

CORE OPERATING LIMITS REPORT (COLR)

FOR

BRAIDWOOD UNIT 2 CYCLE 22

EXELON TRACKING ID:

COLR BRAIDWOOD 2 REVISION 13

CORE OPERATING LIMITS REPORT (COLR) for BRAIDWOOD UNIT 2 CYCLE 22

1.0 CORE OPERATING LIMITS REPORT

This Core Operating Limits Report (COLR) for Braidwood Station Unit 2 Cycle 22 has been prepared in accordance with the requirements of Technical Specification 5.6.5 (ITS).

The Technical Specification Safety Limits and Limiting Conditions for Operation (LCOs) affected by this report are listed below:

SL	2.1.1	Reactor Core Safety Limits (SLs)
LCO	3.1.1	SHUTDOWN MARGIN (SDM)
LCO	3.1.3	Moderator Temperature Coefficient (MTC)
LCO	3.1.4	Rod Group Alignment Limits
LCO	3.1.5	Shutdown Bank Insertion Limits
LCO	3.1.6	Control Bank Insertion Limits
LCO	3.1.8	PHYSICS TESTS Exceptions – MODE 2
LCO	3.2.1	Heat Flux Hot Channel Factor ($F_Q(Z)$)
LCO	3.2.2	Nuclear Enthalpy Rise Hot Channel Factor ($F_{\Delta H}^N$)
LCO	3.2.3	AXIAL FLUX DIFFERENCE (AFD)
LCO	3.2.5	Departure from Nucleate Boiling Ratio (DNBR)
LCO	3.3.1	Reactor Trip System (RTS) Instrumentation
LCO	3.3.9	Boron Dilution Protection System (BDPS)
LCO	3.4.1	Reactor Coolant System (RCS) Pressure, Temperature, and Flow Departure from Nucleate Boiling (DNB) Limits
LCO	3.9.1	Boron Concentration

The portions of the Technical Requirements Manual (TRM) affected by this report are listed below:

TRM TLCO 3.1.b	Boration Flow Paths – Operating
TRM TLCO 3.1.d	Charging Pumps – Operating
TRM TLCO 3.1.f	Borated Water Sources – Operating
TRM TLCO 3.1.g	Position Indication System – Shutdown
TRM TLCO 3.1.h	Shutdown Margin (SDM) – MODE 1 and MODE 2 with $k_{eff} \geq 1.0$
TRM TLCO 3.1.i	Shutdown Margin (SDM) – MODE 5
TRM TLCO 3.1.j	Shutdown and Control Rods
TRM TLCO 3.1.k	Position Indication System – Shutdown (Special Test Exception)

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2.0 OPERATING LIMITS

The cycle-specific parameter limits for the specifications listed in Section 1.0 are presented in the following subsections. These limits are applicable for the entire cycle unless otherwise identified. These limits have been developed using the NRC-approved methodologies specified in Technical Specification 5.6.5.

2.1 Reactor Core Safety Limits (SLs) (SL 2.1.1)

2.1.1 In MODES 1 and 2, the combination of Thermal Power, Reactor Coolant System (RCS) highest loop average temperature, and pressurizer pressure shall not exceed the limits specified in Figure 2.1.1.

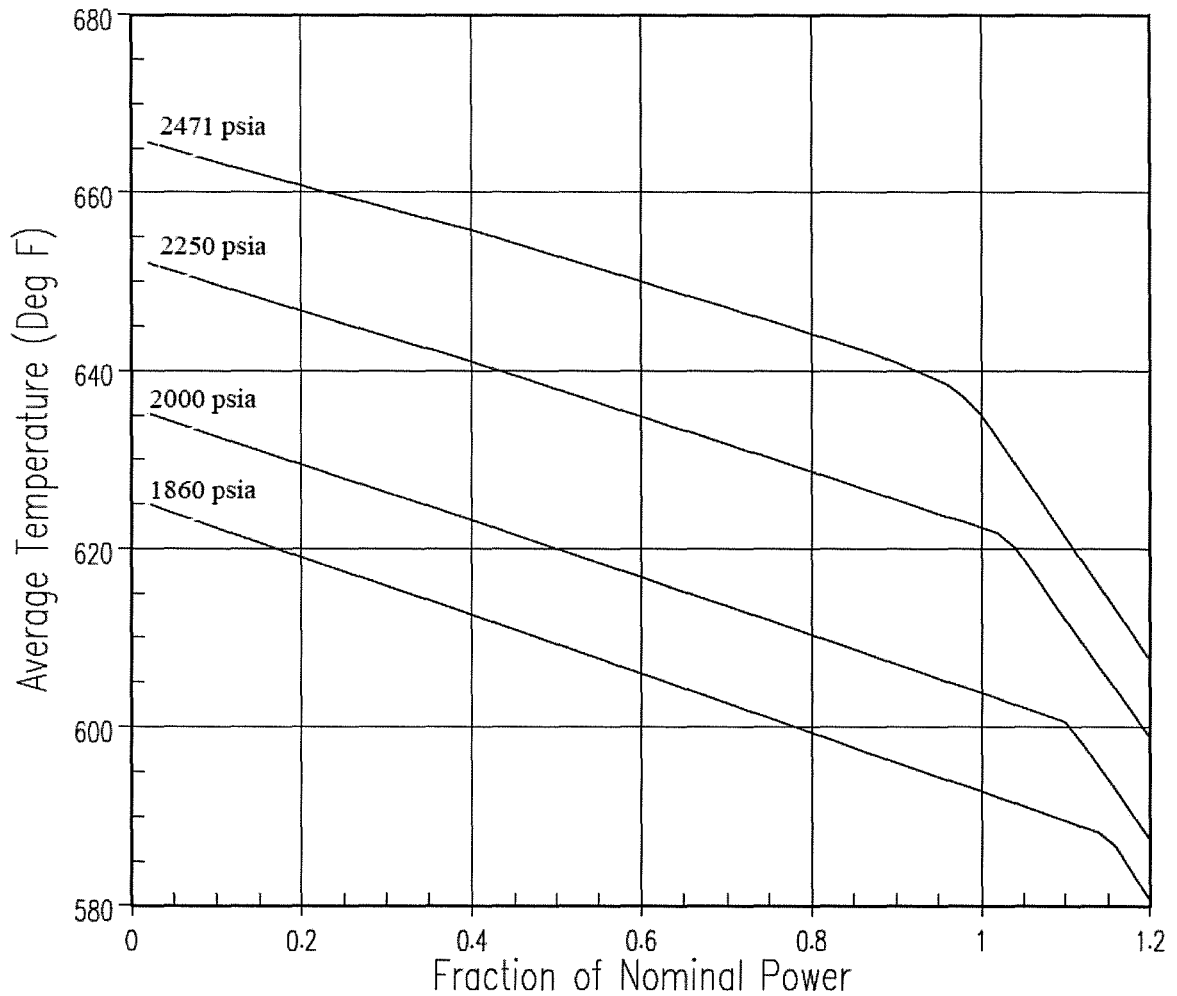


Figure 2.1.1: Reactor Core Limits

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2.2 SHUTDOWN MARGIN (SDM)

The SDM limit for MODES 1, 2, 3, and 4 is:

2.2.1 The SDM shall be greater than or equal to 1.3% $\Delta k/k$ (LCOs 3.1.1, 3.1.4, 3.1.5, 3.1.6, 3.1.8, 3.3.9; TRM TLCOs 3.1.b, 3.1.d, 3.1.f, 3.1.h, and 3.1.j).

The SDM limit for MODE 5 is:

2.2.2 SDM shall be greater than or equal to 1.3% $\Delta k/k$ (LCO 3.1.1, LCO 3.3.9; TRM TLCOs 3.1.i and 3.1.j).

2.3 Moderator Temperature Coefficient (MTC) (LCO 3.1.3)

The Moderator Temperature Coefficient (MTC) limits are:

2.3.1 The BOL/ARO/HZP-MTC upper limit shall be $+2.090 \times 10^{-5} \Delta k/k/^{\circ}F$.

2.3.2 The EOL/ARO/HFP-MTC lower limit shall be $-4.6 \times 10^{-4} \Delta k/k/^{\circ}F$.

2.3.3 The EOL/ARO/HFP-MTC Surveillance limit at 300 ppm shall be $-3.7 \times 10^{-4} \Delta k/k/^{\circ}F$.

2.3.4 The EOL/ARO/HFP-MTC Surveillance limit at 60 ppm shall be $-4.3 \times 10^{-4} \Delta k/k/^{\circ}F$.

where: BOL stands for Beginning of Cycle Life
ARO stands for All Rods Out
HZP stands for Hot Zero Thermal Power
EOL stands for End of Cycle Life
HFP stands for Hot Full Thermal Power

2.4 Shutdown Bank Insertion Limits (LCO 3.1.5)

2.4.1 All shutdown banks shall be fully withdrawn to at least 224 steps.

2.5 Control Bank Insertion Limits (LCO 3.1.6)

2.5.1 The control banks, with Bank A greater than or equal to 224 steps, shall be limited in physical insertion as shown in Figure 2.5.1.

2.5.2 Each control bank shall be considered fully withdrawn from the core at greater than or equal to 224 steps.

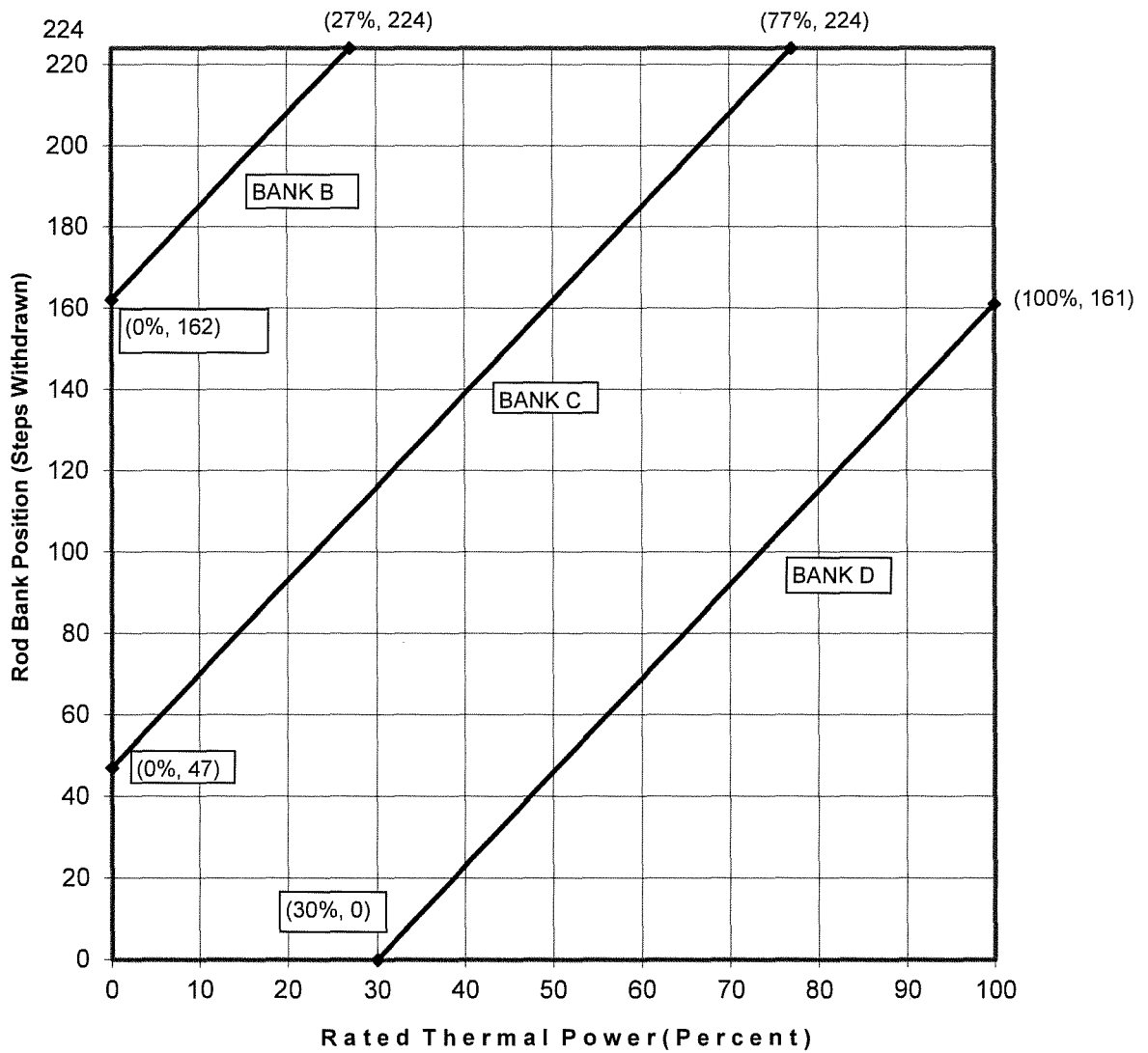
2.5.3 The control banks shall be operated in sequence by withdrawal of Bank A, Bank B, Bank C and Bank D. The control banks shall be sequenced in reverse order upon insertion.

2.5.4 Each control bank not fully withdrawn from the core shall be operated with the following overlap limits as a function of park position:

Park Position (step)	Overlap Limit (step)
226	111
227	112
228	113
229	114

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Figure 2.5.1:
Control Bank Insertion Limits Versus Percent Rated Thermal Power



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2.6 Heat Flux Hot Channel Factor ($F_Q(Z)$) (LCO 3.2.1)

2.6.1 Total Peaking Factor:

$$F_Q(Z) \leq \frac{F_Q^{RTP}}{0.5} \times K(Z) \quad \text{for } P \leq 0.5$$

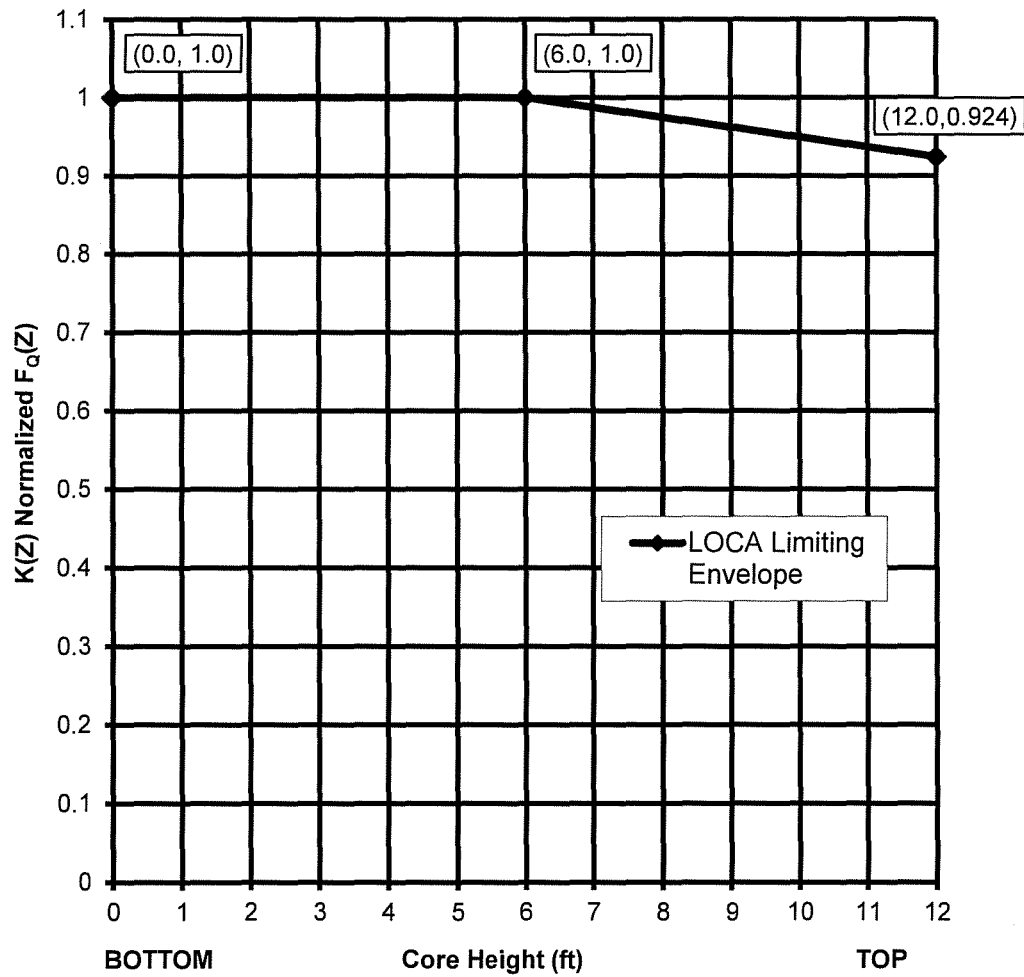
$$F_Q(Z) \leq \frac{F_Q^{RTP}}{P} \times K(Z) \quad \text{for } P > 0.5$$

where: P = the ratio of THERMAL POWER to RATED THERMAL POWER

$$F_Q^{RTP} = 2.60$$

$K(Z)$ is provided in Figure 2.6.1.

Figure 2.6.1
 $K(Z)$ - Normalized $F_Q(Z)$ as a Function of Core Height



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2.6.2 W(Z) Values:

a) When the Power Distribution Monitoring System (PDMS) is OPERABLE, $W(Z) = 1.00000$ for all axial points.

b) When PDMS is inoperable, $W(Z)$ is provided as:

- 1) Table 2.6.2.a are the normal operation $W(Z)$ values that correspond to the NORMAL AXIAL FLUX DIFFERENCE (AFD) Acceptable Operation Limits provided in Figure 2.8.1.a. The Normal AFD Acceptable Operation Limits may be invoked at any time and must be used with the corresponding $W(Z)$ values.
- 2) Table 2.6.2.b are the Expanded normal operation $W(Z)$ values that correspond to the EXPANDED AXIAL FLUX DIFFERENCE (AFD) Acceptable Operation Limits provided in Figure 2.8.1.b. The Expanded AFD Acceptable Operation Limits may be invoked at any time and must be used with the corresponding $W(Z)$ values.

Table 2.6.2.c shows the $F_Q^C(z)$ penalty factors that are greater than 2% per 31 Effective Full Power Days (EFPD). These values shall be used to increase the $F_Q^W(z)$ as per Surveillance Requirement 3.2.1.2. A 2% penalty factor shall be used at all cycle burnups that are outside the range of Table 2.6.2.c.

2.6.3 Uncertainty:

The uncertainty, U_{FQ} , to be applied to the Heat Flux Hot Channel Factor $F_Q(Z)$ shall be calculated by the following formula

$$U_{FQ} = U_{qu} \bullet U_e$$

where:

U_{qu} = Base F_Q measurement uncertainty = 1.05 when PDMS is inoperable
(U_{qu} is defined by PDMS when OPERABLE.)

U_e = Engineering uncertainty factor = 1.03

2.6.4 PDMS Alarms:

$F_Q(Z)$ Warning Setpoint = 2% $F_Q(Z)$ Margin

$F_Q(Z)$ Alarm Setpoint = 0% $F_Q(Z)$ Margin

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Height (feet)	150 MWD/MTU	6000 MWD/MTU	14000 MWD/MTU	20000 MWD/MTU
0.00 (core bottom)	1.2105	1.3465	1.2500	1.2142
0.20	1.1958	1.3171	1.2272	1.1940
0.40	1.1879	1.3047	1.2166	1.1862
0.60	1.1826	1.2922	1.2053	1.1804
0.80	1.1707	1.2294	1.1777	1.1704
1.00	1.1634	1.2142	1.1732	1.1579
1.20	1.1518	1.2014	1.1692	1.1520
1.40	1.1469	1.2026	1.1651	1.1474
1.60	1.1459	1.1934	1.1593	1.1401
1.80	1.1478	1.1813	1.1542	1.1333
2.00	1.1473	1.1699	1.1484	1.1256
2.20	1.1400	1.1571	1.1410	1.1152
2.40	1.1380	1.1429	1.1342	1.1050
2.60	1.1340	1.1318	1.1258	1.0931
2.80	1.1310	1.1309	1.1229	1.0896
3.00	1.1270	1.1290	1.1203	1.0871
3.20	1.1221	1.1262	1.1176	1.0933
3.40	1.1171	1.1233	1.1150	1.1038
3.60	1.1145	1.1184	1.1175	1.1152
3.80	1.1175	1.1145	1.1251	1.1245
4.00	1.1212	1.1097	1.1327	1.1390
4.20	1.1237	1.1074	1.1398	1.1544
4.40	1.1255	1.1073	1.1449	1.1681
4.60	1.1261	1.1054	1.1489	1.1803
4.80	1.1267	1.1042	1.1520	1.1914
5.00	1.1271	1.1025	1.1547	1.1995
5.20	1.1265	1.0994	1.1566	1.2055
5.40	1.1248	1.0968	1.1574	1.2094
5.60	1.1213	1.0939	1.1645	1.2222
5.80	1.1176	1.0910	1.1806	1.2412
6.00	1.1224	1.0940	1.1938	1.2573
6.20	1.1289	1.1024	1.2048	1.2694
6.40	1.1343	1.1099	1.2130	1.2795
6.60	1.1380	1.1165	1.2185	1.2847
6.80	1.1415	1.1236	1.2220	1.2881
7.00	1.1432	1.1306	1.2226	1.2885
7.20	1.1468	1.1376	1.2194	1.2832
7.40	1.1499	1.1447	1.2153	1.2769
7.60	1.1510	1.1513	1.2063	1.2658
7.80	1.1515	1.1590	1.1975	1.2529
8.00	1.1514	1.1652	1.1858	1.2372
8.20	1.1582	1.1704	1.1713	1.2166
8.40	1.1636	1.1756	1.1661	1.1981
8.60	1.1706	1.1787	1.1667	1.1766
8.80	1.1745	1.1823	1.1681	1.1727
9.00	1.1780	1.1932	1.1682	1.1780
9.20	1.1815	1.2030	1.1662	1.1807
9.40	1.1830	1.2131	1.1661	1.2180
9.60	1.1825	1.2233	1.2020	1.2660
9.80	1.1836	1.2410	1.2390	1.3080
10.00	1.1882	1.2578	1.2730	1.3460
10.20	1.2025	1.2744	1.3030	1.3790
10.40	1.2153	1.2888	1.3310	1.4080
10.60	1.2349	1.3019	1.3530	1.4310
10.80	1.2402	1.3104	1.3710	1.4510
11.00	1.2480	1.3184	1.3770	1.4703
11.20	1.2569	1.3201	1.3630	1.4712
11.40	1.2633	1.3316	1.3373	1.4770
11.60	1.2630	1.3343	1.3243	1.4609
11.80	1.2677	1.3390	1.3152	1.4509
12.00 (core top)	1.2784	1.3524	1.3120	1.4477

Note: W(Z) values at 20000 MWD/MTU may be applied to cycle burnups greater than 20000 MWD/MTU to prevent W(Z) function extrapolation

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Table 2.6.2.b				
W(Z) versus Core Height for Expanded AFD Acceptable Operation Limits in Figure 2.8.1.b (Top and Bottom 8% Excluded per Braidwood SR 3.2.1.2 Bases)				
Height (feet)	150 MWD/MTU	6000 MWD/MTU	14000 MWD/MTU	20000 MWD/MTU
0.00 (core bottom)	1.3687	1.5187	1.4044	1.3284
0.20	1.3500	1.4804	1.3764	1.3077
0.40	1.3401	1.4656	1.3634	1.2992
0.60	1.3323	1.4519	1.3502	1.2922
0.80	1.3086	1.3749	1.3166	1.2862
1.00	1.2968	1.3553	1.2957	1.2845
1.20	1.2911	1.3406	1.2734	1.2750
1.40	1.2783	1.3387	1.2595	1.2687
1.60	1.2725	1.3241	1.2468	1.2580
1.80	1.2726	1.3064	1.2329	1.2490
2.00	1.2648	1.2877	1.2221	1.2389
2.20	1.2481	1.2671	1.2119	1.2246
2.40	1.2333	1.2435	1.2029	1.2116
2.60	1.2157	1.2170	1.1915	1.1954
2.80	1.1999	1.1966	1.1813	1.1799
3.00	1.1856	1.1870	1.1710	1.1642
3.20	1.1736	1.1795	1.1645	1.1524
3.40	1.1665	1.1745	1.1605	1.1580
3.60	1.1582	1.1673	1.1602	1.1626
3.80	1.1537	1.1617	1.1596	1.1661
4.00	1.1482	1.1546	1.1580	1.1695
4.20	1.1418	1.1454	1.1551	1.1709
4.40	1.1353	1.1373	1.1515	1.1733
4.60	1.1297	1.1271	1.1525	1.1844
4.80	1.1302	1.1175	1.1546	1.1944
5.00	1.1297	1.1078	1.1547	1.2013
5.20	1.1283	1.0994	1.1566	1.2061
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10.20	1.2025	1.2744	1.3030	1.3790
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12.00 (core top)	1.2784	1.3524	1.3120	1.4477

Note: W(Z) values at 20000 MWD/MTU may be applied to cycle burnups greater than 20000 MWD/MTU to prevent W(Z) function extrapolation

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Table 2.6.2.c Penalty Factors in Excess of 2% per 31 EFPD	
Cycle Burnup (MWD/MTU)	Penalty Factor $F^c_q(z)$
0	1.0200
150	1.0290
310	1.0375
480	1.0440
830	1.0549
1030	1.0549
1380	1.0465
2080	1.0315
2780	1.0260
3130	1.0215
3300	1.0200
9950	1.0200
10100	1.0307
11000	1.0281
11700	1.0280
12230	1.0288
13100	1.0260
13625	1.0240
14500	1.0210
14675	1.0200

Notes:

Linear interpolation is adequate for intermediate cycle burnups.

All cycle burnups outside the range of Table 2.6.2.c shall use a 2% penalty factor for compliance with the 3.2.1.2 Surveillance Requirements.

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2.7 Nuclear Enthalpy Rise Hot Channel Factor ($F_{\Delta H}^{N}$) (LCO 3.2.2)

2.7.1 $F_{\Delta H}^{N} \leq F_{\Delta H}^{RTP} [1.0 + PF_{\Delta H} (1.0 - P)]$

where: P = the ratio of THERMAL POWER to RATED THERMAL POWER (RTP)

$$F_{\Delta H}^{RTP} = 1.70$$

$$PF_{\Delta H} = 0.3$$

2.7.2 Uncertainty:

The uncertainty, $U_{F_{\Delta H}}$, to be applied to the Nuclear Enthalpy Rise Hot Channel Factor $F_{\Delta H}^{N}$ shall be calculated by the following formula:

$$U_{F_{\Delta H}} = U_{F_{\Delta H}m}$$

where:

$$U_{F_{\Delta H}m} = \text{Base } F_{\Delta H}^{N} \text{ measurement uncertainty} = 1.04 \text{ when PDMS is inoperable} \\ (U_{F_{\Delta H}m} \text{ is defined by PDMS when OPERABLE.)}$$

2.7.3 PDMS Alarms:

$$F_{\Delta H}^{N} \text{ Warning Setpoint} = 2\% F_{\Delta H}^{N} \text{ Margin}$$

$$F_{\Delta H}^{N} \text{ Alarm Setpoint} = 0\% F_{\Delta H}^{N} \text{ Margin}$$

2.8 AXIAL FLUX DIFFERENCE (AFD) (LCO 3.2.3)

2.8.1 The AXIAL FLUX DIFFERENCE (AFD) Acceptable Operation Limits are provided in the Figures described below.

- a) Figure 2.8.1.a is the Normal AFD Acceptable Operation Limits associated with the W(Z) values in Table 2.6.2.a. Prior to changing to Figure 2.8.1.a, confirm that the plant is within the specified AFD envelope.
- b) Figure 2.8.1.b is the Expanded AFD Acceptable Operation Limits associated with the W(Z) values in Table 2.6.2.b.

2.9 Departure from Nucleate Boiling Ratio (DNBR) (LCO 3.2.5)

2.9.1 $DNBR_{APSL} \geq 1.563$

The Axial Power Shape Limiting DNBR ($DNBR_{APSL}$) is applicable with THERMAL POWER $\geq 50\%$ RTP when PDMS is OPERABLE.

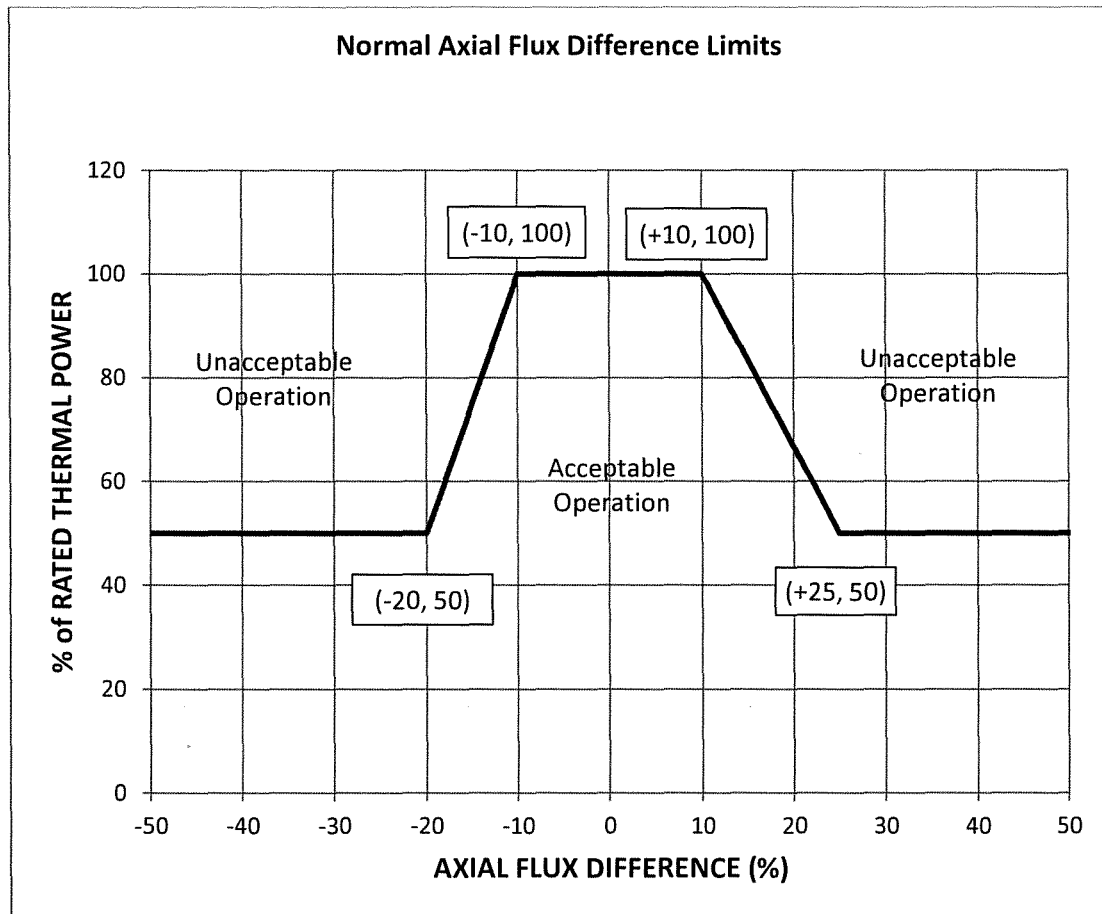
2.9.2 PDMS Alarms:

$$DNBR \text{ Warning Setpoint} = 2\% DNBR \text{ Margin}$$

$$DNBR \text{ Alarm Setpoint} = 0\% DNBR \text{ Margin}$$

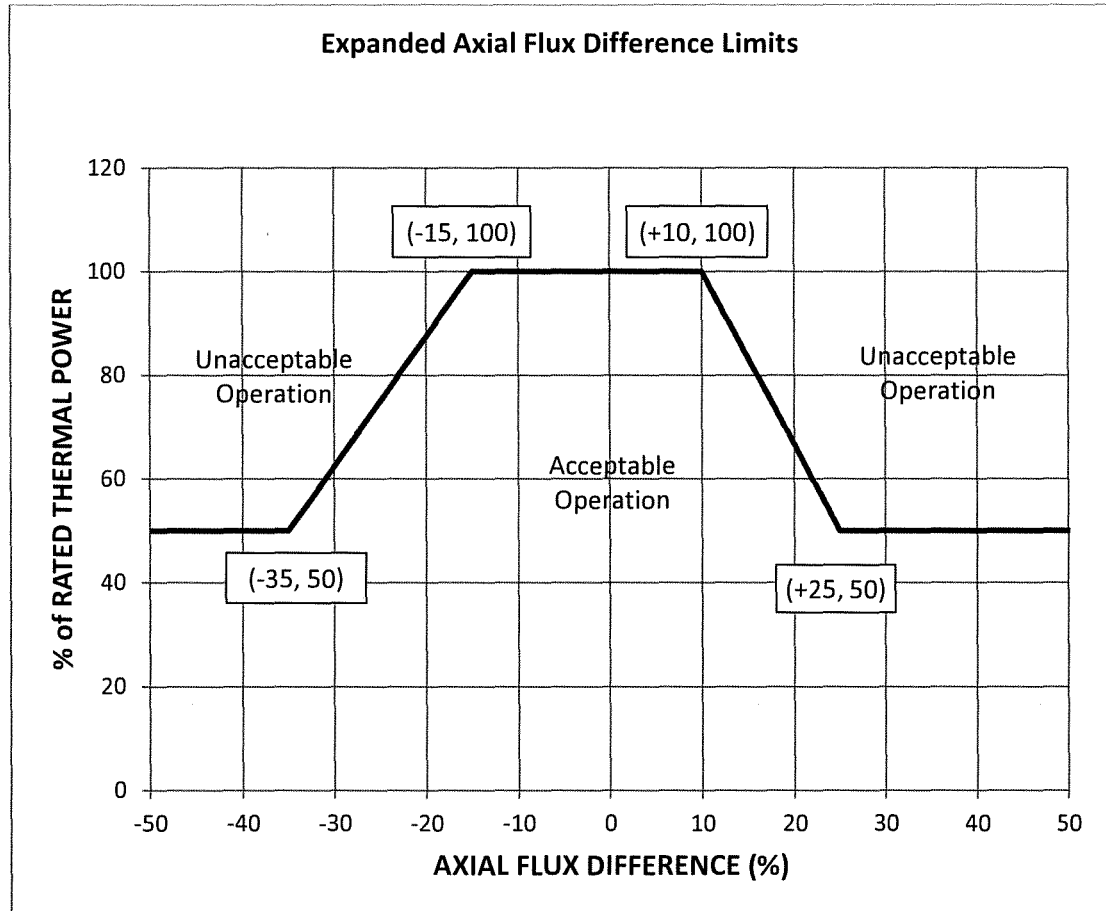
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Figure 2.8.1.a:
Normal Axial Flux Difference Limits
as a Function of Rated Thermal Power



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Figure 2.8.1.b:
Expanded Axial Flux Difference Limits
as a Function of Rated Thermal Power



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- 2.10 Reactor Trip System (RTS) Instrumentation (LCO 3.3.1) - Overtemperature ΔT Setpoint Parameter Values
- 2.10.1 The Overtemperature ΔT reactor trip setpoint K_1 shall be equal to 1.325.
 - 2.10.2 The Overtemperature ΔT reactor trip setpoint T_{avg} coefficient K_2 shall be equal to 0.0297 / °F.
 - 2.10.3 The Overtemperature ΔT reactor trip setpoint pressure coefficient K_3 shall be equal to 0.00135 / psi.
 - 2.10.4 The nominal T_{avg} at RTP (indicated) T' shall be less than or equal to 583.5 °F.
 - 2.10.5 The nominal RCS operating pressure (indicated) P' shall be equal to 2235 psig.
 - 2.10.6 The measured reactor vessel ΔT lead/lag time constant τ_1 shall be equal to 8 sec.
 - 2.10.7 The measured reactor vessel ΔT lead/lag time constant τ_2 shall be equal to 3 sec.
 - 2.10.8 The measured reactor vessel ΔT lag time constant τ_3 shall be less than or equal to 2 sec.
 - 2.10.9 The measured reactor vessel average temperature lead/lag time constant τ_4 shall be equal to 33 sec.
 - 2.10.10 The measured reactor vessel average temperature lead/lag time constant τ_5 shall be equal to 4 sec.
 - 2.10.11 The measured reactor vessel average temperature lag time constant τ_6 shall be less than or equal to 2 sec.
 - 2.10.12 The $f_1 (\Delta I)$ "positive" breakpoint shall be +10% ΔI .
 - 2.10.13 The $f_1 (\Delta I)$ "negative" breakpoint shall be -18% ΔI .
 - 2.10.14 The $f_1 (\Delta I)$ "positive" slope shall be +3.47% / % ΔI .
 - 2.10.15 The $f_1 (\Delta I)$ "negative" slope shall be -2.61% / % ΔI .

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2.11 Reactor Trip System (RTS) Instrumentation (LCO 3.3.1) - Overpower ΔT Setpoint Parameter Values

- 2.11.1 The Overpower ΔT reactor trip setpoint K_4 shall be equal to 1.072.
- 2.11.2 The Overpower ΔT reactor trip setpoint T_{avg} rate/lag coefficient K_5 shall be equal to 0.02 / °F for increasing T_{avg} .
- 2.11.3 The Overpower ΔT reactor trip setpoint T_{avg} rate/lag coefficient K_5 shall be equal to 0 / °F for decreasing T_{avg} .
- 2.11.4 The Overpower ΔT reactor trip setpoint T_{avg} heatup coefficient K_6 shall be equal to 0.00245 / °F when $T > T''$.
- 2.11.5 The Overpower ΔT reactor trip setpoint T_{avg} heatup coefficient K_6 shall be equal to 0 / °F when $T \leq T''$.
- 2.11.6 The nominal T_{avg} at RTP (indicated) T'' shall be less than or equal to 583.5 °F.
- 2.11.7 The measured reactor vessel ΔT lead/lag time constant τ_1 shall be equal to 8 sec.
- 2.11.8 The measured reactor vessel ΔT lead/lag time constant τ_2 shall be equal to 3 sec.
- 2.11.9 The measured reactor vessel ΔT lag time constant τ_3 shall be less than or equal to 2 sec.
- 2.11.10 The measured reactor vessel average temperature lag time constant τ_6 shall be less than or equal to 2 sec.
- 2.11.11 The measured reactor vessel average temperature rate/lag time constant τ_7 shall be equal to 10 sec.
- 2.11.12 The $f_2(\Delta I)$ "positive" breakpoint shall be 0 for all ΔI .
- 2.11.13 The $f_2(\Delta I)$ "negative" breakpoint shall be 0 for all ΔI .
- 2.11.14 The $f_2(\Delta I)$ "positive" slope shall be 0 for all ΔI .
- 2.11.15 The $f_2(\Delta I)$ "negative" slope shall be 0 for all ΔI .

CORE OPERATING LIMITS REPORT (COLR) for BRAIDWOOD UNIT 2 CYCLE 22

2.12 Reactor Coolant System (RCS) Pressure, Temperature, and Flow Departure from Nucleate Boiling (DNB) Limits (LCO 3.4.1)

2.12.1 The pressurizer pressure shall be greater than or equal to 2209 psig.

2.12.2 The RCS average temperature (T_{avg}) shall be less than or equal to 588.6 °F.

2.12.3 The RCS total flow rate shall be greater than or equal to 386,000 gpm.

2.13 Boron Concentration

2.13.1 The refueling boron concentration shall be greater than or equal to the applicable value given in the Table below (LCO 3.9.1). The reported "prior to initial criticality" value also bounds the end-of-cycle requirements for the previous cycle.

2.13.2 To maintain $keff \leq 0.987$ with all shutdown and control rods fully withdrawn in MODES 3, 4, or 5 (TRM TLCO 3.1.g Required Action B.2 and TRM TLCO 3.1.k.2), the Reactor Coolant System boron concentration shall be greater than or equal to the applicable values given in the Table below.

COLR Section	Conditions	Boron Concentration (ppm)
2.13.1	a) prior to initial criticality	1724
	b) for cycle burnups ≥ 0 MWD/MTU and < 16000 MWD/MTU	1820
	c) for cycle burnups $\geq 16,000$ MWD/MTU	1395
2.13.2	a) prior to initial criticality	1768
	b) for cycle burnups ≥ 0 MWD/MTU and < 16000 MWD/MTU	2022
	c) for cycle burnups ≥ 16000 MWD/MTU	1520