QUAD-CITIES NUCLEAR POWER STATION

UNITS 1 AND 2

MONTHLY PERFORMANCE REPORT

DECEMBER, 1987

COMMONWEALTH EDISON COMPANY

AND

IOWA-ILLINOIS GAS & ELECTRIC COMPANY

NRC DOCKET NOS. 50-254 AND 50-265

LICENSE NOS. DPR-29 AND DPR-30

0027H/0061Z

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I. INTRODUCTION

Quad-Cities Nuclear Power Station is composed of two Boiling Water Reactors, each with a Maximum Dependable Capacity of 769 MWe Net, located in Cordova, Illinois. The Station is jointly owned by Commonwealth Edison Company and Iowa-Illinois Gas & Electric Company. The Nuclear Steam Supply Systems are General Electric Company Boiling Water Reactors. The Architect/Engineer was Sargent & Lundy, Incorporated, and the primary construction contractor was United Engineers & Constructors. The Mississippi River is the condenser cooling water source. The plant is subject to license numbers DPR-29 and DPR-30, issued October 1, 1971, and March 21, 1972, respectively, pursuant to Docket Numbers 50-254 and 50-265. The date of initial Reactor criticalities for Units One and Two, respectively were October 18, 1971, and April 26, 1972. Commercial generation of power began on February 18, 1973 for Unit One and March 10, 1973 for Unit Two.

This report was compiled by Verna Koselka and Lynne Deelsnyder, telephone number 309-654-2241, extensions 2240 and 2185.

II. SUMMARY OF OPERATING EXPERIENCE

A. Unit One

December 1-15

Unit One began the month still in a refueling outage. From December 1-4 normal outage testing and surveillances were performed. On December 5 at 0245 the Integrated Leak Rate Test began. The test was completed at 0830 on December 6. On December 7 at 1315 control rod scram timing was resumed and continued until 0138 on the following day, December 8. Normal outage testing and surveillances continued through December 11 when, at 1149, control rod timing was resumed until the main turbine was placed on the turning gear.

December 16-31

From December 16-18 the month continued with more outage testing. On December 18 at 0737 the 1A and 1B circulating water pumps were turned on. At 1700 the main turbine was taken off the turning gear. On December 19 at 0545 the B Core Spray header was filled and normal outage work continued until December 22 when, at 1230, the main generator was filled with hydrogen to begin Startup. At 1617 the main turbine was placed on the turning gear. At 1640 the mode switch was placed in refuel, then to startup at 1735. At 1806, withdrawal of control rods was begun and at 2200 the Unit 1 Reactor achieved criticallity. The head vents were closed at 2228. On December 23, power was held constant while other control rod drives were vented. At 0440 the 1B Reactor Feed Pump was turned on and at 0805 the mode switch was placed in RUN. At 0855 Average Power Range Monitor (APRM) gains were set to 13%. The generator was synchronized to the grid at 1725, but at 1750 the main turbine was tripped due to high vibrations. The main turbine was placed back on the turning gear. The turbine began rolling at 0040 on December 24 and the unit went on line at 0120 at 10 MWe initial load and increasing approximately 3 MWe/min. At 0145 the unit reached 90 MWe; load was reduced at 0225 as per Shift Engineer due to high vibrations on the turbine, and the unit came off line at 0232. The turbine was tripped at 0355. At 0440 the main turbine was placed back on the turning gear and at 0750 the turbine began to roll. The main generator was synchronized to the grid at 1310. At 1330 control rods were withdrawn to increase power to 180 MWe. Load was held at 156 MWe to adjust APRM gains. On December 26 at 1010 hot scram timing began and was completed at 0625 on December 27. At 1105 the Turbine Overspeed Trip Test was performed, but after reaching 1400 RPM's, the turbine began decelerating and subsequently was tripped. The turbine was reset at 1510 and placed in the turning gear. At 1805 turbine was brought up to 1370 rpm and control valves closed, turbine was manually tripped. Turbine problem investigation and repair work continued until December 29 at 1703 when the turbine was synchronized to the generator. Turbine ran until 2040 when it was tripped for overspeed test. Then at 2210 the turbine was synchronized to the generator and load increase was begun using control rod withdrawal and recirc system. Startup testing was performed through December 31.

B. Unit Two

December 1-15

Unit Two began the month of December on EGC and operated in EGC with minor interruptions for normal testing until December 10 when at 0117 the reactor scrammed on a turbine/generator load mismatch. At 0252 the main turbine was placed on the turning gear and at 0345 the mode switch was placed in startup and rod moves were begun to increase power. The reactor achieved criticallity at 1141, control rod moves continued and the mode switch was placed in run at 2220. On December 11 at 0031 the main generator was synchronized to the grid. The initial load was 120 MWe and a power ascent was begun with control rods and recirc pumps. Full power was reached on December 12 at 1110 (818 MWe), but was decreased at 1118 with recirc pumps to 800 MWe because of high MFLD readings. At 1359 control rods were inserted because of high LPRM readings. Power was held constant.

December 16-31

Normal plant operations continued through the remainder of the month with small power reductions and increases as per requested through the load dispatcher. The unit operated in EGC for 353.4 hours for the month of December. Normal surveillance testing was performed during the month.

III. PLANT OR PROCEDURE CHANGES, TESTS, EXPERIMENTS, AND SAFETY RELATED MAINTENANCE

A. Amendments to Facility License or Technical Specifications

Technical Specification Amendment No. 103 was issued on December 17 to facility operating license DPR 29.

This Tech Spec amendment included revisions to plant operating limits, operating domains and surveillance requirements to reflect the new fuel type being utilized for this cycle.

B. Facility or Procedure Changes Requiring NRC Approval

There were no Facility or Procedure changes requiring NRC approval for the reporting period.

C. Tests and Experiments Requiring NRC Approval

There were no Tests or Experiments requiring NRC approval for the reporting period.

D. Corrective Maintenance of Safety Related Equipment

The following represents a tabular summary of the major safety related maintenance performed on Units One and Two during the reporting period. This summary includes the following: Work Request Numbers, Licensee Event Report Numbers, Components, Cause of Malfunctions, Results and Effects on Safe Operation, and Action Taken to Prevent Repetition.

UNIT 1 MAINTENANCE SUMMARY

WORK REQUEST NO.: Q53539

LER NUMBER: N/A

COMPONENT: System 1000 - Journal bearing for 1A RHR S.W. (1-1001-65A) sent to G.E. for repairs.

CAUSE OF MALFUNCTION: The cause for the failed motor bearing on the 1A Residual Heat Removal Service Water (RHRSW) pump (1-1001-65A) was determined to be the result of loose journal bolts. The bolts loosened with vibration allowing bearing oil to leak out, eventually causing its failure.

RESULTS & EFFECTS ON SAFE OPERATION: There were no results or effects on safe operation as all other active components required by Technical Specification 3.5.B.2 were proven operable.

ACTION TAKEN TO PREVENT REPETITION: The journal bearing was removed and sent to General Electric for repair. It was einstalled and operability and vibrational testing were found acceptable. As this :s an isolated incident, no further corrective action is necessary.

WORK REQUEST NO.: Q57667

LER NUMBER: N/A

COMPONENT: System 9400 - Resoldered corroded wire on Control Room Vent CL Monitor, 1/2-9400-103.

CAUSE OF MALFUNCTION: The cause of the malfunction of the chlorine monitor portion of the control room toxic gas analyzer (1/2-9400-103) was a corroded solder joint.

RESULTS & EFFECTS ON SAFE OPERATION: As the control room ventilation was manually placed in the 100 percent recirculation mode as soon as the analyzers were noted to be functioning improperly, preventing any potential intake of toxic gases from outside, safety consequences were minimal.

ACTION TAKEN TO PREVENT REPETITION: The immediate corrective action was to disassemble the chlorine monitor cell and resolder the failed connection. The cell was refilled with electrolyte solution and tested successfully. The control room ventilation was then returned to its normal circulation mode.

UNIT 2 MAINTENANCE SUMMARY

WORK REQUEST NO.: Q57585

LER NUMBER: N/A

COMPONENT: System 1000 - No problems found with valve 2-1001-16B.

CAUSE OF MALFUNCTION: Failure of the 2-1001-16B to reopen after being closed for its Monthly Operability Surveillance is unknown.

RESULTS & EFFECTS ON SAFE OPERATION: There were no results or effects on safe operation as all other safety systems required by Technical Specification 3.5.B.3 were operable.

ACTION TAKEN TO PREVENT REPETITION: During investigation of valve 2-1001-16B by the Electrical Maintenance Department it worked flawlessly. After two more subsequent attempts, six altogether, no further problems were observed. As this is an isolated incident no further corrective action is deemed necessary at this time.

IV. LICENSEE EVENT REPORTS

The following is a tabular summary of all licensee event reports for Quad-Cities Units One and Two occurring during the reporting period, pursuant to the reportable occurrence reporting requirements as set forth in sections 6.6.B.1. and 6.6.B.2. of the Technical Specifications.

UNIT 1

Licensee Event Report Number	Date	Title of Occurrence
87-027	12-1-87	Control Room Vent Isolation (ESF) False Signal - Control Room HVAC Isolation While OJT
87-028	12-2-87	Missing, Damaged Fire Seals - Open Penetration in U2 Cable Tunnel
87-029	12-7-87	B13-1 2nd Level UV Timer Out of Tolerance
87-030	12-19-87	U-1 ATWS Hangers Do Not Meet Design Specifications
87-031	12-23-87	2301-14 Failure (would not open with 3 valve open)
87-032	12-23-87	RCIC Inoperable (failed to inspect during test)
87-033	12-26-87	Inadvertent Rod Scram - During Hot Scram Timing

UNIT 2

87-020	12-10-87	Reactor Scram - T/G Load Mismatch
87-021	12-30-87	SBCS Valve Breaker Failed

V. DATA TABULATIONS

The following data tabulations are presented in this report:

A. Operating Data Report

B. Average Daily Unit Power Level

C. Unit Shutdowns and Power Reductions

APPENDIX C

OPERATING DATA REPORT

DOCKET NO. 50-254

UNIT ONE

DATE JANUARY 8, 1988

COMPLETED BY LYNNE DEELSNYDER

TELEPHONE (309)-654-2241

OPERATING STATUS 0000 120187

1. REPORTING PERIOD: 2400 123187 GROSS HOURS IN REPORTING PERIOD: 744
2. CURRENTLY AUTHORIZED POWER LEVEL (MWt): 2511 MAX. DEPEND. CAPACITY (MWe-Net): 769
   DESIGN ELECTRICAL RATING (MWe-Net): 789
3. POWER LEVEL TO WHICH RESTRICTED (IF ANY) (MWe-Net): N/A
4. REASONS FOR RESTRICTION (IF ANY):

	THIS MONTH	YR TO DATE	CUMULATIVE
5. NUMBER OF HOURS REACTOR WAS CRITICAL	218.0	6251.6	109064.3
6. REACTOR RESERVE SHUTDOWN HOURS	0.0	0.0	3421.9
7. HOURS GENERATOR ON LINE	125.0	6141.7	105458.2
8. UNIT RESERVE SHUTDOWN HOURS	0.0	0.0	909.2
9. GROSS THERMAL ENERGY GENERATED (MWH)	69025	14241357	223299175
10. GROSS ELECTRICAL ENERGY GENERATED (MWH)	30467	4670118	72423502
11. NET ELECTRICAL ENERGY GENERATED (MWH)	25806	4456087	67903289
12. REACTOR SERVICE FACTOR	29.3	71.4	79.6
13. REACTOR AVAILABILITY FACTOR	29.3	71.4	82.1
14. UNIT SERVICE FACTOR	16.8	70.1	76.9
15. UNIT AVAILABILITY FACTOR	16.8	70.1	77.6
16. UNIT CAPACITY FACTOR (Using MDC)	4.5	66.1	64.4
17. UNIT CAPACITY FACTOR (Using Design MWe)	4.4	64.5	62.8
18. UNIT FORCED OUTAGE RATE	12.7	0.6	5.4

19. SHUTDOWNS SCHEDULED OVER NEXT 6 MONTHS (TYPE, DATE, AND DURATION OF EACH):

20. IF SHUT DOWN AT END OF REPORT PERIOD, ESTIMATED DATE OF STARTUP: _____

21. UNITS IN TEST STATUS (PRIOR TO COMMERCIAL OPERATION):

	FORECAST	ACHIEVED
INITIAL CRITICALITY		
INITIAL ELECTRICITY		
COMMERCIAL OPERATION		

APPENDIX C

OPERATING DATA REPORT

DOCKET NO. 50-265

UNIT TWO

DATE JANUARY 8, 1988

COMPLETED BY LYNNE DEELSNYDER

TELEPHONE (309)-654-2241

OPERATING STATUS 0000 120187

1. REPORTING PERIOD: 2400 123187 GROSS HOURS IN REPORTING PERIOD: 744
2. CURRENTLY AUTHORIZED POWER LEVEL (MWt): 2511 MAX. DEPEND. CAPACITY (MWe-Net): 769
   DESIGN ELECTRICAL RATING (MWe-Net): 789
3. POWER LEVEL TO WHICH RESTRICTED (IF ANY) (MWe-Net): N/A
4. REASONS FOR RESTRICTION (IF ANY):

	THIS MONTH	YR TO DATE	CUMULATIVE
5. NUMBER OF HOURS REACTOR WAS CRITICAL	733.6	6941.4	104657.1
6. REACTOR RESERVE SHUTDOWN HOURS	0.0	0.0	2985.8
7. HOURS GENERATOR ON LINE	720.8	6836.2	101535.3
8. UNIT RESERVE SHUTDOWN HOURS	0.0	0.0	702.9
9. GROSS THERMAL ENERGY GENERATED (MWH)	1703136	16030868	217370567
10. GROSS ELECTRICAL ENERGY GENERATED (MWH)	553721	5198492	69557784
11. NET ELECTRICAL ENERGY GENERATED (MWH)	528551	4962988	65560025
12. REACTOR SERVICE FACTOR	98.6	79.2	76.8
13. REACTOR AVAILABILITY FACTOR	98.6	79.2	79.0
14. UNIT SERVICE FACTOR	96.9	78.0	74.5
15. UNIT AVAILABILITY FACTOR	96.9	78.0	75.0
16. UNIT CAPACITY FACTOR (Using MDC)	92.4	73.4	62.6
17. UNIT CAPACITY FACTOR (Using Design MWe)	90.1	71.8	61.0
18. UNIT FORCED OUTAGE RATE	3.1	17.4	8.4

19. SHUTDOWNS SCHEDULED OVER NEXT 6 MONTHS (TYPE, DATE, AND DURATION OF EACH):

20. IF SHUT DOWN AT END OF REPORT PERIOD, ESTIMATED DATE OF STARTUP: _____

21. UNITS IN TEST STATUS (PRIOR TO COMMERCIAL OPERATION):

	FORECAST	ACHIEVED
INITIAL CRITICALITY		
INITIAL ELECTRICITY		
COMMERCIAL OPERATION		

APPENDIX B
AVERAGE DAILY UNIT POWER LEVEL

DOCKET NO. 50-254
UNIT ONE
DATE JANUARY 13, 1988
COMPLETED BY L. DEELSNYDER
TELEPHONE 309-654-2241

MONTH DECEMBER 1987

DAY	AVERAGE DAILY POWER LEVEL (MWe-Net)	DAY	AVERAGE DAILY POWER LEVEL (MWe-Net)
1	-6	17	-5
2	-2	18	-8
3	-11	19	-9
4	-6	20	-9
5	-5	21	-9
6	-6	22	-9
7	-6	23	-14
8	-6	24	53
9	-6	25	133
10	-6	26	147
11	-4	27	53
12	-9	28	-16
13	-1	29	18
14	-6	30	313
15	-5	31	412
16	-6		

INSTRUCTIONS

On this form, list the average daily unit power level in MWe-Net for each day in the reporting month. Compute to the nearest whole megawatt.

These figures will be used to plot a graph for each reporting month. Note that when maximum dependable capacity is used for the net electrical rating of the unit, there may be occasions when the daily average power level exceeds the 100% line (or the restricted power level line). In such cases, the average daily unit power output sheet should be footnoted to explain the apparent anomaly.

APPENDIX B
AVERAGE DAILY UNIT POWER LEVEL

DOCKET NO. 50-265
UNIT TWO
DATE JANUARY 13, 1988
COMPLETED BY L. DEELSNYDER
TELEPHONE 309-654-2241

MONTH DECEMBER 1987

DAY	AVERAGE DAILY POWER LEVEL (MWe-Net)	DAY	AVERAGE DAILY POWER LEVEL (MWe-Net)
1	750	17	756
2	755	18	791
3	705	19	852
4	748	20	709
5	736	21	779
6	754	22	748
7	772	23	737
8	757	24	712
9	757	25	694
10	29	26	723
11	558	27	738
12	722	28	719
13	734	29	715
14	757	30	705
15	720	31	732
16	751		

INSTRUCTIONS

On this form, list the average daily unit power level in MWe-Net for each day in the reporting month. Compute to the nearest whole megawatt.

These figures will be used to plot a graph for each reporting month. Note that when maximum dependable capacity is used for the net electrical rating of the unit, there may be occasions when the daily average power level exceeds the 100% line (or the restricted power level line). In such cases, the average daily unit power output sheet should be footnoted to explain the apparent anomaly.

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APPENDIX D
UNIT SHUTDOWNS AND POWER REDUCTIONS

QTP 300-S13
Revision 6
August 1982

DOCKET NO. 50-254

UNIT NAME QUAD CITIES UNIT ONE

COMPLETED BY L. DEELSNYDER

DATE JANUARY 13, 1988

REPORT MONTH DECEMBER 1987

TELEPHONE 309-654-2241

NO.	DATE	TYPE F OR S	DURATION (HOURS)	REASON	METHOD OF SHUTTING DOWN REACTOR	LICENSEE EVENT REPORT NO.	SYSTEM CODE	COMPONENT CODE	CORRECTIVE ACTIONS/COMMENTS
87-20	870912	S	545.4	C	4	-------	RC	FUELXX	End of Cycle Nine Refueling Outage
87-21	871223	F	7.5	A	9	-------	TA	TG	Generator Tripped Due to Turbine Vibrations
87-22	871224	F	10.6	A	9	-------	TA	TG	Generator Tripped Due to Turbine Vibrations
87-23	871227	S	54.0	B	9	-------	TA	TG	Turbine Tripped for Overspeed Test
87-24	871229	S	1.5	B	9	-------	TA	TG	Turbine Tripped for Overspeed Test

APPROVED
AUG 16 1982
QCOSR

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APPENDIX D
UNIT SHUTDOWNS AND POWER REDUCTIONS

QTP 300-S13
Revision 6
August 1982

DOCKET NO. 50-265

UNIT NAME QUAD CITIES UNIT TWO

COMPLETED BY L. DEELSNYDER

DATE JANUARY 13, 1988

REPORT MONTH DECEMBER 1987

TELEPHONE 309-654-2241

NO.	DATE	TYPE F OR S	DURATION (HOURS)	REASON	METHOD OF SHUTTING DOWN REACTOR	LICENSEE EVENT REPORT NO.	SYSTEM CODE	COMPONENT CODE	CORRECTIVE ACTIONS/COMMENTS
87-22	871210	F	23.2	A	3	2-87-020	TA-TB	TG	Reactor Scram on Turbine/Generator Load Mismatch

APPROVED
AUG 16 1982
QCOSR

VI. UNIQUE REPORTING REQUIREMENTS

The following items are included in this report based on prior commitments to the commission:

A. MAIN STEAM RELIEF VALVE OPERATIONS

There were no Main Steam Relief Valve Operations for the reporting period.

B. CONTROL ROD DRIVE SCRAM TIMING DATA FOR UNITS ONE AND TWO

The basis for reporting this data to the Nuclear Regulatory Commission are specified in the surveillance requirements of Technical Specifications 4.3.C.1 and 4.3.C.2.

The following table is a complete summary of Units One and Two Control Rod Drive Scram Timing for the reporting period. All scram timing was performed with Reactor pressure greater than 800 PSIG.

RESULTS OF SCRAM TIMING MEASUREMENTS

PERFORMED ON UNIT 1 & 2 CONTROL

ROD DRIVES, FROM 1-1-87 TO 12-31-87

DATE	NUMBER OF RODS	AVERAGE TIME IN SECONDS AT % INSERTED FROM FULLY WITHDRAWN				MAX. TIME FOR 90% INSERTION	DESCRIPTION
		5	20	50	90		Technical Specification 3.3.C.1 &
		0.375	0.900	2.00	3.5	7 sec.	3.3.C.2 (Average Scram Insertion Time)
1-27-87	177	0.30	0.67	1.44	2.53	2.91 (K-5)	Unit 2 Hot Scram Timing
2-20-87	1	0.30	0.72	1.58	2.80	2.80 (K-7)	Unit 1 Hot Scram Timing after HCU Replacement (Work Request Q55428)
3-19-87	89	0.29	0.66	1.43	2.52	2.82 (J-11)	Unit 1 Hot Scram Timing
9-6-87	91	0.30	0.67	1.43	2.53	2.77 (G-9)	Unit 2 Hot Scram Timing
11-3-87	2	0.28	0.65	1.40	2.49	2.54 (M-07)	Unit 2 M-7 & C-5 Hot Scram Timing after work on accumulators (Work Requests Q60928 & Q60780)
11-4-87	3	0.31	0.67	1.43	2.51	2.64 (M-06)	Unit 2 M-5 & M-6 Hot Scram Timing after work done on scram outlet valves. (Work Requests Q61254 & Q61256). P-11 scram timed after being stuck.
12-26-87	177	0.30	0.69	1.48	2.60	3.40 (G-4)	U-1 Hot Scram Timing

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VII. REFUELING INFORMATION

The following information about future reloads at Quad-Cities Station was requested in a January 26, 1978, licensing memorandum (78-24) from D. E. O'Brien to C. Reed, et al., titled "Dresden, Quad-Cities, and Zion Station--NRC Request for Refueling Information", dated January 18, 1978.

QTP 300-S32
Revision 1
March 1978

QUAD-CITIES REFUELING INFORMATION REQUEST

*

1. Unit: Q1 Reload: 9 Cycle: 10

2. Scheduled date for next refueling shutdown: 6-24-89

3. Scheduled date for restart following refueling: 9-17-89

4. Will refueling or resumption of operation thereafter require a technical specification change or other license amendment:

   NOT AS YET DETERMINED.

5. Scheduled date(s) for submitting proposed licensing action and supporting information:

   MARCH 24, 1989

6. Important licensing considerations associated with refueling, e.g., new or different fuel design or supplier, unreviewed design or performance analysis methods, significant changes in fuel design, new operating procedures:

   NONE AT PRESENT TIME.

7. The number of fuel assemblies.

   a. Number of assemblies in core: 724

   b. Number of assemblies in spent fuel pool: 1773

8. The present licensed spent fuel pool storage capacity and the size of any increase in licensed storage capacity that has been requested or is planned in number of fuel assemblies:

   a. Licensed storage capacity for spent fuel: 3657

   b. Planned increase in licensed storage: 0

9. The projected date of the last refueling that can be discharged to the spent fuel pool assuming the present licensed capacity: 2008

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APR 2 0 1978

Q. C. O. S. R.

QTP 300-S32
Revision 1
March 1978

QUAD-CITIES REFUELING INFORMATION REQUEST

*

1. Unit: Q2 Reload: 8 Cycle: 9

2. Scheduled date for next refueling shutdown: 4-9-88

3. Scheduled date for restart following refueling: 5-22-88

4. Will refueling or resumption of operation thereafter require a technical specification change or other license amendment: YES. TECHNICAL SPECIFICATION CHANGES WILL BE REQUIRED FOR NEW FUEL TYPES (MAPHLGR CURVES). CHANGE TO MCPR LIMIT AND OPERATION AT INCREASED CORE FLOW/FINAL FEEDWATER TEMP. REDUCTION.

5. Scheduled date(s) for submitting proposed licensing action and supporting information:

   FEBRUARY 22, 1988

6. Important licensing considerations associated with refueling, e.g., new or different fuel design or supplier, unreviewed design or performance analysis methods, significant changes in fuel design, new operating procedures:

   FIRST RELOAD OF GENERAL ELECTRIC, GE8E FUEL WITH 4 WATER-RODS AND LHGR LIMIT OF 14.4 KW/FT.

7. The number of fuel assemblies.

   a. Number of assemblies in core: 724

   b. Number of assemblies in spent fuel pool: 1311

8. The present licensed spent fuel pool storage capacity and the size of any increase in licensed storage capacity that has been requested or is planned in number of fuel assemblies:

   a. Licensed storage capacity for spent fuel: 3897

   b. Planned increase in licensed storage: 0

9. The projected date of the last refueling that can be discharged to the spent fuel pool assuming the present licensed capacity: 2008

APPROVED

APR 2 0 1978

Q. C. O. S. R.

VIII. GLOSSARY

The following abbreviations which may have been used in the Monthly Report, are defined below:

ACAD/CAM	-	Atmospheric Containment Atmospheric Dilution/Containment Atmospheric Monitoring
ANSI	-	American National Standards Institute
APRM	-	Average Power Range Monitor
ATWS	-	Anticipated Transient Without Scram
BWR	-	Boiling Water Reactor
CRD	-	Control Rod Drive
EHC	-	Electro-Hydraulic Control System
EOF	-	Emergency Operations Facility
GSEP	-	Generating Stations Emergency Plan
HEPA	-	High-Efficiency Particulate Filter
HPCI	-	High Pressure Coolant Injection System
HRSS	-	High Radiation Sampling System
IPCLRT	-	Integrated Primary Containment Leak Rate Test
IRM	-	Intermediate Range Monitor
ISI	-	Inservice Inspection
LER	-	Licensee Event Report
LLRT	-	Local Leak Rate Test
LPCI	-	Low Pressure Coolant Injection Mode of RHRS
LPRM	-	Local Power Range Monitor
MAPLHGR	-	Maximum Average Planar Linear Heat Generation Rate
MCPR	-	Minimum Critical Power Ratio
MFLCPR	-	Maximum Fraction Limiting Critical Power Ratio
MPC	-	Maximum Permissible Concentration
MSIV	-	Main Steam Isolation Valve
NIOSH	-	National Institute for Occupational Safety and Health
PCI	-	Primary Containment Isolation
PCIOMR	-	Preconditioning Interim Operating Management Recommendations
RBCCW	-	Reactor Building Closed Cooling Water System
RBM	-	Rod Block Monitor
RCIC	-	Reactor Core Isolation Cooling System
RHRS	-	Residual Heat Removal System
RPS	-	Reactor Protection System
RWM	-	Rod Worth Minimizer
SBGTS	-	Standby Gas Treatment System
SBLC	-	Standby Liquid Control
SDC	-	Shutdown Cooling Mode of RHRS
SDV	-	Scram Discharge Volume
SRM	-	Source Range Monitor
TBCCW	-	Turbine Building Closed Cooling Water System
TIP	-	Traversing Incore Probe
TSC	-	Technical Support Center

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Telephone 309/654-2241

RAR-87-58

December 31, 1987

U.S. NRC
Office of Nuclear Reactor Regulation
Washington, D. C. 20555
Attn: Document Control Desk

Enclosed for your information is the Monthly Performance Report covering the operation of Quad-Cities Nuclear Power Station, Units One and Two, during the month of December, 1987.

Respectfully,

COMMONWEALTH EDISON COMPANY
QUAD-CITIES NUCLEAR POWER STATION

R. A. Robey

R. A. Robey
Services Superintendent

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Enclosure

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