

November 1, 1996

Mr. Robert E. Link, Vice President  
Nuclear Power Department  
Wisconsin Electric Power Company  
231 West Michigan Street, Room P379  
Milwaukee, WI 53201

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SUBJECT: REQUEST FOR ADDITIONAL INFORMATION ON TECHNICAL SPECIFICATION CHANGE REQUEST 194, "LOW-TEMPERATURE OVERPRESSURE PROTECTION SYSTEM" AND REQUEST FOR EXEMPTION FROM THE REQUIREMENTS OF 10 CFR 50.60 - POINT BEACH NUCLEAR PLANT, UNITS 1 AND 2 (TAC NOS. M96571, M96572, M96166 & M96167)

Dear Mr. Link:

We have received your July 1, 1996, request for exemption from the requirements of 10 CFR 50.60 and your September 19, 1996 exigent Technical Specification (TS) change request 194 which proposes changing the TS for the low-temperature, overpressure protection system (LTOP). During the review, the staff determined that additional information was required. Enclosed is the request for additional information (RAI). Please provide your response to these questions by November 11, 1996, if you desire to use the proposed TS during restart from your current outage scheduled for early December. If you have any questions, please contact me at (301) 415-1380.

Sincerely,

Original signed by:

John N. Hannon, Project Director  
Project Directorate III-1  
Division of Reactor Projects III/IV  
Office of Nuclear Reactor Regulation

Docket Nos. 50-266  
and 50-301

Enclosure: RAI

cc w/encl: See next page  
DOCUMENT NAME: G:\WPDOCS\PTBEACH\PTB96571.RAI

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Mr. Robert E. Link, Vice President  
Wisconsin Electric Power Company

Point Beach Nuclear Plant  
Unit Nos. 1 and 2

cc:

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REQUEST FOR ADDITIONAL INFORMATION  
POINT BEACH EXIGENT TECHNICAL SPECIFICATION CHANGE REQUEST 194  
LOW TEMPERATURE OVERPRESSURE PROTECTION SYSTEM  
AND REQUEST FOR EXEMPTION FROM THE  
REQUIREMENTS OF 10 CFR 50.60

1. Why does operation with administrative controls on one reactor coolant pump (RCP) increase the likelihood of spurious actuation of a power-operated relief valve (PORV)? Is one RCP sufficient to provide adequate pressure to the RCP seals? Why does operation with administrative controls on two RCPs increase the likelihood of spurious actuation of a PORV? Are pressure surges associated with RCP start included in the evaluation of the expected pressure at the core midplane of 63 psig higher than the pressure at the pressure sensing points.
2. No instrument uncertainty (pressure or temperature) is accounted for in the low-temperature overpressure (LTOP) setpoints or limits. Be sure to include a discussion of the effects of temperature uncertainty on the enable temperature, bolt-up temperature, and RCP lockout temperature.
3. Does the instrument bias discussed on sheet 2 of the calculation include the static elevation pressure bias in addition to the dynamic effects of the RCPs running? Additionally, there is some effect of having one or more residual heat removal (RHR) pumps running, please provide your evaluation of the effects of running RHR pumps. There is no discussion justifying that the pressure bias values chosen for Point Beach are conservative. Please provide the basis for choosing the values used. For example, are the values generic or plant specific and what assumptions were made?
4. The Westinghouse methodology that is being used to verify the setpoints is not provided. Has the methodology been used in a topical report? If so, please provide the report number and date of the safety evaluation. If not, please provide the methodology used to calculate the pressure overshoot for both the mass and energy addition transients. Additionally, for these calculations please provide the basis for the selection of inputs (i.e., initial reactor coolant system temperature, pressure, steam generator surface area, injection flow rate, PORV flow area, inlet and outlet piping geometries, flow resistances, time delays in valve response and actuation logic) to assure the results will be conservative or limiting.

For the energy addition transient please provide greater detail why the two cases analyzed (100°F at 300psi with one RCP initially running and 250°F at 300psi with one RCP initially running) will bound all the different combinations of initial temperature, pressure and operating pumps.

5. In the determination of the new enable temperature, NRC Branch Technical Position RSB 5-2 is incorrectly referenced by stating that,

$$T_{enable} = RT_{NOT} + 90^{\circ}F.$$

The Branch Technical Position actually defines the enable temperature as the water temperature corresponding to a metal temperature of at least  $RT_{NOT} + 90^{\circ}F$  at the beltline location ( $\frac{1}{2}$  or  $\frac{3}{4}$ t). Please evaluate and account for the temperature difference between the RCS water and the ( $\frac{1}{2}$  or  $\frac{3}{4}$ t) weld location.

ENCLOSURE

6. The maximum allowable pressure is calculated for four different temperatures, 70°F, 100°F, 120°F, and 250°F, however, the steady state pressure vs. temperature curves contained in TS figures 15.3.1-1 and 2 do not appear to correspond to the same values. If this is the case, please describe where these two different sets of limit curves originate. Additionally, a new enable temperature is calculated for this submittal, please describe why the limit curves are also not re-calculated.