

# INFORMATION ONLY

## EMERGENCY CORE COOLING SYSTEMS

ECCS SUBSYSTEMS - T<sub>avg</sub>  $\geq 280^{\circ}\text{F}$

## LIMITING CONDITION FOR OPERATION

3.5.2 Two independent ECCS subsystems shall be OPERABLE with each subsystem comprised of:

- a. One OPERABLE high pressure injection (HPI) pump.
- b. One OPERABLE low pressure injection (LPI) pump.
- c. One OPERABLE decay heat cooler, and
- d. An OPERABLE flow path capable of taking suction from the borated water storage tank (BWST) on a safety injection signal and manually transferring suction to the containment sump during the recirculation phase of operation.

APPLICABILITY: MODES 1, 2 and 3.

### ACTION:

- a. With one ECCS subsystem inoperable, restore the inoperable subsystem to OPERABLE status within 72 hours or be in HOT SHUTDOWN within the next 12 hours.
- b. In the event the ECCS is actuated and injects water into the Reactor Coolant System, a Special Report shall be prepared and submitted to the Commission pursuant to Specification 6.9.2 within 90 days describing the circumstances of the actuation and the total accumulated actuation cycles to date.

## SURVEILLANCE REQUIREMENTS

4.5.2 Each ECCS subsystem shall be demonstrated OPERABLE:

- a. At least once per 31 days by verifying that each valve (manual, power operated or automatic) in the flow path that is not locked, sealed or otherwise secured in position, is in its correct position.

DAVIS-BESSE, UNIT 1

3/4 5-3

Amendment No. 26, 182

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Revised by NRC Letter Dated  
June 6, 1995

## SURVEILLANCE REQUIREMENTS (Continued)

- b. At least once per 18 months, or prior to operation after ECCS piping has been drained by verifying that the ECCS piping is full of water by venting the ECCS pump casings and discharge piping high points. \*\*
- c. By a visual inspection which verifies that no loose debris (rags, trash, clothing, etc.) is present in the containment which could be transported to the containment emergency sump and cause restriction of the pump suction during LOCA conditions. This visual inspection shall be performed:
  - 1. For all accessible areas of the containment prior to establishing CONTAINMENT INTEGRITY, and
  - 2. For all areas of containment affected by an entry, at least once daily while work is ongoing and again during the final exit after completion of work (containment closeout) when CONTAINMENT INTEGRITY is established.
- d. At least once per 18 months by:
  - 1. Verifying that the interlocks:
    - a) Close DH-11 and DH-12 and deenergize the pressurizer heaters, if either DH-11 or DH-12 is open and a simulated reactor coolant system pressure which is greater than the trip setpoint (<438 psig) is applied. The interlock to close DH-11 and/or DH-12 is not required if the valve is closed and 480 V AC power is disconnected from its motor operators.
    - b) Prevent the opening of DH-11 and DH-12 when a simulated or actual reactor coolant system pressure which is greater than the trip setpoint (<438 psig) is applied.
  - 2. a) A visual inspection of the containment emergency sump which verifies that the subsystem suction inlets are not restricted by debris and that the sump components (trash racks, screens, etc.) show no evidence of structural distress or corrosion.
  - b) Verifying that on a Borated Water Storage Tank (BWST) Low-Low Level interlock trip, with the motor operators for the BWST outlet isolation valves and the containment emergency sump recirculation valves energized, the BWST Outlet Valve HV-DH7A (HV-DH7B) automatically close in  $\leq 75$  seconds after the operator manually pushes the control switch to open the Containment Emergency Sump Valve HV-DH9A (HV-DH9B) which should be verified to open in  $\leq 75$  seconds.
- 3. Deleted

\*\* The requirements of this surveillance may be deferred until the Tenth Refueling Outage for the ECCS flowpath which does not have manual high point venting capability.

## EMERGENCY CORE COOLING SYSTEMS

### SURVEILLANCE REQUIREMENTS (Continued)

4. Verifying that a minimum of 290 cubic feet of trisodium phosphate dodecahydrate (TSP) is contained within the TSP storage baskets.
  5. Deleted
  6. Deleted
- e. At least once per 18 months, during shutdown, by
1. Verifying that each automatic valve in the flow path actuates to its correct position on a safety injection test signal.
  2. Verifying that each HPI and LPI pump starts automatically upon receipt of a SFAS test signal.
- f. By performing a vacuum leakage rate test of the watertight enclosure for valves DH-11 and DH-12 that assures the motor operators on valves DH-11 and DH-12 will not be flooded for at least 7 days following a LOCA:
1. At least once per 18 months.
  2. After each opening of the watertight enclosure.
  3. After any maintenance on or modification to the watertight enclosure which could affect its integrity.

The inspection port on the watertight enclosure may be opened without requiring performance of the vacuum leakage rate test, to perform inspections. After use, the inspection port must be verified as closed in its correct position. Provisions of TS 3.0.3 are not applicable during these inspections.

- g. By verifying the correct position of each mechanical position stop for valves DH-14A and DH-14B.
1. Within 4 hours following completion of the opening of the valves to their mechanical position stop or following completion of maintenance on the valve when the LPI system is required to be OPERABLE.
  2. At least once per 18 months.

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## EMERGENCY CORE COOLING SYSTEMS

### SURVEILLANCE REQUIREMENTS (Continued)

- h. By performing a flow balance test, during shutdown, following completion of modifications to the HPI or LPI subsystems that alter the subsystem flow characteristics and verifying the following flow rates:

#### HPI System - Single Pump

Injection Leg 1-1  $\geq$  375 gpm at 400 psig\*  
Injection Leg 1-2  $\geq$  375 gpm at 400 psig\*

Injection Leg 2-1  $\geq$  375 gpm at 400 psig\*  
Injection Leg 2-2  $\geq$  375 gpm at 400 psig\*

#### LPI System - Single Pump

Injection Leg 1  $\geq$  2650 gpm at 100 psig\*\*  
Injection Leg 2  $\geq$  2650 gpm at 100 psig\*\*

\* Reactor coolant pressure at the HPI nozzle in the reactor coolant pump discharge.

\*\* Reactor coolant pressure at the core flood nozzle on the reactor vessel.

3/4.5 EMERGENCY CORE COOLING SYSTEMS (ECCS)BASES**INFORMATION ONLY**3/4.5.1 CORE FLOODING TANKS

The OPERABILITY of each core flooding tank ensures that a sufficient volume of borated water will be immediately forced into the reactor vessel in the event the RCS pressure falls below the pressure of the tanks. This initial surge of water into the vessel provides the initial cooling mechanism during large RCS pipe ruptures.

The limits on volume, boron concentration and pressure ensure that the assumptions used for core flooding tank injection in the safety analysis are met.

The tank power operated isolation valves are considered to be "operating bypasses" in the context of IEEE Std. 279-1971, which requires that bypasses of a protective function be removed automatically whenever permissive conditions are not met. In addition, as these tank isolation valves fail to meet single failure criteria, removal of power to the valves is required.

The one hour limit for operation with a core flooding tank (CFT) inoperable for reasons other than boron concentration not within limits minimizes the time the plant is exposed to a possible LOCA event occurring with failure of a CFT, which may result in unacceptable peak cladding temperatures.

With boron concentration for one CFT not within limits, the condition must be corrected within 72 hours. The 72 hour limit was developed considering that the effects of reduced boron concentration on core subcriticality during reflood are minor. Boiling of the ECCS water in the core during reflood concentrates the boron in the saturated liquid that remains in the core. In addition, the volume of the CFTs is still available for injection. Since the boron requirements are based on the average boron concentration of the total volume of both CFTs, the consequences are less severe than they would be if the contents of a CFT were not available for injection.

The completion times to bring the plant to a MODE in which the Limiting Condition for Operation (LCO) does not apply are reasonable based on operating experience. The completion times allow plant conditions to be changed in an orderly manner and without challenging plant systems.

CFT boron concentration sampling within 6 hours after an 80 gallon volume increase will identify whether inleakage from the RCS has caused a reduction in boron concentration to below the required limit. It is not necessary to verify boron concentration if the added water inventory is from the borated water storage tank (BWST), because the water contained in the BWST is within CFT boron concentration requirements.

3/4.5.2 and 3/4.5.3 ECCS SUBSYSTEMS

The operability of two independent ECCS subsystems with RCS average temperature  $\geq 280^\circ\text{F}$  ensures that sufficient emergency core cooling capability will be available in the event of a LOCA assuming the loss of one subsystem through any single failure consideration. Either subsystem operating in conjunction with the core flooding tanks is capable of supplying sufficient core cooling to maintain the peak cladding temperatures within acceptable limits for all postulated break sizes ranging from the double ended break of the largest RCS cold leg pipe downward. In addition, each ECCS subsystem provides long term core cooling capability in the recirculation mode during the accident recovery period.



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**BASES**

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With the RCS temperature below 280°F, one OPERABLE ECCS subsystem is acceptable without single failure consideration on the basis of the stable reactivity condition of the reactor and the limited core cooling requirements.

The Surveillance Requirements provided to ensure OPERABILITY of each component ensures that, at a minimum, the assumptions used in the safety analyses are met and that subsystem OPERABILITY is maintained.

The function of the trisodium phosphate dodecahydrate (TSP) contained in baskets located in the containment normal sump or on the 565' elevation of containment adjacent to the normal sump, is to neutralize the acidity of the post-LOCA borated water mixture during containment emergency sump recirculation. The borated water storage tank (BWST) borated water has a nominal pH value of approximately 5. Raising the borated water mixture to a pH value of 7 will ensure that chloride stress corrosion does not occur in austenitic stainless steels in the event that chloride levels increase as a result of contamination on the surfaces of the reactor containment building. Also, a pH of 7 is assumed for the containment emergency sump for iodine retention and removal post-LOCA by the containment spray system.

The Surveillance Requirement (SR) associated with TSP ensures that the minimum required volume of TSP is stored in the baskets. The minimum required volume of TSP is the volume that will achieve a post-LOCA borated water mixture pH of  $\geq 7.0$ , conservatively considering the maximum possible sump water volume and the maximum possible boron concentration. The amount of TSP required is based on the mass of TSP needed to achieve the required pH. However, a required volume is verified by the SR, rather than the mass, since it is not feasible to weigh the entire amount of TSP in containment. The minimum required volume is based on the manufactured density of TSP (53 lb/ft<sup>3</sup>). Since TSP can have a tendency to agglomerate from high humidity in the containment, the density may increase and the volume decrease during normal plant operation, however, solubility characteristics are not expected to change. Therefore, considering possible agglomeration and increase in density, verifying the minimum volume of TSP in containment is conservative with respect to ensuring the capability to achieve the minimum required pH. The minimum required volume of TSP to meet all analytical requirements is 250 ft<sup>3</sup>. The surveillance requirement of 290 ft<sup>3</sup> includes 40 ft<sup>3</sup> of spare TSP as margin. Total basket capacity is 325 ft<sup>3</sup>.

Decay Heat Removal System valves DH-11 and DH-12 are located in an area that would be flooded following a LOCA. These valves are located in a watertight enclosure to ensure their operability up to seven days following a LOCA. Surveillance Requirements are provided to verify the acceptable leak tightness of this enclosure. An inspection port is located on this watertight enclosure, which is typically used for performing inspections inside the enclosure. During the vacuum leakage rate test, the inspection port is in a closed position and subject to the test. This inspection port may be subsequently opened for use in viewing inside the enclosure. Opening this inspection port will not require performance of the vacuum leakage rate test because of the design of the closure fitting, which will preclude leakage under LOCA conditions, when properly installed. Proper installation includes independent verification.

Surveillance requirements for throttle valve position stops and flow balance testing provide assurance that proper ECCS flows will be maintained in the event of a LOCA. Maintenance of proper flow resistance and pressure drop in the piping system to each injection point is necessary to: (1) prevent total pump flow from exceeding runout conditions when the system is in its minimum resistance configuration, (2) provide the proper flow split between injection points in accordance with the assumptions used in the ECCS-LOCA analyses, and (3) provide an acceptable level of total ECCS flow to all injection points equal to or above that assumed in the ECCS-LOCA analyses.

EMERGENCY CORE COOLING SYSTEMS**INFORMATION ONLY**BASES (Continued)

Containment Emergency Sump Recirculation Valves DH-9A and DH-9B are de-energized during MODES 1, 2, 3 and 4 to preclude postulated inadvertent opening of the valves in the event of a Control Room fire, which could result in draining the Borated Water Storage Tank to the Containment Emergency Sump and the loss of this water source for normal plant shutdown. Re-energization of DH-9A and DH-9B is permitted on an intermittent basis during MODES 1, 2, 3 and 4 under administrative controls. Station procedures identify the precautions which must be taken when re-energizing these valves under such controls.

Borated Water Storage Tank (BWST) outlet isolation valves DH-7A and DH-7B are de-energized during MODES 1, 2, 3, and 4 to preclude postulated inadvertent closure of the valves in the event of a fire, which could result in a loss of the availability of the BWST. Re-energization of valves DH-7A and DH-7B is permitted on an intermittent basis during MODES 1, 2, 3, and 4 under administrative controls. Station procedures identify the precautions which must be taken when re-energizing these valves under such controls.

3/4.5.4 BORATED WATER STORAGE TANK

The OPERABILITY of the borated water storage tank (BWST) as part of the ECCS ensures that a sufficient supply of borated water is available for injection by the ECCS in the event of a LOCA. The limits on the BWST minimum volume and boron concentration ensure that:

- 1) sufficient water is available within containment to permit recirculation cooling flow to the core following manual switchover to the recirculation mode, and
- 2) The reactor will remain at least 1%  $\Delta k/k$  subcritical in the cold condition at 70°F, xenon free, while only crediting 50% of the control rods' worth following mixing of the BWST and the RCS water volumes.

These assumptions ensure that the reactor remains subcritical in the cold condition following mixing of the BWST and the RCS water volumes.

With either the BWST boron concentration or BWST borated water temperature not within limits, the condition must be corrected in eight hours. The eight hour limit to restore the temperature or boron concentration to within limits was developed considering the time required to change boron concentration or temperature and assuming that the contents of the BWST are still available for injection.

The bottom 4 inches of the BWST are not available, and the instrumentation is calibrated to reflect the available volume. The limits on water volume, and boron concentration ensure a pH value of between 7.0 and 11.0 of the solution sprayed within the containment after a design basis accident. The pH band minimizes the evolution of iodine and minimizes the effect of chloride and caustic stress corrosion cracking on mechanical systems and components.

## ENVIRONMENTAL ASSESSMENT

### Identification of Proposed Action

This proposed action involves the Davis-Besse Nuclear Power Station (DBNPS), Unit Number 1, Operating License Number NPF-3, Appendix A, Technical Specifications (TS). A license amendment request is proposed by Toledo Edison to revise TS 3/4.5.2, "Emergency Core Cooling Systems, ECCS Subsystems - Tavg  $\geq$  280°F" Surveillance Requirement 4.5.2.f. Surveillance Requirement (SR) 4.5.2.f requires that the watertight enclosure which encloses the Decay Heat Removal (DHR) System isolation valves DH-11 and DH-12 be demonstrated operable by performing a vacuum leakage rate test of the enclosure. These valves are located in a common valve pit in the lower elevation of the containment vessel. The lower elevation in containment would be flooded following a Loss-of-Coolant Accident. Since the motor operators for these valves are not qualified for a submerged environment, the watertight enclosure is provided to cover the valve pit to ensure the valves will not be flooded for at least seven days following a LOCA. The watertight enclosure consists of the walls of the valve pit and large 1/4-inch deck plates attached to a steel frame, which cover the valve pit.

Surveillance Requirement 4.5.2.f requires that the vacuum leakage rate test be performed: 1) at least once per 18 months, 2) after each opening of the watertight enclosure, and 3) after any maintenance on or modification to the watertight enclosure which could affect its integrity. Technical Specification 3.0.3 was entered by the DBNPS on February 12, 1997 when it was determined that the Kamlok coupling inspection port on the enclosure had been opened after the vacuum leakage rate test had been performed. The inspection port had been opened in Mode 3 during heatup from the Tenth Refueling Outage to perform an American Society of Mechanical Engineer Boiler and Pressure Vessel (ASME) Code visual Inservice Inspection (ISI) of portions of the decay heat piping located within the enclosure. The ISI is conducted with the piping at full pressure and temperature pursuant to the requirements of the ASME Code. Compliance with the ASME Code ISI requirements is mandated by TS 4.0.5.

Since the vacuum leakage rate test can only be performed in Mode 4, 5, or 6 due to the required testing conditions, opening the inspection port to perform the ISI per TS 4.0.5 in Mode 3 would then require the plant to be cooled down to at least Mode 5 in order to perform the vacuum leakage rate test.

On February 12, 1997, with the plant at 100% rated thermal power it was determined that the inspection port had been opened on May 24, 1996, during Mode 3 after the vacuum leakage rate test had been performed. Technical Specification 3.0.3 was entered and a plant shutdown commenced. This shutdown was terminated and the plant returned to 100% rated thermal power when the NRC staff granted a verbal enforcement discretion from performance of this SR 4.5.2.f on February 12.



The DBNPS is proposing a follow-up license amendment to the granting of this enforcement discretion which would allow the inspection port on the watertight enclosure to be opened for inspections during Modes 1, 2 or 3 without requiring performance of the vacuum leakage rate test. After use, the inspection port would be required to be verified as closed in its correct position. Also, the provisions of TS 3.0.3 would not be applicable during these inspections in order not to require a plant shutdown due to the inspection port being open.

#### Need for the Proposed Action

The changes proposed are needed to replace NRC staff's enforcement discretion verbally granted on February 12, 1997 which allowed continued plant operation. This enforcement discretion remains in effect until the NRC approves the proposed license amendment to revise the TS requirements, or until the DBNPS enters Mode 4 in an outage of sufficient duration to perform the vacuum leakage rate test, which ever occurs first.

#### Environmental Impact of the Proposed Action

As described in the Safety Assessment and Significant Hazards Consideration for the proposed license amendment. Toledo Edison has determined that the ECCS structures, systems and components which could be affected by the proposed license amendment, will continue to be capable of performing their safety functions.

The proposed license amendment will reduce the potential for unduly requiring cooldown and heatup transitions of plant equipment, thus preserving the cycling margin between plant design and actual operating history.

The proposed license amendment involves a change to a requirement with respect to the use of plant components located within the restricted area as defined in 10CFR Part 20. As discussed in the Safety Assessment and Significant Hazards Consideration, this proposed license amendment does not involve a significant hazards consideration. The proposed change to allow continued plant operation does not alter source terms, containment isolation or allowable releases. In addition, the proposed change does not involve an increase in the amounts, and no change in the types, of any radiological effluents that may be allowed to be released offsite. Furthermore, there is no increase in the individual or cumulative occupational radiation exposure.

With regard to potential non-radiological impacts, the proposed license amendment involves no increase in the amounts or change in types of any non-radiological effluents that may be released offsite, and has no other environmental impact.

Based on the above, Toledo Edison concludes that there are no significant radiological or non-radiological environmental impacts associated with the proposed license amendment.

#### Alternatives to the Proposed Action

Since Toledo Edison has concluded that the environmental effects of the proposed action are not significant, any alternatives will have only similar or greater environmental impacts. The principal alternative would be not to grant the license amendment. This would not reduce the environmental impacts attributable to the plant. Furthermore, it would force a cooldown of the plant after performing inspections utilizing the inspection port.

#### Alternative Use of Resources

This action does not involve the use of resources not previously considered in the Final Environmental Statement Related to the Operation of the Davis-Besse Nuclear Power Station, Unit Number 1 (NUREG 75/097).

#### Finding of No Significant Impact

Toledo Edison has reviewed the proposed license amendment against the categorical exclusion criteria of 10CFR51.22(c)(9) for an environmental assessment. As demonstrated in the proposed license amendment's Safety Assessment and Significant Hazards Consideration the proposed changes do not involve a significant hazards consideration, do not increase the types or amounts of effluents that may be released offsite, and do not increase individual or cumulative occupational radiation exposures. Accordingly, Toledo Edison finds that the proposed license amendment, if approved by the Nuclear Regulatory Commission, will have no significant impact on the environment and that no environmental assessment is required.