error from nonzero scores = 0.0064

number of nonzero history tallies = 39087	efficiency for the nonzero tallies = 0.0002
history number of largest tally = 47078243	largest unnormalized history tally = 3.73827E-01
(largest tally)/(average tally) = 1.72556E+05	(largest tally)/(avg nonzero tally) = 3.93396E+01

(confidence interval shift)/mean = 0.0001	shifted confidence interval center = 5.68371E-09
---	--

if the largest history score sampled so far were to occur on the next history, the tfc bin quantities would change as follows:

estimated quantities	value at nps	value at nps+1	value(nps+1)/value(nps)-1.
mean	5.68309E-09	5.68881E-09	0.001006
relative error	8.16920E-03	8.22268E-03	0.006548
variance of the variance	1.70279E-03	1.87581E-03	0.101605
shifted center	5.68371E-09	5.68375E-09	0.000006
figure of merit	1.24775E+01	1.23157E+01	-0.012968

the estimated inverse power slope of the 200 largest tallies starting at 6.41056E-02 is 6.2335  
the large score tail of the empirical history score probability density function appears to have no unsampled regions.

fom = (histories/minute)\*(f(x) signal-to-noise ratio)\*\*2 = (1.428E+05)\*( 9.349E-03)\*\*2 = (1.428E+05)\*(8.740E-05) = 1.248E+01

```

1tally      14      nps = 171447570
  
```

## ATTACHMENT A – Responses to RAI

+ 2-M from Package Surface Neutron Dose Rate (mrem/hr) @ Z = 111.12500  
tally type 4 track length estimate of particle flux.  
particle(s): neutrons  
this tally is modified by dose function DE14 and DF14.

volumes  
cell: 302  
1.01958E+03

cell 302  
7.14939E-10 0.0099

---



---

results of 10 statistical checks for the estimated answer for the tally fluctuation chart (tfc) bin of tally										14
tfc bin behavior	--mean-- behavior	-----relative error----- value decrease decrease rate	-----variance of the variance----- value decrease decrease rate	--figure of merit-- value behavior	-pdf- slope					
desired	random	<0.10	yes	1/sqrt(nps)	<0.10	yes	1/nps	constant	random	>3.00
observed	random	0.01	yes	yes	0.00	yes	yes	constant	random	10.00
passed?	yes	yes	yes	yes	yes	yes	yes	yes	yes	yes

---



---

this tally meets the statistical criteria used to form confidence intervals: check the tally fluctuation chart to verify.  
the results in other bins associated with this tally may not meet these statistical criteria.

----- estimated confidence intervals: -----

estimated asymmetric confidence interval(1,2,3 sigma): 7.0789E-10 to 7.2206E-10; 7.0081E-10 to 7.2914E-10; 6.9373E-10 to 7.3623E-10  
estimated symmetric confidence interval(1,2,3 sigma): 7.0786E-10 to 7.2202E-10; 7.0077E-10 to 7.2910E-10; 6.9369E-10 to 7.3619E-10

1analysis of the results in the tally fluctuation chart bin (tfc) for tally 14 with nps = 171447570 print table 160

normed average tally per history = 7.14939E-10	unnormed average tally per history = 7.28934E-07
estimated tally relative error = 0.0099	estimated variance of the variance = 0.0001
relative error from zero tallies = 0.0074	relative error from nonzero scores = 0.0066

number of nonzero history tallies = 18389	efficiency for the nonzero tallies = 0.0001
history number of largest tally = 160886395	largest unnormalized history tally = 2.35213E-02
(largest tally)/(average tally) = 3.22681E+04	(largest tally)/(avg nonzero tally) = 3.46099E+00

(confidence interval shift)/mean = 0.0001	shifted confidence interval center = 7.14977E-10
---	--

if the largest history score sampled so far were to occur on the next history, the tfc bin quantities would change as follows:

estimated quantities	value at nps	value at nps+1	value(nps+1)/value(nps)-1.
mean	7.14939E-10	7.15074E-10	0.000188
relative error	9.90682E-03	9.90675E-03	-0.000008
variance of the variance	1.20396E-04	1.20440E-04	0.000360
shifted center	7.14977E-10	7.14977E-10	0.000000
figure of merit	8.48433E+00	8.48446E+00	0.000016

the estimated slope of the 198 largest tallies starting at 1.61949E-02 appears to be decreasing at least exponentially.  
the empirical history score probability density function appears to be increasing at the largest history scores:  
please examine. see print table 161.  
the large score tail of the empirical history score probability density function appears to have no unsampled regions.

fom = (histories/minute)\*(f(x) signal-to-noise ratio)\*\*2 = (1.428E+05)\*( 7.709E-03)\*\*2 = (1.428E+05)\*(5.943E-05) = 8.484E+00

1tally 24 nps = 171447570  
+ Package Surface Gamma Dose Rate (mrem/hr) @ Z = 111.12500  
tally type 4 track length estimate of particle flux.  
particle(s): photons  
this tally is modified by dose function DE24 and DF24.

volumes  
cell: 301  
3.81204E+02

cell 301  
2.62073E-10 0.0085

## ATTACHMENT A – Responses to RAI

results of 10 statistical checks for the estimated answer for the tally fluctuation chart (tfc) bin of tally 24

tfc bin behavior	--mean-- behavior	-----relative error----- value decrease decrease rate	----variance of the variance---- value decrease decrease rate	--figure of merit-- value behavior	-pdf- slope
desired	random	<0.10 yes 1/sqrt(nps)	<0.10 yes 1/nps	constant random	>3.00
observed	random	0.01 yes yes	0.00 yes yes	constant random	4.56
passed?	yes	yes yes yes	yes yes yes	yes yes	yes

this tally meets the statistical criteria used to form confidence intervals: check the tally fluctuation chart to verify.  
the results in other bins associated with this tally may not meet these statistical criteria.

----- estimated confidence intervals: -----

estimated asymmetric confidence interval(1,2,3 sigma): 2.5990E-10 to 2.6434E-10; 2.5768E-10 to 2.6656E-10; 2.5546E-10 to 2.6878E-10  
estimated symmetric confidence interval(1,2,3 sigma): 2.5985E-10 to 2.6429E-10; 2.5763E-10 to 2.6651E-10; 2.5541E-10 to 2.6873E-10

1analysis of the results in the tally fluctuation chart bin (tfc) for tally 24 with nps = 171447570 print table 160

normed average tally per history = 2.62073E-10	unnormed average tally per history = 9.99030E-08
estimated tally relative error = 0.0085	estimated variance of the variance = 0.0038
relative error from zero tallies = 0.0047	relative error from nonzero scores = 0.0070

number of nonzero history tallies = 44645	efficiency for the nonzero tallies = 0.0003
history number of largest tally = 56671873	largest unnormalized history tally = 2.66690E-02
(largest tally)/(average tally) = 2.66949E+05	(largest tally)/(avg nonzero tally) = 6.95137E+01

(confidence interval shift)/mean = 0.0002	shifted confidence interval center = 2.62116E-10
---	--

if the largest history score sampled so far were to occur on the next history, the tfc bin quantities would change as follows:

estimated quantities	value at nps	value at nps+1	value(nps+1)/value(nps)-1.
mean	2.62073E-10	2.62481E-10	0.001557
relative error	8.46907E-03	8.59762E-03	0.015179
variance of the variance	3.81789E-03	4.64129E-03	0.215670
shifted center	2.62116E-10	2.62122E-10	0.000020
figure of merit	1.16095E+01	1.12650E+01	-0.029681

the estimated inverse power slope of the 200 largest tallies starting at 3.19323E-03 is 4.5605  
the large score tail of the empirical history score probability density function appears to have no unsampled regions.

fom = (histories/minute)\*(f(x) signal-to-noise ratio)\*\*2 = (1.428E+05)\*( 9.018E-03)\*\*2 = (1.428E+05)\*(8.132E-05) = 1.161E+01

1tally 34 nps = 171447570  
+ 2-M from Package Surface Gamma Dose Rate (mrem/hr) @ Z = 111.12500  
tally type 4 track length estimate of particle flux.  
particle(s): photons  
this tally is modified by dose function DE34 and DF34.

volumes  
cell: 302  
1.01958E+03

cell 302  
3.11558E-11 0.0095

results of 10 statistical checks for the estimated answer for the tally fluctuation chart (tfc) bin of tally 34

tfc bin behavior	--mean-- behavior	-----relative error----- value decrease decrease rate	----variance of the variance---- value decrease decrease rate	--figure of merit-- value behavior	-pdf- slope
desired	random	<0.10 yes 1/sqrt(nps)	<0.10 yes 1/nps	constant random	>3.00
observed	random	0.01 yes yes	0.00 yes yes	constant random	10.00
passed?	yes	yes yes yes	yes yes yes	yes yes	yes

this tally meets the statistical criteria used to form confidence intervals: check the tally fluctuation chart to verify.  
the results in other bins associated with this tally may not meet these statistical criteria.

## ATTACHMENT A – Responses to RAI

----- estimated confidence intervals: -----

estimated asymmetric confidence interval(1,2,3 sigma): 3.0860E-11 to 3.1455E-11; 3.0563E-11 to 3.1753E-11; 3.0266E-11 to 3.2050E-11  
estimated symmetric confidence interval(1,2,3 sigma): 3.0858E-11 to 3.1453E-11; 3.0561E-11 to 3.1751E-11; 3.0263E-11 to 3.2048E-11

1analysis of the results in the tally fluctuation chart bin (tfc) for tally 34 with nps = 171447570 print table 160

normed average tally per history = 3.11558E-11	unnormed average tally per history = 3.17657E-08
estimated tally relative error = 0.0095	estimated variance of the variance = 0.0003
relative error from zero tallies = 0.0070	relative error from nonzero scores = 0.0065
number of nonzero history tallies = 20228	efficiency for the nonzero tallies = 0.0001
history number of largest tally = 141742412	largest unnormalized history tally = 1.99122E-03
(largest tally)/(average tally) = 6.26847E+04	(largest tally)/(avg nonzero tally) = 7.39577E+00
(confidence interval shift)/mean = 0.0001	shifted confidence interval center = 3.11579E-11

if the largest history score sampled so far were to occur on the next history, the tfc bin quantities would change as follows:

estimated quantities	value at nps	value at nps+1	value(nps+1)/value(nps)-1.
mean	3.11558E-11	3.11672E-11	0.000366
relative error	9.54731E-03	9.55082E-03	0.000367
variance of the variance	2.69260E-04	2.70617E-04	0.005037
shifted center	3.11579E-11	3.11579E-11	0.000000
figure of merit	9.13532E+00	9.12861E+00	-0.000734

the estimated slope of the 200 largest tallies starting at 1.14935E-03 appears to be decreasing at least exponentially.  
the empirical history score probability density function appears to be increasing at the largest history scores:  
please examine. see print table 161.  
the large score tail of the empirical history score probability density function appears to have no unsampled regions.

fom = (histories/minute)\*(f(x) signal-to-noise ratio)\*\*2 = (1.428E+05)\*( 7.999E-03)\*\*2 = (1.428E+05)\*(6.399E-05) = 9.135E+00

1status of the statistical checks used to form confidence intervals for the mean for each tally bin

tally result of statistical checks for the tfc bin (the first check not passed is listed) and error magnitude check for all bins

4	passed the 10 statistical checks for the tally fluctuation chart bin result
passed all bin error check:	1 tally bins all have relative errors less than 0.10 with no zero bins
14	passed the 10 statistical checks for the tally fluctuation chart bin result
passed all bin error check:	1 tally bins all have relative errors less than 0.10 with no zero bins
24	passed the 10 statistical checks for the tally fluctuation chart bin result
passed all bin error check:	1 tally bins all have relative errors less than 0.10 with no zero bins
34	passed the 10 statistical checks for the tally fluctuation chart bin result
passed all bin error check:	1 tally bins all have relative errors less than 0.10 with no zero bins

the 10 statistical checks are only for the tally fluctuation chart bin and do not apply to other tally bins.

1tally fluctuation charts

nps	mean	tally error	4 vov	4 slope	fom	nps	mean	tally error	14 vov	14 slope	fom	nps	mean	tally error	24 vov	24 slope	fom
16384000	5.9170E-09	0.0265	0.0142	2.7	12	7.4784E-10	0.0313	0.0012	2.4	9.0E+00	2.5732E-10	0.0261	0.0194	3.0	13		
32768000	5.8371E-09	0.0180	0.0056	3.7	13	7.3031E-10	0.0224	0.0006	2.3	8.7E+00	2.5931E-10	0.0197	0.0172	2.8	11		
49152000	5.8140E-09	0.0155	0.0062	3.8	12	7.2340E-10	0.0184	0.0004	2.1	8.6E+00	2.6214E-10	0.0163	0.0133	2.5	11		
65536000	5.8045E-09	0.0134	0.0045	3.1	12	7.1340E-10	0.0160	0.0003	2.0	8.5E+00	2.6326E-10	0.0145	0.0141	2.7	10		
81920000	5.7419E-09	0.0120	0.0035	3.2	12	7.1880E-10	0.0143	0.0003	2.1	8.5E+00	2.6244E-10	0.0126	0.0103	3.2	11		
98304000	5.7412E-09	0.0109	0.0028	4.3	12	7.1736E-10	0.0131	0.0002	2.2	8.5E+00	2.6052E-10	0.0114	0.0079	3.6	11		
114688000	5.7437E-09	0.0101	0.0024	5.8	12	7.1261E-10	0.0121	0.0002	2.6	8.5E+00	2.6185E-10	0.0106	0.0069	3.5	11		
131072000	5.7188E-09	0.0093	0.0020	6.1	13	7.1480E-10	0.0113	0.0002	10.0	8.5E+00	2.6196E-10	0.0098	0.0057	3.6	11		
147456000	5.6975E-09	0.0088	0.0018	6.7	13	7.1275E-10	0.0107	0.0001	10.0	8.5E+00	2.6231E-10	0.0092	0.0047	3.8	11		
163840000	5.6938E-09	0.0084	0.0018	5.7	12	7.1530E-10	0.0101	0.0001	10.0	8.5E+00	2.6166E-10	0.0087	0.0040	4.4	12		
171447570	5.6831E-09	0.0082	0.0017	6.2	12	7.1494E-10	0.0099	0.0001	10.0	8.5E+00	2.6207E-10	0.0085	0.0038	4.6	12		

nps	mean	tally error	34 vov	34 slope	fom
16384000	3.0563E-11	0.0308	0.0029	2.3	9.2E+00
32768000	3.0828E-11	0.0222	0.0015	2.2	8.9E+00
49152000	3.1033E-11	0.0180	0.0010	3.6	9.0E+00
65536000	3.0838E-11	0.0156	0.0007	10.0	9.0E+00
81920000	3.0875E-11	0.0139	0.0006	10.0	9.0E+00
98304000	3.0942E-11	0.0127	0.0005	10.0	9.1E+00

## ATTACHMENT A – Responses to RAI

```
114688000 3.1228E-11 0.0117 0.0004 10.0 9.1E+00
131072000 3.1171E-11 0.0109 0.0003 10.0 9.1E+00
147456000 3.1194E-11 0.0103 0.0003 10.0 9.2E+00
163840000 3.1136E-11 0.0098 0.0003 10.0 9.1E+00
171447570 3.1156E-11 0.0095 0.0003 10.0 9.1E+00
```

\*\*\*\*\*

```
dump no. 2 on file NCT_HP_SC-30G3_252cf_0.r nps = 171447570 coll = 22808604502 ctm = 1200.92
nrn = 420792660560
tally data written to file NCT_HP_SC-30G3_252cf_0.m
```

8 warning messages so far.

run terminated when it had used 1200 minutes of computer time.

computer time = 1201.20 minutes

mcnp version 6 02/20/18

08/29/21 09:52:54

probid = 08/29/21 09:02:49

## 2. SC-30G3 HAC Model with <sup>252</sup>Cf – Polyethylene with Secondary Gammas

Code Name & Version = MCNP\_6.20, 6.2.0



```
+-----+
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+-----+
```

```
1mcnp version 6 1d=02/20/18 08/29/21 11:11:43
*****
i=HAC_HP_SC-30G3_252cf_0.i name=HAC_HP_SC-30G3_252cf_0. tasks 24
```

probid = 08/29/21 11:11:43

warning. universe map (print table 128) disabled.

comment. Physics models disabled.

```
1- title HP/SC-30G3 with a Concentrated 252Cf Neutron Source - HAC
2- c
3- c Universe Fill Boundary
4- c
5- 1 0 -107 108 -109 fill=1 $Shielded Container
6- imp:n=1 imp:p=1 trcl=1
7- c
8- c Payload Cell $Material Density 100%
9- c
10- 2 1 -0.9400 -1 2 -3 $Payload
11- imp:n=1 imp:p=1 u=1
12- c
13- c Shielded Container Cells $Material Density 100%
14- c
15- 3 2 -7.8526 -11 12 -13 -14 $Lower Flange Steel
16- ((11 :13 :-15 :-16)
```



## ATTACHMENT A – Responses to RAI

17-				(11 :16 :-17 :-18)	
18-				(11 :18 :-19 :-20)	
19-				(11 :20 :-21 :-22)	
20-				(-12 :26 :27)	
21-				(23 :24 :-27))	
22-				imp:n=1 imp:p=1	u=1
23-	4	3	-11.3500	-23 -24 25	\$Lower Flange Upper Lead
24-				imp:n=1 imp:p=1	u=1
25-	5	3	-11.3500	-26 -27 28	\$Lower Flange Lower Lead
26-				imp:n=1 imp:p=1	u=1
27-	6	2	-7.8526	(12 -26 -31):	\$Lower Flange Base Steel
28-				(-29 31 -32)	
29-				imp:n=1 imp:p=1	u=1
30-	7	2	-7.8526	16 33 -34 -45	\$Inner Shell Steel
31-				imp:n=1 imp:p=1	u=1
32-	8	3	-11.3500	(-16 17 18 -35):	\$Sidewall Lead
33-				(16 34 -35 -40):	
34-				(-18 19 20 -35):	
35-				(34 40 -43 -45)	
36-				imp:n=1 imp:p=1	u=1
37-	9	2	-7.8526	22 36 -37 -45	\$Outer Shell Steel
38-				imp:n=1 imp:p=1	u=1
39-	10	2	-7.8526	((38 -39 -41 45):	\$Upper Flange Steel
40-				(40 43 -44 -45))	
41-				((-38 :41 :42))	
42-				imp:n=1 imp:p=1	u=1
43-	11	2	-7.8526	-49 50 -51 -52	\$Lid Steel
44-				((39 :41 :-50 :-80)	
45-				(-41 :63 :-64 :65)	
46-				(-50 :51 :-65 :83)	
47-				(51 :-57 :58 :-59)	
48-				(-53 :54 :-55 :59))	
49-				imp:n=1 imp:p=1	u=1
50-	12	2	-7.8526	-50 -80 82 83	\$Lid Ring Steel
51-				(80 :-81 :-83 :-84)	
52-				imp:n=1 imp:p=1	u=1
53-	13	2	-7.8526	-81 86 -87 -89	\$Lid Base Steel
54-				(81 :-83 :87 :-88)	
55-				imp:n=1 imp:p=1	u=1
56-	14	3	-11.3500	-50 -82 85	\$Lid Plate Lead
57-				imp:n=1 imp:p=1	u=1
58-	15	3	-11.3500	53 -54 55 -56	\$Lid Ring Lead
59-				imp:n=1 imp:p=1	u=1
60-	16	2	-7.8526	59 60 -61 -62	\$Lid Ring Cover Plate Steel
61-				imp:n=1 imp:p=1	u=1
62-	c				
63-	c				
64-	c				
65-	17	1	-0.9400	((13 -33 -86):	\$Payload Cavity
66-				(-13 15 16 -33):	
67-				(-33 86 89):	
68-				(-33 -45 81 84 -89):	
69-				(-33 -45 80 -84):	
70-				(-38 42 45 80):	
71-				(-41 -42 80))	
72-				(1 :-2 :3)	
73-				imp:n=1 imp:p=1	u=1
74-	18	0		-23 -25 27	\$Lower Flange Upper Lead
75-				imp:n=1 imp:p=1	u=1
76-	19	0		(-26 -28 29 31):	\$ Axial Cavity
77-				(-28 -29 32)	\$Lower Flange Lower Lead
78-				imp:n=1 imp:p=1	u=1
79-	20	0		(-20 21 22 -36):	\$Sidewall Lead Outer Radial Gap
80-				(20 35 -36 -40):	
81-				(-36 40 44 -45)	
82-				imp:n=1 imp:p=1	u=1
83-	21	0		41 -63 64 -65	\$Lid Gasket Recess Cavity
84-				imp:n=1 imp:p=1	u=1
85-	22	0		53 -54 56 -59	\$Lid Lead Ring Axial Cavity
86-				imp:n=1 imp:p=1	u=1
87-	23	0		(-82 83 -87 88):	\$Lid Lead Plate Axial Cavity
88-				(-82 -85 87)	
89-				imp:n=1 imp:p=1	u=1
90-	24	0		((11 :-12 :14 :22)	\$Exterior Void
91-				(-22 :37 :45):	
92-				(-45 :49 :51 :52)):	
93-				(12 -29 -30):	
94-				(-51 57 -58 62):	
95-				(57 59 -60 -62):	
96-				(-58 59 61 -62))	
97-				imp:n=1 imp:p=1	u=1

## ATTACHMENT A – Responses to RAI

98-	C								
99-	C	HalfPACT Package Cells						\$Material Density 100%	
100-	C								
101-		201	4	-8.0128	(201 -202 204 -205):			\$HalfPACT ICV/OCV Steel Structure	
102-					(-202 203 -204):				
103-					(-202 205 -206)				
104-					imp:n=1 imp:p=1				
105-	C								
106-	C	HalfPACT Package Void Cells							
107-	C								
108-		202	0		-201 204 -205			\$HalfPACT ICV Interior Void	
109-					#1				
110-					imp:n=1 imp:p=1				
111-		203	0		(202 203 -206 -211):			\$HalfPACT OCA Foam Void	
112-					(-203 -211 214):				
113-					(206 -211 -215)				
114-					imp:n=1 imp:p=1				
115-		204	0		(211 -212 214 -215):			\$HalfPACT OCA Steel Structure	
116-					(-212 213 -214):				
117-					(-212 215 -216)				
118-					imp:n=1 imp:p=1				
119-		205	0		-999			\$HalfPACT OCA Exterior Void	
120-					((212 213 -216):				
121-					(-213):				
122-					(216))				
123-					(-301 :302 :303)				
124-					imp:n=1 imp:p=1				
125-	C								
126-	C	HalfPACT Package 1-meter Tally Cell							
127-	C								
128-		301	0		301 -302 -303			\$Package Side Middle @ 1-meter	
129-					imp:n=1 imp:p=1				
130-	C								
131-	C	world Cell							
132-	C								
133-		999	0		999				
134-					imp:n=0 imp:p=0				
135-									
136-	C								
137-	C	Payload Surfaces							
138-	C								
139-		1	c/z	0.00000	24.77769	1.27000		\$Radius	
140-		2	pz	51.07305				\$Plane, Bottom	
141-		3	pz	53.61305				\$Plane, Top	
142-	C								
143-	C	Shielded Container Lower Flange Surfaces							
144-	C								
145-		11	cz	35.43300				\$Radius, Outer	
146-		12	pz	0.38100				\$Plane, Lower Flange Bottom	
147-		13	pz	14.16304				\$Plane, Lower Flange Top	
148-		14	kz	-35.24250	1.00000	1		\$Chamfer, Bottom Outer Corner	
149-		15	cz	25.79370				\$Radius, Inner Shell Step	
150-		16	pz	13.97000				\$Plane, Inner Shell Step	
151-		17	cz	27.19070				\$Radius, Inner Lead Step	
152-		18	kz	10.47452	192.3724	-1		\$Cone, Inner Lead Step Vertex	
153-		19	cz	31.43250				\$Radius, Outer Lead Step	
154-		20	pz	5.08000				\$Plane, Outer Lead Step	
155-		21	cz	34.23920				\$Radius, Outer Shell Step	
156-		22	pz	4.44500				\$Plane, Outer Shell Step	
157-		23	cz	25.40000				\$Radius, Upper Lead Plate Recess	
158-		24	pz	10.18540				\$Plane, Upper Lead Plate Recess	
159-		25	pz	6.18490				\$Plane, Upper Lead Plate Bottom	
160-		26	cz	29.21000				\$Radius, Lower Lead Plate Recess	
161-		27	pz	5.71500				\$Plane, Lower Lead Plate Recess	
162-		28	pz	4.00050				\$Plane, Lower Lead Plate Bottom	
163-		29	cz	29.07030				\$Radius, Base Plate	
164-		30	pz	0.38100				\$Plane, Base Plate Bottom	
165-		31	pz	2.54000				\$Plane, Base Plate Weld Elevation	
166-		32	pz	3.81000				\$Plane, Base Plate Top	
167-	C								
168-	C	Shielded Container Sidewall Inner Shell Surfaces							
169-	C								
170-		33	cz	26.04770				\$Radius, Inner	
171-		34	cz	27.19070				\$Radius, Outer	
172-	C								
173-	C	Shielded Container Sidewall Lead Shell Surface							
174-	C								
175-		35	cz	33.47720				\$Radius, Outer	
176-	C								
177-	C	Shielded Container Sidewall Outer Shell Surfaces							
178-	C								

## ATTACHMENT A – Responses to RAI

179-	36	c	34.29000				\$Radius, Inner
180-	37	c	35.43300				\$Radius, Outer
181-		C					
182-		C					Shielded Container Upper Flange Surfaces
183-		C					
184-	38	c	25.72385				\$Radius, Inner
185-	39	c	35.43300				\$Radius, Outer
186-	40	p	97.15500				\$Plane, Upper Flange Bottom
187-	41	p	101.91750				\$Plane, Upper Flange Top
188-	42	k	30.60680	0.13247	1		\$Chamfer, Top Inner Corner
189-	43	c	27.24150				\$Radius, Inner Shell Step
190-	44	c	34.23920				\$Radius, Outer Shell Step
191-	45	p	97.79000				\$Plane, Shell Step Top
192-		C					
193-		C					Shielded Container Lid Surfaces
194-		C					
195-	49	c	35.43300				\$Radius, Lid Outer
196-	50	p	100.34270				\$Plane, Lid Bottom
197-	51	p	106.62920				\$Plane, Lid Top
198-	52	k	142.57020	1.00000	-1		\$Chamfer, Top Outside Corner
199-	53	c	22.54250				\$Radius, Lead Ring Recess Inner
200-	54	c	29.84500				\$Radius, Lead Ring Recess Outer
201-	55	p	104.21620				\$Plane, Lead Ring Recess Bottom
202-	56	p	105.93070				\$Plane, Lead Ring Top
203-	57	c	22.22500				\$Radius, Lead Ring Cover Recess Inner
204-	58	c	30.16250				\$Radius, Lead Ring Cover Recess Outer
205-	59	p	106.14660				\$Plane, Lead Ring Cover Recess Bottom
206-	60	c	22.27580				\$Radius, Lead Ring Cover Inner
207-	61	c	30.11170				\$Radius, Lead Ring Cover Outer
208-	62	p	106.55579				\$Plane, Lead Ring Cover Top
209-	63	c	28.57500				\$Radius, Gasket Recess Outer
210-	64	c	26.33980				\$Radius, Gasket Recess Inner
211-	65	p	102.23500				\$Plane, Gasket Recess Top
212-		C					
213-		C					Shielded Container Lid Ring Surfaces
214-		C					
215-	80	c	25.66035				\$Radius, Outer Upper
216-	81	c	25.52700				\$Radius, Outer Lower
217-	82	c	24.13000				\$Radius, Inner
218-	83	p	93.28150				\$Plane, Bottom
219-	84	k	26.24737	0.13247	1		\$Cone, Outer Radius Transition
220-	85	p	95.19920				\$Plane, Lead Plate Bottom
221-		C					
222-		C					Shielded Container Lid Base Surfaces
223-		C					
224-	86	p	90.52560				\$Plane, Bottom
225-	87	p	94.52610				\$Plane, Top
226-	88	c	24.06650				\$Radius, Lid Ring Step
227-	89	k	20.58124	0.13247	1		\$Chamfer, Bottom Outside Corner
228-		C					
229-		C					Shielded Container Universe Fill Boundary Surfaces
230-		C					
231-	107	c	35.43301				\$Radius, Fill Boundary
232-	108	p	-0.00001				\$Plane, Fill Boundary Bottom
233-	109	p	107.32771				\$Plane, Fill Boundary Top
234-		C					
235-		C					HalfPACT Package ICV/OCV Surfaces
236-		C					
237-	201	c	92.23375				\$Radius, Shell Inner
238-	202	c	93.34500				\$Radius, Shell Outer
239-	203	p	22.86000				\$Plane, Lower Head Bottom
240-	204	p	24.13000				\$Plane, Lower Head Top
241-	205	p	198.12000				\$Plane, Upper Head Bottom
242-	206	p	199.39000				\$Plane, Upper Head Top
243-		C					
244-		C					HalfPACT Package OCA Surfaces
245-		C					
246-	211	c	109.22000				\$Radius, Shell Inner
247-	212	c	109.85500				\$Radius, Shell Outer
248-	213	p	2.54000				\$Plane, Lower Head Bottom
249-	214	p	3.17500				\$Plane, Lower Head Top
250-	215	p	219.39250				\$Plane, Upper Head Bottom
251-	216	p	220.02750				\$Plane, Upper Head Top
252-		C					
253-		C					HalfPACT Package Tally Surfaces
254-		C					
255-	301	p	209.85500				\$Plane, Side Disk Inside @ 1.00-meter
256-	302	p	209.95500				\$Plane, Side Disk Outside @ 1.00-meter
257-	303	c/y	0.00000	111.12500	2.54000		\$Radius, Side Disk
258-		C					
259-		C					World Surface (Problem Boundary)

## ATTACHMENT A – Responses to RAI

```

260-      c
261-      999      sz  114.93500      400
262-
263-      c
264-      c      Physics Cards
265-      c
266-      mode n      p
comment. photonuclear physics may be needed (phys:p).
267-      c
268-      c      Material Cards
269-      c
270-      m1      1001.84C -0.143704      $Payload (Polyethylene)
271-      1002.84C -0.000033      6000.84C -0.856263
272-      plib = 84P
273-      c
274-      m2      26054.84C -0.058450      $Carbon Steel
275-      26056.84C -0.917540      26057.84C -0.021190      26058.84C -0.002820
276-      plib = 84P
277-      c
278-      m3      82204.84C -0.014000      $Lead
279-      82206.84C -0.241000      82207.84C -0.221000      82208.84C -0.524000
280-      plib = 84P
281-      c
282-      m4      14028.84C -0.009222      $Stainless Steel (ASTM A240, Type 304)
283-      14029.84C -0.000469      14030.84C -0.000309      24050.84C -0.008256
284-      24052.84C -0.159199      24053.84C -0.018052      24054.84C -0.004494
285-      25055.84C -0.020000      26054.84C -0.039746      26056.84C -0.623927
286-      26057.84C -0.014409      26058.84C -0.001918      28058.84C -0.068077
287-      28060.84C -0.026223      28061.84C -0.001140      28062.84C -0.003635
288-      28064.84C -0.000926
289-      plib = 84P
290-      c
291-      c      Specify Universe Transformations
292-      c
293-      *tr1      0.00000  56.80073  58.78195
294-      c
295-      c      Specify Explicit Analysis for Weight Windows Evaluation
296-      c
297-      cut:n  2j      0
298-      cut:p  2j      0
299-      c
300-      c      Source Cards
301-      c
302-      sdef par=1 axs=0 0 1 erg=d1 pos=d2 rad=d3 ext=d4
303-      sc1 Concentrated 252Cf Neutron Source
304-      si1 L 0.100000 0.500000 1.000000 2.000000 3.000000
305-      4.000000 6.000000 8.000000 10.000000 15.000000
306-      sp1 0.00E+00 1.80E+11 2.71E+11 5.36E+11 4.10E+11
307-      2.73E+11 2.66E+11 8.53E+10 2.44E+10 8.36E+09
308-      si2 L 0.000000 81.57842 111.12500
309-      sp2 1
310-      si3 0.000000 1.27000
311-      sp3 -21 1
312-      si4 -1.27000 1.27000
313-      sp4 -21 0 0
314-      c
315-      c      Package Tally Cards
316-      c
317-      f4:n 301
318-      fc4 Package 1-Meter Neutron Dose Rate (mrem/hr) @ Z = 111.12500
319-      sd4 2.02683
320-      f14:p 301
321-      fc14 Package 1-Meter Gamma Dose Rate (mrem/hr) @ Z = 111.12500
322-      sd14 2.02683
323-      c
324-      c      ANSI/ANS-6.1.1-1977 Neutron Flux-to-Dose Rate Factor Cards
325-      c
326-      de0 2.50E-08 1.00E-07 1.00E-06 1.00E-05 1.00E-04 $Energy (Mev)
327-      1.00E-03 1.00E-02 1.00E-01 5.00E-01 1.00E+00
328-      2.50E+00 5.00E+00 7.00E+00 1.00E+01 1.40E+01
329-      2.00E+01
330-      df0 3.67E-03 3.67E-03 4.46E-03 4.54E-03 4.18E-03 $Factor (mrem/hr)
331-      3.76E-03 3.56E-03 2.17E-02 9.26E-02 1.32E-01
332-      1.25E-01 1.56E-01 1.47E-01 1.47E-01 2.08E-01
333-      2.27E-01
334-      c
335-      c      ANSI/ANS-6.1.1-1977 Gamma Flux-to-Dose Rate Factor Cards
336-      c
337-      de14 0.01 0.03 0.05 0.07 0.10 $Energy (Mev)
338-      0.15 0.20 0.25 0.30 0.35
339-      0.40 0.45 0.50 0.55 0.60

```

# ATTACHMENT A – Responses to RAI

```

340-          0.65    0.70    0.80    1.00    1.40
341-          1.80    2.20    2.60    2.80    3.25
342-          3.75    4.25    4.75    5.00    5.25
343-          5.75    6.25    6.75    7.50    9.00
344-          11.00   13.00   15.00
345- df14 3.96E-03 5.82E-04 2.90E-04 2.58E-04 2.83E-04 $Factor (mrem/hr)
346-      3.79E-04 5.01E-04 6.31E-04 7.59E-04 8.78E-04
347-      9.85E-04 1.08E-03 1.17E-03 1.27E-03 1.36E-03
348-      1.44E-03 1.52E-03 1.68E-03 1.98E-03 2.51E-03
349-      2.99E-03 3.42E-03 3.82E-03 4.01E-03 4.41E-03
350-      4.83E-03 5.23E-03 5.60E-03 5.80E-03 6.01E-03
351-      6.37E-03 6.74E-03 7.11E-03 7.66E-03 8.77E-03
352-      1.03E-02 1.18E-02 1.33E-02
353- c
354- c Runtime and Print Cards
355- c
356- prdmp      j      j      1      2
357- ctme      9600

*****
* Random Number Generator = 1 *
* Random Number Seed = 19073486328125 *
* Random Number Multiplier = 19073486328125 *
* Random Number Adder = 0 *
* Random Number Bits Used = 48 *
* Random Number Stride = 152917 *
*****

comment. total nubar used if fissionable isotopes are present.

surface 11 and surface 37 are the same. 37 will be deleted.
surface 11 and surface 39 are the same. 39 will be deleted.
surface 11 and surface 49 are the same. 49 will be deleted.
surface 12 and surface 30 are the same. 30 will be deleted.
surface 17 and surface 34 are the same. 34 will be deleted.
surface 21 and surface 44 are the same. 44 will be deleted.
surface 31 and surface 213 are the same. 213 will be deleted.

comment. 7 surfaces were deleted for being the same as others.
1cells

print table 60

cell mat atom density gram density volume mass pieces neutron importance photon importance photon wt generation
1 1 0 0.00000E+00 0.00000E+00 4.23329E+05 0.00000E+00 1 1.0000E+00 1.0000E+00 -1.000E+00
2 2 1 1.21080E-01 9.40000E-01 1.28704E+01 1.20981E+01 1 1.0000E+00 1.0000E+00 -1.000E+00
3 3 2 8.46854E-02 7.85260E+00 1.86223E+04 1.46234E+05 1 1.0000E+00 1.0000E+00 -1.000E+00
4 4 3 3.29855E-02 1.13500E+01 8.10833E+03 9.20296E+04 1 1.0000E+00 1.0000E+00 -1.000E+00
5 5 3 3.29855E-02 1.13500E+01 4.59569E+03 5.21611E+04 1 1.0000E+00 1.0000E+00 -1.000E+00
6 6 2 8.46854E-02 7.85260E+00 9.15889E+03 7.19211E+04 1 1.0000E+00 1.0000E+00 -1.000E+00
7 7 2 8.46854E-02 7.85260E+00 1.60239E+04 1.25829E+05 1 1.0000E+00 1.0000E+00 -1.000E+00
8 8 3 3.29855E-02 1.13500E+01 1.07766E+05 1.22315E+06 1 1.0000E+00 1.0000E+00 -1.000E+00
9 9 2 8.46854E-02 7.85260E+00 2.33702E+04 1.83517E+05 1 1.0000E+00 1.0000E+00 -1.000E+00
10 10 2 8.46854E-02 7.85260E+00 8.54592E+03 6.71077E+04 1 1.0000E+00 1.0000E+00 -1.000E+00
11 11 2 8.46854E-02 7.85260E+00 1.87689E+04 1.47384E+05 1 1.0000E+00 1.0000E+00 -1.000E+00
12 12 2 8.46854E-02 7.85260E+00 1.61985E+03 1.27201E+04 1 1.0000E+00 1.0000E+00 -1.000E+00
13 13 2 8.46854E-02 7.85260E+00 7.90534E+03 6.20775E+04 1 1.0000E+00 1.0000E+00 -1.000E+00
14 14 3 3.29855E-02 1.13500E+01 9.40856E+03 1.06787E+05 1 1.0000E+00 1.0000E+00 -1.000E+00
15 15 3 3.29855E-02 1.13500E+01 2.06057E+03 2.33874E+04 1 1.0000E+00 1.0000E+00 -1.000E+00
16 16 2 8.46854E-02 7.85260E+00 5.27705E+02 4.14386E+03 1 1.0000E+00 1.0000E+00 -1.000E+00
17 17 1 1.21080E-01 9.40000E-01 0.00000E+00 0.00000E+00 0 1.0000E+00 1.0000E+00 -1.000E+00
18 18 0 0.00000E+00 0.00000E+00 9.52407E+02 0.00000E+00 1 1.0000E+00 1.0000E+00 -1.000E+00
19 19 0 0.00000E+00 0.00000E+00 5.43116E+02 0.00000E+00 1 1.0000E+00 1.0000E+00 -1.000E+00
20 20 0 0.00000E+00 0.00000E+00 1.59468E+04 0.00000E+00 1 1.0000E+00 1.0000E+00 -1.000E+00
21 21 0 0.00000E+00 0.00000E+00 1.22433E+02 0.00000E+00 1 1.0000E+00 1.0000E+00 -1.000E+00
22 22 0 0.00000E+00 0.00000E+00 2.59479E+02 0.00000E+00 1 1.0000E+00 1.0000E+00 -1.000E+00
23 23 0 0.00000E+00 0.00000E+00 1.24321E+03 0.00000E+00 1 1.0000E+00 1.0000E+00 -1.000E+00
24 24 0 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0 1.0000E+00 1.0000E+00 -1.000E+00
25 201 4 8.80954E-02 8.01280E+00 1.82252E+05 1.46035E+06 1 1.0000E+00 1.0000E+00 -1.000E+00
26 202 0 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0 1.0000E+00 1.0000E+00 -1.000E+00
27 203 0 0.00000E+00 0.00000E+00 3.27072E+06 0.00000E+00 1 1.0000E+00 1.0000E+00 -1.000E+00
28 204 0 0.00000E+00 0.00000E+00 1.42644E+05 0.00000E+00 1 1.0000E+00 1.0000E+00 -1.000E+00
29 205 0 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0 1.0000E+00 1.0000E+00 -1.000E+00
30 301 0 0.00000E+00 0.00000E+00 2.02683E+00 0.00000E+00 1 1.0000E+00 1.0000E+00 -1.000E+00

```

## ATTACHMENT A – Responses to RAI

```

31      999      0 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00      0 0.0000E+00 0.0000E+00 -1.000E+00
total
4.27451E+06 3.77881E+06
minimum source weight = 1.0000E+00    maximum source weight = 1.0000E+00
comment.  threading will be used when possible in portions of mcnp6.
comment.  threading will be used for n/p/e table physics.
comment.  threading will generally not be used for model physics.

1 warning message so far.
1cross-section tables
XSDIR used: C:\MCNP\MCNP_DATA\xsdir_mcnp6.2
print table 100

table    length

tables from file xdata/endl71x/H/1001.714nc
1001.84c  15325 H1 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53)    mat 125    12/17/12
Energy range: 1.0000E-11 to 2.0000E+01 MeV.
particle-production data for deuterons being expunged from 1001.84c
temperature = 2.1543E-07 adjusted to 2.5300E-08

tables from file xdata/endl71x/H/1002.714nc
1002.84c  7283 H2 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53)    mat 128    12/17/12
Energy range: 1.0000E-11 to 1.5000E+02 MeV.
particle-production data for protons being expunged from 1002.84c
particle-production data for tritons being expunged from 1002.84c
temperature = 2.1543E-07 adjusted to 2.5300E-08

tables from file xdata/endl71x/C/6000.714nc
6000.84c  55343 C0 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53)    mat 600    12/20/12
Energy range: 1.0000E-11 to 1.5000E+02 MeV.
particle-production data for protons being expunged from 6000.84c
particle-production data for deuterons being expunged from 6000.84c
particle-production data for alphas being expunged from 6000.84c
temperature = 2.1543E-07 adjusted to 2.5300E-08

tables from file xdata/endl71x/Si/14028.714nc
14028.84c 169896 Si28 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53)    mat1425    12/14/12
Energy range: 1.0000E-11 to 1.5000E+02 MeV.
particle-production data for protons being expunged from 14028.84c
particle-production data for deuterons being expunged from 14028.84c
particle-production data for tritons being expunged from 14028.84c
particle-production data for alphas being expunged from 14028.84c
temperature = 2.1543E-07 adjusted to 2.5300E-08

tables from file xdata/endl71x/Si/14029.714nc
14029.84c 158834 Si29 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53)    mat1428    12/14/12
Energy range: 1.0000E-11 to 1.5000E+02 MeV.
particle-production data for protons being expunged from 14029.84c
particle-production data for deuterons being expunged from 14029.84c
particle-production data for tritons being expunged from 14029.84c
particle-production data for alphas being expunged from 14029.84c
temperature = 2.1543E-07 adjusted to 2.5300E-08

tables from file xdata/endl71x/Si/14030.714nc
14030.84c 130018 Si30 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53)    mat1431    12/16/12
Energy range: 1.0000E-11 to 1.5000E+02 MeV.
particle-production data for protons being expunged from 14030.84c
particle-production data for deuterons being expunged from 14030.84c
particle-production data for tritons being expunged from 14030.84c
particle-production data for alphas being expunged from 14030.84c
temperature = 2.1543E-07 adjusted to 2.5300E-08

tables from file xdata/endl71x/Cr/24050.714nc
24050.84c 291186 Cr50 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53)    mat2425    12/13/12
Energy range: 1.0000E-11 to 1.5000E+02 MeV.
particle-production data for protons being expunged from 24050.84c
particle-production data for deuterons being expunged from 24050.84c
particle-production data for tritons being expunged from 24050.84c
particle-production data for alphas being expunged from 24050.84c
temperature = 2.1543E-07 adjusted to 2.5300E-08

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## ATTACHMENT A – Responses to RAI

tables from file xdata/endl71x/Cr/24052.714nc

24052.84c	310582	Cr52 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53)	mat2431	12/13/12
		Energy range: 1.00000E-11 to 1.50000E+02 Mev.		
		particle-production data for protons being expunged from 24052.84c		
		particle-production data for deuterons being expunged from 24052.84c		
		particle-production data for tritons being expunged from 24052.84c		
		particle-production data for alphas being expunged from 24052.84c		
		temperature = 2.1543E-07 adjusted to 2.5300E-08		

tables from file xdata/endl71x/Cr/24053.714nc

24053.84c	254692	Cr53 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53)	mat2434	12/13/12
		Energy range: 1.00000E-11 to 1.50000E+02 Mev.		
		particle-production data for protons being expunged from 24053.84c		
		particle-production data for deuterons being expunged from 24053.84c		
		particle-production data for tritons being expunged from 24053.84c		
		particle-production data for alphas being expunged from 24053.84c		
		temperature = 2.1543E-07 adjusted to 2.5300E-08		

tables from file xdata/endl71x/Cr/24054.714nc

24054.84c	190185	Cr54 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53)	mat2437	12/13/12
		Energy range: 1.00000E-11 to 1.50000E+02 Mev.		
		particle-production data for protons being expunged from 24054.84c		
		particle-production data for deuterons being expunged from 24054.84c		
		particle-production data for tritons being expunged from 24054.84c		
		particle-production data for alphas being expunged from 24054.84c		
		temperature = 2.1543E-07 adjusted to 2.5300E-08		

tables from file xdata/endl71x/Mn/25055.714nc

25055.84c	455909	Mn55 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53)	mat2525	12/18/12
		Energy range: 1.00000E-11 to 6.00000E+01 Mev.		
		particle-production data for protons being expunged from 25055.84c		
		particle-production data for deuterons being expunged from 25055.84c		
		particle-production data for tritons being expunged from 25055.84c		
		particle-production data for helions being expunged from 25055.84c		
		particle-production data for alphas being expunged from 25055.84c		
		probability tables used from 1.2500E-01 to 1.0000E+00 mev.		
		temperature = 2.1543E-07 adjusted to 2.5300E-08		

tables from file xdata/endl71x/Fe/26054.714nc

26054.84c	217705	Fe54 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53)	mat2625	12/22/12
		Energy range: 1.00000E-11 to 1.50000E+02 Mev.		
		particle-production data for protons being expunged from 26054.84c		
		particle-production data for deuterons being expunged from 26054.84c		
		particle-production data for tritons being expunged from 26054.84c		
		particle-production data for alphas being expunged from 26054.84c		
		temperature = 2.1543E-07 adjusted to 2.5300E-08		

tables from file xdata/endl71x/Fe/26056.714nc

26056.84c	352429	Fe56 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53)	mat2631	12/22/12
		Energy range: 1.00000E-11 to 1.50000E+02 Mev.		
		particle-production data for protons being expunged from 26056.84c		
		particle-production data for deuterons being expunged from 26056.84c		
		particle-production data for tritons being expunged from 26056.84c		
		particle-production data for alphas being expunged from 26056.84c		
		temperature = 2.1543E-07 adjusted to 2.5300E-08		

tables from file xdata/endl71x/Fe/26057.714nc

26057.84c	241212	Fe57 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53)	mat2634	12/22/12
		Energy range: 1.00000E-11 to 1.50000E+02 Mev.		
		particle-production data for protons being expunged from 26057.84c		
		particle-production data for deuterons being expunged from 26057.84c		
		particle-production data for tritons being expunged from 26057.84c		
		particle-production data for alphas being expunged from 26057.84c		
		temperature = 2.1543E-07 adjusted to 2.5300E-08		

tables from file xdata/endl71x/Fe/26058.714nc

26058.84c	135502	Fe58 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53)	mat2637	12/22/12
		Energy range: 1.00000E-11 to 2.00000E+01 Mev.		
		particle-production data for protons being expunged from 26058.84c		
		particle-production data for alphas being expunged from 26058.84c		
		temperature = 2.1543E-07 adjusted to 2.5300E-08		

## ATTACHMENT A – Responses to RAI

tables from file xdata/endl71x/Ni/28058.714nc						
28058.84c	420627	Ni58 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 1.50000E+02 Mev. particle-production data for protons being expunged from 28058.84c particle-production data for deuterons being expunged from 28058.84c particle-production data for tritons being expunged from 28058.84c particle-production data for alphas being expunged from 28058.84c temperature = 2.1543E-07 adjusted to 2.5300E-08	mat2825	12/15/12		
tables from file xdata/endl71x/Ni/28060.714nc						
28060.84c	344192	Ni60 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 1.50000E+02 Mev. particle-production data for protons being expunged from 28060.84c particle-production data for deuterons being expunged from 28060.84c particle-production data for tritons being expunged from 28060.84c particle-production data for alphas being expunged from 28060.84c temperature = 2.1543E-07 adjusted to 2.5300E-08	mat2831	12/17/12		
tables from file xdata/endl71x/Ni/28061.714nc						
28061.84c	190713	Ni61 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 1.50000E+02 Mev. particle-production data for protons being expunged from 28061.84c particle-production data for deuterons being expunged from 28061.84c particle-production data for tritons being expunged from 28061.84c particle-production data for alphas being expunged from 28061.84c temperature = 2.1543E-07 adjusted to 2.5300E-08	mat2834	12/13/12		
tables from file xdata/endl71x/Ni/28062.714nc						
28062.84c	169202	Ni62 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 1.50000E+02 Mev. particle-production data for protons being expunged from 28062.84c particle-production data for deuterons being expunged from 28062.84c particle-production data for tritons being expunged from 28062.84c particle-production data for alphas being expunged from 28062.84c probability tables used from 6.0000E-01 to 1.0000E+00 mev. temperature = 2.1543E-07 adjusted to 2.5300E-08	mat2837	12/17/12		
tables from file xdata/endl71x/Ni/28064.714nc						
28064.84c	152759	Ni64 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 1.50000E+02 Mev. particle-production data for protons being expunged from 28064.84c particle-production data for deuterons being expunged from 28064.84c particle-production data for tritons being expunged from 28064.84c particle-production data for alphas being expunged from 28064.84c temperature = 2.1543E-07 adjusted to 2.5300E-08	mat2843	12/17/12		
tables from file xdata/endl71x/Pb/82204.714nc						
82204.84c	392627	Pb204 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 2.00000E+02 Mev. particle-production data for protons being expunged from 82204.84c particle-production data for deuterons being expunged from 82204.84c particle-production data for tritons being expunged from 82204.84c particle-production data for helions being expunged from 82204.84c particle-production data for alphas being expunged from 82204.84c temperature = 2.1543E-07 adjusted to 2.5300E-08	mat8225	12/22/12		
tables from file xdata/endl71x/Pb/82206.714nc						
82206.84c	801388	Pb206 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 2.00000E+02 Mev. particle-production data for protons being expunged from 82206.84c particle-production data for deuterons being expunged from 82206.84c particle-production data for tritons being expunged from 82206.84c particle-production data for helions being expunged from 82206.84c particle-production data for alphas being expunged from 82206.84c temperature = 2.1543E-07 adjusted to 2.5300E-08	mat8231	12/22/12		
tables from file xdata/endl71x/Pb/82207.714nc						
82207.84c	353707	Pb207 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 2.00000E+02 Mev. particle-production data for protons being expunged from 82207.84c particle-production data for deuterons being expunged from 82207.84c particle-production data for tritons being expunged from 82207.84c particle-production data for helions being expunged from 82207.84c	mat8234	12/22/12		



## ATTACHMENT A – Responses to RAI

particle-production data for alphas being expunged from 82207.84c  
temperature = 2.1543E-07 adjusted to 2.5300E-08

tables from file xdata/endl71x/Pb/82208.714nc

82208.84c 317905 Pb208 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) mat8237 12/22/12  
Energy range: 1.00000E-11 to 1.50000E+02 Mev.  
particle-production data for protons being expunged from 82208.84c  
particle-production data for deuterons being expunged from 82208.84c  
particle-production data for tritons being expunged from 82208.84c  
particle-production data for alphas being expunged from 82208.84c  
temperature = 2.1543E-07 adjusted to 2.5300E-08

tables from file xdata/mcplib84

1000.84p	1974	Update of MCPLIB04 Photon Compton Broadening Data For MCNP5 see LA-UR-	12-00018	01/03/12
		Energy range: 1.00000E-03 to 1.00000E+05 Mev.		
6000.84p	3228	Update of MCPLIB04 Photon Compton Broadening Data For MCNP5 see LA-UR-	12-00018	01/03/12
		Energy range: 1.00000E-03 to 1.00000E+05 Mev.		
14000.84p	4868	Update of MCPLIB04 Photon Compton Broadening Data For MCNP5 see LA-UR-	12-00018	01/03/12
		Energy range: 1.00000E-03 to 1.00000E+05 Mev.		
24000.84p	5758	Update of MCPLIB04 Photon Compton Broadening Data For MCNP5 see LA-UR-	12-00018	01/03/12
		Energy range: 1.00000E-03 to 1.00000E+05 Mev.		
25000.84p	5674	Update of MCPLIB04 Photon Compton Broadening Data For MCNP5 see LA-UR-	12-00018	01/03/12
		Energy range: 1.00000E-03 to 1.00000E+05 Mev.		
26000.84p	5794	Update of MCPLIB04 Photon Compton Broadening Data For MCNP5 see LA-UR-	12-00018	01/03/12
		Energy range: 1.00000E-03 to 1.00000E+05 Mev.		
28000.84p	5902	Update of MCPLIB04 Photon Compton Broadening Data For MCNP5 see LA-UR-	12-00018	01/03/12
		Energy range: 1.00000E-03 to 1.00000E+05 Mev.		
82000.84p	10086	Update of MCPLIB04 Photon Compton Broadening Data For MCNP5 see LA-UR-	12-00018	01/03/12
		Energy range: 1.00000E-03 to 1.00000E+05 Mev.		

total 6172505

comment. 24 cross sections modified by free gas thermal treatment.

maximum photon energy set to 100.0 mev (maximum electron energy)

tables from file xdata/el03

1000.03e	2329		6/6/98
		Energy range: 1.00000E-03 to 1.00000E+03 Mev.	
6000.03e	2333		6/6/98
		Energy range: 1.00000E-03 to 1.00000E+03 Mev.	
14000.03e	2339		6/6/98
		Energy range: 1.00000E-03 to 1.00000E+03 Mev.	
24000.03e	2345		6/6/98
		Energy range: 1.00000E-03 to 1.00000E+03 Mev.	
25000.03e	2345		6/6/98
		Energy range: 1.00000E-03 to 1.00000E+03 Mev.	
26000.03e	2345		6/6/98
		Energy range: 1.00000E-03 to 1.00000E+03 Mev.	
28000.03e	2347		6/6/98
		Energy range: 1.00000E-03 to 1.00000E+03 Mev.	
82000.03e	2373		6/6/98
		Energy range: 1.00000E-03 to 1.00000E+03 Mev.	

1particles and energy limits

print table 101

particle type	particle cutoff energy	maximum particle energy	smallest table maximum	largest table maximum	always use table below	always use model above
1 n neutron	0.0000E+00	1.0000E+36	2.0000E+01	2.0000E+02	1.0000E+36	1.0000E+36
2 p photon	1.0000E-03	1.0000E+02	1.0000E+05	1.0000E+05	1.0000E+36	1.0000E+36
3 e electron	1.0000E-03	1.0000E+02	1.0000E+02	1.0000E+02	1.0000E+36	1.0000E+36

warning. material 2 has been set to a conductor.

warning. material 3 has been set to a conductor.

warning. material 4 has been set to a conductor.

comment. setting up hash-based fast table search for xsec tables

=====> Set up arrays for hash-based fast table search for xsec data

number of hash bins = 8192  
min hash table energy = 1.00000E-11  
max hash table energy = 2.00000E+02

# ATTACHMENT A – Responses to RAI

nuclide	ne	emin	emax	ave_bins	min_bins	max_bins
1001.84c	590	1.00000E-11	2.00000E+01	0.1	0.0	1.0
1002.84c	583	1.00000E-11	1.50000E+02	0.1	0.0	2.0
6000.84c	1328	1.00000E-11	1.50000E+02	0.2	0.0	9.0
14028.84c	8019	1.00000E-11	1.50000E+02	1.0	0.0	115.0
14029.84c	4979	1.00000E-11	1.50000E+02	0.6	0.0	85.0
14030.84c	6089	1.00000E-11	1.50000E+02	0.7	0.0	89.0
24050.84c	29758	1.00000E-11	1.50000E+02	3.6	0.0	176.0
24052.84c	30705	1.00000E-11	1.50000E+02	3.7	0.0	214.0
24053.84c	21659	1.00000E-11	1.50000E+02	2.6	0.0	114.0
24054.84c	14261	1.00000E-11	1.50000E+02	1.7	0.0	155.0
25055.84c	11703	1.00000E-11	6.00000E+01	1.4	0.0	87.0
26054.84c	18775	1.00000E-11	1.50000E+02	2.3	0.0	156.0
26056.84c	26742	1.00000E-11	1.50000E+02	3.3	0.0	164.0
26057.84c	15731	1.00000E-11	1.50000E+02	1.9	0.0	175.0
26058.84c	10972	1.00000E-11	2.00000E+01	1.3	0.0	106.0
28058.84c	43443	1.00000E-11	1.50000E+02	5.3	0.0	285.0
28060.84c	33910	1.00000E-11	1.50000E+02	4.1	0.0	177.0
28061.84c	11091	1.00000E-11	1.50000E+02	1.4	0.0	96.0
28062.84c	11345	1.00000E-11	1.50000E+02	1.4	0.0	134.0
28064.84c	10310	1.00000E-11	1.50000E+02	1.3	0.0	276.0
82204.84c	11175	1.00000E-11	2.00000E+02	1.4	0.0	108.0
82206.84c	33882	1.00000E-11	2.00000E+02	4.1	0.0	256.0
82207.84c	11334	1.00000E-11	2.00000E+02	1.4	0.0	111.0
82208.84c	7220	1.00000E-11	1.50000E+02	0.9	0.0	112.0

\*\*\*\*\*

dump no. 1 on file HAC\_HP\_SC-30G3\_252cf\_0.r nps = 0 coll = 0 ctm = 0.00  
nrn = 0

4 warning messages so far.  
warning. no photon-production mt found in acegam. zaid = 26056.84c  
nps = 27141026 nrn = 13 erg = 3.0000E+00

\*\*\*\*\*

dump no. 2 on file HAC\_HP\_SC-30G3\_252cf\_0.r nps = 323186056 coll = 26502596325 ctm = 1440.23  
nrn = 467834919751

\*\*\*\*\*

dump no. 3 on file HAC\_HP\_SC-30G3\_252cf\_0.r nps = 614221246 coll = 50367516678 ctm = 2880.31  
nrn = 889104062435  
warning. no reaction mt found. collision resampled. zaid = 26056.84c  
nps = 818273327 nrn = 19 erg = 8.0000E+00

\*\*\*\*\*

dump no. 4 on file HAC\_HP\_SC-30G3\_252cf\_0.r nps = 895132329 coll = 73403005255 ctm = 4320.63  
nrn = 1295733093149

\*\*\*\*\*

dump no. 5 on file HAC\_HP\_SC-30G3\_252cf\_0.r nps = 1220682347 coll = 100095115108 ctm = 5760.71  
nrn = 1766909838954

\*\*\*\*\*

dump no. 6 on file HAC\_HP\_SC-30G3\_252cf\_0.r nps = 1525439704 coll = 125084263532 ctm = 7201.14  
nrn = 2208025119877

\*\*\*\*\*

dump no. 7 on file HAC\_HP\_SC-30G3\_252cf\_0.r nps = 1830484900 coll = 150098473162 ctm = 8641.72  
nrn = 2649588136506  
1problem summary

run terminated when it had used 9600 minutes of computer time.  
+ 08/29/21 17:52:00

====> 304.79 M histories/hr (based on wall-clock time in mcrun)

title HP/SC-30G3 with a Concentrated 252Cf Neutron Source - HAC probid = 08/29/21 11:11:43  
neutron creation tracks weight energy neutron loss tracks weight energy

# ATTACHMENT A – Responses to RAI

(per source particle)				(per source particle)			
source	2033074578	1.0000E+00	3.1172E+00	escape	683906531	3.3639E-01	4.1288E-01
nucl. interaction	0	0.	0.	energy cutoff	0	0.	0.
particle decay	0	0.	0.	time cutoff	0	0.	0.
weight window	0	0.	0.	weight window	0	0.	0.
cell importance	0	0.	0.	cell importance	0	0.	0.
weight cutoff	0	0.	0.	weight cutoff	0	0.	0.
e or t importance	0	0.	0.	e or t importance	0	0.	0.
dxtran	0	0.	0.	dxtran	0	0.	0.
forced collisions	0	0.	0.	forced collisions	0	0.	0.
exp. transform	0	0.	0.	exp. transform	0	0.	0.
upscattering	0	0.	6.1536E-07	downscattering	0	0.	2.6539E+00
photonuclear	0	0.	0.	capture	1353909062	6.6594E-01	2.8846E-02
(n,xn)	9481476	4.6636E-03	5.6812E-03	loss to (n,xn)	4740461	2.3317E-03	2.7216E-02
prompt fission	0	0.	0.	loss to fission	0	0.	0.
delayed fission	0	0.	0.	nucl. interaction	0	0.	0.
prompt photofis	0	0.	0.	particle decay	0	0.	0.
tabular boundary	0	0.	0.	tabular boundary	0	0.	0.
tabular sampling	0	0.	0.	elastic scatter	0	0.	0.
total	2042556054	1.0047E+00	3.1228E+00	total	2042556054	1.0047E+00	3.1228E+00
number of neutrons banked	4741015			average time of (shakes)	cutoffs		
neutron tracks per source particle	1.0047E+00			escape	6.1747E+03	tco	1.0000E+33
neutron collisions per source particle	7.0908E+01			capture	1.3619E+04	eco	0.0000E+00
total neutron collisions	144160829333			capture or escape	1.1121E+04	wc1	0.0000E+00
net multiplication	1.0023E+00 0.0000			any termination	1.1095E+04	wc2	0.0000E+00
photon creation	tracks	weight	energy	photon loss	tracks	weight	energy
		(per source particle)				(per source particle)	
source	0	0.	0.	escape	157478484	8.0204E-02	1.4484E-01
nucl. interaction	0	0.	0.	energy cutoff	1061	5.5091E-07	4.2450E-04
particle decay	0	0.	0.	time cutoff	0	0.	0.
weight window	0	0.	0.	weight window	0	0.	0.
cell importance	0	0.	0.	cell importance	0	0.	0.
weight cutoff	0	0.	0.	weight cutoff	0	0.	0.
e or t importance	0	0.	0.	e or t importance	0	0.	0.
dxtran	0	0.	0.	dxtran	0	0.	0.
forced collisions	0	0.	0.	forced collisions	0	0.	0.
exp. transform	0	0.	0.	exp. transform	0	0.	0.
from neutrons	2440949891	1.2243E+00	3.0040E+00	compton scatter	0	0.	1.9035E+00
bremsstrahlung	4204284469	2.1052E+00	1.7735E-01	capture	10148504172	5.0858E+00	6.5249E-01
p-annihilation	569261250	2.8452E-01	1.4539E-01	pair production	284630625	1.4226E-01	7.0044E-01
photonuclear	0	0.	0.	photonuclear abs	0	0.	0.
electron x-rays	0	0.	0.	loss to photofis	0	0.	0.
compton fluores	0	0.	0.				
muon capt fluores	0	0.	0.				
1st fluorescence	2901168004	1.4556E+00	7.2256E-02				
2nd fluorescence	474950728	2.3858E-01	2.6882E-03				
cerenkov	0	0.	0.				
(gamma,xgamma)	0	0.	0.				
tabular sampling	0	0.	0.				
prompt photofis	0	0.	0.				
total	10590614342	5.3082E+00	3.4017E+00	total	10590614342	5.3082E+00	3.4017E+00
number of photons banked	-900489313			average time of (shakes)	cutoffs		
photon tracks per source particle	5.2092E+00			escape	1.0792E+04	tco	1.0000E+33
photon collisions per source particle	1.1090E+01			capture	6.9760E+03	eco	1.0000E-03
total photon collisions	22547069686			capture or escape	7.0352E+03	wc1	0.0000E+00
				any termination	7.1523E+03	wc2	0.0000E+00
computer time so far in this run	9600.50 minutes			maximum number ever in bank	46		
computer time in mcrun	9600.19 minutes			bank overflows to backup file	0		
source particles per minute	2.1177E+05			most random numbers used was	45974 in history 1047247824		
random numbers generated	2942781100613						
warning. random number period exceeded. decrease stride.							
range of sampled source weights = 1.0000E+00 to 1.0000E+00							
neutron reaction mt loop failed 2 times.							
neutron-induced photon production mt loop failed 65 times.							
number of histories processed by each thread							
84645960	85438011	85079714	85357919	84646597	84895613	85017058	85077777
84236851	84607752	84756563	84626736	84930480	84623769	84826210	84718752
84964207	83421924	84236175	84025050				
1neutron activity in each cell							
print table 126							

# ATTACHMENT A – Responses to RAI

	cell	tracks entering	population	collisions	collisions * weight (per history)	number weighted energy	flux weighted energy	average track weight (relative)	average track mfp (cm)
1	1	0	0	0	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
2	2	2307754045	2033226974	1650092846	8.1162E-01	3.5963E-03	2.3981E+00	1.0000E+00	3.1855E+00
3	3	11005586	5402926	28502779	1.4020E-02	9.2593E-04	6.0883E-01	1.0000E+00	4.8409E+00
4	4	2868290	1552760	5160609	2.5383E-03	1.8440E-03	6.5578E-01	1.0000E+00	4.1829E+00
5	5	2996465	1669591	2514937	1.2370E-03	2.6225E-03	6.1715E-01	1.0000E+00	4.2897E+00
6	6	2235349	1635586	5048955	2.4834E-03	4.1607E-03	6.2766E-01	1.0000E+00	5.6384E+00
7	7	3096831175	1420735462	3863812092	1.9005E+00	5.9751E-04	1.0280E+00	1.0000E+00	3.5255E+00
8	8	2040041339	1184385006	7067749918	3.4764E+00	7.0240E-04	8.8932E-01	1.0000E+00	4.0674E+00
9	9	1285727330	852831841	1303179382	6.4099E-01	1.1539E-03	8.8584E-01	1.0000E+00	4.2287E+00
10	10	4536267	2989646	10620916	5.2241E-03	3.0422E-03	5.7314E-01	1.0000E+00	5.5195E+00
11	11	4071920	2579670	10454821	5.1424E-03	4.9863E-03	5.7144E-01	1.0000E+00	6.0244E+00
12	12	2359725	1335982	2745688	1.3505E-03	1.4060E-03	5.0842E-01	1.0000E+00	4.6709E+00
13	13	5244133	2731504	15514088	7.6309E-03	4.5676E-04	6.0392E-01	1.0000E+00	3.9992E+00
14	14	2615064	1361818	5923995	2.9138E-03	1.7110E-03	6.1119E-01	1.0000E+00	4.0708E+00
15	15	975206	770209	679248	3.3410E-04	6.2477E-03	5.5605E-01	1.0000E+00	4.3843E+00
16	16	730416	651471	193871	9.5359E-05	4.9148E-03	5.7335E-01	1.0000E+00	6.1199E+00
17	17	3440843524	2034767376	12933224936	6.3614E+01	9.2736E-05	5.1400E-01	1.0000E+00	1.0504E+00
18	18	2094771	1073824	0	0.0000E+00	2.1624E-03	6.3588E-01	1.0000E+00	0.0000E+00
19	19	2798911	1476580	0	0.0000E+00	2.9217E-03	6.1176E-01	1.0000E+00	0.0000E+00
20	20	1457474597	852833470	0	0.0000E+00	8.4494E-04	8.4216E-01	1.0000E+00	0.0000E+00
21	21	479830	368184	0	0.0000E+00	6.0015E-03	5.3609E-01	1.0000E+00	0.0000E+00
22	22	703782	589389	0	0.0000E+00	5.3776E-03	5.6977E-01	1.0000E+00	0.0000E+00
23	23	2806593	1224469	0	0.0000E+00	1.4646E-03	6.3637E-01	1.0000E+00	0.0000E+00
24	24	1050726952	757059578	0	0.0000E+00	4.0511E-03	6.1070E-01	1.0000E+00	0.0000E+00
25	201	915025572	757104085	856410252	4.2124E-01	2.4439E-03	1.0196E+00	1.0000E+00	3.4655E+00
26	202	1084586397	757072004	0	0.0000E+00	1.4003E-03	7.5526E-01	1.0000E+00	0.0000E+00
27	203	683906531	683906531	0	0.0000E+00	4.2957E-03	1.1882E+00	1.0000E+00	0.0000E+00
28	204	683906531	683906531	0	0.0000E+00	4.2549E-03	1.1994E+00	1.0000E+00	0.0000E+00
29	205	684177774	683906531	0	0.0000E+00	4.1279E-03	1.2237E+00	1.0000E+00	0.0000E+00
30	301	271243	271243	0	0.0000E+00	3.1297E-03	1.2517E+00	1.0000E+00	0.0000E+00

total 18779795318 12729420241 144160829333 7.0908E+01  
1photon activity in each cell

print table 126

	cell	tracks entering	population	collisions	collisions * weight (per history)	number weighted energy	flux weighted energy	average track weight (relative)	average track mfp (cm)
1	1	0	0	0	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
2	2	51035602	57628225	7372921	3.6678E-03	1.7944E+00	1.7944E+00	1.0104E+00	1.7954E+01
3	3	90463423	121520724	310467576	1.5347E-01	1.2659E+00	1.2659E+00	1.0047E+00	1.8947E+00
4	4	20266924	66613356	118283165	5.8489E-02	1.7537E+00	1.7537E+00	1.0050E+00	1.3289E+00
5	5	3141452	8300457	13305008	6.5954E-03	1.7077E+00	1.7077E+00	1.0073E+00	1.3484E+00
6	6	1314907	2327645	5418113	2.6947E-03	1.3203E+00	1.3203E+00	1.0104E+00	1.9938E+00
7	7	1421851306	2219029206	3338769379	1.6555E+00	1.7326E+00	1.7326E+00	1.0081E+00	2.1743E+00
8	8	1183105778	5777237939	10506276671	5.2779E+00	1.7731E+00	1.7731E+00	1.0218E+00	1.3183E+00
9	9	141178822	387172238	494640174	2.4968E-01	1.8696E+00	1.8696E+00	1.0254E+00	2.1868E+00
10	10	2780049	4836583	12166162	6.0425E-03	1.3487E+00	1.3487E+00	1.0093E+00	1.9419E+00
11	11	2733904	4675657	12684691	6.3104E-03	1.2680E+00	1.2680E+00	1.0108E+00	1.9144E+00
12	12	5852506	6964625	11588935	5.7275E-03	1.3172E+00	1.3172E+00	1.0046E+00	1.9578E+00
13	13	84899447	111613983	276255764	1.3654E-01	1.2548E+00	1.2548E+00	1.0046E+00	1.8804E+00
14	14	18789867	63646283	114850091	5.6803E-02	1.7527E+00	1.7527E+00	1.0052E+00	1.3285E+00
15	15	571848	1407782	2261716	1.1254E-03	1.7176E+00	1.7176E+00	1.0108E+00	1.2599E+00
16	16	219123	243236	116570	5.8619E-05	1.4991E+00	1.4991E+00	1.0189E+00	2.1005E+00
17	17	666493443	1550930051	6867492721	3.3977E+00	1.0842E+00	1.0842E+00	1.0053E+00	1.3200E+01
18	18	2200419	2145342	0	0.0000E+00	1.7085E+00	1.7085E+00	1.0066E+00	0.0000E+00
19	19	1547653	1321695	0	0.0000E+00	1.4895E+00	1.4895E+00	1.0088E+00	0.0000E+00
20	20	200386627	179991105	0	0.0000E+00	1.8933E+00	1.8933E+00	1.0253E+00	0.0000E+00
21	21	412550	371007	0	0.0000E+00	1.2894E+00	1.2894E+00	1.0066E+00	0.0000E+00
22	22	200514	188016	0	0.0000E+00	1.5556E+00	1.5556E+00	1.0173E+00	0.0000E+00
23	23	20737982	19472197	0	0.0000E+00	1.3918E+00	1.3918E+00	1.0047E+00	0.0000E+00
24	24	220729124	187469538	0	0.0000E+00	1.3509E+00	1.3509E+00	1.0208E+00	0.0000E+00
25	201	166442868	333107075	455120029	2.3252E-01	1.7414E+00	1.7414E+00	1.0383E+00	2.0723E+00
26	202	235652886	195496052	0	0.0000E+00	1.5248E+00	1.5248E+00	1.0345E+00	0.0000E+00
27	203	157478484	157478484	0	0.0000E+00	1.8535E+00	1.8535E+00	1.0371E+00	0.0000E+00
28	204	157478484	157478484	0	0.0000E+00	1.8408E+00	1.8408E+00	1.0366E+00	0.0000E+00
29	205	157532084	157478484	0	0.0000E+00	1.8075E+00	1.8075E+00	1.0356E+00	0.0000E+00
30	301	53600	53600	0	0.0000E+00	1.6795E+00	1.6795E+00	1.0335E+00	0.0000E+00

total 5015551676 11776199069 22547069686 1.1251E+01  
1summary of photons produced in neutron collisions in the tabular range

production by cell of photons created with energies above local photon energy cutoffs

cell	number of photons	weight per source neut	energy per source neut	avg photon energy	mev/gm per source neut	weight/neut collision	energy/neut collision
------	-------------------	------------------------	------------------------	-------------------	------------------------	-----------------------	-----------------------

# ATTACHMENT A – Responses to RAI

1	1	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
2	2	8175770	4.02138E-03	1.32613E-02	3.29769E+00	1.09614E-03	4.95473E-03	1.63392E-02
3	3	3001631	1.49710E-03	5.11483E-03	3.41649E+00	3.49771E-08	1.06786E-01	3.64835E-01
4	4	193688	1.04152E-04	1.27614E-04	1.22526E+00	1.38666E-09	4.10317E-02	5.02746E-02
5	5	79594	4.22666E-05	4.94623E-05	1.17025E+00	9.48261E-10	3.41683E-02	3.99853E-02
6	6	321801	1.61423E-04	3.70800E-04	2.29708E+00	5.15565E-09	6.50005E-02	1.49311E-01
7	7	700594869	3.48527E-01	1.17071E+00	3.35903E+00	9.30397E-06	1.83389E-01	6.16010E-01
8	8	457830965	2.40533E-01	3.02984E-01	1.25964E+00	2.47708E-07	6.91905E-02	8.71549E-02
9	9	174623251	8.67750E-02	2.58443E-01	2.97831E+00	1.40827E-06	1.35377E-01	4.03193E-01
10	10	675943	3.37086E-04	8.55644E-04	2.53835E+00	1.27503E-08	6.45256E-02	1.63789E-01
11	11	585045	2.93575E-04	6.48497E-04	2.20897E+00	4.40004E-09	5.70895E-02	1.26109E-01
12	12	192268	9.60974E-05	3.04373E-04	3.16734E+00	2.39286E-08	7.11564E-02	2.25376E-01
13	13	2055052	1.02531E-03	3.87013E-03	3.77461E+00	6.23436E-08	1.34363E-01	5.07169E-01
14	14	204224	1.10009E-04	1.35581E-04	1.23245E+00	1.26964E-09	3.77545E-02	4.65305E-02
15	15	15836	8.26501E-06	9.18342E-06	1.11112E+00	3.92665E-10	2.47382E-02	2.74871E-02
16	16	11388	5.69784E-06	1.23690E-05	2.17082E+00	2.98490E-09	5.97517E-02	1.29710E-01
17	17	983764120	4.83880E-01	1.10166E+00	2.27673E+00	1.10166E+00	7.60649E-03	1.73179E-02
18	18	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
19	19	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
20	20	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
21	21	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
22	22	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
23	23	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
24	24	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
25	201	108623387	5.69148E-02	1.45460E-01	2.55576E+00	9.96064E-08	1.35113E-01	3.45316E-01
26	202	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
27	203	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
28	204	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
29	205	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
30	301	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
31	999	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
total			2440948832	1.22433E+00	3.00402E+00	2.45360E+00		

1energy distribution of photons produced in neutron collisions in the tabular range

all sampled photons from neutron collisions in the tabular range, without regard to energy cutoffs

energy interval	number of photons	number frequency	cum number distribution	weight of photons	weight frequency	cum weight distribution
20.000	104	4.26064E-08	4.26064E-08	5.78489E-08	4.72493E-08	4.72493E-08
15.000	909	3.72396E-07	4.15002E-07	5.07419E-07	4.14445E-07	4.61695E-07
10.000	179920	7.37090E-05	7.41240E-05	1.07944E-04	8.81652E-05	8.86269E-05
9.000	12119465	4.96506E-03	5.03918E-03	6.04701E-03	4.93903E-03	5.02765E-03
8.000	6566555	2.69016E-03	7.72935E-03	3.63379E-03	2.96797E-03	7.99563E-03
7.000	190746973	7.81446E-02	8.58739E-02	9.41896E-02	7.69314E-02	8.49270E-02
6.000	43603564	1.78634E-02	1.03737E-01	2.19742E-02	1.79479E-02	1.02875E-01
5.000	45932324	1.88174E-02	1.22555E-01	2.32742E-02	1.90097E-02	1.21885E-01
4.000	82018695	3.36011E-02	1.56156E-01	4.12015E-02	3.36522E-02	1.55537E-01
3.000	62358094	2.55467E-02	1.81702E-01	3.20269E-02	2.61587E-02	1.81695E-01
2.000	1102886161	4.51827E-01	6.33529E-01	5.45554E-01	4.45593E-01	6.27288E-01
1.000	229695318	9.41008E-02	7.27630E-01	1.17402E-01	9.58907E-02	7.23179E-01
0.500	537184744	2.20072E-01	9.47702E-01	2.73268E-01	2.23197E-01	9.46376E-01
0.100	105367630	4.31667E-02	9.90869E-01	5.39467E-02	4.40621E-02	9.90438E-01
0.010	19259006	7.88996E-03	9.98759E-01	1.01193E-02	8.26515E-03	9.98703E-01
0.000	3030429	1.24150E-03	1.00000E+00	1.58782E-03	1.29689E-03	1.00000E+00
<----- energy interval containing the global photon energy cutoff, 1.000E-03 Mev						
total	2440949891	1.00000E+00		1.22433E+00	1.00000E+00	

warning. 1059 photons from neutron collisions were created below a local photon energy cutoff and were not followed.

1tally 4 nps = 2033074578  
+ Package 1-Meter Neutron Dose Rate (mrem/hr) @ Z = 111.12500  
tally type 4 track length estimate of particle flux.  
particle(s): neutrons  
this tally is modified by dose function DE4 and DF4.  
volumes  
cell: 301  
2.02683E+00  
cell 301  
5.54561E-07 0.0023

results of 10 statistical checks for the estimated answer for the tally fluctuation chart (tfc) bin of tally

4

# ATTACHMENT A – Responses to RAI

tfc bin behavior	--mean-- behavior	-----relative error----- value decrease decrease rate	----variance of the variance---- value decrease decrease rate	--figure of merit-- value behavior	-pdf- slope
desired	random	<0.10 yes 1/sqrt(nps)	<0.10 yes 1/nps	constant	>3.00
observed	random	0.00 yes yes	0.00 yes yes	constant	1.62
passed?	yes	yes yes yes	yes yes yes	yes yes yes	no

warning. the tally in the tally fluctuation chart bin did not pass 1 of the 10 statistical checks.

1analysis of the results in the tally fluctuation chart bin (tfc) for tally 4 with nps = 2033074578 print table 160

normed average tally per history = 5.54561E-07  
estimated tally relative error = 0.0023  
relative error from zero tallies = 0.0019

unnormed average tally per history = 1.12400E-06  
estimated variance of the variance = 0.0000  
relative error from nonzero scores = 0.0012

number of nonzero history tallies = 271243  
history number of largest tally = 1091724254  
(largest tally)/(average tally) = 1.93193E+04

efficiency for the nonzero tallies = 0.0001  
largest unnormalized history tally = 2.17149E-02  
(largest tally)/(avg nonzero tally) = 2.57749E+00

(confidence interval shift)/mean = 0.0000

shifted confidence interval center = 5.54562E-07

if the largest history score sampled so far were to occur on the next history, the tfc bin quantities would change as follows:

estimated quantities	value at nps	value at nps+1	value(nps+1)/value(nps)-1.
mean	5.54561E-07	5.54566E-07	0.000010
relative error	2.28417E-03	2.28417E-03	-0.000001
variance of the variance	6.03118E-06	6.03127E-06	0.000015
shifted center	5.54562E-07	5.54562E-07	0.000000
figure of merit	1.99648E+01	1.99648E+01	0.000002

the estimated inverse power slope of the 19 largest tallies starting at 2.11742E-02 is 1.6174  
the empirical history score probability density function appears to be increasing at the largest history scores:  
please examine. see print table 161.  
the large score tail of the empirical history score probability density function appears to have no unsampled regions.

fom = (histories/minute)\*(f(x) signal-to-noise ratio)\*\*2 = (2.118E+05)\*( 9.709E-03)\*\*2 = (2.118E+05)\*(9.427E-05) = 1.996E+01

1unnormed tally density for tally 4 nonzero tally mean(m) = 8.425E-03 nps = 2033074578 print table 161

abscissa tally number	ordinate num den	log plot of tally probability density function in tally fluctuation chart bin(d=decade,slope= 1.6)
7.94-07	1 3.01-03	-2.521 *****
1.00-06	0 0.00+00	0.000 *****
1.26-06	0 0.00+00	0.000 *****
1.58-06	0 0.00+00	0.000 *****
2.00-06	1 1.20-03	-2.921 *****
2.51-06	0 0.00+00	0.000 *****
3.16-06	1 7.56-04	-3.121 *****
3.98-06	1 6.01-04	-3.221 *****
5.01-06	0 0.00+00	0.000 *****
6.31-06	2 7.58-04	-3.120 *****
7.94-06	1 3.01-04	-3.521 *****
1.00-05	1 2.39-04	-3.621 *****
1.26-05	2 3.80-04	-3.420 *****
1.58-05	6 9.05-04	-3.043 *****
2.00-05	7 8.39-04	-3.076 *****
2.51-05	8 7.62-04	-3.118 *****
3.16-05	4 3.03-04	-3.519 *****
3.98-05	8 4.81-04	-3.318 *****
5.01-05	10 4.77-04	-3.321 *****
6.31-05	9 3.41-04	-3.467 *****
7.94-05	17 5.12-04	-3.291 *****
1.00-04	23 5.50-04	-3.260 *****
1.26-04	28 5.32-04	-3.274 *****
1.58-04	33 4.98-04	-3.303 *****
2.00-04	38 4.55-04	-3.342 *****
2.51-04	58 5.52-04	-3.258 *****
3.16-04	69 5.22-04	-3.282 *****
3.98-04	29528 1.77-01	-0.751 *****
5.01-04	23179 1.11-01	-0.956 *****
6.31-04	1784 6.76-03	-2.170 *****
7.94-04	3246 9.77-03	-2.010 *****
1.00-03	1053 2.52-03	-2.599 *****
1.26-03	2391 4.54-03	-2.343 *****
1.58-03	2656 4.01-03	-2.397 *****

## ATTACHMENT A – Responses to RAI

```

2.00-03 3439 4.12-03 -2.385 *****
2.51-03 3642 3.47-03 -2.460 *****
3.16-03 4881 3.69-03 -2.433 *****
3.98-03 5382 3.23-03 -2.490 *****
5.01-03 5968 2.85-03 -2.545 *****
6.31-03 9081 3.44-03 -2.463 *****
7.94-03 10594 3.19-03 -2.496 *****
1.00-02 19642 4.70-03 -2.328 *****
1.26-02 28281 5.37-03 -2.270 *****
1.58-02 115804 1.75-02 -1.758 *****
2.00-02 64 7.67-06 -5.115 *
2.51-02 300 2.86-05 -4.544 *****
total 271243 1.33-04 d-----d-----d-----d-----d-----d-----

```

```

tally 14 nps = 2033074578
+ Package 1-Meter Gamma Dose Rate (mrem/hr) @ Z = 111.12500
tally type 4 track length estimate of particle flux.
particle(s): photons
this tally is modified by dose function DE14 and DF14.

volumes
cell: 301
2.02683E+00

cell 301
3.23972E-09 0.0058

```

results of 10 statistical checks for the estimated answer for the tally fluctuation chart (tfc) bin of tally 14										
tfc bin behavior	--mean-- behavior	-----relative error----- value	decrease	decrease rate	----variance of the variance---- value	decrease	decrease rate	--figure of merit-- value	behavior	-pdf-slope
desired	random	<0.10	yes	1/sqrt(nps)	<0.10	yes	1/nps	constant	random	>3.00
observed	random	0.01	yes	yes	0.00	yes	yes	constant	random	10.00
passed?	yes	yes	yes	yes	yes	yes	yes	yes	yes	yes

this tally meets the statistical criteria used to form confidence intervals: check the tally fluctuation chart to verify.  
the results in other bins associated with this tally may not meet these statistical criteria.

----- estimated confidence intervals: -----

estimated asymmetric confidence interval(1,2,3 sigma): 3.2209E-09 to 3.2587E-09; 3.2019E-09 to 3.2777E-09; 3.1830E-09 to 3.2966E-09  
estimated symmetric confidence interval(1,2,3 sigma): 3.2208E-09 to 3.2587E-09; 3.2018E-09 to 3.2776E-09; 3.1829E-09 to 3.2965E-09

1analysis of the results in the tally fluctuation chart bin (tfc) for tally 14 with nps = 2033074578 print table 160

```

normed average tally per history = 3.23972E-09      unnormed average tally per history = 6.56636E-09
estimated tally relative error   = 0.0058           estimated variance of the variance = 0.0001
relative error from zero tallies = 0.0043           relative error from nonzero scores = 0.0039

number of nonzero history tallies = 53417            efficiency for the nonzero tallies = 0.0000
history number of largest tally   = 206186010        largest unnormalized history tally = 1.85739E-03
(largest tally)/(average tally) = 2.82865E+05        (largest tally)/(avg nonzero tally)= 7.43199E+00

(confidence interval shift)/mean = 0.0000            shifted confidence interval center = 3.23980E-09

```

if the largest history score sampled so far were to occur on the next history, the tfc bin quantities would change as follows:

estimated quantities	value at nps	value at nps+1	value(nps+1)/value(nps)-1.
mean	3.23972E-09	3.24017E-09	0.000139
relative error	5.84651E-03	5.84735E-03	0.000144
variance of the variance	8.64087E-05	8.66313E-05	0.002576
shifted center	3.23980E-09	3.23980E-09	0.000000
figure of merit	3.04738E+00	3.04651E+00	-0.000288

the estimated slope of the 200 largest tallies starting at 1.16074E-03 appears to be decreasing at least exponentially.  
the empirical history score probability density function appears to be increasing at the largest history scores:  
please examine. see print table 161.  
the large score tail of the empirical history score probability density function appears to have no unsampled regions.

fom = (histories/minute)\*(f(x) signal-to-noise ratio)\*\*2 = (2.118E+05)\*( 3.793E-03)\*\*2 = (2.118E+05)\*(1.439E-05) = 3.047E+00

## ATTACHMENT A – Responses to RAI

1status of the statistical checks used to form confidence intervals for the mean for each tally bin

tally result of statistical checks for the tfc bin (the first check not passed is listed) and error magnitude check for all bins

4 missed 1 of 10 tfc bin checks: the slope of decrease of largest tallies is less than the minimum acceptable value of 3.0  
passed all bin error check: 1 tally bins all have relative errors less than 0.10 with no zero bins

14 passed the 10 statistical checks for the tally fluctuation chart bin result  
passed all bin error check: 1 tally bins all have relative errors less than 0.10 with no zero bins

the 10 statistical checks are only for the tally fluctuation chart bin and do not apply to other tally bins.

warning. 1 of the 2 tally fluctuation chart bins did not pass all 10 statistical checks.  
tally fluctuation charts

nps	mean	tally error	4 vov	slope	fom	mean	tally error	14 vov	slope	fom
131072000	5.5824E-07	0.0090	0.0001	2.0	21	3.2913E-09	0.0231	0.0014	1.6	3.2E+00
262144000	5.5493E-07	0.0064	0.0000	1.7	21	3.2564E-09	0.0163	0.0007	2.2	3.2E+00
393216000	5.5100E-07	0.0052	0.0000	1.5	21	3.2540E-09	0.0133	0.0004	4.2	3.2E+00
524288000	5.5226E-07	0.0045	0.0000	1.4	20	3.2545E-09	0.0115	0.0003	3.6	3.2E+00
655360000	5.5355E-07	0.0040	0.0000	1.4	20	3.2481E-09	0.0102	0.0003	2.3	3.1E+00
786432000	5.5361E-07	0.0037	0.0000	10.0	19	3.2505E-09	0.0094	0.0002	1.9	3.0E+00
917504000	5.5422E-07	0.0034	0.0000	10.0	20	3.2366E-09	0.0087	0.0002	8.3	3.0E+00
1048576000	5.5483E-07	0.0032	0.0000	10.0	20	3.2405E-09	0.0081	0.0002	10.0	3.0E+00
1179648000	5.5478E-07	0.0030	0.0000	10.0	20	3.2402E-09	0.0077	0.0001	10.0	3.0E+00
1310720000	5.5461E-07	0.0028	0.0000	10.0	20	3.2345E-09	0.0073	0.0001	10.0	3.0E+00
1441792000	5.5516E-07	0.0027	0.0000	10.0	20	3.2361E-09	0.0069	0.0001	10.0	3.1E+00
1572864000	5.5411E-07	0.0026	0.0000	7.8	20	3.2345E-09	0.0066	0.0001	10.0	3.1E+00
1703936000	5.5391E-07	0.0025	0.0000	2.7	20	3.2371E-09	0.0064	0.0001	10.0	3.1E+00
1835008000	5.5429E-07	0.0024	0.0000	3.1	20	3.2372E-09	0.0062	0.0001	10.0	3.0E+00
1966080000	5.5448E-07	0.0023	0.0000	1.6	20	3.2375E-09	0.0059	0.0001	10.0	3.0E+00
2033074578	5.5456E-07	0.0023	0.0000	1.6	20	3.2397E-09	0.0058	0.0001	10.0	3.0E+00

\*\*\*\*\*

dump no. 8 on file HAC\_HP\_SC-30G3\_252cf\_0.r nps = 2033074578 coll = 166707899019 ctm = 9600.19  
nrn = 2942781100613  
tally data written to file HAC\_HP\_SC-30G3\_252cf\_0.m

10 warning messages so far.

run terminated when it had used 9600 minutes of computer time.

computer time = 9600.51 minutes

mcnp version 6 02/20/18

08/29/21 17:52:00

probid = 08/29/21 11:11:43

### 3. SC-55G1 NCT Model with <sup>252</sup>Cf – Polyethylene with Secondary Gammas

Code Name & Version = MCNP\_6.20, 6.2.0



```
+-----+
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```



## ATTACHMENT A – Responses to RAI

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+-----+

1mcnp version 6 ld=02/20/18 08/29/21 17:56:08  
\*\*\*\*\*  
i=NCT\_HP\_SC-55G1\_252cf\_0.i name=NCT\_HP\_SC-55G1\_252cf\_0. tasks 24

probid = 08/29/21 17:56:08

warning. universe map (print table 128) disabled.

comment. Physics models disabled.

```
1- title HP/SC-55G1 with a Concentrated 252Cf Neutron Source - NCT
2- c
3- c Universe Fill Boundary
4- c
5- 1 0 -97 98 -99 fill=1 $Shielded Container 1
6- imp:n=1 imp:p=1 trcl=1
7- 2 0 -97 98 -99 fill=1 $Shielded Container 2
8- imp:n=1 imp:p=1 trcl=2
9- c
10- c Payload Cell $Material Density 100%
11- c
12- 3 1 -0.9400 -1 2 -3 $Payload
13- imp:n=1 imp:p=1 u=1
14- c
15- c Shielded Container Cells $Material Density 100%
16- c
17- 4 2 -7.8526 -11 12 -13 -14 $Base Steel
18- imp:n=1 imp:p=1 u=1
19- 5 2 -7.8526 13 15 -16 -18 20 $Sidewall Steel
20- (-15 :17 :18 :19)
21- imp:n=1 imp:p=1 u=1
22- 6 2 -7.8526 -24 25 -26 -28 $Lid Steel
23- ((18 :-25 :-27)
24- (18 :27 :-30 :-31)
25- (-18 :-27 :32 :33)
26- (-25 :27 :-29))
27- imp:n=1 imp:p=1 u=1
28- c
29- c Cavity (Void) Cells
30- c
31- 7 1 -0.9400 ((13 -15 -25): $Payload Cavity
32- (15 -17 -19 -25):
33- (17 -18 -20):
34- (-17 -18 30 31):
35- (-17 25 29):
36- (-17 27 -29 -31):
37- (18 27 -32 -33))
38- (1 :-2 :3)
39- imp:n=1 imp:p=1 u=1
40- 8 0 (11 :-12 :13 :14) $Exterior Void
41- (-13 :16 :18)
42- (-18 :24 :26 :28)
43- imp:n=1 imp:p=1 u=1
44- c
45- c HalfPACT Package Cells $Material Density 100%
46- c
47- 201 4 -8.0128 (201 -202 204 -205): $HalfPACT ICV/OCV Steel Structure
48- (-202 203 -204):
49- (-202 205 -206)
50- imp:n=1 imp:p=1
51- 202 5 -0.1322 (202 203 -206 -211): $HalfPACT OCA Polyurethane Foam
52- (-203 -211 214):
53- (206 -211 -215)
54- imp:n=1 imp:p=1
55- 203 4 -8.0128 (211 -212 214 -215): $HalfPACT OCA Steel Structure
56- (-212 213 -214):
57- (-212 215 -216)
58- imp:n=1 imp:p=1
59- c
60- c HalfPACT Package Void Cells
61- c
62- 204 0 -201 204 -205 $HalfPACT ICV Interior Void
63- #1 #2
64- imp:n=1 imp:p=1
65- 205 0 ((-999 212 213 -216): $HalfPACT OCA Exterior Void
66- (-999 -213):
67- (-999 216))
```

## ATTACHMENT A – Responses to RAI

```

68-          (-301 :302:-305 :306)
69-          (-303 :304:-305 :306)
70-          imp:n=1  imp:p=1
71-  c
72-  c  HalfPACT Package Surface and 2-meter Tally Cells
73-  c
74-    301  0          301 -302  305 -306          $Package Side Middle @ Surface
75-          imp:n=1  imp:p=1
76-    302  0          303 -304  305 -306          $Package Side Middle @ 2-meters
77-          imp:n=1  imp:p=1
78-  c
79-  c  World Cell
80-  c
81-    999  0          999
82-          imp:n=0  imp:p=0
83-
84-  c
85-  c  Payload Surfaces
86-  c
87-    1      cz      1.27000          $Radius
88-    2      pz      50.10150          $Plane, Bottom
89-    3      pz      52.64150          $Plane, Top
90-  c
91-  c  Shielded Container Base Surfaces
92-  c
93-    11     cz      37.33800          $Radius, Base Outer
94-    12     pz      0.00000          $Plane, Base Bottom
95-    13     pz      5.96900          $Plane, Base Top
96-    14     kz      -37.02050  1.00000  1 $Chamfer, Base Bottom Outside Corner
97-  c
98-  c  Shielded Container Sidewall Surfaces
99-  c
100-    15     cz      31.75000          $Radius, Sidewall Inner
101-    16     cz      37.33800          $Radius, Sidewall Outer
102-    17     cz      31.95320          $Radius, Lid Engagement Step
103-    18     pz      99.31400          $Plane, Sidewall Top
104-    19     kz      64.70650  1.00000  1 $Cone, Lid Engagement Transition
105-    20     kz      11.20580  0.13247  $Chamfer, Top Inside Corner
106-  c
107-  c  Shielded Container Lid Surfaces
108-  c
109-    24     cz      37.33800          $Radius, Lid Outer
110-    25     pz      96.77400          $Plane, Lid Bottom
111-    26     pz      102.87000          $Plane, Lid Top
112-    27     cz      31.91510          $Radius, Lid Step
113-    28     kz      139.89050  1.00000  -1 $Chamfer, Top Outside Corner
114-    29     kz      9.72298  0.13247  1 $Chamfer, Bottom Outside Corner
115-    30     cz      31.76270          $Radius, Vent Port Groove Inner
116-    31     pz      98.39960          $Plane, Vent Port Groove Bottom
117-    32     cz      33.78200          $Radius, Gasket Recess Outer
118-    33     pz      99.63150          $Plane, Gasket Recess Top
119-  c
120-  c  Shielded Container Universe Fill Boundary Surfaces
121-  c
122-    97     cz      37.33801          $Radius, Fill Boundary
123-    98     pz      -0.00001          $Plane, Fill Boundary Bottom
124-    99     pz      102.87001          $Plane, Fill Boundary Top
125-  c
126-  c  HalfPACT Package ICV/OCV Surfaces
127-  c
128-    201     cz      92.23375          $Radius, Shell Inner
129-    202     cz      93.34500          $Radius, Shell Outer
130-    203     pz      22.86000          $Plane, Lower Head Bottom
131-    204     pz      24.13000          $Plane, Lower Head Top
132-    205     pz      198.12000          $Plane, Upper Head Bottom
133-    206     pz      199.39000          $Plane, Upper Head Top
134-  c
135-  c  HalfPACT Package OCA Surfaces
136-  c
137-    211     cz      118.74500          $Radius, Shell Inner
138-    212     cz      119.38000          $Radius, Shell Outer
139-    213     pz      0.00000          $Plane, Lower Head Bottom
140-    214     pz      0.63500          $Plane, Lower Head Top
141-    215     pz      229.23500          $Plane, Upper Head Bottom
142-    216     pz      229.87000          $Plane, Upper Head Top
143-  c
144-  c  HalfPACT Package Tally Surfaces
145-  c
146-    301     cz      119.38000          $Radius, Inner (at Surface)
147-    302     cz      119.48000          $Radius, Outer (at Surface)
148-    303     cz      319.38000          $Radius, Inner (at 2.000-Meters)

```

## ATTACHMENT A – Responses to RAI

```

149-      304      cz  319.48000      $Radius, Outer (at 2.001-Meters)
150-      305      pz  108.58500      $Plane, Bottom Elevation
151-      306      pz  113.66500      $Plane, Top Elevation
152-      c
153-      c      Define World Surface (Problem Boundary)
154-      c
155-      999      sz  114.93500      400
156-
157-      c
158-      c      Physics Cards
159-      c
160-      mode n      p
comment. photonuclear physics may be needed (phys:p).
161-      c
162-      c      Material Cards
163-      c
164-      m1      1001.84C -0.143685      $Payload (Polyethethylene)
165-      1002.84C -0.000033      6000.84C -0.856282
166-      plib = 84P
167-      c
168-      m2      26054.84C -0.058450      $Carbon Steel
169-      26056.84C -0.917540      26057.84C -0.021190      26058.84C -0.002820
170-      plib = 84P
171-      c
172-      m4      14028.84C -0.009222      $Stainless Steel (ASTM A240, Type 304)
173-      14029.84C -0.000469      14030.84C -0.000309      24050.84C -0.008256
174-      24052.84C -0.159199      24053.84C -0.018052      24054.84C -0.004494
175-      25055.84C -0.020000      26054.84C -0.039746      26056.84C -0.623927
176-      26057.84C -0.014409      26058.84C -0.001918      28058.84C -0.068077
177-      28060.84C -0.026223      28061.84C -0.001140      28062.84C -0.003635
178-      28064.84C -0.000926
179-      plib = 84P
180-      c
181-      m5      1001.84C -0.069992      $Urethane Foam
182-      1002.84C -0.000008      6000.84C -0.600000      7014.84C -0.079709
183-      7015.84C -0.000291      8016.84C -0.239909      8017.84C -0.000091
184-      14028.84C -0.009222      14029.84C -0.000469      14030.84C -0.000309
185-      plib = 84P
186-      c
187-      c      Specify Universe Transformations
188-      c
189-      *tr1 -37.97300  0.00000  59.75349      $shielded Container 1
190-      *tr2  37.97300  0.00000  59.75349      $shielded Container 2
191-      c
192-      c      Specify Explicit Analysis for Weight Windows Evaluation
193-      c
194-      cut:n 2j      0
195-      cut:p 2j      0
196-      c
197-      c      Source Cards
198-      c
199-      sdef par=1 axs=0 0 1 erg=d1 pos=d2 rad=d3 ext=d4
200-      sc1 Concentrated 252Cf Neutron Source
201-      si1 L 0.100000 0.500000 1.000000 2.000000 3.000000
202-      4.000000 6.000000 8.000000 10.000000 15.000000
203-      sp1 0.00E+00 1.80E+11 2.71E+11 5.36E+11 4.10E+11
204-      2.73E+11 2.66E+11 8.53E+10 2.44E+10 8.36E+09
205-      si2 L -37.97300 0.00000 111.12500 37.97300 0.00000 111.12500
206-      sp2 1 1
207-      si3 0.00000 1.27000
208-      sp3 -21 1 1
209-      si4 -1.27000 1.27000
210-      sp4 -21 0 0
211-      c
212-      c      Package Tally Cards
213-      c
214-      f4:n 301
215-      fc4 Package Surface Neutron Dose Rate (mrem/hr) @ Z = 111.12500
216-      sd4 381.20362
217-      f14:n 302
218-      fc14 2-M from Package Surface Neutron Dose Rate (mrem/hr) @ Z = 111.12500
219-      sd14 1019.57524
220-      f24:p 301
221-      fc24 Package Surface Gamma Dose Rate (mrem/hr) @ Z = 111.12500
222-      sd24 381.20362
223-      f34:p 302
224-      fc34 2-M from Package Surface Gamma Dose Rate (mrem/hr) @ Z = 111.12500
225-      sd34 1019.57524
226-      c
227-      c      ANSI/ANS-6.1.1-1977 Neutron Flux-to-Dose Rate Factor Cards
228-      c

```

# ATTACHMENT A – Responses to RAI

```

229-    de0    2.50E-08  1.00E-07  1.00E-06  1.00E-05  1.00E-04 $Energy (Mev)
230-          1.00E-03  1.00E-02  1.00E-01  5.00E-01  1.00E+00
231-          2.50E+00  5.00E+00  7.00E+00  1.00E+01  1.40E+01
232-          2.00E+01
233-    df0    3.67E-03  3.67E-03  4.46E-03  4.54E-03  4.18E-03 $Factor (mrem/hr)
234-          3.76E-03  3.56E-03  2.17E-02  9.26E-02  1.32E-01
235-          1.25E-01  1.56E-01  1.47E-01  1.47E-01  2.08E-01
236-          2.27E-01
237-    c
238-    c    ANSI/ANS-6.1.1-1977 Gamma Flux-to-Dose Rate Factor Cards
239-    c
240-    de24    0.01      0.03      0.05      0.07      0.10      $Energy (Mev)
241-          0.15      0.20      0.25      0.30      0.35
242-          0.40      0.45      0.50      0.55      0.60
243-          0.65      0.70      0.80      1.00      1.40
244-          1.80      2.20      2.60      2.80      3.25
245-          3.75      4.25      4.75      5.00      5.25
246-          5.75      6.25      6.75      7.50      9.00
247-          11.00     13.00     15.00
248-    df24    3.96E-03  5.82E-04  2.90E-04  2.58E-04  2.83E-04 $Factor (mrem/hr)
249-          3.79E-04  5.01E-04  6.31E-04  7.59E-04  8.78E-04
250-          9.85E-04  1.08E-03  1.17E-03  1.27E-03  1.36E-03
251-          1.44E-03  1.52E-03  1.68E-03  1.98E-03  2.51E-03
252-          2.99E-03  3.42E-03  3.82E-03  4.01E-03  4.41E-03
253-          4.83E-03  5.23E-03  5.60E-03  5.80E-03  6.01E-03
254-          6.37E-03  6.74E-03  7.11E-03  7.66E-03  8.77E-03
255-          1.03E-02  1.18E-02  1.33E-02
256-    de34    0.01      0.03      0.05      0.07      0.10      $Energy (Mev)
257-          0.15      0.20      0.25      0.30      0.35
258-          0.40      0.45      0.50      0.55      0.60
259-          0.65      0.70      0.80      1.00      1.40
260-          1.80      2.20      2.60      2.80      3.25
261-          3.75      4.25      4.75      5.00      5.25
262-          5.75      6.25      6.75      7.50      9.00
263-          11.00     13.00     15.00
264-    df34    3.96E-03  5.82E-04  2.90E-04  2.58E-04  2.83E-04 $Factor (mrem/hr)
265-          3.79E-04  5.01E-04  6.31E-04  7.59E-04  8.78E-04
266-          9.85E-04  1.08E-03  1.17E-03  1.27E-03  1.36E-03
267-          1.44E-03  1.52E-03  1.68E-03  1.98E-03  2.51E-03
268-          2.99E-03  3.42E-03  3.82E-03  4.01E-03  4.41E-03
269-          4.83E-03  5.23E-03  5.60E-03  5.80E-03  6.01E-03
270-          6.37E-03  6.74E-03  7.11E-03  7.66E-03  8.77E-03
271-          1.03E-02  1.18E-02  1.33E-02
272-    c
273-    c    Runtime and Print Cards
274-    c
275-    prdmp    j      j      1      2
276-    ctme     1200

*****
* Random Number Generator = 1 *
* Random Number Seed = 19073486328125 *
* Random Number Multiplier = 19073486328125 *
* Random Number Adder = 0 *
* Random Number Bits Used = 48 *
* Random Number Stride = 152917 *
*****

comment. total nubar used if fissionable isotopes are present.

surface 11 and surface 16 are the same. 16 will be deleted.
surface 11 and surface 24 are the same. 24 will be deleted.
surface 12 and surface 213 are the same. 213 will be deleted.
surface 212 and surface 301 are the same. 301 will be deleted.
surface 1098 and surface 2098 are the same. 2098 will be deleted.
surface 1099 and surface 2099 are the same. 2099 will be deleted.

comment. 6 surfaces were deleted for being the same as others.

warning. 1 cells appear to consist of more than one piece.
1cells

print table 60

cell mat atom density gram density volume mass neutron importance photon importance photon wt generation

```

# ATTACHMENT A – Responses to RAI

1	1	0	0.00000E+00	0.00000E+00	4.50548E+05	0.00000E+00	1	1.0000E+00	1.0000E+00	-1.000E+00
2	2	0	0.00000E+00	0.00000E+00	4.50548E+05	0.00000E+00	1	1.0000E+00	1.0000E+00	-1.000E+00
3	3	1	1.21070E-01	9.40000E-01	1.28704E+01	1.20981E+01	1	1.0000E+00	1.0000E+00	-1.000E+00
4	4	2	8.46854E-02	7.85260E+00	2.61311E+04	2.05197E+05	1	1.0000E+00	1.0000E+00	-1.000E+00
5	5	2	8.46854E-02	7.85260E+00	1.13098E+05	8.88115E+05	1	1.0000E+00	1.0000E+00	-1.000E+00
6	6	2	8.46854E-02	7.85260E+00	2.35256E+04	1.84737E+05	1	1.0000E+00	1.0000E+00	-1.000E+00
7	7	1	1.21070E-01	9.40000E-01	0.00000E+00	0.00000E+00	0	1.0000E+00	1.0000E+00	-1.000E+00
8	8	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0	1.0000E+00	1.0000E+00	-1.000E+00
9	201	4	8.80954E-02	8.01280E+00	1.82252E+05	1.46035E+06	1	1.0000E+00	1.0000E+00	-1.000E+00
10	202	5	1.11837E-02	1.32200E-01	5.29418E+06	6.99890E+05	1	1.0000E+00	1.0000E+00	-1.000E+00
11	203	4	8.80954E-02	8.01280E+00	1.65455E+05	1.32576E+06	1	1.0000E+00	1.0000E+00	-1.000E+00
12	204	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0	1.0000E+00	1.0000E+00	-1.000E+00
13	205	0	0.00000E+00	0.00000E+00	2.57789E+08	0.00000E+00	2	1.0000E+00	1.0000E+00	-1.000E+00
14	301	0	0.00000E+00	0.00000E+00	3.81204E+02	0.00000E+00	1	1.0000E+00	1.0000E+00	-1.000E+00
15	302	0	0.00000E+00	0.00000E+00	1.01958E+03	0.00000E+00	1	1.0000E+00	1.0000E+00	-1.000E+00
16	999	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0	0.0000E+00	0.0000E+00	-1.000E+00

total 2.64496E+08 4.76406E+06

minimum source weight = 1.0000E+00 maximum source weight = 1.0000E+00

comment. threading will be used when possible in portions of mcnp6.

comment. threading will be used for n/p/e table physics.

comment. threading will generally not be used for model physics.

2 warning messages so far.

1cross-section tables print table 100

XSDIR used: C:\MCNP\MCPN\_DATA\xsdir\_mcnp6.2

table	length						
tables from file xdata/endf71x/H/1001.714nc							
1001.84c	15325	H1 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53)		mat 125	12/17/12		
		Energy range: 1.00000E-11 to 2.00000E+01 Mev.					
		particle-production data for deuterons being expunged from 1001.84c					
		temperature = 2.1543E-07 adjusted to 2.5300E-08					
tables from file xdata/endf71x/H/1002.714nc							
1002.84c	7283	H2 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53)		mat 128	12/17/12		
		Energy range: 1.00000E-11 to 1.50000E+02 Mev.					
		particle-production data for protons being expunged from 1002.84c					
		particle-production data for tritons being expunged from 1002.84c					
		temperature = 2.1543E-07 adjusted to 2.5300E-08					
tables from file xdata/endf71x/C/6000.714nc							
6000.84c	55343	C0 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53)		mat 600	12/20/12		
		Energy range: 1.00000E-11 to 1.50000E+02 Mev.					
		particle-production data for protons being expunged from 6000.84c					
		particle-production data for deuterons being expunged from 6000.84c					
		particle-production data for alphas being expunged from 6000.84c					
		temperature = 2.1543E-07 adjusted to 2.5300E-08					
tables from file xdata/endf71x/N/7014.714nc							
7014.84c	102640	N14 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53)		mat 725	12/16/12		
		Energy range: 1.00000E-11 to 1.50000E+02 Mev.					
		particle-production data for protons being expunged from 7014.84c					
		particle-production data for deuterons being expunged from 7014.84c					
		particle-production data for alphas being expunged from 7014.84c					
		temperature = 2.1543E-07 adjusted to 2.5300E-08					
tables from file xdata/endf71x/N/7015.714nc							
7015.84c	28412	N15 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53)		mat 728	12/16/12		
		Energy range: 1.00000E-11 to 2.00000E+01 Mev.					
		temperature = 2.1543E-07 adjusted to 2.5300E-08					
tables from file xdata/endf71x/O/8016.714nc							
8016.84c	264772	O16 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53)		mat 825	12/13/12		
		Energy range: 1.00000E-11 to 1.50000E+02 Mev.					
		particle-production data for protons being expunged from 8016.84c					
		particle-production data for deuterons being expunged from 8016.84c					
		particle-production data for tritons being expunged from 8016.84c					
		particle-production data for alphas being expunged from 8016.84c					
		temperature = 2.1543E-07 adjusted to 2.5300E-08					

## ATTACHMENT A – Responses to RAI

tables from file xdata/endl71x/0/8017.714nc

8017.84c	4921	017 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 2.00000E+01 MeV. temperature = 2.1543E-07 adjusted to 2.5300E-08	mat 828	12/13/12
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warning. 8017.84c lacks gamma-ray production cross sections.

tables from file xdata/endl71x/Si/14028.714nc

14028.84c	169896	Si28 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 1.50000E+02 MeV. particle-production data for protons being expunged from 14028.84c particle-production data for deuterons being expunged from 14028.84c particle-production data for tritons being expunged from 14028.84c particle-production data for alphas being expunged from 14028.84c temperature = 2.1543E-07 adjusted to 2.5300E-08	mat1425	12/14/12
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tables from file xdata/endl71x/Si/14029.714nc

14029.84c	158834	Si29 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 1.50000E+02 MeV. particle-production data for protons being expunged from 14029.84c particle-production data for deuterons being expunged from 14029.84c particle-production data for tritons being expunged from 14029.84c particle-production data for alphas being expunged from 14029.84c temperature = 2.1543E-07 adjusted to 2.5300E-08	mat1428	12/14/12
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tables from file xdata/endl71x/Si/14030.714nc

14030.84c	130018	Si30 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 1.50000E+02 MeV. particle-production data for protons being expunged from 14030.84c particle-production data for deuterons being expunged from 14030.84c particle-production data for tritons being expunged from 14030.84c particle-production data for alphas being expunged from 14030.84c temperature = 2.1543E-07 adjusted to 2.5300E-08	mat1431	12/16/12
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tables from file xdata/endl71x/Cr/24050.714nc

24050.84c	291186	Cr50 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 1.50000E+02 MeV. particle-production data for protons being expunged from 24050.84c particle-production data for deuterons being expunged from 24050.84c particle-production data for tritons being expunged from 24050.84c particle-production data for alphas being expunged from 24050.84c temperature = 2.1543E-07 adjusted to 2.5300E-08	mat2425	12/13/12
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tables from file xdata/endl71x/Cr/24052.714nc

24052.84c	310582	Cr52 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 1.50000E+02 MeV. particle-production data for protons being expunged from 24052.84c particle-production data for deuterons being expunged from 24052.84c particle-production data for tritons being expunged from 24052.84c particle-production data for alphas being expunged from 24052.84c temperature = 2.1543E-07 adjusted to 2.5300E-08	mat2431	12/13/12
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tables from file xdata/endl71x/Cr/24053.714nc

24053.84c	254692	Cr53 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 1.50000E+02 MeV. particle-production data for protons being expunged from 24053.84c particle-production data for deuterons being expunged from 24053.84c particle-production data for tritons being expunged from 24053.84c particle-production data for alphas being expunged from 24053.84c temperature = 2.1543E-07 adjusted to 2.5300E-08	mat2434	12/13/12
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tables from file xdata/endl71x/Cr/24054.714nc

24054.84c	190185	Cr54 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 1.50000E+02 MeV. particle-production data for protons being expunged from 24054.84c particle-production data for deuterons being expunged from 24054.84c particle-production data for tritons being expunged from 24054.84c particle-production data for alphas being expunged from 24054.84c temperature = 2.1543E-07 adjusted to 2.5300E-08	mat2437	12/13/12
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tables from file xdata/endl71x/Mn/25055.714nc

## ATTACHMENT A – Responses to RAI

25055.84c	455909	Mn55 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 6.00000E+01 Mev. particle-production data for protons being expunged from 25055.84c particle-production data for deuterons being expunged from 25055.84c particle-production data for tritons being expunged from 25055.84c particle-production data for helions being expunged from 25055.84c particle-production data for alphas being expunged from 25055.84c probability tables used from 1.2500E-01 to 1.0000E+00 mev. temperature = 2.1543E-07 adjusted to 2.5300E-08  tables from file xdata/endl71x/Fe/26054.714nc	mat2525	12/18/12
26054.84c	217705	Fe54 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 1.50000E+02 Mev. particle-production data for protons being expunged from 26054.84c particle-production data for deuterons being expunged from 26054.84c particle-production data for tritons being expunged from 26054.84c particle-production data for alphas being expunged from 26054.84c temperature = 2.1543E-07 adjusted to 2.5300E-08  tables from file xdata/endl71x/Fe/26056.714nc	mat2625	12/22/12
26056.84c	352429	Fe56 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 1.50000E+02 Mev. particle-production data for protons being expunged from 26056.84c particle-production data for deuterons being expunged from 26056.84c particle-production data for tritons being expunged from 26056.84c particle-production data for alphas being expunged from 26056.84c temperature = 2.1543E-07 adjusted to 2.5300E-08  tables from file xdata/endl71x/Fe/26057.714nc	mat2631	12/22/12
26057.84c	241212	Fe57 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 1.50000E+02 Mev. particle-production data for protons being expunged from 26057.84c particle-production data for deuterons being expunged from 26057.84c particle-production data for tritons being expunged from 26057.84c particle-production data for alphas being expunged from 26057.84c temperature = 2.1543E-07 adjusted to 2.5300E-08  tables from file xdata/endl71x/Fe/26058.714nc	mat2634	12/22/12
26058.84c	135502	Fe58 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 2.00000E+01 Mev. particle-production data for protons being expunged from 26058.84c particle-production data for alphas being expunged from 26058.84c temperature = 2.1543E-07 adjusted to 2.5300E-08  tables from file xdata/endl71x/Ni/28058.714nc	mat2637	12/22/12
28058.84c	420627	Ni58 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 1.50000E+02 Mev. particle-production data for protons being expunged from 28058.84c particle-production data for deuterons being expunged from 28058.84c particle-production data for tritons being expunged from 28058.84c particle-production data for alphas being expunged from 28058.84c temperature = 2.1543E-07 adjusted to 2.5300E-08  tables from file xdata/endl71x/Ni/28060.714nc	mat2825	12/15/12
28060.84c	344192	Ni60 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 1.50000E+02 Mev. particle-production data for protons being expunged from 28060.84c particle-production data for deuterons being expunged from 28060.84c particle-production data for tritons being expunged from 28060.84c particle-production data for alphas being expunged from 28060.84c temperature = 2.1543E-07 adjusted to 2.5300E-08  tables from file xdata/endl71x/Ni/28061.714nc	mat2831	12/17/12
28061.84c	190713	Ni61 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 1.50000E+02 Mev. particle-production data for protons being expunged from 28061.84c particle-production data for deuterons being expunged from 28061.84c particle-production data for tritons being expunged from 28061.84c particle-production data for alphas being expunged from 28061.84c temperature = 2.1543E-07 adjusted to 2.5300E-08  tables from file xdata/endl71x/Ni/28062.714nc	mat2834	12/13/12
28062.84c	169202	Ni62 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53)	mat2837	12/17/12

# ATTACHMENT A – Responses to RAI

Energy range: 1.00000E-11 to 1.50000E+02 Mev.  
 particle-production data for protons being expunged from 28062.84c  
 particle-production data for deuterons being expunged from 28062.84c  
 particle-production data for tritons being expunged from 28062.84c  
 particle-production data for alphas being expunged from 28062.84c  
 probability tables used from 6.0000E-01 to 1.0000E+00 mev.  
 temperature = 2.1543E-07 adjusted to 2.5300E-08

tables from file xdata/endl71x/Ni/28064.714nc

28064.84c 152759 Ni64 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) mat2843 12/17/12  
 Energy range: 1.00000E-11 to 1.50000E+02 Mev.  
 particle-production data for protons being expunged from 28064.84c  
 particle-production data for deuterons being expunged from 28064.84c  
 particle-production data for tritons being expunged from 28064.84c  
 particle-production data for alphas being expunged from 28064.84c  
 temperature = 2.1543E-07 adjusted to 2.5300E-08

tables from file xdata/mcplib84

1000.84p	1974	Update of MCPLIB04 Photon Compton Broadening Data For MCNP5 see LA-UR-	12-00018	01/03/12
		Energy range: 1.00000E-03 to 1.00000E+05 Mev.		
6000.84p	3228	Update of MCPLIB04 Photon Compton Broadening Data For MCNP5 see LA-UR-	12-00018	01/03/12
		Energy range: 1.00000E-03 to 1.00000E+05 Mev.		
7000.84p	3270	Update of MCPLIB04 Photon Compton Broadening Data For MCNP5 see LA-UR-	12-00018	01/03/12
		Energy range: 1.00000E-03 to 1.00000E+05 Mev.		
8000.84p	3348	Update of MCPLIB04 Photon Compton Broadening Data For MCNP5 see LA-UR-	12-00018	01/03/12
		Energy range: 1.00000E-03 to 1.00000E+05 Mev.		
14000.84p	4868	Update of MCPLIB04 Photon Compton Broadening Data For MCNP5 see LA-UR-	12-00018	01/03/12
		Energy range: 1.00000E-03 to 1.00000E+05 Mev.		
24000.84p	5758	Update of MCPLIB04 Photon Compton Broadening Data For MCNP5 see LA-UR-	12-00018	01/03/12
		Energy range: 1.00000E-03 to 1.00000E+05 Mev.		
25000.84p	5674	Update of MCPLIB04 Photon Compton Broadening Data For MCNP5 see LA-UR-	12-00018	01/03/12
		Energy range: 1.00000E-03 to 1.00000E+05 Mev.		
26000.84p	5794	Update of MCPLIB04 Photon Compton Broadening Data For MCNP5 see LA-UR-	12-00018	01/03/12
		Energy range: 1.00000E-03 to 1.00000E+05 Mev.		
28000.84p	5902	Update of MCPLIB04 Photon Compton Broadening Data For MCNP5 see LA-UR-	12-00018	01/03/12
		Energy range: 1.00000E-03 to 1.00000E+05 Mev.		

total 4704155

comment. 24 cross sections modified by free gas thermal treatment.

maximum photon energy set to 100.0 mev (maximum electron energy)

tables from file xdata/e103

1000.03e	2329		6/6/98
		Energy range: 1.00000E-03 to 1.00000E+03 Mev.	
6000.03e	2333		6/6/98
		Energy range: 1.00000E-03 to 1.00000E+03 Mev.	
7000.03e	2333		6/6/98
		Energy range: 1.00000E-03 to 1.00000E+03 Mev.	
8000.03e	2333		6/6/98
		Energy range: 1.00000E-03 to 1.00000E+03 Mev.	
14000.03e	2339		6/6/98
		Energy range: 1.00000E-03 to 1.00000E+03 Mev.	
24000.03e	2345		6/6/98
		Energy range: 1.00000E-03 to 1.00000E+03 Mev.	
25000.03e	2345		6/6/98
		Energy range: 1.00000E-03 to 1.00000E+03 Mev.	
26000.03e	2345		6/6/98
		Energy range: 1.00000E-03 to 1.00000E+03 Mev.	
28000.03e	2347		6/6/98
		Energy range: 1.00000E-03 to 1.00000E+03 Mev.	

1particles and energy limits

print table 101

particle type	particle cutoff energy	maximum particle energy	smallest table maximum	largest table maximum	always use table below	always use model above
1 n neutron	0.0000E+00	1.0000E+36	2.0000E+01	1.5000E+02	1.0000E+36	1.0000E+36
2 p photon	1.0000E-03	1.0000E+02	1.0000E+05	1.0000E+05	1.0000E+36	1.0000E+36
3 e electron	1.0000E-03	1.0000E+02	1.0000E+02	1.0000E+02	1.0000E+36	1.0000E+36

warning. material 2 has been set to a conductor.

warning. material 4 has been set to a conductor.

comment. setting up hash-based fast table search for xsec tables



# ATTACHMENT A – Responses to RAI

=====> Set up arrays for hash-based fast table search for xsec data

number of hash bins = 8192  
min hash table energy = 1.00000E-11  
max hash table energy = 1.50000E+02

nuclide	ne	emin	emax	ave_bins	min_bins	max_bins
1001.84c	590	1.00000E-11	2.00000E+01	0.1	0.0	1.0
1002.84c	583	1.00000E-11	1.50000E+02	0.1	0.0	2.0
6000.84c	1328	1.00000E-11	1.50000E+02	0.2	0.0	11.0
7014.84c	1826	1.00000E-11	1.50000E+02	0.2	0.0	18.0
7015.84c	939	1.00000E-11	2.00000E+01	0.1	0.0	7.0
8016.84c	2961	1.00000E-11	1.50000E+02	0.4	0.0	33.0
8017.84c	620	1.00000E-11	2.00000E+01	0.1	0.0	1.0
14028.84c	8019	1.00000E-11	1.50000E+02	1.0	0.0	115.0
14029.84c	4979	1.00000E-11	1.50000E+02	0.6	0.0	102.0
14030.84c	6089	1.00000E-11	1.50000E+02	0.7	0.0	88.0
24050.84c	29758	1.00000E-11	1.50000E+02	3.6	0.0	180.0
24052.84c	30705	1.00000E-11	1.50000E+02	3.7	0.0	201.0
24053.84c	21659	1.00000E-11	1.50000E+02	2.6	0.0	114.0
24054.84c	14261	1.00000E-11	1.50000E+02	1.7	0.0	121.0
25055.84c	11703	1.00000E-11	6.00000E+01	1.4	0.0	109.0
26054.84c	18775	1.00000E-11	1.50000E+02	2.3	0.0	139.0
26056.84c	26742	1.00000E-11	1.50000E+02	3.3	0.0	156.0
26057.84c	15731	1.00000E-11	1.50000E+02	1.9	0.0	200.0
26058.84c	10972	1.00000E-11	2.00000E+01	1.3	0.0	102.0
28058.84c	43443	1.00000E-11	1.50000E+02	5.3	0.0	302.0
28060.84c	33910	1.00000E-11	1.50000E+02	4.1	0.0	179.0
28061.84c	11091	1.00000E-11	1.50000E+02	1.4	0.0	94.0
28062.84c	11345	1.00000E-11	1.50000E+02	1.4	0.0	143.0
28064.84c	10310	1.00000E-11	1.50000E+02	1.3	0.0	272.0

\*\*\*\*\*

dump no. 1 on file NCT\_HP\_SC-55G1\_252Cf\_0.r nps = 0 coll = 0 ctm = 0.00  
nrn = 0

5 warning messages so far.  
1problem summary

run terminated when it had used 1200 minutes of computer time.

+

08/29/21 18:46:12

=====> 215.37 M histories/hr (based on wall-clock time in mcrun)

title HP/SC-55G1 with a Concentrated 252Cf Neutron Source - NCT probid = 08/29/21 17:56:08

neutron creation	tracks	weight (per source particle)	energy	neutron loss	tracks	weight (per source particle)	energy
source	179610771	1.0000E+00	3.1174E+00	escape	904560	5.0362E-03	8.7319E-03
nucl. interaction	0	0.	0.	energy cutoff	0	0.	0.
particle decay	0	0.	0.	time cutoff	0	0.	0.
weight window	0	0.	0.	weight window	0	0.	0.
cell importance	0	0.	0.	cell importance	0	0.	0.
weight cutoff	0	0.	0.	weight cutoff	0	0.	0.
e or t importance	0	0.	0.	e or t importance	0	0.	0.
dxtran	0	0.	0.	dxtran	0	0.	0.
forced collisions	0	0.	0.	forced collisions	0	0.	0.
exp. transform	0	0.	0.	exp. transform	0	0.	0.
upscattering	0	0.	1.2557E-06	downscattering	0	0.	3.0820E+00
photonuclear	0	0.	0.	capture	178716470	9.9502E-01	2.6014E-02
(n,xn)	20518	1.1424E-04	1.4017E-04	loss to (n,xn)	10259	5.7118E-05	8.1118E-04
prompt fission	0	0.	0.	loss to fission	0	0.	0.
delayed fission	0	0.	0.	nucl. interaction	0	0.	0.
prompt photofis	0	0.	0.	particle decay	0	0.	0.
tabular boundary	0	0.	0.	tabular boundary	0	0.	0.
tabular sampling	0	0.	0.	elastic scatter	0	0.	0.
total	179631289	1.0001E+00	3.1175E+00	total	179631289	1.0001E+00	3.1175E+00
number of neutrons banked	10259			average time of (shakes)			cutoffs
neutron tracks per source particle	1.0001E+00			escape	1.3396E+04		tco 1.0000E+33
neutron collisions per source particle	1.2434E+02			capture	1.6719E+04		eco 0.0000E+00
total neutron collisions	22333348203			capture or escape	1.6702E+04		wc1 0.0000E+00
net multiplication	1.0001E+00 0.0000			any termination	1.6701E+04		wc2 0.0000E+00

# ATTACHMENT A – Responses to RAI

photon creation	tracks	weight (per source particle)	energy (particle)	photon loss	tracks	weight (per source particle)	energy (particle)		
source	0	0.	0.	escape	13326433	7.4366E-02	8.7364E-02		
nucl. interaction	0	0.	0.	energy cutoff	5	2.8874E-08	9.1603E-05		
particle decay	0	0.	0.	time cutoff	0	0.	0.		
weight window	0	0.	0.	weight window	0	0.	0.		
cell importance	0	0.	0.	cell importance	0	0.	0.		
weight cutoff	0	0.	0.	weight cutoff	0	0.	0.		
e or t importance	0	0.	0.	e or t importance	0	0.	0.		
dxtran	0	0.	0.	dxtran	0	0.	0.		
forced collisions	0	0.	0.	forced collisions	0	0.	0.		
exp. transform	0	0.	0.	exp. transform	0	0.	0.		
from neutrons	183724143	1.0235E+00	2.3508E+00	compton scatter	0	0.	2.1216E+00		
bremsstrahlung	71282465	3.9732E-01	2.0634E-02	capture	294501761	1.6408E+00	1.1456E-01		
p-annihilation	9293618	5.1847E-02	2.6494E-02	pair production	4646809	2.5923E-02	7.6020E-02		
photonuclear	0	0.	0.	photonuclear abs	0	0.	0.		
electron x-rays	0	0.	0.	loss to photofis	0	0.	0.		
compton fluores	0	0.	0.						
muon capt fluores	0	0.	0.						
1st fluorescence	48174782	2.6844E-01	1.7244E-03						
2nd fluorescence	0	0.	0.						
cerenkov	0	0.	0.						
(gamma,xgamma)	0	0.	0.						
tabular sampling	0	0.	0.						
prompt photofis	0	0.	0.						
total	312475008	1.7411E+00	2.3997E+00	total	312475008	1.7411E+00	2.3997E+00		
number of photons banked	264300221			average time of (shakes)	cutoffs				
photon tracks per source particle	1.7397E+00			escape	1.6422E+04	tco	1.0000E+33		
photon collisions per source particle	1.1707E+01			capture	1.3736E+04	eco	1.0000E-03		
total photon collisions	2102691841			capture or escape	1.3853E+04	wc1	0.0000E+00		
				any termination	1.3886E+04	wc2	0.0000E+00		
computer time so far in this run	1200.62 minutes			maximum number ever in bank	29				
computer time in mcrun	1200.38 minutes			bank overflows to backup file	0				
source particles per minute	1.4963E+05								
random numbers generated	451701521423			most random numbers used was	46208 in history 41959132				
range of sampled source weights = 1.0000E+00 to 1.0000E+00									
number of histories processed by each thread									
7413106	7500612	7511946	7508849	7522273	7493121	7521121	7483149		
7528186	7415717	7344968	7449988	7497170	7513192	7501470	7502756		
7454180	7501672	7492271	7503335				7492285		
							7480655		
1neutron activity in each cell				print table 126					
	cell	tracks entering	population	collisions	collisions * weight (per history)	number weighted energy	flux weighted energy	average track weight (relative)	average track mfp (cm)
1	1	0	0	0	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
2	2	0	0	0	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
3	3	207549317	179610503	167527844	9.3273E-01	2.2112E-03	2.3257E+00	1.0000E+00	3.0958E+00
4	4	129624	91929	535901	2.9837E-03	9.6647E-04	1.1447E+00	1.0000E+00	4.3005E+00
5	5	4967796	3052661	20055802	1.1166E-01	6.8054E-04	1.2127E+00	1.0000E+00	4.0111E+00
6	6	128432	86933	496791	2.7659E-03	9.0300E-04	1.1649E+00	1.0000E+00	4.1846E+00
7	7	209017886	179558016	22133691671	1.2323E+02	6.9376E-05	4.4644E-01	1.0000E+00	9.5226E-01
8	8	2207459	1279003	0	0.0000E+00	1.1026E-03	7.7940E-01	1.0000E+00	0.0000E+00
9	201	2174681	1151214	2308648	1.2854E-02	1.4352E-03	1.0605E+00	1.0000E+00	2.9817E+00
10	202	1659535	1101581	8042364	4.4777E-02	5.8075E-04	9.3843E-01	1.0000E+00	1.8314E+01
11	203	1121278	978222	689182	3.8371E-03	1.0700E-03	1.2175E+00	1.0000E+00	2.7516E+00
12	204	2246518	1281169	0	0.0000E+00	2.1295E-03	1.3205E+00	1.0000E+00	0.0000E+00
13	205	915993	904560	0	0.0000E+00	1.9091E-03	1.6725E+00	1.0000E+00	0.0000E+00
14	301	34061	34061	0	0.0000E+00	2.4167E-03	1.7074E+00	1.0000E+00	0.0000E+00
15	302	11087	11087	0	0.0000E+00	2.3200E-03	1.9392E+00	1.0000E+00	0.0000E+00
total	432163667	369140939	22333348203	1.2434E+02					
1photon activity in each cell	print table 126								
	cell	tracks entering	population	collisions	collisions * weight (per history)	number weighted energy	flux weighted energy	average track weight (relative)	average track mfp (cm)
1	1	0	0	0	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
2	2	0	0	0	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
3	3	3100935	3968434	462872	2.5771E-03	1.8601E+00	1.8601E+00	1.0000E+00	1.9029E+01
4	4	11788598	14665123	44991208	2.5061E-01	9.2073E-01	9.2073E-01	1.0005E+00	1.7650E+00
5	5	144162951	178114686	561345723	3.1276E+00	9.9228E-01	9.9228E-01	1.0008E+00	1.8199E+00
6	6	11676279	14081753	42560563	2.3707E-01	9.1943E-01	9.1943E-01	1.0005E+00	1.7622E+00

## ATTACHMENT A – Responses to RAI

7	7	26871349	203104315	1389262306	7.7359E+00	8.8936E-01	8.8936E-01	1.0001E+00	1.2276E+01
8	8	32527417	25840038	0	0.0000E+00	8.9743E-01	8.9743E-01	1.0022E+00	0.0000E+00
9	201	26992732	25991432	39881352	2.2262E-01	9.2413E-01	9.2413E-01	1.0026E+00	1.7213E+00
10	202	19341219	17585434	9731396	5.4314E-02	8.7902E-01	8.7902E-01	1.0026E+00	9.6477E+01
11	203	17160862	17544007	14456421	8.0728E-02	9.4249E-01	9.4249E-01	1.0030E+00	1.7468E+00
12	204	30476892	26034740	0	0.0000E+00	1.0200E+00	1.0200E+00	1.0017E+00	0.0000E+00
13	205	13490645	13326433	0	0.0000E+00	1.1501E+00	1.1501E+00	1.0024E+00	0.0000E+00
14	301	497002	497002	0	0.0000E+00	1.0763E+00	1.0763E+00	1.0024E+00	0.0000E+00
15	302	160952	160952	0	0.0000E+00	1.2171E+00	1.2171E+00	1.0019E+00	0.0000E+00
total		338247833	540914349	2102691841	1.1711E+01				

summary of photons produced in neutron collisions in the tabular range

production by cell of photons created with energies above local photon energy cutoffs

cell	number of photons	weight per source neut	energy per source neut	avg photon energy	mev/gm per source neut	weight/neut collision	energy/neut collision
1	1	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
2	2	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
3	3	956007	5.32266E-03	1.61704E-02	3.03803E+00	1.33660E-03	5.70656E-02
4	4	81281	4.64008E-04	1.41689E-03	3.05359E+00	6.90503E-09	1.55515E-01
5	5	3822911	2.16684E-02	7.10207E-02	3.27762E+00	7.99679E-08	1.94052E-01
6	6	77914	4.44866E-04	1.38502E-03	3.11333E+00	7.49722E-09	1.60838E-01
7	7	178356548	9.93017E-01	2.25323E+00	2.26907E+00	2.25323E+00	8.05815E-03
8	8	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
9	201	294817	1.78438E-03	5.17628E-03	2.90088E+00	3.54455E-09	1.38824E-01
10	202	29572	1.64646E-04	4.58428E-04	2.78432E+00	6.55000E-10	3.67706E-03
11	203	105088	6.43015E-04	1.96102E-03	3.04972E+00	1.47917E-09	1.67579E-01
12	204	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
13	205	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
14	301	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
15	302	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
16	999	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
total	183724138	1.02351E+00	2.35081E+00	2.29682E+00			

energy distribution of photons produced in neutron collisions in the tabular range

all sampled photons from neutron collisions in the tabular range, without regard to energy cutoffs

energy interval	number of photons	number frequency	cum number distribution	weight of photons	weight frequency	cum weight distribution
20.000	4	2.17718E-08	2.17718E-08	2.52213E-08	2.46420E-08	2.46420E-08
15.000	44	2.39489E-07	2.61261E-07	2.53735E-07	2.47907E-07	2.72549E-07
10.000	1330	7.23911E-06	7.50038E-06	8.54827E-06	8.35193E-06	8.62447E-06
9.000	52742	2.87072E-04	2.94572E-04	2.98369E-04	2.91515E-04	3.00140E-04
8.000	29877	1.62619E-04	4.57191E-04	1.88405E-04	1.84078E-04	4.84218E-04
7.000	832038	4.52874E-03	4.98593E-03	4.65205E-03	4.54519E-03	5.02941E-03
6.000	189968	1.03398E-03	6.01991E-03	1.08625E-03	1.06130E-03	6.09071E-03
5.000	191017	1.03969E-03	7.05961E-03	1.09978E-03	1.07452E-03	7.16522E-03
4.000	4017239	2.18656E-02	2.89252E-02	2.24050E-02	2.18903E-02	2.90556E-02
3.000	599060	3.26065E-03	3.21859E-02	3.38591E-03	3.30814E-03	3.23637E-02
2.000	175248872	9.53870E-01	9.86055E-01	9.75781E-01	9.53368E-01	9.85732E-01
1.000	1057331	5.75499E-03	9.91810E-01	6.00239E-03	5.86452E-03	9.91596E-01
0.500	1148691	6.25226E-03	9.98063E-01	6.55112E-03	6.40065E-03	9.97997E-01
0.100	290749	1.58253E-03	9.99645E-01	1.65650E-03	1.61845E-03	9.99615E-01
0.010	59508	3.23899E-04	9.99969E-01	3.58229E-04	3.50001E-04	9.99965E-01
0.000	5673	3.08778E-05	1.00000E+00	3.53671E-05	3.45547E-05	1.00000E+00
<----- energy interval containing the global photon energy cutoff, 1.000E-03 Mev						
total	183724143	1.00000E+00		1.02351E+00	1.00000E+00	

warning. 5 photons from neutron collisions were created below a local photon energy cutoff and were not followed.

```

tally      4      nps = 179610771
+          Package Surface Neutron Dose Rate (mrem/hr) @ Z = 111.12500
          tally type 4      track length estimate of particle flux.
          particle(s): neutrons
          this tally is modified by dose function DE4 and DF4.

          volumes
            cell:      301
                  3.81204E+02

cell 301
      5.75450E-09 0.0082
  
```



# ATTACHMENT A – Responses to RAI

```

7.94-03 852 2.90-03 -2.537 *****
1.00-02 976 2.64-03 -2.578 *****
1.26-02 1920 4.13-03 -2.384 *****
1.58-02 10992 1.88-02 -1.726 *****
2.00-02 4527 6.14-03 -2.212 *****
2.51-02 1635 1.76-03 -2.754 *****
3.16-02 572 4.90-04 -3.310 *****
3.98-02 328 2.23-04 -3.652 *****
5.01-02 195 1.05-04 -3.977 *****
6.31-02 138 5.92-05 -4.228 *****
7.94-02 82 2.79-05 -4.554 *****
1.00-01 47 1.27-05 -4.895 *****
1.26-01 32 6.88-06 -5.162 *****
1.58-01 22 3.76-06 -5.425 *****
2.00-01 21 2.85-06 -5.545 *****
2.51-01 5 5.39-07 -6.269 *****
3.16-01 6 5.14-07 -6.289 *****
3.98-01 4 2.72-07 -6.565 *****
5.01-01 2 1.08-07 -6.966 *
total 34057 1.90-04 d-----d-----d-----d-----d-----d-----d-----d-----

```

tally 14 nps = 179610771  
 + 2-M from Package Surface Neutron Dose Rate (mrem/hr) @ Z = 111.12500  
 tally type 4 track length estimate of particle flux.  
 particle(s): neutrons  
 this tally is modified by dose function DE14 and DF14.

volumes  
 cell: 302  
 1.01958E+03

cell 302  
 5.13940E-10 0.0118

results of 10 statistical checks for the estimated answer for the tally fluctuation chart (tfc) bin of tally 14

tfc bin behavior	--mean-- behavior	-----relative error----- value	decrease	decrease rate	----variance of the variance---- value	decrease	decrease rate	--figure of merit-- value	behavior	-pdf- slope
desired	random	<0.10	yes	1/sqrt(nps)	<0.10	yes	1/nps	constant	random	>3.00
observed	random	0.01	yes	yes	0.00	yes	yes	constant	random	10.00
passed?	yes	yes	yes	yes	yes	yes	yes	yes	yes	yes

this tally meets the statistical criteria used to form confidence intervals: check the tally fluctuation chart to verify.  
 the results in other bins associated with this tally may not meet these statistical criteria.

----- estimated confidence intervals: -----

estimated asymmetric confidence interval(1,2,3 sigma): 5.0792E-10 to 5.2004E-10; 5.0186E-10 to 5.2610E-10; 4.9580E-10 to 5.3216E-10  
 estimated symmetric confidence interval(1,2,3 sigma): 5.0788E-10 to 5.2000E-10; 5.0182E-10 to 5.2606E-10; 4.9576E-10 to 5.3212E-10

1analysis of the results in the tally fluctuation chart bin (tfc) for tally 14 with nps = 179610771 print table 160

normed average tally per history = 5.13940E-10  
 estimated tally relative error = 0.0118  
 relative error from zero tallies = 0.0095

unnormed average tally per history = 5.24001E-07  
 estimated variance of the variance = 0.0002  
 relative error from nonzero scores = 0.0070

number of nonzero history tallies = 11086  
 history number of largest tally = 164142676  
 (largest tally)/(average tally) = 4.24835E+04

efficiency for the nonzero tallies = 0.0001  
 largest unnormalized history tally = 2.22614E-02  
 (largest tally)/(avg nonzero tally) = 2.62218E+00

(confidence interval shift)/mean = 0.0001

shifted confidence interval center = 5.13978E-10

if the largest history score sampled so far were to occur on the next history, the tfc bin quantities would change as follows:

estimated quantities	value at nps	value at nps+1	value(nps+1)/value(nps)-1.
mean	5.13940E-10	5.14062E-10	0.000237
relative error	1.17908E-02	1.17904E-02	-0.000035
variance of the variance	1.64429E-04	1.64458E-04	0.000180
shifted center	5.13978E-10	5.13978E-10	0.000000
figure of merit	5.99232E+00	5.99274E+00	0.000071





# ATTACHMENT A – Responses to RAI

variance of the variance	1.70047E-05	1.71047E-05	0.005881
shifted center	1.86528E-10	1.86528E-10	0.000000
figure of merit	9.92202E+01	9.91976E+01	-0.000228

the estimated inverse power slope of the 200 largest tallies starting at 8.55647E-04 is 4.4286  
the empirical history score probability density function appears to be increasing at the largest history scores:  
please examine. see print table 161.  
the large score tail of the empirical history score probability density function appears to have no unsampled regions.

fom = (histories/minute)\*(f(x) signal-to-noise ratio)\*\*2 = (1.496E+05)\*( 2.575E-02)\*\*2 = (1.496E+05)\*(6.631E-04) = 9.922E+01

1status of the statistical checks used to form confidence intervals for the mean for each tally bin

tally result of statistical checks for the tfc bin (the first check not passed is listed) and error magnitude check for all bins

- 4 missed 1 of 10 tfc bin checks: the estimated mean has a trend during the last half of the problem  
passed all bin error check: 1 tally bins all have relative errors less than 0.10 with no zero bins
- 14 passed the 10 statistical checks for the tally fluctuation chart bin result  
passed all bin error check: 1 tally bins all have relative errors less than 0.10 with no zero bins
- 24 missed 2 of 10 tfc bin checks: the variance of the variance does not monotonically decrease over the last half of problem  
passed all bin error check: 1 tally bins all have relative errors less than 0.10 with no zero bins
- 34 passed the 10 statistical checks for the tally fluctuation chart bin result  
passed all bin error check: 1 tally bins all have relative errors less than 0.10 with no zero bins

the 10 statistical checks are only for the tally fluctuation chart bin and do not apply to other tally bins.

warning. 2 of the 4 tally fluctuation chart bins did not pass all 10 statistical checks.  
1tally fluctuation charts

nps	mean	tally error	4 vov	slope	fom	mean	tally error	14 vov	slope	fom	mean	tally error	24 vov	slope	fom
16384000	5.8550E-09	0.0260	0.0079	2.8	13	5.2106E-10	0.0386	0.0017	1.7 6.1E+00	1.7526E-09	0.0057	0.0015	3.1	278	
32768000	5.6875E-09	0.0195	0.0084	2.9	12	5.2677E-10	0.0272	0.0009	1.7 6.1E+00	1.7527E-09	0.0040	0.0005	4.2	280	
49152000	5.6624E-09	0.0160	0.0070	3.0	12	5.2368E-10	0.0223	0.0006	1.7 6.1E+00	1.7507E-09	0.0034	0.0012	3.3	268	
65536000	5.6018E-09	0.0137	0.0052	3.8	12	5.2262E-10	0.0194	0.0004	1.7 6.1E+00	1.7509E-09	0.0029	0.0008	3.0	270	
81920000	5.5984E-09	0.0121	0.0037	4.4	12	5.2263E-10	0.0173	0.0004	1.7 6.1E+00	1.7519E-09	0.0026	0.0005	3.3	273	
98304000	5.6134E-09	0.0111	0.0043	3.9	12	5.2001E-10	0.0158	0.0003	2.0 6.1E+00	1.7515E-09	0.0024	0.0004	3.0	272	
114688000	5.6582E-09	0.0102	0.0037	4.0	12	5.1890E-10	0.0147	0.0003	10.0 6.0E+00	1.7478E-09	0.0022	0.0003	2.9	274	
131072000	5.6723E-09	0.0096	0.0033	3.7	12	5.1761E-10	0.0138	0.0002	10.0 6.0E+00	1.7486E-09	0.0020	0.0003	3.3	275	
147456000	5.7024E-09	0.0089	0.0027	3.8	13	5.1484E-10	0.0130	0.0002	10.0 6.0E+00	1.7493E-09	0.0020	0.0011	3.3	266	
163840000	5.7280E-09	0.0086	0.0026	3.9	12	5.1540E-10	0.0123	0.0002	10.0 6.0E+00	1.7486E-09	0.0019	0.0010	3.1	263	
179610771	5.7545E-09	0.0082	0.0024	4.2	12	5.1394E-10	0.0118	0.0002	10.0 6.0E+00	1.7499E-09	0.0018	0.0009	3.1	264	

nps	mean	tally error	34 vov	slope	fom
16384000	1.8738E-10	0.0096	0.0002	3.3	99
32768000	1.8658E-10	0.0068	0.0001	10.0	100
49152000	1.8645E-10	0.0055	0.0001	1.7	99
65536000	1.8698E-10	0.0048	0.0000	1.7	99
81920000	1.8658E-10	0.0043	0.0000	1.8	99
98304000	1.8657E-10	0.0039	0.0000	2.6	99
114688000	1.8621E-10	0.0036	0.0000	3.8	99
131072000	1.8641E-10	0.0034	0.0000	4.5	99
147456000	1.8649E-10	0.0032	0.0000	4.4	99
163840000	1.8637E-10	0.0030	0.0000	5.8	99
179610771	1.8653E-10	0.0029	0.0000	4.4	99

\*\*\*\*\*

dump no. 2 on file NCT\_HP\_SC-55G1\_252cf\_0.r nps = 179610771 coll = 24436040044 ctm = 1200.38  
nrn = 451701521423  
tally data written to file NCT\_HP\_SC-55G1\_252cf\_0.m

9 warning messages so far.

run terminated when it had used 1200 minutes of computer time.

computer time = 1200.62 minutes

mcnp version 6 02/20/18

08/29/21 18:46:12

probid = 08/29/21 17:56:08



## 4. SC-55G1 HAC Model with <sup>252</sup>Cf – Polyethylene with Secondary Gammas

Code Name & Version = MCNP\_6.20, 6.2.0



```

-----
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|-----
  
```

```

1mcnp version 6 ld=02/20/18 08/29/21 21:19:57
*****
i=HAC_HP_SC-55G1_252Cf_0.i name=HAC_HP_SC-55G1_252Cf_0. tasks 24
  
```

probid = 08/29/21 21:19:57

warning. universe map (print table 128) disabled.

comment. Physics models disabled.

```

1- title HP/SC-55G1 with a Concentrated 252Cf Neutron Source - HAC
2- c
3- c Universe Fill Boundary
4- c
5- 1 0 -97 98 -99 fill=1 $Shielded Container 1
6- imp:n=1 imp:p=1 trcl=1
7- 2 0 -97 98 -99 fill=1 $Shielded Container 2
8- imp:n=1 imp:p=1 trcl=2
9- c
10- c Payload Cell $Material Density 100%
11- c
12- 3 1 -0.9400 -1 2 -3 $Payload
13- imp:n=1 imp:p=1 u=1
14- c
15- c Shielded Container Cells $Material Density 100%
16- c
17- 4 2 -7.8526 -11 12 -13 -14 $Base Steel
18- imp:n=1 imp:p=1 u=1
19- 5 2 -7.8526 13 15 -16 -18 20 $Sidewall Steel
20- (-15 :17 :18 :19)
21- imp:n=1 imp:p=1 u=1
22- 6 2 -7.8526 -24 25 -26 -28 $Lid Steel
23- ((18 :-25 :-27)
24- (18 :27 :-30 :-31)
25- (-18 :-27 :32 :33)
26- (-25 :27 :-29))
27- imp:n=1 imp:p=1 u=1
28- c
29- c Cavity (Void) Cells
30- c
31- 7 1 -0.9400 ((13 -15 -25): $Payload Cavity
32- (15 -17 -19 -25):
33- (17 -18 -20):
34- (-17 -18 30 31):
35- (-17 25 29):
36- (-17 27 -29 -31):
37- (18 27 -32 -33))
38- (1 :-2 :3)
  
```

## ATTACHMENT A – Responses to RAI

39-				imp:n=1	imp:p=1	u=1	
40-	8	0		(11 : -12 :13 :14)			\$Exterior Void
41-				(-13 :16 :18)			
42-				(-18 :24 :26 :28)			
43-				imp:n=1	imp:p=1	u=1	
44-	C						
45-	C		HalfPACT Package Cells				\$Material Density 100%
46-	C						
47-		201	4	-8.0128	(201 -202 204 -205):		\$HalfPACT ICV/OCV Steel Structure
48-					(-202 203 -204):		
49-					(-202 205 -206)		
50-					imp:n=1	imp:p=1	
51-	C						
52-	C		HalfPACT Package Void Cells				
53-	C						
54-		202	0		-201 204 -205		\$HalfPACT ICV Interior Void
55-					#1 #2		
56-					imp:n=1	imp:p=1	
57-		203	0		(202 203 -206 -211):		\$HalfPACT OCA Polyurethane Foam
58-					(-203 -211 214):		
59-					(206 -211 -215)		
60-					imp:n=1	imp:p=1	
61-		204	0		(211 -212 214 -215):		\$HalfPACT OCA Steel Structure
62-					(-212 213 -214):		
63-					(-212 215 -216)		
64-					imp:n=1	imp:p=1	
65-		205	0		-999		\$HalfPACT OCA Exterior Void
66-					((212 213 -216):		
67-					(-213):		
68-					(216))		
69-					(-301 :302 :303)		
70-					imp:n=1	imp:p=1	
71-	C						
72-	C		HalfPACT Package 1-meter Tally Cell				
73-	C						
74-		301	0		301 -302 -303		\$Package Side Middle @ 1-Meter
75-					imp:n=1	imp:p=1	
76-	C						
77-	C		World Cell				
78-	C						
79-		999	0		999		
80-					imp:n=0	imp:p=0	
81-							
82-	C						
83-	C		Payload Surfaces				
84-	C						
85-		1	c/z	0.00000	30.47999	1.27000	\$Radius
86-		2	pz	50.10150			\$Plane, Bottom
87-		3	pz	52.64150			\$Plane, Top
88-	C						
89-	C		Shielded Container Base Surfaces				
90-	C						
91-		11	cz	36.77920			\$Radius, Base Outer
92-		12	pz	0.59690			\$Plane, Base Bottom
93-		13	pz	5.96900			\$Plane, Base Top
94-		14	kz	-37.02050	1.00000	1	\$Chamfer, Base Bottom Outside Corner
95-	C						
96-	C		Shielded Container Sidewall Surfaces				
97-	C						
98-		15	cz	31.75000			\$Radius, Sidewall Inner
99-		16	cz	36.77920			\$Radius, Sidewall Outer
100-		17	cz	31.95320			\$Radius, Lid Engagement Step
101-		18	pz	99.31400			\$Plane, Sidewall Top
102-		19	kz	64.70650	1.00000	1	\$Cone, Lid Engagement Transition
103-		20	kz	11.20580	0.13247		\$Chamfer, Top Inside Corner
104-	C						
105-	C		Shielded Container Lid Surfaces				
106-	C						
107-		24	cz	36.77920			\$Radius, Lid Outer
108-		25	pz	96.77400			\$Plane, Lid Bottom
109-		26	pz	102.26040			\$Plane, Lid Top
110-		27	cz	31.91510			\$Radius, Lid Step
111-		28	kz	139.89050	1.00000	-1	\$Chamfer, Top Outside Corner
112-		29	kz	9.72298	0.13247	1	\$Chamfer, Bottom Outside Corner
113-		30	cz	31.76270			\$Radius, Vent Port Groove Inner
114-		31	pz	98.39960			\$Plane, Vent Port Groove Bottom
115-		32	cz	33.78200			\$Radius, Gasket Recess Outer
116-		33	pz	99.63150			\$Plane, Gasket Recess Top
117-	C						
118-	C		Shielded Container Universe Fill Boundary Surfaces				
119-	C						

## ATTACHMENT A – Responses to RAI

```

120-      97      cz      36.77921      $Radius, Fill Boundary
121-      98      pz      -0.00001      $Plane, Fill Boundary Bottom
122-      99      pz      102.87001      $Plane, Fill Boundary Top
123-      C
124-      C      HalfPACT Package ICV/OCV Surfaces
125-      C
126-      201      cz      92.23375      $Radius, Shell Inner
127-      202      cz      93.34500      $Radius, Shell Outer
128-      203      pz      22.86000      $Plane, Lower Head Bottom
129-      204      pz      24.13000      $Plane, Lower Head Top
130-      205      pz      198.12000      $Plane, Upper Head Bottom
131-      206      pz      199.39000      $Plane, Upper Head Top
132-      C
133-      C      HalfPACT Package OCA Surfaces
134-      C
135-      211      cz      118.74500      $Radius, Shell Inner
136-      212      cz      119.38000      $Radius, Shell Outer
137-      213      pz      0.00000      $Plane, Lower Head Bottom
138-      214      pz      0.63500      $Plane, Lower Head Top
139-      215      pz      229.23500      $Plane, Upper Head Bottom
140-      216      pz      229.87000      $Plane, Upper Head Top
141-      C
142-      C      HalfPACT Package Tally Surfaces
143-      C
144-      301      py      219.38000      $Plane, Side Disk Inside @ 1.00-meter
145-      302      py      219.48000      $Plane, Side Disk Outside @ 1.00-meter
146-      303      c/y      0.00000 111.12500 2.54000 $Radius, Side Disk
147-      C
148-      C      Define World Surface (Problem Boundary)
149-      C
150-      999      sz      114.93500      400
151-
152-      C
153-      C      Physics Cards
154-      C
155-      mode n p
comment. photonuclear physics may be needed (phys:p).
156-      C
157-      C      Material Cards
158-      C
159-      m1      1001.84C -0.143685      $Payload (Polyethylene)
160-      1002.84C -0.000033      6000.84C -0.856282
161-      plib = 84P
162-      C
163-      m2      26054.84C -0.058450      $Carbon Steel
164-      26056.84C -0.917540      26057.84C -0.021190      26058.84C -0.002820
165-      plib = 84P
166-      C
167-      m4      14028.84C -0.009222      $Stainless Steel (ASTM A240, Type 304)
168-      14029.84C -0.000469      14030.84C -0.000309      24050.84C -0.008256
169-      24052.84C -0.159199      24053.84C -0.018052      24054.84C -0.004494
170-      25055.84C -0.020000      26054.84C -0.039746      26056.84C -0.623927
171-      26057.84C -0.014409      26058.84C -0.001918      28058.84C -0.068077
172-      28060.84C -0.026223      28061.84C -0.001140      28062.84C -0.003635
173-      28064.84C -0.000926
174-      plib = 84P
175-      C
176-      C      Specify Universe Transformations
177-      C
178-      *tr1 -36.77922 41.00094 59.75349      $shielded Container 1
179-      *tr2 36.77922 41.00094 59.75349      $shielded Container 2
180-      C
181-      C      Specify Explicit Analysis for Weight windows Evaluation
182-      C
183-      cut:n 2j 0
184-      cut:p 2j 0
185-      C
186-      C      Source Cards
187-      C
188-      sdef par=1 axs=0 0 1 erg=d1 pos=d2 rad=d3 ext=d4
189-      sc1 Concentrated 252Cf Neutron Source
190-      si1 L 0.100000 0.500000 1.000000 2.000000 3.000000
191-      4.000000 6.000000 8.000000 10.000000 15.000000
192-      sp1 0.00E+00 1.80E+11 2.71E+11 5.36E+11 4.10E+11
193-      2.73E+11 2.66E+11 8.53E+10 2.44E+10 8.36E+09
194-      si2 L -36.77922 71.48093 111.12500 36.77922 71.48093 111.12500
195-      sp2 1 1
196-      si3 0.00000 1.27000
197-      sp3 -21 1 1
198-      si4 -1.27000 1.27000
199-      sp4 -21 0 0

```

# ATTACHMENT A – Responses to RAI

```

200- c
201- c Package Tally Cards
202- c
203- f4:n 301
204- fc4 1-M from Package Surface Neutron Dose Rate (mrem/hr) @ Z = 111.12500
205- sd4 2.02683
206- f14:p 301
207- fc14 1-M from Package Surface Gamma Dose Rate (mrem/hr) @ Z = 111.12500
208- sd14 2.02683
209- c
210- c ANSI/ANS-6.1.1-1977 Neutron Flux-to-Dose Rate Factor Cards
211- c
212- de0 2.50E-08 1.00E-07 1.00E-06 1.00E-05 1.00E-04 $Energy (Mev)
213- 1.00E-03 1.00E-02 1.00E-01 5.00E-01 1.00E+00
214- 2.50E+00 5.00E+00 7.00E+00 1.00E+01 1.40E+01
215- 2.00E+01
216- df0 3.67E-03 3.67E-03 4.46E-03 4.54E-03 4.18E-03 $Factor (mrem/hr)
217- 3.76E-03 3.56E-03 2.17E-02 9.26E-02 1.32E-01
218- 1.25E-01 1.56E-01 1.47E-01 1.47E-01 2.08E-01
219- 2.27E-01
220- c
221- c ANSI/ANS-6.1.1-1977 Gamma Flux-to-Dose Rate Factor Cards
222- c
223- de14 0.01 0.03 0.05 0.07 0.10 $Energy (Mev)
224- 0.15 0.20 0.25 0.30 0.35
225- 0.40 0.45 0.50 0.55 0.60
226- 0.65 0.70 0.80 1.00 1.40
227- 1.80 2.20 2.60 2.80 3.25
228- 3.75 4.25 4.75 5.00 5.25
229- 5.75 6.25 6.75 7.50 9.00
230- 11.00 13.00 15.00
231- df14 3.96E-03 5.82E-04 2.90E-04 2.58E-04 2.83E-04 $Factor (mrem/hr)
232- 3.79E-04 5.01E-04 6.31E-04 7.59E-04 8.78E-04
233- 9.85E-04 1.08E-03 1.17E-03 1.27E-03 1.36E-03
234- 1.44E-03 1.52E-03 1.68E-03 1.98E-03 2.51E-03
235- 2.99E-03 3.42E-03 3.82E-03 4.01E-03 4.41E-03
236- 4.83E-03 5.23E-03 5.60E-03 5.80E-03 6.01E-03
237- 6.37E-03 6.74E-03 7.11E-03 7.66E-03 8.77E-03
238- 1.03E-02 1.18E-02 1.33E-02
239- c
240- c Runtime and Print Cards
241- c
242- prdmp j j 1 2
243- ctme 9600

```

```

*****
* Random Number Generator = 1 *
* Random Number Seed = 19073486328125 *
* Random Number Multiplier = 19073486328125 *
* Random Number Adder = 0 *
* Random Number Bits Used = 48 *
* Random Number Stride = 152917 *
*****

```

comment. total nubar used if fissionable isotopes are present.

```

surface 11 and surface 16 are the same. 16 will be deleted.
surface 11 and surface 24 are the same. 24 will be deleted.
surface 1098 and surface 2098 are the same. 2098 will be deleted.
surface 1099 and surface 2099 are the same. 2099 will be deleted.

```

comment. 4 surfaces were deleted for being the same as others.  
1cells

print table 60

cell	mat	atom density	gram density	volume	mass	pieces	neutron importance	photon importance	photon wt generation
1	1	0.00000E+00	0.00000E+00	4.37163E+05	0.00000E+00	1	1.0000E+00	1.0000E+00	-1.000E+00
2	2	0.00000E+00	0.00000E+00	4.37163E+05	0.00000E+00	1	1.0000E+00	1.0000E+00	-1.000E+00
3	3	1.21070E-01	9.40000E-01	1.28704E+01	1.20981E+01	1	1.0000E+00	1.0000E+00	-1.000E+00
4	4	2.846854E-02	7.85260E+00	2.28296E+04	1.79272E+05	1	1.0000E+00	1.0000E+00	-1.000E+00
5	5	2.846854E-02	7.85260E+00	1.00953E+05	7.92741E+05	1	1.0000E+00	1.0000E+00	-1.000E+00
6	6	2.846854E-02	7.85260E+00	2.04841E+04	1.60853E+05	1	1.0000E+00	1.0000E+00	-1.000E+00
7	7	1.21070E-01	9.40000E-01	0.00000E+00	0.00000E+00	0	1.0000E+00	1.0000E+00	-1.000E+00
8	8	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0	1.0000E+00	1.0000E+00	-1.000E+00
9	201	4.80954E-02	8.01280E+00	1.82252E+05	1.46035E+06	1	1.0000E+00	1.0000E+00	-1.000E+00
10	202	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0	1.0000E+00	1.0000E+00	-1.000E+00

# ATTACHMENT A – Responses to RAI

11	203	0	0.00000E+00	0.00000E+00	5.29418E+06	0.00000E+00	1	1.0000E+00	1.0000E+00	-1.000E+00
12	204	0	0.00000E+00	0.00000E+00	1.65455E+05	0.00000E+00	1	1.0000E+00	1.0000E+00	-1.000E+00
13	205	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0	1.0000E+00	1.0000E+00	-1.000E+00
14	301	0	0.00000E+00	0.00000E+00	2.02683E+00	0.00000E+00	1	1.0000E+00	1.0000E+00	-1.000E+00
15	999	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0	0.0000E+00	0.0000E+00	-1.000E+00

total 6.66049E+06 2.59323E+06

minimum source weight = 1.0000E+00 maximum source weight = 1.0000E+00

comment. threading will be used when possible in portions of mcnp6.

comment. threading will be used for n/p/e table physics.

comment. threading will generally not be used for model physics.

1 warning message so far.

1cross-section tables print table 100

XSDIR used: C:\MCNP\MCNP\_DATA\xsdir\_mcnp6.2

table	length						
tables from file xdata/endl71x/H/1001.714nc							
1001.84c	15325	H1 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53)	mat 125	12/17/12			
		Energy range: 1.00000E-11 to 2.00000E+01 Mev.					
		particle-production data for deuterons being expunged from 1001.84c					
		temperature = 2.1543E-07 adjusted to 2.5300E-08					
tables from file xdata/endl71x/H/1002.714nc							
1002.84c	7283	H2 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53)	mat 128	12/17/12			
		Energy range: 1.00000E-11 to 1.50000E+02 Mev.					
		particle-production data for protons being expunged from 1002.84c					
		particle-production data for tritons being expunged from 1002.84c					
		temperature = 2.1543E-07 adjusted to 2.5300E-08					
tables from file xdata/endl71x/C/6000.714nc							
6000.84c	55343	C0 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53)	mat 600	12/20/12			
		Energy range: 1.00000E-11 to 1.50000E+02 Mev.					
		particle-production data for protons being expunged from 6000.84c					
		particle-production data for deuterons being expunged from 6000.84c					
		particle-production data for alphas being expunged from 6000.84c					
		temperature = 2.1543E-07 adjusted to 2.5300E-08					
tables from file xdata/endl71x/Si/14028.714nc							
14028.84c	169896	Si28 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53)	mat1425	12/14/12			
		Energy range: 1.00000E-11 to 1.50000E+02 Mev.					
		particle-production data for protons being expunged from 14028.84c					
		particle-production data for deuterons being expunged from 14028.84c					
		particle-production data for tritons being expunged from 14028.84c					
		particle-production data for alphas being expunged from 14028.84c					
		temperature = 2.1543E-07 adjusted to 2.5300E-08					
tables from file xdata/endl71x/Si/14029.714nc							
14029.84c	158834	Si29 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53)	mat1428	12/14/12			
		Energy range: 1.00000E-11 to 1.50000E+02 Mev.					
		particle-production data for protons being expunged from 14029.84c					
		particle-production data for deuterons being expunged from 14029.84c					
		particle-production data for tritons being expunged from 14029.84c					
		particle-production data for alphas being expunged from 14029.84c					
		temperature = 2.1543E-07 adjusted to 2.5300E-08					
tables from file xdata/endl71x/Si/14030.714nc							
14030.84c	130018	Si30 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53)	mat1431	12/16/12			
		Energy range: 1.00000E-11 to 1.50000E+02 Mev.					
		particle-production data for protons being expunged from 14030.84c					
		particle-production data for deuterons being expunged from 14030.84c					
		particle-production data for tritons being expunged from 14030.84c					
		particle-production data for alphas being expunged from 14030.84c					
		temperature = 2.1543E-07 adjusted to 2.5300E-08					
tables from file xdata/endl71x/Cr/24050.714nc							
24050.84c	291186	Cr50 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53)	mat2425	12/13/12			
		Energy range: 1.00000E-11 to 1.50000E+02 Mev.					
		particle-production data for protons being expunged from 24050.84c					

## ATTACHMENT A – Responses to RAI

		particle-production data for deuterons being expunged from 24050.84c particle-production data for tritons being expunged from 24050.84c particle-production data for alphas being expunged from 24050.84c temperature = 2.1543E-07 adjusted to 2.5300E-08			
		tables from file xdata/endl71x/Cr/24052.714nc			
24052.84c	310582	Cr52 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 1.50000E+02 Mev. particle-production data for protons being expunged from 24052.84c particle-production data for deuterons being expunged from 24052.84c particle-production data for tritons being expunged from 24052.84c particle-production data for alphas being expunged from 24052.84c temperature = 2.1543E-07 adjusted to 2.5300E-08	mat2431	12/13/12	
		tables from file xdata/endl71x/Cr/24053.714nc			
24053.84c	254692	Cr53 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 1.50000E+02 Mev. particle-production data for protons being expunged from 24053.84c particle-production data for deuterons being expunged from 24053.84c particle-production data for tritons being expunged from 24053.84c particle-production data for alphas being expunged from 24053.84c temperature = 2.1543E-07 adjusted to 2.5300E-08	mat2434	12/13/12	
		tables from file xdata/endl71x/Cr/24054.714nc			
24054.84c	190185	Cr54 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 1.50000E+02 Mev. particle-production data for protons being expunged from 24054.84c particle-production data for deuterons being expunged from 24054.84c particle-production data for tritons being expunged from 24054.84c particle-production data for alphas being expunged from 24054.84c temperature = 2.1543E-07 adjusted to 2.5300E-08	mat2437	12/13/12	
		tables from file xdata/endl71x/Mn/25055.714nc			
25055.84c	455909	Mn55 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 6.00000E+01 Mev. particle-production data for protons being expunged from 25055.84c particle-production data for deuterons being expunged from 25055.84c particle-production data for tritons being expunged from 25055.84c particle-production data for helions being expunged from 25055.84c particle-production data for alphas being expunged from 25055.84c probability tables used from 1.2500E-01 to 1.0000E+00 mev. temperature = 2.1543E-07 adjusted to 2.5300E-08	mat2525	12/18/12	
		tables from file xdata/endl71x/Fe/26054.714nc			
26054.84c	217705	Fe54 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 1.50000E+02 Mev. particle-production data for protons being expunged from 26054.84c particle-production data for deuterons being expunged from 26054.84c particle-production data for tritons being expunged from 26054.84c particle-production data for alphas being expunged from 26054.84c temperature = 2.1543E-07 adjusted to 2.5300E-08	mat2625	12/22/12	
		tables from file xdata/endl71x/Fe/26056.714nc			
26056.84c	352429	Fe56 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 1.50000E+02 Mev. particle-production data for protons being expunged from 26056.84c particle-production data for deuterons being expunged from 26056.84c particle-production data for tritons being expunged from 26056.84c particle-production data for alphas being expunged from 26056.84c temperature = 2.1543E-07 adjusted to 2.5300E-08	mat2631	12/22/12	
		tables from file xdata/endl71x/Fe/26057.714nc			
26057.84c	241212	Fe57 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 1.50000E+02 Mev. particle-production data for protons being expunged from 26057.84c particle-production data for deuterons being expunged from 26057.84c particle-production data for tritons being expunged from 26057.84c particle-production data for alphas being expunged from 26057.84c temperature = 2.1543E-07 adjusted to 2.5300E-08	mat2634	12/22/12	
		tables from file xdata/endl71x/Fe/26058.714nc			
26058.84c	135502	Fe58 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 2.00000E+01 Mev.	mat2637	12/22/12	

## ATTACHMENT A – Responses to RAI

particle-production data for protons being expunged from 26058.84c  
particle-production data for alphas being expunged from 26058.84c  
temperature = 2.1543E-07 adjusted to 2.5300E-08

tables from file xdata/endl71x/Ni/28058.714nc

28058.84c	420627	Ni58 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 1.50000E+02 Mev. particle-production data for protons being expunged from 28058.84c particle-production data for deuterons being expunged from 28058.84c particle-production data for tritons being expunged from 28058.84c particle-production data for alphas being expunged from 28058.84c temperature = 2.1543E-07 adjusted to 2.5300E-08	mat2825	12/15/12
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tables from file xdata/endl71x/Ni/28060.714nc

28060.84c	344192	Ni60 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 1.50000E+02 Mev. particle-production data for protons being expunged from 28060.84c particle-production data for deuterons being expunged from 28060.84c particle-production data for tritons being expunged from 28060.84c particle-production data for alphas being expunged from 28060.84c temperature = 2.1543E-07 adjusted to 2.5300E-08	mat2831	12/17/12
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tables from file xdata/endl71x/Ni/28061.714nc

28061.84c	190713	Ni61 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 1.50000E+02 Mev. particle-production data for protons being expunged from 28061.84c particle-production data for deuterons being expunged from 28061.84c particle-production data for tritons being expunged from 28061.84c particle-production data for alphas being expunged from 28061.84c temperature = 2.1543E-07 adjusted to 2.5300E-08	mat2834	12/13/12
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tables from file xdata/endl71x/Ni/28062.714nc

28062.84c	169202	Ni62 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 1.50000E+02 Mev. particle-production data for protons being expunged from 28062.84c particle-production data for deuterons being expunged from 28062.84c particle-production data for tritons being expunged from 28062.84c particle-production data for alphas being expunged from 28062.84c probability tables used from 6.0000E-01 to 1.0000E+00 mev. temperature = 2.1543E-07 adjusted to 2.5300E-08	mat2837	12/17/12
-----------	--------	--	---------	----------

tables from file xdata/endl71x/Ni/28064.714nc

28064.84c	152759	Ni64 ENDF71x (jlconlin) Ref. see jlconlin (ref 09/10/2012 10:00:53) Energy range: 1.00000E-11 to 1.50000E+02 Mev. particle-production data for protons being expunged from 28064.84c particle-production data for deuterons being expunged from 28064.84c particle-production data for tritons being expunged from 28064.84c particle-production data for alphas being expunged from 28064.84c temperature = 2.1543E-07 adjusted to 2.5300E-08	mat2843	12/17/12
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tables from file xdata/mcplib84

1000.84p	1974	Update of MCPLIB04 Photon Compton Broadening Data For MCNP5 see LA-UR- Energy range: 1.00000E-03 to 1.00000E+05 Mev.	12-00018	01/03/12
6000.84p	3228	Update of MCPLIB04 Photon Compton Broadening Data For MCNP5 see LA-UR- Energy range: 1.00000E-03 to 1.00000E+05 Mev.	12-00018	01/03/12
14000.84p	4868	Update of MCPLIB04 Photon Compton Broadening Data For MCNP5 see LA-UR- Energy range: 1.00000E-03 to 1.00000E+05 Mev.	12-00018	01/03/12
24000.84p	5758	Update of MCPLIB04 Photon Compton Broadening Data For MCNP5 see LA-UR- Energy range: 1.00000E-03 to 1.00000E+05 Mev.	12-00018	01/03/12
25000.84p	5674	Update of MCPLIB04 Photon Compton Broadening Data For MCNP5 see LA-UR- Energy range: 1.00000E-03 to 1.00000E+05 Mev.	12-00018	01/03/12
26000.84p	5794	Update of MCPLIB04 Photon Compton Broadening Data For MCNP5 see LA-UR- Energy range: 1.00000E-03 to 1.00000E+05 Mev.	12-00018	01/03/12
28000.84p	5902	Update of MCPLIB04 Photon Compton Broadening Data For MCNP5 see LA-UR- Energy range: 1.00000E-03 to 1.00000E+05 Mev.	12-00018	01/03/12

total 4296792

comment. 20 cross sections modified by free gas thermal treatment.

maximum photon energy set to 100.0 mev (maximum electron energy)

tables from file xdata/e103

1000.03e 2329

6/6/98

# ATTACHMENT A – Responses to RAI

```

6000.03e 2333 Energy range: 1.00000E-03 to 1.00000E+03 MeV. 6/6/98
14000.03e 2339 Energy range: 1.00000E-03 to 1.00000E+03 MeV. 6/6/98
24000.03e 2345 Energy range: 1.00000E-03 to 1.00000E+03 MeV. 6/6/98
25000.03e 2345 Energy range: 1.00000E-03 to 1.00000E+03 MeV. 6/6/98
26000.03e 2345 Energy range: 1.00000E-03 to 1.00000E+03 MeV. 6/6/98
28000.03e 2347 Energy range: 1.00000E-03 to 1.00000E+03 MeV. 6/6/98
Energy range: 1.00000E-03 to 1.00000E+03 MeV.

```

1particles and energy limits

print table 101

particle type	particle cutoff energy	maximum particle energy	smallest table maximum	largest table maximum	always use table below	always use model above
1 n neutron	0.0000E+00	1.0000E+36	2.0000E+01	1.5000E+02	1.0000E+36	1.0000E+36
2 p photon	1.0000E-03	1.0000E+02	1.0000E+05	1.0000E+05	1.0000E+36	1.0000E+36
3 e electron	1.0000E-03	1.0000E+02	1.0000E+02	1.0000E+02	1.0000E+36	1.0000E+36

warning. material 2 has been set to a conductor.

warning. material 4 has been set to a conductor.

comment. setting up hash-based fast table search for xsec tables

=====> Set up arrays for hash-based fast table search for xsec data

```

number of hash bins = 8192
min hash table energy = 1.00000E-11
max hash table energy = 1.50000E+02

```

nuclide	ne	emin	emax	ave_bins	min_bins	max_bins
1001.84c	590	1.00000E-11	2.00000E+01	0.1	0.0	1.0
1002.84c	583	1.00000E-11	1.50000E+02	0.1	0.0	2.0
6000.84c	1328	1.00000E-11	1.50000E+02	0.2	0.0	11.0
14028.84c	8019	1.00000E-11	1.50000E+02	1.0	0.0	115.0
14029.84c	4979	1.00000E-11	1.50000E+02	0.6	0.0	102.0
14030.84c	6089	1.00000E-11	1.50000E+02	0.7	0.0	88.0
24050.84c	29758	1.00000E-11	1.50000E+02	3.6	0.0	180.0
24052.84c	30705	1.00000E-11	1.50000E+02	3.7	0.0	201.0
24053.84c	21659	1.00000E-11	1.50000E+02	2.6	0.0	114.0
24054.84c	14261	1.00000E-11	1.50000E+02	1.7	0.0	121.0
25055.84c	11703	1.00000E-11	6.00000E+01	1.4	0.0	109.0
26054.84c	18775	1.00000E-11	1.50000E+02	2.3	0.0	139.0
26056.84c	26742	1.00000E-11	1.50000E+02	3.3	0.0	156.0
26057.84c	15731	1.00000E-11	1.50000E+02	1.9	0.0	200.0
26058.84c	10972	1.00000E-11	2.00000E+01	1.3	0.0	102.0
28058.84c	43443	1.00000E-11	1.50000E+02	5.3	0.0	302.0
28060.84c	33910	1.00000E-11	1.50000E+02	4.1	0.0	179.0
28061.84c	11091	1.00000E-11	1.50000E+02	1.4	0.0	94.0
28062.84c	11345	1.00000E-11	1.50000E+02	1.4	0.0	143.0
28064.84c	10310	1.00000E-11	1.50000E+02	1.3	0.0	272.0

\*\*\*\*\*

```

dump no. 1 on file HAC_HP_SC-55G1_252cf_0.r nps = 0 coll = 0 ctm = 0.00
nrn = 0

```

3 warning messages so far.

```

warning. no photon-production mt found in acegam. zaid = 26056.84c
nps = 27141026 nrn = 13 erg = 3.0000E+00

```

\*\*\*\*\*

```

dump no. 2 on file HAC_HP_SC-55G1_252cf_0.r nps = 382297793 coll = 29964768786 ctm = 1440.43
nrn = 534477762467

```

\*\*\*\*\*

```

dump no. 3 on file HAC_HP_SC-55G1_252cf_0.r nps = 764447475 coll = 59915947296 ctm = 2880.55
nrn = 1068710571155
warning. no reaction mt found. collision resampled. zaid = 26056.84c

```



# ATTACHMENT A – Responses to RAI

```

nps = 818273327    nrn = 19 erg = 8.0000E+00

*****

dump no. 4 on file HAC_HP_SC-55G1_252cf_0.r    nps = 1146655242    coll = 89870161452    ctm = 4320.91
nrn = 1602991344587

*****

dump no. 5 on file HAC_HP_SC-55G1_252cf_0.r    nps = 1528907608    coll = 119828474388    ctm = 5761.36
nrn = 2137347427868

*****

dump no. 6 on file HAC_HP_SC-55G1_252cf_0.r    nps = 1911064501    coll = 149779406265    ctm = 7201.38
nrn = 2671570026561

*****

dump no. 7 on file HAC_HP_SC-55G1_252cf_0.r    nps = 2293383107    coll = 179741622542    ctm = 8641.82
nrn = 3205995547567
1problem summary

+ run terminated when it had used 9600 minutes of computer time.
+ 08/30/21 04:00:00

====> 382.14 M histories/hr (based on wall-clock time in mcrun)

```

title HP/SC-55G1 with a Concentrated 252cf Neutron Source - HAC probid = 08/29/21 21:19:57

neutron creation	tracks	weight (per source particle)	energy	neutron loss	tracks	weight (per source particle)	energy
source	2547729148	1.0000E+00	3.1171E+00	escape	856856895	3.3632E-01	4.5571E-01
nucl. interaction	0	0.	0.	energy cutoff	0	0.	0.
particle decay	0	0.	0.	time cutoff	0	0.	0.
weight window	0	0.	0.	weight window	0	0.	0.
cell importance	0	0.	0.	cell importance	0	0.	0.
weight cutoff	0	0.	0.	weight cutoff	0	0.	0.
e or t importance	0	0.	0.	e or t importance	0	0.	0.
dxtran	0	0.	0.	dxtran	0	0.	0.
forced collisions	0	0.	0.	forced collisions	0	0.	0.
exp. transform	0	0.	0.	exp. transform	0	0.	0.
upscattering	0	0.	5.9837E-07	downscattering	0	0.	2.6157E+00
photonuclear	0	0.	0.	capture	1692102746	6.6416E-01	3.9878E-02
(n,xn)	2460986	9.6595E-04	1.2615E-03	loss to (n,xn)	1230493	4.8298E-04	7.0557E-03
prompt fission	0	0.	0.	loss to fission	0	0.	0.
delayed fission	0	0.	0.	nucl. interaction	0	0.	0.
prompt photofis	0	0.	0.	particle decay	0	0.	0.
tabular boundary	0	0.	0.	tabular boundary	0	0.	0.
tabular sampling	0	0.	0.	elastic scatter	0	0.	0.
total	2550190134	1.0010E+00	3.1184E+00	total	2550190134	1.0010E+00	3.1184E+00

photon creation	tracks	weight (per source particle)	energy	photon loss	tracks	weight (per source particle)	energy
source	0	0.	0.	escape	502481113	1.9923E-01	3.1167E-01
nucl. interaction	0	0.	0.	energy cutoff	2423	1.0057E-06	1.7045E-04
particle decay	0	0.	0.	time cutoff	0	0.	0.
weight window	0	0.	0.	weight window	0	0.	0.
cell importance	0	0.	0.	cell importance	0	0.	0.
weight cutoff	0	0.	0.	weight cutoff	0	0.	0.
e or t importance	0	0.	0.	e or t importance	0	0.	0.
dxtran	0	0.	0.	dxtran	0	0.	0.
forced collisions	0	0.	0.	forced collisions	0	0.	0.
exp. transform	0	0.	0.	exp. transform	0	0.	0.
from neutrons	2996399012	1.1853E+00	3.0496E+00	compton scatter	0	0.	2.2413E+00
bremsstrahlung	2083260954	8.2413E-01	8.0519E-02	capture	5852054839	2.3147E+00	1.6789E-01
p-annihilation	445776204	1.7647E-01	9.0177E-02	pair production	222888102	8.8234E-02	5.0185E-01
photonuclear	0	0.	0.	photonuclear abs	0	0.	0.
electron x-rays	0	0.	0.	loss to photofis	0	0.	0.
compton fluores	0	0.	0.				
muon capt fluores	0	0.	0.				
1st fluorescence	1051990307	4.1621E-01	2.6735E-03				

number of neutrons banked	1230493	average time of (shakes)	cutoffs
neutron tracks per source particle	1.0010E+00	escape 1.9583E+03	tco 1.0000E+33
neutron collisions per source particle	6.7287E+01	capture 1.2433E+04	eco 0.0000E+00
total neutron collisions	171429580080	capture or escape 8.9120E+03	wc1 0.0000E+00
net multiplication	1.0005E+00 0.0000	any termination 8.9077E+03	wc2 0.0000E+00

# ATTACHMENT A – Responses to RAI

```

2nd Fluorescence      0  0.  0.
cerenkov               0  0.  0.
(gamma,xgamma)        0  0.  0.
tabular sampling       0  0.  0.
prompt photofis        0  0.  0.
total                  6577426477  2.6022E+00  3.2229E+00

number of photons banked 1230466453
photon tracks per source particle 2.5817E+00
photon collisions per source particle 1.1088E+01
total photon collisions 28248005354

average time of (shakes)
escape 7.5916E+03
capture 7.0153E+03
capture or escape 7.0609E+03
any termination 7.1352E+03

cutoffs
tco 1.0000E+33
eco 1.0000E-03
wc1 0.0000E+00
wc2 0.0000E+00

computer time so far in this run 9600.74 minutes
computer time in mcrun 9600.48 minutes
source particles per minute 2.6538E+05
random numbers generated 3561588808224

maximum number ever in bank 39
bank overflows to backup file 0

most random numbers used was 46183 in history 1047247824

```

warning. random number period exceeded. decrease stride.

range of sampled source weights = 1.0000E+00 to 1.0000E+00

neutron reaction mt loop failed 1 times.

neutron-induced photon production mt loop failed 77 times.

```

number of histories processed by each thread
105684883 106253009 106926525 106711270 106915672 106201649 106592336 106040859 105937688 105041781
106213201 105932338 106574949 105507782 106023518 106273833 106342464 105150249 106378980 105505997
106080128 106176685 106682425 106580927

1neutron activity in each cell

```

print table 126

cell	tracks entering	population	collisions	collisions * weight (per history)	number weighted energy	flux weighted energy	average track weight (relative)	average track mfp (cm)
1	1	0	0	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
2	2	0	0	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
3	3	2892478628	2547789081	2070298499	8.1261E-01	3.5891E-03	2.3966E+00	3.1843E+00
4	4	10312093	7754542	34460241	1.3526E-02	1.2941E-03	4.7948E-01	5.5048E+00
5	5	2759562567	1751672453	10557674701	4.1440E+00	1.2318E-03	1.0873E+00	4.4347E+00
6	6	9673881	6775867	27851291	1.0932E-02	1.0166E-03	4.6496E-01	5.1195E+00
7	7	4108903735	2547555802	157863644903	6.1962E+01	9.4765E-05	5.2825E-01	1.0641E+00
8	8	1259352652	938726237	0	0.0000E+00	3.3600E-03	4.9497E-01	0.0000E+00
9	201	1084563811	932938079	875650445	3.4370E-01	7.9607E-03	1.1656E+00	1.0000E+00
10	202	1280727771	939518659	0	0.0000E+00	5.4867E-03	1.0513E+00	0.0000E+00
11	203	856856895	856856895	0	0.0000E+00	1.3930E-02	1.3191E+00	0.0000E+00
12	204	856856895	856856895	0	0.0000E+00	1.3817E-02	1.3306E+00	0.0000E+00
13	205	857068581	856856895	0	0.0000E+00	1.3554E-02	1.3528E+00	0.0000E+00
14	301	211686	211686	0	0.0000E+00	1.1487E-02	1.4461E+00	0.0000E+00

```

total 15976569195 12243513091 171429580080 6.7287E+01
1photon activity in each cell

```

print table 126

cell	tracks entering	population	collisions	collisions * weight (per history)	number weighted energy	flux weighted energy	average track weight (relative)	average track mfp (cm)
1	1	0	0	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
2	2	0	0	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
3	3	73826392	81626576	11044019	4.3711E-03	1.7056E+00	1.7056E+00	1.7323E+01
4	4	98666001	138179384	390177183	1.5388E-01	1.2432E+00	1.2432E+00	1.8543E+00
5	5	1799073189	4816253646	14324667640	5.6650E+00	1.4703E+00	1.4703E+00	1.9760E+00
6	6	97492944	132230505	367829558	1.4506E-01	1.2476E+00	1.2476E+00	1.8566E+00
7	7	1015866218	2081628616	11854166185	4.6746E+00	9.7812E-01	9.7812E-01	1.2365E+01
8	8	857171040	713994831	0	0.0000E+00	1.3455E+00	1.3455E+00	0.0000E+00
9	201	693582058	915701178	1300120769	5.1607E-01	1.3176E+00	1.3176E+00	1.8736E+00
10	202	856346030	724522558	0	0.0000E+00	1.3132E+00	1.3132E+00	0.0000E+00
11	203	502481113	502481113	0	0.0000E+00	1.5361E+00	1.5361E+00	0.0000E+00
12	204	502481113	502481113	0	0.0000E+00	1.5455E+00	1.5455E+00	0.0000E+00
13	205	502596717	502481113	0	0.0000E+00	1.5599E+00	1.5599E+00	0.0000E+00
14	301	115604	115604	0	0.0000E+00	1.5415E+00	1.5415E+00	0.0000E+00

```

total 6999698419 11111696237 28248005354 1.1159E+01
1summary of photons produced in neutron collisions in the tabular range

```

production by cell of photons created with energies above local photon energy cutoffs

cell	number of photons	weight per source neut	energy per source neut	avg photon energy	mev/gm per source neut	weight/neut collision	energy/neut collision
------	-------------------	------------------------	------------------------	-------------------	------------------------	-----------------------	-----------------------

## ATTACHMENT A – Responses to RAI

1	1	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
2	2	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
3	3	10249586	4.02303E-03	1.32627E-02	3.29670E+00	1.09626E-03	4.95078E-03	1.63212E-02
4	4	2549095	1.01595E-03	3.30675E-03	3.25483E+00	1.84454E-08	7.51117E-02	2.44476E-01
5	5	1669971958	6.63331E-01	1.87449E+00	2.82588E+00	2.36457E-06	1.60072E-01	4.52344E-01
6	6	2174188	8.66683E-04	2.97011E-03	3.42699E+00	1.84647E-08	7.92808E-02	2.71695E-01
7	7	1202629388	4.72040E-01	1.07553E+00	2.27848E+00	1.07553E+00	7.61815E-03	1.73578E-02
8	8	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
9	201	108822376	4.40716E-02	8.00051E-02	1.81534E+00	5.47848E-08	1.28228E-01	2.32777E-01
10	202	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
11	203	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
12	204	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
13	205	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
14	301	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
15	999	0	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
total			2996396591	1.18535E+00	3.04957E+00	2.57272E+00		

energy distribution of photons produced in neutron collisions in the tabular range

all sampled photons from neutron collisions in the tabular range, without regard to energy cutoffs

energy interval	number of photons	number frequency	cum number distribution	weight of photons	weight frequency	cum weight distribution
20.000	357	1.19143E-07	1.19143E-07	1.59520E-07	1.34576E-07	1.34576E-07
15.000	1624	5.41984E-07	6.61127E-07	7.19030E-07	6.06597E-07	7.41173E-07
10.000	277607	9.26469E-05	9.33080E-05	1.29735E-04	1.09449E-04	1.10190E-04
9.000	17112203	5.71092E-03	5.80423E-03	6.76596E-03	5.70799E-03	5.81818E-03
8.000	6323805	2.11047E-03	7.91470E-03	2.66228E-03	2.24599E-03	8.06417E-03
7.000	270492318	9.02725E-02	9.81872E-02	1.06504E-01	8.98507E-02	9.79149E-02
6.000	60349003	2.01405E-02	1.18328E-01	2.40669E-02	2.03036E-02	1.18219E-01
5.000	60387929	2.01535E-02	1.38481E-01	2.42338E-02	2.04444E-02	1.38663E-01
4.000	104025112	3.47167E-02	1.73198E-01	4.13885E-02	3.49167E-02	1.73580E-01
3.000	93888618	3.13338E-02	2.04532E-01	3.75812E-02	3.17047E-02	2.05284E-01
2.000	1308211051	4.36594E-01	6.41126E-01	5.14507E-01	4.34055E-01	6.39339E-01
1.000	285582967	9.53087E-02	7.36435E-01	1.13758E-01	9.59700E-02	7.35309E-01
0.500	648266578	2.16349E-01	9.52783E-01	2.56721E-01	2.16578E-01	9.51888E-01
0.100	101870789	3.39977E-02	9.86781E-01	4.06220E-02	3.42700E-02	9.86158E-01
0.010	36390621	1.21448E-02	9.98926E-01	1.50260E-02	1.26765E-02	9.98834E-01
0.000	3218430	1.07410E-03	1.00000E+00	1.38203E-03	1.16593E-03	1.00000E+00
<----- energy interval containing the global photon energy cutoff, 1.000E-03 Mev						
total		2996399012	1.00000E+00	1.18535E+00	1.00000E+00	

warning. 2421 photons from neutron collisions were created below a local photon energy cutoff and were not followed.

1tally 4 nps = 2547729148  
+ 1-M from Package Surface Neutron Dose Rate (mrem/hr) @ Z = 111.12500  
tally type 4 track length estimate of particle flux.  
particle(s): neutrons  
this tally is modified by dose function DE4 and DF4.  
volumes  
cell: 301  
2.02683E+00  
cell 301  
3.82781E-07 0.0025

results of 10 statistical checks for the estimated answer for the tally fluctuation chart (tfc) bin of tally 4

tfc bin behavior	--mean-- behavior	-----relative error----- value	decrease	decrease rate	----variance of the variance---- value	decrease	decrease rate	--figure of merit-- value	behavior	-pdf-slope
desired	random	<0.10	yes	1/sqrt(nps)	<0.10	yes	1/nps	constant	random	>3.00
observed	random	0.00	yes	yes	0.00	yes	yes	constant	random	6.74
passed?	yes	yes	yes	yes	yes	yes	yes	yes	yes	yes

this tally meets the statistical criteria used to form confidence intervals: check the tally fluctuation chart to verify.  
the results in other bins associated with this tally may not meet these statistical criteria.

----- estimated confidence intervals: -----

estimated asymmetric confidence interval(1,2,3 sigma): 3.8182E-07 to 3.8374E-07; 3.8087E-07 to 3.8470E-07; 3.7991E-07 to 3.8566E-07

## ATTACHMENT A – Responses to RAI

estimated symmetric confidence interval(1,2,3 sigma): 3.8182E-07 to 3.8374E-07; 3.8086E-07 to 3.8470E-07; 3.7991E-07 to 3.8566E-07

1analysis of the results in the tally fluctuation chart bin (tfc) for tally 4 with nps = 2547729148 print table 160

normed average tally per history = 3.82781E-07	unnormed average tally per history = 7.75832E-07
estimated tally relative error = 0.0025	estimated variance of the variance = 0.0000
relative error from zero tallies = 0.0022	relative error from nonzero scores = 0.0012
number of nonzero history tallies = 211686	efficiency for the nonzero tallies = 0.0001
history number of largest tally = 248095536	largest unnormalized history tally = 2.21871E-02
(largest tally)/(average tally) = 2.85978E+04	(largest tally)/(avg nonzero tally) = 2.37614E+00
(confidence interval shift)/mean = 0.0000	shifted confidence interval center = 3.82782E-07

if the largest history score sampled so far were to occur on the next history, the tfc bin quantities would change as follows:

estimated quantities	value at nps	value at nps+1	value(nps+1)/value(nps)-1.
mean	3.82781E-07	3.82785E-07	0.000011
relative error	2.50359E-03	2.50359E-03	-0.000001
variance of the variance	7.22367E-06	7.22378E-06	0.000016
shifted center	3.82782E-07	3.82782E-07	0.000000
figure of merit	1.66181E+01	1.66181E+01	0.000002

the estimated inverse power slope of the 127 largest tallies starting at 2.18128E-02 is 6.7401  
the empirical history score probability density function appears to be increasing at the largest history scores:  
please examine. see print table 161.  
the large score tail of the empirical history score probability density function appears to have no unsampled regions.

fom = (histories/minute)\*(f(x) signal-to-noise ratio)\*\*2 = (2.654E+05)\*( 7.913E-03)\*\*2 = (2.654E+05)\*(6.262E-05) = 1.662E+01

1tally 14 nps = 2547729148  
+ 1-M from Package Surface Gamma Dose Rate (mrem/hr) @ Z = 111.12500  
tally type 4 track length estimate of particle flux.  
particle(s): photons  
this tally is modified by dose function DE14 and DF14.  
volumes  
cell: 301  
2.02683E+00  
cell 301  
5.28270E-09 0.0039

results of 10 statistical checks for the estimated answer for the tally fluctuation chart (tfc) bin of tally 14										
tfc bin behavior	--mean-- behavior	-----relative error-----			----variance of the variance----			--figure of merit--		-pdf-slope
		value	decrease	decrease rate	value	decrease	decrease rate	value	behavior	
desired	random	<0.10	yes	1/sqrt(nps)	<0.10	yes	1/nps	constant	random	>3.00
observed	random	0.00	yes	yes	0.00	yes	yes	constant	random	8.48
passed?	yes	yes	yes	yes	yes	yes	yes	yes	yes	yes

this tally meets the statistical criteria used to form confidence intervals: check the tally fluctuation chart to verify.  
the results in other bins associated with this tally may not meet these statistical criteria.

----- estimated confidence intervals: -----

estimated asymmetric confidence interval(1,2,3 sigma): 5.2621E-09 to 5.3034E-09; 5.2415E-09 to 5.3240E-09; 5.2209E-09 to 5.3446E-09  
estimated symmetric confidence interval(1,2,3 sigma): 5.2621E-09 to 5.3033E-09; 5.2415E-09 to 5.3239E-09; 5.2208E-09 to 5.3446E-09

1analysis of the results in the tally fluctuation chart bin (tfc) for tally 14 with nps = 2547729148 print table 160

normed average tally per history = 5.28270E-09	unnormed average tally per history = 1.07071E-08
estimated tally relative error = 0.0039	estimated variance of the variance = 0.0000
relative error from zero tallies = 0.0029	relative error from nonzero scores = 0.0026
number of nonzero history tallies = 115276	efficiency for the nonzero tallies = 0.0000
history number of largest tally = 2525101600	largest unnormalized history tally = 2.13481E-03
(largest tally)/(average tally) = 1.99382E+05	(largest tally)/(avg nonzero tally) = 9.02134E+00
(confidence interval shift)/mean = 0.0000	shifted confidence interval center = 5.28276E-09

## ATTACHMENT A – Responses to RAI

if the largest history score sampled so far were to occur on the next history, the tfc bin quantities would change as follows:

estimated quantities	value at nps	value at nps+1	value(nps+1)/value(nps)-1.
mean	5.28270E-09	5.28311E-09	0.000078
relative error	3.90370E-03	3.90417E-03	0.000123
variance of the variance	3.62324E-05	3.63647E-05	0.003651
shifted center	5.28276E-09	5.28276E-09	0.000000
figure of merit	6.83526E+00	6.83558E+00	-0.000245

the estimated inverse power slope of the 198 largest tallies starting at 9.60280E-04 is 8.4811  
the empirical history score probability density function appears to be increasing at the largest history scores:  
please examine. see print table 161.  
the large score tail of the empirical history score probability density function appears to have no unsampled regions.

fom = (histories/minute)\*(f(x) signal-to-noise ratio)\*\*2 = (2.654E+05)\*( 5.075E-03)\*\*2 = (2.654E+05)\*(2.576E-05) = 6.835E+00

1status of the statistical checks used to form confidence intervals for the mean for each tally bin

tally result of statistical checks for the tfc bin (the first check not passed is listed) and error magnitude check for all bins

- 4 passed the 10 statistical checks for the tally fluctuation chart bin result  
passed all bin error check: 1 tally bins all have relative errors less than 0.10 with no zero bins
- 14 passed the 10 statistical checks for the tally fluctuation chart bin result  
passed all bin error check: 1 tally bins all have relative errors less than 0.10 with no zero bins

the 10 statistical checks are only for the tally fluctuation chart bin and do not apply to other tally bins.

1tally fluctuation charts

nps	mean	tally error	4 vov	slope	fom	mean	tally error	14 vov	slope	fom
131072000	3.7835E-07	0.0111	0.0001	2.0	16	5.1443E-09	0.0173	0.0007	2.5	6.8E+00
262144000	3.8218E-07	0.0078	0.0001	1.9	17	5.1508E-09	0.0122	0.0004	1.9	6.7E+00
393216000	3.8374E-07	0.0064	0.0000	1.6	17	5.1783E-09	0.0100	0.0002	2.8	6.8E+00
524288000	3.8405E-07	0.0055	0.0000	1.5	17	5.1808E-09	0.0086	0.0002	10.0	6.8E+00
655360000	3.8391E-07	0.0049	0.0000	1.5	17	5.2055E-09	0.0077	0.0001	10.0	6.8E+00
786432000	3.8315E-07	0.0045	0.0000	10.0	17	5.2240E-09	0.0070	0.0001	4.2	6.8E+00
917504000	3.8289E-07	0.0042	0.0000	10.0	17	5.2149E-09	0.0065	0.0001	2.7	6.8E+00
1048576000	3.8257E-07	0.0039	0.0000	10.0	17	5.2217E-09	0.0061	0.0001	2.1	6.8E+00
1179648000	3.8264E-07	0.0037	0.0000	10.0	17	5.2255E-09	0.0058	0.0001	2.0	6.8E+00
1310720000	3.8332E-07	0.0035	0.0000	10.0	17	5.2345E-09	0.0055	0.0001	2.0	6.8E+00
1441792000	3.8323E-07	0.0033	0.0000	10.0	17	5.2427E-09	0.0052	0.0001	1.9	6.8E+00
1572864000	3.8283E-07	0.0032	0.0000	10.0	17	5.2610E-09	0.0050	0.0001	2.1	6.8E+00
1703936000	3.8259E-07	0.0031	0.0000	10.0	17	5.2740E-09	0.0048	0.0001	2.2	6.8E+00
1835008000	3.8281E-07	0.0029	0.0000	10.0	17	5.2751E-09	0.0046	0.0000	2.5	6.8E+00
1966080000	3.8269E-07	0.0028	0.0000	10.0	17	5.2753E-09	0.0044	0.0000	3.0	6.8E+00
2097152000	3.8291E-07	0.0028	0.0000	10.0	17	5.2757E-09	0.0043	0.0000	3.6	6.8E+00
2228224000	3.8256E-07	0.0027	0.0000	10.0	17	5.2735E-09	0.0042	0.0000	4.7	6.8E+00
2359296000	3.8277E-07	0.0026	0.0000	7.2	17	5.2841E-09	0.0041	0.0000	6.9	6.8E+00
2490368000	3.8280E-07	0.0025	0.0000	7.0	17	5.2835E-09	0.0039	0.0000	10.0	6.8E+00
2547729148	3.8278E-07	0.0025	0.0000	6.7	17	5.2827E-09	0.0039	0.0000	8.5	6.8E+00

\*\*\*\*\*

dump no. 8 on file HAC\_HP\_SC-55G1\_252Cf\_0.r nps = 2547729148 coll = 199677585434 ctm = 9600.48  
nrn = 356158808224  
tally data written to file HAC\_HP\_SC-55G1\_252Cf\_0.m

7 warning messages so far.

run terminated when it had used 9600 minutes of computer time.

computer time = 9600.75 minutes

mcnp version 6 02/20/18 08/30/21 04:00:00 probid = 08/29/21 21:19:57

## **ATTACHMENT B – Summary of Revisions**

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<b><u>Summary</u></b>	<b><u>Pg.</u></b>
TRUPACT-II SAR, Revision 25	B-2
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CH-TRAMPAC, Revision 6	B-4
CH-TRU Payload Appendices, Revision 5	B-5
HPT-REP-0001, Revision 1	B-6
SCA-CAL-0005, Revision 0	B-8

## ATTACHMENT B – Summary of Revisions

TRUPACT-II SAR, Revision 25, October 2021			
Section	Page	Change Description	Justification
General		Revised header for date.	Administrative change. No impact to safety basis.
5.3.1	5.3-1	Deleted the following text: “Any significant deviation from the NCT configuration assumption is precluded through the use of preshipment radiological surveys of the package to validate that the source(s) are reasonably distributed within the package. However, it should be noted that even without the preshipment measurement confirmation, HAC dose rate requirements are ensured by these conservative analysis assumptions.”	As described in the response to RAI-Sh-10, the sentences have been removed to avoid confusion and/or conflicting interpretation.
5.3.1.7	5.3-4	Revised Reference 4 from Rev. 0 to Rev. 1.	In response to RAI-St-1, HPT-REP-0001, <i>Regulatory Hypothetical Accident Condition Type B Testing for the HalfPACT Shielded Container Payloads</i> , was revised to add the DOT-7A Type A 4-foot drop test results for the SC-55G1.
5.4.5	5.4-13	Added new Section 5.4.5, <i>Evaluation for Axial Gaps in the Sidewall Lead</i>	In response to RAI-Sh-8, a new Section 5.4.5 was added to summarize the results of SCA-CAL-0005, <i>Effect of Axial Gaps in the SC-30G2, SC-30G3, and SC-55G2 Lead Sidewalls</i> .
5.5.8	5.5-39	Corrected the DCF equation for the SC-55G1 from “ $DCF_{SC-55G1} = 0.0051 \cdot p^3 - 0.0987 \cdot p^2 + 0.8030 \cdot p + 0.2342$ ” to “ $DCF_{SC-55G1} = 0.0024 \cdot p^3 - 0.0668 \cdot p^2 + 0.7557 \cdot p + 0.2630$ ”	In response to RAI-Sh-3, the DCF equation for the SC-55G1 has been corrected in Section 5.5.8 of the TRUPACT-II SAR.

## ATTACHMENT B – Summary of Revisions

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HalfPACT SAR, Revision 8, October 2021			
Section	Page	Change Description	Justification
General		Revised header for date.	Administrative change. No impact to safety basis.



## ATTACHMENT B – Summary of Revisions

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CH-TRAMPAC, Revision 6, October 2021			
Section	Page	Change Description	Justification
General		Revised header for date.	Administrative change. No impact to safety basis.

## ATTACHMENT B – Summary of Revisions

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CH-TRU Payload Appendices, Revision 5, October 2021			
Section	Page	Change Description	Justification
General		Revised header for date.	Administrative change. No impact to safety basis.
4.7	4.7-5	Revised the reference to HPT-REP-0001 from Rev. 0 to Rev. 1.	Administrative change. No impact to safety basis.
4.8	4.8-5	Revised the reference to HPT-REP-0001 from Rev. 0 to Rev. 1.	Administrative change. No impact to safety basis.
4.9	4.9-5	Revised the reference to HPT-REP-0001 from Rev. 0 to Rev. 1.	Administrative change. No impact to safety basis.
4.10	4.10-5	Revised the reference to HPT-REP-0001 from Rev. 0 to Rev. 1.	Administrative change. No impact to safety basis.

## ATTACHMENT B – Summary of Revisions

HPT-REP-0001, Revision 1, October 2021			
Section	Page	Change Description	Justification
General	Various	Revised text to consistently use “HAC Type B” and “DOT-7A Type” terms to differentiate tests.	Administrative change.
1.2	1	Added text to clarify testing performed previously for the SC-30G1.	In response to RAI-St-1; text added to clarify that Type A 4-foot drop tests are to support certification of shielded containers as DOT-7A Type A packaging in accordance with 49 CFR §178.350 requirements. Added text to help distinguish the difference between drop tests.
1.2	2	Inserted a table and text providing a summary of all Type A and Type B drop testing.	In response to RAI-St-1, the revisions summarize the drop tests that were performed for each shielded container.
2.0	3	Added Reference 11 for new SCA-CAL-0005, <i>Effect of Axial Gaps in the SC-30G2, SC-30G3, and SC-55G2 Lead Sidewalls</i> , Rev. 0.	In response to RAI-Sh-08, SCA-CAL-0005, <i>Effect of Axial Gaps in the SC-30G2, SC-30G3, and SC-55G2 Lead Sidewalls</i> was developed and is now referenced in HPT-REP-0001, Rev. 1.
6.1	31	Added new Section 6.1.1, <i>SC-55G1 Shielded Container HAC Type B Tests</i> (heading only).	This section heading was added to clarify that Section 6.1.1 is specific to the HAC Type B 30-foot drop tests.
6.1.2	45	Added new Section 6.1.2, <i>SC-55G1 Shielded Container DOT-7A Type A Tests</i> (heading only).	This section heading was added to clarify that Section 6.1.2 is specific to the DOT-7A Type A tests.
6.1.2.1	45 – 47	Added new Section 6.1.2.1, <i>SC-55G1 Free Drop Tests</i> .	In response to RAI-St-1(b), Section 6.1.2.1 was added to discuss the DOT-7A Type A 4-foot drop tests that were conducted on the SC-55G1.
6.2	48	Added new Section 6.2.1, <i>SC-30G3 Shielded Container HAC Type B Tests</i> (heading only).	This section heading was added to clarify that Section 6.2.1 is specific to the HAC Type B 30-foot drop tests.
6.2.1.2.1	48	Added reference to Figure 6-30.	Administrative change. No impact to safety basis.
6.2.1.2.2	49	Changed to reference Figure 6-33.	Administrative change. No impact to safety basis.
6.2.1.2.3	49	Changed to reference Figure 6-30.	Administrative change. No impact to safety basis.

## ATTACHMENT B – Summary of Revisions

HPT-REP-0001, Revision 1, October 2021			
Section	Page	Change Description	Justification
6.2.1.2.3	51	Moved Figure 6.30 – Pre-End Drop Relative Position of the SC-30G3 Lateral Dunnage.	Administrative change. No impact to safety basis.
6.2.1.2.3	53	Corrected figure title of Figure 6.33 – SC-30G3 Side Drop Radial Flattening of the ICV Shell.	Administrative change. No impact to safety basis.
6.2.1.3, 7.1.2.2, 7.1.3.2,	60, 87, 101	Revised text to reference the new shielding evaluation as Reference 11.	In response to RAI-Sh-08, SCA-CAL-0005, <i>Effect of Axial Gaps in the SC-30G2, SC-30G3, and SC-55G2 Lead Sidewalls</i> , was developed.
6.2.2	68 – 79	Added new Section 6.2.2, <i>SC-30G3 Shielded Container DOT-7A Type A Tests</i> .	In response to RAI-St-01(b), Section 6.2.2 was added to discuss the DOT-7A Type A 4-foot drop tests that were conducted on the SC-30G3.
7.1.1	80 – 83	Revised Section 7.1.1, <i>Type B HAC Test versus DOT-7A Type A Test Comparison</i> , and added new Section 7.1.1.1, <i>SC-30G3 Visible Damage Comparison</i> . Also revised heading for Section 7.1.1.2, <i>SC-30G3 Impact Acceleration Comparison</i> .	In response to RAI-St-01(b), revised Section 7.1.1 and added Section 7.1.1.1 to clarify the basis for comparison of visible damage between DOT-7A Type A (bare) 4-foot drops versus the HAC Type B (protected) 30-foot drops.

## ATTACHMENT B – Summary of Revisions

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SCA-CAL-0005, Revision 0, October 2021			
Section	Page	Change Description	Justification
All	All	New document provided as part of RAI Response: SCA-CAL-0005, <i>Effect of Axial Gaps in the SC-30G2, SC-30G3, and SC-55G2 Lead Sidewalls</i> , Rev. 0.	In response to RAI-Sh-08, SCA-CAL-0005, <i>Effect of Axial Gaps in the SC-30G2, SC-30G3, and SC-55G2 Lead Sidewalls</i> was developed.