

11/10/77
P3
LED 213
H. W. KELLIGE COMPANY

3-3-77 Rev. 11
2-14-77 Rev. 1
1-21-77 5.

Q.A. INSTRUCTION

NUMBER 98

PROCEDURE FOR INSPECTION OF EXISTING CONCRETE
EXPANSION ANCHORS IN RANGER INSTALLATION

The following attached procedure is to be used to provide instructions for personnel performing inspections of existing concrete expansion anchors.

This instruction will not become a part of Engineering specifications, but remain a Q.A. Instruction.

J.P. Runyan
J.P. Runyan
Field Q.A./Q.C. Manager

JPR/ss

FOR INFORMATION
ONLY

PREPARED BY: T. A. SCANNELL (ENG)
J. P. RHYAN (QA/QC)
(M. W. KELLOGG)

REVISION 10 7-27-77
REVISION 11 3-3-77
REVISION 1 2-14-77
REVISION: -0
DATE: 1-17-77
X90-20

APPROVED BY:

[Signature]
Cullman Kellogg John D. Ryan 1/21/77

Page 1 of 8

PROGRAM FOR INSPECTION AND ACCEPTANCE OF EXISTING CONCRETE
EXPANSIONS ANCHORS IN PIPE HANGER INSTALLATIONS

DIABLO CANYON POWER PLANT (UNITS I & II)

PURPOSE

To determine the integrity of each anchor installation on each support and thus accept or reject. If rejected, then repair or replace.

SCOPE

This program will define the following: (Ref. CHART 1)

- I. Hangers that are to have anchors inspected.
- II. Means to provide hanger drawings.
- III. Procedure for inspection of concrete anchors.
- IV. Hanger identification and inspection assignments.
- V. The acceptance criteria.
- VI. Suggested methods of rework.
- VII. The means to perform rework.
- VIII. The acceptance of reworked anchors.
- IX. The completion and submittal of program to P.E. & E.

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APPARATUS

Refer to PERFORMANCE PROCEDURE, SECTION III.

PERFORMANCE PROCEDURE

- I. Hangers to have anchors inspected.
 - A. Large Bore design Class I, PG&E Code Class A, B, C & Section I.
 - B. Large Bore design Class I, PG&E Code Class E.
 - C. Large Bore design Class II, PG&E Code Class E.
(Individually identified by PG&E only.)
 1. P.G. & E.
 2. Grinnell
 - D. Small Bore design Class I, PG&E Code Class A, B, C & Section I.
 - E. Small Bore design Class I, PG&E Code Class E.
 - F. Anchor installations previously inspected in accordance with the requirements of "Inspection Procedure for Installed Flush Steel Concrete Anchors," by T. E. Niemi will be reviewed by the inspection coordinator to the requirements of this procedure. He will do one of the following: (1) accept as is, (2) issue for reinspection, or (3) rework to comply with the acceptance criteria of Section V of this program.
 - G. Unit II anchor installations inspected by QC (W.W. Kellogg) and having complied with hold point items 2 and 3 of the "Support Inspection Process Sheet," QA Form F-68, Rev. 4, are to be excluded from this program.
 - H. Hanger installations employing the use of anchors on plates that experience, under all conditions, no forces other than compression will be excluded from this program. In this situation the anchor is never subjected to pull out or shear forces as a result of hanger loading.
- II. Means to provide hanger drawings.

The Hanger Drawing Control Department will review every Unit I & II hanger drawing on file pertaining to each of the categories listed in Section I above. All hanger drawings incorporating the use of concrete expansion anchors will be extracted and reviewed for the latest revision; any pending Minor

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Variation or current As Built must be used if it concerns anchors. A copy will be made of each hanger drawing reflecting the latest anchor requirements. The copies of the drawings will then be separated into groups by area and elevation and given to the Inspection Coordinator.

III. Procedure for inspection of existing concrete anchors.
(See REFERENCE A)

IV. Hanger identification and inspection assignments.

The Inspection Coordinator will direct the program for locating and identifying each hanger within an area and elevation. He will issue the hanger drawings to M. W. Kellogg personnel and they will in turn locate and identify the hanger. Identification will be made by marking the base plate with the hanger symbol using either permanent ink or paint markers.

If it appears that scaffolding may be required for inspection, it will then be noted on the drawing. The drawings will then be separated into sub-groups by confinement and returned to the Inspection Coordinator.

The Inspection Coordinator in conjunction with the Production Coordinator will arrange for scaffolding and assign inspection teams to confinements. These teams will then perform inspections as defined in the Performance Procedure, Section III (See REFERENCE A).

V. Acceptance criteria.

Upon completion of the inspection and documentation of each support according to Performance Procedure, Section III (See

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REFERENCE A), the auditor will attach the hanger drawing to the Anchor Inspection Check List¹ sheet, or sheets; thus making a package. The package will then be given to the Inspection Coordinator for his review, he will do one of the following:

- (1) accept as is, according to criteria within this section,
- (2) reject and request rework per Sections VI and VII, or
- (3) when not clearly defined by acceptance criteria or in any other way questionable, submit to QA/QC Manager or his appointee for his disposition.

The QA/QC Manager or his appointee will, upon receipt and review of the package from the Inspection Coordinator, either return it to the Inspection Coordinator with defined rework, accept it as is, or transmit to P.G. & E. for their disposition.

Failure of one or more anchor installations to meet the following requirements will result in the necessity to rework.

A. Expander plug driven dimensions.

Plug depths are to be within the following minimum and maximum tolerances to be acceptable for each anchor recorded on the Anchor Inspection Check List.

TABLE I

SEE PAGE 4A OF 8 FOR TABLE 1.

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¹ Performance Procedure, Section III - Reference A, Attachment 3

ACCEPTANCE CRITERIA

PAGE 4A of 8

OFFICE & REWORKREV. 3-3-77 *for RDC*
REV. 7-27-77 *for RDC*TABLE 1MEASURED WITH GAUGE

<u>SIZE</u>	<u>HILTI</u>			<u>PHILLIPS</u>		
	<u>MIN.</u>	<u>FULL**</u>	<u>MAX.</u>	<u>MIN.</u>	<u>FULL**</u>	<u>MAX.</u>
1/2	2 22/32	2 27/32	3 3/32	* 23/32	2 25/32	2 29/32
5/8	3 3/32	3 11/32	3 19/32	* 26/32	3 13/32	3 20/32
3/4	* 1 16/32	3 29/32	4 7/32	1 3/32	4 1/32	4 6/32
7/8	-----	-----	-----	1 13/32	4 8/32	4 14/32

HILTIPHILLIPS* MEASURED WITHOUT GAUGE

<u>SIZE</u>	<u>MIN.</u>	<u>FULL**</u>	<u>MAX.</u>	<u>MIN.</u>	<u>FULL**</u>	<u>MAX.</u>
1/2	31/32	1 6/32	1 12/32	23/32	1 5/32	1 9/32
5/8	1 3/32	1 13/32	1 19/32	26/32	1 12/32	1 19/32
3/4	1 16/32	1 30/32	2 4/32	1 4/32	1 25/32	1 30/32
7/8	-----	-----	-----	1 14/32	2 7/32	2 13/32

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Add 2" to the above dimensions when alternate test gauge was used, refer to Reference A, Attachment 6.

*Measurement taken from top of shield to top of plug, refer to reference A, Paragraph 6.3.8.

B. Angular misalignment of anchor.

0° - 5° Deviation from perpendicular to the plane of the plate is acceptable.

6° - 15° Is acceptable provided the anchor is otherwise ~~unmodified and the expander plug is driven to "Full"~~ dimension in Table 1.

+15° Is unacceptable.

C. Anchors with thread end cut off.

Both Phillips and Hilti are acceptable if the thread end is cut off provided there are at least four (4) full threads remaining. In addition, the plug must be driven to within the "Min" and "Max" dimensions for Hilti anchors and within the "Max" and "Full" dimensions for Phillips anchors given in Table 1. It is also necessary to be within the 0° - 5° range (Reference Paragraph D, above), and no other modifications have been discovered.

D. The following miscellaneous conditions are unacceptable.

1. Stripped threads in anchor preventing bolt tightening.
2. Plate interference with bolt installation or removal.
3. Loose anchors.
4. Anchors with incorrect expander plug.

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E. Undersized anchors (diameter).

When an anchor is found to be undersized, the Anchor Inspection Check List will indicate this condition. The Inspection

Coordinator will submit all such drawing packages to the QA/QC Manager or his appointee for disposition to rework or transmit to P.G. & E. for their disposition.

F. All packages containing one or more inaccessible anchors will be submitted to the QA/QC Manager or appointee by the Inspection Coordinator for transmittal to P.G. & E. for disposition.

G. Unmodified anchors overembedded 1/2 inch or less are acceptable.

VI. The suggested methods of rework.

When an anchor installation is determined unacceptable by the acceptance criteria Section V, then rework will result. The following are suggested methods of rework to be employed.

- A. Install a new anchor either a kwik bolt (Hilti) or a wedge anchor (Phillips) of the same bolt diameter as the originally required anchor. The relocation installation will be made in accordance with ESD-223, paragraph 3.2.1.1 and the shield of the unacceptable anchor may be considered comparable to grout if left installed. This may be done by drilling through the plate and into the concrete and installing to manufacturer's recommended procedure.
- B. Remove the unacceptable anchor and replace with a new one of the size originally required. A Hilti expansion anchor may be removed by drilling through the plug and extracting same. The anchor shield is then readily removed. A Phillips expansion anchor may be removed by using an all

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thread rod with threads removed from one end. Thread this modified rod into the anchor slowly and thereby extract the anchor shield. Remove the plug from hole. In both Hilti and Phillips anchor removal, either the base plate will have to be removed, or the hole in the plate enlarged enough to remove the unacceptable anchor.

- C. If due to inaccessibility the rework described in Paragraphs A and B, above, cannot be performed, contact the Chief Field Engineer or his appointee for disposition.

VII. The means to perform rework.

The Inspection Coordinator will initiate the issuance of any and all rework. He will log the rework package out to the Production Coordinator who will determine which type of rework (See Section VI) can be employed with the most expediency and best results. The Production Coordinator will then assign fitter work crews to rework items per Section VIII.

VIII. Acceptance of reworked anchors.

When rework requires the installation of a new anchor, the fitter performing the work shall notify the QC auditor. The auditor will witness the installation of the anchor assuring that the requirements of ESD-223, Paragraph 3.2.1.1 and Paragraph 3.2.1.2 and the attached QA Instruction, Number 97 are met.

When the installation is complete, the auditor will indicate "Rework Complete", stamp "Accept", initial and date the Anchor Inspection Check List; he will then return the Anchor Inspection Check List and hanger drawing to the Inspection Coordinator for incorporation into the final package.

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ONLY

IX. The completion and submittal of program to P.G. & E.

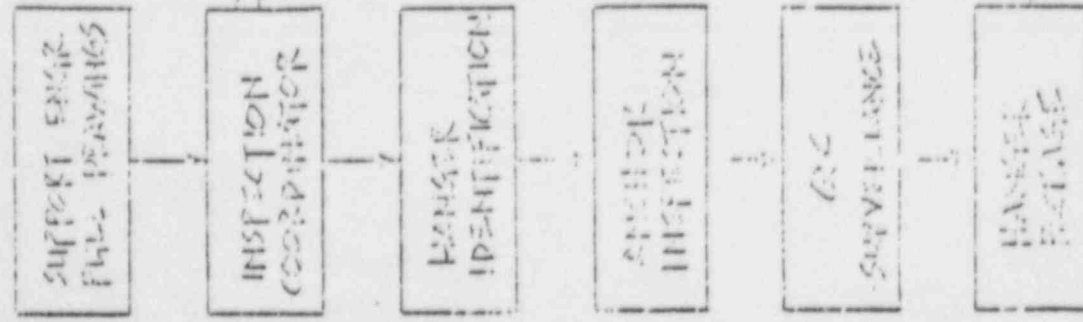
When all inspection and required rework is complete, the "Accept" packages will be segregated by area and elevation, indexed and boxed.

Indexing will be numerically by hanger symbol number.

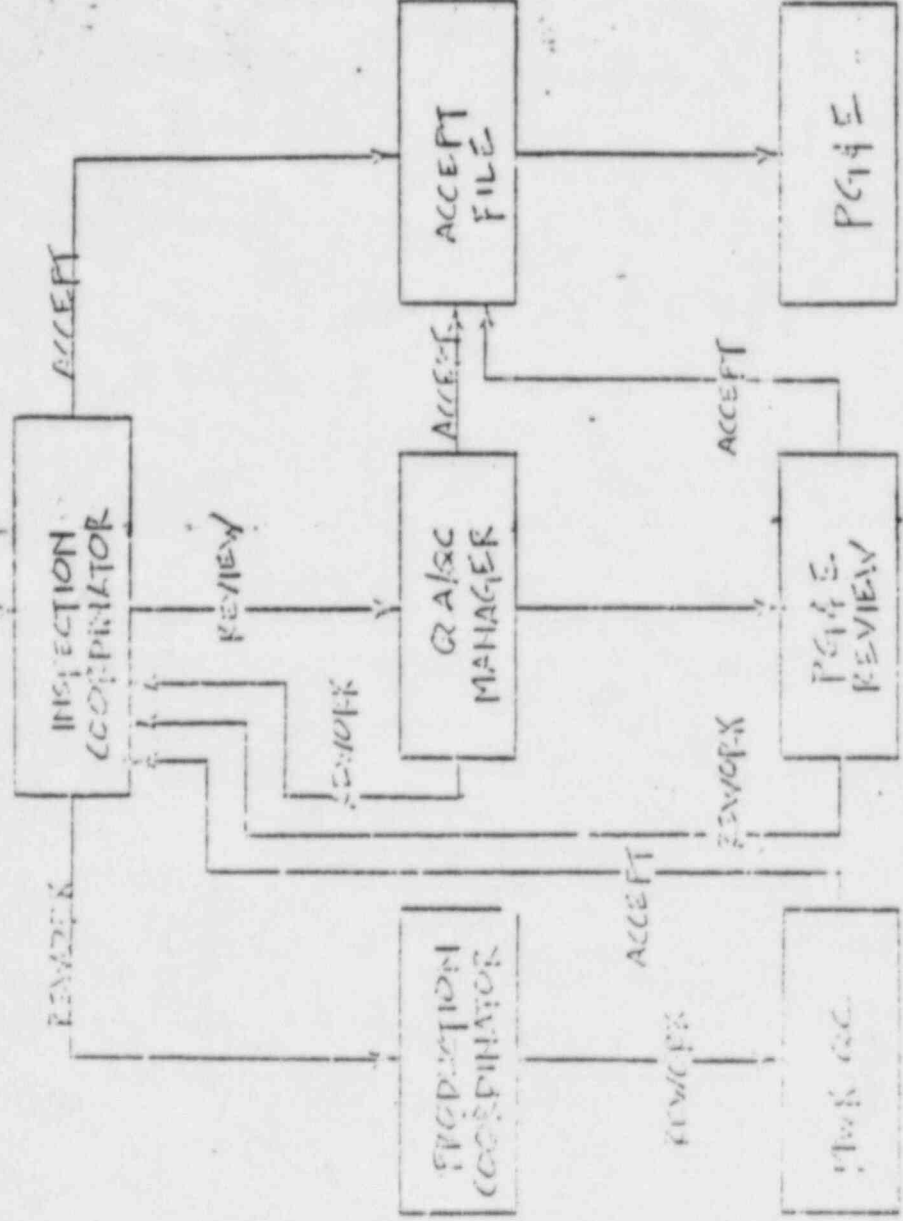
These boxes will then be transmitted to P.G. & E.

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PGandE RESOLUTION SHEET

IDVP FILE NO: 1016

1. Description of Concern

- [X] Open Item with future action by PGandE
[] Deviation
[] Class ____ Error
Description: *... CONCERN*

Description:

1 Class _____ Error
Description: RELIANT ASSOCIATES IS CONCERNED THAT THE CONCRETE ANCHOR ALLOW
ON PAGE DWG. 054162 DO NOT AGREE WITH DEM-M9, APPENDIX C.

2. Significance of Concern

- Discrepancy Report # _____ initiated
Nonconformance Report # _____ initiated
Discrepancy Report or Nonconformance Report not required.
Yes [X] No Are there any (generic) items?

Comments:

[X] No Are there any (generic) items?
CORRECT DESIGN CRITERIA FOR CONCRETE ANCHORS. CANNOT BE DETERM.

3. Description of Resolution

Description of Resolution

ADDRESS THE DIFFERENCES BETWEEN THE TWO STANDARDS AND PROVIDE THE SAFETY FACTORS REPRESENTED IN DWG. 054162

4. Description of Physical Modifications

- ☐ Yes ☒ No Will physical modifications be required?
Scheduled Completion Date:
Description:

Description:

Task Leader

Group Leader

ONLY

<u>1. Unkaid</u>	<u>6/18/82</u>
<u>JK We Sell</u>	<u>Date</u>
<u>Fatty A. Mowry</u>	<u>6/24/82</u>
	<u>Date</u>

ATTACHMENT 6

PGandE Completion Sheet
IDVP File No: _____

1. Description of Concern

- ☒ Open Item with future action by PGandE
☐ Deviation
☐ Class _____ Error

Description:

RL CLOUD ASSOCIATES IS CONCERNED THAT THE CONCRETE ANCHOR ALLOWABLE ON PG&E DWG. 054162 DO NOT AGREE WITH DCM-M9, APPENDIX C.

2. Significance of Concern

- ☐ Discrepancy Report # _____ initiated
☐ Nonconformance Report # _____ initiated
☒ Discrepancy Report or Nonconformance Report not initiated
☐ Yes ☒ No Are they any related (generic) items?

Comments:

CONCRETE DESIGN CRITERIA FOR CONCRETE ANCHOR CANNOT BE DETERMINED

3. Description of Completion

ADDRESS THE DIFFERENCES BETWEEN THE TWO STANDARDS AND PROVIDE SAFETY FACTORS REPRESENTED IN DWG. 054162

4. Description of Physical Modifications

- ☐ Yes ☒ No Were physical modifications required?

Completion Date:

Description:

Task Leader

Michael K. [Signature] 6/18/82
Date

Group Leader

Fathy A. Mossy 6/24/82
Date

Verification Program Manager

Date

PACIFIC GAS AND ELECTRIC COMPANY
ENGINEERING DEPARTMENT
DESIGN CALCULATION COVER SHEETS

File No. 52.7.11.5.8

Calculation No. EDS 1016

Project Diablo Canyon Date 6-23-82

Engineering Discipline CIVIL

Structure, System, or Component ELECTRICAL RACEWAY SUPPORTS

Type of or Purpose of Design Calculations _____

RESOLVE RLCR EDS 1016

No. of Sheets 36

SAR change required ☐ Yes ☒ No
(Nuclear Projects only)

	Signature	Discipline/Dept	Date
Preparer	<u>[Signature]</u>	<u>Civil</u>	<u>6/23/82</u>
Checker	<u>[Signature]</u>	<u>CIVIL</u>	<u>6/23/82</u>

Approval:

	Signature	Discipline/Dept	Date
Discipline Engineer (if required)	<u>Fathy A. Morsy</u>	<u>Civil</u>	<u>7/6/82</u>
Group Leader/Supervisor	_____	_____	_____

Record of Revisions

Rev.No.	Date	Reason for Revision	Rev.by	Checked by	Approval	
					Engr	GL/Supr

GENERAL COMPUTATION SHEET

SHEET NO. 1 OF 26 SHEETS

JOB } NO. 52.7.11.58

FILE } LOCATION

SUBJECT

E01 1016

Diablo Canyon Power Plant Project

MADE BY

Mike Jan

DATE

6/16/82

CHECKED BY

MNP

APPROVED BY

TABLE OF CONTENT

I. OBJECTIVE

II. RESOLUTION

III. APPENDIX

a. APPENDIX A

b. APPENDIX B

c. APPENDIX C

d. APPENDIX D

FOR ONLY

SUBJECT EOI 1016
Diablo Canyon Power Plant Project
MADE BY Mike Gaur DATE 6/16/82 CHECKED BY MNP APPROVED BY _____

1. Objective:

This documentation is to resolve a RLCA Open Item (EOI 1016).

Robert L. Cloud Associates is concerned that the concrete anchor allowables on P.G. & E. drawing 054162 Rev. 3 do not agree with those on DEM-M9, Appendix C, Rev. 7; therefore, the correct design criteria for concrete anchor cannot be determined (See Appendix A). This documentation will address the difference between the two standards and will provide the safety factors represented in drawing 054162.

ONLY

SUBJECT E01 1016
Diablo Canyon Power Plant Project
MADE BY Mike [signature] DATE 6/16/82 CHECKED BY MNP APPROVED BY _____

I. Resolution:

Drawing 054162 (see Appendix B) is a P.G. & E. Engineering Standard which was first developed in 1973. It provides guidelines for the use of concrete anchors within P.G. & E. system, including those used in Diablo Canyon Project.

Design Criteria Memorandum DCM-119, Rev. 4 was issued in November 1981 for design verification of class pipe supports in Diablo Canyon.

Whereas DCM-119 was developed to insure compliance with NRC I-E Bulletin 79-02 for pipe supports, Engineering Standard Dwg. 054162 provides reasonably conservative allowable loads for all other applications of concrete anchors throughout the P.G. & E. system, including the Diablo Canyon Project.

Test results of various anchor types and sizes have been assembled (see Appendix C). Results of 4

SUBJECT EOI 1016
Diablo Canyon Power Plant Project

MADE BY Mike Jan DATE 6/18/82 CHECKED BY MNP APPROVED BY _____

1. Resolution (Cont.)

Concrete anchor sizes have been plotted for graphic presentation (see Appendix D). Based on the data available, the average safety factors of allowable loads on Div. 054162 for all the anchor sizes ^{other than pipe supports} used in Diablo Canyon Project have been summarized in table below:

Anchor Diameter (inch)	Safety Factors									
	$f'_c = 2 \text{ ksi}$		$f'_c = 3 \text{ ksi}$		$f'_c = 4 \text{ ksi}$		$f'_c = 5 \text{ ksi}^*$		$f'_c = 6 \text{ ksi}$	
	P	S	P	S	P	S	P	S	P	S
1/4	7.25	5.86	9.02	7.13	8.21	7.57	7.72	8.44	6.90	9.07
3/8	7.34	7.55	7.20	7.10	7.12	7.68	6.6	8.42	5.87	8.90
1/2	5.55	7.84	6.01	7.42	6.15	7.52	6.15	7.33	6.09	6.97
5/8	4.51	8.78	4.72	7.12	5.03	7.92	4.55	7.57	3.85	7.09
3/4	4.30	7.95	4.64	6.83	5.05	8.14	4.66	7.93	4.19	7.54

* No test data available for 5 ksi concrete. Safety factors obtained by interpolating test data of 4 ksi & 6 ksi strength concrete

GENERAL COMPUTATION SHEET

SHEET NO. 5 OF 36 SHEETS
JOB FILE NO. 52-7-11.5
LOCATION 2-11-5

SUBJECT EOI 1016
Diablo Canyon Power Plant Project
MADE BY Mike Gm DATE 6/16/82 CHECKED BY MNP APPROVED BY _____

II. APPENDIX

a. APPENDIX A

10-11-82

ERROR AND OPEN ITEM SHEETAPPENDIX A

1. Classification

☐ Error
or
☒ Open Item

Error Classification
☐ Class (A, B, C, or D)

2. Description

The anchor allowables on PGandE drawing 054162 Revision 3 do not agree with those on DCM-M9, Appendix C, Revision 7.

3. Significance

The correct design criteria for anchor bolts cannot be determined.

4. Recommendation

PGandE to address the differences between the two standards.

5. Reported

☒ PGandE
☐ NRC

Transmittal Date 2/11/82

Ref. & Date _____

6. Final Resolution

Frank Long 2/4/82
Signed/Date

Edward Dorison 2/11/82
Project Engineer/Date
Prior to Release
ok Ric

Project Administrator/Date

ROBERT L. CLOUD ASSOCIATES, INC.
125 UNIVERSITY AVENUE
BERKELEY, CALIFORNIA 94710
(415) 841-8286

CONC,
EXP,
ANCHOR
RECEIVED BY R. R. FRAY
MAR 10 1982
D.C. VERIFICATION
PROGRAM MANAGER
log # 105
sh. 7 1/2

March 10, 1982

F 105-4

Mr. Roy Fray
Diablo Canyon Verification
Program Manager
Pacific Gas and Electric Company
77 Beale Street
San Francisco, CA 94106

APPENDIX A

Dear Mr. Fray:

Please address EOI 1016 by listing the safety factors represented
in drawing 054162.

Yours truly,

Edward Denison

Edward Denison

ONLY

slit. 8/2

ROBERT L. CLOUD ASSOCIATES, INC.
125 UNIVERSITY AVENUE
BERKELEY, CALIFORNIA 94710
(415) 841-9296

RECEIVED BY R. R. FRAY

APR 19 1982

D.C. VERIFICATION
PROGRAM MANAGER

log #184

APPENDIX A

April 16, 1982

P 105-4

Mr. Roy Fray
Diablo Canyon Verification
Program Manager
Pacific Gas and Electric Company
77 Beale Street
San Francisco, CA 94106

Dear Mr. Fray:

Please find attached a list of documents that Robert L. Cloud Associates needs to have formally transmitted from PGandE for the Seismic Verification Program.

Yours truly,

Edward Denison

Edward Denison

Attachment

Request Number 163

ONLY

To Roy R. Fray
Diablo Canyon
Verification Program Manager

Request No. 163

Requested by Edward Denison

Date 4/16/82

Attention of: ☒ Civil/E.P. Wollak
☐ Drawings and Records/D.E. Peazant
☐ Electrical/W. Vahlstrom
☐ I&C/T.N. Crawford
☐ Mechanical Systems/R.M. Lavery
☐ Piping/M.R. Tresler
☒ R. Fray - EOI 1016

APPENDIX A

Please provide the following Drawings/Documents for use in the
Diablo Canyon Verification Program:

safety factors represented in
drawing 054162

ATTACHMENT 1

sl.
DCVP PROCEDURE NO: 1
REVISION: 1
DATE: 3-4-82

TO: R.P. WOLLAK

FROM: Verification Program Manager

APPENDIX A

FILE: M&NE - 1.061 Cloud Seismic Verification Program

SUBJECT: Request for Information for a DCVP consultant.

Consultant: Robert L. Cloud Associates, Inc. Request No: 163

A. Please supply the following information:

1. See attached Request for Information

2. _____

3. _____

4. _____

Please notify by Telepho
only as soon as request
fulfilled; Ext. 3377

B. Name of Requester RLCA/Dennis Peazant

Extension

C. Date of Request

4/16/82

D. Form of Request: Telephone _____

Letter (attached) _____

X

E. Remark:

ONLY

ATTACHMENT 2

DCVP PROCEDURE NO: _____

REVISION: 1

DATE: 3-4-82

File No. 52.7.11.4.3

ht. 11/31

TO: Verification Program Manager

FROM:

FILE: M&NE - 1.061 Cloud Seismic Verification Program

SUBJECT: Request for information for a DCVP Consultant.

Consultant: Robert L. Cloud Associates, Inc. Request No: 163

A. List of information attached:

1. Safety factors represented in P.E. & Dwg 054162
2. Plots of test data
3. References of test data
4. _____

B. Name of Person Supply Information Mike Yan Extension 8-4879

C. Name of Person Checking Information Neeraj Punglia Extension 8-6220

D. Remarks:

Design Drafting
62-3690

PACIFIC GAS AND ELECTRIC COMPANY

GENERAL COMPUTATION SHEET

SHEET NO. 12 OF 36 SHEET
JOB FILE NO. 52.7.11.5.8
LOCATION

SUBJECT

EOI 1016

Diablo Canyon Power Plant Project

MADE BY

Mike Yan

DATE

6/16/82

CHECKED BY

MNP

APPROVED BY

II. APPENDIX

b. APPENDIX B

ONLY

SKT. K

A.2.9 For anchors which will be subjected simultaneously to pullout and shear forces, the allowable load values used must satisfy the following formula (Figure 1):

$$\left(\frac{P_C}{P_D}\right)^{5/3} + \left(\frac{S_C}{S_D}\right)^{5/3} \geq 1$$

Where P_D , S_D = allowable loads (pullout, shear), reduced for spacing or edge distance if appropriate

P_C , S_C = allowable loads to be used in cases where pullout and shear loads may occur simultaneously

Note: For convenience in calculation, exponents in the above formula may, conservatively, be reduced to 1.0.

TABLE A
ALLOWABLE LOAD (KIPS) ON EXPANSION ANCHORS

NOMINAL DIAMETER (INCH)	CONCRETE STRENGTH, f'_c									
	2 ksi		3 ksi		4 ksi		5 ksi		6 ksi	
	P	S	P	S	P	S	P	S	P	S
1/4	.25	.30	.275	.30	.30	.30	.325	.30	.35	.30
3/8	.40	.54	.50	.60	.60	.67	.70	.73	.80	.80
1/2	.70	.74	.87	.89	1.05	1.04	1.23	1.19	1.40	1.34
5/8	1.20	1.00	1.50	1.25	1.80	1.50	2.10	1.75	2.40	2.00
3/4	1.80	1.50	2.35	1.80	2.90	2.10	3.45	2.40	4.00	2.70
7/8	2.50	2.00	3.35	2.35	4.20	2.70	5.05	3.05	5.90	3.40
1	3.30	2.50	4.30	2.90	5.50	3.30	6.60	3.70	7.70	4.10
1 1/4	5.30	3.40	6.65	3.95	8.00	4.50	9.35	5.10	10.70	5.70

NOTE: P, PULLOUT; S, SHEAR

For expansion anchors installed in lightweight aggregate concrete, assume $f'_c = 2$ ksi. See par. A.2.6.

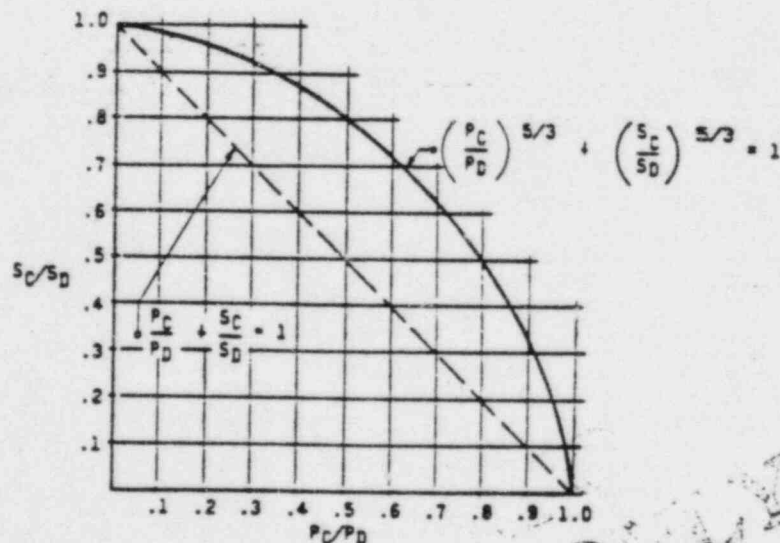


FIGURE 1
REDUCTION FACTORS FOR COMBINED PULLOUT AND SHEAR

sh. 15/36

B. INSTALLATION

B.1.0 APPLICATIONS

B.1.1 Provisions of this standard shall apply to the following concrete expansion anchors. Other expansion anchors shall not be used without specific authorization of the Engineer.

SHELL ANCHORS: • PHILLIPS SELF-DRILLING, PHILLIPS NONDRILLING, DIAMOND, HILTI HDI, RAWL SABER-TOOTH,

STUD ANCHORS: • KWIK-BOLT, PARABOLT, PHILLIPS WEDGE, PHILLIPS SLEEVE, WEJ-IT ANKR-TITE.

• PHILLIPS STUD ANCHOR may be used in sizes up to 1/4" diameter.

• WEJ-IT (original style, with spade-shape wedges) may be used, provided embedment is 125% of that shown in Table B, with 50% of the allowable load values shown in Table A.

B.1.2 Anchors must be at least 1/2" diameter when used for structural connections or for anchorage of pipes, conduits or ducts greater than 2" diameter.

B.1.3 Anchors shall not be installed in prestressed concrete elements nor used to connect concrete elements which must have a specific value of fire resistance.

B.2.0 INSTALLATION

B.2.1 Installation of anchors shall be according to manufacturer's instructions as to tools, torque and tightening procedure.

B.2.2 If a hole cannot be drilled to the correct depth (e.g., if reinforcing steel is encountered while drilling), a new hole shall be drilled. There shall be at least 1/2" of sound concrete between abandoned hole and new hole. If an unused hole is within 4.5 nominal diameters of an expansion anchor, center to center, the unused hole shall be filled with grout or with an expanded anchor.

B.2.3 If axis of a drilled hole deviates from normal to concrete surface by more than 5° the hole shall not be used unless specifically authorized by the Engineer.

B.2.4 Minimum required embedment, for shell type anchors, is equal to the length of shell. For most shell anchors the shell may be recessed not more than 1/4 of the nominal diameter. Installed shells recessed to greater depths shall not be used unless specifically authorized by the Engineer.

Minimum required embedment for stud type anchors is given in Table B.

Embedment length is exclusive of thickness of any grout pad or other overlay.

B.2.5 Anchors shall be installed according to manufacturer's instructions. If, after starting from finger-tightened position, anchor slips more than 10% of minimum required embedment while being tightened, one of the following remedial actions shall be taken:

- Remove bolt or nut, reset anchor, repeat tightening;
- Remove anchor, substitute larger diameter or longer anchor;
- Drill new hole and install additional anchor which satisfies the requirements of this standard.

B.2.6 Anchor spacing, center to center, shall be not less than 6 times nominal diameter of anchor nor shall edge distance be less than 3 times nominal diameter nor less than 3 inches unless specifically authorized by the Engineer.

B.2.7 If edge of concrete is chamfered, edge distance shall be measured from nearest edge of chamfer.

B.3.0 PROOF LOADING

When required by the Engineer, proof loading shall be done according to the following instructions:

B.3.1 Whenever an installation crew starts installing anchors at a job site, each of the anchors installed by that crew shall at first be proof loaded in tension to 250% of the allowable pullout load designated by the Engineer. After five successive anchor installations have been completed without failure, a random selection of 10% of the anchors of each size installed by the crew thereafter on the same project shall be tested in the above manner.

4/16/36

8.3.2 If proof loading is done by jacking against a surface area of concrete surrounding the anchor, the jacking pressure shall be distributed over an annular area of inner diameter at least 3 times the minimum required embedment given in Table 8.

8.3.3 Criteria for failure of an anchor during proof loading are:
(1) concrete cracks; (2) anchor breaks, or (3) anchor slip during the test is greater than 5% of the minimum required embedment.

TABLE 8
MINIMUM EMBEDMENT REQUIRED FOR STUD-TYPE
EXPANSION ANCHORS INSTALLED IN CONCRETE

Nominal Diameter (inches)	Minimum Embedment (inches)
1/4	1-1/8
3/8	1-3/4
1/2	2-1/4
5/8	2-7/8
3/4	3-3/8
7/8	4
1	4-1/2
1-1/4	5-5/8

SUBJECT EOI 1016
Diablo Canyon Power Plant Project
MADE BY Mike Yan DATE 6/16/82 CHECKED BY MNP APPROVED BY _____

II. APPENDIX

C. APPENDIX C

References of Test Data:

1. Pittsburgh Testing Laboratory (PTL) Report No. 93110 (1956)
and 94277 (1958)
2. PTL Report No. 96844, 96902, 97562 (1962)
3. PTL Report No. 99009 (1963)
4. PTL Report No. 100019, 100037 (1964)
5. Phillips Dril Company, Reported by T.G. Bixby (1964);
see also Phillips Dril Co. Brochure (1970) citing reports
from PTL and Smith-Emery Co.
6. PTL Report No. 105228 (1971).
7. Abbott A. Hanks Testing Laboratories, Report No. 8783K (1973).
8. Abbott A. Hanks Testing Laboratories, Report No. 6099 (1977).



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APPENDIX C

Ref. 1

ORDER No. CH-3071, CH-4457

LABORATORY No. 93110 (10-31-56)
94277 (6-30-58)

CLIENT'S No. PO-5903P, 821

REPORT
(Consolidated)

TESTS OF: RED HEAD SELF-DRILLING CONCRETE ANCHORS

Cat. No.	Bolt Size	PULLOUT TESTS			SHEAR TESTS		
		Tensile Load, Lbs.	Average Load, Lbs.	Type of Failure	Shear Load, Lbs.	Average Load, Lbs.	Type of Failure
S-14	1/4"	3,728 331%	4,009 355%	Concrete Failed Concrete Failed Anchor Pulled Out*	1,000 82%	1,363 821%	4.5 Bolt, Shear Bolt, Shear Bolt, Shear
		5,125 417%			1,550 137%		
		3,175 282%			1,540 136%		
S-16	1/4"	4,625 410%	4,425 393%	Concrete Failed Concrete Failed Concrete Failed	1,930 171%	2,073 184%	Bolt, Shear Bolt, Shear Bolt, Shear
		5,025 446%			2,240 197%		
		3,625 322%			2,050 182%		
S-38	3/8"	6,125 544%	6,175 548%	Concrete Failed Concrete Failed Concrete Failed	3,270 290%	3,443 305%	5.2 Bolt, Shear Bolt, Shear Bolt, Shear
		6,425 570%			3,320 294%		
		5,975 530%			3,740 332%		
S-12	1/2"	9,809 671%	9,259 825%	Concrete Failed Concrete Failed Anchor Pulled Out*	6,660 391%	6,856 609%	6.8 Bolt, Shear Bolt, Shear Bolt, Shear
		9,109 609%			7,020 623%		
		8,859 786%			6,890 612%		
S-58	3/4"	15,025 131%	12,758 1133%	Concrete Failed Concrete Failed Anchor Pulled Out*	12,160 1020%	12,153 1079%	8.4 Bolt, Shear Bolt, Shear Bolt, Shear
		11,075 983%			11,500 921%		
		12,175 1072%			12,800 1137%		
S-34	3/4"	17,325 153%	17,675 1570%	Concrete Failed Concrete Failed Concrete Failed	14,600 1247%	16,516 1467%	8.1 Bolt, Shear Bolt, Shear Bolt, Shear
		17,675 1574%			17,400 1545%		
		18,025 1621%			17,550 1557%		
S-78	3/4"	19,025 1690%	19,442 1727%	Concrete Failed Concrete Failed Concrete Failed	18,250 1674%	18,816 1671%	7.1 Bolt, Shear Bolt, Shear Bolt, Shear
		20,725 1840%			18,900 1678%		
		18,575 1650%			18,700 1671%		
T-32	Wire			WIRE BROKE			

CONCRETE USED FOR TESTS RANGED FROM 3125 TO 4280, OR AN AVERAGE OF 3700.

*Anchor capacities where "Anchor Pulled Out" were substantially the same as in the case of concrete failures, or higher.

$$P_A = \frac{P_u}{P_A} \quad f'_c = 3.5 \text{ ksi Reduced to } 3.0 \text{ ksi}$$

Procedure for tensile tests was axial loading until ultimate failure of concrete or anchors. Procedure for shear tests was loading to a steel plate bolted to the anchors in a plane perpendicular to the axis of the anchor. Concrete blocks used for tests were of a 1:3:5 mix, having a compressive strength as indicated in each table at 28 days. Compressive strengths were checked using standard 6" x 12" test cylinders.

NOTE: Tests show ultimate total loads — not safe working loads. See manufacturer's recommended safety factors.

$$P_A = P_{A3} + .802(P_{A4} - P_{A3})$$

P_{A3}, P_{A4} = allowable load from Table A, Dug 054162, at $f'_c = 3, 4$ ksi, respectively

PITTSBURGH TESTING LABORATORY

W. H. Levelius, District Manager



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ORDER No.

CH 6677 - CH 6758

CLIENT'S No.

F. Verstein

LABORATORY No. 96844, 96902
97562

APPENDIX C

Ref. 2

REPORT

March 23, 1962

PULLOUT TESTS OF ~~ANCHORS~~ NON-DRILLING CONCRETE ANCHORS

for

PHILLIPS DRILL COMPANY
MICHIGAN CITY, INDIANA

Anchor Size	Pullout Load, lbs.	Average lbs.	P_u/P_a
1/4"	2810 2860 2680 3300	2912	0.34162
3/8"	5450 4550 4600 4700	4825	10.1
1/2"	8140 7520 7320 7500	7620	8.8
5/8"	12000 11400 10600 11280	11570	7.9
			7.0

* Block cracked diagonally. On all other tests, a conical concrete disc failed. Size of concrete spall recorded by client.

$f'_c = 3.51$

Respectfully submitted,

PITTSBURGH TESTING LABORATORY

W. H. Lovellius,
District Manager

3cc: Client

WHL/rg

Average f'_c

Manufacturers recommended safe working load in 3500 PSI concrete - 25% of the average pull-out loads shown above.
NOTE: Tests were made in concrete blocks having compressive strength ranging from 2460 to 3840 PSI.

* Currently being marketed as Red Head Non-Drill Anchors.

Phillips Drill Co., Michigan City, Indiana



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APPENDIX C

Ref. 3 41.2

ORDER NO. CH 7899

CLIENTS No. 9823

LABORATORY No. 99009

September 30, 1963

REPORT

PULLOUT AND SHEAR TESTS FOR "STUD ANCHORS"

for

PHILLIPS DRILL COMPANY, MICHIGAN CITY, INDIANA

TENSILE TESTS

Anchor Diameter	Pullout Load, Lbs.	P_A	Pullout Average	$\frac{P_A}{P_A}$	Type of Failure
1/4"	2370	300	2660	8.9	Concrete Failed
	2850				Concrete Failed
	2750				Concrete Failed
3/8"	4210	590	4290	7.3	Concrete Failed
	4710				Concrete Failed
	3950				Concrete Failed
1/2"	6220	1030	5620	5.5	Concrete Failed
	4850				Concrete Failed
	5780				Concrete Failed

SHEAR TESTS

Anchor Diameter	Shear Load, Lbs.	S_A	Shear Average	$\frac{S_A}{S_A}$	Type of Failure
1/4"	2260	300	2020	6.7	Stud Sheared
	1940				Stud Sheared
	1850				Stud Sheared
3/8"	4660	660	5170	7.8	Stud Sheared
	5590				Stud Sheared
	5270				Stud Sheared
1/2"	8500	1025	8710	8.5	Stud Sheared
	9180				Stud Sheared
	8440				Stud Sheared

Concrete used for above tests averaged 3910 psi compressive strength.

$$P_A = P_{A3} + .910 \cdot (P_{A4} - P_{A3})$$

f_c

PITTSBURGH TESTING LABORATORY

W. H. Levelius, District Manager

3cc: Client

Manufacturers recommended safe working load in 3500 PSI concrete — 25% of the average pull-out loads shown above.

* Currently being marketed as Red-Head Stud Anchors.



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ORDER NO. CH 8539

CLIENT'S NO.

REPORT

LABORATORY No. 100019, 100037

9-30-64

APPENDIX C

Ref. 4

Tests of:

Concrete Anchors

Reported to:

The Phillips Drill Co.
Michigan City, Indiana

In accordance with your instructions we have completed Pull-Out and Shear tests of anchors identified as:

- 1) Phillips Red Head Non Drill Anchors
- 2) Phillips Red Head Stud Anchors

Tests were conducted in blocks supplied by the client. Compression test cylinders and cores from actual blocks were used to establish strength's of the blocks.

Pull-Out tests were conducted by applying tension loads to the anchor through threaded rods held in the jaws of the 300,000 lb. Baldwin Testing Machine. (Calibrated September, 1964) The block was restrained on the under side of the moveable crosshead with the rod producing through the jaw opening. Shear tests were conducted by applying a load through a plate bolted to the anchor, with the load travelling perpendicular to the anchor axis.

TEST RESULTS

Concrete Compression Values:

- 1) Theoretical: 2000 PSI
Actual: 1820 PSI (Average of 3 cores)
- 2) Theoretical: 4000 PSI
Actual: 4060 PSI (Average of 3 cores)

4000 x 1.015

Cylinder compression tests yielded approximately the same results.

Pull-Out Tests

- 1) Non-Drill Anchors (J Series)
Pull-Out Strength, lbs.

Size	2000 PSI	Failure Type	4000 PSI	Failure Type
1/4	2580	5X7" Spall	(NOT TESTED)	
	2310	3X3" Spall		
	2540	4 X 5" Spall		
	2476	Average		

(continued)



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(Revised to correct 10-9-64)

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Sht. 22/36

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CH 3532

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9-20-64

Size	2000 PSI	Failure Type	4000 PSI	Failure Type
1/2	4050 4020 3950 4000	Block Block Block Average	(NOT TESTED)	
3/4	7330 7100 7180 7203	Block Block Block Average	17000 17150 17350 17166	12 X 12" sp. Block split Block split Average

2) Stud Anchors (JS. Series)

Pull-Out Strength, lbs.

Size	2000 PSI	Failure Type	4000 PSI	Failure Type
1/4 (1 5/8")	1414 1532 1340 1462	5X6" Spall " 3X6" Spall Average	(NOT TESTED)	
1/2 (2 1/4")	3280 2780 2930 2993	6X9" Spall 9X11 1/2 Spall 6X9" Spall Average	(NOT TESTED)	
5/8 (2 3/4")	(NOT TESTED)		10480 8770 8470 9240	5.8 Block 4.9 Block 4.7 6X10 Spall 5.1 Average
3/4 (3 1/2")	7400 6670 6040 6703	9X10 Spall Block Block Average	13000 12750 12200 12650	4.5 Block 4.4 Block 4.2 Block 4.4 Average

When the failure is described "Block", this indicates the block cracked or overstressed. "Anchor" describes the condition of the anchor pulling out without a spall.

$f'_c = 4 \text{ ksi}$

$\frac{P_u}{P_A}$

054162

(continued)



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Aut. 23/36

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CH 8500

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Shear Tests

1) Stud Anchors (JS Series)

Shear Load, lbs.

Size	2000 FSI	Failure Type	4000 FSI	Failure Type
1/8	1620	Bolt	(NOT TESTED)	
	1475	Bolt		
	1260	Bolt		
	1457	Average		
1/2	5700	Bolt	(NOT TESTED)	
	5260	Bolt		
	5510	Bolt		
	5323	Average		
5/8	(NOT TESTED)			
3/4	10500	Block	11653	7.8 Bolt
			12003	8.0 Bolt
			11803	7.9 Bolt
			11816	7.9 Average
	10200	Bolt	19403	9.2 Bolt
			16703	7.9 Bolt
			17953	8.5 Bolt
			17353	8.3 Average

"Bolt" type failure designates bolt shear; "Block" designates the block failed.

$f_c = 4 \text{ Ksi}$ S_u/S_y 054162

Respectfully submitted,
PITTSBURGH TESTING LABORATORY

W. H. Leveltus M.

W. H. LEVELTUS, MANAGER
CHICAGO DISTRICT

PHILLIPS DRILL COMPANY
MICHIGAN CITY, INDIANA

APPENDIX C

Ref. S 1/3

PULLOUT AND SHEAR CAPACITY OF THE PHILLIPS
REDHEAD NON-DRILL AND REDHEAD STUD ANCHORS
IN SEVERAL STRENGTHS OF CONCRETE.

TABLE I

LOAD	DIA.	REDHEAD STUD					REDHEAD NON-DRILL					P _u /F _c =25
		2000	2500	3000	3500	4000	2000	2500	3000	3500	4000	
PULLOUT CAPACITY	1/4	1560	1800	2110	2400	2830	2500	2650	2850	3000	3120	10.
	3/8	2280	2660	3100	3550	4200	3300	3650	4100	4500	4800	8.
	1/2	3360	3900	4550	5200	6180	4400	5100	5900	6800	7400	7.
	5/8	4600	5300	6150	7100	8400	5600	6600	8000	9700	10,750	5.
	3/4	7150	8300	9600	11,100	13,200	7700	9600	12,200	15,500	17,800	5.
SHEAR CAPACITY	1/4	1650	1800	1980	2110	2320						
	3/8	3350	3700	4070	4500	4950						
	1/2	5650	6350	7000	7700	8600	SEE TABLE II					
	5/8	8400	9500	10,500	11,700	13,200	next sheet					
	3/4	11,500	13,100	14,600	16,200	18,500						

RECOMMENDED WORKING LOADS EQUAL 25% OF
THE CAPACITY VALUES GIVEN ABOVE.

Embedment:

	3 KSI	P _u /P _a	4 KSI
15/8"	7.7	1/4"	9.4
17/8"	6.2	3/8"	7.0
2 1/2"	5.2	1/2"	5.9
2 3/4"	4.1	5/8"	4.7
3 1/4"	4.1	3/4"	4.5
	3 KSI	S _u /S _A	4 KSI
	6.6	1/4"	7.7
	6.8	3/8"	7.4
	7.9	1/2"	8.3
	8.4	5/8"	8.8
	8.1	3/4"	8.8

Sht. 25/36

APPENDIX C

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PHILLIPS DRILL COMPANY
MICHIGAN CITY, INDIANA

SHEAR CAPACITY OF THE REDHEAD NON-DRILL
ANCHORS IN SEVERAL STRENGTHS OF CONCRETE

TABLE II

LOAD	Dia.	REDHEAD NON-DRILL ANCHOR					054162
		2000	2500	3000	3500	4000	S _u /S _A f _c 3500
SHEAR CAPACITY	1/4	2300	2300	2300	2300	—	7.7
	3/8	4000	4450	4450	4450	—	7.0
	1/2	4700	5400	6200	7000	—	7.2
	5/8	5600	6400	7300	8100	—	5.9
	3/4	8000	8900	10,000	11,300	—	5.8

TAKEN FROM A REPORT BY MORRIS DOBERNE, C.E., S.E.
ENTITLED: A REPORT ON SHEAR AND PULLOUT OF THE
PHILLIPS REDHEAD ANCHOR AND CAST-IN-PLACE BOLTS.

RECOMMENDED WORKING LOAD EQUALS 25 % OF
THE CAPACITY VALUES GIVEN ABOVE.

PHILLIPS DRILL COMPANY, INC.

General Offices
Michigan City, Indiana 46360

Pullout and Shear Ultimate Capacities For The Phillips Red Head Non-Drill and Red Head Stud Anchors In Several Strengths of Concrete

PHILLIPS CONCRETE ANCHORS	CAT. NO.	BOLT SIZE	PULLOUT CAPACITY 1.					SHEAR CAPACITY 2.				
			CONCRETE STRENGTH, PSI					CONCRETE STRENGTH, PSI				
			2000	2500	3000	3500	4000	2000	2500	3000	3500	4000
RED HEAD STUD	JS-14	1/4	1560	1800	2110	2400	2830	1650	1800	1980	2110	2320
	JS-38	3/8	2280	2660	3100	3550	4200	3350	3700	4070	4500	4950
	JS-12	1/2	3360 ²⁴⁰⁰ ₍₄₎	3900	4550	5200	6180 ⁵⁴⁰⁰ ₍₄₎	5650 ⁵⁰⁰⁰ ₍₃₎	6350	7000	7700	8600 ⁷⁵⁰⁰ ₍₂₎
	JS-58	5/8	4600 ⁴⁰⁰⁰ ₍₄₎	5300	6150	7100	8400 ⁷²⁰⁰ ₍₄₎	8400 ⁷²⁰⁰ ₍₄₎	9500	10500	11700	13200 ¹¹⁵⁰⁰ ₍₄₎
	JS-34	3/4	7150 ⁶⁰⁰⁰ ₍₄₎	8300	9600	11100	13200 ¹¹⁵⁰⁰ ₍₃₎	11500 ¹⁰⁰⁰⁰ ₍₇₎	13100	14600	16200	18500 ¹⁶⁵⁰⁰ ₍₈₎
RED HEAD NON-DRILL	J-14	1/4	2500	2650	2850	3000	3120	2300	2300	2300	2300	2300
	J-38	3/8	3300	3650	4100	4500	4800	4000	4450	4450	4450	4450
	J-12	1/2	4400 ³⁸⁰⁰ ₍₃₎	5100	5900	6800	7400 ⁶⁵⁰⁰ ₍₃₎	4700 ⁴⁰⁰⁰ ₍₄₎	5400	6200	7000	7900 ⁷⁰⁰⁰ ₍₄₎
	J-58	5/8	5600 ⁴⁸⁰⁰ ₍₃₎	6600	8000	9700	10750 ⁹⁵⁰⁰ ₍₄₎	5600 ⁴⁸⁰⁰ ₍₄₎	6400	7300	8100	9100 ⁸⁰⁰⁰ ₍₄₎
	J-34	3/4	7700 ⁶⁵⁰⁰ ₍₄₎	9600	12200	15500	17800 ¹⁵⁵⁰⁰ ₍₄₎	8000 ⁷⁰⁰⁰ ₍₅₎	8900	10000	11300	12900 ¹¹⁵⁰⁰ ₍₅₎

1. All Pullout Tests Resulted In The Fracturing Or Coning (Conical Spalling) Of The Concrete.
 2. The Shear Tests Resulted In The Shearing Of The Bolts Or Studs Except For The Largest Sizes Where Fracturing Of The Concrete Occurred.
- The Above Values Were Derived From Actual Tests Conducted By Pittsburgh Testing Laboratory, Chicago, And Smith-Emery Company Los Angeles, And Represent The Average Of Three Tests.
- The Manufacturer's Recommended Working Load Equals 25% Of The Ultimate Capacity Values Given Above.

APPENDIX C
Ref. 5 3/5
At. 26/36



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FORM 407-UM

sh. 27/36
APPENDIX C

Ref. 6

ORDER No. CH-1597
CLIENT's No. 21060

LABORATORY No. 105228

March 31, 1971

REPORT

TESTS OF: Concrete Anchors

REPORTED TO: Phillips Drill Company, Inc.
P. O. Box 364
Michigan City, Indiana 46360

In accordance with your instructions we have completed pullout and shear tests of anchors identified as:

PHILLIPS RED HEAD WEDGE ANCHORS

Tests were conducted in blocks of limestone aggregate concrete from a local batching plant and poured in our facility. Compression test cylinders were used to establish strengths of the concrete.

The anchors were inserted into pre-drilled holes and expanded by tightening the nuts with a 12" adjustable wrench.

Pullout tests were conducted by applying tension loads to the anchor through a threaded rod held in the upper crosshead jaws and extending through the movable crosshead of the 300,000 lb. Baldwin Testing Machine. The block was restrained on the underside of the movable crosshead via a steel frame which placed the reaction load 5" minimum from the anchor location. Shear tests were conducted by applying a load through a plate mounted to the block by the anchor, with the load applied perpendicular to the anchor axis.

TESTS OF: RED HEAD WEDGE ANCHORS

Anchor Body Diameter	Test No.	PULL-OUT				Type of Failure	SHEAR				Location of Failure
		Total Load Pull-Out Lbs.	Average Load Pull-Out Lbs.				Total Load Shear Lbs.	Average Load Shear Lbs.			
1/4"	1	2303	290	2346	8.1	Concrete Failed	1940	340	2100	7.0	Shear
	2	2393				Concrete Failed	2250				Shear
	3	2343				Concrete Failed	2110				Shear
3/8"	1	3863	570	3943	6.9	Concrete Failed	4640	650	3946	6.1	Shear
	2	4063				Concrete Failed	3740				Shear
	3	3903				Concrete Failed	3460				Shear
1/2"	1	5759	990	5219	5.3	Concrete Failed	7500	990	7067	7.1	Shear
	2	4849				Concrete Failed	6700				Shear
	3	5049				Concrete Failed	7000				Shear
5/8"	1	7429	1710	7782	4.5	Concrete Failed	10,400	1420	10,800	7.6	Shear
	2	8289				Concrete Failed	12,100				Shear
	3	7629				Concrete Failed	10,900				Shear
3/4"	1	12,679	2730	2,069	4.4	Concrete Failed	18,600	2010	19,133	9.5	Block Split
	2	12,279				Concrete Failed	17,500				Block Split
	3	11,229				Concrete Failed	21,300				Anchor Shear

Tests were conducted in concrete blocks having compressive strength on an average of 3690 P.S.I.

P_A	$\frac{P_u}{P_A}$
-------	-------------------

f'_c

PITTSBURGH TESTING LABORATORY

District Manager

Manufacturers' recommended safe working loads in 3690 PSI concrete = 25% of the average loads shown above.

$$P_A = P_{A_3} + (f'_c - 3)(P_{A_4} - P_{A_3}); S_A, \text{ similarly.}$$

AVERAGE ULTIMATE TENSILE & SHEAR LOADS*

APPENDIX C 1973
Ref. 7 4/28/36

CONCRETE STRENGTH		2000 PSI				4000 PSI				6000 PSI			
Diameter	Embedment	Tension		Shear		Tension		Shear		Tension		Shear	
1/4"	1 1/8"	3.9	975	5.5	1653	4.8	1455	8.7	2612	5.0	1755	8.0	2389
	1 1/2"		1875		1653		2225		2612		2935		2389
	1 3/4"		2275		1653		2700		2612		3300		2389
	2"		2525		1653		3125		2612		3350		2389
	2 1/4"		2680		1653		3310		2612		3350		2389
	2 1/2"		2800		1653		3350		2612		3350		2389
3/8"	1 5/8"	5.6	2245	6.9	3748	3.9	2355	7.6	5107	3.5	2810	7.8	6266
	2"		2725		3748		3025		5107		3650		6266
	2 1/2"		3075		3748		3900		5107		4450		6266
	3"		3300		3792		4300		5419		5000		6266
	3 1/2"		3425		3792		4600		5419		5275		6266
	4"		3520		3792		4750		5419		5375		6266
	4 1/2"		3580		3792		4800		5419		5400		6266
1/2"	2 1/4"	6.5	4545	10.0	7444	5.2	5510	8.0	8316	4.9	6845	7.0	9341
	2 3/4"		5800		7444		7200		8316		9800		9341
	3 1/2"		7000		7444		9450		8316		13200		9341
	4 1/2"		7275		8897		11225		10232		14550		11522
	5 1/2"		8250		8897		12050		10232		15150		11522
	6"		9000		8897		12300		10232		15300		11522

tual Concrete Strengths

2178 psi 4027 psi
= 2000 x 1.09 = 4000 x 1.01

*See sheet A-3 for notes

F.S. = $\frac{P_u}{P_A}$; P_u = ultimate load shown here
 P_A = allowable load from Table A, Dwg 054162-Rev 3.

A-1

No adjustments for variation of
embedment or of f'

HILTI

KWIK-BOLT

File No. H2189
Report No. 878

AVERAGE ULTIMATE TENSILE & SHEAR LOADS*

APPENDIX C

Ref. 7

CONCRETE STRENGTH		2000 PSI		4000 PSI		6000 PSI	
Diameter	Embedment	Tension	Shear	Tension	Shear	Tension	Shear
5/8"	2 3/4"	5410	11198	6600	11562	7700	13500
	3 1/2"	6250	11198	9100	11562	9560	13500
	4 1/2"	7000	11198	12000	11562	14500	13500
	5 1/2"	7550	13378	14300	15437	20300	15437
	6 1/2"	8025	13378	16000	15437	21000	15437
	7 1/2"	9000	13378	17000	15437	21000	15437
3/4"	3 1/4"	8155	13257	10150	17133	10860	18102
	4"	9700	13257	13400	17133	13700	18102
	5"	11700	13257	16500	17133	17600	18102
	6"	13800	15195	18000	18466	22500	21009
	7"	15800	15195	21000	18466	23600	21009
	8"	16000	15195	23000	18466	23600	21009
	9"	16000	15195	23500	18466	23600	21009
1"	4 1/2"	14000	27355	16000	26879	20500	32112
	5"	15500	27355	18900	26879	24400	32112
	6"	17600	27355	24650	26879	32200	32112
	7"	18200	27355	27500	26879	35000	32112
	8"	18200	27355	27500	34491	35000	36394
	9"	18200	27355	27500	34491	35000	36394
	10"	18200	27355	27500	34491	35000	36394

Actual Concrete Strengths

2178 psi 4027 psi 6119 psi

*See sheet A-3 for notes

A-2

HILTI
KWIK-BOLT

sh. 30/136

AVERAGE ULTIMATE TENSILE & SHEAR LOADS*

APPENDIX C

Ref. 7

CONCRETE STRENGTH		2000 PSI		4000 PSI		6000 PSI	
Diameter	Embedment	Tension	Shear	Tension	Shear	Tension	Shear
1 1/4"	5 1/2"	3.6 19000	4.2 36750	2.9 23000	3.7 35680	2.9 31200	3.7 45195
	6 1/2"	21600	36750	27100	35680	36500	45195
	7 1/2"	23600	36750	31100	35680	42000	45195
	8 1/2"	25100	39843	34600	35680	44400	47098
	9 1/2"	26200	39843	37800	35680	44400	47098
	10 1/2"	26800	39843	40900	35680	44400	4959

Actual Concrete Strengths

2178 psi 4027 psi 6119 psi

*Tension values obtained from best fit curve through mean values of test data. Curves and test data contained in A. A. Hanks Report No. 8784 (HILTI No. TR-111A).

Shear values are minimum mean values at each embedment based on failure across threaded section of the anchor.



ABBOT A. HANKS, INC.
TESTING LABORATORIES
Established 1866



1115 INDIANA STREET, P.O. BOX 77265
SAN FRANCISCO, CA 94107
(415) 282-8600

APPENDIX C

Ref. 8

Sh. 31/30

Laboratory Report

File No's. H22148-S01
H221100-02

Report No's. 6099
6100, 6101,
6102, 1513,
1514

March 24, 1977

HILTI FASTENING SYSTEMS
1 Cummings Point Road
Stamford, Connecticut 06904

SUBJECT: SUMMARY REPORT - HILTI HDI CONCRETE FLUSH ANCHORS TEST PROGR

Tension (pullout) and shear tests were conducted in three 8" thick non-reinforced slabs utilizing limestone aggregate designed for 28 day compressive strengths of 2000 psi, 4000 psi and 6000 psi. Standard 6 x 12 inch cylinders were cast and tested in accordance with ASTM C31 and C39 respectively to determine the actual average concrete strengths during testing.

The test program substantially meets the static test criteria for tests in concrete described in ASTM E488-76, "Standard Test Methods for Strengths of Anchors in Concrete and Masonry Elements".

Loads shown are average ultimate loads in pounds.

We certify that the test values reported are indicative of the performance of HDI anchors when used in concrete strengths and under conditions as noted in the applicable reports.

Concrete Strength* Anchor Size	2000 PSI		3850 4000 PSI		6200 6000 PSI	
	Tension	Shear	Tension	Shear	Tension	Shear
HDI - 1/4	1904	1738	2251	1781	3075	3050
HDI - 3/8	3174	3970	4942	4225	5650	5900
HDI - 1/2	3997	5873	6751	6224	10200	9350
HDI - 5/8	5549	8883	9696	12205	10400	13600
HDI - 3/4	8857	15195	16034	17609	16400	21200

* Actual Average Concrete Strengths: 2000 psi, 3850 psi, 6200 psi

ABBOT A. HANKS, INC. TESTING LABORATORIES	7.9	7.3	8.4	6.4	6.9	7.3
	5.7	7.9	6.6	6.1	7.1	6.8
	4.6	8.9	5.5	8.3	4.2	6.6
	4.9	10.1	5.7	8.6	4.0	7.7

Lee W. Mattis

Vice President/Engineering

PG 4 E. FACTOR OF SAFETY
(HILTI TEST) ÷ (STD #054162-3)^{TR} - 110

⊗ F/S for 6200 psi, as shown, are for allowables extrapolated to 6.2 Ksi in T_a
If based on 6.0 Ksi value.
Sec. A.2.2) these F/S

OAKLAND LABORATORY: 2898 GLASCOCK STREET, OAKLAND 94601

Design Drafting
82-3690

PACIFIC GAS AND ELECTRIC COMPANY
GENERAL COMPUTATION SHEET

2.
SHEET NO. 32 OF 36 SHEET
JOB } NO. 52.7.11.5.8
FILE }
LOCATION

SUBJECT EOI 1016
Diablo Canyon Power Plant Project
MADE BY Mike Jones DATE 6/16/82 CHECKED BY MNP APPROVED BY _____

II. APPENDIX

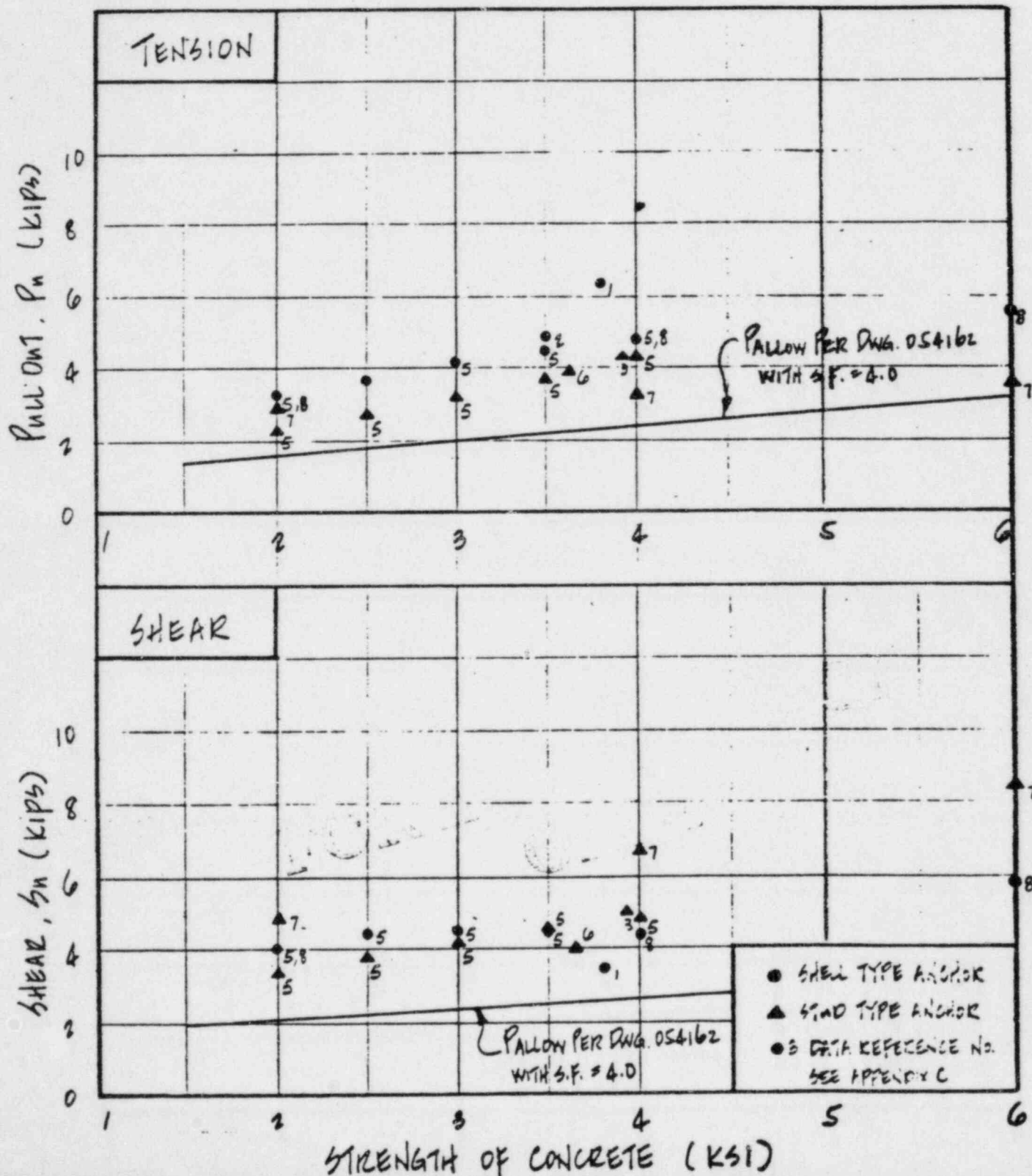
d. APPENDIX D

GENERAL COMPUTATION SHEET

SUBJECT EOG 1016
Duke Canyon Power Plant Project - APPENDIX D
MADE BY Mike Jan DATE 6/16/82 CHECKED BY TMP APPROVED BY _____

ANCHOR DIAMETER = $\boxed{\frac{3}{8}''}$

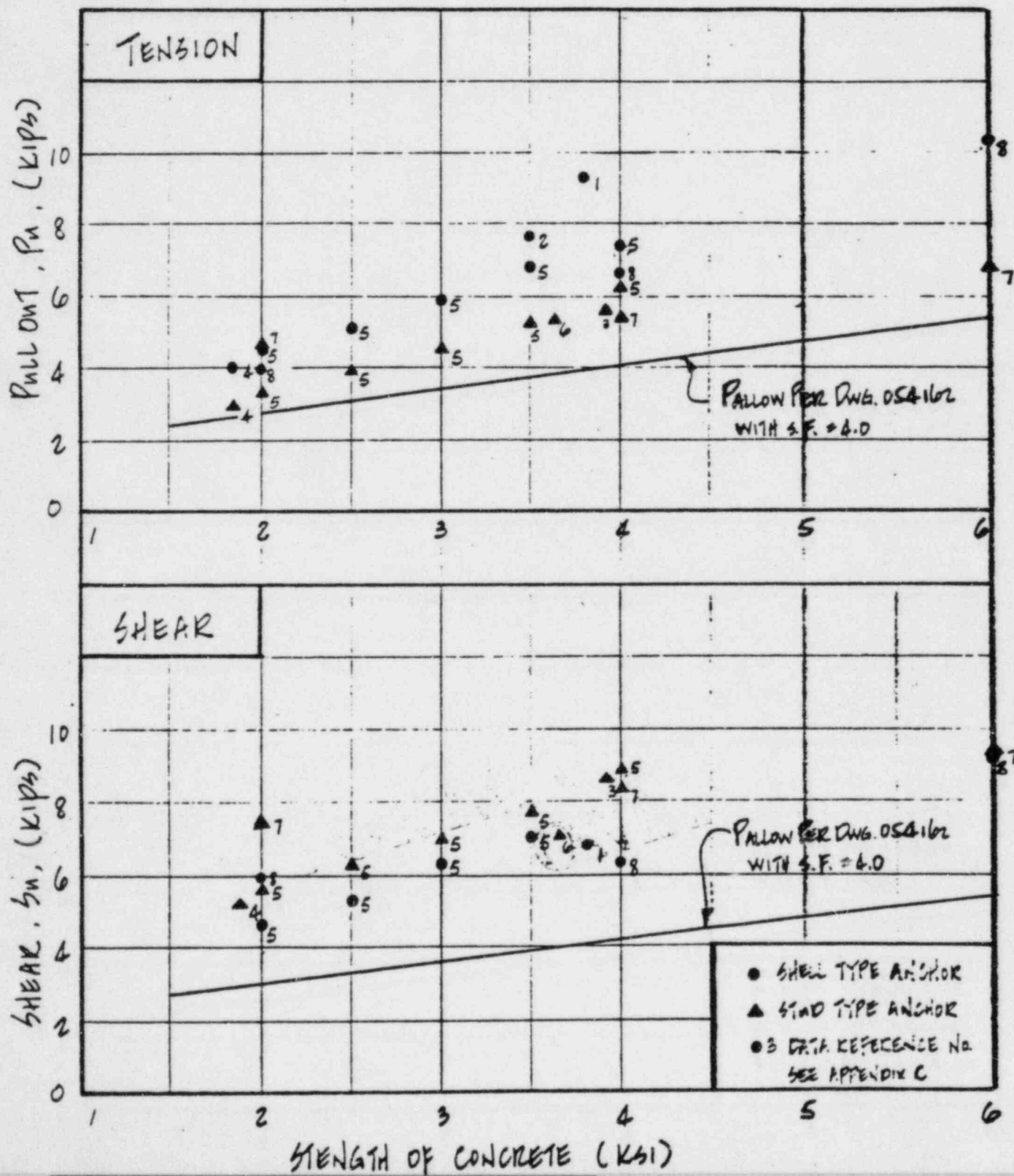
EMBEDMENT LENGTH = $\boxed{1\frac{3}{4}''}$



SUBJECT EOG 1016
Duke's Canyon Power Plant Project - APPENDIX D
MADE BY Mike Gam DATE 6/16/82 CHECKED BY MNP APPROVED BY _____

ANCHOR DIAMETER = $\boxed{\frac{1}{2}''}$

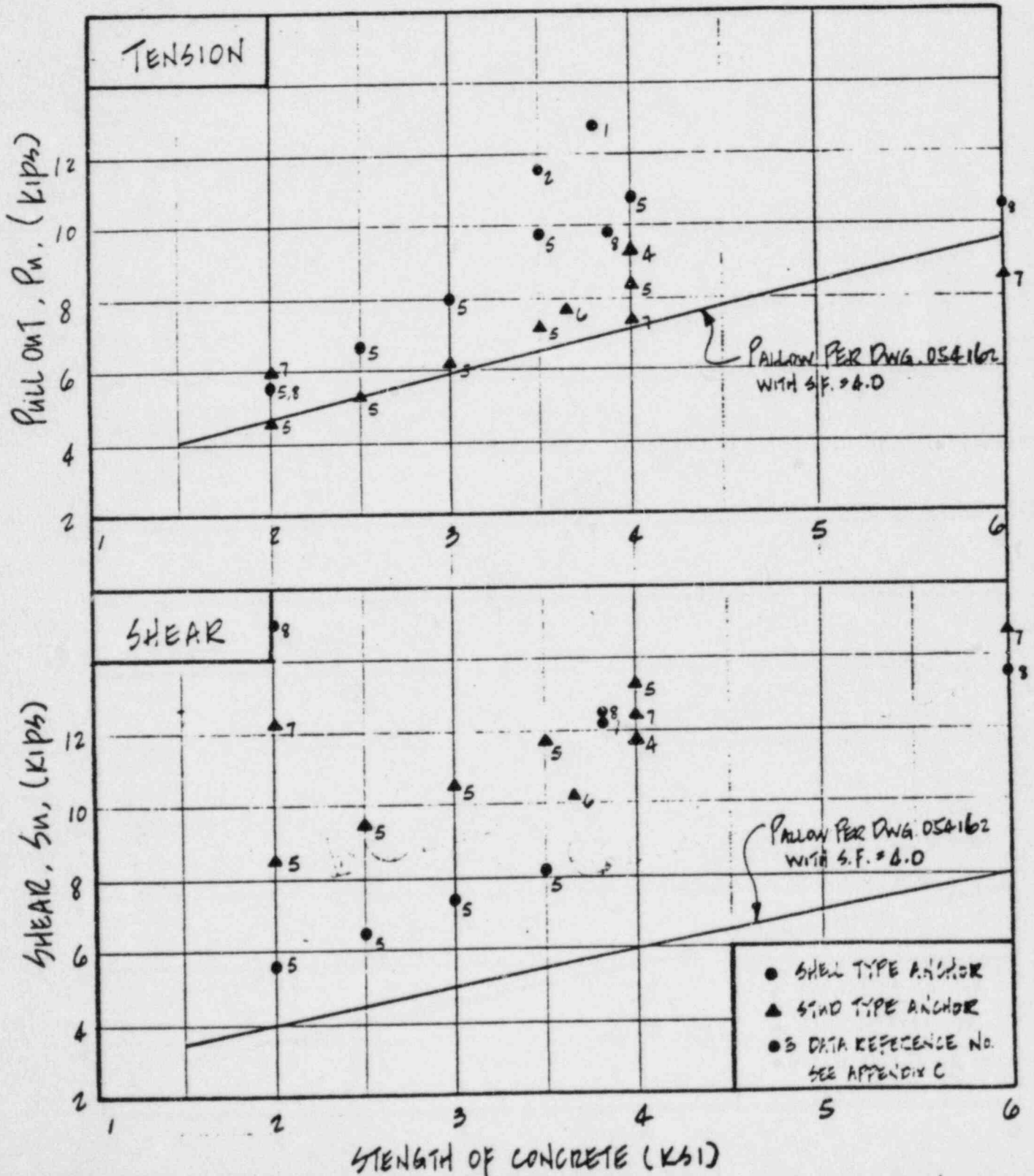
EMBEDMENT LENGTH = $\boxed{2\frac{1}{4}''}$



GENERAL COMPUTATION SHEET

SUBJECT 203 1016
Diablo Canyon Power Plant Project - APPENDIX D
MADE BY Mike Jones DATE 6/16/82 CHECKED BY MNP APPROVED BY _____

ANCHOR DIAMETER = $\boxed{5/8}$ EMBEDMENT LENGTH = $\boxed{27/8}$

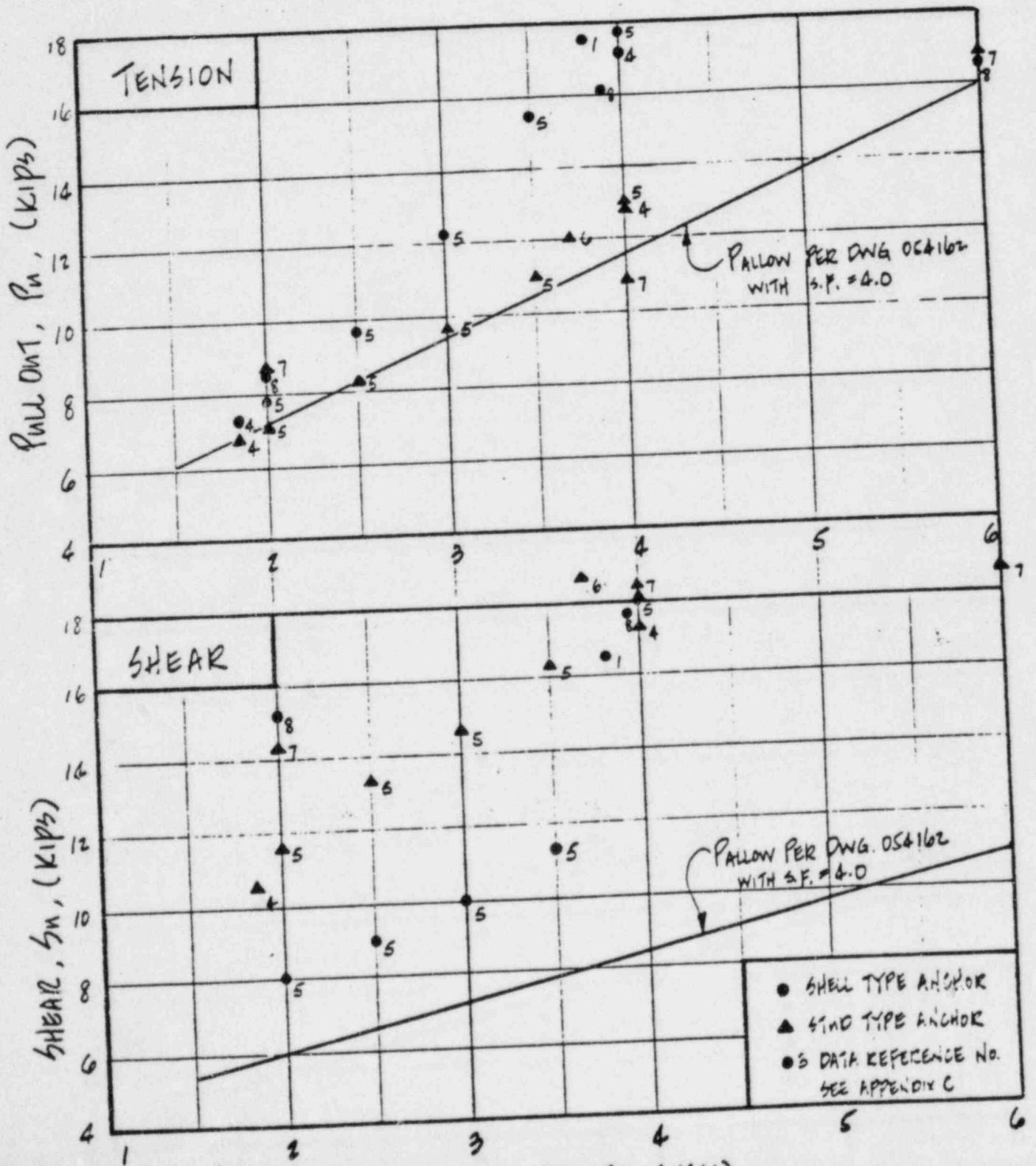


GENERAL COMPUTATION SHEET

SHEET NO. 36 OF 36 SHEETS
JOB FILE NO. 52.7.11.5.8
LOCATION _____

SUBJECT ES 1016
Diablo Canyon Power Plant Project - APPENDIX D
MADE BY Mike Jones DATE 6/16/82 CHECKED BY MNP APPROVED BY _____

ANCHOR DIAMETER = $\boxed{\frac{3}{4}''}$ EMBEDMENT LENGTH = $\boxed{3\frac{3}{8}''}$



Cont./Supp. Scott

Cont./Supp. I.D. No.

PG&E No.

283

3

INSPECTION SECTION

Discrepant Item: Units I & II. Concrete flush shell anchors installed by Scott Co. for the air conditioning seismic supports.

Explanation of Discrepancy: Possible existence of incorrectly installed concrete anchors. (Continued on Page 2).

Δ E Nemi
Field Engr./Inspector

3-2-77
Date

CLASSIFICATION & DISPOSITION

Minor Variation ☐Deviation ☒

Disposition: Accept all Scott Company installed air conditioning seismic support anchors as is. Data contained in the "Procedure for Establishing Acceptance Criteria for Concrete Anchor Installations - Diablo Canyon" on file in the QA vault on site and gathered during an inspection performed by PG&E show that Phillips anchors increase their strength as they are displaced from their embedment. Displacement of the ductwork up

The following members of the Material Review Board concur with the above Disposition: (For Minor Variations, only Resident Engineer's signature required.)

to one inch is acceptable to the responsible Engineer. The duct work can easily tolerate the small movements that anchors might be displaced when subjected to design loads.

Don Ray
Name

3/23/77
Date

Isaacoff
Name

APR - 8 1977
Date

Robert Brathorn
Responsible Engineer

5-2-77
Date

R. D. Etker
Resident Engineer

3-2-77
Date

[Signature]
Name

3/23/77
Date

Name

Date

E. Wollak
Supervising Engineer

5/2/77
Date

DISPOSITION ACCOMPLISHED

Remarks: N/A

Field Engineer/Inspector

Date

STEPS TO PREVENT RECURRENCE (Deviations Only)

Scott Company has discontinued using Phillips anchors and will only use anchors manufactured by The Hilti Corp. Scott Co. has initialed an installation procedure for installing Hilti anchors, I-41-2 to assure they are installed correctly.

R. D. Etker
Resident Engineer

6-13-77
Date

Copies

Attachments

Report Completed

Coor. Q.C. Engr. Dir.-Q.A.

1. Data Sheets

3. Scott Co. Procedure for Anchor Installation

Proj. Super.

Resp. Engr.

2. Telecon dtd 3-2-77

Resident Engr.

Proj. Engr.

Q.A.-Site

Supv. Insp. Engr. (G.O.)

Don Ray
Coordinating QC Engineer

6/28/77
Date

00373-1739

Cont./Supp. Scott

Cont./Supp. I.D. No. _____

 PG&E No. 283

EXPLANATION OF DISCREPANCY:

Of seventy-seven anchor installations inspected, Thirty-three did not have their expansion plugs driven far enough to meet minimum acceptance limits established for Fullman Kellogg.

An attempt was made to drive the expansion plugs further during the inspection. Typically, they could not be driven more than $3/32"$ and then only with great effort.

Masonry bits were used to drill the holes. Bit wear caused slightly undersized holes and the drill point formed a conical shaped bottom. Both of these conditions prevent the expansion plugs from being fully driven.

Inplace pull out tests were performed on eleven of the thirty-three anchors, in accordance with the "Procedure for Establishing Acceptance Criteria for Concrete Anchor Installations - Diablo Canyon Power Plant". Eight of the anchors exceeded the values in Table A of Drawing No. 054162 for 5 kip concrete without being displaced more than 0.010". All eleven anchors significantly exceeded the Table A values without being displaced more than 5% of their minimum embedment (0.120" and 0.160" for 5/8" and 3/4" anchors, respectively). These eleven anchors were typical of the worst case conditions encountered during the inspection.

With the exception of the underdriven expansion plugs, the anchors were installed satisfactorily in all other respects. Also reference PG&E Deviation #282.

SUMMARY OF IN-PLACE TEST RESULTS ON ANCHORS EXHIBITING WORST CASE CONDITIONS

Size of Phillips Anchor	Distance Plug was Driven	% of Allowable Distance	Force Developed by Test	Factor of Safety	Anchor Displaced by Test	% of Allowable Displacement
5/8"	15/32"	94%	4320lb.	2.05	0.034"	28%
5/8"	13/32"	81%	4330lb.	2.06	0.015"	13%
5/8"	1/2 "	100%	4320lb.	2.05	0.026"	22%
5/8"	17/32"	106%	4320lb.	2.05	≈ 0.125"	104%
5/8"	3/8 "	75%	4320lb.	2.05	0.010"	8%
3/4"	1/4 "	50%	3770lb.	1.09	0.010"	6%
3/4"	9/32"	56%	5800lb.	1.68	0.16 "	100%
*3/4"	9/32"	56%	7160lb.	2.08	0.235"	147%
3/4"	3/8 "	75%	4700lb.	1.36	0.010"	6%
3/4"	17/32"	106%	4350lb.	1.26	0.010"	6%
3/4"	15/32"	94%	4120lb.	1.19	0.007"	4%
3/4"	- 9/16"	56%	6960lb.	2.02	0.008"	5%

*Continuation of test on preceeding anchor.

003743-1740

CONTRACTOR

Scott

AREA

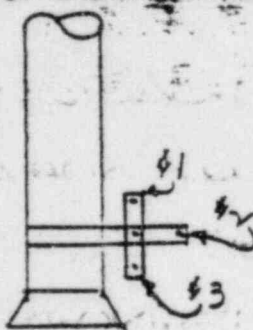
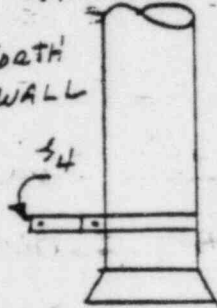
H

ELEVATION

60'

SYSTEM

Sketch of anchor pattern if applicable. GAS DELAY TANK 1-3

EAST
WALLNORTH
WALLREFERENCE ANCHOR NUMBER (Apply
reference numbers to sketch)

ANCHOR TYPE AND SIZE INSTALLED

*OBVIOUS IRREGULARITIES (yes/no)

THREADED END CUT OFF (yes/no)
(If yes, record number of threads
remaining in entry. If less than
4 full threads*.)ANCHOR DEPTH GREATER THAN 1/8"
BELOW SURFACE (yes/no) (If yes,
record in entry. If greater than
1/2"*.)MORE THAN 5 DEGREES FROM PERPEN-
DICULAR (yes/no) (If yes, record
in entry. If greater than 15°*.)

AS FOUND PLUG DEPTH

AS LEFT PLUG DEPTH (If not
within +1/16" of fully driven
acceptance criteria*.)

DISTANCE PLUG DRIVEN BY RESETTING

POSSIBLE EXP. END CUT OFF (yes/no)

REMARKS BRACKETS DO NOT FIT TOGETHER WELL.

*If yes, describe in "Remarks" and
check "Review Required" box.

DATA TAKEN BY/DATE: Walker/2-11-77

REVIEWED BY/DATE: SEN 2/18/77
(If required)

00373-1741

CONTRACTOR

Scott

AREA

H

ELEVATION

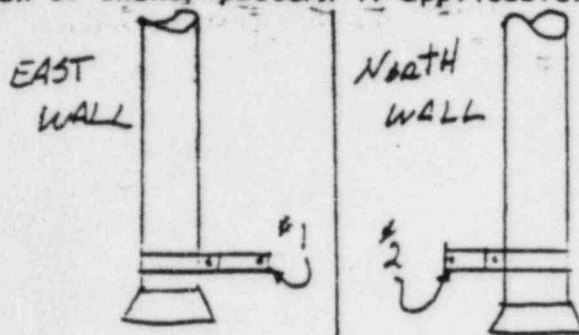
+60'

SYSTEM

A/C

Sketch of anchor pattern if applicable.

GAS DECK TANK 1-2



REFERENCE ANCHOR NUMBER (Apply reference numbers to sketch)

1

2

ANCHOR TYPE AND SIZE INSTALLED

5/8P

5/8P

*OBVIOUS IRREGULARITIES (yes/no)

No

No

THREADED END CUT OFF (yes/no)
(If yes, record number of threads remaining in entry. If less than 4 full threads*.)

No

No

ANCHOR DEPTH GREATER THAN 1/8" BELOW SURFACE (yes/no) (If yes, record in entry. If greater than 1/2"*.)

No

No

MORE THAN 5 DEGREES FROM PERPENDICULAR (yes/no) (If yes, record in entry. If greater than 15°*.)

No

No

AS FOUND PLUG DEPTH

1 15/32

1 14/32

AS LEFT PLUG DEPTH (If not within +1/16" of fully driven acceptance criteria*.)

1 14/32

1 15/32

DISTANCE PLUG DRIVEN BY RESETTING

1/32

1/32

POSSIBLE EXP. END CUT OFF (yes/no)

No

No

REMARKS

*If yes, describe in "Remarks" and check "Review Required" box.

DATA TAKEN BY/DATE: W. Allen 2-11-77REVIEWED BY/DATE: SSD 2/18/77
(If required)

00373-1742

SHEET 1

CONTRACTOR

SCOTT

AREA

GE

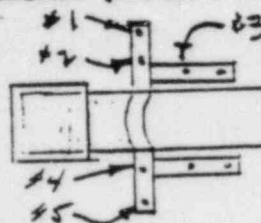
ELEVATION

73'

SYSTEM

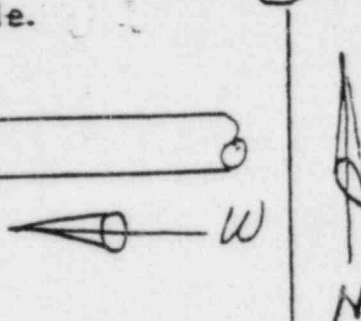
A/C

Sketch of anchor pattern if applicable.



Looking Up To Ceiling
Center of Rm

N LINE



Room ABOVE
BORON INJECTION
TANK 1-1 @
73' ELEV.

REFERENCE ANCHOR NUMBER (Apply
reference numbers to sketch)

ANCHOR TYPE AND SIZE INSTALLED

*OBVIOUS IRREGULARITIES (yes/no)

THREADED END CUT OFF (yes/no)
(If yes, record number of threads
remaining in entry. If less than
4 full threads*.)

ANCHOR DEPTH GREATER THAN 1/8"
BELOW SURFACE (yes/no) (If yes,
record in entry. If greater than
1/2"*.)

MORE THAN 5 DEGREES FROM PERPEN-
DICULAR (yes/no) (If yes, record
in entry. If greater than 15*.)

AS FOUND PLUG DEPTH

AS LEFT PLUG DEPTH (If not
within +1/16" of fully driven
acceptance criteria*.)

DISTANCE PLUG DRIVEN BY RESETTING

POSSIBLE EXP. END CUT OFF (yes/no)

REMARKS

1	2	3	4
5/8P	5/8P	5/8P	5/8P
No	No	No	No
No	No	No	No
No	-4/32	No	No
No	No	No	No
1 18/32	1 14/32	1 16/32	1 13/32
1 13/32	1 12/32	1 18/32	1 12/32
0	2 1/32	0	1/32
No	No	No	No

*If yes, describe in "Remarks" and
check "Review Required" box.

DATA TAKEN BY/DATE: Walker/2-11-77

REVIEWED BY/DATE: LSN 2/14/77
(If required)

00373-1751

CONTRACTOR South AREA GE ELEVATION 73'

SYSTEM AL

Sketch of anchor pattern if applicable.

SEE SHEET #1

REFERENCE ANCHOR NUMBER (Apply reference numbers to sketch)

ANCHOR TYPE AND SIZE INSTALLED

*OBVIOUS IRREGULARITIES (yes/no)

THREADED END CUT OFF (yes/no)
(If yes, record number of threads remaining in entry. If less than 4 full threads*.)

ANCHOR DEPTH GREATER THAN 1/8" BELOW SURFACE (yes/no) (If yes, record in entry. If greater than 1/2"*.)

MORE THAN 5 DEGREES FROM PERPENDICULAR (yes/no) (If yes, record in entry. If greater than 15°*.)

AS FOUND PLUG DEPTH

AS LEFT PLUG DEPTH (If not within +1/16" of fully driven acceptance criteria*.)

DISTANCE PLUG DRIVEN BY RESETTING

POSSIBLE EXP. END CUT OFF (yes/no)

REMARKS

*If yes, describe in "Remarks" and check "Review Required" box.

DATA TAKEN BY/DATE: Adelman/2-11-77

REVIEWED BY/DATE: SEN 2/14/77
(If required)

CONTRACTOR

SOS-11

AREA

H

ELEVATION

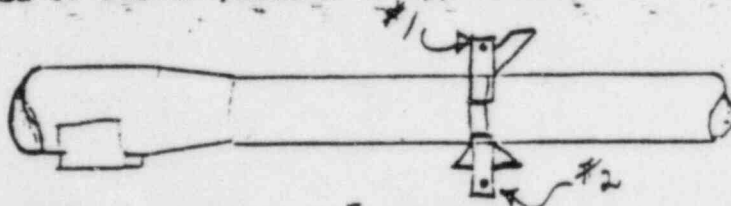
73'

SYSTEM

N/C

Sketch of anchor pattern if applicable:

CONTAINMENT SPRAY Pump 1-1

NORTH WALL ON 15TH LINE

REFERENCE ANCHOR NUMBER (Apply reference numbers to sketch)

ANCHOR TYPE AND SIZE INSTALLED

*OBVIOUS IRREGULARITIES (yes/no)

THREADED END CUT OFF (yes/no)
(If yes, record number of threads remaining in entry. If less than 4 full threads*.)

ANCHOR DEPTH GREATER THAN 1/8" BELOW SURFACE (yes/no) (If yes, record in entry. If greater than 1/2"*.)

MORE THAN 5 DEGREES FROM PERPENDICULAR (yes/no) (If yes, record in entry. If greater than 15°*.)

AS FOUND PLUG DEPTH

AS LEFT PLUG DEPTH (If not within +1/16" of fully driven acceptance criteria*.)

DISTANCE PLUG DRIVEN BY RESETTING

POSSIBLE EXP. END CUT OFF (yes/no)

REMARKS #1 Pull tested: 0.010" @ 150 lbs, 0.013" @ 434

*If yes, describe in "Remarks" and check "Review Required" box.

DATA TAKEN BY/DATE: Walden/2-11-77

REVIEWED BY/DATE: DEN 2/18/78
(If required)

00373-1753

ANCHOR Pull TEST

CONTRACTOR : SCOTT

ANCHOR LOCATION: CONT. SPRAY PUMP 1-1 RM, EL 73

ANCHOR REF. No.: # 1 DATE: 2/17/77

PERFORMED BY: ΔΕ Νienir

	<u>GAGE PRESS.</u>	<u>APPLIED FORCE</u>	<u>MOMENT</u>
0037			
00	650 psi	2350 lb	0.001"
00	810	2970	.002"
	870	3210	.003
	950	3530	.004
	1000	3730	.005
	1020	3810	.006
	1060	3960	.007
	1090	4040	.008
	1090	4070	.009
	1110	4150	0.010
	1130	4240	0.011
	1150	4320	0.012
	1160	4340	0.013"

5/8 PHILLIPS

PLUG DRIVEN 3/8"

SCOTT

AREA

十一

ELEVATION

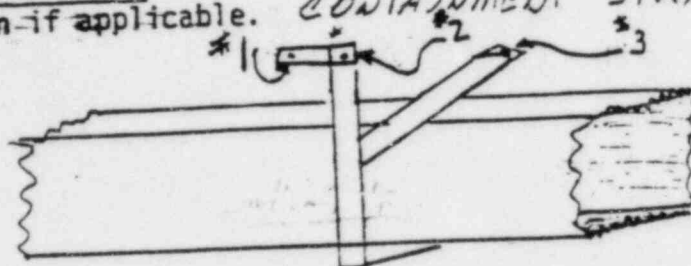
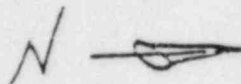
737

SYSTEM

A-7C

Sketch of anchor pattern if applicable.

CONTAINMENT SPRAY Pumps 1-2



REFERENCE ANCHOR NUMBER (Apply
reference numbers to sketch)

ANCHOR TYPE AND SIZE INSTALLED

*OBVIOUS IRREGULARITIES (yes/no)

THREADED END CUT OFF (yes/no)
(If yes, record number of threads
remaining in entry. If less than
4 full threads*.)

ANCHOR DEPTH GREATER THAN 1/8"
BELOW SURFACE (yes/no) (If yes,
record in entry. If greater than
1/2"*.)

MORE THAN 5 DEGREES FROM PERPENDICULAR (yes/no) (If yes, record in entry. If greater than 15⁰*)

AS FOUND PLUG DEPTH

AS LEFT PLUG DEPTH (If not within $\pm 1/16"$ of fully driven acceptance criteria*.)

DISTANCE PLUG DRIVEN BY RESETTING

POSSIBLE EXP. END CUT OFF (yes/no)

REMARKS

1	2	3	
3/4 P		3/4 P	
No		No	
No		No	
No		No	
No		No	
No		No	
1 29/32		1 23/32	
1 29/32		1 23/32	
0		0	
No		No	

can not get socket on BAT HEAD. BOLT HEAD.
COND BE WLODED TO HANGER.

*If yes, describe in "Remarks" and check "Review Required" box.

DATA TAKEN BY/DATE: Walden/2-11-77

REVIEWED BY/DATE: SEN 2/18/7
(If required)

CONTRACTOR

Scott

AREA

K

ELEVATION

85' ±

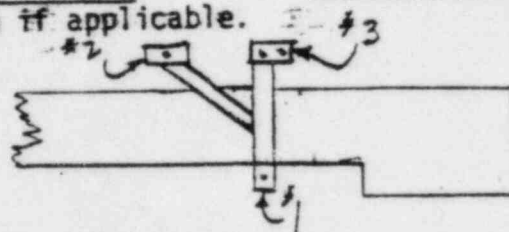
SYSTEM

A/E

LET DOWN HEAT EXCH. 1-1 Room

Sketch of anchor pattern if applicable.

16'



LOOKING EAST

15'

REFERENCE ANCHOR NUMBER (Apply reference numbers to sketch)

1

2

3

ANCHOR TYPE AND SIZE INSTALLED

3/4" P

3/4" P

3/4" P

*OBVIOUS IRREGULARITIES (yes/no)

No

No

No

THREADED END CUT OFF (yes/no)
(If yes, record number of threads remaining in entry. If less than 4 full threads*.)

No

No

No

ANCHOR DEPTH GREATER THAN 1/8"
BELOW SURFACE (yes/no) (If yes, record in entry. If greater than 1/2"*.)

No

No

No

MORE THAN 5 DEGREES FROM PERPEN-
DICULAR (yes/no) (If yes, record in entry. If greater than 15°*.)

No

No

No

AS FOUND PLUG DEPTH

AS LEFT PLUG DEPTH (If not within +1/16" of fully driven acceptance criteria*.)

4 3/32" long
2 3/32"

1 23/32"
1 23/32"

5 1/32" long
2 4/32"
2 4/32"
5 1/32" long

DISTANCE PLUG DRIVEN BY RESETTING

0

0

0

POSSIBLE EXP. END CUT OFF (yes/no)

No

No

No

REMARKS

*If yes, describe in "Remarks" and check "Review Required" box.

DATA TAKEN BY/DATE: W. Allen / 2-15-77REVIEWED BY/DATE: JEN 2/18/77
(If required)

00373-1756

4 anchors)

CONTRACTOR

SATT

AREA

K

ELEVATION

85'

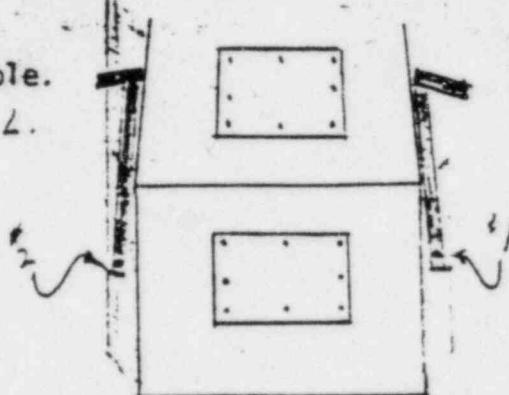
SYSTEM

A/2

Sketch of anchor pattern if applicable.

UNIT ON 17th LINE WALL.

Looking South



REFERENCE ANCHOR NUMBER (Apply reference numbers to sketch)

1

2

ANCHOR TYPE AND SIZE INSTALLED

1/2 H

1/2 H

*OBVIOUS IRREGULARITIES (yes/no)

No

No

THREADED END CUT OFF (yes/no)
(If yes, record number of threads remaining in entry. If less than 4 full threads*.)

No

No

ANCHOR DEPTH GREATER THAN 1/8"
BELOW SURFACE (yes/no) (If yes,
record in entry. If greater than
1/2"*.)

- 2/32

- 7/32

MORE THAN 5 DEGREES FROM PERPEN-
DICULAR (yes/no) (If yes, record
in entry. If greater than 15°*.)

No

No

AS FOUND PLUG DEPTH

31/32

30/32

1 2/32

AS LEFT PLUG DEPTH (If not
within +1/16" of fully driven
acceptance criteria*.)

1 1/32

1 0/32

DISTANCE PLUG DRIVEN BY RESETTING

+ 3/32

+ 4/32

POSSIBLE EXP. END CUT OFF (yes/no)

No

No

REMARKS

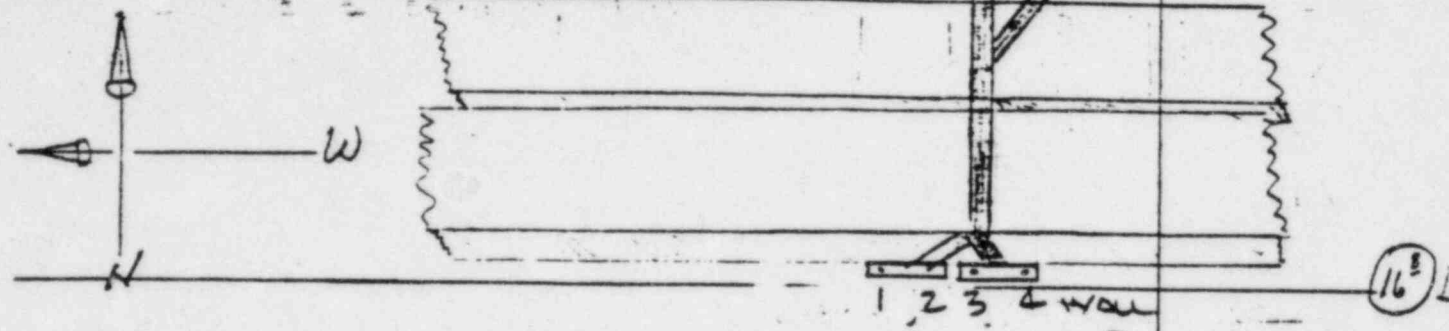
*If yes, describe in "Remarks" and
check "Review Required" box.DATA TAKEN BY/DATE: Wallace/2-15-7REVIEWED BY/DATE: SEN 2/18
(If required)

00373-1757

00373-1758

CONTRACTOR SCOTT AREA K ELEVATION 100' +

SYSTEM A/C (CEILING) ⊕ LINE
Sketch of anchor pattern if applicable.



REFERENCE ANCHOR NUMBER (Apply reference numbers to sketch)	<u>1</u>	<u>2</u>	<u>3</u>	<u>4</u>
ANCHOR TYPE AND SIZE INSTALLED	<u>3/4 P</u>	<u>3/4 P</u>	<u>3/4 P</u>	<u>3/4 P</u>
*OBVIOUS IRREGULARITIES (yes/no)	<u>No</u>	<u>No</u>	<u>No</u>	<u>No</u>
THREADED END CUT OFF (yes/no) (If yes, record number of threads remaining in entry. If less than 4 full threads*.)	<u>No</u>	<u>No</u>	<u>No</u>	<u>No</u>
ANCHOR DEPTH GREATER THAN 1/8" BELOW SURFACE (yes/no) (If yes, record in entry. If greater than 1/2"*.)	<u>No</u>	<u>No</u>	<u>No</u>	<u>No</u>
MORE THAN 5 DEGREES FROM PERPENDICULAR (yes/no) (If yes, record in entry. If greater than 15°*.)	<u>No</u>	<u>No</u>	<u>No</u>	<u>No</u>
AS FOUND PLUG DEPTH	<u>8/32 low</u>	<u>7/32</u>	<u>7/32</u>	<u>7/32</u>
AS LEFT PLUG DEPTH (If not within +1/16" of fully driven acceptance criteria*.)	<u>2 7/32</u> <u>5/32</u>	<u>2 6/32</u> <u>5/32</u>	<u>2 6/32</u> <u>5/32</u>	<u>2 6/32</u> <u>6/32</u>
DISTANCE PLUG DRIVEN BY RESETTING	<u>3/32</u>	<u>2/32</u>	<u>2/32</u>	<u>1/32</u>
POSSIBLE EXP. END CUT OFF (yes/no)	<u>No</u>	<u>No</u>	<u>No</u>	<u>No</u>
REMARKS	<u># Pull test on #4 = 3770 lb anchor displaced 0.010</u> <u>#3: 0.010" @ 980 lbs, 0.235" at 7160 lb</u>			

*If yes, describe in "Remarks" and check "Review Required" box.

DATA TAKEN BY/DATE: Weller/2-14-77
REVIEWED BY/DATE: SEN 2/18/77
(If required)

ANCHOR PULL TEST

CONTRACTOR: SCOTT

ANCHOR LOCATION: EL 100' AREA K NEAR DUNE

ANCHOR REF. No.: #3 DATE: 2/16/77

PERFORMED BY: SS Niemi

<u>GAUGE PRESS.</u>	<u>APPLIED FORCE</u>	<u>MOVEMENT</u>	<u>GAUGE PRESS.</u>	<u>APPLIED FORCE</u>	<u>MOVEMENT</u>
280 PSI	920 PSI	.010 "	1660	6380	.190 "
353	1180	.020	1700	6540	.200 "
440	1540	.030	1850	7160	.235 "
500	1770	.040			
570	2045	.050			
630	2270	.060			
720	2620	.070			
850	3130	.080			
980	3650	.090			
1080	4040	.100			
1180	4420	.110			
1290	4860	.120			
1380	5220	.125			
1390	5280	.140			
1460	5560	.150			
1520	5800	.160			
1590	6090	.170			

3/4 PHILLIPS

Plug driven 9/32"

4 anchors)

CONTRACTOR

Scott

AREA

J

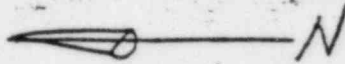
ELEVATION

100' +

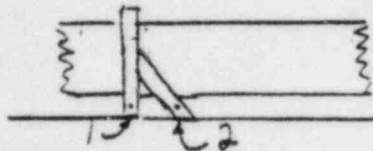
SYSTEM

ATC

Sketch of anchor pattern if applicable.



(u) LINE



Looking up



3' by WALL LINE

SPP HEAT XER RM

REFERENCE ANCHOR NUMBER (Apply reference numbers to sketch)

ANCHOR TYPE AND SIZE INSTALLED

*OBVIOUS IRREGULARITIES (yes/no)

THREADED END CUT OFF (yes/no)
(If yes, record number of threads remaining in entry. If less than 4 full threads*.)

ANCHOR DEPTH GREATER THAN 1/8" BELOW SURFACE (yes/no) (If yes, record in entry. If greater than 1/2"*.)

MORE THAN 5 DEGREES FROM PERPENDICULAR (yes/no) (If yes, record in entry. If greater than 15°*.)

AS FOUND PLUG DEPTH

AS LEFT PLUG DEPTH (If not within +1/16" of fully driven acceptance criteria*.)

DISTANCE PLUG DRIVEN BY RESETTING

POSSIBLE EXP. END CUT OFF (yes/no)

REMARKS #3 PULL TESTED TO 4700 lb, Anchor displaced 0.010

	<u>1</u>	<u>2</u>	<u>3</u>	<u>4</u>
REFERENCE ANCHOR NUMBER				
ANCHOR TYPE AND SIZE INSTALLED	<u>3/4 P</u>	<u>3/4 P</u>	<u>3/4 P</u>	<u>3/4 P</u>
*OBVIOUS IRREGULARITIES (yes/no)	<u>No</u>	<u>No</u>	<u>No</u>	<u>No</u>
THREADED END CUT OFF (yes/no)	<u>No</u>	<u>No</u>	<u>No</u>	<u>No</u>
ANCHOR DEPTH GREATER THAN 1/8" BELOW SURFACE (yes/no)	<u>No</u>	<u>No</u>	<u>- 7/32</u>	<u>No</u>
MORE THAN 5 DEGREES FROM PERPENDICULAR (yes/no)	<u>No</u>	<u>No</u>	<u>No</u>	<u>No</u>
AS FOUND PLUG DEPTH	<u>2 4/32</u>	<u>2 7/32</u>	<u>2 1/32</u>	<u>2 7/32</u>
AS LEFT PLUG DEPTH	<u>2 7/32</u>	<u>2 4/32</u>	<u>2 1/32</u>	<u>2 7/32</u>
DISTANCE PLUG DRIVEN BY RESETTING	<u>0</u>	<u>3/32</u>	<u>0</u>	<u>3/32</u>
POSSIBLE EXP. END CUT OFF (yes/no)	<u>No</u>	<u>No</u>	<u>No</u>	<u>No</u>

*If yes, describe in "Remarks" and check "Review Required" box.

DATA TAKEN BY/DATE: Wally 2-14-77

REVIEWED BY/DATE: SEN 2/18/77
(If required)

00373-1760

CONTRACTOR

Scott

AREA

K

ELEVATION

100' +

SYSTEM

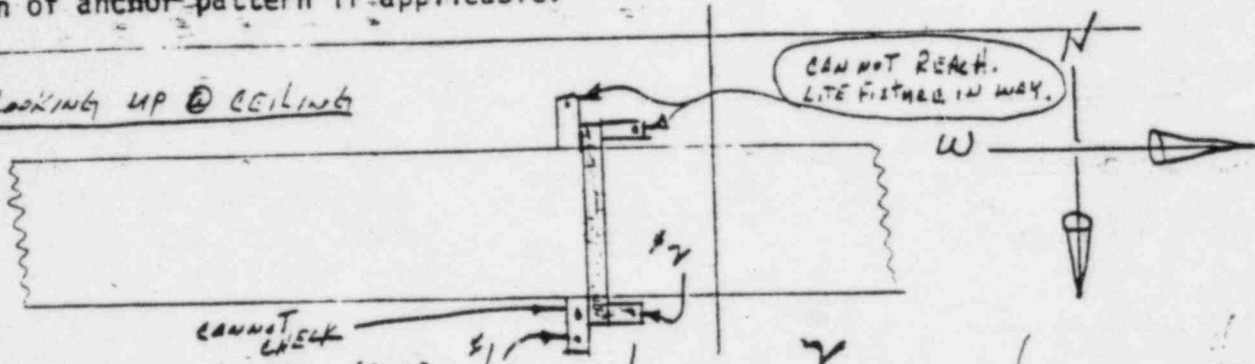
A/C

(5) LINE

Sketch of anchor pattern if applicable.

(16) LINE

Looking up @ ceiling



REFERENCE ANCHOR NUMBER (Apply reference numbers to sketch)

ANCHOR TYPE AND SIZE INSTALLED

*OBVIOUS IRREGULARITIES (yes/no)

THREADED END CUT OFF (yes/no)
(If yes, record number of threads remaining in entry. If less than 4 full threads*.)

ANCHOR DEPTH GREATER THAN 1/8"
BELOW SURFACE (yes/no) (If yes,
record in entry. If greater than
1/2"*.)

MORE THAN 5 DEGREES FROM PERPEN-
DICULAR (yes/no) (If yes, record
in entry. If greater than 15*.)

AS FOUND PLUG DEPTH

AS LEFT PLUG DEPTH (If not
within +1/16" of fully driven
acceptance criteria*.)

DISTANCE PLUG DRIVEN BY RESETTING

POSSIBLE EXP. END CUT OFF (yes/no)

REMARKS

*If yes, describe in "Remarks" and
check "Review Required" box.

DATA TAKEN BY/DATE: Wallen/2-14-7

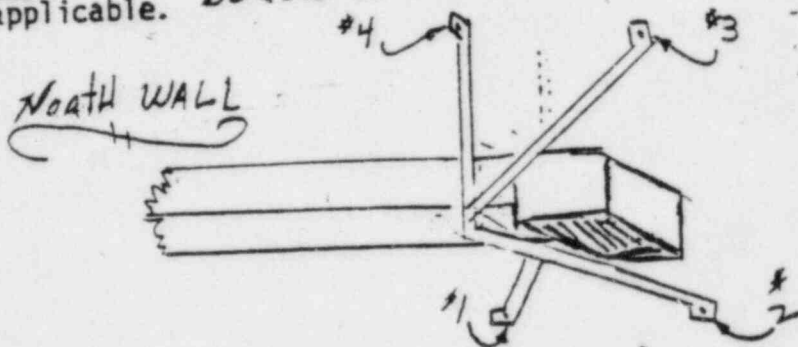
REVIEWED BY/DATE: SEN 2/18/1
(If required)

00373-1761

Page 1 of 1
 Use additional pages if there are more than 4 anchors

CONTRACTOR SLOTT AREA K ELEVATION 100' +

SYSTEM AC
 Sketch of anchor pattern if applicable. Boron Concentration Sys. Tank Area



REFERENCE ANCHOR NUMBER (Apply reference numbers to sketch)

ANCHOR TYPE AND SIZE INSTALLED

*OBVIOUS IRREGULARITIES (yes/no)

THREADED END CUT OFF (yes/no)
 (If yes, record number of threads remaining in entry. If less than 4 full threads*.)

ANCHOR DEPTH GREATER THAN 1/8" BELOW SURFACE (yes/no) (If yes, record in entry. If greater than 1/2"*.)

MORE THAN 5 DEGREES FROM PERPENDICULAR (yes/no) (If yes, record in entry. If greater than 15°*.)

AS FOUND PLUG DEPTH

AS LEFT PLUG DEPTH (If not within +1/16" of fully driven acceptance criteria*.)

DISTANCE PLUG DRIVEN BY RESETTING

POSSIBLE EXP. END CUT OFF (yes/no)

REMARKS

1	2	3	4
<u>3/4 P</u>	<u>3/4 P</u>	<u>3/4 P</u>	<u>3/4 P</u>
<u>NO</u>	<u>NO</u>	<u>NO</u>	<u>NO</u>
<u>NO</u>	<u>NO</u>	<u>NO</u>	<u>NO</u>
<u>1 1/32</u>	<u>NO</u>	<u>NO</u>	<u>NO</u>
<u>1 1/32</u>	<u>NO</u>	<u>NO</u>	<u>NO</u>
<u>1 1/2</u>	<u>NO</u>	<u>NO</u>	<u>NO</u>
<u>1 25/32</u>	<u>4/32</u>	<u>4/32</u>	<u>2/32</u>
<u>1 25/32</u>	<u>2 5/32</u>	<u>2 5/32</u>	<u>2 11/32</u>
	<u>4/32</u>	<u>3/32</u>	<u>2/32</u>
<u>1 1/32</u>	<u>0</u>	<u>1/32</u>	<u>0</u>
<u>NO</u>	<u>NO</u>	<u>NO</u>	<u>NO</u>

*If yes, describe in "Remarks" and check "Review Required" box.

DATA TAKEN BY/DATE: Wallen/2-14-77

REVIEWED BY/DATE: JEN 2/18/77
 (If required)

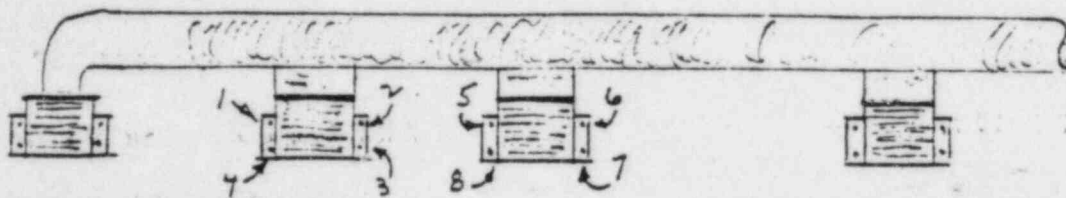
00373-1762

Page 1 of 1
(Use additional pages
if there are more than
4 anchors)

☐ Anchor Installation Okay
☐ Review Required

SUBSET 1

CONTRACTOR SCOTT AREA K ELEVATION 102' +
SYSTEM A/C
Sketch of anchor pattern if applicable.



16 LINE

REFERENCE ANCHOR NUMBER (Apply
reference numbers to sketch)

ANCHOR TYPE AND SIZE INSTALLED

*OBVIOUS IRREGULARITIES (yes/no)

THREADED END CUT OFF (yes/no)
(If yes, record number of threads
remaining in entry. If less than
4 full threads*.)

ANCHOR DEPTH GREATER THAN 1/8"
BELOW SURFACE (yes/no) (If yes,
record in entry. If greater than
1/2"*.)

MORE THAN 5 DEGREES FROM PERPEN-
DICULAR (yes/no) (If yes, record
in entry. If greater than 15°*.)

AS FOUND PLUG DEPTH

AS LEFT PLUG DEPTH (If not
within +1/16" of fully driven
acceptance criteria*.)

DISTANCE PLUG DRIVEN BY RESETTING

POSSIBLE EXP. END CUT OFF (yes/no)

REMARKS

1	2	3	4
<u>1/2 P</u>	<u>1/2 P</u>	<u>1/2 P</u>	<u>1/2 P</u>
<u>No</u>	<u>No</u>	<u>No</u>	<u>No</u>
<u>No</u>	<u>No</u>	<u>No</u>	<u>No</u>
<u>No</u>	<u>No</u>	<u>No</u>	<u>No</u>
<u>No</u>	<u>No</u>	<u>No</u>	<u>No</u>
<u>1 8/32</u>	<u>1 11/32</u> <u>1 1/32 = ONLY</u>	<u>1 10/32</u>	<u>1 6/32</u>
<u>1 8/32</u>	<u>1 7/32</u>	<u>1 7/32</u>	<u>1 5/32</u>
<u>0</u>	<u>2/32</u>	<u>3/32</u>	<u>3/32</u>
<u>NO</u>	<u>NO</u>	<u>NO</u>	<u>NO</u>

MAV = 1 8/32"

*If yes, describe in "Remarks" and
check "Review Required" box.

DATA TAKEN BY/DATE: Walden / 2-14-77

REVIEWED BY/DATE: J2N 2/18/77
(If required)

CONTRACTOR SCH AREA K ELEVATION 102 +
 SYSTEM A/C
 Sketch of anchor pattern if applicable.

SEE SHEET #1

	<u>5</u>	<u>6</u>	<u>7</u>	<u>8</u>
REFERENCE ANCHOR NUMBER (Apply reference numbers to sketch)				
ANCHOR TYPE AND SIZE INSTALLED	<u>1/2 P</u>	<u>1/2 P</u>	<u>1/2 P</u>	<u>1/2 P</u>
*OBVIOUS IRREGULARITIES (yes/no)	<u>No</u>	<u>No</u>	<u>No</u>	<u>No</u>
THREADED END CUT OFF (yes/no) (If yes, record number of threads remaining in entry. If less than 4 full threads*.)	<u>No</u>	<u>No</u>	<u>No</u>	<u>No</u>
ANCHOR DEPTH GREATER THAN 1/8" BELOW SURFACE (yes/no) (If yes, record in entry. If greater than 1/2"*.)	<u>No</u>	<u>No</u>	<u>No</u>	<u>No</u>
MORE THAN 5 DEGREES FROM PERPENDICULAR (yes/no) (If yes, record in entry. If greater than 15°*.)	<u>No</u>	<u>No</u>	<u>No</u>	<u>No</u>
AS FOUND PLUG DEPTH	<u>1 5/8</u>	<u>1 7/8</u>	<u>1 6/8</u>	<u>1 7/8</u>
AS LEFT PLUG DEPTH (If not within +1/16" of fully driven acceptance criteria*.)	<u>1 5/8</u>	<u>1 5/8</u>	<u>1 6/8</u>	<u>1 7/8</u>
DISTANCE PLUG DRIVEN BY RESETTING	<u>0</u>	<u>2 3/8</u>	<u>0</u>	<u>0</u>
POSSIBLE EXP. END CUT OFF (yes/no)	<u>No</u>	<u>No</u>	<u>No</u>	<u>No</u>
REMARKS				

*If yes, describe in "Remarks" and check "Review Required" box.

DATA TAKEN BY/DATE: C. Walker / 2-14-77
 REVIEWED BY/DATE: JEN 2/18/77
 (If required)

0,0373-1764

There are _____ anchors)

CONTRACTOR Scott

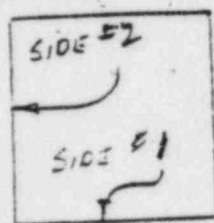
AREA H

ELEVATION 115'

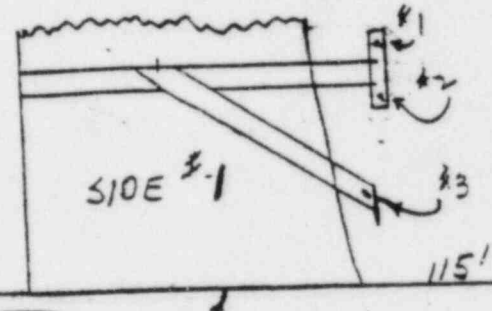
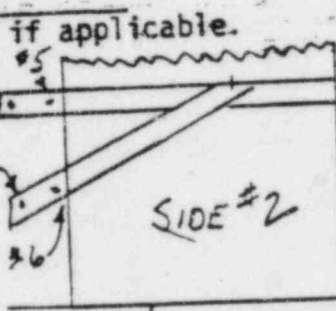
SYSTEM A/C

Sketch of anchor pattern if applicable.

(N) LINE



LOOKING DOWN



REFERENCE ANCHOR NUMBER (Apply reference numbers to sketch)

ANCHOR TYPE AND SIZE INSTALLED

*OBVIOUS IRREGULARITIES (yes/no)

THREADED END CUT OFF (yes/no)
(If yes, record number of threads remaining in entry. If less than 4 full threads*.)

ANCHOR DEPTH GREATER THAN 1/8" BELOW SURFACE (yes/no) (If yes, record in entry. If greater than 1/2"*.)

MORE THAN 5 DEGREES FROM PERPENDICULAR (yes/no) (If yes, record in entry. If greater than 15°*.)

AS FOUND PLUG DEPTH

AS LEFT PLUG DEPTH (If not within +1/16" of fully driven acceptance criteria*.)

DISTANCE PLUG DRIVEN BY RESETTING

POSSIBLE EXP. END CUT OFF (yes/no)

REMARKS #3 Pulled tested: 0.010" at 4350 lb.

1	2	3	4
<u>3/4 P</u>	<u>3/4 P</u>	<u>3/4 P</u>	<u>3/4 P</u>
<u>NO</u>	<u>NO</u>	<u>NO</u>	<u>NO</u>
<u>NO</u>	<u>NO</u>	<u>NO</u>	<u>NO</u>
<u>NO</u>	<u>NO</u>	<u>NO</u>	<u>NO</u>
<u>NO</u>	<u>NO</u>	<u>NO</u>	<u>NO</u>
<u>NO</u>	<u>NO</u>	<u>NO</u>	<u>NO</u>
<u>1 31/32</u>	<u>1 26/32</u>	<u>2 2/32</u>	<u>1 26/32</u>
<u>1 10/32</u>	<u>1 26/32</u>	<u>1 28/32</u>	<u>1 25/32</u>
<u>2/32</u>	<u>0</u>	<u>5/32</u>	<u>1/32</u>
<u>NO</u>	<u>NO</u>	<u>NO</u>	<u>NO</u>

DATA TAKEN BY/DATE: Wallin/2-11-77

REVIEWED BY/DATE: SEN 2/18/
(If required)

*If yes, describe in "Remarks" and check "Review Required" box.

00373-1165

ANCHOR PULL TEST

CONTRACTOR: SCOTT

ANCHOR LOCATION: EL 115' AREA K, NEAR CLEV.

ANCHOR REF. NO.: # 3 DATE: 2/17/77

PERFORMED BY: _____

	<u>GAUGE PRESS.</u>	<u>APPLIED FORCE</u>	<u>Movement</u>		<u>GAUGE PRESS.</u>	<u>APPLIED FORCE</u>	<u>Movement</u>
3	470 PSI.	1650 lb	.001"				
1	900	3340	.002				
6	1000	3730	.003				
0	1040	3895	.004				
0	1070	4000	.005"				
	1090	4080	.006"				
	1120	4200	.007"				
	1120	4200	.008				
	1160	4350	.009"				
	1160	4350	.010"				

3/4" PHILLIPS

PLUG DRIVEN 17/32"

CONTRACTOR

Scott

AREA

H

ELEVATION

115

SYSTEM

A/C

Sketch of anchor pattern if applicable.

SEE SHEET #1

REFERENCE ANCHOR NUMBER (Apply reference numbers to sketch)

ANCHOR TYPE AND SIZE INSTALLED

*OBVIOUS IRREGULARITIES (yes/no)

THREADED END CUT OFF (yes/no)
(If yes, record number of threads remaining in entry. If less than 4 full threads*.)

ANCHOR DEPTH GREATER THAN 1/8" BELOW SURFACE (yes/no) (If yes, record in entry. If greater than 1/2"*.)

MORE THAN 5 DEGREES FROM PERPENDICULAR (yes/no) (If yes, record in entry. If greater than 15*.)

AS FOUND PLUG DEPTH

AS LEFT PLUG DEPTH (If not within +1/16" of fully driven acceptance criteria*.)

DISTANCE PLUG DRIVEN BY RESETTING

POSSIBLE EXP. END CUT OFF (yes/no)

REMARKS #6 Pull test: 0.007" @ 4120 lbs

#7 Pull test: 0.005" @ 6960 lbs

*If yes, describe in "Remarks" and check "Review Required" box.

DATA TAKEN BY/DATE: Walden/2-11-77

REVIEWED BY/DATE: DSD 2/18/77
(If required)

ANCHOR Pull TEST

CONTRACTOR : SCOTT

ANCHOR LOCATION : EL 115', NEXT TO ELEV. AREA K

ANCHOR REF. NO. : # 6 DATE : 2/17/77

PERFORMED BY : SE Nienin

0003731768

<u>GAUGE PRESS.</u>	<u>APPLIED FORCE</u>	<u>MOMENT</u>	<u>GAUGE PRESS.</u>	<u>APPLIED FORCE</u>	<u>MOMENT</u>
200 PSI	600 lb	.003"			
300	980	.005			
360	1230	.006			
470	1660	.007			
1100	4120	.007			

3/4 PHILLIPS
PLUG DRIVEN 15/32"

ANCHOR PULL TEST

CONTRACTOR : SCOTT

ANCHOR LOCATION : EL' 115 NEAR ELEV. AREA 1C

ANCHOR REF. No.: #7 DATE: 2/17/77

PERFORMED BY: SE Njéni

<u>GAUGE PRESS.</u>	<u>APPLIED FORCE</u>	<u>MOVEMENT</u>
600 PSI	2160 lb	.001"
740	2700	.002
900	3340	.003
1100	4120	.003
1300	4910	.004
1800	6960	.008

<u>GAUGE PRESS.</u>	<u>APPLIED FORCE</u>	<u>MOVEMENT</u>
---------------------	----------------------	-----------------

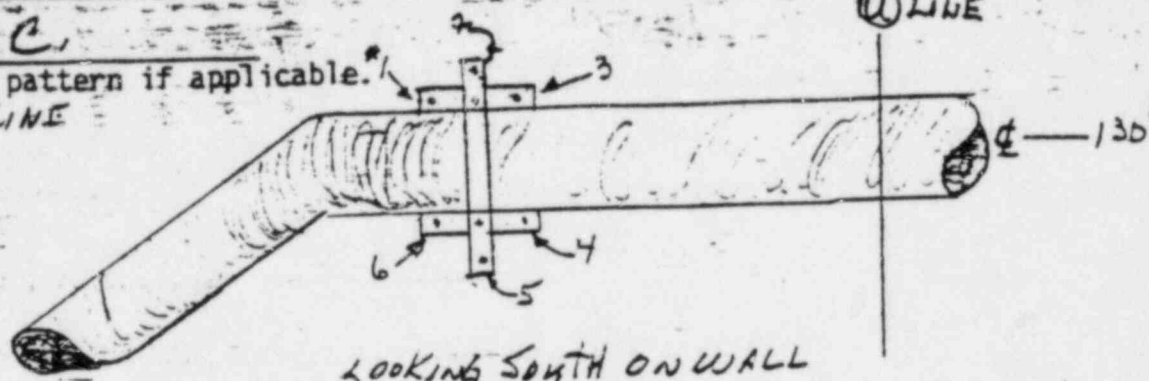
3/4 PHILLIPS
PLUG DRIVEN 18/32"

CONTRACTOR Soot AREA L ELEVATION 115'

SYSTEM A.C.
Sketch of anchor pattern if applicable.

LINE

LINE



REFERENCE ANCHOR NUMBER (Apply reference numbers to sketch)

ANCHOR TYPE AND SIZE INSTALLED

*OBVIOUS IRREGULARITIES (yes/no)

THREADED END CUT OFF (yes/no)
(If yes, record number of threads remaining in entry. If less than 4 full threads*.)

ANCHOR DEPTH GREATER THAN 1/8" BELOW SURFACE (yes/no) (If yes, record in entry. If greater than 1/2"*.)

MORE THAN 5 DEGREES FROM PERPENDICULAR (yes/no) (If yes, record in entry. If greater than 15*.)

AS FOUND PLUG DEPTH

AS LEFT PLUG DEPTH (If not within +1/16" of fully driven acceptance criteria*.)

DISTANCE PLUG DRIVEN BY RESETTING

POSSIBLE EXP. END CUT OFF (yes/no)

REMARKS

MAX ALLOWABLE = 1 18/32"

1	2	3	4
5/8P	5/8P	5/8P	5/8P
No	No	No	No
No	No	No	No
No	No	No	No
No	No	No	No
No	No	No	No
1 20/32	1 18/32	1 20/32	1 19/32
1 14/32	1 17/32	1 14/32	1 17/32
4/32	1/32	1/32	2/32
No	No	No	No

*If yes, describe in "Remarks" and check "Review Required" box.

DATA TAKEN BY/DATE: Walsh/2-15-7

REVIEWED BY/DATE: SEN 2/18/7
(If required)

CONTRACTOR

Scott

AREA

2

ELEVATION

115' 7

SYSTEM

A/C

Sketch of anchor pattern if applicable.

REFERENCE ANCHOR NUMBER (Apply reference numbers to sketch)

ANCHOR TYPE AND SIZE INSTALLED

*OBVIOUS IRREGULARITIES (yes/no)

THREADED END CUT OFF (yes/no)
(If yes, record number of threads remaining in entry. If less than 4 full threads*.)

ANCHOR DEPTH GREATER THAN 1/8" BELOW SURFACE (yes/no) (If yes, record in entry. If greater than 1/2"*.)

MORE THAN 5 DEGREES FROM PERPENDICULAR (yes/no) (If yes, record in entry. If greater than 15°*.)

AS FOUND PLUG DEPTH

AS LEFT PLUG DEPTH (If not within +1/16" of fully driven acceptance criteria*.)

DISTANCE PLUG DRIVEN BY RESETTING

POSSIBLE EXP. END CUT OFF (yes/no)

REMARKS

5

6

5/8 P

5/8 P

No

No

No

No

No

No

No

No

17/32

17/32

3/32

4/32

No

No

MAX ALLOWABLE = 18/32

DATA TAKEN BY/DATE: C. Wallum / 2-15-77

REVIEWED BY/DATE: SEN 2/19
(If required)

*If yes, describe in "Remarks" and check "Review Required" box.

00373-1771

ANCHOR Pull TEST

CONTRACTOR : SCOTT

ANCHOR LOCATION : FIRE PUMP ROOM, EL 115'

ANCHOR REF. No.: #5 DATE: 2/17/77

PERFORMED BY: JE Niemi

	<u>GAUGE PRESS.</u>	<u>APPLIED FORCE</u>	<u>MOVEMENT</u>		<u>GAUGE PRESS.</u>	<u>APPLIED FORCE</u>	<u>MOVEMENT</u>
3	650 PSI	2350 lb	0.001"		1020	3810	0.019
0	700	2550	0.002		1050	3840	0.020
0	725	2640	0.003		1080	4040	0.022
	750	2740	0.004		1100	4110	0.023
	800	2930	0.005		1110	4160	0.024
	825	3040	0.006		1125	4210	0.025
	835	3070	0.007		1150	4320	0.026
	850	3140	0.008				
	875	3230	0.009				
	900	3340	0.010				
	910	3380	0.011				
	920	3410	0.012				
	930	3450	0.013				
	940	3500	0.014				
	950	3530	0.015				
	975	3630	0.016				

5/8 PHILLIPS
PLUG DRIVEN 16/32"

PACIFIC GAS AND ELECTRIC COMPANY
STATION CONSTRUCTION DEPARTMENT
Diablo Canyon Project

SAN FRANCISCO TELEPHONE CALLS

INCOMING ☐

OUTGOING ☒

PERSON CALLED: ELLIOTT NICHOLS

DATE CALLED:

MARCH 2, 1977

TIME: 0810

SUBJECT:

ACCEPTABLE LIMITS FOR MOVEMENTS
OF THE CLASS I A/C DUCTWORK

DRAWING NO.

CHG: ☒

SPEC. NO.: 8727 4R NO.: ☒

REASON FOR CALL:

TO VERIFY WITH THE RESPONSIBLE
ENGINEER THAT THE A/C DUCTS CAN
TOLERATE THE SMALL MOVEMENTS THAT COULD
OCCUR WHEN THE CONCRETE ARCHES SUPPORTING
THE DUCTS ARE SUBJECTED TO DESIGN
LOADS.

DATE OF REPLY:

SAME

TIME:

SAME

REPLY RECEIVED:

NICHOLS SAID THAT SLIGHT DEFORMATIONS
OF THE SHEET METAL CAUSED BY DUCT
MOVEMENTS UP TO ONE INCH ARE ACCEPTABLE.
H.E. STATED THAT THE SMALL ARCHES MOVEMENTS
(0.120" TO 0.160") CAN BE EASILY TOLERATED
BY THE DUCTWORK.

NOTE: (1) FOLLOW UP ON EACH CALL, VENDOR PROBLEMS, ENGINEERING CHANGES, ETC. KEEP
CLOSE CHECK FOR TIME LAPSE BETWEEN DATE CALLED AND ANSWER TO CALL OR PROBLEM.
(2) IF THIS CONVERSATION CONSTITUTES A DES. CHANGE, THE RESPECTIVE CONTRACTOR AND
DESIGN ENGINEER WILL RECEIVE A COPY.

SIGNED:

DE Miami

CHECK

Call Change
Drawing Change

Copy is to be returned
to Ingr. Dept. for
their information

Call requires a
Contractor DNR

INSTALLATION OF HILTI ANCHORS
(LROP INS)

- 0033778
- (1) Obtain proper drill and setting tool for size anchor being installed using Figure 1 for reference.
 - (2) Drill hole indicated in Figure 1 (hole depth indicated does not include conical section caused by drill point) keeping drill perpendicular to concrete surface. Finished hole must be perpendicular to concrete surface with a maximum deviation of 5°.
 - (3) Insert anchor and assure that expander is in anchor. (NOTE) Top of anchor must be flush or slightly recessed (not to exceed 1/8") from concrete surface.
 - (4) Using proper setting tool expand anchor by driving expander plug until shoulder on the tool is flush with top of anchor.
 - (5) Using your assigned I.D. Symbol stamp the head of bolt in each anchor you have installed.
 - (6) Center to center spacing of anchors shall not be less than 12 nominal diameters and distance to edge of concrete shall not be less than 3" or less than 6 diameters, whichever is greater, except when design or lack of space dictates otherwise. (Refer to Figure 2)
 - (7) When, due to encounter with steel a new hole is drilled, a minimum of 1" solid concrete must be left between holes. If new hole is within 4½ diameters of the original hole the blank hole must be grouted.
 - (8) If completed installation appears discrepant in any manner the employee shall notify Scott Co. Q.C. Inspector immediately.

APPROVAL (AS NOTED)	
<input type="checkbox"/>	Approved as to Substance
<input type="checkbox"/>	Subject to Notations Shown
<input type="checkbox"/>	Not Approved
<input type="checkbox"/>	Revised Drawings Required
<input type="checkbox"/>	Furnish Reproducibles
<input checked="" type="checkbox"/>	Approved for Constr.
Resident Engineer <u>R. D. T. V. A.</u>	
By <u>R. D. T. V. A.</u>	Date <u>4/9/77</u>
PACIFIC GAS & ELECTRIC CO. Diablo Canyon	

ANCHOR Pull TEST

CONTRACTOR : SCOTT

ANCHOR LOCATION : EL 115' FIRE PUMP ROOM

ANCHOR REF. No.: #3 DATE: 2/17/77

PERFORMED BY: AE Niemi

GAUGE PRESS.	APPLIED FORCE	MOVEMENT	GAUGE PRESS.	APPLIED FORCE	MOVEMENT
110 PSI	310 lb	.002"	721	2621	0.020
150	430	.003	750	2740	.022
170	500	.004	800	2930	.023
210	620	.005	840	3100	.024
240	760	.006	880	3260	.025
280	910	.007	900	3340	.026
320	1070	.008	950	3540	.027
360	1230	.009	990	3700	.028
420	1450	.010	1020	3800	.029
450	1580	.011	1050	3920	.030
530	1880	.012	1070	4000	.031
630	2180	.013	1100	4120	.032
650	2350	.015	1120	4200	.033
670	2430	.016	1140	4280	.034
680	2470	.017	1150	4320	.035
700	2550	.018			

5/8 PHILLIPS
15/16"

ANCHOR PULL TEST

CONTRACTOR: SCOTT

ANCHOR LOCATION: ELIIS' FIRE PUMP ROOM

ANCHOR REF. NO.: #4 DATE: 2/17/77

PERFORMED BY: SE Niemi

<u>GAUGE PRESS.</u>	<u>APPLIED FORCE</u>	<u>MOVEMENT</u>	<u>GAUGE PRESS.</u>	<u>APPLIED FORCE</u>	<u>MOVEMENT</u>
0 300 psi	980	0.002"			
0 325	1080	0.003			
825	3040	0.004			
875	3240	0.005			
900	3340	0.006			
925	3430	0.007			
950	3530	0.008			
1000	3720	0.010			
1050	3930	0.011			
1075	4020	0.012			
1100	4120	0.013			
1125	4210	0.014			
1150	4330	0.015			

S/B PHILLIPS
PWG DRIVEN 13/32

CONTRACTOR

Scott

AREA

J

ELEVATION

115' +

SYSTEM

A/E

Sketch of anchor pattern if applicable.

SEE SHEET #1

00373-1/15

REFERENCE ANCHOR NUMBER (Apply reference numbers to sketch)

5

ANCHOR TYPE AND SIZE INSTALLED

5/8 P

*OBVIOUS IRREGULARITIES (yes/no)

NO

THREADED END CUT OFF (yes/no)
(If yes, record number of threads remaining in entry. If less than 4 full threads*.)

NO

ANCHOR DEPTH GREATER THAN 1/8" BELOW SURFACE (yes/no) (If yes, record in entry. If greater than 1/2"*.)

NO

MORE THAN 5 DEGREES FROM PERPENDICULAR (yes/no) (If yes, record in entry. If greater than 15*.)

NO

AS FOUND PLUG DEPTH

1 26/32

AS LEFT PLUG DEPTH (If not within +1/16" of fully driven acceptance criteria*.)

1 26/32

DISTANCE PLUG DRIVEN BY RESETTING

75"

POSSIBLE EXP. END CUT OFF (yes/no)

NO

REMARKS

*If yes, describe in "Remarks" and check "Review Required" box.

DATA TAKEN BY/DATE: Warden/2-15-7

REVIEWED BY/DATE: SSN 2/18
(If required)

CONTRACTOR

SCOTT

AREA

J

ELEVATION

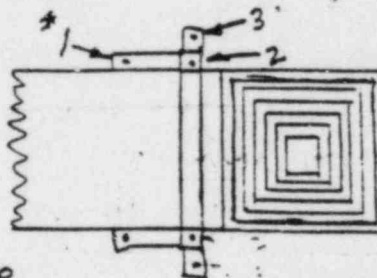
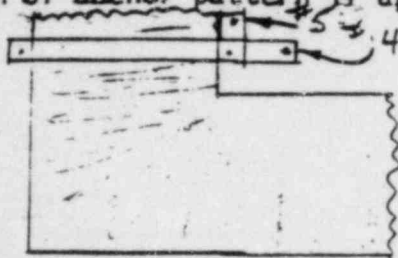
115' +

SYSTEM

A/C

Sketch of anchor pattern if applicable.

Aux. FW. HYDRAZINE & Ammonia PPS. Rm.



Looking UP

REFERENCE ANCHOR NUMBER (Apply reference numbers to sketch)

1

2

3

4

ANCHOR TYPE AND SIZE INSTALLED

5/8P

5/8P

5/8P

5/8P

*OBVIOUS IRREGULARITIES (yes/no)

No

No

No

No

THREADED END CUT OFF (yes/no)
(If yes, record number of threads remaining in entry. If less than 4 full threads*.)

No

No

No

No

ANCHOR DEPTH GREATER THAN 1/8" BELOW SURFACE (yes/no) (If yes, record in entry. If greater than 1/2"*.)

No

No

No

No

MORE THAN 5 DEGREES FROM PERPENDICULAR (yes/no) (If yes, record in entry. If greater than 15°*.)

No

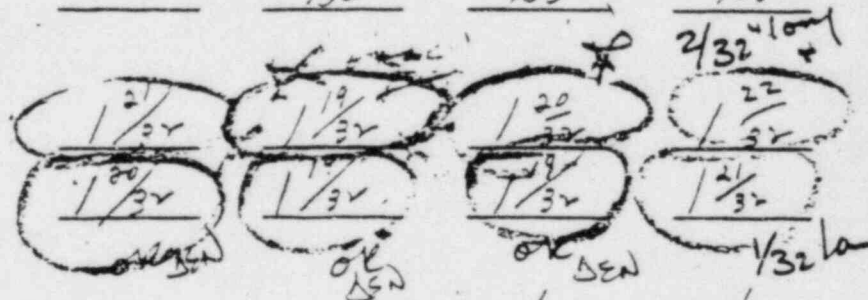
No

No

No

AS FOUND PLUG DEPTH

AS LEFT PLUG DEPTH (If not within +1/16" of fully driven acceptance criteria*.)



DISTANCE PLUG DRIVEN BY RESETTING

1/32

0

1/32

1/32

POSSIBLE EXP. END CUT OFF (yes/no)

no

no

no

no

REMARKS #3 Pull tested: 1450 lbs; 0.010" @ 4320#, 0.034"

#4 Pull tested: 0.010" @ 3725#, 0.015" @ 4320#

#5 Pull tested: 0.010" @ 3240#, 0.026" @ 4320#

*If yes, describe in "Remarks" and check "Review Required" box.

DATA TAKEN BY/DATE: W. W. W. / 2-15-77

REVIEWED BY/DATE: D. W. W. / 2/18/77
(If required)

Page 1 of 1
 (Use additional pages
 if there are more than
 4 anchors)

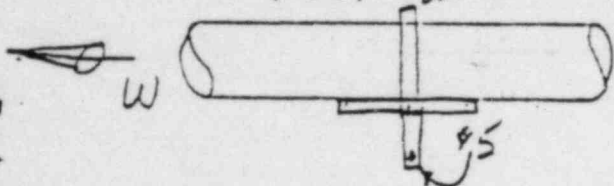
☐ Anchor Installation Okay
☐ Review Required

CONTRACTOR Scott AREA K ELEVATION 60'

SYSTEM A/C

Sketch of anchor pattern if applicable.

NORTH WALL



MONITOR TANK 1-1 AREA
SEE SHEET #1

REFERENCE ANCHOR NUMBER (Apply
reference numbers to sketch)

ANCHOR TYPE AND SIZE INSTALLED

*OBVIOUS IRREGULARITIES (yes/no)

THREADED END CUT OFF (yes/no)
 (If yes, record number of threads
 remaining in entry. If less than
 4 full threads*.)

ANCHOR DEPTH GREATER THAN 1/8"
 BELOW SURFACE (yes/no) (If yes,
 record in entry. If greater than
 1/2"*.)

MORE THAN 5 DEGREES FROM PERPEN-
 DICULAR (yes/no) (If yes, record
 in entry. If greater than 15°*.)

AS FOUND PLUG DEPTH

AS LEFT PLUG DEPTH (If not
 within +1/16" of fully driven
 acceptance criteria*.)

DISTANCE PLUG DRIVEN BY RESETTING

POSSIBLE EXP. END CUT OFF (yes/no)

REMARKS

<u>5</u>			
<u>5/8P</u>			
<u>NO</u>			
<u>NO</u>			
<u>NO</u>			
<u>NO</u>			
<u>NO</u>			
<u>1 16/32</u>			
<u>1 15/32</u>			
<u>1 3/32</u>			
<u>NO</u>			

*If yes, describe in "Remarks" and
 check "Review Required" box.

DATA TAKEN BY/DATE: Walter / 2-11-77

REVIEWED BY/DATE: SEP 2/18/77
 (If required)

00373-1743

Page 1 of 1
 1. There are 4 anchors.

SHEET 1

CONTRACTOR

Scott

AREA

K

ELEVATION

60.1

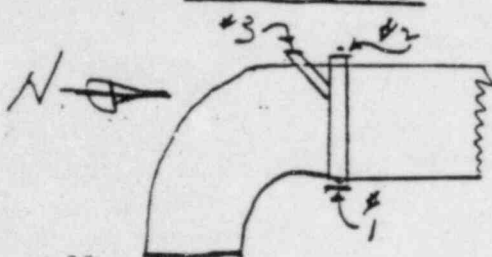
SYSTEM

A/C

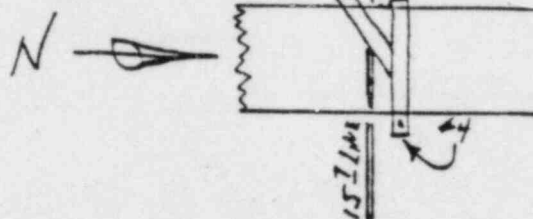
Sketch of anchor pattern if applicable.

Monitor Tank #1-1

WEST WALL



WEST WALL



REFERENCE ANCHOR NUMBER (Apply reference numbers to sketch)

ANCHOR TYPE AND SIZE INSTALLED

*OBVIOUS IRREGULARITIES (yes/no)

THREADED END CUT OFF (yes/no)
 (If yes, record number of threads remaining in entry. If less than 4 full threads*.)

ANCHOR DEPTH GREATER THAN 1/8"
 BELOW SURFACE (yes/no) (If yes, record in entry. If greater than 1/2"*.)

MORE THAN 5 DEGREES FROM PERPEN-
 DICULAR (yes/no) (If yes, record in entry. If greater than 15°*.)

AS FOUND PLUG DEPTH

AS LEFT PLUG DEPTH (If not within +1/16" of fully driven acceptance criteria*.)

DISTANCE PLUG DRIVEN BY RESETTING

POSSIBLE EXP. END CUT OFF (yes/no)

REMARKS

1	2	3	4
3/4 P	3/4 P	3/4 P	3/4 P
No			No
No			No
No			No
No			No
No			No
1 29/32			1 28/32
1 28/32			1 28/32
1/32			0
No			No

CANNOT GET READINGS BECAUSE OF SPINDLING ANCHOR.

CANNOT GET READINGS BECAUSE, CANNOT GET WRENCH OR SOCKET ON BOLT HEAD, AS STEEL & CONCRETE ARE TOO CLOSE TO BOLT.

*If yes, describe in "Remarks" and check "Review Required" box.

DATA TAKEN BY/DATE: Walden/2-11-77

REVIEWED BY/DATE: SEN 2/18/77
 (If required)

00373-1744

ANCHOR INSPECTION CHECK LIST

Page 1 of 1
(Use additional pages if there are more than 4 anchors)

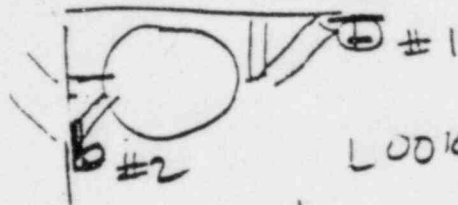
☒ Anchor Installation Okay
☐ Review Required

CONTRACTOR SCOTT AREA K ELEVATION 64

SYSTEM A/C
Sketch of anchor pattern if applicable.

VALVE ROOM BETWEEN
RHR PUMPS,

NORTH EAST CORNER OF ROOM, 2' ABOVE FLOOR
GRATING



REFERENCE ANCHOR NUMBER (Apply reference numbers to sketch)	1	2		
ANCHOR TYPE AND SIZE INSTALLED	<u>S/S P</u>	<u>S/S P</u>	<u></u>	<u></u>
*OBVIOUS IRREGULARITIES (yes/no)	<u>NO</u>	<u>NO</u>	<u></u>	<u></u>
THREADED END CUT OFF (yes/no) (If yes, record number of threads remaining in entry. If less than 4 full threads*.)	<u>NO</u>	<u>NO</u>	<u></u>	<u></u>
ANCHOR DEPTH GREATER THAN 1/8" BELOW SURFACE (yes/no) (If yes, record in entry. If greater than 1/2"*.)	<u>NO</u>	<u>NO</u>	<u></u>	<u></u>
MORE THAN 5 DEGREES FROM PERPENDICULAR (yes/no) (If yes, record in entry. If greater than 15°*.)	<u>NO</u>	<u>NO</u>	<u></u>	<u></u>
AS FOUND PLUG DEPTH Plug to shoulder	<u>1 1/32</u>	<u>1 3/32</u>	<u></u>	<u></u>
AS LEFT PLUG DEPTH (If not within +1/16" of fully driven acceptance criteria*.)	<u>1 5/32</u>	<u>1 1/32</u>	<u></u>	<u></u>
DISTANCE PLUG DRIVEN BY RESETTING	<u>1/32</u>	<u>1/32</u>	<u></u>	<u></u>
POSSIBLE EXP. END CUT OFF (yes/no)	<u>NO</u>	<u>NO</u>	<u></u>	<u></u>

REMARKS -

*If yes, describe in "Remarks" and check "Review Required" box.

DATA TAKEN BY/DATE: A E Nimm 2/1

REVIEWED BY/DATE: AND 2/18/12

00373-1/45

Page 1 of 1
 Date installed
 if there are more than
 4 anchors)

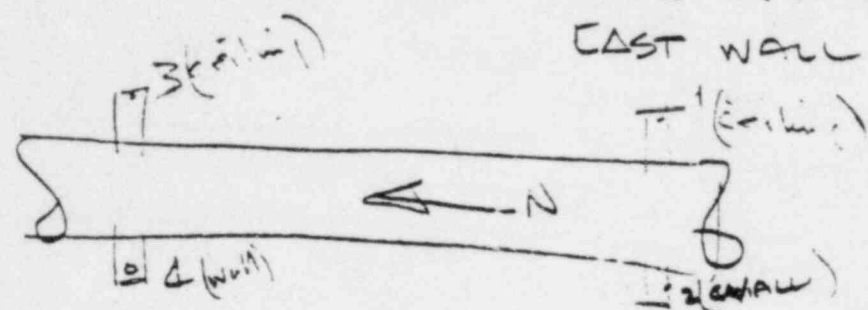
☒ Review Required

CONTRACTOR SCOTT AREA K ELEVATION 64

SYSTEM AIR CONDIT.

Sketch of anchor pattern if applicable.

WATER CHAMBER ROOM #1-1
 EAST WALL 8' ABOVE FLOOR



REFERENCE ANCHOR NUMBER (Apply reference numbers to sketch)	<u>1</u>	<u>2</u>	<u>3</u>	<u>4</u>
ANCHOR TYPE AND SIZE INSTALLED	<u>5/8"</u>	<u>5/8"</u>	<u>5/8"</u>	<u>5/8"</u>
*OBVIOUS IRREGULARITIES (yes/no)	<u>NO</u>	<u>NO</u>	<u>NO</u>	<u>NO</u>
THREADED END CUT OFF (yes/no) (If yes, record number of threads remaining in entry. If less than 4 full threads*.)	<u>NO</u>	<u>NO</u>	<u>NO</u>	<u>NO</u>
ANCHOR DEPTH GREATER THAN 1/8" BELOW SURFACE (yes/no) (If yes, record in entry. If greater than 1/2"*.)	<u>NO</u>	<u>NO</u>	<u>NO</u>	<u>NO</u>
MORE THAN 5 DEGREES FROM PERPENDICULAR (yes/no) (If yes, record in entry. If greater than 15°*.)	<u>NO</u>	<u>NO</u>	<u>NO</u>	<u>NO</u>
AS FOUND PLUG DEPTH	<u>1 13/32</u>	<u>1 17/32</u>	<u>1 17/32</u>	<u>1 14/32</u>
AS LEFT PLUG DEPTH (If not within +1/16" of fully driven acceptance criteria*.)	<u>1 11/32</u>	<u>1 17/32</u>	<u>1 14/32</u>	<u>1 15/32</u>
DISTANCE PLUG DRIVEN BY RESETTING	<u>2/32</u>	<u>0</u>	<u>1/32</u>	<u>1/32</u>
POSSIBLE EXP. END CUT OFF (yes/no)	<u>NO</u>	<u>NO</u>	<u>NO</u>	<u>NO</u>

REMARKS * Pull testd #2: 0.010" @ 2010 lbs, 0.045 @ 2750
approx 1/8" @ 4340 lbs.

*If yes, describe in "Remarks" and check "Review Required" box.

DATA TAKEN BY/DATE: JEN 2/10/77

REVIEWED BY/DATE: JEN 2/18/77
 (If required)

00373-1746

ANCHOR PULL TEST

CONTRACTOR: SCOTT

ANCHOR LOCATION: EL 64' WATER CHAMBER 1-1 RM

ANCHOR REF. No.: #2 DATE: 2/17/77

PERFORMED BY: SE Niemi

	<u>GAUGE PRESS.</u>	<u>APPLIED FORCE</u>	<u>MOVEMENT</u>		<u>GAUGE PRESS.</u>	<u>APPLIED FORCE</u>	<u>MOVEMENT</u>
7							
3							
7							
4							
7							
0							
0	510 PSI	1610 lb.	0.003"				
0	530	1850	.004				
	540	1930	.006				
	550	1960	.008				
	560	2010	.010				
	570	2040	.015				
	580	2080	.019				
	610	2200	.025				
	630	2280	.030				
	660	2390	.035				
	710	2580	.040				
	760	2780	.045				

TOTAL ANCHOR DISPLACEMENT
WAS $2 \frac{1}{8}$ " AT
1150 PSI, 4320 lb.

$5/8$ PHILLIPS
PLUG DRIVEN $17/32$ "

DESIGN LOAD in 5 KIP
CONCRETE
2100 lbs

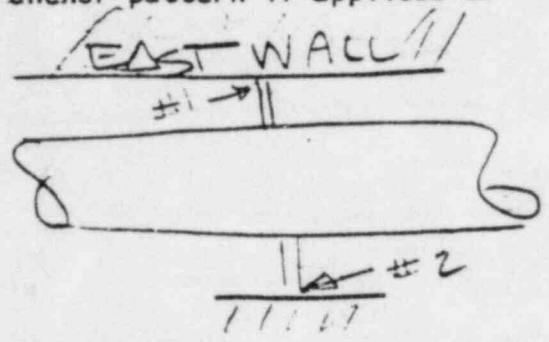
DIAL INDICATOR
WAS BUMPED, READINGS
BEYOND .045"
WERE NOT TAKEN

Page 1 of 1
(Use additional pages if there are more than 4 anchors)

CONTRACTOR SCOTT AREA K ELEVATION 64

SYSTEM A/C
Sketch of anchor pattern if applicable.

Borax injection tank room



6' Above floor

REFERENCE ANCHOR NUMBER (Apply reference numbers to sketch)	<u>1</u>	<u>2</u>		
ANCHOR TYPE AND SIZE INSTALLED	<u>5/8P</u>	<u>5/8P</u>		
*OBVIOUS IRREGULARITIES (yes/no)	<u>NO</u>	<u>NO</u>		
THREADED END CUT OFF (yes/no) (If yes, record number of threads remaining in entry. If less than 4 full threads*.)	<u>NO</u>	<u>NO</u>		
ANCHOR DEPTH GREATER THAN 1/8" BELOW SURFACE (yes/no) (If yes, record in entry. If greater than 1/2"*.)	<u>NO</u>	<u>NO</u>		
MORE THAN 5 DEGREES FROM PERPENDICULAR (yes/no) (If yes, record in entry. If greater than 15°*.)	<u>NO</u>	<u>NO</u>		
AS FOUND PLUG DEPTH	<u>1 17/32</u>	<u>1 17/32</u>		
AS LEFT PLUG DEPTH (If not within +1/16" of fully driven acceptance criteria*.)	<u>1 14/32</u>	<u>1 7/32</u>		
DISTANCE PLUG DRIVEN BY RESETTING	<u>30/32</u>	<u>0</u>		
POSSIBLE EXP. END CUT OFF (yes/no)	<u>NO</u>	<u>NO</u>		
REMARKS				

*If yes, describe in "Remarks" and check "Review Required" box.

DATA TAKEN BY/DATE: SE Niemi 2/10/

REVIEWED BY/DATE: SEN 2/18/
(If required)

00373-1748

Page 1 of 2
 (Use additional pages
 if there are more than
 4 anchors)

☒ Anchor Installation Okay
☐ Review Required

CONTRACTOR SCOTT AREA K ELEVATION 64'

SYSTEM AIR CONDITIONING
 Sketch of anchor pattern if applicable.

00373-1/49

REQUIREMENTS WATER
 CHAMBER Rm 1-2
 WEST WALL 6'6" ABOVE
 FLOOR

REFERENCE ANCHOR NUMBER (Apply reference numbers to sketch)	1	2	3	4
ANCHOR TYPE AND SIZE INSTALLED	<u>5/8"</u>	<u>5/8"</u>	<u>5/8"</u>	<u>7/8"</u>
*OBVIOUS IRREGULARITIES (yes/no)	<u>NO</u>	<u>NO</u>	<u>NO</u>	<u>NO</u>
THREADED END CUT OFF (yes/no) (If yes, record number of threads remaining in entry. If less than 4 full threads*.)	<u>NO</u>	<u>NO</u>	<u>NO</u>	<u>NO</u>
ANCHOR DEPTH GREATER THAN 1/8" BELOW SURFACE (yes/no) (If yes, record in entry. If greater than 1/2"*.)	<u>NO</u>	<u>NO</u>	<u>NO</u>	<u>NO</u>
MORE THAN 5 DEGREES FROM PERPENDICULAR (yes/no) (If yes, record in entry. If greater than 15°*.)	<u>NO</u>	<u>NO</u>	<u>NO</u>	<u>NO</u>
AS FOUND PLUG DEPTH <u>Should be to</u>	<u>1 17/32</u>	<u>1 15/32</u>	<u>1 18/32</u>	<u>1 16/32</u>
AS LEFT PLUG DEPTH (If not within +1/16" of fully driven acceptance criteria*.)	<u>1 15/32</u>	<u>1 15/32</u>	<u>1 16/32</u>	<u>1 15/32</u>
DISTANCE PLUG DRIVEN BY RESETTING	<u>2 3/32</u>	<u>2 3/32</u>	<u>2 3/32</u>	<u>1 3/32</u>
POSSIBLE EXP. END CUT OFF (yes/no)	<u>NO</u>	<u>NO</u>	<u>NO</u>	<u>NO</u>
REMARKS				

*If yes, describe in "Remarks" and check "Review Required" box.

DATA TAKEN BY/DATE: DE Niewi 2/16/7
 REVIEWED BY/DATE: SEN 2/18/7
 (If required)

Page 2 of 2
 (Use additional pages
 if there are more than
 4 anchors)

Anchor Installation Okay

☐ Review Required

CONTRACTOR

SCOTT

AREA

K

ELEVATION

144

SYSTEM

A/C

Sketch of anchor pattern if applicable.

See page 1

REFERENCE ANCHOR NUMBER (Apply
reference numbers to sketch)

5

6

ANCHOR TYPE AND SIZE INSTALLED

5/8P

5/8P

*OBVIOUS IRREGULARITIES (yes/no)

NO

NO

THREADED END CUT OFF (yes/no)
(If yes, record number of threads
remaining in entry. If less than
4 full threads*.)

NO

NO

ANCHOR DEPTH GREATER THAN 1/8"
BELOW SURFACE (yes/no) (If yes,
record in entry. If greater than
1/2"*.)

NO

1/8

MORE THAN 5 DEGREES FROM PERPEN-
DICULAR (yes/no) (If yes, record
in entry. If greater than 15°*.)

NO

50

AS FOUND PLUG DEPTH

1 12/32

1 14/32

AS LEFT PLUG DEPTH (If not
within +1/16" of fully driven
acceptance criteria*.)

1 12/32

1 12/32

DISTANCE PLUG DRIVEN BY RESETTING

1/32

2/32

POSSIBLE EXP. END CUT OFF (yes/no)

NO

NO

REMARKS

*If yes, describe in "Remarks" and
 check "Review Required" box.

DATA TAKEN BY/DATE: 18/10/7
 REVIEWED BY/DATE: SEN 2/18/7
 (If required)

00373-1750

if there are more than
4 anchors)

CONTRACTOR

SCOT

AREA

K

ELEVATION

121

SYSTEM

ATC

Sketch of anchor pattern if applicable.

See page 1

REFERENCE ANCHOR NUMBER (Apply
reference numbers to sketch)

5

6

ANCHOR TYPE AND SIZE INSTALLED

S/BP

S/BP

*OBVIOUS IRREGULARITIES (yes/no)

NO

NO

THREADED END CUT OFF (yes/no)
(If yes, record number of threads
remaining in entry. If less than
4 full threads*.)

NO

NO

ANCHOR DEPTH GREATER THAN 1/8"
BELOW SURFACE (yes/no) (If yes,
record in entry. If greater than
1/2"*.)

NO

1/8

MORE THAN 5 DEGREES FROM PERPEN-
DICULAR (yes/no) (If yes, record
in entry. If greater than 15*.)

NO

OK
50

AS FOUND PLUG DEPTH

1 13/32

1 14/32

AS LEFT PLUG DEPTH (If not
within +1/16" of fully driven
acceptance criteria*.)

1 12/32

1 12/32

DISTANCE PLUG DRIVEN BY RESETTING

1/32

2/32

POSSIBLE EXP. END CUT OFF (yes/no)

NO

NO

REMARKS

*If yes, describe in "Remarks" and
check "Review Required" box.

DATA TAKEN BY/DATE: 19 Diani 2/10/

REVIEWED BY/DATE: SEN 2/18/
(If required)

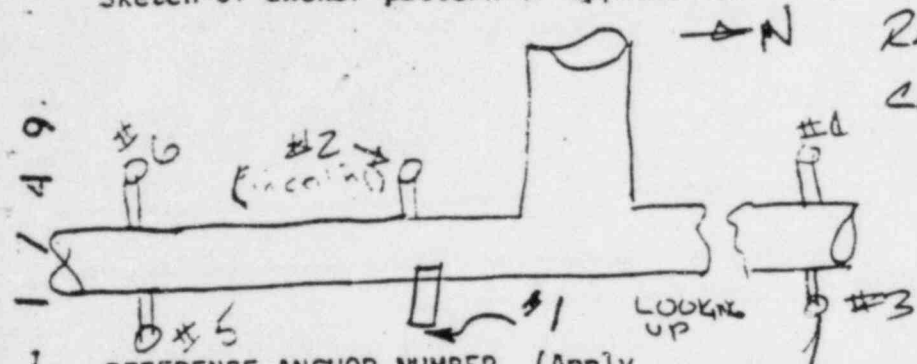
00373-1750

☒ Anchor Installation Okay
☐ Review Required

Use additional pages if there are more than 4 anchors)

CONTRACTOR Scott AREA K ELEVATION 64'

SYSTEM Air Conditioning
Sketch of anchor pattern if applicable.



RECIRCULATING WATER
CHAMBER Rm 1-2
WEST WALL 6'6" ABOVE
FLOOR

REFERENCE ANCHOR NUMBER (Apply reference numbers to sketch)	1	2	3	4
ANCHOR TYPE AND SIZE INSTALLED	5/8 P	5/8 P	5/8	5/8 P
*OBVIOUS IRREGULARITIES (yes/no)	NO	NO	NO	NO
THREADED END CUT OFF (yes/no) (If yes, record number of threads remaining in entry. If less than 4 full threads*.)	NO	NO	NO	NO
ANCHOR DEPTH GREATER THAN 1/8" BELOW SURFACE (yes/no) (If yes, record in entry. If greater than 1/2"*.)	NO	NO	NO	NO
MORE THAN 5 DEGREES FROM PERPENDICULAR (yes/no) (If yes, record in entry. If greater than 15°*.)	NO	NO	NO	NO
AS FOUND PLUG DEPTH <u>Should be to</u>	1 17/32	1 19/32	1 18/32	1 16/32
AS LEFT PLUG DEPTH (If not within ±1/16" of fully driven acceptance criteria*.)	1 15/32	1 15/32	1 16/32	1 15/32
DISTANCE PLUG DRIVEN BY RESETTING	2/32	2/32	2/32	1/32
POSSIBLE EXP. END CUT OFF (yes/no)	NO	NO	NO	NO

REMARKS _____

*If yes, describe in "Remarks" and check "Review Required" box.

DATA TAKEN BY/DATE: AE Njemi 2/16/

REVIEWED BY/DATE: SEN 2/18
(If required)

4 anchors)

CONTRACTOR

SCOTT

AREA

K

ELEVATION

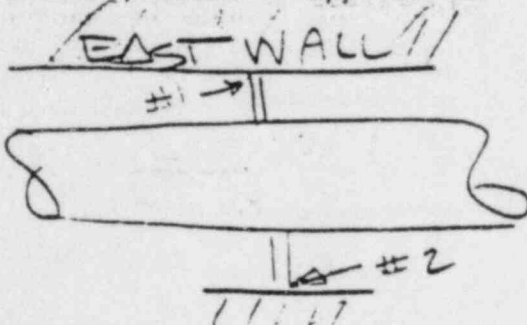
64

SYSTEM

A/C

Sketch of anchor pattern if applicable.

Boron injection tank
room



6' Above
floor

REFERENCE ANCHOR NUMBER (Apply
reference numbers to sketch)

1

2

ANCHOR TYPE AND SIZE INSTALLED

5/8P

5/8P

*OBVIOUS IRREGULARITIES (yes/no)

NO

NO

THREADED END CUT OFF (yes/no)

NO

NO

(If yes, record number of threads
remaining in entry. If less than
4 full threads*.)

ANCHOR DEPTH GREATER THAN 1/8"

BELOW SURFACE (yes/no) (If yes,
record in entry. If greater than
1/2"*.)

NO

NO

MORE THAN 5 DEGREES FROM PERPEN-
DICULAR (yes/no) (If yes, record
in entry. If greater than 15°*.)

NO

NO

AS FOUND PLUG DEPTH

1 17/32

1 17/32

AS LEFT PLUG DEPTH (If not
within +1/16" of fully driven
acceptance criteria*.)

1 14/32

1 7/32

DISTANCE PLUG DRIVEN BY RESETTING

3 1/32

0

POSSIBLE EXP. END CUT OFF (yes/no)

NO

NO

REMARKS

*If yes, describe in "Remarks" and
check "Review Required" box.

DATA TAKEN BY/DATE: SE Wiam 2/10/77

REVIEWED BY/DATE: SEN 2/18/77
(If required)

00373-1748

ANCHOR PULL TEST

CONTRACTOR: SCOTT

ANCHOR LOCATION: EL 64' WATER CHAMBER 1-1 RM

ANCHOR REF. NO.: #2 DATE: 2/17/77

PERFORMED BY: SS Niemi

GAUGE PRESS	APPLIED FORCE	Movement
510 PSI	1810 lb.	0.003"
530	1850	.004
540	1930	.006
550	1960	.008
560	2010	.010
570	2040	.015
580	2080	.019
610	2200	.025
630	2280	.030
660	2370	.035
710	2580	.040
760	2780	.045

GAUGE PRESS	APPLIED FORCE	Movement
-------------	---------------	----------

TOTAL ANCHOR DISPLACEMENT
WAS $2 \frac{1}{8}$ " AT
1150 PSI, 4320 lb.

$\frac{5}{8}$ PHILLIPS
PLUG DRIVEN 17/32"

DESIGN LOAD in 5 KIP
CONCRETE:
2100 lbs

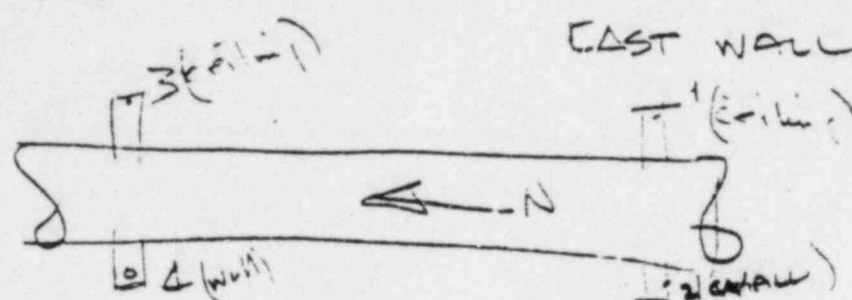
DIAL INDICATOR
WAS BUMPED, READINGS
BEYOND .045"
WERE NOT TAKEN

CONTRACTOR SCOTT AREA K ELEVATION 64

SYSTEM Air Cond.

Sketch of anchor pattern if applicable.

WATER CHAMBER ROOM #1-1
EAST WALL 8' ABOVE FLOOR



REFERENCE ANCHOR NUMBER (Apply reference numbers to sketch)

ANCHOR TYPE AND SIZE INSTALLED

*OBVIOUS IRREGULARITIES (yes/no)

THREADED END CUT OFF (yes/no)
(If yes, record number of threads remaining in entry. If less than 4 full threads*.)

ANCHOR DEPTH GREATER THAN 1/8" BELOW SURFACE (yes/no) (If yes, record in entry. If greater than 1/2"*.)

MORE THAN 5 DEGREES FROM PERPENDICULAR (yes/no) (If yes, record in entry. If greater than 15°*.)

AS FOUND PLUG DEPTH

AS LEFT PLUG DEPTH (If not within +1/16" of fully driven acceptance criteria*.)

DISTANCE PLUG DRIVEN BY RESETTING

POSSIBLE EXP. END CUT OFF (yes/no)

REMARKS * Pull test #2: 0.010" @ 2010 lbs, 0.045" @ 2
approx 1/8" @ 4340 lbs.

*If yes, describe in "Remarks" and check "Review Required" box.

DATA TAKEN BY/DATE: JEN 2/10/7-
REVIEWED BY/DATE: JEN 2/18/7-
(If required)

(Use additional pages

if there are more than
4 anchors)☐ Review RequiredCONTRACTOR SCOTTAREA KELEVATION 64SYSTEM A/C

Sketch of anchor pattern if applicable.

VALVE ROOM BETWEEN
RHR PUMPS,NORTH EAST CORNER OF ROOM, 2' ABOVE FLOOR
GRATINGREFERENCE ANCHOR NUMBER (Apply
reference numbers to sketch)

ANCHOR TYPE AND SIZE INSTALLED

*OBVIOUS IRREGULARITIES (yes/no)

THREADED END CUT OFF (yes/no)
(If yes, record number of threads
remaining in entry. If less than
4 full threads*.)ANCHOR DEPTH GREATER THAN 1/8"
BELOW SURFACE (yes/no) (If yes,
record in entry. If greater than
1/2"*.)MORE THAN 5 DEGREES FROM PERPEN-
DICULAR (yes/no) (If yes, record
in entry. If greater than 15°*.)

AS FOUND PLUG DEPTH Plug to shoulder

AS LEFT PLUG DEPTH (If not
within +1/16" of fully driven
acceptance criteria*.)

DISTANCE PLUG DRIVEN BY RESETTING

POSSIBLE EXP. END CUT OFF (yes/no)

REMARKS

1	2		
S/BP	S/BP		
NO	NO		
NO	NO		
NO	NO		
1 1/32	1 5/32		
1 5/32	1 1/32		
1/32	1/32		
NO	NO		

*If yes, describe in "Remarks" and
check "Review Required" box.DATA TAKEN BY/DATE: SE Niman 2/REVIEWED BY/DATE: SEN 2/18/12

00373-1/45

if there are more than 4 anchors)

SHEET 1

CONTRACTOR

Scott

AREA

K

ELEVATION

60'

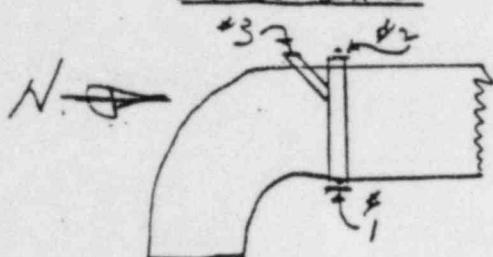
SYSTEM

A/C

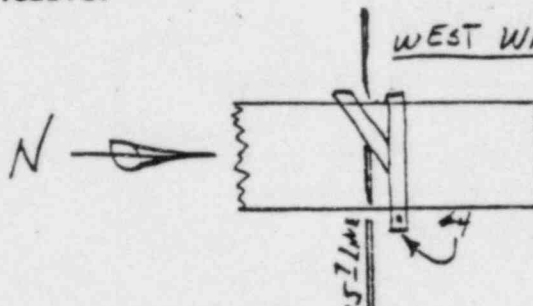
Sketch of anchor pattern if applicable.

MONITOR TANK #1-1

WEST WALL



WEST WALL



REFERENCE ANCHOR NUMBER (Apply reference numbers to sketch)

ANCHOR TYPE AND SIZE INSTALLED

*OBVIOUS IRREGULARITIES (yes/no)

THREADED END CUT OFF (yes/no)
(If yes, record number of threads remaining in entry. If less than 4 full threads*.)

ANCHOR DEPTH GREATER THAN 1/8" BELOW SURFACE (yes/no) (If yes, record in entry. If greater than 1/2"*.)

MORE THAN 5 DEGREES FROM PERPENDICULAR (yes/no) (If yes, record in entry. If greater than 15°*.)

AS FOUND PLUG DEPTH

AS LEFT PLUG DEPTH (If not within +1/16" of fully driven acceptance criteria*.)

DISTANCE PLUG DRIVEN BY RESETTING

POSSIBLE EXP. END CUT OFF (yes/no)

REMARKS

1	2	3	4
3/4 P	3/4 P	3/4 P	3/4 P
No			No
No			No
No			No
No			No
No			No
1 29/32			1 26/32
1 28/32			1 28/32
1/32			0
No			No

CANNOT GET RECORDS BECAUSE OF SPACING HANGER.

CANNOT GET RECORDS BECAUSE, CANNOT GET WRENCH OR SOCKET ON BOLT HEAD, AS STEEL & CONCRETE ARE TOO CLOSE TO BOLT.

*If yes, describe in "Remarks" and check "Review Required" box.

DATA TAKEN BY/DATE: Walters 12-11-7

REVIEWED BY/DATE: SEN 2/18/8
(If required)

CONTRACTOR

Scott

AREA

K

ELEVATION

60'

SYSTEM

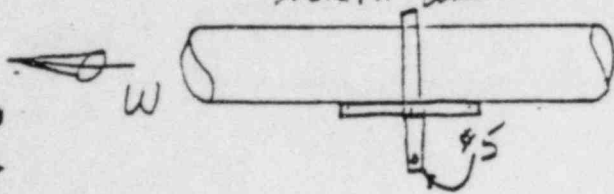
A/C

Sketch of anchor pattern if applicable.

MONITOR TANK 1-1 AREA

SEE SHEET #1

NORTH WALL



REFERENCE ANCHOR NUMBER (Apply reference numbers to sketch)

5

ANCHOR TYPE AND SIZE INSTALLED

5/8P

*OBVIOUS IRREGULARITIES (yes/no)

NO

THREADED END CUT OFF (yes/no)
(If yes, record number of threads remaining in entry. If less than 4 full threads*.)

NO

ANCHOR DEPTH GREATER THAN 1/8" BELOW SURFACE (yes/no) (If yes, record in entry. If greater than 1/2"*.)

NO

MORE THAN 5 DEGREES FROM PERPENDICULAR (yes/no) (If yes, record in entry. If greater than 15*.)

NO

AS FOUND PLUG DEPTH

1 16/32

AS LEFT PLUG DEPTH (If not within +1/16" of fully driven acceptance criteria*.)

1 15/32

DISTANCE PLUG DRIVEN BY RESETTING

1 3/32

POSSIBLE EXP. END CUT OFF (yes/no)

NO

REMARKS

*If yes, describe in "Remarks" and check "Review Required" box.

DATA TAKEN BY/DATE: Walter / 2-11-77

REVIEWED BY/DATE: SEN 2/18/77
(If required)

00373-1743

CONTRACTOR

Scott

AREA

J

ELEVATION

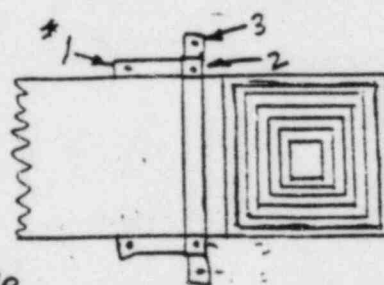
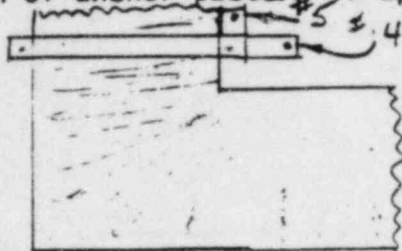
115' +

SYSTEM

A/C

Sketch of anchor pattern if applicable.

Aux. FW. HYDRAZINE & Ammonia PPS. Rm.



Looking UP

REFERENCE ANCHOR NUMBER (Apply reference numbers to sketch)

ANCHOR TYPE AND SIZE INSTALLED

*OBVIOUS IRREGULARITIES (yes/no)

THREADED END CUT OFF (yes/no)
(If yes, record number of threads remaining in entry. If less than 4 full threads*.)

ANCHOR DEPTH GREATER THAN 1/8"
BELOW SURFACE (yes/no) (If yes,
record in entry. If greater than
1/2"*.)

MORE THAN 5 DEGREES FROM PERPEN-
DICULAR (yes/no) (If yes, record
in entry. If greater than 15*.)

AS FOUND PLUG DEPTH

AS LEFT PLUG DEPTH (If not
within +1/16" of fully driven
acceptance criteria*.)

DISTANCE PLUG DRIVEN BY RESETTING

POSSIBLE EXP. END CUT OFF (yes/no)

REMARKS #3 Pull tested: 1320 lbs; 0.010" @ 4320#, 0.034".

#4 Pull tested: 0.010" @ 3725#, 0.015" @ 4320#

#5 Pull tested: 0.010" @ 3240#, 0.026" @ 4320#

*If yes, describe in "Remarks" and
check "Review Required" box.

DATA TAKEN BY/DATE: Wulfsberg/2-15-77

REVIEWED BY/DATE: DSN 2/16/77
(If required)

Are additional notes
if there are more than
4 anchors?

☐ Anchor Installation Okay
☐ Review Required

CONTRACTOR Scott AREA J ELEVATION 115' +
SYSTEM A/E
Sketch of anchor pattern if applicable.

SEE SHEET #1

00373-115

REFERENCE ANCHOR NUMBER (Apply
reference numbers to sketch)

ANCHOR TYPE AND SIZE INSTALLED

*OBVIOUS IRREGULARITIES (yes/no)

THREADED END CUT OFF (yes/no)
(If yes, record number of threads
remaining in entry. If less than
4 full threads*.)

ANCHOR DEPTH GREATER THAN 1/8"
BELOW SURFACE (yes/no) (If yes,
record in entry. If greater than
1/2"*.)

MORE THAN 5 DEGREES FROM PERPEN-
DICULAR (yes/no) (If yes, record
in entry. If greater than 15°*.)

AS FOUND PLUG DEPTH

AS LEFT PLUG DEPTH (If not
within $\pm 1/16$ " of fully driven
acceptance criteria*.)

DISTANCE PLUG DRIVEN BY RESETTING

POSSIBLE EXP. END CUT OFF (yes/no)

REMARKS

<u>5</u>	<u>(</u>	<u>1</u>	<u>7</u>
<u>5/8 P</u>	<u>(</u>	<u>1</u>	<u>7</u>
<u>NO</u>	<u>(</u>	<u>1</u>	<u>7</u>
<u>NO</u>	<u>(</u>	<u>1</u>	<u>7</u>
<u>NO</u>	<u>(</u>	<u>1</u>	<u>7</u>
<u>NO</u>	<u>(</u>	<u>1</u>	<u>7</u>
<u>NO</u>	<u>(</u>	<u>1</u>	<u>7</u>
<u>1 3/4</u>	<u>(</u>	<u>1</u>	<u>7</u>
<u>1 3/4</u>	<u>(</u>	<u>1</u>	<u>7</u>
<u>7 1/2</u>	<u>(</u>	<u>1</u>	<u>7</u>
<u>NO</u>	<u>(</u>	<u>1</u>	<u>7</u>

*If yes, describe in "Remarks" and
check "Review Required" box.

DATA TAKEN BY/DATE: Washburn/2-15-7

REVIEWED BY/DATE: SEN 2/18/
(If required)

4

PROCEDURE FOR ESTABLISHING ACCEPTANCE
CRITERIA FOR CONCRETE ANCHOR INSTALLATIONS

DIABLO CANYON POWER PLANT

Prepared By: Thomas E Niemi

Approved By: MR. Trecker

Revision: 2 Date: 12/10/76

PURPOSE

This procedure will develop inspection criteria that can be used to evaluate concrete anchor installations in the field.

SCOPE

This procedure will determine minimum acceptance criteria for misinstalled concrete anchors for the following conditions in nominal 3,000 psi design concrete: (1) wedge plugs not driven fully, (2) field modified anchors, (3) angular misalignment, and (4) effects of overembedment on shear strength.

This procedure will test 1/2", 5/8", 3/4" and 7/8" concrete anchors (flush shell type) manufactured by both the Phillips Drill Company, Inc. and the Hilti Corporation.

TEST PROCEDURE

A. TEST FIXTURE

The test fixture consists of a base, support structure, hydraulic cylinder with a hollow ram, pressure gauge, hand operated hydraulic pump, hydraulic hose and threaded rods of required sizes to fit anchors. (See Figure 1)

Also, a dial indicator with a magnetic base and various accessories to measure anchor movement will be used.

B. CALIBRATION OF TEST FIXTURE

1. Assemble the hydraulic cylinder, hand pump, pressure hose and calibrated pressure gauge.

- 00373-1516
2. Using the concrete compression tester in the concrete testing lab, determine the load applied by the cylinder at various pressure readings as read on the pressure gauge. Record data on Data Sheet No. 1, "Hydraulic Cylinder Force."

NOTE: Make ten calibration runs. At each pressure plateau, record the hydraulic pressure and applied force. Average the ten readings at each pressure plateau and plot the average value on Figure 2.

3. Using the data from Data Sheet 1, develop a curve for Figure 2, "Cylinder Force vs. Hydraulic Pressure."

C. GENERAL TEST INSTRUCTIONS

1. Install anchor of type and size required for testing.
2. Position test fixture over embedded anchor and connect to anchor with threaded rod of required size.
3. Position dial indicator to detect anchor movement. The dial indicator should contact the shoulder of the anchor if possible. Use the dial indicator accessories, (i.e. magnetic base and extension rods) as required to assure that equipment deflection and rod stretch is not affecting the dial indicator.
4. Increase hydraulic pressure until the dial indicator detects movement of the anchor. Record hydraulic pressure on applicable data sheet at which movement is detected.
5. Continue increasing hydraulic pressure until one of the following conditions exist:
 - a. the anchor has slipped five percent of the minimum embedment depth,
 - b. the concrete cracks, or
 - c. the anchor breaks.

Record on applicable data sheet.

6. Vent hydraulic pressure and remove test apparatus.
7. Using Figure 2, "Cylinder Force vs. Hydraulic Pressure," determine load applied to anchor at which anchor movement is detected. Record the force on the applicable data sheet.

D. TESTING TO DETERMINE ACCEPTANCE CRITERIA

1.0 Unmodified Hilti Anchors

1.1 Plug Depth Before Driving

- a. For each size of Hilti anchors, select ten at random.
- b. Insert the expansion plug (by hand) as far as possible. Tap the plug lightly to assure it is seated on it's taper.
- c. Measure and record the distance from the threaded end shoulder to the top of the plug on Data Sheet No. 2 for ten anchors.
- d. From the data obtained, determine the average dimension that the plug can be inserted for each size of Hilti anchors and record on Data Sheet No. 2.

1.2 Minimum Depth of Expansion Plug to Meet Design Load

- a. Drill holes in 3,000 psi concrete of the required diameter for each size of Hilti anchors to depths at which the anchors will be flush with the surface of the concrete.

- b. Install anchor and drive the expansion plug 1/8". Record on Data Sheet No. 3.

NOTE: The depth of the expansion plug is determined by subtracting the average dimension for each size of Hilti anchor (obtained in Section 1.1) from the distance of the plug to the anchor threaded end shoulder after driving.

- c. Perform pull test on anchor and record data at which anchor movement (or failure) is detected on Data Sheet 3. Record the pressure for both initial movement of the anchor and when the anchor has been displaced five percent of minimum embedment.

NOTE: The following are minimum acceptable values for anchor strengths, both for PHILLIPS and HILTI anchors. They are 10% greater than Table A values for 3,000 psi concrete in PG&E Engineering Standard No. 054162, Revision 2.

<u>Anchor Size</u>	<u>Min. Acceptable Force</u>
1/2"	965 lbs.
5/8"	1,650 lbs.
3/4"	2,585 lbs.
7/8"	3,685 lbs.

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d. Compare pull-out force at initial anchor movement with the minimum acceptable values. If the minimum acceptable force is not met, rerun the test with the anchor expansion plug driven deeper. Increase plug depths in 1/8" increments. Use a new anchor, expansion plug and hole for each test.

e. If the minimum pull-out force is exceeded, run four more anchor pull tests with the plug driven the same minimum amount. Record data on Data Sheet No. 3.

NOTE: Five consecutive pull tests at a selected expansion plug depth must pass the minimum acceptable pull-out force before this plug depth can be established as a minimum field inspection criterion. If, during testing, any anchor fails at the selected plug depth, this depth is not satisfactory and the next deeper increment must be tested.

f. Determine the minimum expansion plug depth for 1/2", 5/8" and 3/4" HILTI Anchors and record findings on Data Sheet No. 3.

g. After once having determined the minimum plug depth to meet design load for each size of anchor, drive the expansion plug deeper in 1/8" increments and perform a pull test at each deeper increment until 300% design load is reached. Record information on Data Sheet No. 3.

h. For each anchor size, drive the expansion plug fully one time and test per above. Record findings on Data Sheet No. 3.

2.0 Unmodified Phillips Anchors

2.1 Plug Depth Before Driving

NOTE: Use Phillips test gauge as shown in Figure 3 for each size of Phillips anchors for measurements.

a. Select ten Phillips anchors. Insert the expansion plugs (by hand) as far as possible. Tap the plug lightly to assure that it is seated on it's taper.

b. Insert test gauge in each selected anchor and measure from the top of the expansion plug to the shoulder of the test gauge. Record the information on Data Sheet No. 2.

NOTE: It is extremely important that the test gauge be inserted as far as possible when obtaining measurements to assure that the test gauge is at the end of the threaded section.

- c. From the data obtained above, determine the average dimension that the plug can be inserted for each size of Phillips anchors and record on Data Sheet No. 2.

2.2 Minimum Depth of Expansion Plug to Meet Design Load

- a. Test Phillips anchors as outlined in Section 2.1 except for the following.
- (1) The depth of the expansion plug is the difference from the top of the plug to the shoulder of the test gauge (after driving plug) and the distance determined in 2.1.
 - (2) Record pull-out data on Data Sheet No. 4 and develop minimum field acceptance criteria for Phillips anchors.
 - (3) Perform Step 1.2.g for Phillips anchors and record on Data Sheet 4.
 - (4) Perform Step 1.2.h for each size of Phillips anchors and record on Data Sheet 4.

3.0 Modified Anchors

3.1 HILTI ANCHORS - Establishing a Reference Point for a Modified Anchor

- a. Select ten Hilti anchors at random for 1/2", 5/8" and 3/4".
- b. Record the distance from the face of the threaded end to the end of the threaded section for each anchor. Record measurements on Data Sheet No. 5.
- c. Drill holes of required diameters to the depths noted below.

<u>Anchor Size</u>	<u>Hole Depth</u>
1/2"	1 3/8"
5/8"	1 3/4"
3/4"	2 1/16"

- d. Install anchor in the holes and drive the plug until the end of the threaded section is just visible.
- e. Perform one pull test on each size anchor with the plugs driven to this depth and record the required information on Data Sheet No. 5.

NOTE: If the anchor fails to meet minimum acceptance criteria at the plug depths in Step 3, reperform this test with the plugs driven deep enough to pass minimum acceptance criteria.

3.2 PHILLIPS ANCHORS - Establishing a Reference Point for a Modified Anchor

NOTE: The distance that the expansion plug is driven can be determined by measuring from the plug to the end of the threaded section. Since this measurement has previously been obtained in Section 2.0, this test on Phillips anchors is not required.

3.3 HILTI ANCHORS - Expansion End Cut Off
(Perform this test for each size of anchor)

- a. For each size of anchor, determine the minimum depth that the plug must be driven to meet minimum acceptable design load. Record on Data Sheet No. 15. (See Section 1.2 and Data Sheet No. 3 for minimum plug depth)
- b. Insert the expansion plug by hand, as far as possible. Tap the plug lightly to assure that it is seated on it's taper.
- c. Measure overall length of unmodified anchor and record on Data Sheet No. 15.
- d. Measure the distance from the shoulder of the expansion end to the plug. Record on Data Sheet 15.
- e. Subtract the minimum distance that the plug must be driven to meet design load (obtained from Data Sheet No. 3) from the distance obtained in Step d. Cut off this amount from the anchor expansion end. Record information on Data Sheet No. 15.
- f. Drill a hole in concrete to the required depth so that the modified anchor will be flush or slightly above the surface of the concrete. Record hole depth on Data Sheet No. 15.
- g. Insert the anchor and drive the expansion plug fully. Record the distance that the plug was driven.
- h. Perform a pull test on the modified anchor and record information on Data Sheet No. 15.
- i. Repeat Steps e through h for the same size anchor, except decrease the amount cut off in 1/4" increments until 300% design load is reached.
- j. Perform this test for each size of Hilti anchor.

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3.4 PHILLIPS ANCHORS - Expansion End Cut Off
(Perform this test for each anchor size)

- a. Remove 3/4" from the expansion end of the anchor.
- b. Measure the overall length of the modified anchor and record on Data Sheet No. 16.
- c. Drill hole depth as required to allow the anchor to be flush with the top surface after fully driving expansion plug. Record hole depth on Data Sheet No. 16.
- d. Insert anchor in hole and drive plug fully.
- e. Measure the distance that the plug has been driven using the appropriate test gauge. Record on Data Sheet No. 16.
- f. Perform a pull test on the anchor and record information on Data Sheet No. 16.
- g. Repeat this test, increasing the amount removed from the expansion end in 1/4" increments, until the anchor no longer meets minimum design load.

3.5 HILTI and PHILLIPS ANCHORS - Threaded End Cut Off

- a. Obtain one anchor for each size and type.
- b. Cut off the threaded end until four full threads remain on each anchor.
- c. Perform a pull test on each anchor. The hole depth should be deep enough so that the anchors are flush with the top surface of the concrete after driving their expansion plugs. The plugs should be driven fully for each anchor. Record information on Data Sheet No. 6.

NOTE: The pull test need not be performed to failure. Terminate the test at 300% of the design load.

4.0 Angular Misalignment

4.1 15° Misalignment - Plugs at Minimum Depth to Meet Design Load.

- a. Perform one pull test for each size and type of anchor. The plugs are to be inserted to the minimum depths that have been determined to meet design load (Sections 1.0 and 2.0). The holes are to be drilled as close to 15° from vertical as possible. The hole depths are to be flush with the surface of the concrete after driving the expansion plugs. Record information on Data Sheet No. 8.

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4.2 15° Misalignment - Plugs Fully Inserted.

- a. Perform one pull test for each size and type of anchor with their holes as close to 15° from vertical as possible. The expansion plugs are to be driven fully and the hole depths are to be deep enough for the tops of the anchors to be flush with the surface of the concrete. Record on Data Sheet No. 7.

5.0 Shear Loading Over Embedded Anchors

5.1 HILTI ANCHORS - Perform Once for Each Size of Anchor.

- a. Drill holes of required size in a vertical concrete surface. Hole depths should be sufficiently deep to embed the anchors 1/2" below the surface of the concrete.

NOTE: Drill the holes at the required height above the floor so that the hydraulic cylinder may be placed on the floor and apply a shear force to the anchor bolt.

- b. Drive the expansion plugs fully on each anchor to be tested.
- c. Insert a bolt of the proper size through the shear load test fixture shown in Figure 4. Tighten the bolt.
- d. Position the hydraulic cylinder under the test fixture.
- e. Increase the hydraulic pressure until the anchor or the bolt fails, or 300% design load is reached. Record information on Data Sheet No. 9.

6.0 Discussion and Conclusions

6.1 Anchor Uniformity

Data Sheets 2 and 5 indicate that anchors are manufactured with sufficient uniformity to use various reference points on the anchors to measure distances that expansion plugs are driven. Measurements were repeatable within 1/16" and in most cases, 1/32".

6.2 Expansion Plugs - Minimum and Fully Driven Distances

The following table summarizes test results for both (1) fully driven expansion plugs and (2) expansion plugs driven to minimum depths and still meet acceptance criteria. The results are from Data Sheets 3 and 4, including the remarks for each entry. An anchor was considered to have failed when it's total displacement exceeded 0.010".

Anchor Size and Type	1/2" HILTI	.5/8" HILTI	3/4" HILTI	1/2" PHILLIPS	5/8" PHILLIPS	3/4" PHILLIPS	7/8" PHILLIPS
Minimum Acceptable Force Required	965 lbs.	1650 lbs.	2585 lbs.	965 lbs.	1650 lbs.	2585 lbs.	3685 lbs.
Min. Acceptable Plug Driven Distance % of Fully Driven Plug Distance	3/8" 63%	3/8" 55%	1/4" 29%	3/16" 50%	1/2" 76%	1/2" 84%	1/2" 73%
Ave. Force Dev. at Min. Plug % of Driven Dis. Min. Ac- ceptable Force	4010 lb. 416%	3039 lb. 184%	3475 lb. 134%	1606 lb. 166%	3312 lb. 201%	6576 lb. 254%	5692 lb. 154%
Fully Driven Plug Distance	19/32"	11/16"	7/8"	3/8"	21/32"	19/32"	11/16"
Force Developed For Fully Driven Plug % of Min. Acceptable Force	4910 lb. 508%	6140 lb. 372%	11,000 lb. 426%	3740 lb. 388%	2380 lb. 144%	6750 lb. 261%	5890 lb. 160%

Testing was performed in the northwest corner of the Diablo Canyon auxiliary building, elevation 64. Concrete in that area is typical of 3000 psi concrete used throughout the plant.

Anchor slippage was the predominate mode of failure, even for fully driven expansion plugs. Hilti anchors generally held until the applied force was sufficient to cause them to move. Once movement began, it continued quickly to failure. Generally, the force required to maintain a steady displacement was less than the force that initially caused slippage.

Phillips anchors also failed by slipping, however, their mode of slippage was different than Hilti anchors. Once slipping began, and if the applied force was then held constant, the anchors would eventually stop slipping. Increasing the force would reinitiate anchor slipping. Holding

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the force constant at a larger value would allow the anchor to stabilize again. Further force application would cause the same effect until the point at which the anchor no longer stabilized; it would either slip to failure (especially true for small expansion plug driven distances) or the concrete failed because it's shear cone became too small (especially true for anchors with their expansion plugs driven farther or fully driven).

Some Phillips anchors were tested into the slip range and ultimately to failure. Several tests were performed in which the load was held constant after slipping had begun. After a short time, the anchor displacement stabilized. The load was released and then, slowly reapplied. The anchor was able to withstand the load at which slipping had originally begun without further displacement. The force required to reinitiate slipping was approximately the same as that at which the anchor had previously stabilized. Larger forces would then cause correspondingly larger anchor displacements until the ultimate force was reached causing total failure.

Conclusion - Anchors with their expansion plugs driven at least the distances shown in the above table will develop sufficient strengths to meet minimum acceptable loads.

6.3 Modified Anchors - Threaded End Cut Off

Results obtained from Data Sheet 5 indicate that if Hilti expansion plugs are driven to the point at which the end of the threaded section is just visible, only the 3/4" Hilti anchor will develop sufficient force to meet the acceptance criterion. The expansion plugs for 1/2" and 5/8" Hilti anchors must be driven 3/16" and 3/32" beyond the end of the threaded section, respectively, to meet acceptance criteria. These additional plug depths were required to meet the minimum plug driven distances previously established.

Data Sheet No. 6 contains results of anchors modified by cutting off the threaded end until four full threads remained. Generally, concrete failure, either cracking or shear cone pull-out, occurred during Hilti anchor testing. This can be attributed to the anchors being closer to the surface of the concrete. Phillips anchors exhibited their typical slipping phenomenon during this testing phase; their failure occurred with no apparent concrete damage. The effective grip area of Phillips anchors is farther below the concrete surface than that for Hilti anchors, hence the differences in failure modes. The following summarizes results of Data Sheet No. 6:

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Forces Developed With Threaded End Cut Off

<u>Anchor Size and Type</u>	<u>Max. Amount Cut Off</u>	<u>Force Dev. at Failure</u>	<u>% of Min. Acceptable Force</u>
1/2" Hilti	1/2"	2860 lb.	296%
5/8" Hilti	25/32"	4710 lb.	285%
3/4" Hilti	1 1/8"	7350 lb.	284%
1/2" Phillips	5/8"	3340 lb.	346%
5/8" Phillips	1/2"	5310 lb.	322%
3/4" Phillips	1 1/8"	7770 lb.	301%
7/8" Phillips	15/16"	11,200 lb.	304%

Conclusion - Anchors with their threaded end cut off to the extent shown above, will meet minimum acceptable loads. However, their expansion plugs must be fully driven and hole depths must be sufficient to allow the anchors to be flush with the concrete surface.

6.4 Modified Anchors - Expansion End Cut Off

Cutting off the expansion end reduced the anchor's ability to withstand loads. The forces required to cause initial movements of Hilti anchors decreased as more of the expansion ends were removed. However, the reverse is true for Phillips anchors. In all cases, the modified anchors were able to exceed the minimum acceptable test loads. The following summarizes test results contained in Data Sheets 15 and 16:

Expansion End Cut Off

<u>Anchor Size and Type</u>	<u>Max. Amount Cut Off</u>	<u>Force Dev. at Failure</u>	<u>% of Min. Acceptable Force</u>
1/2" Hilti	9/32"	3210 lb.	333%
5/8" Hilti	3/8"	3175 lb.	192%
3/4" Hilti	11/16"	3500 lb.	135%
1/2" Phillips	7/8"	2080 lb.	216%
5/8" Phillips	1"	2980 lb.	181%
3/4" Phillips	1 1/16"	3730 lb.	144%
7/8" Phillips	1 1/2"	9570 lb.	260%

Conclusion - The expansion end of anchors can be cut off to the extent shown above and still maintain sufficient strengths to meet acceptance criteria. However, the expansion plugs must be driven fully and hole depth must be sufficient to allow the anchor to be flush with the concrete surface.

6.5 Angular Misalignment

Anchors installed approximately 15° from vertical were still able to meet minimum acceptance criteria. The following summarizes test results contained in Data Sheet 7 and 8:

<u>Plugs Fully Driven</u>			<u>Plugs Driven Min. Distance</u>	
<u>Anchor Size and Type</u>	<u>Applied Force</u>	<u>% of Min. Acceptable Load</u>	<u>Applied Force</u>	<u>% of Min. Acceptable Load</u>
1/2" Hilti	3130 lb.	324%	3100 lb.	322%
5/8" Hilti	5725 lb.	347%	1740 lb.	105%
3/4" Hilti	8820 lb.	341%	2670 lb.	103%
1/2" Phillip	2900 lb.	300%	2170 lb.	225%
5/8" Phillip	5725 lb.	347%	2940 lb.	178%
3/4" Phillip	7770 lb.	300%	4120 lb.	135%
7/8" Phillip	11,420 lb.	310%	10,000 lb.	271%

Phillips anchors did not exhibit the previously experienced slip phenomenon when angularly misinstalled. They generally were able to sustain larger loads than equivalent properly installed anchors.

Conclusion - Anchors with expansion plugs driven at least the minimum distances previously established can be misinstalled up to 15° from vertical and still meet minimum acceptance criteria.

6.6 Over Embedment Effects on Shear Strengths

All Hilti anchors easily exceeded 300% minimum acceptable shear strength values. There was no evidence of concrete failure after testing, however, threads on the bolts were slightly flattened. Several bolts were bent approximately two to five degrees.

Minimum acceptable shear strength values are 10% greater than Table A shear values for 3000 psi concrete in PG&E Engineering Standard 054162, Revision 2.

Phillips anchors were not tested because their self drilling feature prevents overembedment. However, the same test results would have been obtained had Phillips anchors been tested.

Conclusion - Over embedding anchors up to 1/2" below the surface of the concrete will not affect the shear strength of the bolted connection.

6.7 Testing in 5000 psi Concrete

Testing was not performed in 5000 psi concrete because design did not take credit for the extra strength developed by

5000 psi concrete. Also, the failure mode predominately encountered was anchor slippage, not concrete failure. In the few cases where concrete failed, stronger concrete should produce more favorable results.

Since testing in 5000 psi concrete was not performed, Data Sheets 10 through 14 have been deleted from the procedure.

APPENDIX

CONTENTS:

1. Figure 1 - Pull Test Fixture
2. Figure 2 - Cylinder Force vs. Hydraulic Pressure
3. Figure 3 - Phillips Anchor Test Gauge
4. Figure 4 - Shear Test Fixture
5. Data Sheet 1 - Hydraulic Cylinder Force
6. Data Sheet 2 - Initial Plug Depth
7. Data Sheet 3 - Minimum Expansion Plug Depth to Meet Design Load
8. Data Sheet 4 - Minimum Expansion Plug Depth to Meet Design Load
9. Data Sheet 5 - Hilti Anchor-Threaded End Cut Off
10. Data Sheet 6 - Load Limits for Four Full Threads
11. Data Sheet 7 - 15° Misalignment-Plugs Fully Driven
12. Data Sheet 8 - 15° Misalignment-Plugs at Minimum Depth to Meet Design Load
13. Data Sheet 9 - Shear Strength-Anchor 1/2" Below Surface of Concrete
14. Data Sheet 10 - Pull Out Force at Min. Plug Depth-5,000 psi Concrete
15. Data Sheet 11 - Hilti Anchor-Thread End Cut Off, 5,000 psi Concrete
16. Data Sheet 12 - 15° Misalignment-Plug Fully Driven, 5,000 psi Concrete
17. Data Sheet 13 - 15° Misalignment-Plugs at Minimum Depth to Meet Design Load, 5,000 psi Concrete
18. Data Sheet 14 - Anchors 1/2" Below Surface of Concrete, 5,000 psi Concrete

19. Data Sheet 15 - Hilti Anchor-Expansion End Cut Off

20. Data Sheet 16 - Phillips Anchor-Expansion End Cut Off

21. Data Sheet 17 - Instruments Used During Testing

22. References:

- a. "Concrete Expansion Anchors for Static and Seismic Loading",
Engineering Design Standard 054162, Change 2, 4/17/73.

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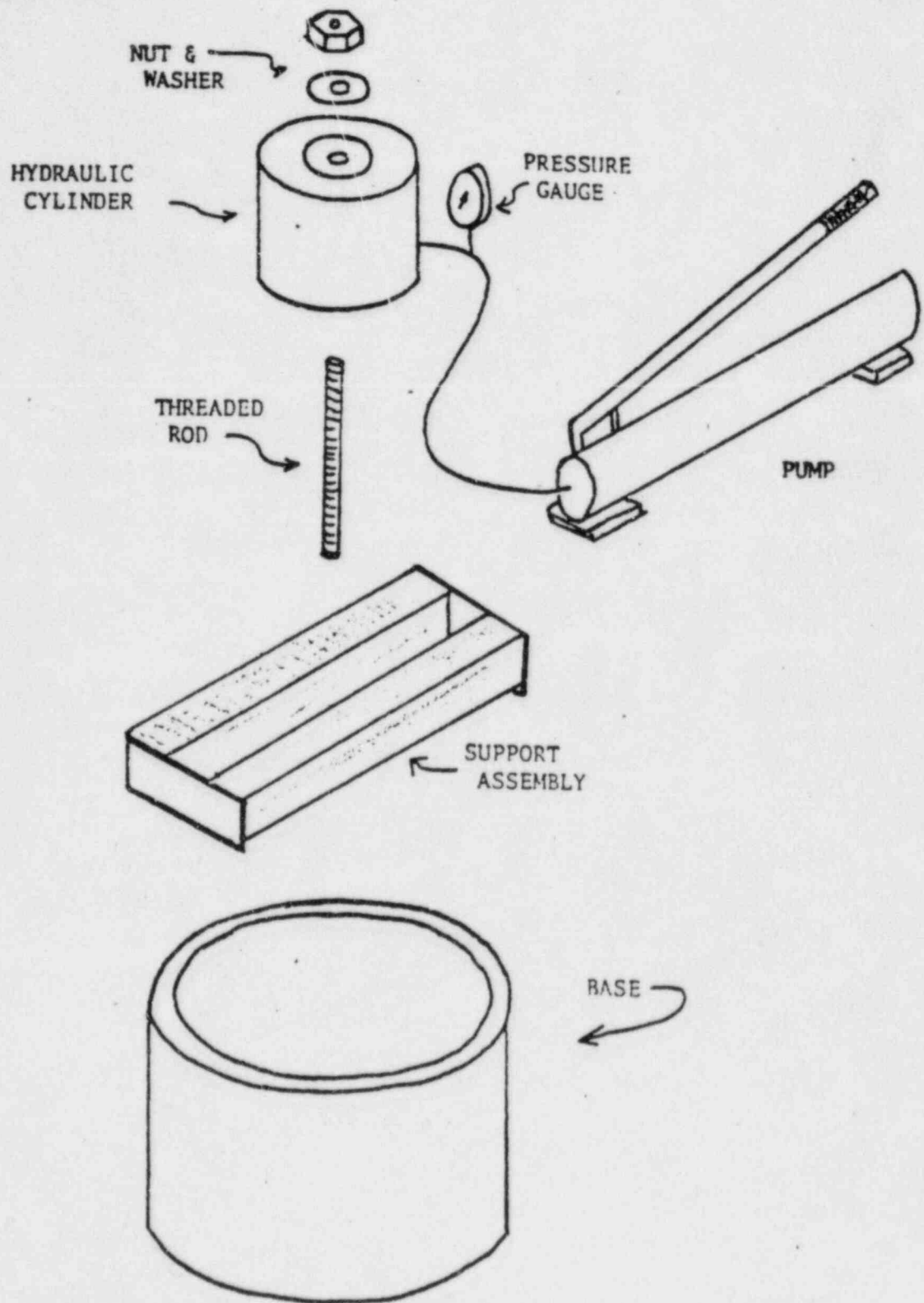


FIGURE 1 - PULL TEST FIXTURE

6
Acceptance Criteria For Concrete Expansion Anchors
Diablo Canyon Project

October 2, 1978

MR. C. K. MAXFIELD:

1. This letter supersedes the following documents:

- a. May 4, 1976 letter, E. P. Wollak to G. S. Bates on Diablo Canyon project - Spacing Between Concrete Expansion Anchors.
- b. January 7, 1977 letter, E. P. Wollak to G. S. Bates on Concrete Anchors - Diablo Canyon.
- c. February 25, 1977 letter, E. P. Wollak to G. S. Bates on Concrete Anchors.
- d. June 22, 1978 letter, E. P. Wollak to M. R. Tresler on drawing No. 054162 - Design Criteria Clarification for Concrete Expansion Anchors and Raceway Supports.
- e. April 14, 1978, DCPD telephone conversation between D. Wright and I. Sokoloff on Concrete Anchors.

The acceptance and/or repair criteria contained in the following documents are also superseded:

- f. June 30, 1978, Civil Engineering memorandum to the file by E. P. Wollak on Concrete Expansion Anchor Testing and Acceptance Criteria - Diablo Canyon.
- g. March 14, 1977. Deviation Report No. 282, Revision 1.
- h. March 2, 1977. Deviation Report No. 283.

2. General

All new concrete expansion anchors shall be installed to meet the criteria set forth on Engineering Standard Drawing No. 054162.

3. Spacing

- a. If 12-diameter spacing cannot be met and allowable reduction cannot be determined according to the rules on drawing No. 054162, or if the utilization of tolerances allowed by other rules are not possible, the installation shall be marked for the Responsible Civil Engineer's inspection.

The Responsible Civil Engineer will visually inspect the marked locations and designate what corrective action, if any, is required.

For those only where an immediate decision cannot be made, a Construction Problem Control Sheet (DP) shall be submitted for further investigation by the Engineering Department.

b. Anchor spacing embedded to Unistrut:

- 1) An embedded unistrut is considered loaded only at that point where the raceway support, pipe support, etc. is attached.
- 2) Anchors may be installed $\frac{1}{2}$ " clear from any embedded unistrut, provided there is no loading of the unistrut within 12 nominal diameters of that anchor. (Exception: Unistrut saddle brackets, see item c.1 below).

c. Minimum spacing of anchors for saddle brackets:

- 1) Where two unistrut saddle brackets are installed the two outer anchors shall be used to determine spacing.

d. Method of attachment trays to supports:

- 1) Mounting strap supplied with tray hardware must be installed on the inside of the support construction, not on the outer edge where it may slip off the support. (Also, strap must be attached to bottom of tray). See cable tray note 2, drawing No. 050029.
- 2) Square-headed bolts may be used with the above strap, provided they are set flush with the raised ribs of the tray bottoms and do not cause damage to wire in trays.

e. No raceway supports are to be mounted to any electrical equipment except where specifically authorized by the Engineering Department on the design drawing.

f. Anchors may be installed within $\frac{1}{2}$ " clear of sleeve passing through concrete walls, provided the sleeve thickness is at least $\frac{1}{2}$ ".

4. Improper Installation

a. Expander plugs not fully driven:

Unmodified anchors may be rated at full value if the expander plug has been driven at least the amount shown below:

<u>Size</u>	<u>Hilti</u>	<u>Phillips</u>
1/2	3/8	5/16
5/8	3/8	1/2
3/4	7/16	1/2
7/8	—	9/16

Axis of anchor not normal to concrete surface:

- Modified anchors which deviate from the normal shall be rated as follows:

Deviation Angle	Driven Distance of Expander Plug	Allowable Load (% of Allowable From Dwg. 054162)
0° - 15°	Full Distance	100%
> 15° - 45°	Full Distance	Interpolate between 60% at 15° and zero at 45°
0° - 5°	As in Par. 4a	100%
> 5° - 15°	As in Par. 4a	Interpolate between 90% at 5° and 60% at 15°

c. Anchor overembedded:

Unmodified anchors which have not more than $\frac{1}{2}$ " overembedment may be rated at full value for shear only and for combinations of shear and tension. Anchors which will be loaded in tension only may be over-embedded to any depth without penalty.

5. Unauthorized Modifications (Shell Anchors)

a. Part of threaded end removed:

If at least 4 threads remain in a cut-off anchor, if the anchor does not deviate more than 5° from normal, and if the expander plug has been driven at least the amount required in Par. 4.a., the anchor may be rated at full value.

b. Part of expansion end removed:

Shell anchors, which have been modified by cutting off part of the expansion end, may be rated at full value if the anchor does not deviate more than 5° from normal, if the expander plug has been driven as far as possible (flush with the cut-off end), and if the inferred length of cut-off does not exceed 60% of nominal diameter for shell anchors (100% of nominal diameter for Phillips shell anchors).

6. Nonconforming anchors:

- If possible, the defective anchor should be properly driven to meet the criteria for a fully acceptable anchor.
- If a. is not possible, the Responsible Engineer should be consulted to determine whether the anchor, either for full or reduced capacity (Par. 4 and 5 above), was necessary to resist the design loads, or whether the other anchors in the same group are sufficient to resist the design loads; or

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Mr. C. K. Maxfield

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October 2, 1978

- c. Replace defective anchor by installing an additional anchor.
- d. If an anchor has been properly installed to replace a nonconforming one, the latter may be left in place and considered equivalent to one which has been removed and the hole filled with grout.
- e. Whenever an anchor is installed that is of a smaller size than that shown on the design drawing, the Responsible Engineer must be consulted to determine the adequacy of the installation.

E. P. WOLLAK

EPW(3586):ml

cc RDEtzler
VJGhio
JBHoch/DLPolley
GVRichards
CWSteinhardt
RFWischow
JLWoodward/LGRasmussen

DISCREPANCY REPORT

Page 1 of 2

Spec. No. 8827

Cont./Supp. Scott

Cont./Supp.I.D. No. _____

PG&E No. _____

283

INSPECTION SECTION

Discrepant Item: Unit I & II. Concrete flush shell anchors installed by Scott Co. for the air conditioning seismic supports.

Explanation of Discrepancy: Possible existence of incorrectly installed concrete anchors. (Continued on Page 2).

DE Nemi
Field Engr./Inspector

3-2-77
Date

CLASSIFICATION & DISPOSITION

Minor Variation ☐

Deviation ☒

Disposition: Accept all Scott Company installed air conditioning seismic support anchors as is. Data contained in the "Procedure for Establishing Acceptance Criteria for Concrete Anchor Installations - Diablo Canyon" on file in the QA vault on site and gathered during an inspection performed by PG&E show that Phillips anchors increase their strength as they are displaced from their embedment. Displacement of the ductwork up

The following members of the Material Review Board concur with the above Disposition: (For Minor Variations, only Resident Engineer's signature required.)

to one inch is acceptable to the responsible Engineer. The duct work can easily tolerate the small movements that anchors might be displaced when subjected to design loads.

Don Ray
Name

3/23/77
Date

R. D. Etyler
Resident Engineer

3-2-77
Date

J. Sawicki
Name

APR - 8 1977
Date

[Signature]
Name

3/23/77
Date

Robert B. Brown
Responsible Engineer

5-2-77
Date

EP Wollak
Supervising Engineer

5/2/77
Date

DISPOSITION ACCOMPLISHED

Remarks: N/A

Field Engineer/Inspector

Date

STEPS TO PREVENT RECURRENCE (Deviations Only)

Scott Company has discontinued using Phillips anchors and will only use anchors manufactured by The Hilti Corp. Scott Co. has initialed an installation procedure for installing Hilti anchors, I-41-2 to assure they are installed correctly.

R. D. Etyler
Resident Engineer

6-13-77
Date

Copies	Attachments	Report Completed
Coor.Q.C. Engr. Dir.-Q.A.	1. Data Sheets	3. Scott Co. Procedure for Anchor Installation
Proj. Super. Resp. Engr.	2. Telecon dtd 3-2-77	
Resident Engr. Proj. Engr.		
Q.A.-Site Supv.Insp.Engr. (G.O.)		

Don Ray
Coordinating QC Engineer

6/28/77
Date

DISCREPANCY REPORT

Page 2 of 2

Cont./Supp. Scott

Cont./Supp.I.D. No. _____

PG&E No. 283

EXPLANATION OF DISCREPANCY:

Of seventy-seven anchor installations inspected, Thirty-three did not have their expansion plugs driven far enough to meet minimum acceptance limits established for Fullman Kellogg.

An attempt was made to drive the expansion plugs further during the inspection. Typically, they could not be driven more than $3/32"$ and then only with great effort.

Masonry bits were used to drill the holes. Bit wear caused slightly undersized holes and the drill point formed a conical shaped bottom. Both of these conditions prevent the expansion plugs from being fully driven.

Inplace pull out tests were performed on eleven of the thirty-three anchors, in accordance with the "Procedure for Establishing Acceptance Criteria for Concrete Anchor Installations - Diablo Canyon Power Plant". Eight of the anchors exceeded the values in Table A of Drawing No. 054162 for 5 kip concrete without being displaced more than 0.010". All eleven anchors significantly exceeded the Table A values without being displaced more than 5% of their minimum embedment (0.120" and 0.160" for 5/8" and 3/4" anchors, respectively). These eleven anchors were typical of the worst case conditions encountered during the inspection.

With the exception of the underdriven expansion plugs, the anchors were installed satisfactorily in all other respects. Also reference PG&E Deviation #282.

SUMMARY OF IN-PLACE TEST RESULTS ON ANCHORS EXHIBITING WORST CASE CONDITIONS

Size of Phillips Anchor	Distance Plug was Driven	% of Allowable Distance	Force Developed by Test	Factor of Safety	Anchor Displaced by Test	% of Allowable Displacement
5/8"	15/32"	94%	4320lb.	2.05	0.034"	28%
5/8"	13/32"	81%	4330lb.	2.06	0.015"	13%
5/8"	1/2 "	100%	4320lb.	2.05	0.026"	22%
5/8"	17/32"	106%	4320lb.	2.05	≈0.125"	104%
5/8"	3/8 "	75%	4320lb.	2.05	0.010"	8%
3/4"	1/4 "	50%	3770lb.	1.09	0.010"	6%
3/4"	9/32"	56%	5800lb.	1.68	0.16 "	100%
*3/4"	9/32"	56%	7160lb.	2.08	0.235"	147%
3/4"	3/8 "	75%	4700lb.	1.36	0.010"	6%
3/4"	17/32"	106%	4350lb.	1.26	0.010"	6%
3/4"	15/32"	94%	4120lb.	1.19	0.007"	4%
3/4"	9/16"	56%	6960lb.	2.02	0.008"	5%

*Continuation of test on preceeding anchor.

[illegible]

A.2.9 For anchors which will be subjected simultaneously to pullout and shear forces, the allowable load values used must satisfy the following formula (Figure 1):

$$\left(\frac{P_C}{P_D}\right)^{5/3} + \left(\frac{S_C}{S_D}\right)^{5/3} \leq 1$$

Where P_D, S_D = allowable loads (pullout, shear), reduced for spacing or edge distance if appropriate

P_C, S_C = allowable loads to be used in cases where pullout and shear loads may occur simultaneously

Note: For convenience in calculation, exponents in the above formula may, conservatively, be reduced to 1.0.

TABLE A
ALLOWABLE LOAD (KIPS) ON EXPANSION ANCHORS

NOMINAL DIAMETER (INCH)	CONCRETE STRENGTH, f_c'									
	2 ksi		3 ksi		4 ksi		5 ksi		6 ksi	
	P	S	P	S	P	S	P	S	P	S
1/4	.25	.30	.275	.30	.30	.30	.325	.30	.35	.30
3/8	.40	.54	.50	.60	.60	.67	.70	.73	.80	.80
1/2	.70	.74	.87	.89	1.05	1.04	1.23	1.19	1.40	1.34
5/8	1.20	1.00	1.50	1.25	1.80	1.50	2.10	1.75	2.40	2.00
3/4	1.60	1.50	2.35	1.80	2.90	2.10	3.45	2.40	4.00	2.70
7/8	2.50	2.00	3.35	2.35	4.20	2.70	5.05	3.05	5.90	3.40
1	3.30	2.50	4.30	2.90	5.50	3.30	6.60	3.70	7.70	4.10
1 1/4	5.30	3.40	6.65	3.95	8.00	4.50	9.35	5.10	10.70	5.70

NOTE: P, PULLOUT; S, SHEAR

For expansion anchors installed in lightweight aggregate concrete, assume $f_c' = 2$ ksi.
See par. A.2.6.

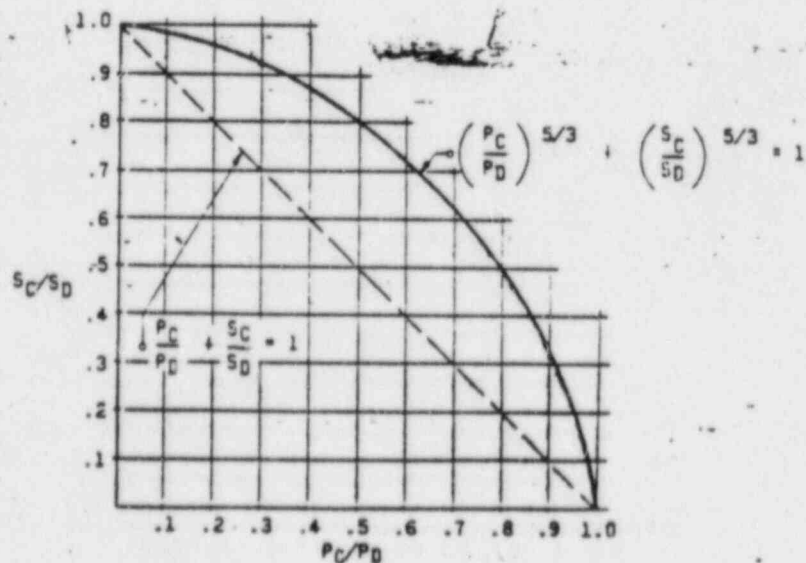


FIGURE 1
REDUCTION FACTORS FOR COMBINED PULLOUT AND SHEAR

B. INSTALLATION

B.1.0 APPLICATIONS

- B.1.1 Provisions of this standard shall apply to the following concrete expansion anchors. Other expansion anchors shall not be used without specific authorization of the Engineer.

SHELL ANCHORS: • PHILLIPS SELF-DRILLING, PHILLIPS NONDRILLING, DIAMOND, HILTI HDI, RAWL SABER-TOOTH,

STUD ANCHORS: • KWIK-BOLT, PARABOLT, PHILLIPS WEDGE, PHILLIPS SLEEVE, WEJ-IT ANKR-TITE,

• PHILLIPS STUD ANCHOR may be used in sizes up to 3/4" diameter.

• WEJ-IT (original style, with spade-shape wedges) may be used, provided embedment is 125% of that shown in Table B, with 50% of the allowable load values shown in Table A.

- B.1.2 Anchors must be at least 1/2" diameter when used for structural connections or for anchorage of pipes, conduits or ducts greater than 2" diameter.

- B.1.3 Anchors shall not be installed in prestressed concrete elements nor used to connect concrete elements which must have a specific value of fire resistance.

B.2.0 INSTALLATION

- B.2.1 Installation of anchors shall be according to manufacturer's instructions as to tools, torque and tightening procedure.

- B.2.2 If a hole cannot be drilled to the correct depth (e.g., if reinforcing steel is encountered while drilling), a new hole shall be drilled. There shall be at least 1/2" of sound concrete between abandoned hole and new hole. If an unused hole is within 4.5 nominal diameters of an expansion anchor, center to center, the unused hole shall be filled with grout or with an expanded anchor.

- B.2.3 If axis of a drilled hole deviates from normal to concrete surface by more than 5° the hole shall not be used unless specifically authorized by the Engineer.

- B.2.4 Minimum required embedment, for shell type anchors, is equal to the length of shell. For most shell anchors the shell may be recessed not more than 1/4 of the nominal diameter. Installed shells recessed to greater depths shall not be used unless specifically authorized by the Engineer.

Minimum required embedment for stud type anchors is given in Table B.

Embedment length is exclusive of thickness of any grout pad or other overlay.

- B.2.5 Anchors shall be installed according to manufacturer's instructions. If, after starting from finger-tightened position, anchor slips more than 10% of minimum required embedment while being tightened, one of the following remedial actions shall be taken:

- Remove bolt or nut, reset anchor, repeat tightening;
- Remove anchor, substitute larger diameter or longer anchor;
- Drill new hole and install additional anchor which satisfies the requirements of this standard.

- B.2.6 Anchor spacing, center to center, shall be not less than 6 times nominal diameter of anchor nor shall edge distance be less than 3 times nominal diameter nor less than 3 inches unless specifically authorized by the Engineer.

- B.2.7 If edge of concrete is chamfered, edge distance shall be measured from nearest edge of chamfer.

B.3.0 PROOF LOADING

When required by the Engineer, proof loading shall be done according to the following instructions:

- B.3.1 Whenever an installation crew starts installing anchors at a job site, each of the anchors installed by that crew shall at first be proof loaded in tension to 250% of the allowable pullout load designated by the Engineer. After five successive anchor installations have been completed without failure, a random selection of 10% of the anchors of each size installed by the crew thereafter on the same project shall be tested in the above manner.

8.3.2 If proof loading is done by jacking against a surface area of concrete surrounding the anchor, the jacking pressure shall be distributed over an annular area of inner diameter at least 3 times the minimum required embedment given in Table 8.

8.3.3 Criteria for failure of an anchor during proof loading are:
(1) concrete cracks, (2) anchor breaks, or (3) anchor slip during the test is greater than 5% of the minimum required embedment.

TABLE 8
MINIMUM EMBEDMENT REQUIRED FOR STUD-TYPE
EXPANSION ANCHORS INSTALLED IN CONCRETE

Nominal Diameter (Inches)	Minimum Embedment (Inches)
1/4	1-1/8
3/8	1-3/4
1/2	2-1/4
5/8	2-7/8
3/4	3-3/8
7/8	4
1	4-1/2
1-1/4	5-5/8

CONCRETE EXPANSION ANCHORS FOR
STATIC AND SEISMIC LOADING

PG&E CO.

DRAWING NUMBER

REV.

SHEET 4 OF 4 SHEETS

054162

3

REVISIONS

DISCREPANCY REPORT

Page 1 of 2

No. 8802

Cont./Supp. H.P. Foley

Cont./Supp. I.D. No. _____

PG&E No. 288 R1

INSPECTION SECTION

Unit I & II

Discrepant Item:

H.P. Foley installed concrete wedge stud anchor bolts.

Explanation of Discrepancy: H.P. Foley Company ordered and installed some concrete anchor bolts which were too short to meet minimum embedment criteria of the installation drawings.

Robert J. Thompson 4-19-77
Field Engr./Inspector Date

CLASSIFICATION & DISPOSITION

Minor Variation ☐

Deviation ☒

Disposition: see attached.

The following members of the Material Review Board concur with the above Disposition:
(For Minor Variations, only Resident Engineer's signature required.)

INDEXED RMS

Don Day 4/20/77
Name Date
House JUN 14 1977
Name Date
E. W. Lenz 6/16/77
Responsible Engineer Date

Robert J. Thompson 4-20-77
Resident Engineer Date
Ed Wallack 4/21/77
Name Date
James H. Wilson 6/16/76
Supervising Engineer Date

DISPOSITION ACCOMPLISHED

Remarks: N.A.

Field Engineer/Inspector _____ Date _____

STEPS TO PREVENT RECURRENCE (Deviations Only)

The majority of the improperly installed anchor bolts were installed prior to implementation of installation procedures by the H.P. Foley Company. This procedure is now in effect.

H. J. Thompson / DOR 6-22-77
Resident Engineer Date

Copies Attachments
Coor. Q.C. Engr. Dir.-Q.A. WA-1
Proj. Super. Resp. Engr. E-72 -1/2"
Resident Engr. Proj. Engr. E-72 -3/8"
Q.A.-Site Supv. Insp. Engr. (G.O.)

Report Completed

Don Day 7/6/77
Coordinating QC Engineer Date

Discrepancy Report
DR-288

Explanation of Discrepancy: A test was performed (Electrical Department Test Procedure WA-1) to determine the minimum embedment required to meet design loading by H.P. Foley Company installed electrical raceway and equipment supports. The maximum design loadings for various sized anchors was determined by multiplying the Table A values in 054162 by 1.66 by the direction E.P. Wollak, Supervising Civil Engineer. As a result of test WA-1 it was determined that embedments of 1 1/8" for 3/8" anchors and 1 1/2" for 1/2" anchors would give adequate pull out strengths.

A field inspection was made of 508 1/2" anchors and 514 3/8" anchors to determine embedment. As part of the inspection the nuts were removed from the studs and the exposed studs were measured. During this inspection no stud anchors were found to have embedments less than the values determined in WA-1. Upon reinstalling the nuts on the studs and torquing the nuts, five 1/2" and two 3/8" stud anchors were discovered not to be set in the concrete. In further torquing two of the 1/2" and both of the 3/8" studs set with adequate embedment after some slippage. Three of the 1/2" anchors were pulled out of the wall and later replaced by H.P. Foley in accordance with their installation procedures.

1/2" and 3/8" stud anchors were inspected because these sizes represent well over 99% of the stud anchors used for raceway support.

Disposition: Accept as is.

An inspection of a representative sample of installed stud anchors shows that less than 1% are improperly installed. A vast majority of the stud anchors installed by H.P. Foley are installed with embedments exceeding those required in 054162. This and the conservation of the raceway support design means that it is unlikely that the failure of one anchor in a support would cause the support to fail. It is extremely unlikely that the small number of improperly installed stud anchors would lead to failure of mutually redundant circuits.

INSPECTION REPORT

File 4-12-77

Discrepancy Report No. DR-288

Description of Work to be performed:

Inspect embedment of 3/8 inch wedge stud anchors.

Inspection Hold Points:

Determine stud length using ultrasonic transducer. Measure stud length exposed from concrete. Calculate stud embedment. Accept embedments of 1 1/8 inch or more. Reject embedments less than 1 1/8 inch.
NOTE: Any 3/8" stud anchor with less than 1 inch exposed will be acceptable and it is not necessary to measure stud length ultrasonically. Mark acceptable studs with green paint. Mark rejected studs with red paint.
Inspect 500 anchors.

Inspector assigned E. Whited

Inspection plan approval

R. J. Thompson Jr.
Resident Engineer

Summary of Inspection Results:

See attached

Inspected by:

R. J. Thompson Jr.

Date

4/15/77

Repair work completed by:

N/A

Date

Approved by:

R. J. Thompson Jr.

Date

4/18/77

Summary of Inspection Results (Continued)

Results of Inspection of 3/8 inch wedge stud anchors

514 bolts were inspected per DR 288 and the following listing of amounts and location were found to be acceptable by visual measurement criteria:

Amount	Area	Elevation
69	D	85
42	C	85
42	B	85
24	B	82
6	A	below 85
44	FE-FW	85
10	K	100
26	K	73
65	H	128
60	H	115
60	H	100
<u>448</u>		

The following list shows amounts and location of studs that were inspected with an ultrasonic measuring device and were acceptable:

Amount	Area	Elevation
3	D	85
2	C	85
2	B	82
5	FE-FW	85
2	GW	115
4	K	100
9	K	73
3	K	64
13	K	below 64
15	H	128
5	H	115
1	H	100
<u>64</u>		

2 suspect studs on K6679, when nuts were torqued to specs. (25 pounds), pulled out of concrete two inches. When checked ultrasonically it was noted that they were 3 1/2 inch studs and the embed was acceptable. However, with that much stud out of the concrete, it required two washers for spacers between clamp and threads in order to tighten nuts.

Additionally; visual inspection of acceptable anchor bolts, by measuring thread length, indicated that the embed of these bolts exceeded 1 1/2". The ultrasonic tests showed that, in all but the two above mentioned bolts, the embed was two inches or more.

INSPECTION REPORT

Discrepancy Report No. DR-288

Date April 8, 1977

Description of Work to be performed:

Inspect inbedment of 1/2 inch wedge stud anchors. Check 500 anchors at random in various locations in the plant.

Inspection Hold Points:

Measure exposed length. If exposed length is less than or equal to 1 1/2" then accept. If greater than 1 1/2" then measure thread length. If thread length 1 1/8" then reject. If thread length 1 1/2" and exposed length is 2 1/2" accept. If exposed length is between 2 1/2" and 2 3/4" reject. Between 2 3/4" and 4" accept. Reject 4".

(see attached)

Inspector assigned C. Holmes

Inspection plan approval

Robert J. Thompson
Resident Engineer

Summary of Inspection Results:

See attached.

Inspected by: C. R. Holmes Date 4/11/77

Repair work completed by: N/A Date _____

Approved by: R. J. Thompson Date 4/16/77

INSPECTION REPORT
(Continued)

DR-288

Exposed length	Thread Length	Accept/Reject
$\leq 1\frac{1}{2}"$	-	Accept
$> 1\frac{1}{2}"$	1 1/8	Reject
$\leq 2\frac{1}{2}"$	1 1/4	Accept
$2\frac{3}{4} > EL > 2\frac{1}{2}$	1 1/4	Reject
$4 \geq EL \geq 2\frac{3}{4}$	1 1/4	Accept
> 4	1 1/4	Reject

Paint end of acceptable studs green, rejected red. Note the location of all rejected studs.

SUMMARY OF INSPECTION RESULTS (Continued)

508 wedge stud anchors were inspected, at random, in the following amounts by area and elevation:

Amount	Area	Elevation
9	H	128
41	A	85
1	B	85
80	K	115
43	K	100
41	K	85
41	K	73
43	F&G	117
124	GW	115
70	GE	115
15	GE	100
<u>508</u>		

DISCREPANCIES:

- 2 - 2 3/4" x 1/2" wedge stud anchors were found in area GW, Elev. 117' on J wall between 15 15' lines that pulled out to 1 3/4" before setting up.
- 1 - 2 3/4" x 1/2" wedge stud anchor was found in Diesel Gen 1-3 room at approx. 88', over s. compressor, that pulled out same as above.
- 1 - 2 3/4" x 1/2" wedge stud anchor was found in Diesel Gen. 1-3 room at approx. 88' over n. compressor, that would only spin in hole. The threads were damaged on this stud and a thread chaser was used to clean up threads, when nut was replaced and tightened the stud set up to torque spec's with acceptable embed.
- 1 - 2 3/4" x 1/2" wedge stud anchor on right upper support for LPH65C (n. wall dsl. gen. 1-3 rm) pulled out of wall as nut was tightened. This happened to be the first suspect stud we came across and nut was not tightened to see how far stud would move before setting tight. After experiencing some similar situations we returned to this stud, tightened it to torque set and found it to have an acceptable embed.

STATION CONST. DEPT.
DIABLO CANYON PROJECT
UNIT _____ GM _____

PACIFIC GAS and ELECTRIC CO.

TEST PROCEDURE

☐ ELECTRICAL
☐ INSTRUMENTATION

TEST PROCEDURE WA-1

CONCRETE WEDGE ANCHORS

PURPOSE:

Determine the minimum embedment required to meet design loading required by H.P. Foley Company installed electrical raceway and equipment supports.

SCOPE:

This procedure will provide data to develop acceptance criteria for concrete anchors for the following conditions in nominal 3,000 PSI and 5,000 PSI design concrete:
(1.) effects at various stages of less than minimum embedment and (2.) angular misalignment.

MATERIAL SPECIFICATION:

Anchors, drills and drill bits, of proper size and type, from regular construction supplies normally used for installation. During this test Hilti Kwik Bolts and Phillips Red Head Wedge Anchors will be tested.

Concrete test slab to be selected from an area on the construction site of the concrete strength noted in Table 1A:

TABLE OF CHANGES

No.	DATE	DESCRIPTION	BY	APPD.
0	3-4-77	Original Typing	<i>cur</i>	<i>RD</i>
1	3-29-77	General Revision	<i>RJD</i>	<i>RD</i>

PREPARED BY *W. Needham* DATE 3-24-77 T.P. No. WA-1 REV. 1
APPROVED BY *R. J. Thompson* DATE 3-29-77 PAGE 1 OF 6

INSTALLATION PROCEDURE:

1. Anchors are to be installed in predrilled holes of the depth and diameter for each anchor as listed in Table 1A. After the hole is drilled, it must be cleared of all loose material. Minimum anchor spacing* to be no less than 12X normal hole diameter.
2. Insert anchor to a sufficient depth that the expanded anchor, by tightening to the torque value shown on Table 1A, is within 1/16" of the depth specified in Table 1A.
3. Measure the exposed anchor length. Record in exposed length column in Table 1A.

TEST PROCEDURE:

1. Position test fixture over embedded anchor and connect to anchor with threaded rod of required size. (Reference Figure 1) Anchors will be pulled perpendicular to the concrete unless otherwise noted in the remarks column.
2. Position dial indicator to detect anchor movement. The dial indicator extension rods shall be attached on the threaded part of the anchor.
3. Increase hydraulic pressure until the dial indicator detects movement of the anchor. Record hydraulic pressure in applicable column on Table 1B.
4. Continue increasing hydraulic pressure until one of the following conditions exist:
 - a. the anchor has slipped greater than 5% of minimum embedment
 - b. the concrete cracks
 - c. the hydraulic pressure reaches the equivalent of 1.06 times (or greater) the force specified in P G & E drawing 054162 for the appropriate concrete strength.
 - d. the anchor breaks.

CAUTION: Particular care should be taken when using the dial indicator on shallow set anchors so that a quick release will not damage the dial indicator.

5. Vent hydraulic pressure and remove test apparatus.
6. Using Figure 2, "Cylinder Force vs. Hydraulic Pressure," determine load applied to anchor at which anchor failure is detected. Record the force in the applicable column on Table 1B. (Figure 2 was developed using Hydraulic Jack listed below and a calibrated gauge. See Procedure for Establishing Acceptance Criteria For Concrete Anchor Installations. Prepared by Thomas E. Niemi, 12-10-76.)

TEST EQUIPMENT

The test fixture consists of a base, support structure, hydraulic cylinder with a hollow ram, pressure gauge, hand operated hydraulic pump, hydraulic hose, threaded rods and long nuts of required size to fit anchors. (See Figure 1.)

Also a dial indicator with a magnetic base and various accessories to measure anchor movement.

Hydraulic Jack - Enerpac 20 Ton, Model RCH-202, OGI.

Pressure Gauge - Ashcroft 2,000 PSIG Duragauge.

TEST NO.	ALLOWED MOVEMENT	CURT PRESS. AT INITIAL MOVEMENT	CURT PRESS. AT ANCHOR SET	DISPLACEMENT AT SET (INCHES)	PASS OR FAIL	CURT PRESS. AT FAILURE (PSI)	TENSILE FAIL FORCE (LBS.)	TYPE FAILURE	REMARKS
1	.113	450	450	.001	P				
			500	.002					
			550	.002					
			600	.005					
			650	.008					TEST DISCONTINUED
2	.113	530	550	.002	P				
			600	.006					
			650	.010					TEST DISCONTINUED
3	.113	420	650	.025	P				
			700	.034					
			750	.039					
			800	.050		810	2990	concrete	
4									NO SET
5	.113	440				460	1600	concrete	
6									NOT TESTED
7	.113	200	250	.002					
			300	.003					
			350	.004					
			400	.005					
			425	.012	✓				
			450	.025	F	450	1575	concrete	

T.P. 117-1 REV. 1

TESTED BY C. Needham DATE 2-20-77

NO.	DATE	AT INITIAL LOAD (LBS.)	AT RECORD SET	AT SET (INCHES)	OR FAIL	AT FAILURE (PSI)	FAIL FORCE (LBS.)	REMARKS
8	.113	200	250	.003				
			300	.005				
			350	.008				
			400	.014				
9			425	.050	F	425	1500	concrete
10								NO TEST
11								NO TEST
12								NO TEST
13	.113	400	425	.003	✓			
			450	.004	P			
			500	.005				
			550	.008				
			600	.020				
				NO SET				
14	.113	360	400	.005	✓	650	2350	concrete
			450	.010	P			
				NO SET				
15	.113	400		.030 2ND SET	F	500	1775	concrete
						590	2155	concrete

TESTED BY C Needham

DATE 3-29-77

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PAGE 461
REV. 1
C

NO.	ALL OVER	AT INITIAL LOAD SET	AT ANCHOR SET	AT SET (INCHES)	OR FAIL	AT FAILURE (FSI)	TENSILE FAIL FORCE (LBS.)	TYPE FAILURE	REMARKS
16	.113	500	500	.001	P				
			550	.002					
			600	.006					
			650	.010					
			700	.020					TEST DISCONTINUED
17	.113	300	425	.007	✓				
			450	.009	P				
			500	.010					
			550	.013					
			600	.017		650	2350	concrete	
18	.113	250	425	.020	✓				
			450	.020	P				
			500	.030					
				.060 NO SET		550	1975	concrete	
19	.113	350	425	.009	✓				
			450	.010	P				
			500	.011					
			550	.015					
20			600	.018					

TESTED BY C Needham

DATE 3-29-77

T.P. 11/1-1
REV. 1
DATE 201

NO.	ALLOY OVERLAP	AT INITIAL PROPERT	AT RICHOP SET	AT SFT (INCHES)	OR FAIL	AT FAILURE (PSI)	FAIL FORCE (LBS.)	REMARKS
22	.113		550	.002				
			600	.004				
			650	.008@2min				
23	.113	450	625	.028	P			Axis @ 19°
			650	.031@3min				
24	.113	350	625	.027	P			Axis @ 21°
			650	.033@3min				
25	.113	480	625	.027	P			Axis @ 20°
			650	.027@3min				
26	.113	330	600	.020	P			Axis @ 20°
			625	.025				
			650	.030@3min				
27	.113	475	500	.004	P			
			550	.005				
			600	.006				
			650	.012				
			700	.021				
			750	.030				
			800	.040				
			850	.046				
CONT.								

DATE 3-30-77

TESTED BY C Needham

N.	OVER	AT INITIAL IMPEMENT	AT ANCHOR SET	AT SET (INCHES)	OR FAIL	AT FAILURE (PSI)	TESTILE FAIL FORCE (LBS.)	TIME TO FAILURE	REMARKS
27			900	.059					
			950	.064					
			1000	.071					DISCONTINUED TEST
28									NO TEST
29									NO TEST
30									NO TEST
31									NO TEST
32									NO TEST
33	.113	425	425	.003	✓				
			450	.005	P				
			500	.007					
			550	.010					
			600	.020					
			650	.028					
			700	.038					
			750	.050					
			800	.060					
			850	.070					
			900	.085					
			950	.099					
			1000	.102					DISCONTINUED TEST

TESTED BY C. Needham

DATE 3-30-77

T.P. 17-1 REV. 1
PAGE 4 of 6

ALLOCATION NUMBER	AGE IN DAYS AT INITIAL MOVEMENT	AGE IN DAYS AT NEXT SET	DATE OF SET (INCHES)	FAIL OR FAIL	AT FAILURE (PSI)	LOAD FAIL FORCE (LBS.)	REMARKS
4							NO TEST
5	.113	360	.002	✓			
		425	.002	P			
		450	.004				
		500	.009				
		550	.008		600	2175	concrete
6	.113	250	.008	✓			
		425	.008	P			
		450	.009				
		500	.008		550	1975	concrete
7	.113	360	.008	✓			
		425	.009	P			
		450	.012				
		500	.018				
		550	.027				
		600	.035				
		650	.048				
		700	.002	✓			
8	.113	280	.002	P			
		425	.002				
		450	.003				
		500	.004				
		550	.007				
		600	.014		700	2550	concrete
		650					
							DISCONTINUED TEST

TESTED BY C. Needham

DATE 3-31-77

T.P. 111-1 REV. 1
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NO.	ALLIGATOR POVERTY	LOAD AT INITIAL POVERTY	LOAD AT ANCHOR SET	DEFORMATION AT SET (INCHES)	LOAD OR FAIL	LOAD AT FAILURE (PSI)	FAILURE FAIL FORCE (LBS.)	REMARKS
9								NO TEST
10	.113	450	450	.001	✓			
			500	.003	P			
			550	.005				
			600	.008				
			650	.010				
			700	.014				
			750	.019				DISCONTINUED TEST
11								NO SET
12	.088	270	300	.001	✓			
			325	.001	✓			
			350	.002	P			
			375	.002				
			400	.002				
			425	.003				
			450	.004				
			475	.005				
			500	.010				
			525	.010				
			550	.015				DISCONTINUED TEST AFTER 3 MIN OF SET

T.P. 111-1 REV. 1
PAGE 4 of 6

TESTED BY C Needham DATE 3-31-77

ALLIGATOR COVERING	DATE PULSED AT INITIAL TENSILE	DATE PULSED AT ANCHOR SET	DISPLACEMENT AT SET (INCHES)	PASS OR FAIL	STRESS AT FAILURE (PSI)	TENSILE FAIL FORCE (LBS.)	TYPE FAILURE	REMARKS
4 .088	500	500	.001	P				NO TEST
		525	.002					
		550	.002					DISCONTINUED TEST
								NO TEST
								NO TEST
7 .088	110	270	.015	✓				
		300	.016	P				
		325	.020					
		350	.024					
		375	.035					
		400	.052		400	1400	concrete	FAILED AFTER 5 MIN
8 .088	120	270	.022	✓				
		300	.023	P				
		325	.028					
		350	.045		350	1200	concrete	FAILED AFTER 5 MIN
9 .088	240	270	.006	✓				
		300	.007	P				
		325	.008					
		350	.009					

T.P. 117-1 REV. 1/6

DATE 3-31-77

C Needham

TESTED BY

ALLGAGE TOWEENT	GAUGES AT INITIAL PROPERTY	GAUGES AT ANCHOR SET	DISPLACEMENT AT SET (INCHES)	PASS OR FAIL	AT FAILURE (PSI)	FAIL FORCE (LBS.)	REMARKS
9		375	.012				
		400	.019				
		425	.032				
		450	.050		450	1575	concrete
0 .088	240	270	.001	✓			
		300	.001	P			
		325	.002				
		350	.003				
		375	.003				
		400	.006				
		425	.020		425	1500	concrete
51 .088	190	270	.003	✓			
		300	.003	P			
		325	.003				
		350	.004				
		375	.006				
		400	.007				
		425	.0209		425	1500	concrete

T.P. 117-1 REV. 1
PAGE 4 of 6

TESTED BY C Needham DATE 4-1-77

COVER	AT INITIAL MOVEMENT	AT MAXIMUM SET	AT SET (INCHES)	OR FAIL	AT FAILURE (PSI)	FAIL FORCE (LBS.)	REMARKS
52 .088	325	325	.001	P			
		350	.002				
		375	.004				
		400	.005				
		425	.007				
		450	.025		450	1575	concrete
53 .088	140	270	.019	✓			
		300	.021	P			
		325	.025				
		350	.027				
		375	.030				
		400	.035				
		425	.038				
		450	.042				
54 .088	160	270	.001	✓			
		300	.001	P			
		325	.002				
		350	.003				
		375	.005				
		400	.007				

TESTED BY C Needham

DATE 4-1-77

ALLOU- MENT	LOAD PRESS. AT INITIAL PROPERTY	LOAD PRESS. AT ANCHOR SET	DEFLAC- TION AT SET (INCHES)	PASS OR FAIL	LOAD PRESS. AT FAILURE (PSI)	LOAD FORCE (LBS.)	TYPE FAILURE	REMARKS
4		425	.010					
5	.088	160		F	270	830	concrete	DISCONTINUED TEST INSPECTION OF CONCRETE SHOWED CRACK
6	.056	200	.003	P	225	700	concrete	
7	.056	200	.001	P				
		225	.002					
		250	.005					
		275	.014		275	900	concrete	
8	.056	200	.002	P				
		225	.003		250	800	concrete	
9	.056	200	.003	P				
		225	.004					
		250	.017		275	900	concrete	NO TEST
10								
11	.144	190	.062	✓				
		700	.067	P				
		750	.085					
		800	.105		850	3125	concrete	
12	.144	160	.040@5mm	✓				
		700	.048@3mm	P				
		750	.060@3mm					

TESTED BY C Needham

DATE 4-8-77

T.P. 117-1 REV. 1
101

NO.	PLACEMENT	AT INITIAL HEIGHT	AT ANCHOR SET	AT SET (INCHES)	OR FAIL	AT FAILURE (PSI)	FAIL FORCE (LBS.)	REMARKS
2			800	.092 @ 4 min		820	3020	concrete
3	.088	170			F	170	520	concrete
4	.088	110	270	.027 @ 1 min	✓			
			300	.029 @ 2 min	P			
			325	.032 @ 1 min				
			350	.047 @ 4 min		375	1300	concrete
5								NO TEST
6								NO TEST
7	.088	180	270	.004	✓			
			300	.006 @ 1 min	P			
			325	.006 @ 1 min				
			350	.011 @ 2 min				
			375	.017 @ 1 min				
			400	.027 @ 2 min				
			425	.040 @ 1 min		450	1575	concrete
8								NO TEST
9	.088	100			F	240	790	concrete
10	.088	140	270	.012 @ 1 min	✓			
			300	.013 @ 2 min	P			
			325	.014 @ 2 min				
OUT			350	.015 @ 1 min				

TESTED BY C Macdhan

DATE 4-8-77

T.P. 11-1 REV. 1
DATE 4/1/77

REPAIR

HOLE
DEPTH

AXIS OF
ANCHOR TO
SLAB

INSTALLATION
SET TORQUE
(FT. LBS.)

CONCRETE
STRENGTH
(KSI)

MAXIMUM
TEST PRESS.
(PSI)

ACTUAL
EMBEDMENT

EXPOSED
LENGTH

TEST
EMBEDMENT

TEST
NO.

ANCHOR
DIAMETER, LENGTH
& ETC.

T.P. 1A-1 REV. 1

3-29-77

DATE

TESTED BY C Needham

1	1/2 x 3 3/4 H/H		2 1/4"	1 1/2"	425	3	45	< 5°	1 1/16
2	1		2 7/16"	1 5/16"	↑	↑	↑	↑	1 9/16
3			2 3/8"	1 3/8"					1 5/8
4			N/D SET	✓					1 1/4
5			2 1/16"	1 1/16"					1 5/16
6			2 3/4"	1"					1 1/4
7			2 1/16"	1 1/16"					1 3/8
8			2 5/8"	1 1/8"					1 3/8
9			2 1/16"	1 1/16"					1 3/8
10			2 3/8"	1 3/8"					1 9/16
11			2 5/8"	1 1/8"					1 1/2
12			2 3/8"	1 3/8"					1 1/2
13			2 1/2"	1 1/4"					1 7/16
14			2 1/2"	1 1/4"					1 1/2
15			2 1/2"	1 1/4"					1 7/16
16			2 1/4"	1 1/2"					1 3/4
17			2 5/16"	1 7/16"					1 11/16
18			2 5/16"	1 7/16"					1 11/16
19			2 1/16"	1 11/16"	↓	↓	↓	↓	1 15/16
20			2 5/16"	1 7/16"					1 15/16
21	1 1/2 x 3 3/4 H/H		2 1/16"	1 11/16"	425	3	45	< 5°	1 7/8

ANCHOR TYPE, LENGTH (IN.)	TEST NO.	TEST EMBEDMENT	EXPOSED LENGTH	ACTUAL EMBEDMENT	MAXIMUM TEST PRESS. (PSI)	CONCRETE STRENGTH (KSI)	INSTALLATION SET TORQUE (FT. LBS.)	AXIS OF ANCHOR TO SLAB	HOLE DEPTH
1" x 3 3/4" H.H.	22		2 1/16"	1 11/16"	425	3	45	< 5°	1 5/16"
1" x 3 3/4" H.H.	23		2 1/4"	1 1/2"	↑	↑	↑	19°	1 1/16"
1" x 3 3/4" H.H.	24		2 3/16"	1 9/16"				21°	1 3/4"
1" x 3 3/4" H.H.	25		2 1/16"	1 11/16"				20°	1 5/16"
1" x 3 3/4" H.H.	26		1 5/16"	1 13/16"				20°	2"
1" x 3 3/4" H.H.	27		1 5/32"	2 9/32"				< 5°	2 7/16"
1" x 3 3/4" H.H.	28		1 5/8"	2 1/8"				↑	2 13/32"
1" x 3 3/4" H.H.	29		1 5/16"	2 7/16"					2 21/32"
1" x 3 3/4" H.H.	30		1 3/8"	2 3/8"					2 1/16"
1" x 3 3/4" H.H.	31		1"	2 3/4"					2 15/16"
1" x 3 3/4" H.H.	32		1"	2 3/4"					2 1/2"
1" x 3 3/4" H.H.	33		1 7/16"	2 5/16"					2 1/16"
1" x 3 3/4" H.H.	34		1 7/32"	2 17/32"					1 7/16"
1" x 4 1/4" Red- head	35		3 1/16"	1 3/16"					1 7/16"
1" x 4 1/4" Red- head	36		3 1/8"	1 1/8"					1 21/32"
1" x 4 1/4" Red- head	37		2 13/16"	1 7/16"					1 21/32"
1" x 4 1/4" Red- head	38		2 13/16"	1 7/16"					1 15/16"
1" x 4 1/4" Red- head	39		2 1/2"	1 3/4"					1 29/32"
1" x 4 1/4" Red- head	40		2 5/8"	1 5/8"	425	3	45	< 5°	

T.P. 1A-1 REV. 1

2-20-77

DATE

1 Woodham

TESTED BY

ANCHOR TYPE, LENGTH & ETC.	TEST NO.	TEST EVIDENCE	EMBEDMENT LENGTH	ACTUAL EMBEDMENT	TEST PRESS. (PSI)	STRENGTH (KSI)	SET TORQUE (FT. LBS.)	ANCHOR TO SLAB	DEPTH
3/8" x 3 1/2" H/H/H	41		NO SET	✓	270	3	25	< 5°	13/8"
↑	42		2 1/4"	1 1/4"	↑	↑	↑	↑	15/8"
↑	43		2 1/8"	13/8"					1 1/16"
↑	44		2 3/16"	15/16"					1 1/16"
↑	45		2 9/16"	15 1/16"					1 1/4"
↑	46		2 1/8"	13/8"					1 3/4"
↑	47		2 5/16"	13/16"					1 3/8"
↑	48		2 5/16"	13/16"					1 7/16"
↑	49		2 3/8"	1 1/8"					1 1/32"
3/8" x 3 1/2" H/H/H	50		2 3/8"	1 1/8"					1 3/8"
3/8" x 5" Red head	51		4"	1"					1 5/16"
↑	52		4"	1"					1 5/16"
↑	53		3 7/8"	1 1/8"					1 7/16"
↑	54		3 13/16"	1 3/16"					1 1/2"
3 1/8" 5" Red head	55		3 7/8"	1 1/8"	270		25		1 7/16"
1 1/4" x 2 1/4" H/H/H	56		1 7/16"	13/16"	160		10		1 1/16"
↑	57		1 1/2"	3/4"	↑		↑		1"
↑	58		1 1/2"	3/4"	↑		↑		1 1/8"
↑	59		1 3/8"	7/8"	↑		↑		1 1/8"
1 1/4" x 2 1/4" H/H/H	60		1 1/4"	1"	160	3	10	< 5°	1 3/16"

REPAIR

ANCHOR SPACER, LENGTH & ETC.	TEST NO.	TEST EMBEDMENT	EXPOSED LENGTH	ACTUAL EMBEDMENT	MAXIMUM TEST PRESS. (PSI)	CONCRETE STRENGTH (KSI)	INSTALLATION SET TORQUE (FT. LBS.)	AXIS OF ANCHOR TO SLAB	HOLE DEPTH
1" x 4 1/2" H/H/H	61		2 7/8"	1 5/8"	685	3	60	< 5°	1 5/16"
1" x 4 1/2" H/H/H	62		2 7/8"	1 5/8"	685	1	60	↓	1 7/8"
1" x 3 1/2" H/H/H	63		2 9/16"	1 5/16"	270		45	↓	1 1/4"
1" x 4 1/2" H/H/H	64		2 7/16"	1 1/16"	↓		↓	↓	1 5/16"
1" x 4 1/2" H/H/H	65		2 5/16"	1 3/16"	↓		↓	↓	1 3/8"
1" x 4 1/2" H/H/H	66		2 5/16"	1 3/16"	↓		↓	↓	1 7/16"
1" x 4 1/2" H/H/H	67		2 3/8"	1 1/8"	↓		↓	↓	1 5/16"
1" x 4 1/2" H/H/H	68		2 1/4"	1 1/4"	↓		↓	↓	1 3/8"
1" x 4 1/2" H/H/H	69		2 3/8"	1 1/8"	↓		↓	↓	1 5/16"
1" x 4 1/2" H/H/H	70		2 1/2"	1"	↓		↓	↓	1 1/4"
1" x 3 1/2" H/H/H	71		2 13/32"	1 3/32"	270	3	45	< 5°	1 3/8"

T.P. 1/A-1 REV. 1

DATE 4-8-77

TESTED BY R. M. Beckham

NO.	OVER EX. (INCHES)	AT INITIAL LOAD (LBS.)	AT ACCEPT SET	AT SET (INCHES)	OR AT FAILURE FAIL	AT FAILURE (PST)	FAIL FORCE (LBS.)	REMARKS
1	.113	200		.065 @ 1 min	F	575	2075	concrete
2	.113	330	575	.007 @ 5 min	✓			
			600	.011 @ 4 min	P			
			650	.019 @ 5 min				
			700	.045 @ 8 min		700	2550	concrete
3	.113	500	575	.015 @ 2 min	✓			
			600	.022 @ 3 min	P			
			650	.055 @ 12 min				
			650	.060 @ 15 min				
			700	.069 @ 3 min				
			700	.075 @ 6 min				
			700	.080 @ 9 min				
			700	.095 @				
4	.113	260		.035 @ 5 min	F	700	2550	concrete
5	.113	350	575	.025 @ 2 min	✓	575	2075	concrete
			600	.027 @ 2 min	P			
			650	.039 @ 4 min				
			700	.115 @ 6 min		700	2550	concrete

T.P. 117-1 REV. 1

DATE 4-4-77

TESTED BY C Needham

REMARKS

TYPE FAILURE

TENSILE
FAIL FORCE
(LBS.)POND
OR
FAIL
AT FAILURE
(PSI)DILATED TO
AT SET
(INCHES)GROUT PLUG
AT ANCHOR
SETCOUL PLUG
AT INITIAL
TENSILEALLG
OVERCENT
(INCHES)TEST
NO.

6 .113

410

575

.048 @ 10 min

✓

Maximum
slip

2750

7 .113

555

575

.001 @ 2 min

✓

8 .113

340

575

.004 @ 1 min

P

concrete

2950

800

T.P. 117-1 REV. 1

DATE 4-4-77

TESTED BY C. Needham

TEST NO.	ALLOVED OVERSTRESS	AT INITIAL LOAD SET	AT NICHING SET	AT SET (INCHES)	OR FAIL	AT FAILURE (PSI)	FAIL FORCE (LBS.)	REMARKS
15	.088	110	345	.007	✓			
			375	.015 @ 6 min	P			
			400	.019				
			425	.030 @ 5 min				
			450	.041				
			475	.051				
			500	.055 (set)				
16	.088	70	345	.006 @ 4 min	✓			
			375	.010 @ 3 min	P			
			400	.014 @ 3 min				
			425	.035 @ 3 min				
			450	.061 @ 10 min				
			475	.065 ^A		475	1700	concrete
17	.088	80	345	.050	✓			
			375	.065 @ 3 min	P			
			400	.071 @ 5 min				
			425	.093 @ 5 min				
			450	.100 @ 1 min		450	1575	maximum movement

T.P. 11f-1
REV. 1

DATE 4-5-77

TESTED BY C Needham

TEST NO.	ALLOWED MOVEMENT	LOAD PRESS. AT INITIAL MOVEMENT	LOAD PRESS. AT ARCHING SET	DISPLACEMENT AT SET (INCHES)	FROM OR FAIL	LOAD PRESS. AT FAILURE (PSI)	LOAD CELL FAIL FORCE (LBS.)	TYPE FAILURE	REMARKS
18	.088	110	345	.054 @ 10 min	✓				
			375	.062 @ 6 min	P				
			400	.069 @ 5 min					
			425	.082 @ 8 min					
			450	.098 @ 3 min		450	1575	maximum movement	
19									NO TEST
20									NO TEST
21									NO TEST
22	.056	80	185	.001	✓				
			200	.001	P				
			225	.003					
			250	.007					
			275	.014		300	100	concrete	
23	.056	120	185	.002	✓				
			200	.002	P				
			225	.008					
			250	.017					
			275	.023					
			300	.030		325	1100	concrete	

TESTED BY C Needham

DATE

4-8-77

T.P. 117-1 REV. 1

TEST NO.	ALLIANCE MOVEMENT	LOAD (LBS.) AT INITIAL MOVEMENT	LOAD (LBS.) AT ANCHOR SET	DISPLACEMENT AT SET (INCHES)	OR FAIL	AT FAILURE (PSI)	FAIL FORCE (LBS.)	REMARKS
24	.056	175	185	.002	✓			
			200	.002	P			
			225	.004				
			250	.009 @ 2 min				
			275	.015 @ 1 min				
			300	.020 @ 2 min		325	1100	concrete
25	.144	500			F	945	3486	concrete
26	.144	630			F	700	2550	concrete
27	.144	650	945	.090 @ 3 min	✓			
			1000	.110 @ 5 min	P			
			1050	.118 @ 2 min				
			1100	.130 @ 2 min		1150	4325	concrete
28	.144	300			F	945	3486	concrete
29	.144	400	945	.110 @ 3 min	✓			
			1000	.130	P			
			1050	.140		1100	4125	concrete
30	.144	440	945	.139 @ 1 min	✓			
			1000	.144 @ 1 min	P			
			1050	.155 @ 1 min				
			1100	.165 @ 1 min				
31			1150	.175 @ 1 min				

T.P. 117-1 REV. 1/6

DATE 4-8-77

TESTED BY C Needham

TEST NO.	ALLOWED MOVEMENT	GAUGE PLACES AT INITIAL MOVEMENT	LOAD AT ANCHOR SET	DEFL. (INCHES) AT SET	PAGE OR FAIL	AT FAILURE (PSI)	FAILURE FAIL FORCE (LBS.)	TYPE FAILURE	REMARKS
30			1200	.190 @ 1 min				maximum movement	
31	.088	120	1250	.250 @ 1 min	F	375	1300	concrete	
32	.088	135	345	.020 @ 3 min	✓				
			375	.021 @ 1 min	P				
			400	.022					
			425	.023					
			450	.026					
			475	.040 @ 2 min		500	1775	concrete	
33	.088	180	345	.037 @ 4 min	F	370	1280	concrete	NO TEST
34									NO TEST
35									
36	.088	220	345	.021 @ 1 min	✓				
			375	.022	P				
			400	.024					
			425	.027					
			450	.030					
			475	.034		500	1775	concrete	
37									NO TEST

T.P. 117-1 REV. 1

DATE 4-8-77

TESTED BY C Needham

REMARKS

TYPE FAILURE

TENSILE
FAIL FORCE
(LBS.)LOAD AT FAILURE
AT FAILURE
(PSI)PASS
OR
FAILDISTANCE
AT SFT
(INCHES)LOAD AT
AT ANCHOR
SETLOAD AT
AT INITIAL
MOVEMENTST
D.

DISCONTINUED TEST

T.P. 117-1
REV. 1

DATE 4-8-77

TESTED BY C Needham

REIN

ANCHOR QUANTITY, LENGTH & ETC.	TEST NO.	TEST EMBEDMENT LENGTH	ACTUAL EMBEDMENT	MAXIMUM TEST PRESS. (PSI)	CONCRETE STRENGTH (KSI)	INSTALLATION SET TORQUE (FT. LBS.)	AXIS OF ANCHOR TO SLAB	HOLE DEPTH
1/2 x 3 3/4" H/H/H	1	2 3/8"	1 3/8"	575	5	45	< 5°	1 19/32"
↑	2	2 5/16"	1 7/16"	↑	↑	↑		1 19/32"
↑	3	2 3/16"	1 9/16"					1 11/16"
↑	4	2 7/16"	1 5/16"					1 11/16"
↑	5	2 3/16"	1 9/16"					1 11/16"
1/2 x 3 3/4" H/H/H	6	2 1/16"	1 11/16"					1 7/8"
1/2 x 5 1/2" Red-head	7	4 1/8"	1 3/8"			↓		1 11/16"
1/2 x 5 1/2" Red-head	8	4 1/8"	1 3/8"	575		45		1 11/16"
3/8 x 3 1/2" H/H/H	9	2 3/8"	1 1/8"	345		25		1 1/4"
" "	10	2 5/8"	7/8"	↑		↑		1 1/4"
3/8 x 3 1/2" H/H/H	11	2 3/8"	1 1/8"					1 1/4"
3/8 x 5" Red-head	12	3 7/8"	1 1/8"					1 1/4"
3/8 x 3 1/2" H/H/H	13	2 7/16"	1 1/16"					1 1/4"
↑	14	2 5/16"	1 3/16"					1 1/4"
↑	15	2 5/16"	1 3/16"					1 1/4"
↑	16	2 1/4"	1 1/4"					1 3/8"
↑	17	2 3/16"	1 5/16"					1 3/8"
↑	18	2 7/32"	1 9/32"			↓		1 3/8"
3/8 x 3 1/2" H/H/H	19	2 1/16"	1 7/16"	345		25	↑	1 5/8"
1/2 x 3 3/4" H/H/H	20	1 5/8"	2 1/8"	575	5	45	< 5°	2 3/16"

T.P. 1A-1 REV. 1

DATE 4-11-77

TESTED BY C Needham

ANCHOR DIMENSIONS, LENGTH IN FEET	TEST NO.	TEST EMBEDMENT	EXPOSED LENGTH	ACTUAL EMBEDMENT	MAXIMUM TEST PRESS. (PSI)	CONCRETE STRENGTH (KSI)	INSTALLATION SET TORQUE (FT. LBS.)	AXIS OF ANCHOR TO SLAB	HOLE DEPTH	REMARKS
1/4" x 2 1/4" H1/H1	21		1 1/4"	1"	185	5	10	< 5°	1 1/8"	
" " "	22		1 1/2"	3/4"	↑	↑	↑	↑	1"	
1/4" x 2 1/4" H1/H1	23		1 7/16"	13/16"	↑		↓		1"	
1/4" x 3" H1/H1	24		2 3/16"	13/16"	185		10		7/8"	
5/8" x 4 1/2" H1/H1	25		2 3/4"	13/4"	945		60		1 7/8"	
	26		2 15/16"	1 9/16"	↑		↑		1 3/4"	
	27		2 1/2"	2"	↑		↑		2 1/8"	
	28		2 1/2"	2"	↑		↑		2 1/8"	
	29		2 1/2"	2"	↑		↑		2 1/8"	
5/8" x 4 1/2" H1/H1	30		2 1/4"	2 1/4"	945		60		2 3/8"	
3/8" x 3 1/2" H1/H1	31		2 1/2"	1"	345		45		1 5/16"	
	32		2 3/8"	1 1/8"	↑		↑		1 3/8"	
	33		2 13/32"	1 3/32"	↑		↑		1 11/32"	
	34		2 1/4"	1 1/4"	↑		↑		1 13/32"	
	35		2 3/16"	1 5/16"	↑		↑		1 7/16"	
	36		2 3/8"	1 1/8"	↑		↑		1 3/8"	
	37		2 5/16"	1 3/16"	↑		↑		1 11/32"	
3/8" x 3 1/2" H1/H1	38		2 3/8"	1 1/8"	345	5	45	< 5°	1 3/8"	

TESTED BY C. Needham

DATE 4-8-77

T.P. 11A-1

REV. 1

PERFORMED BY:

C Needham

DATE: 4-20-77

APPROVED BY:

Robert J. Thompson

DATE: 4-20-77

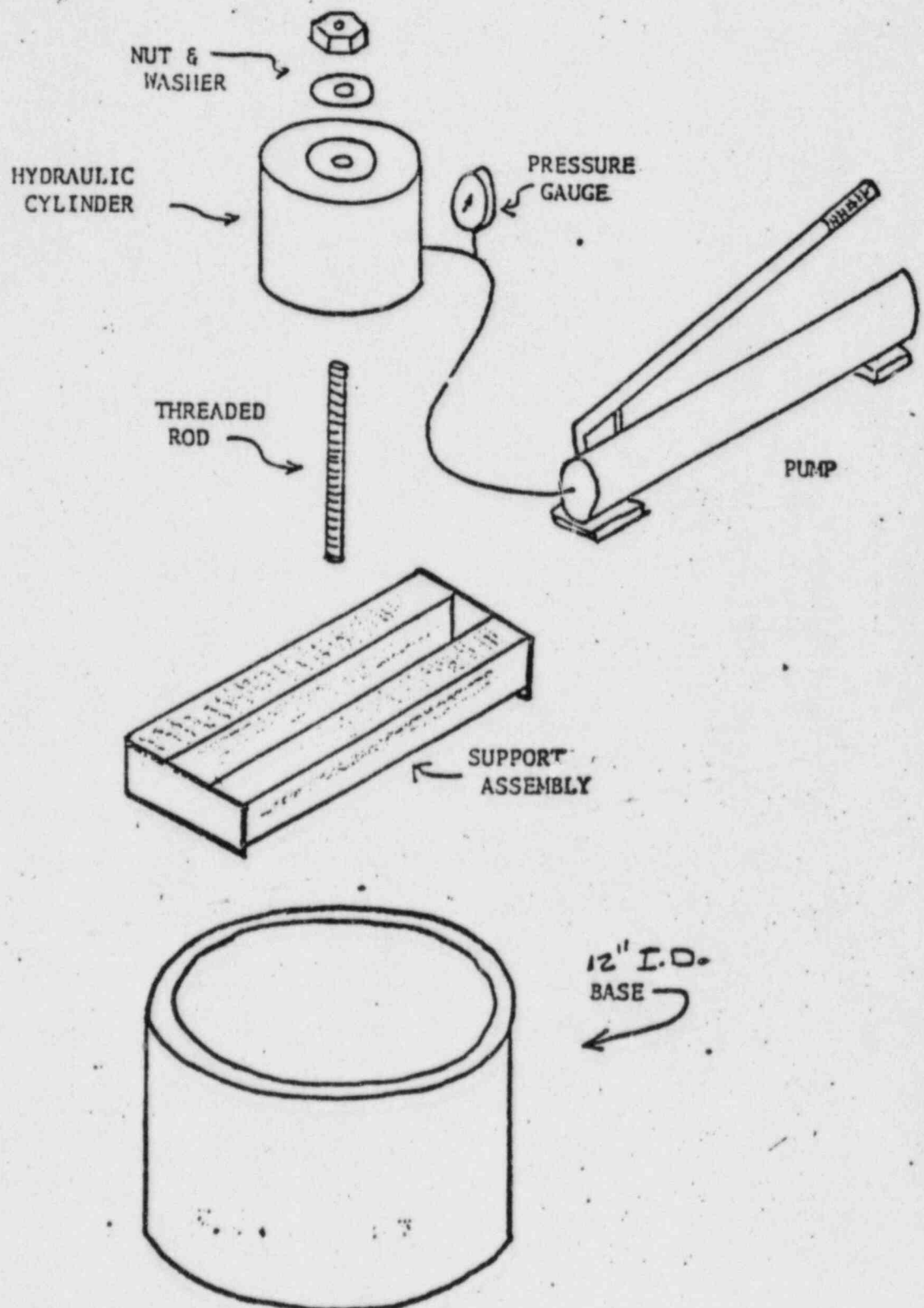
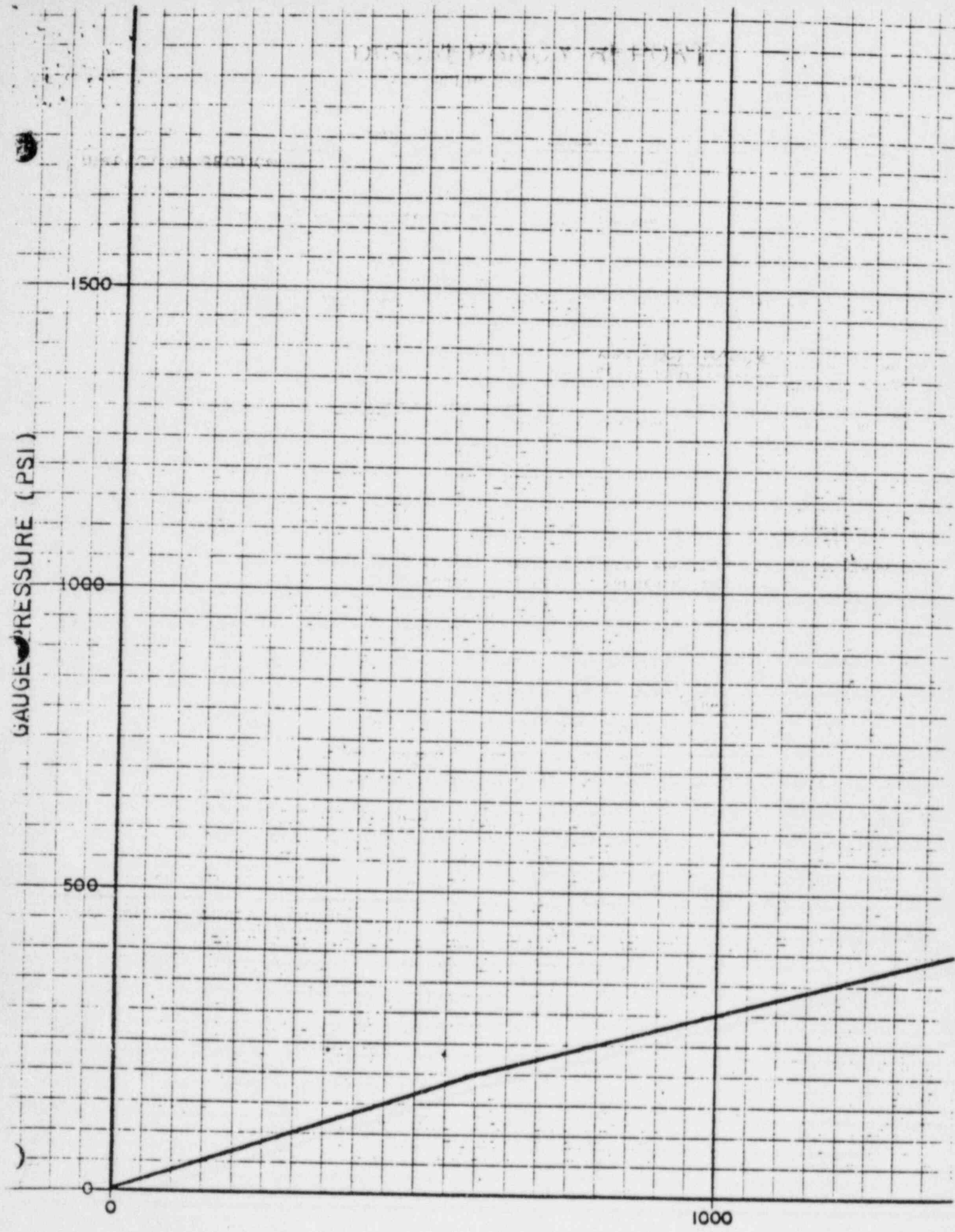
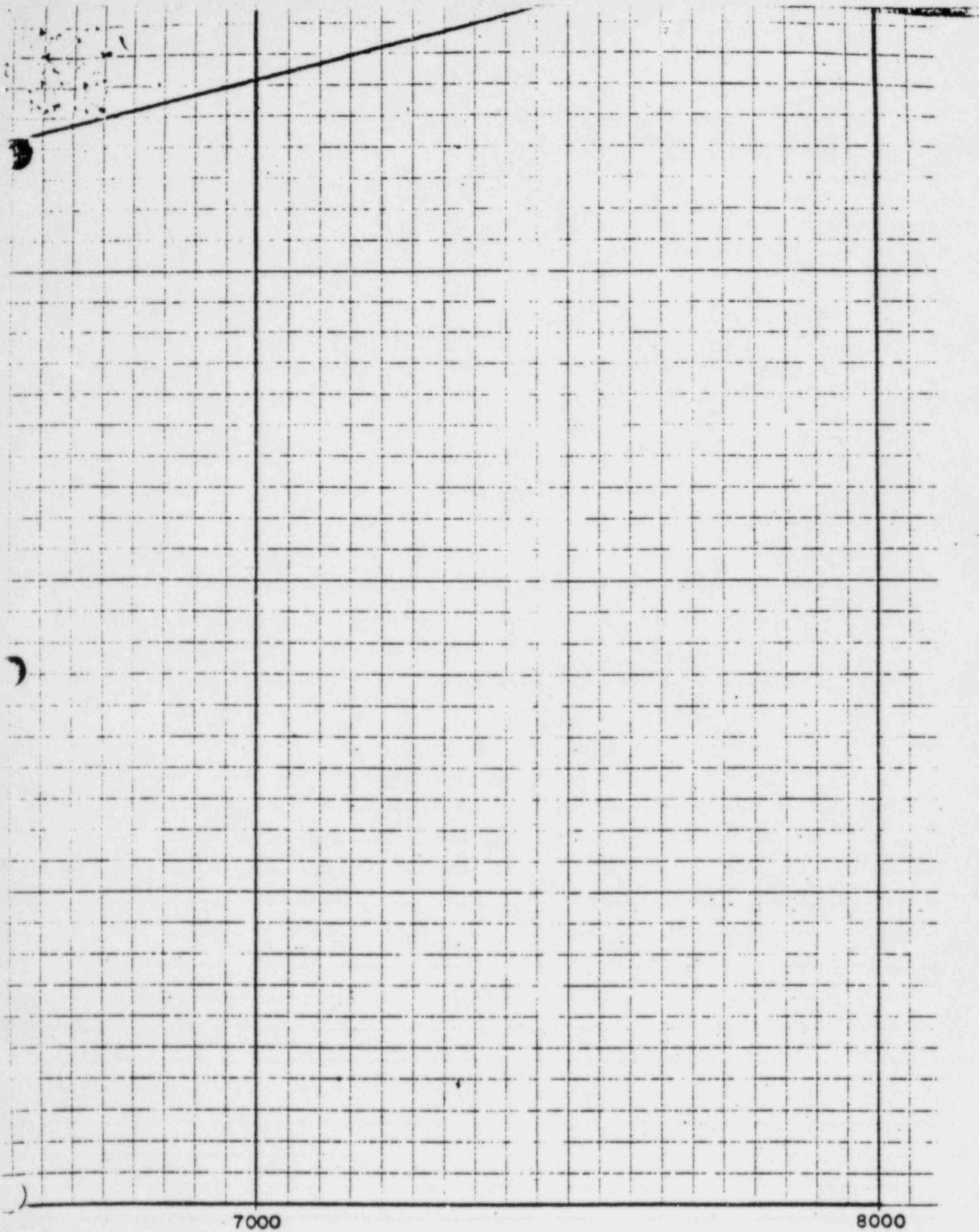
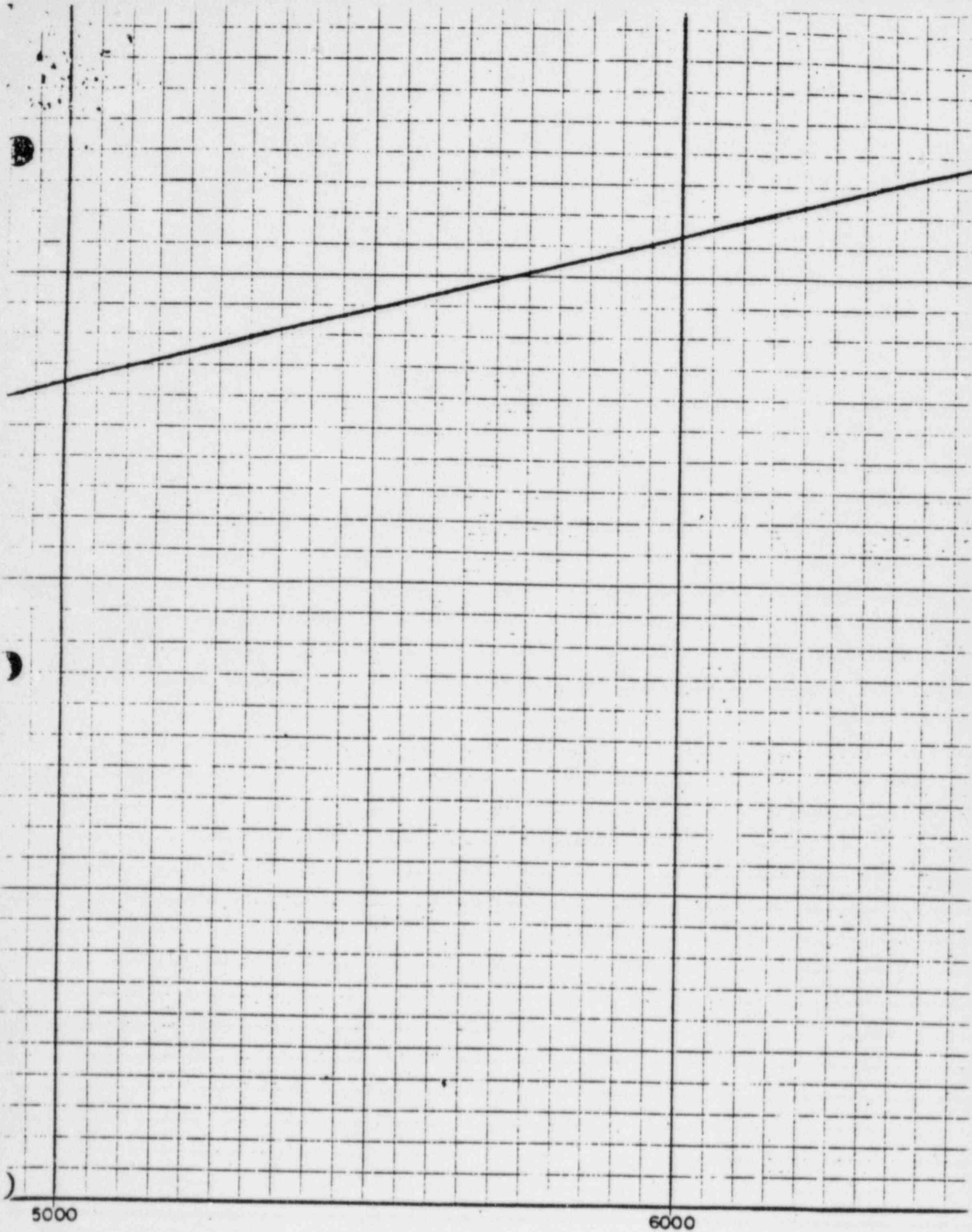


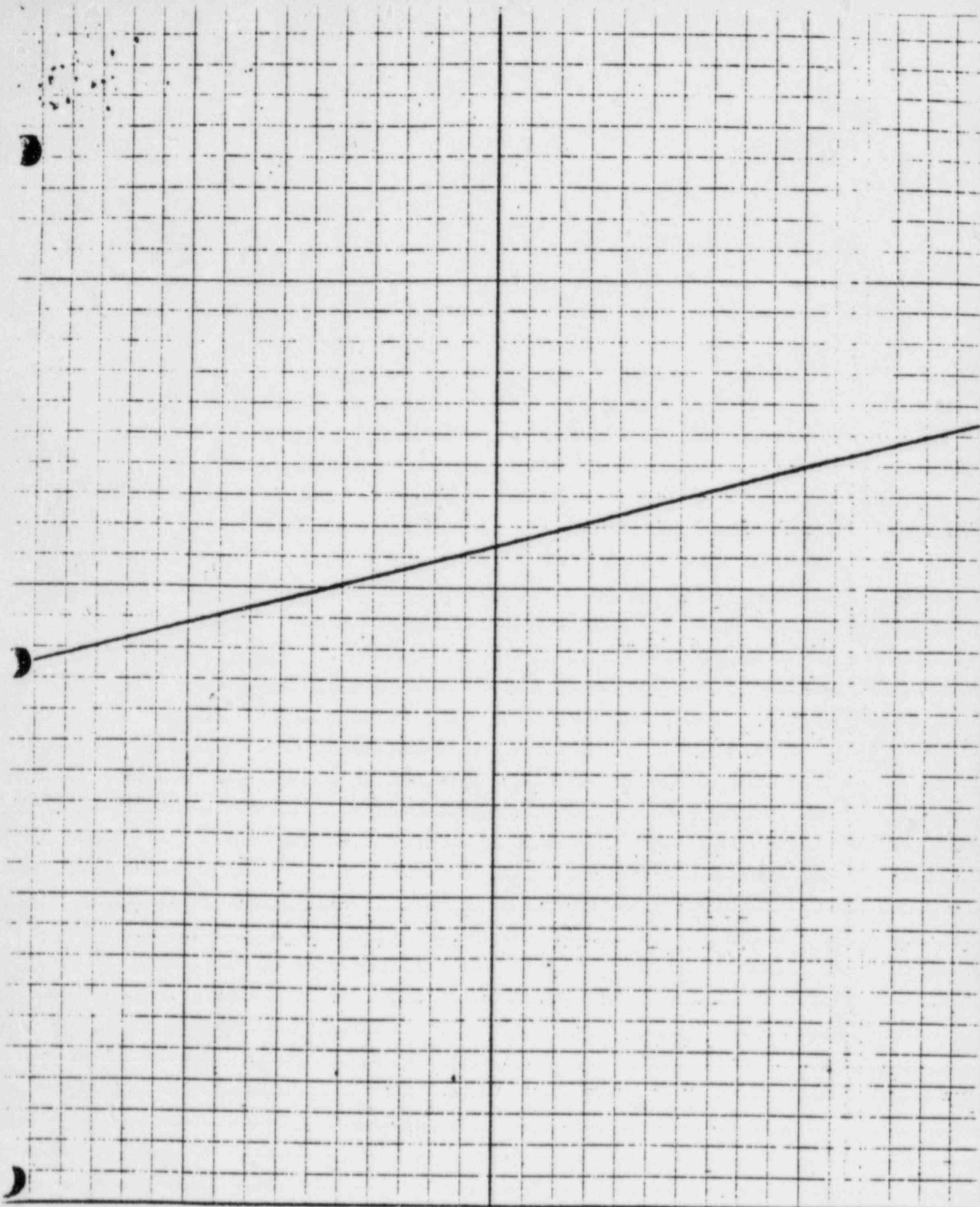
FIGURE 1 - PULL TEST FIXTURE

DESIGN PRESSURE AT 1000'



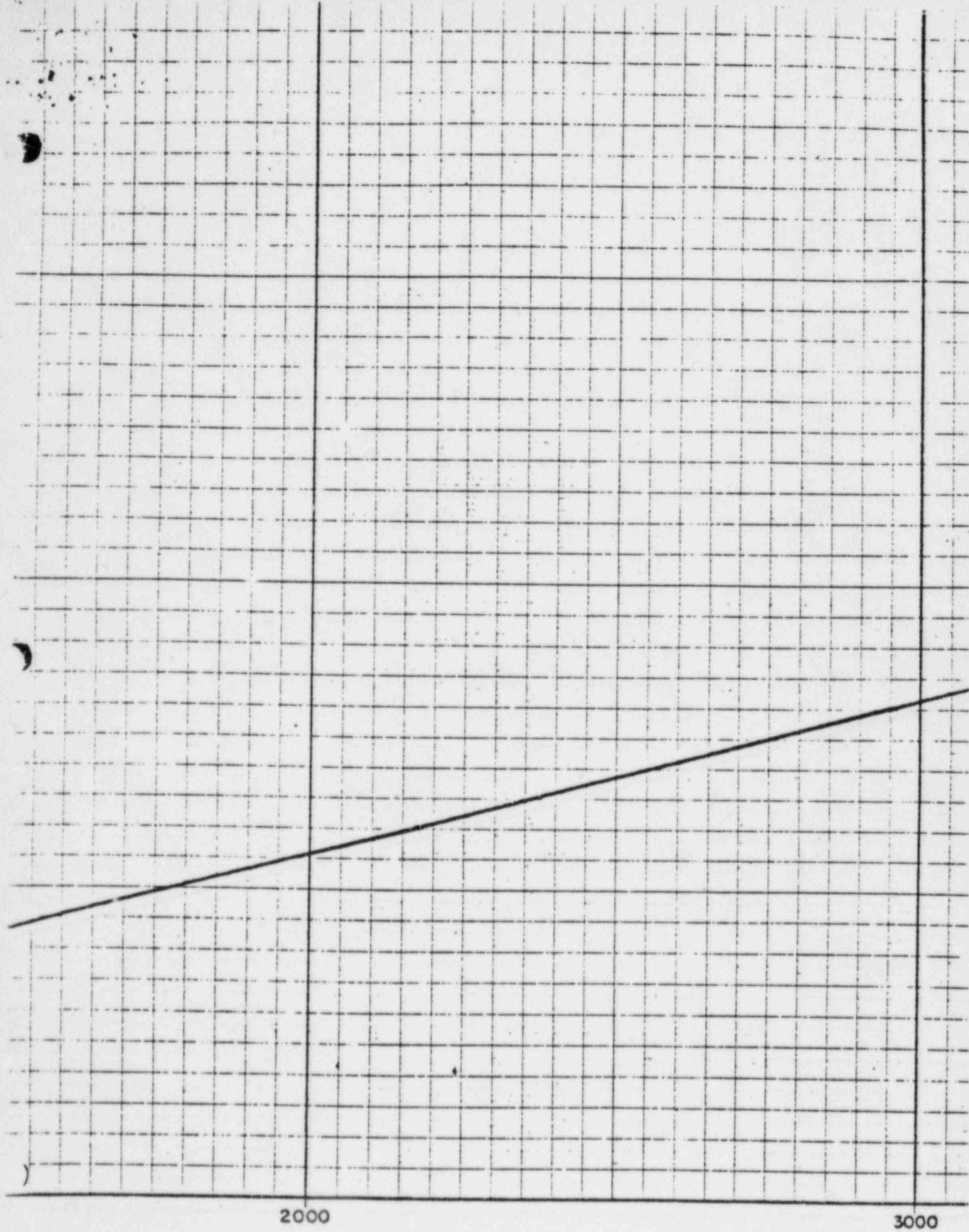






4000
APPLIED FORCE (POUNDS)

FIGURE -2 CYLINDER FORCE vs HYD. PRESSURE



DISCREPANCY REPORT

PRELIMINARY

Page of

Spec. No.

Cont./Supp.

Cont./Supp. I.D. No.

PG&E No. 288

INSPECTION SECTION

SUPERSEDED BY REV. /

Discrepant Item: Units I and II Various anchor bolts of 1/4",
3/8", 1/2" diameter purchased by H. P. Foley Company.

Explanation of Discrepancy: Anchor bolts which are too short to be
properly embedded per Dwg. 054162-2 have been on the job and may
have been installed.

Douglas Wright
Field Engr./Inspector

3-30-77
Date

CLASSIFICATION & DISPOSITION

Minor Variation ☐

Deviation ☒

Disposition:

The following members of the Material Review Board concur with the above Disposition:
(For Minor Variations, only Resident Engineer's signature required.)

L. J. Thompson
Resident Engineer

3-31-77
Date

<u> </u> Name	<u> </u> Date	<u> </u> Name	<u> </u> Date
<u> </u> Name	<u> </u> Date	<u> </u> Name	<u> </u> Date
<u> </u> Responsible Engineer	<u> </u> Date	<u> </u> Supervising Engineer	<u> </u> Date

DISPOSITION ACCOMPLISHED

Remarks:

Field Engineer/Inspector

Date

STEPS TO PREVENT RECURRENCE (Deviations Only)

Copies Attachments
Coor. Q.C. Engr. Dir. - Q.A.
Proj. Super. Resp. Engr.
Resident Engr. Proj. Engr.
Q.A. - Site Supv. Insp. Engr. (G.O.)

Resident Engineer

Date

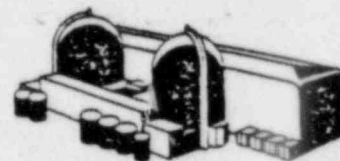
Report Completed

Coordinating QC Engineer

Date

INTEROFFICE MEMORANDUM

Diablo Canyon Project



PACIFIC GAS AND ELECTRIC COMPANY
BECHTEL POWER CORPORATION

To Mike Yan
Subject Anchor Bolt Verification
Re Letter Of
Copies To G. H. Moore wo/a
G. L. Parkinson wo/a
J. K. McCall wo/a
File wa

File No.
Date September 10, 1982
From R. D. Etzler
Of General Construction
At Diablo Canyon Site

As per your verbal request we have completed the investigation of all supports that our documents (S.I.W.S.) indicated as as having less than 2½" anchor bolt embedment.

Anchor bolt types and length were ascertained with the aid of an ultrasonic tester.

Seven (7) supports were inaccessible because of pyrocrete or equipment.

Seven (7) supports could not be located, one of which, GE/GW-140-3-6 can be assumed to be an inspector error.

Seven (7) supports are noted abandoned based on material evidence in the field.

Anchor bolts in seven (7) supports will be modified in the field to meet the criteria of Dwg. 050030.

Forty-four (44) supports have bolts with less than 2½" embedment. The enclosed "As Builts" indicate type of bolt (H = Hilti, P. R. H. = Philipps Red Head) and their respective projection from face of concrete.

The remaining supports meet existing criteria per Dwg. 050030. (73)

R. D. Etzler
R. D. Etzler
Project Superintendent

PG-E

52 3408 (1/77)

①
NO ACCESS
②
NOT FOUND

AS BUILT REMARKS
REQUIRED
NO YES



S-20	A-107-4-70		X	
S-20	104		X	
S-40	-7-95	X		
S-20	9-21		X	
S-7	9-20	X		
S-7	9-12		X	
S-20	8-47 ①	X		COVERED WITH PYROCRETE
S-41	8-5			
S-258	9-73	X		
S-102	-119-2-33		X	
S-4B	3-43		X	
S-18	C-104-3-20	X		
S-4B	D-140-5-57	X		
S-4B	-12	X		
S-20	E-123-5-8	X		} NO LONGER { ABANDONED IN EXISTENCE { ABANDONED
S-243	-10	X		
S-20	^{FE} FW-117-1-148	X		
S-20	150	X		
S-20	2-79 ②			
S-20	F-117-2-	X		SEE "WALK DOWN" NOTE
S-4B	F-140-1-66		X	
S-20	2-178		X	
S-20	2-○		X	} A COMPLETE WALK DOWN CONFIRMED ALL OF THE SUPPORT TYPES TO HAVE EMBEDMENTS (OF ANCH. OF 2 1/4" OR MORE
S-4B	2-	X		
S-20	2-	X		
S-4B	2-	X		
S-289	2-	X		
S-4B	2-	X		
S-202	5-	X		
S-243	5-35	X		

PG-E
62.3408 (5/77)

① ②
NO ACCESS
NOT FOUND

AS BUILT
REQUIRED
NO YES

REMARKS

S-19A G-117-2-	X		} SEE "WALKDOWN" NOTE ON SHEET 1 OF 6
20 -6-	X		
1B 140-1-	X		
315 1-	X		
20 4-	X		
202 4-	X		
41 4-5	X		
41 7-	X		} SEE PAGE 6 OF 6 FOR S-4B/G-140-B-1023 B S-102/ -1-  S-332/ -1- 
4B 7-243		X	
4B 7-243 ^B		X	
19A ^{GE} GW -100-2-152			
20 -115-2-101		X	
20 -115 2-118		X	
18 140-1-142	X		
18 140-1-90	X		
20 140-1-62		X	
20 140-1-3	X		
18 115-4-79	X		
41 115-4-216		X	
18 115-4-206			REPLACE
20 115-4-198		X	
20 115-4-239			COVERED WITH PYROCRETE NO DISCREPANT EMBEDMENT ENTIRE CONDUIT RUN
20 140-3-6			
242 140-4-109		X	
18 4-131			②
20 4-142	X		
20 4-143		X	
20 4-151		X	
20 4-155	X		
20 4-161		X	
20 4-152	X		
40 4-170	X		
20 4-185			

		① ACCESS NO	② NOT FOUND NO	AS BUILT REMARKS	
				REQUIRED	
				NO	YES
J-4B	GE AW-140-4-207			X	
4B	4-216			X	
288	4-300				X
288	4-550			X	
102	6-303			X	
102	6-301			X	
102	6-177			X	
98	6-1			X	
19A	7-137			X	
18	7-22			X	
18	7-23				REPLACE
19A	7-253			X	
18	H-85-2-39			X	ABANDONED
289	3-11				X
60B	100-1-111	①			
87	109	①			
87	108	①			
19A	115-1-1			X	ABANDONED
242	2-11				X
114	3-95			X	
19A	3-17			X	ABANDONED
299	128-12-6				X
19A	1-62			X	
233	1-59				X
87	1-58				X
93	1-54			X	
20	1-45			X	ALL CAPSCREWS INTO EMB. UNISTRUT
20	1-6			X	
98	1-4			X	
289	3-76				W.R. INSTALL NEW BRACE
98	5-40			X	
98	5-23			X	

		① ACCESS	② NOT FOUND	AS BUILT REQUIRED	REMARKS
		0	2	NO	YES
S-88	CSR-127-3-77				X
417	-3-327				X
181	-453				X
85	480				X
101	422				
98	4-106			X	ABANDONED
98	4-104			X	
98	4-107			X	↓
136	4-121				X
88	4-152				X
88	4-180			X	
18	5-254		①		
19A	5-251			X	
88	5-261				X
88	6-166				X
88	6-417			X	
102	7-135			X	
183	7-171			X	ALL CAP SCREWS INTO EMB. UNISTRUT
145	7-213			X	

NO ACCESS ①
NOT FOUND ②

AS BUILT REMARKS
REQUIRED
NO YES

X

X

X

X

✕

REPLACE

②

2

✱

✱

REPLACE

REPLACE

x

✱

✱

✱

①

2

ABANDONED

10

10


①

G.C. EL./D.C.P.P.
KARL ESSEL
NOV - 20 - 1982

PAGE 4

D.R. 288 "CUT BOLT"

THE FOLLOWING SUPPORTS WITH "CUT-BOLT" INDICATION ON THEIR RESPECTIVE S.I.W.S (H.P. FOLEY) ARE DEEMED ACCEPTABLE :

DETAIL ^H	SUPPORT I.D. #	BASIS FOR ACCEPTANCE	
1	S-88 A-85-9-7	NO CUT BOLTS.	O.K
	S-40 A-107-9-77	DET. REQUIRES 4 BOLTS, THIS SUPPORT HAS 8 A.B., ONE OF WHICH IS CUT.	O.K
	S-20 D-104-5-117	NO CUT BOLTS.	O.K
	S-243 G-140-1- 	NO CUT BOLTS WERE FOUND ON ANY OF THE S-243'S FOR CONDUIT KX 887 IN THIS GRID.	O.K
5	S-243 GE/W-115-1-126	THESE SUPPORTS W ABANDONED WHEN THE CONDUIT WAS REROUTED.	O.K
	S-20 -1-101		O.K
	S-20 2-91		O.K
	S-183 2-129	4 BOLTS CUT. EACH CUT BOLT IS THE INNER BOLT IN A P1331 BRACKET:  U.S. OF SLAB CUT BOLT	O.K
	S-19A H-85-4-22	ONE BOLT WAS CUT. THE NEXT SUPPORT S-19A H-85-4-23 TAKES OVER THE FUNCTION FOR H-85-4-22 WITH ALL SPAN REQUIREMENTS.	O.K
10	S-576 H-115-3-66	NO CUT BOLTS.	O.K
	S-19A H-128-2-125	NO CUT BOLTS.	O.K
	S-18 -2-112	NO CUT BOLT.	O.K
	S-243 -2-94	ONE BOLT CUT. 2'-0" TO NEXT SUPPORT. NO OVERSPANS IF S-243 WAS ELIMINATED.	O.K
	S-264 -5-44	ONE BOLT CUT, INSIDE BOLT OF P1331 BRACKET.	O.K

CONTINUED ON NEXT PAGE

G.C. EL./D.C.P.P.
KARL ISSEL
NOV - 20 - 1982

PAGE 5

D.R. 288 "CUT BOLT"

	DETAIL NO	SUPPORT I.D. NO	BASIS FOR ACCEPTANCE	
15	S-18	H-128-5-41	NO CUT BOLT.	O.K.
	S-18	-5-28	↓	O.K.
	S-18	-5-27		O.K.
	S-18	-5-25		O.K.
	S-101	CSR-127-7-80	ONE BOLT CUT. OUTSIDE BOLT IN P1331 BRACKET.	O.K.
20	S-20	K-73-6-11 (K5886)	THIS SUPPORT WAS REMOVED (SOMETIME IN THE PAST) AND REPLACED BY AN S-235.	O.K.
	S-19A	K-100-7-121	ONE BOLT CUT. THIS BOLT IS INSIDE AN S-19A WHICH IS ONLY 9" DISTANCED FROM THE NEXT S-19A. BOTH S-19AS ARE HOLDING AN CONDULET TO THE WALL. THIS CONDULET IS THE TERMINAL POINT FOR K 9156, A 3/4" R.I. THE FIRST SUPPORT, 13" AWAY FROM THE TERMINATION, IS AN S-19A.	O.K.
22	S-87	K-140-9-33	NO CUT BOLTS.	O.K.
23	S-243	K-85-1-56	NO CUT BOLTS.	O.K.

PGWE

62-3408 5/77

SHEET 6 OF 6


AS BUILT REMARKS

REQUIRED

NO YES

S-4B G-140-8-1023 B

X

S-102 G-140-1-

X

S-332 G-140-1-

W.R. ADD ONE SADDLE
NEXT TO UNDEREMB. BOLT

ALSO NOT FOUND OR INACCESSIBLE

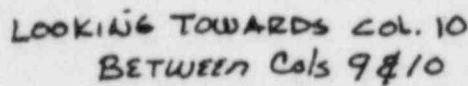
S-18 GE/GW-140-4-465

S-18

5-72

S-19A K -100-6-64 INACCESSIBLE

11.



R.V. Montzorc
G.C. STA. Elec.
DCPP 9-10-82

APPROVED BY																	
		REV.	DATE	DESCRIPTION							GM	DWN.	CHKD.	SUPV.	APVD		
GM		<p style="text-align: center;"> <i>"AS BUILT"</i> <i>G-140-1-noteq</i> <i>S-102</i> <i>MOUNTED FROM CEILING</i> PACIFIC GAS AND ELECTRIC COMPANY SAN FRANCISCO, CALIFORNIA </p>														B/M	
SUPV.																DWG. LIST	
DSGN.																SUPSDS	
DWN.																SUPSD BY	
CHKD.																SHEET NO.	SHEET:
O.K.																DRAWING NUMBER	REV.
DATE	SCALE																

PG-E

62 DASH 4/77

①
NO ACCESS
②
NOT FOUND

		AS BUILT REQUIRED		REMARKS
		NO	YES	
S-20	A-107-4-70		X	
S-20	104		X	
S-40	-7-95	X		
S-20	9-21		X	
S-7	9-20	X		
S-7	9-12		X	
S-20	8-47 ①	X		COVERED WITH PYROCRETE
S-41	8-5			
S-258	9-73	X		
S-102	-119-2-33		X	
S-4B	3-43		X	
S-1B	C-104-3-20	X		
S-4B	D-140-5-57	X		
S-4B	-12	X		
S-20	E-123-5-8	X		} NO LONGER { ABANDONED IN EXISTENCE { ABANDONED
S-243	-10	X		
S-20	FE FW -117-1-148	X		
S-20	150	X		
S-20	2-79 ②			
S-20	F-117-2-	X		SEE "WALK DOWN" NOTE
S-4B	F-140-1-66		X	
S-20	2-178		X	
S-20	2-○		X	
S-4B	2-	X		} A COMPLETE WALKDOWN CONFIRMED ALL OF THESE SUPPORT TYPES TO HAVE EMBEDMENTS (OF ANCH. B OF 2 1/4" OR MORE
S-20	2-	X		
S-4B	2-	X		
S-289	2-	X		
S-4B	2-	X		
S-202	5-	X		
S-243	5-35	X		

PG-E
6/2/80 1/77

① ②

① ACCESS
② NOT FOUNDAS BUILT
REQUIRED
NO YES

REMARKS

S-19A G-117-2-

20 -6-

1B 140-1-

315 1-

20 4-

202 4-

41 4-5

41 7-

4B 7-243

4B 7-243^B

19AGE - 100-2-152

20 -115-2-101

20 -115 2-118

18 140-1-142

18 140-1-90

20 140-1-62

20 140-1-3

18 115-4-79

41 115-4-216

18 115-4-206

20 115-4-198

20 115-4-239

20 140-3-6

242 140-4-109

18 4-131

20 4-142

20 4-143

20 4-151

20 4-155

20 4-161

20 4-152

40 4-170

SEE "WALK DOWN" NOTE
ON SHEET 1 OF 6SEE PAGE 6 OF 6 FOR
S-4B/G-140-B-1023 B

S-102/ -1-

S-332/ -1-

REPLACE

COVERED WITH
PYROCRETE
NO DISCREPANT EMBEDMEN
ENTIRE CONDUIT RUN

PG-E

62-3408 8/77

①
NO ACCESS
②
NOT FOUND

AS BUILT
REQUIRED
NO YES

REMARKS

J-4B	GE				
4B	GW	140-4-207	X		
288		4-216	X		
288		4-300		X	
288		4-550	X		
102		6-303	X		
102		6-301	X		
102		6-177	X		
98		6-1	X		
19A		7-137	X		
18		7-22	X		
18		7-23	—		REPLACE
19A		7-253	X		
18	H-85-2-	39	X		ABANDONED
289		3-11		X	
60B		100-1-111	①		
87		109	①		
87		108	①		
19A		115-1-1	X		ABANDONED
242		2-11		X	
114		3-95	X		
19A		3-17	X		ABANDONED
299		128-12-6		X	
19A		1-62	X		
233		1-59		X	
87		1-58		X	
93		1-54	X		
20		1-45	X		ALL CAPSCREWS INTO EMB. UNISTRUT
20		1-6	X		
98		1-4	X		
289		3-76	—		W.R. INSTALL NEW BRACE E-1202
98		5-40	X		
98		5-23	X		

①
ACCESS
②
NOT FOUND

AS BUILT REMARKS
REQUIRED
NO YES

5-88 CSR-127-3-77

417 -3-327

181 -453

85 480

101 422

98 4-106

98 4-104

98 4-107

136 4-121

88 4-152

88 4-180

18 5-254 ①

19A 5-251

88 5-261

88 6-166

88 6-417

102 7-135

183 7-171

145 7-213

ABANDONED



ALL CAP SCREWS
INTO EMB. UNISTRUT

①
ACCESS
②
NOT FOUND

AS BUILT REMARKS
REQUIRED
NO YES

S-477 J-115- 3-49

X

20 5-7

X

383 10-63

X

64 10-43

X

477 1-59

X

18 J-140-4-50

REPLACE

20 3-11

20 3-10

18 K-73-1-162 ②

18 1-161 ②

18 K-85-2-96

X

18 2-95

X

18 2-69

REPLACE

18 2-68

REPLACE

202 2-25

X

85 4-24

X

19A K-100-3-40

X

116 6-34

X

18 7-176 ①

215 7-29

X

ABANDONED

243 11-40

X

18 K-115-4-69

X

202 1-21

X

18 K-140-9-2

X

87 9-37

X

19A K-154-1-218

X

19A 1-19 ①

20 L-140-7-123

X

20 2-3

X

40 G-17.5-4-7

X


AS BUILT REMARKS

REQUIRED

NO YES

S-4B G-140-8-1023 B

X

S-102 G-140-1-

X

S-332 G-140-1-

W.R. ADD ONE SADDLE
NEXT TO UNDEREMB. BOLT

ALSO NOT FOUND OR INACCESSIBLE

S-18 GE/GW-140-4-465

S-18

S-72

S-19A K -100-6-64 INACCESSIBLE

—A2

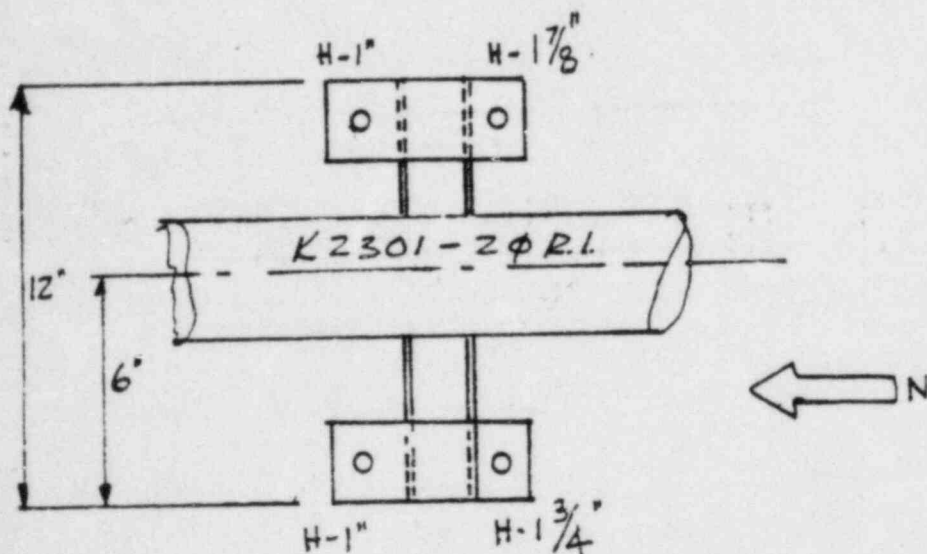
60" South

K6266-1 ϕ R.I. (Yt) 56" North

R.V. Monterole
G.C. STA. ELEC
DCPP
9-3-82

[illegible]

NOTE: ALL BOLTS $\frac{1}{2}$ " ϕ x $3\frac{3}{4}$ " H/t/t/s



SPANS

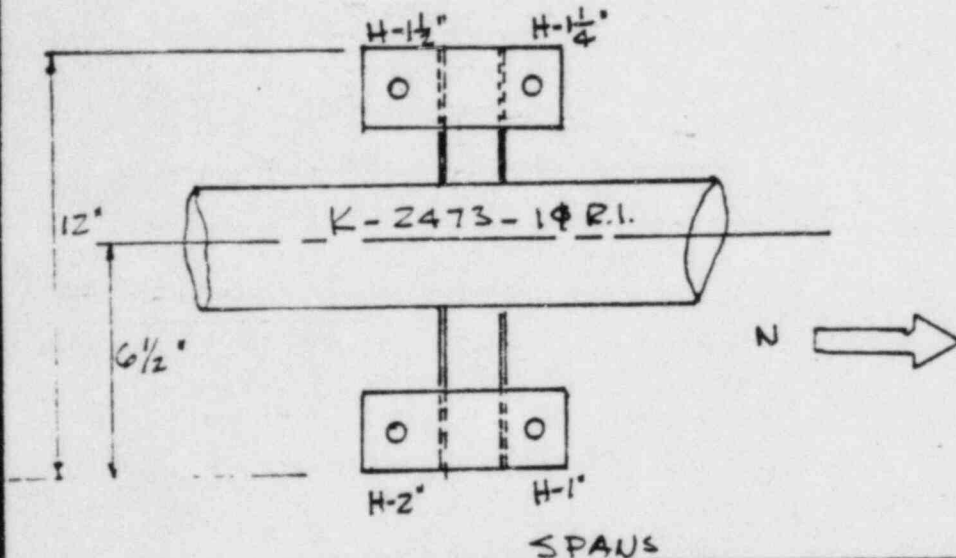
53" North to S-20

K-2301-2 ϕ -R.I. 65" south To S-20

RV. Monterole
GC. STA. Elec
DCPP 9-7-82

APPROVED BY																						
		REV.	DATE	DESCRIPTION								GM	DWN.	CHKD.	SUPV.	APVD.						
GM		<p align="center"> <i>"AS BOLT"</i> A-107-4-70 S-20 <i>WALL Mounted</i> PACIFIC GAS AND ELECTRIC COMPANY SAN FRANCISCO, CALIFORNIA </p>																	B/M			
SUPV.																			DWG. LIST			
DSGN.																			SUPSDS			
DWN.																			SUPSD BY			
CHKD.																			SHEET NO.		SHEETS	
O.K.																			DRAWING NUMBER		REV.	
DATE		SCALE																				

NOTE: ALL BOLTS $\frac{1}{2} \phi \times 3 \frac{3}{4}''$ H/H/H



44" NORTH TO S-20 K-2473-1 ϕ R.I. - 42" SOUTH TO S-20

R.V. Monterok
G.C. STA. Elec
DCPP 9-7-82

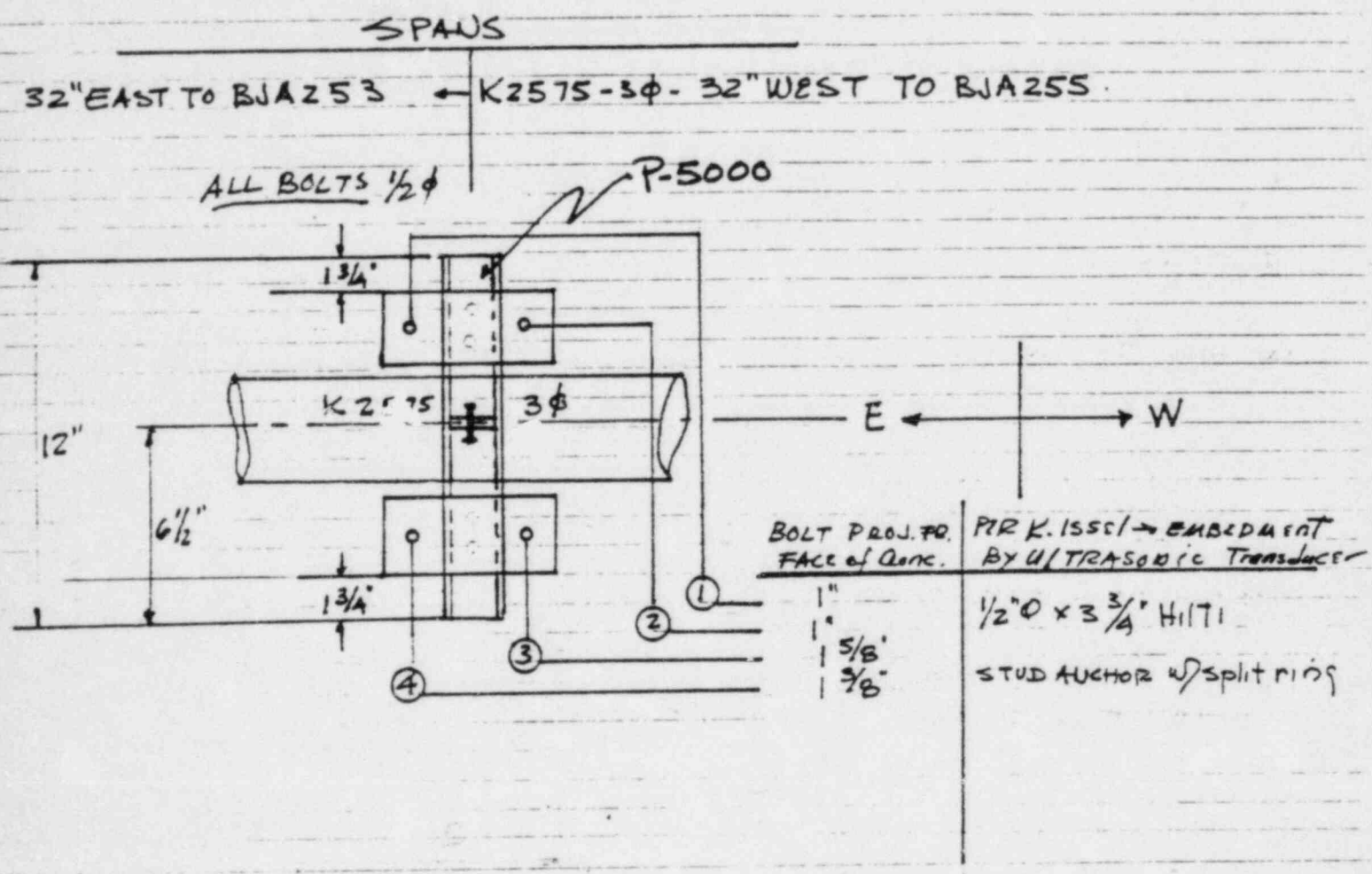
APPROVED BY																	
		REV.	DATE	DESCRIPTION								GM	DWN.	CHKD.	SUPV.	APVD.	
GM		<p style="text-align: center;"> <i>"As BUILT"</i> <i>A-107-4-104</i> <i>3-20</i> <i>WALL MOUNTED</i> PACIFIC GAS AND ELECTRIC COMPANY SAN FRANCISCO, CALIFORNIA </p>													B/M		
SUPV.															DWG. LIST		
DSGN.															SUPSDS		
DWN.															SUPSD BY		
CHKD.															SHEET NO.		SHEETS
O.K.															DRAWING NUMBER		REV.
DATE	SCALE																

ORIGINAL

"AS BUILT" Support No. A-107-9-21

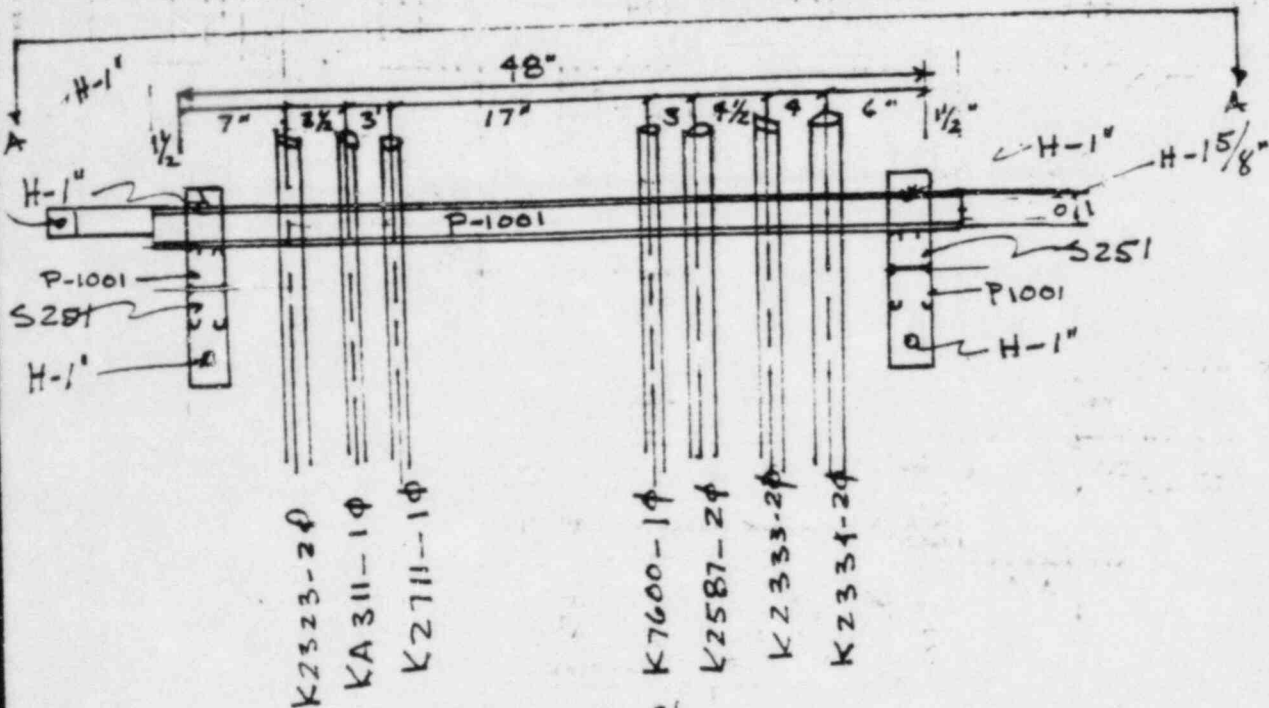
DETAIL No. S-20

WALL Mounted



R.V. Montecarlo
G.C. STA. Elec.
9-1-82

NOTE: ALL BOLTS $\frac{1}{2}\phi \times 3 \times \frac{3}{4}$ HHT's



Looking South.



Sec. A-A

SPANS

DOWN 12" TO PANEL

{	K2334-2φ	} UP 70" TO S-7
	K2333-2φ	
	K2587-2φ	
	K2711-1φ	UP 56" TO S-20
	K-7600-1φ	UP 48" TO S243
{	K-2323-2φ	} UP 54" TO S-7
	KA311-1φ	

R.V. Monterak
G.C. STA. Elec
DCPP
9-7-82

APPROVED BY

REV. DATE

DESCRIPTION

GM DWN. CHKD. SUPV. APVD.

GM

SUPV.

DSGN.

DWN.

CHKD.

O.K.

DATE

SCALE

"AS BUILT"

A-107-9-12

S-7

WALL MOUNTED

PACIFIC GAS AND ELECTRIC COMPANY
SAN FRANCISCO, CALIFORNIA

B/M

DWG. LIST

SUPSDS

SUPSD BY

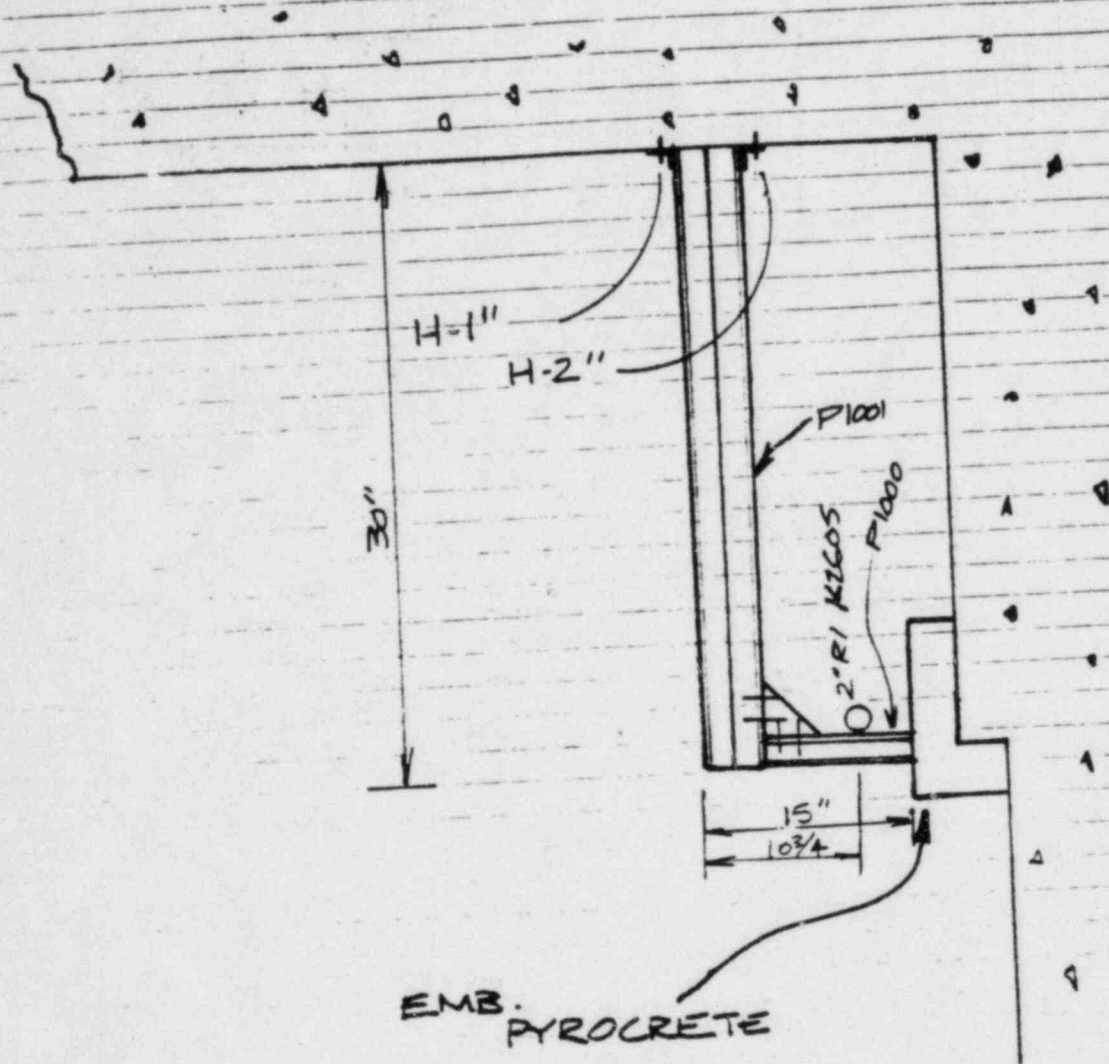
SHEET NO.

DRAWING NUMBER REV.

SHEETS

DATE: 9.8.82

S-102 A-119-2-33

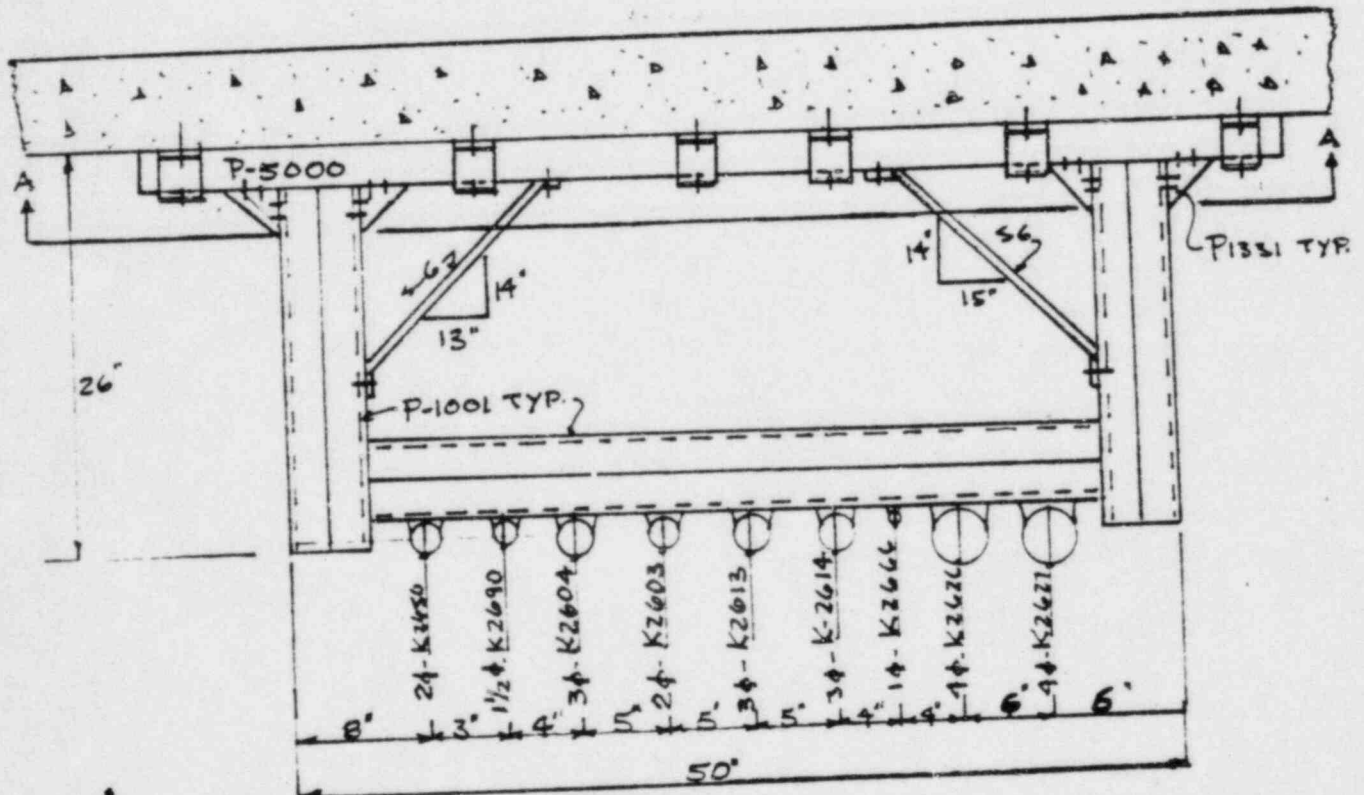
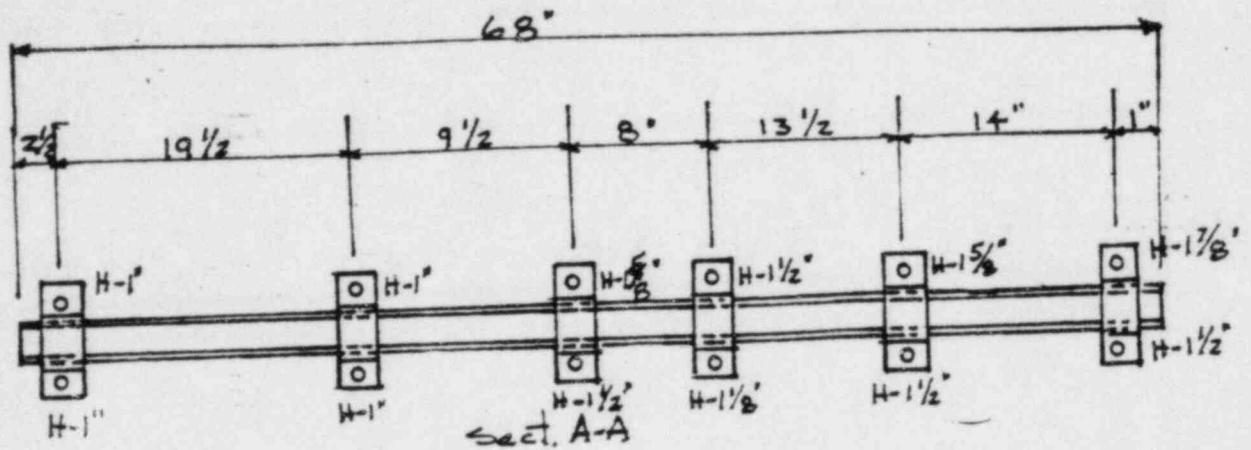


Spans

BY M. CAMPBELL

SOUTH — Wall — 45"
NORTH — PYROCRETE — 30"

NOTE: ALL BOLTS $\frac{1}{2}\phi$



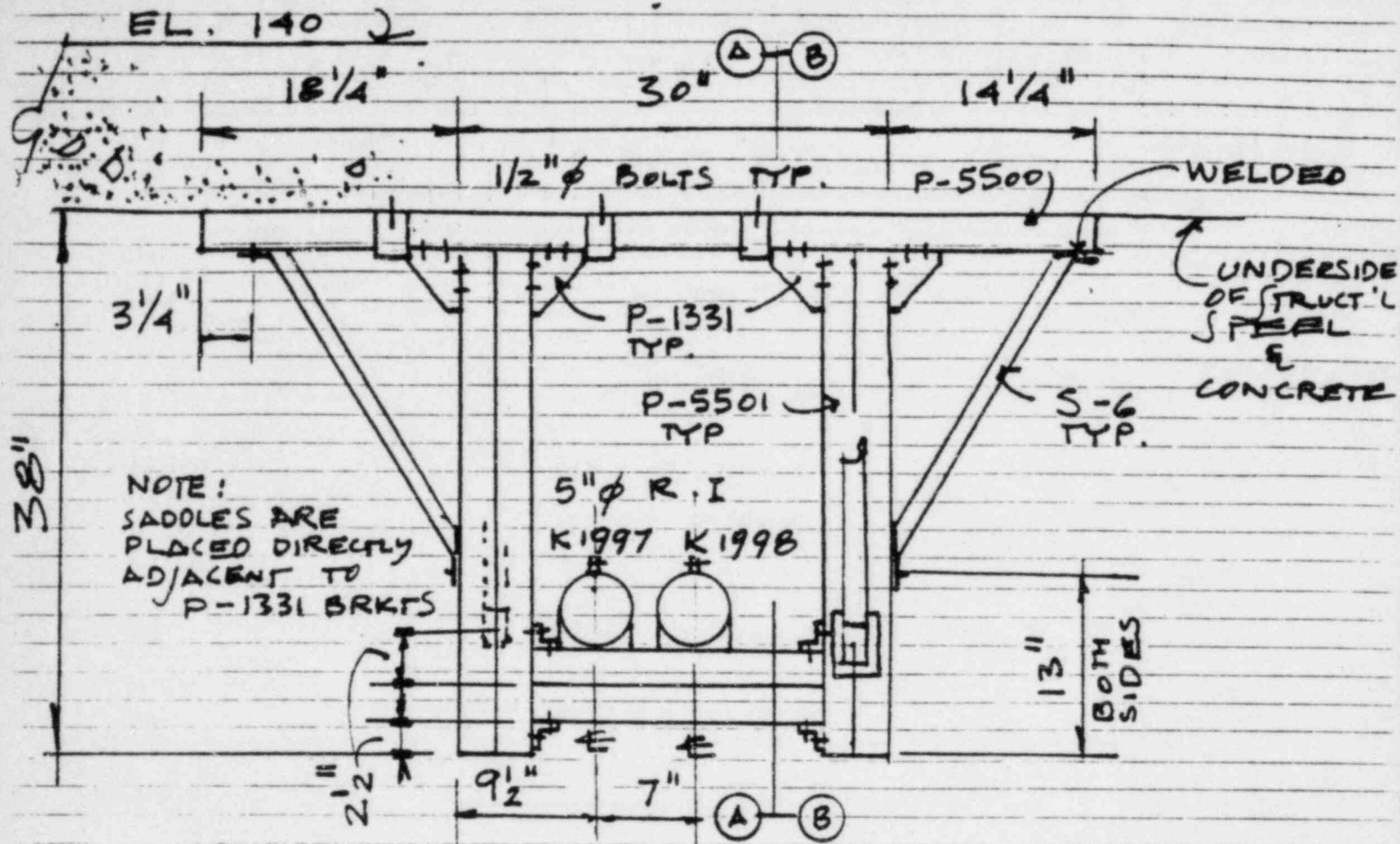
SPANS

45" EAST TO WALL	K-2650-2φ-	96" WEST TO S4B	20' Monterey 60' STA ELEC. DCPP 9-8-82
	K-2604-3φ-		
	K-2605-2φ-		
	K-2613-3φ-		
	K-2614-3φ-		
	K-2626-4φ-		
	K-2626-1φ-		
	K-2627-4φ-		
K-2690-1 1/2φ-95' WEST TO S1B			
APPROVED BY		GM	DWN. CHKD. SUPV. AP
REV.	DATE	DESCRIPTION	

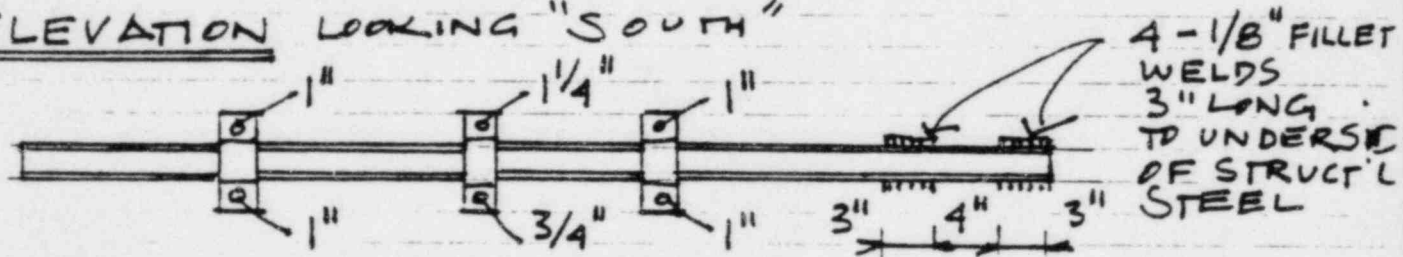
GM	
SUPV.	
DSGN.	
DWN.	
CHKD.	
O.K.	
DATE	SCALE

"AS BUILT"
A-119-3-43
Mounted at ceiling
PACIFIC GAS AND ELECTRIC COMPANY
SAN FRANCISCO, CALIFORNIA

B/M	
DWG. LIST	
SUPSDS	
SUPSD BY	
SHEET NO.	SHEET
DRAWING NUMBER	RE



ELEVATION LOOKING "SOUTH"



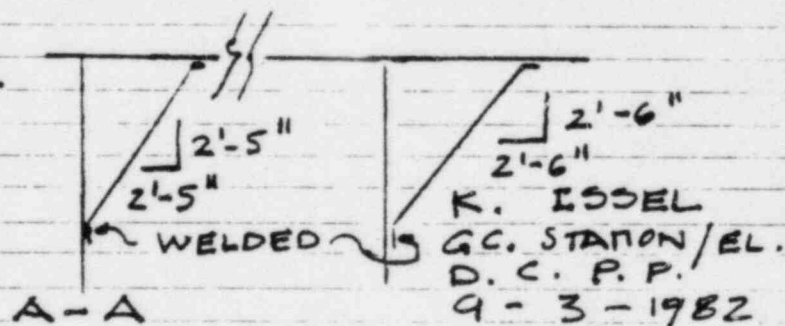
REFLECTED PLAN OF P-5500 WITH BOLT PROJECTIONS MEASURED FROM FACE OF CONCRETE.

NOTE : ALL A. BOLTS ARE 1/2" φ x 3 3/4" HILTI'S

SPANS :

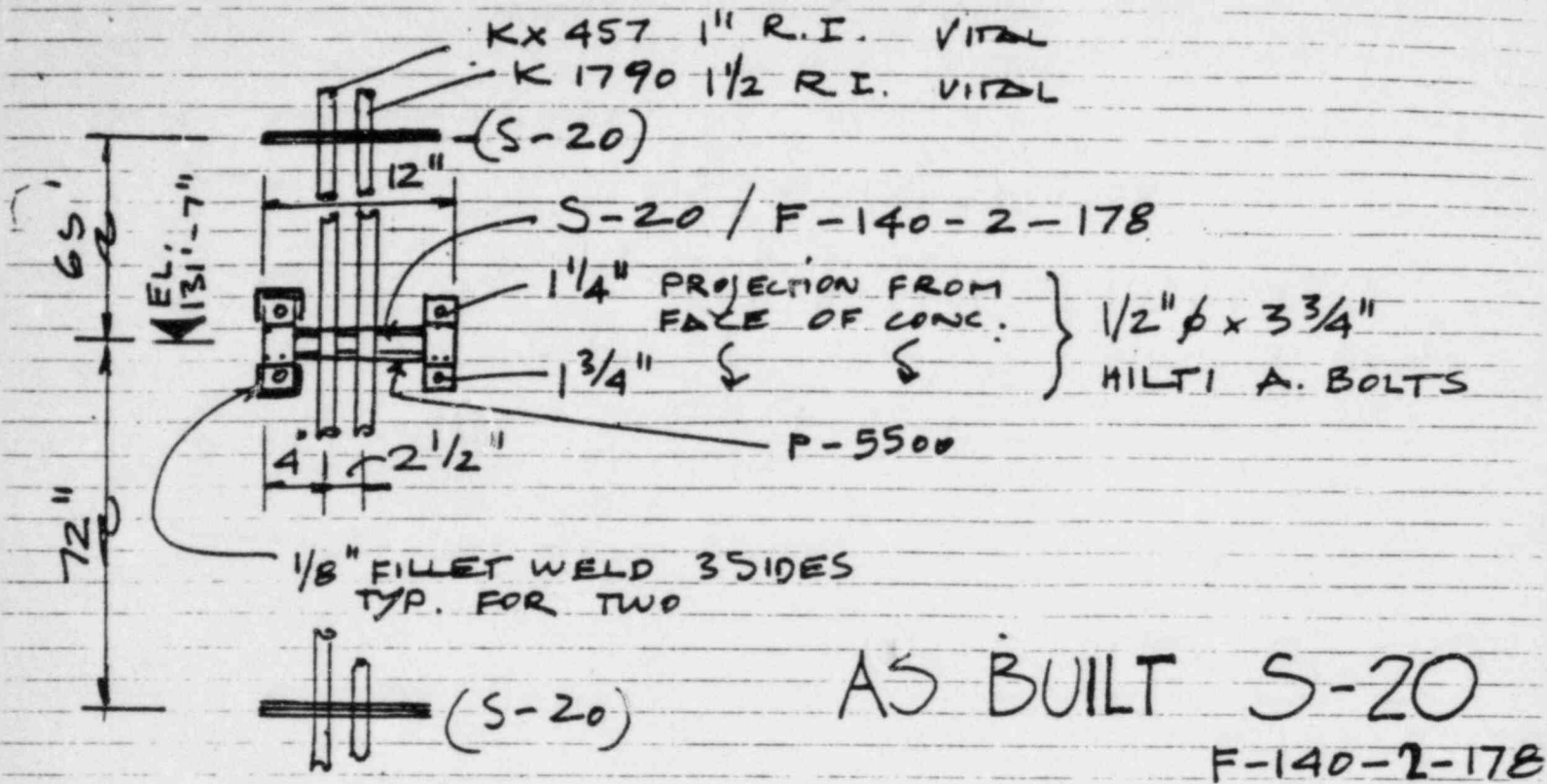
74" "SOUTH"
TO S-4B
F-140-1-65

66" "NORTH"
TO S-4B
F-140-1-66

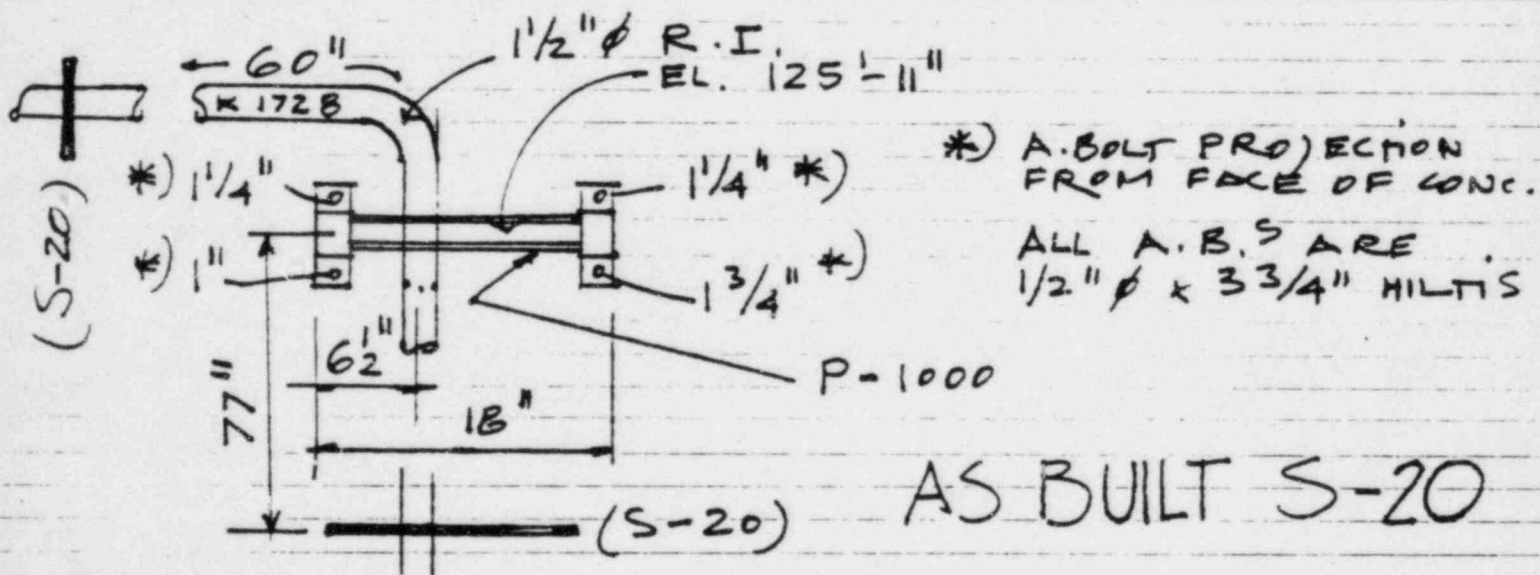


S-4B

AS BUILT F-140-1-66



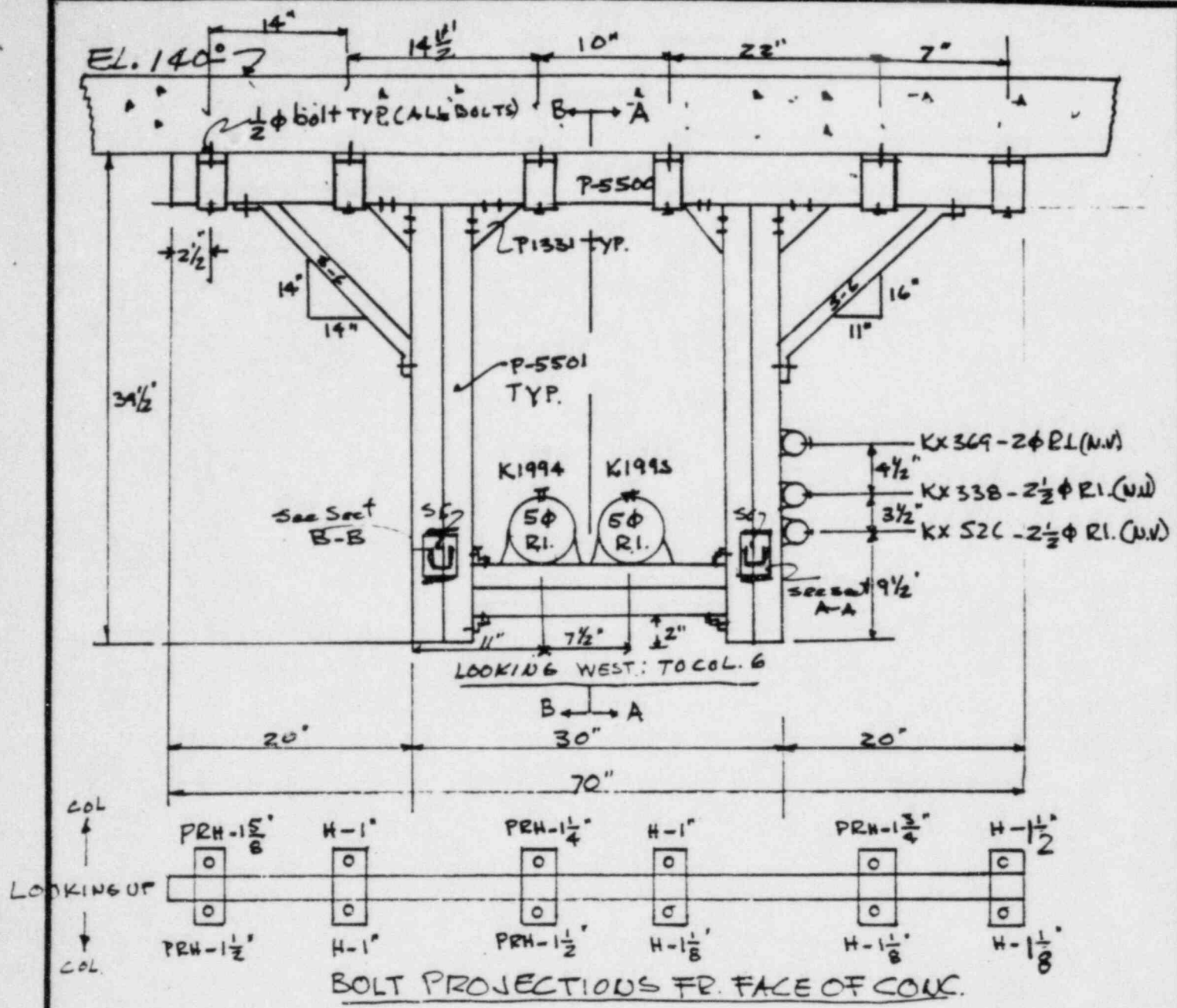
ELEVATION OF S-20 ATTACHED TO CRANE WALL



ELEVATION OF S-20 ATTACHED TO CRANE WALL

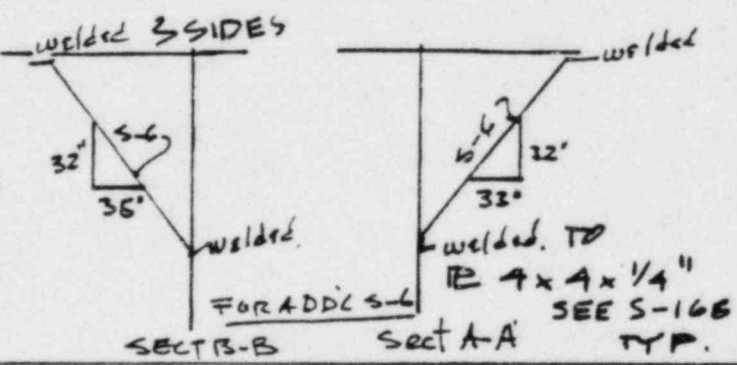
K. ISSEL
G.C. STATION / EL
D.C. P. P.
9-3-1982

ORIGINAL

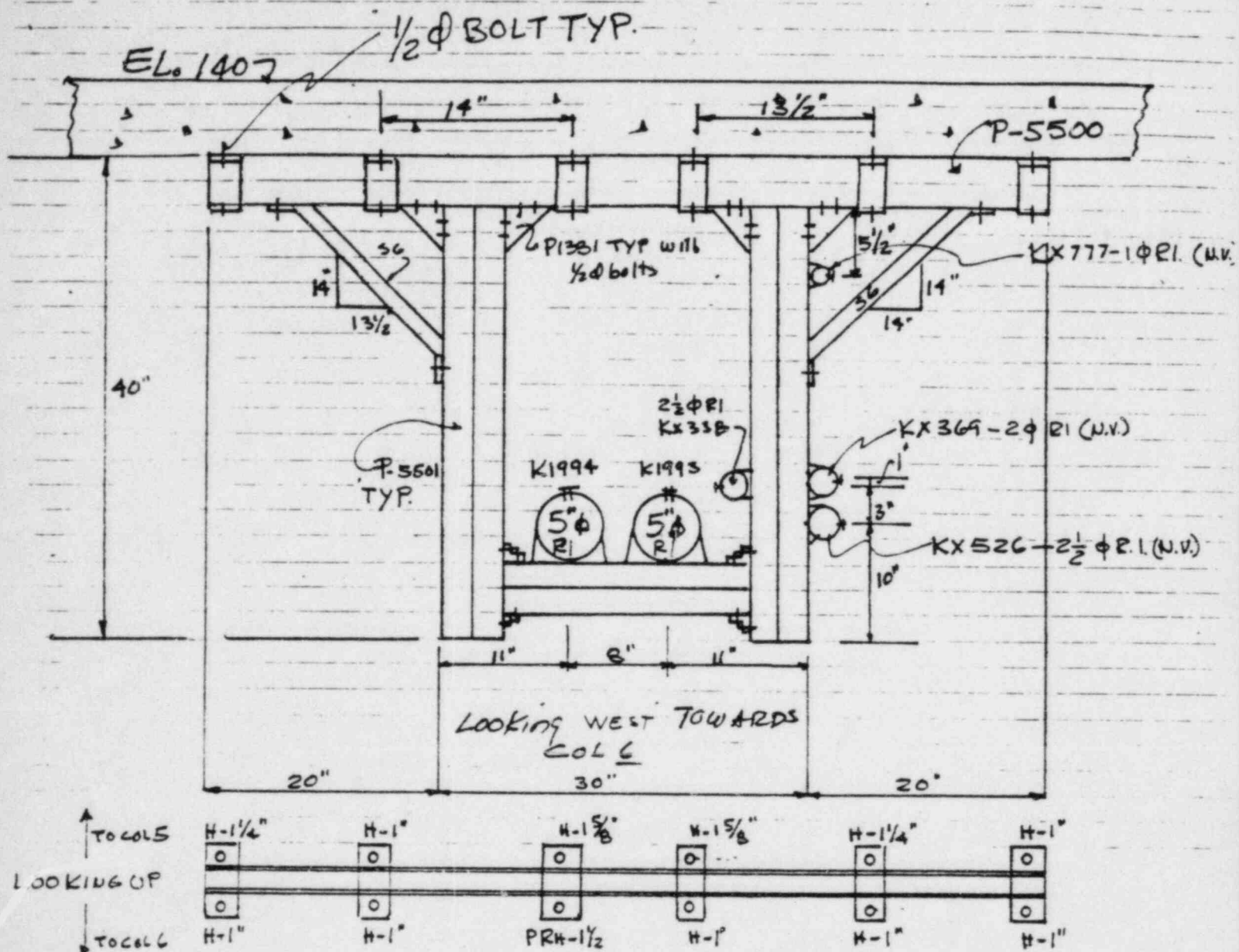


SPANS

36" TO S-39 NOTAG	{	K1994-5φ-R1	{	96" TO
		K1993-5φ-R1		S4B
109" TO S4B NOTAG		KX 526-2 1/2 φ R1.		(South)
		KX 338-2 1/2 φ R1.		
		KX 369-2 φ R1.		

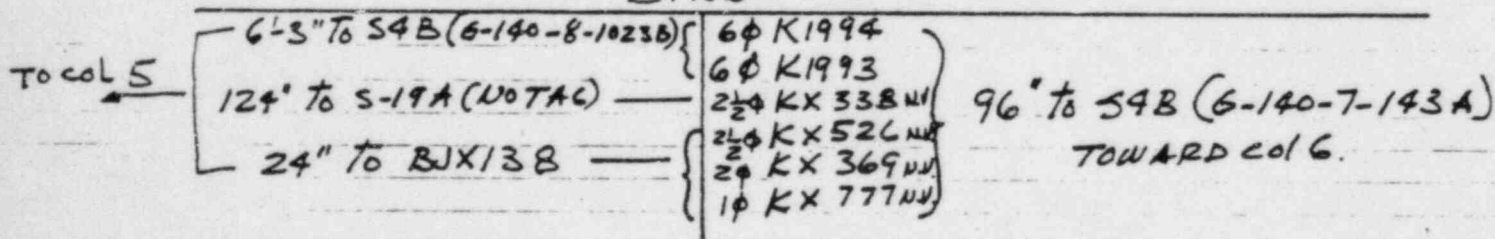


APPROVED BY															
REV.		DATE		DESCRIPTION		9-2-B2		GM		DWN.		CHKD.		SUPV. APVD.	
GM				"AS BUILT" G-140-7-243 S-4B						B/M					
SUPV.										DWG. LIST					
DSGN.										SUPSDS					
DWN.										SUPSD BY					
CHKD.										SHEET NO.		SHEETS			
O.K.										DRAWING NUMBER		REV.			
DATE		SCALE													
PACIFIC GAS AND ELECTRIC COMPANY SAN FRANCISCO, CALIFORNIA															



PROJECTIONS OF BOLTS FR. FACE OF CONC.

SPANS



"AS BUILT" G-140-7-243B

S-4B

R.V. Montemarle
G.C. STA. DCP
9-2-82

NOTES:

ALL BOLTS $\frac{1}{2}\phi$

CAP
SCREWS

insert

KT 302-1 ϕ N.V.

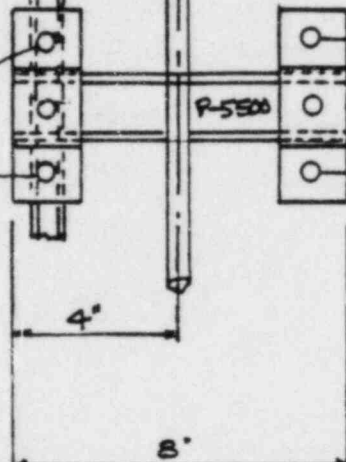
BOLT PROJ.
FR FACE CONX

EMBEDMENT PER
ULTRASONIC TRANS.

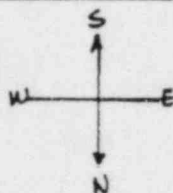
$\frac{1}{2}\phi \times 3\frac{3}{4}$

Hilti's

H-1 $\frac{5}{8}$ "
H-2"



LOOKING UP



SPANS

78" EAST TO S-20

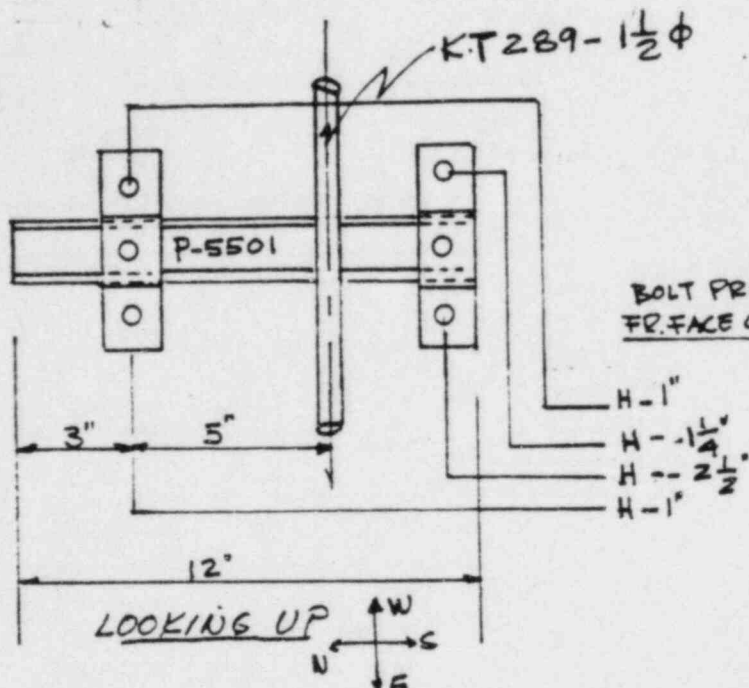
KT 302-1 ϕ - 51" NORTH TO S-20

R.V. Montecarlo
O.C. STA. Elec. DCPD
9-3-82

APPROVED BY											
REV.	DATE	DESCRIPTION				GM	DWN.	CHKD.	SUPV.	APVD.	
GM		<p>"AS BUILT"</p> <p>GE/GW-115-2-101</p> <p>S-20</p> <p>MOUNTED IN CEILING</p> <p>PACIFIC GAS AND ELECTRIC COMPANY</p> <p>SAN FRANCISCO, CALIFORNIA</p>						B/M			
SUPV.								DWG. LIST			
DSGN.								SUPSDS			
DWN.								SUPSD BY			
CHKD.								SHEET NO.			SHEETS
O.K.		DRAWING NUMBER			REV.						
DATE	SCALE										

"天竺" 天竺

ALL BOLTS
1/2" TYP



EMBEDMENT PER
ULTRASONIC TRAUS.

 $\frac{1}{2}'' \phi \times 3\frac{3}{4}''$

$\text{H} - \text{I}^-$
 $\text{H} - \text{I}^- \cdot \text{N}^{\text{H}} - \text{I}^-$
 $\text{H} - \text{I}^- \cdot \text{N}^{\text{H}} - \text{I}^-$

SPAN

78" EAST TO S20-KT289- $1\frac{1}{2}\phi$ - 78" WEST TO S19A

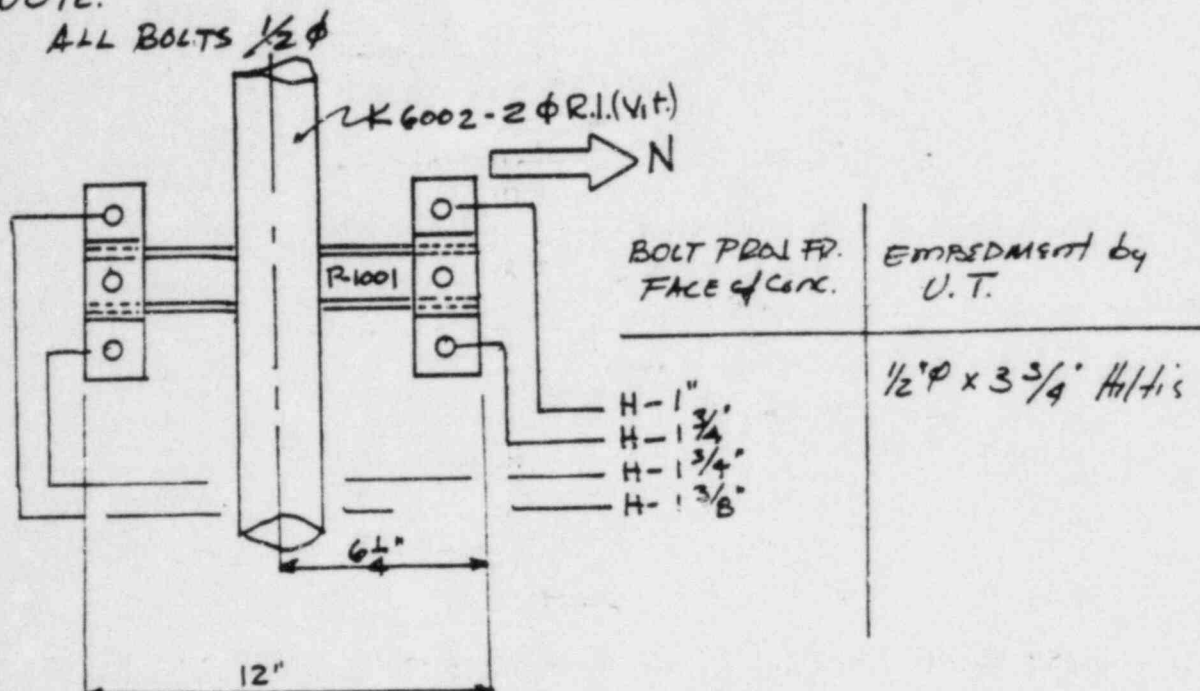
R.V. Montero/c

G.C. STA ELEC.	DCPP
9-B-B2	

[illegible]

GM	<p><i>GE/GW-115-2-118</i></p> <p><i>S 20</i></p> <p><i>MTD in ceiling</i></p> <p>PACIFIC GAS AND ELECTRIC COMPANY</p> <p>SAN FRANCISCO, CALIFORNIA</p>	B/M
SUPV.		DWG. LIST
DSGN.		SUPSDS
DWN.		SUPSD BY
CHKD.		SHEET NO. SHEETS
O.K.		DRAWING NUMBER REV.
DATE	SCALE	

ALL BOLTS $\frac{1}{2} \phi$



SPAN

South 46" to S-20	K 600Z-2Φ R.I. NORTH 29" to S-20
-------------------	----------------------------------

R.V. Montano
G.C. STA. ELEC

APPROVED BY

GM	
SUPV.	
DSGN.	
DWN.	
CHKD.	
O.K.	
DATE	SCALE

REV.	DATE
------	------

DESCRIPTION

GM

DWN.	CHKD.	SUPV.	APVD.
------	-------	-------	-------

B/M

DWG. LIST

SUPSDS

SUPSD BY

SHEET NO.

SHEETS

SHEET NO.	SHEETS
DRAWING NUMBER	REV.

"AS BUILT"

GE/GW-140-1-62, DET. 520
WALL MOUNTED

PACIFIC GAS AND ELECTRIC COMPANY
SAN FRANCISCO, CALIFORNIA

RP

9-3-

7	5	7

GM

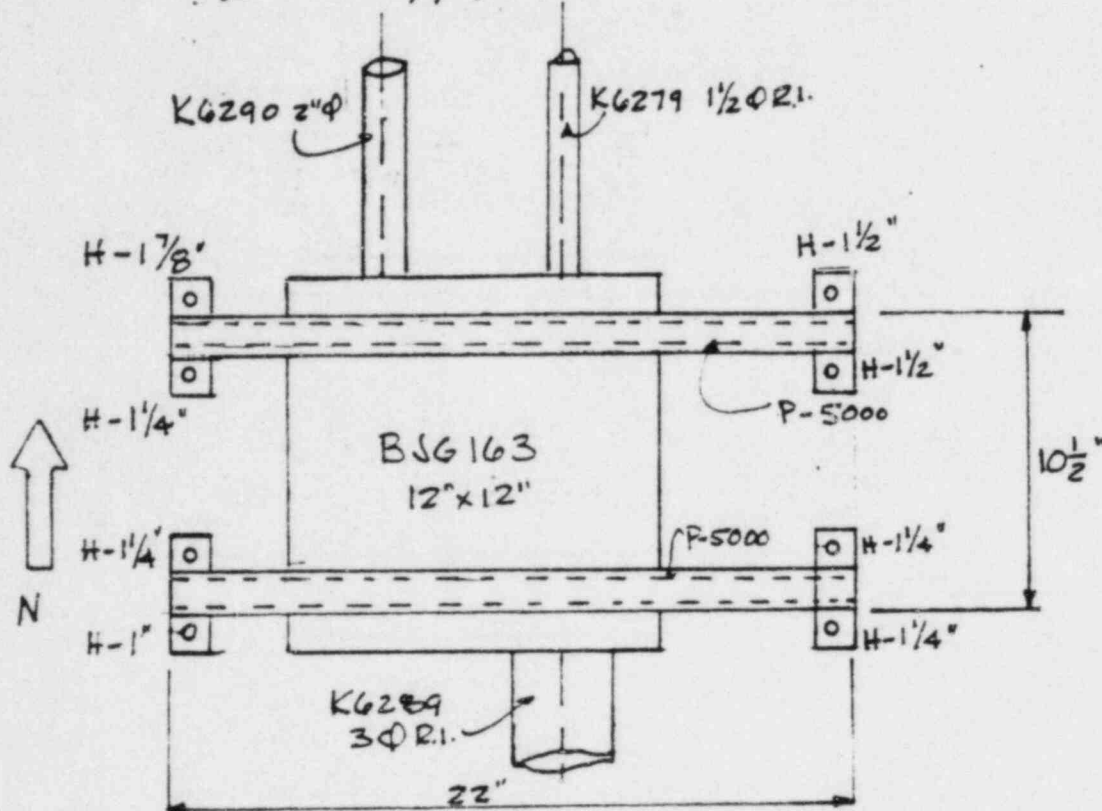
DWN

CHKD.

SUPV

APVD.

Notes: ALL bolts $\frac{1}{2}" \phi \times 3 \frac{3}{4}"$ H/H's



LOOKING DOWN FROM Bottom of 140° S Lab.

SPANS

FROM BOX
BSG 163

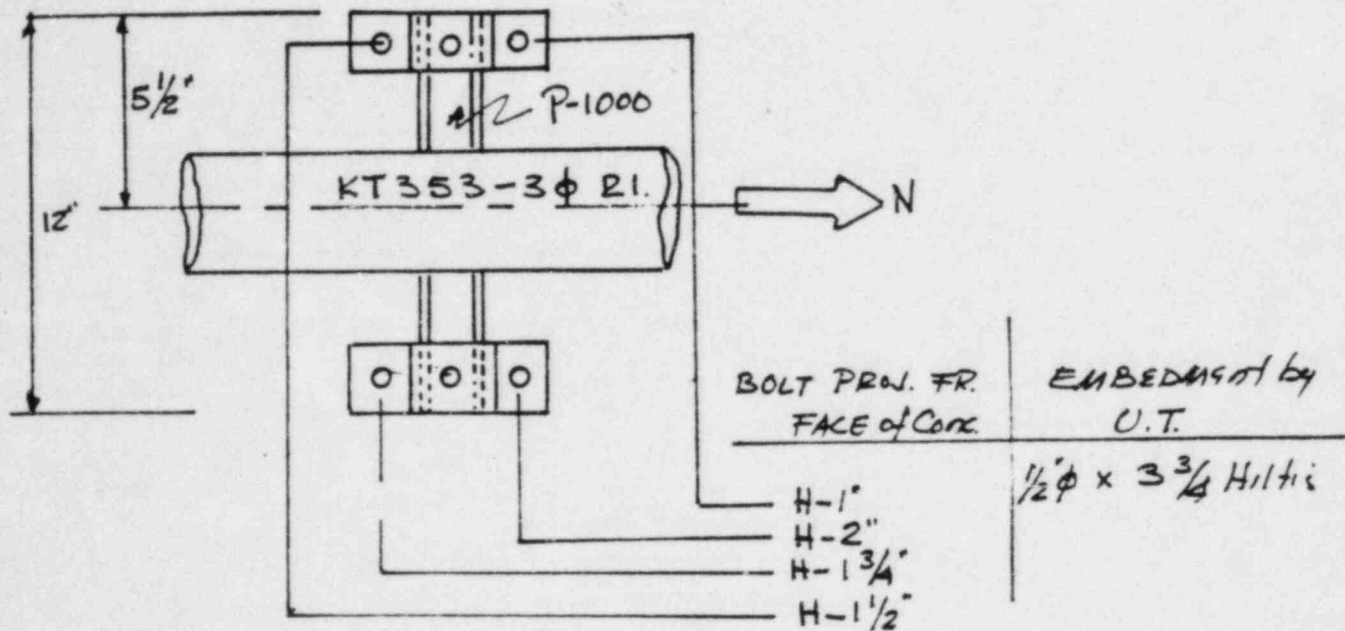
$\left. \begin{array}{l} K6279 - 1 \frac{1}{2} \phi R.I. \\ K6290 - 2 \phi R.I. \end{array} \right\} 24" \text{ NORTH TO S-20}$
 $K6289 - 3 \phi R.I. \rightarrow 12" \text{ TO S-20 SOUTH}$

R.V. Monterole
G.C. STA. Elec
DCPP
9-7-82

APPROVED BY											
REV		DATE		DESCRIPTION		GM		DWN.		CHKD. SUPV. APVD.	
GM		SUPV.		DSGN.		DWN.		CHKD.		O.K.	
DATE		SCALE		<p>"AS BUILT"</p> <p>GE/GW-115-4-216</p> <p>S-41</p> <p>Mounted on ceiling</p> <p>PACIFIC GAS AND ELECTRIC COMPANY</p> <p>SAN FRANCISCO, CALIFORNIA</p>		B/M		DWG. LIST		SUPSDS	
								SHEET NO.		SHEETS	
								DRAWING NUMBER		REV.	

MICROFILM

NOTE: ALL BOLTS $\frac{1}{2}$ ϕ



SPAN

16" South To S-19A — KT353-3φ R.I. — 48" NORTH TO S-20

R.V. Montero/c
G.C. STA. ELEC
DCPP 9-3-82

APPROVED BY											

Technical drawing of a 4-cylinder engine block. The block is shown in a side view with four cylinders. The dimensions and part numbers are as follows:

- Dimensions:**
 - Overall length: 27"
 - Distance between cylinder centers: 6 1/2", 4 1/2", 5", 5", 6"
 - Block height (left): H - 1 1/2"
 - Block height (right): H - 1 3/4"
 - Block height (bottom right): H - 1 1/4"
- Part Numbers:**
 - Cylinder 1 (left): K6233 - 3φ R.I.
 - Cylinder 2: K6232 - 3φ R.I.
 - Cylinder 3: K6495 - 3φ R.I.
 - Cylinder 4 (right): KT305 - 3φ R.I.
- Other Labels:**
 - Left side: P-5501
 - Right side: H - 1 3/4"
 - Bottom right: H - 1 1/4"

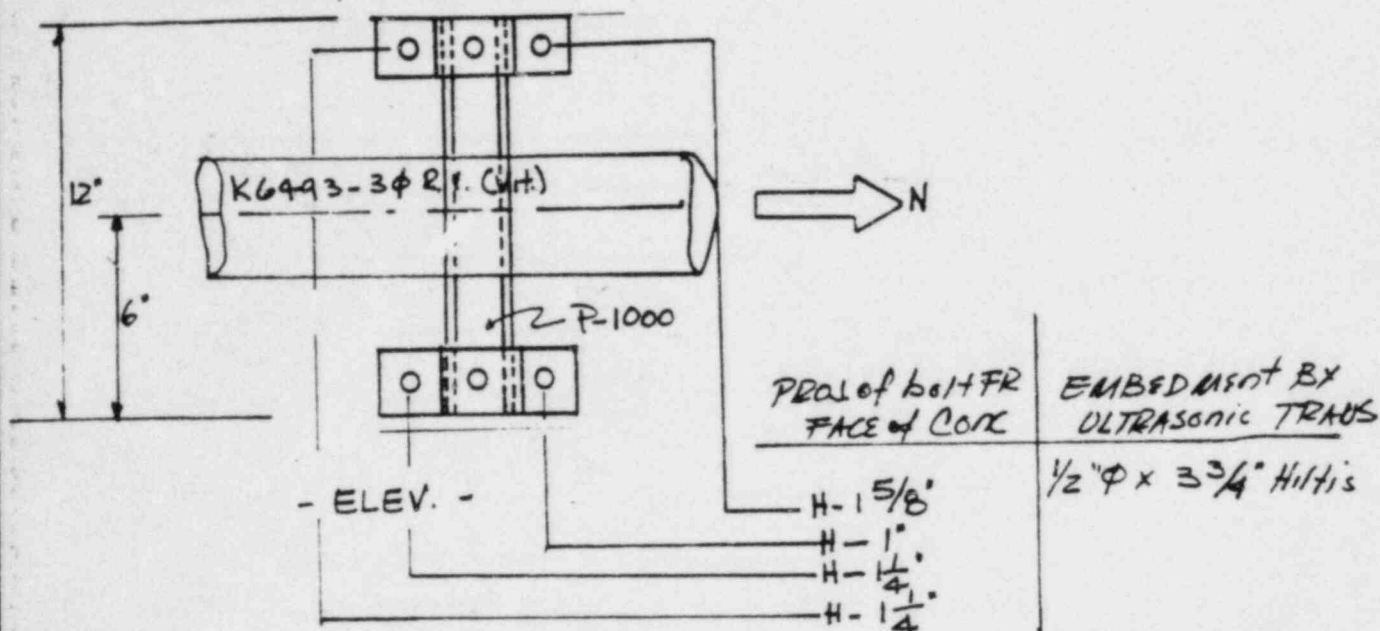
SPANS

48" DN TO S-20	{	KT 305 - 3φ R.I.	}	48" UP TO S-20
		KG 495 - 3φ R.I.		
		KG 232 - 3φ R.I.		
		KG 233 - 3φ R.I.		

R.V. Montenegro
6C STA. ELEC
DCPP

[illegible]

NOTE: ALL BOLTS $\frac{1}{2} \phi$



SPANS

30' SOUTH TO BJG 207 - K6493-3Φ-R.1 - 48' NORTH TO S19A

R.V. Montezale
G.C. ELEC. DCPP
9-3-82

APPROVED BY																	
		REV.	DATE	DESCRIPTION								GM	DWN.	CHKD.	SUPV.	APVD.	
GM		<p>"AS BUILT"</p> <p>GE/GW-140-4-161</p> <p>5-20</p> <p>MOUNTED ON WALL</p> <p>PACIFIC GAS AND ELECTRIC COMPANY</p> <p>SAN FRANCISCO, CALIFORNIA</p>												B/M			
SUPV.														DWG. LIST			
DSGN.														SUPSDS			
DWN.														SUPSD BY			
CHKD.														SHEET NO.		SHEETS	
O.K.														DRAWING NUMBER		REV.	
DATE		SCALE															

Hand-drawn structural detail of a beam-column joint. The beam is labeled "EL. 1402" and has a height of 16". The column has a width of 15". A diagonal reinforcement bar is labeled "K7250-1 1/2 d". The joint is labeled "P-1000". Dimensions include 13 1/2" for the horizontal distance from the column face to the bar end, 5" for the vertical distance from the beam top to the bar end, and 1 1/2" for the bar diameter. A coordinate system shows North (N) pointing left, South (S) pointing right, East (E) pointing up, and West (W) pointing down.

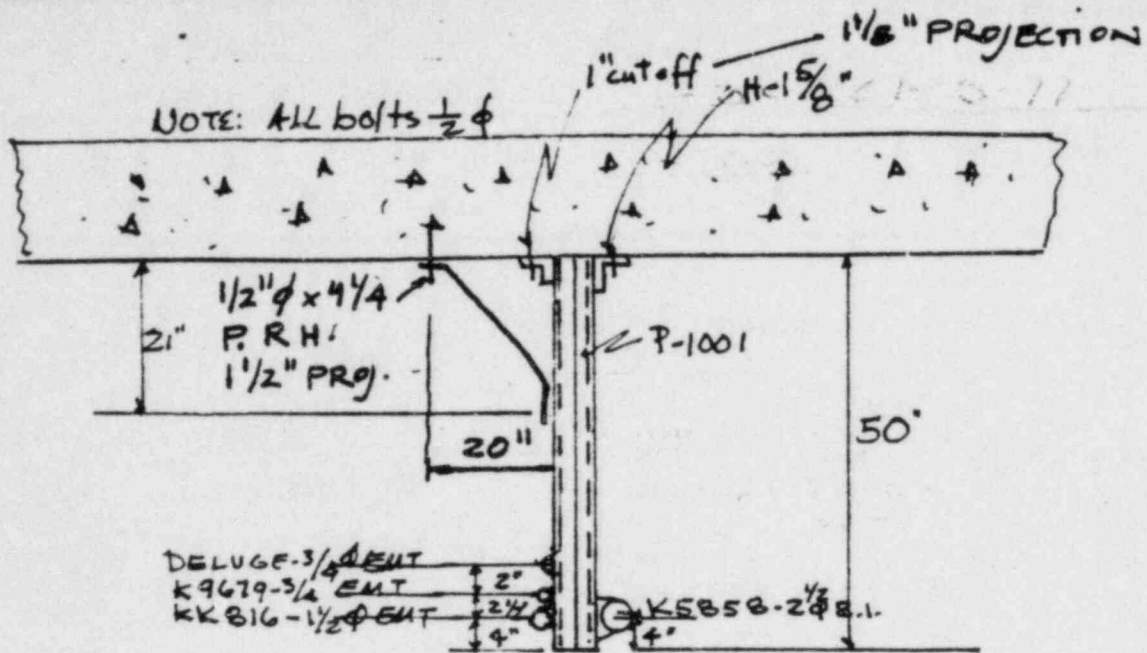
SPAN

48° EAST TO S 288 K 7250 - 1½ Q - 14' WEST TO S-40

R.V. Montero/c
G.C. STA. Elec
DCPP

[illegible]

GM	<p align="center"> <i>"AS BUILT"</i> <i>GE/GW-140-4-300</i> <i>S-288</i> <i>Ceiling Mtd.</i> </p> <p align="center"> PACIFIC GAS AND ELECTRIC COMPANY SAN FRANCISCO, CALIFORNIA </p>	B/M
SUPV.		DWG. LIST
DSGN.		SUPSDS
DWN.		SUPSD BY
CHKD.		SHEET NO. SHEETS
O.K.		DRAWING NUMBER REV.
DATE	SCALE	



LOOKING SOUTH

SPANS

96" North to S-202	DELUGE- $\frac{3}{4}\phi$ ENT-64" South to S-18	
	K9679- $\frac{3}{4}\phi$ ENT-70"	S-18
	KK816- $1\frac{1}{2}\phi$ ENT-72"	S-18
	K5858- $2\frac{1}{2}\phi$ R.I.-56"	S-18

R.V. Montez
GC STA. Elec
DCPP

APPROVED BY					9-7-82				
REV.	DATE	DESCRIPTION	GM	DWN.	CHKD.	SUPV.	APVD.		

GM
SUPV.
DSGN.
DWN.
CHKD.
O.K.
DATE
SCALE

"AS BUILT"
S-289
H-85-3-11
Mounted on ceiling
PACIFIC GAS AND ELECTRIC COMPANY
SAN FRANCISCO, CALIFORNIA

B/M
DWG. LIST
SUPSDS
SUPSD BY
SHEET NO. SHEETS
DRAWING NUMBER REV.

Structural drawing of a window frame. The drawing includes the following details:

- Top Header:** Labeled with various material specifications: $H-1''$, $H-1''$, $H-1\frac{1}{2}''$, $H-1''$, $H-1''$, $H-1''$, $H-2''$, $H-1''$, $H-1''$, $H-1\frac{1}{4}''$.
- Left Sill:** Labeled with material specifications: $S-6\frac{1}{2}''$, $4''$, $13\frac{1}{2}''$.
- Right Sill:** Labeled with material specifications: $S-6\frac{1}{2}''$, $14''$, $12''$.
- Vertical Members:** Labeled with material specifications: $P-5501$, $P-1331$ TYP.
- Horizontal Members:** Labeled with material specifications: $P-5501$, $K 8687$ R.I., $K 8688$ R.I.
- Dimensions:**
 - Overall width: $36''$
 - Overall height: $40''$
 - Distance between vertical members: $6''$
 - Distance between horizontal members: $10\frac{1}{2}''$
- Other Labels:** 3ϕ (three circles) are shown at the bottom of the vertical members.

90" WEST TO S271 { K8687-34-R.1 } 41" EAST TO WALL
K8688-34-R.1

R.V. Montero/c
GC STA. ELEC

DEPT.
9-10-82

APPROVED BY						DEPT.			
						9-10-82			
REV.	DATE	DESCRIPTION				GM	DWN.	CHKD.	SUPV. APVD.

GM	
SUPV.	
DSGN.	
DWN.	
CHKD.	
O.K.	
DATE	SCALE

B/M	
DWG. LIST	
SUPSDS	
SUPSD BY	
SHEET NO.	SHEETS
DRAWING NUMBER	REV.

Diagram of a three-span continuous beam with dimensions:

- Span 1 (Left): $H - 1\frac{3}{4}'$ (top), $H - 1\frac{1}{4}"$ (bottom)
- Span 2 (Middle): $H - 1\frac{3}{8}"$ (top), $H - 1"$ (bottom)
- Span 3 (Right): $H - 1\frac{1}{2}"$ (top), $H - 1"$ (bottom)

Section A-A

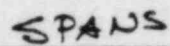
SPANS

48" TO TRAY NORTH KG588 - 3φ R.I. - 69½" Sootb to S102

R.V. Monterok
G.C. STA. ELAS
DCPP

9-9-82

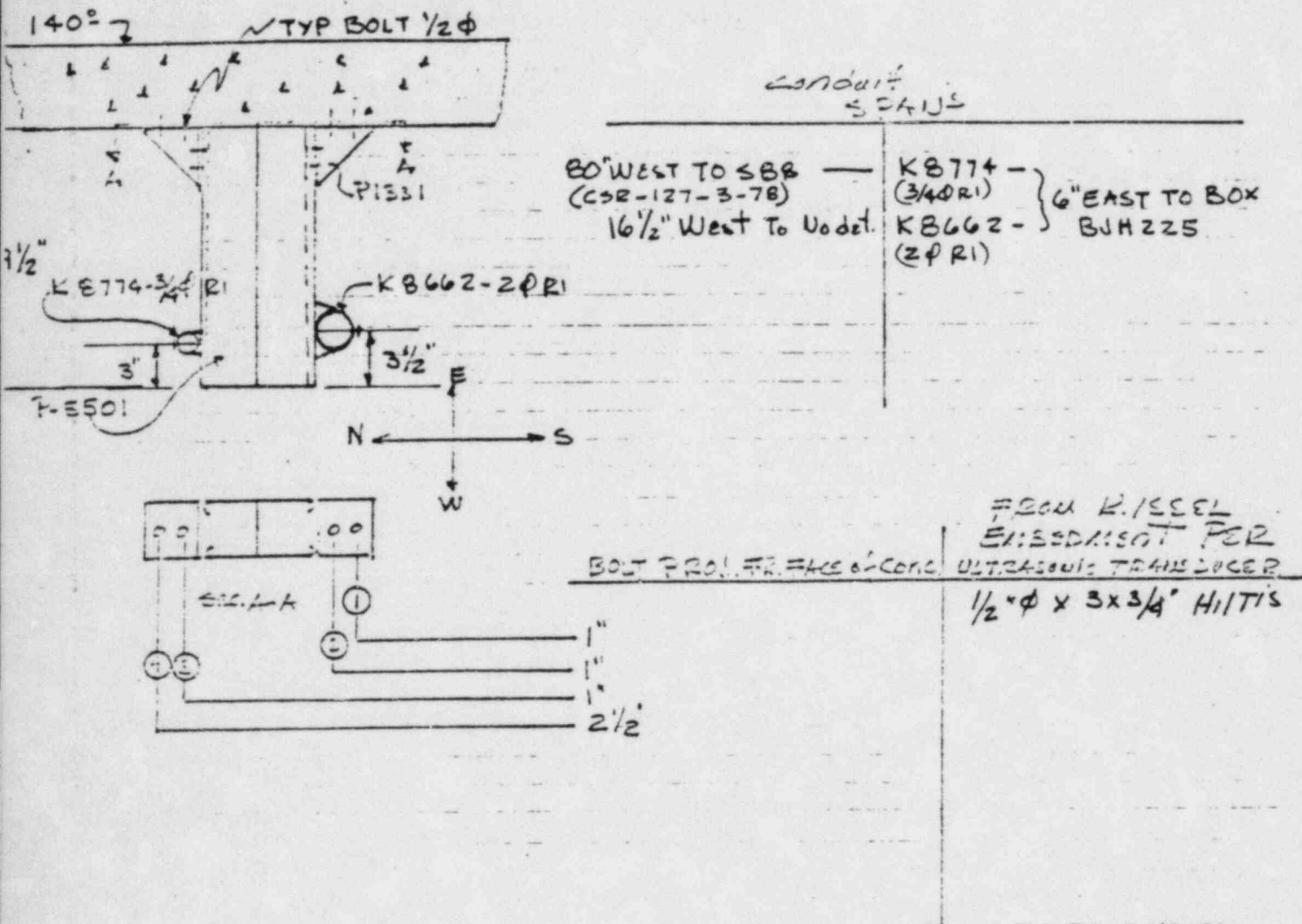
GM	<p style="text-align: center;"><i>"AS BUILT"</i> <i>H-128-1-59</i> <i>S-233</i> <i>Mounted From Ceiling</i> PACIFIC GAS AND ELECTRIC COMPANY SAN FRANCISCO, CALIFORNIA</p>	B/M	
SUPV.		DWG. LIST	
DSGN.		SUPSDS	
DWN.		SUPSD BY	
CHKD.		SHEET NO.	SHEETS
O.K.		DRAWING NUMBER	REV.
DATE	SCALE		



K7730 - 2 1/2 ϕ RI - 53' South, then EAST
TO S-28B

APPROVED BY																			
		REV.	DATE	DESCRIPTION								GM	DWN.	CHKD.	SUPV.	APVD.			
GM		<p style="text-align: center;"> <i>"As Built"</i> <i>H-128-1-58</i> <i>S-87</i> <i>Mounted at ceiling</i> PACIFIC GAS AND ELECTRIC COMPANY SAN FRANCISCO, CALIFORNIA </p>													B/M				
SUPV.															DWG. LIST				
DSGN.															SUPSDS				
DWN.															SUPSD BY				
CHKD.															SHEET NO.				SHEETS
O.K.												DRAWING NUMBER				REV.			
DATE												SCALE							

"AS BUILT" SUPPORT NO. CSR-127-3-77
 DETAIL NO. S-88



R. I. Montford
 G. C. STA.
 SEPT. 1982

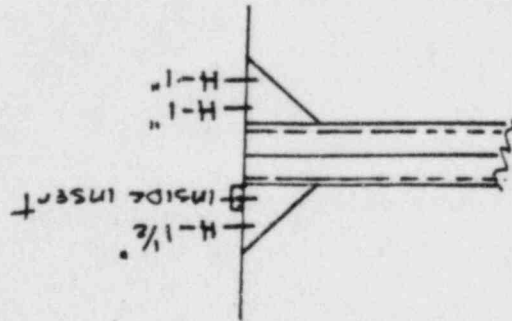
PAGE 2 of 2

CSR-127-S-327

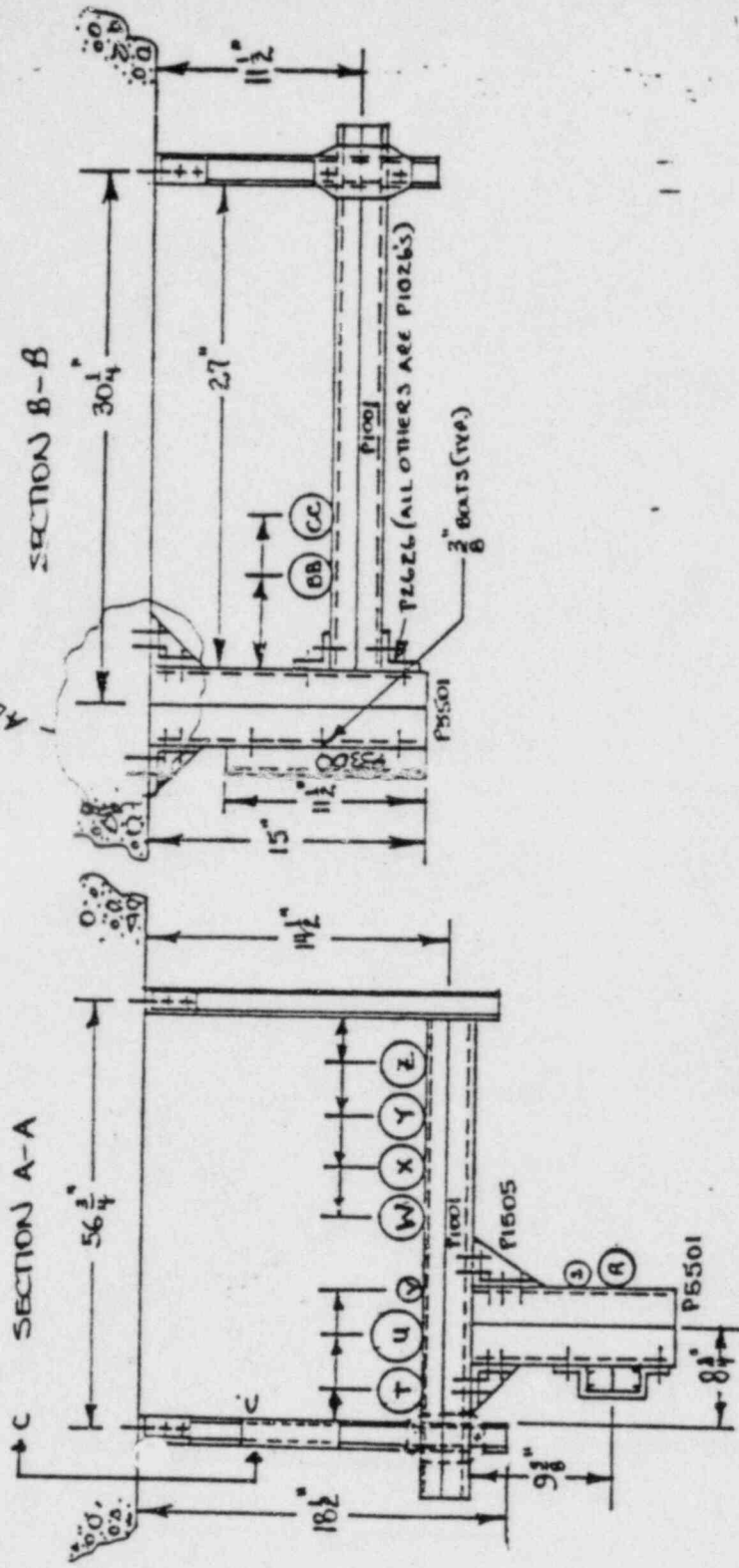
S-417

REFER LIST 49

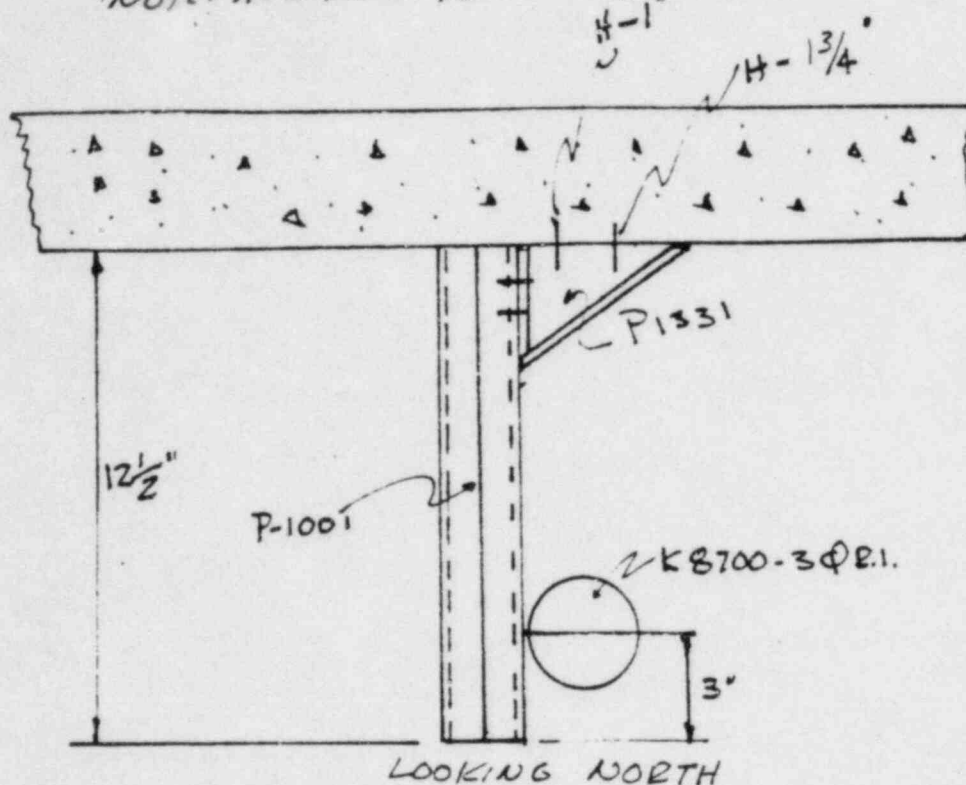
ALL BOLTS (TYPE) INSERT



Section C-C



NOTE: ALL BOLTS $\frac{1}{2}$ " ϕ x $3\frac{3}{4}$ ". 4141's

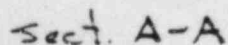


≤ PAUS

66' South To S243 KB700-3φ R.I. - 42' NORTH TO S-129

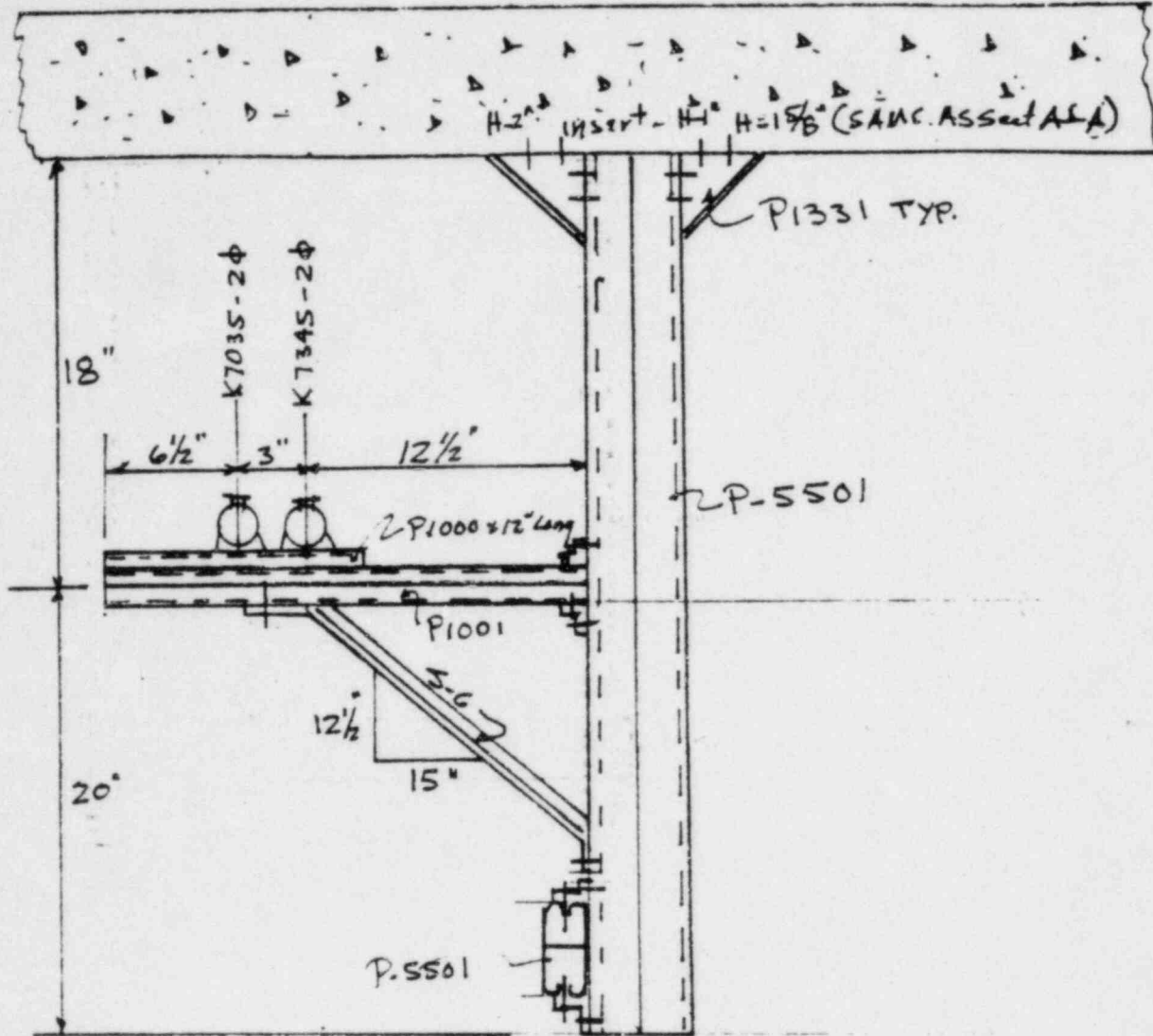
RV. Monterde
G.C. STA. Elec
DCPP 9-7-82

APPROVED BY	
REV.	DATE DESCRIPTION GM DWN. CHKD. SUPV. APVD.
GM SUPV. DSGN. DWN. CHKD. O.K.	"AS BUILT" <i>CSP-127-3-480</i> <i>S-85</i> <i>ceiling mounted</i> PACIFIC GAS AND ELECTRIC COMPANY SAN FRANCISCO, CALIFORNIA
DATE SCALE	B/M DWG. LIST SUSDS SUSPD BY SHEET NO. SHEETS DRAWING NUMBER REV.



R.V. Montezale
GC. STA. ELEC.
DCPP 9-10-82

APPROVED BY																
REV.	DATE	DESCRIPTION									GM	DWN.	CHKD.	SUPV.	APVD.	
GM		<p align="center"><i>* AS BUILT *</i></p> <p align="center"><i>CSR-127-4-121</i></p> <p align="center"><i>5.136</i></p> <p align="center"><i>Ceiling & WALL MOUNTED</i></p> <p align="center">PACIFIC GAS AND ELECTRIC COMPANY</p> <p align="center">SAN FRANCISCO, CALIFORNIA</p>										B/M				
SUPV.												DWG. LIST				
DSGN.												SUSPDS				
DWN.												SUPSD BY				
CHKD.												SHEET NO.				SHEETS
O.K.												DRAWING NUMBER				REV.
DATE		SCALE														



SECTION B-B

SPANS

50" WEST TO S135

KT 818 - $1\frac{1}{2}\phi$ - 100" EAST TO S135

96" NORTH TO S 121

K 7035-24-

12" NORTH TO TRAY

K7345-2φ-

31" south to block wall.

R.V. Monterde
G.C. STA. Elec.
DCPP 9-10-82

APPROVED BY																				
		REV.	DATE	DESCRIPTION									GM	DWN.	CHKD.	SUPV.	APVD.			
GM		<p align="center"><i>"AS BUILT"</i> <i>CSR-127-4-121</i> <i>S-13C</i> <i>Ceiling & Wall Mounted</i> PACIFIC GAS AND ELECTRIC COMPANY SAN FRANCISCO, CALIFORNIA</p>																B/M		
SUPV.																		DWG. LIST		
DSGN.																		SUPSDS		
DWN.																		SUPSD BY		
CHKD.																		SHEET NO.	SHEETS	
O.K.																		DRAWING NUMBER	REV.	
DATE																		SCALE		

K-11

"AS BUILT" SUPPORT NO.

CSR-127-4-152

DETAIL NO.

S-88

S-101

S-100

S-100

S-100

S-100

S-115

S-115

S-115

IF

EL. 140'-2" 1/2" bolt TYP.

12"

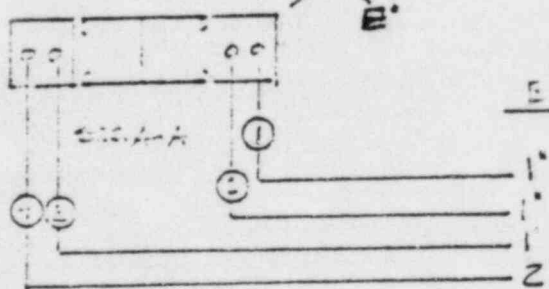
K2775- 3/4" R.I.

3 1/2"

NW

N

E



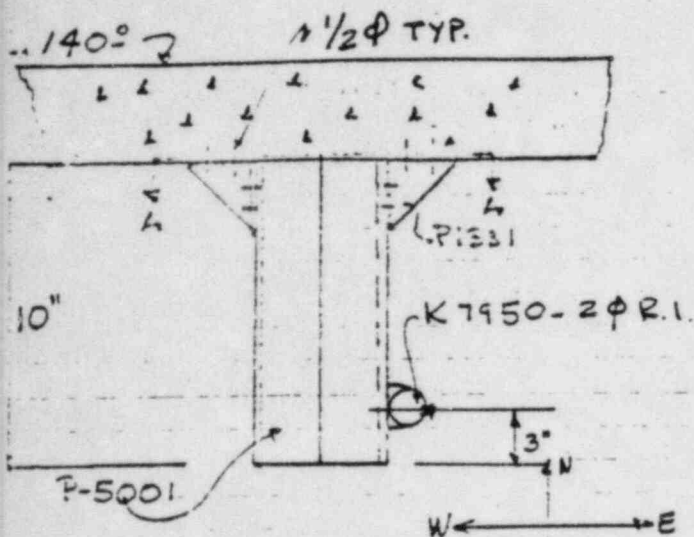
CONDUIT
SPACERS

97" SOUTH TO SBB K-2775- 3/4" R.I. 44" L
CELL.

FROM R.I.
EXPOSED
BOLT FROM FR. FACE OF CONC. ULTRASONIC TR
1/2" ϕ x 3 3/4"

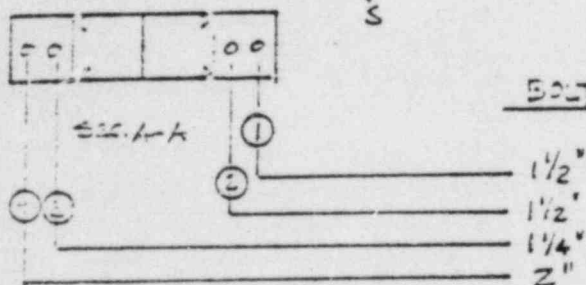
R. Monter
C.E. 571.
SEPT. 19.

"AS BUILT" SUPPORT NO. CSR-127-5-261
 DETAIL NO. S-88



CONDUIT
SEALING

48" TO WALL (NORTH) K7950 - 97" South to rack
 No. 17 Control Box

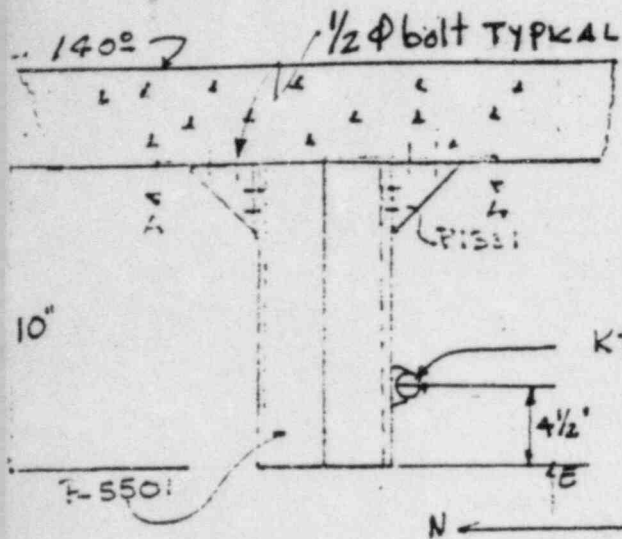


BOLT PROJ. FR. FACE OF CONC. FROM R/SEEL
 EMBEDMENT PER
 ULTRASONIC TRANSDUCER

1/2" x 3 3/4"
 HILTI

R. Monteleone
 C.E. STA.
 SEPT. 1982

"AC RAIL" SUPPORT NO. CSR-127-6-166
 DETAIL NO. S-88



CONDUIT
 S-113

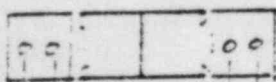
72° WEST TO S-143 KT 776-1φ RI. 69° EAST TO
 S-70

KT 776-2φ RI.

4 1/2'
 1E

N ← → S

W



5/16\"



1

2

BOLT FROM FR. FACE OF CONC. ULTRASONIC TRANSDUCER

1 1/4"

2" (note: no nut provided)

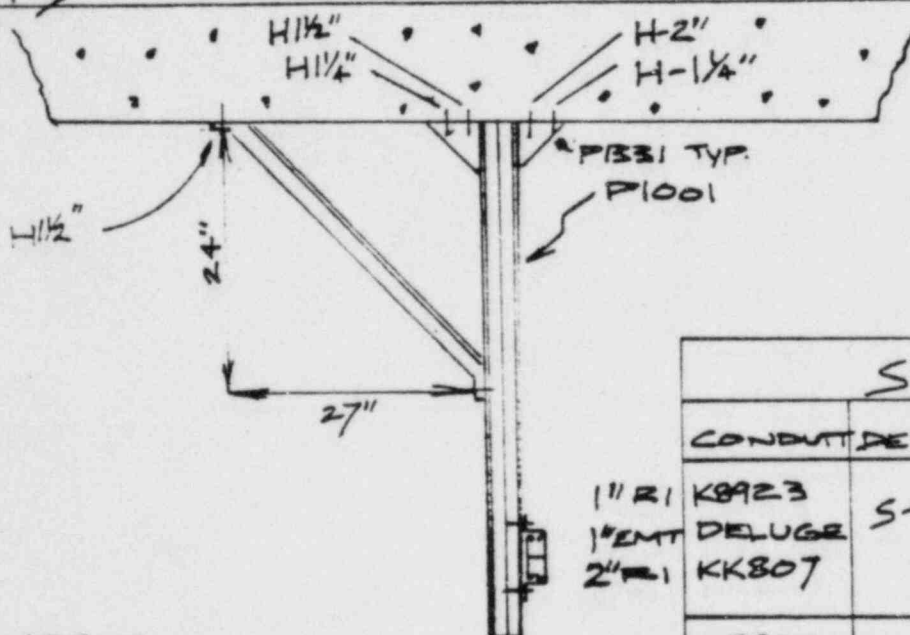
1 1/4"

1"

FROM K. IESSEL
 EXCEEDMENT PER
 ULTRASONIC TRANSDUCER

1/2" φ x 3 3/4"
 HILTI

R. Monteleone
 C.E. STA.
 SEPT. 1982



SPANS			
CONDUIT DETAIL			
K8923 DELUGE KK807	S-383	WEST	76"
K8923 DELUGE KK807	S-202	EAST	100"

[illegible]

GM	
SUPV.	
DSGN.	
DWN.	
CHKD.	
O.K.	
DATE	SCALE

J-115-10-63 S-383

AS-BUILT

BY M. CAMPBELL

PACIFIC GAS AND ELECTRIC COMPANY

SAN FRANCISCO, CALIFORNIA

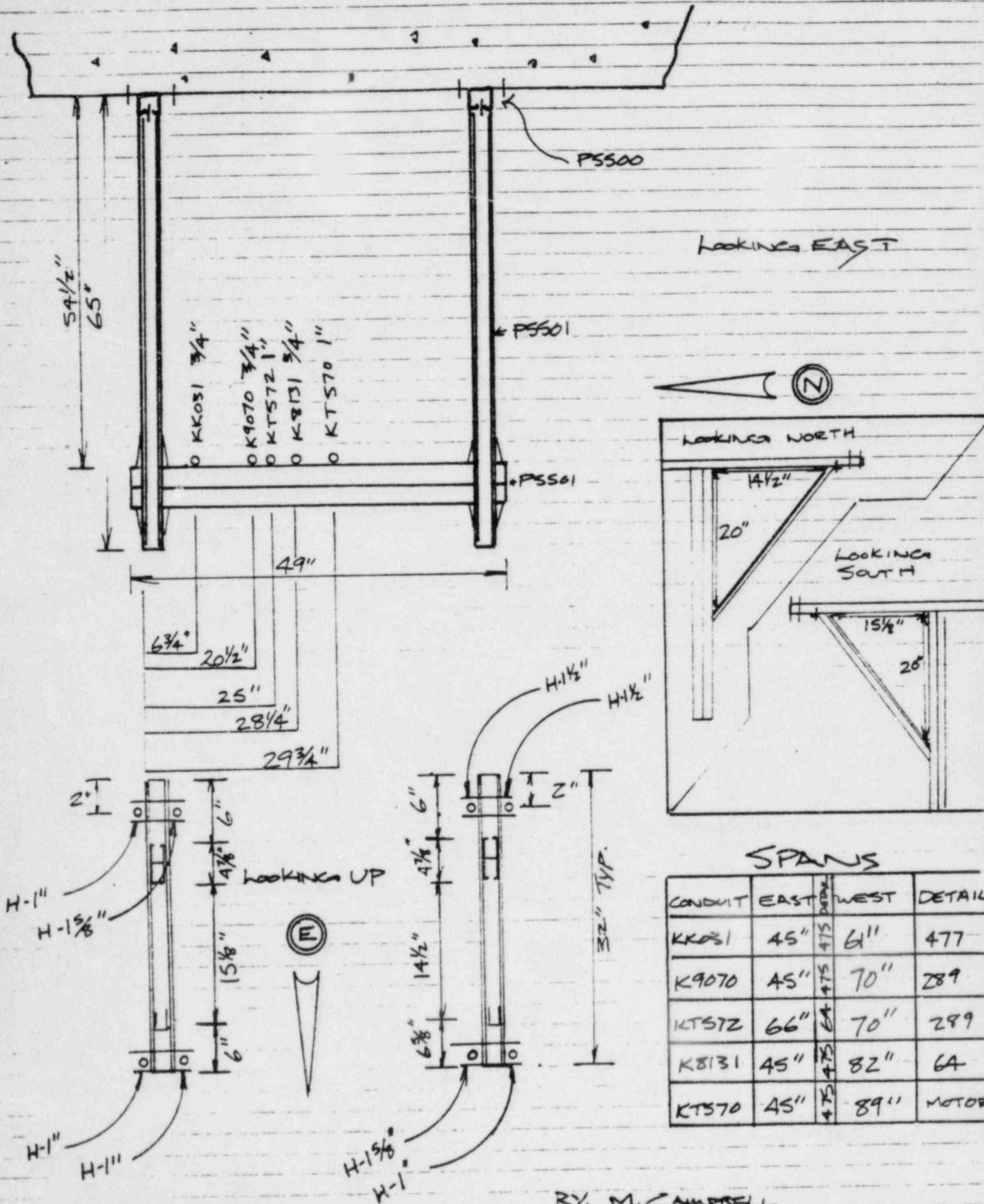
DATE 9.7.82

B/M	
DWG. LIST	
SUPPDS	
SI 13 BY	
SHEET NO.	SHEETS
DRAWING NUMBER	REV.

S-477

J-115-11-59

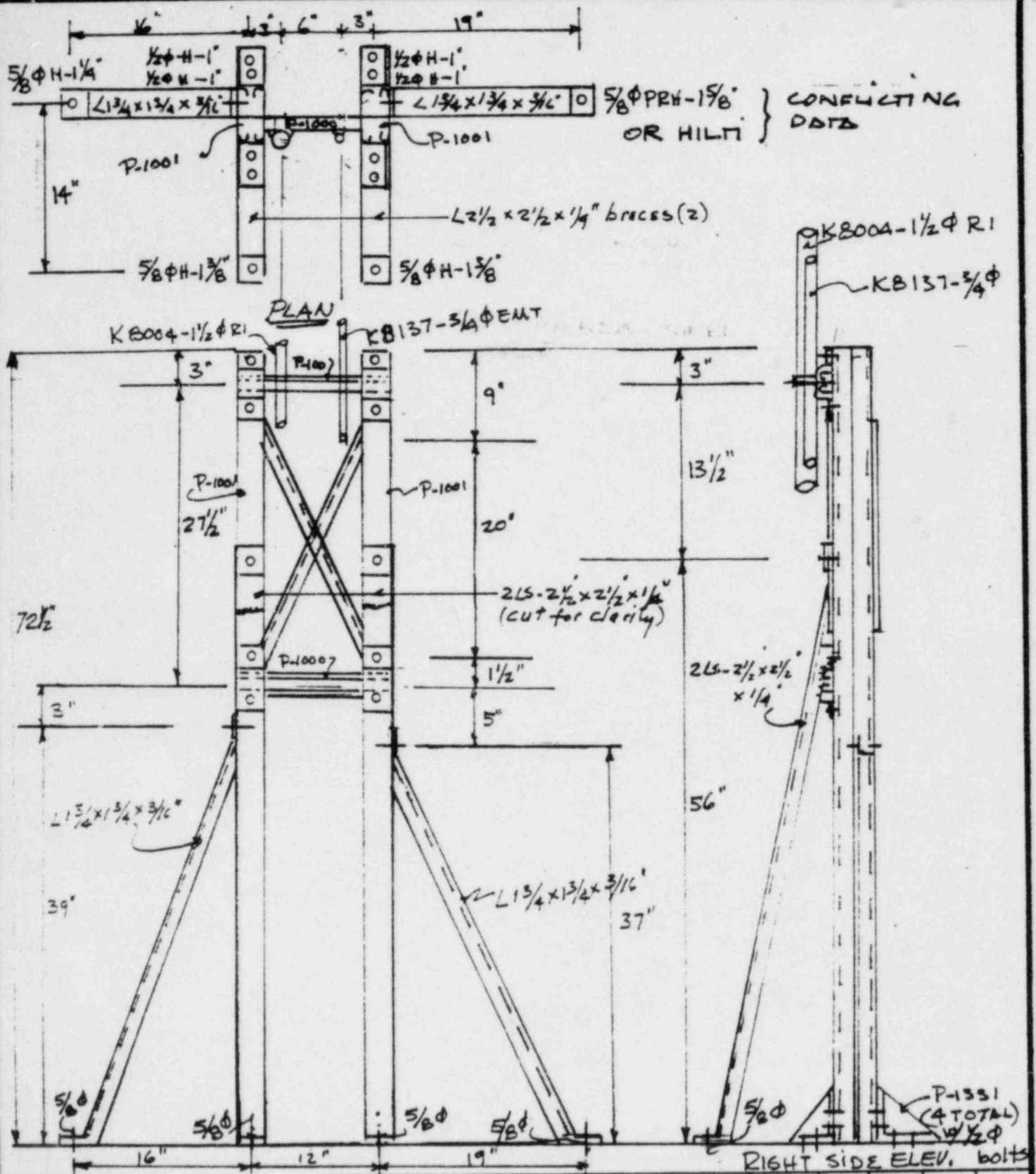
PAGE 1 OF 1



SPANS

CONDUIT	EAST	WEST	DETAIL
KK031	45"	61"	477
K9070	45"	70"	289
KTS72	66"	70"	289
K8131	45"	82"	6A
KTS70	45"	89"	MOTOR

BY: M. CAMPBELL



APPROVED BY

FRONT ELEV.

SPANS

38" Danno To Velve KB137-3/4" EMT-37" UP TO TRAY (MSA)

(KB004-1 1/2" R1, 96" TO BOX SQB 79 DWG.)

GM
SUPV.
DSGN.
DWN.
CHKD.
O.K.

DATE

SCALE

"AS BUILT"
J-115-10-43
3-67

FLOOR Mounted

PACIFIC GAS AND ELECTRIC COMPANY
SAN FRANCISCO, CALIFORNIA

R.V. Montemur
GC STA. ELEC
DCPP 1-10-82

B/M

DWG. LIST

SUPSDS

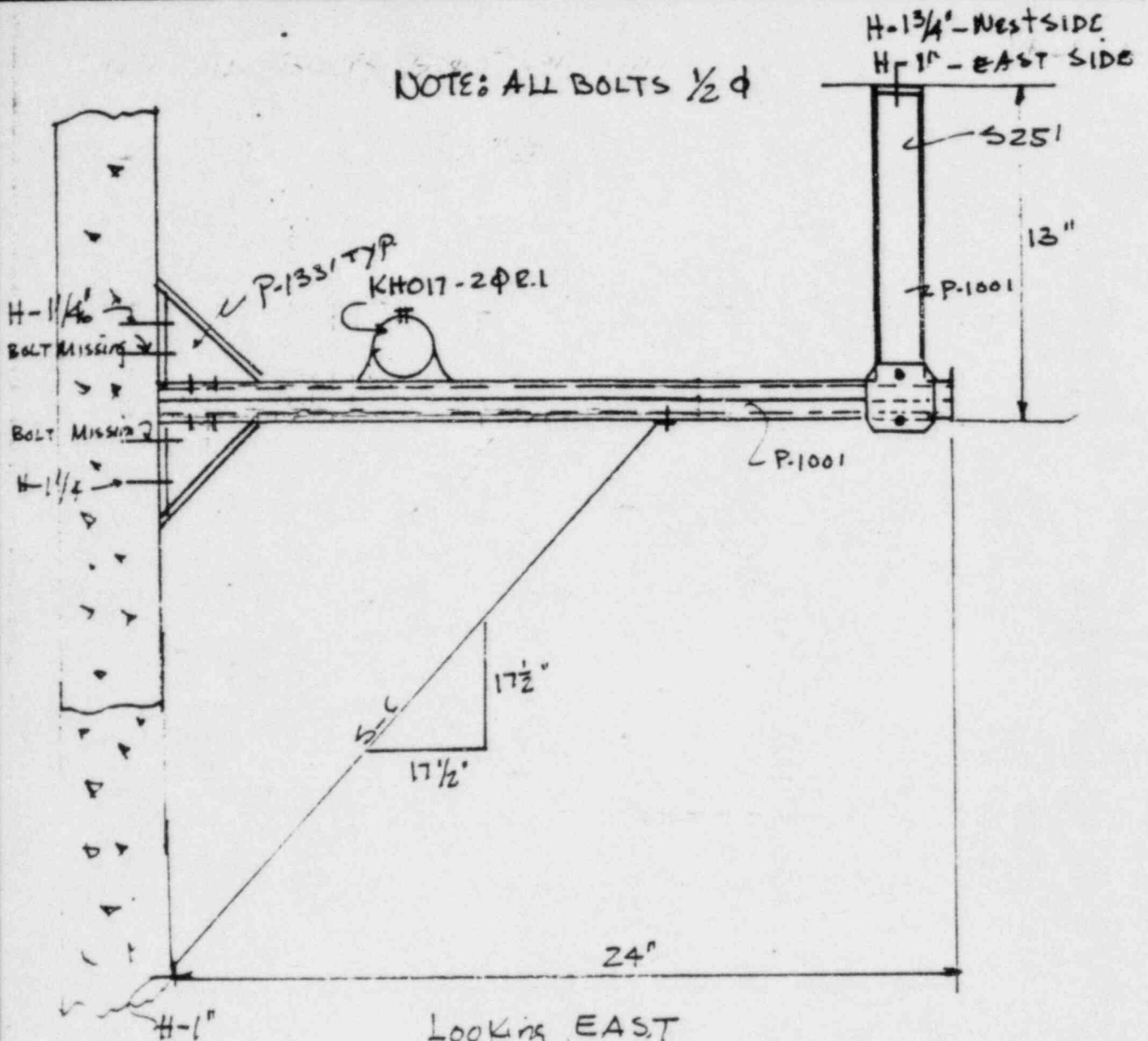
SUPSD BY

SHEET NO.

SHEETS

DRAWING NUMBER REV.

NOTE: ALL BOLTS $\frac{1}{2}$ ϕ

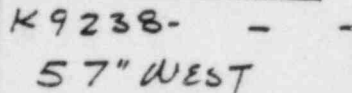


Looking EAST
SPAN
50' to S-202 EAST KH017-2 ϕ R1 - 28" to WALL WEST

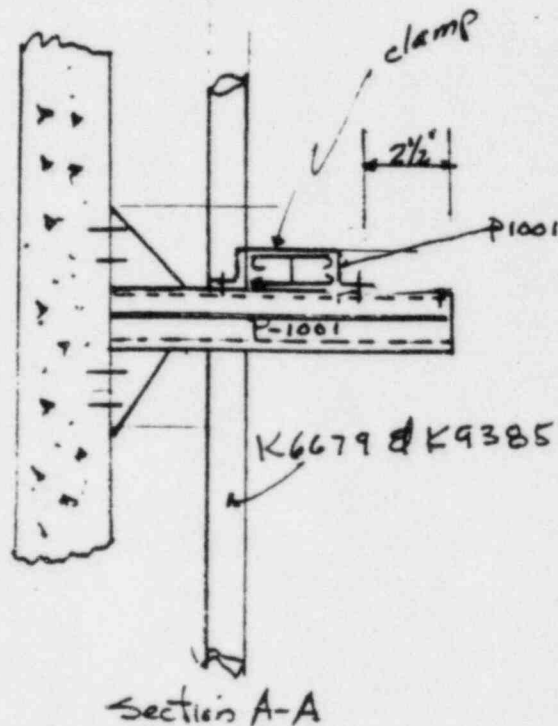
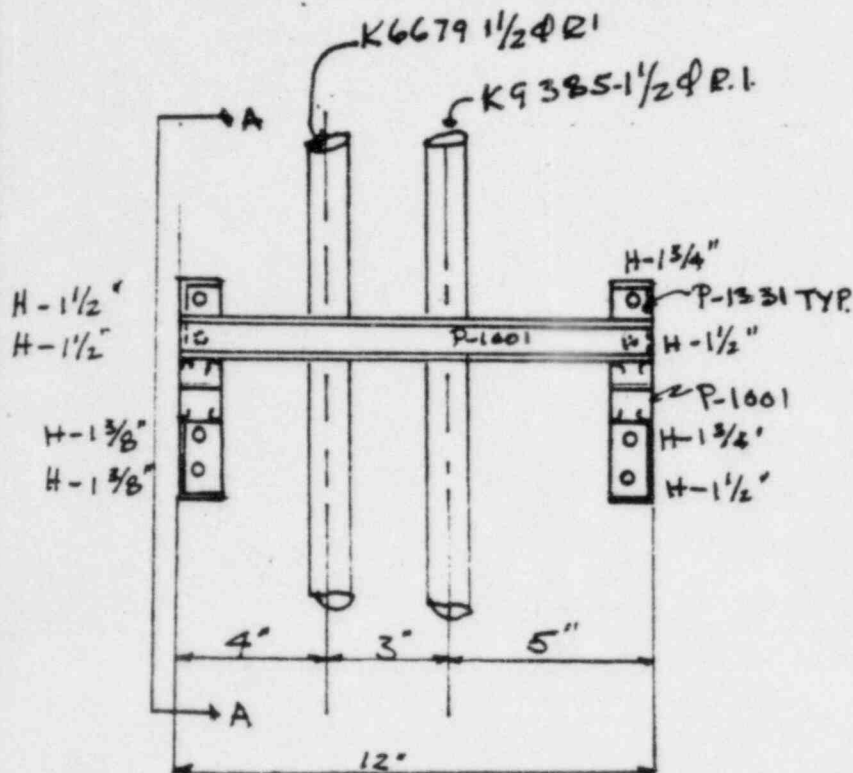
R.V. Montfort 2
GC STA. DCP
9-7-82

APPROVED BY											
REV.		DATE		DESCRIPTION		GM		DWN.		CHKD. SUPV. APVD.	
GM				AS BUILT				B/M			
SUPV.				K-85-2.25				DWG. LIST			
DSGN.				S-202				SUPSDS			
DWN.				Mounted on wall & ceiling				SUPSD BY			
CHKD.				PACIFIC GAS AND ELECTRIC COMPANY				SHEET NO.		SHEETS	
O.K.				SAN FRANCISCO, CALIFORNIA				DRAWING NUMBER		REV.	
DATE		SCALE									

2004-01-16

[illegible]

Note: ALL BOLTS $\frac{1}{2}\phi \times 3\frac{3}{4}"$ H/1/4" S



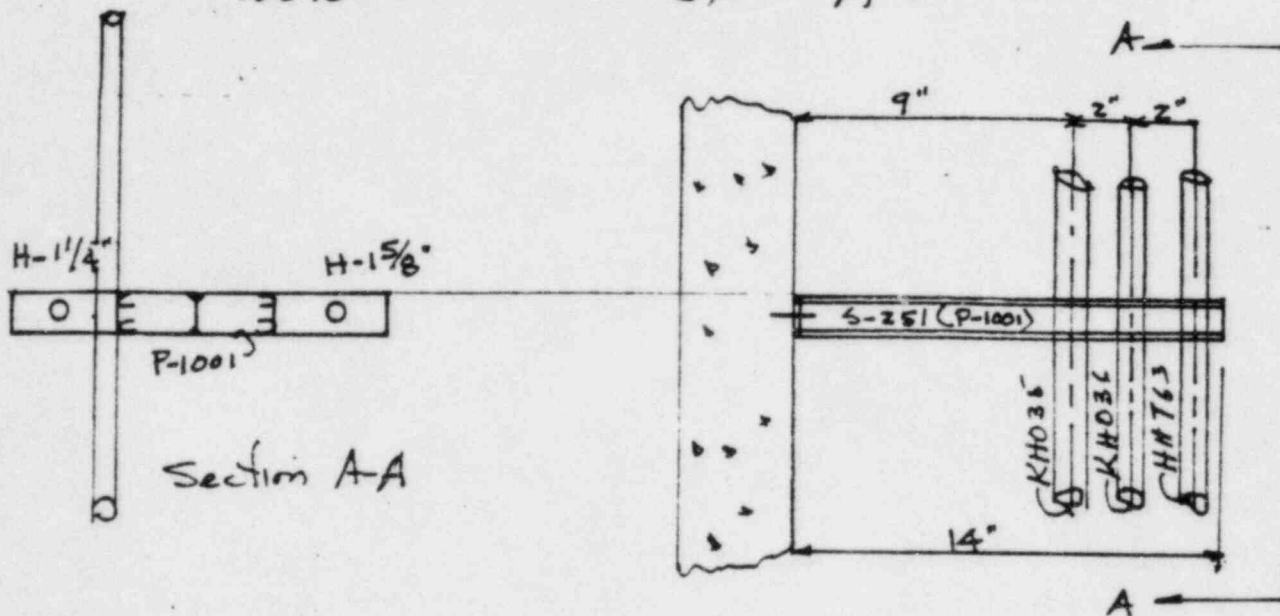
SPANS

UP 90" TO 19B	- K6679-1 1/2 phi R.I.	} On to Panel 31"
UP 92" TO 519A	- K9385-1 1/2 phi R.I.	

R.V. Montero
G.C. STA. DCPP
9-7-82

APPROVED BY											

NOTE: ALL BOLTS $\frac{1}{2}\phi \times 3\frac{3}{4}$ " H. 1/16"

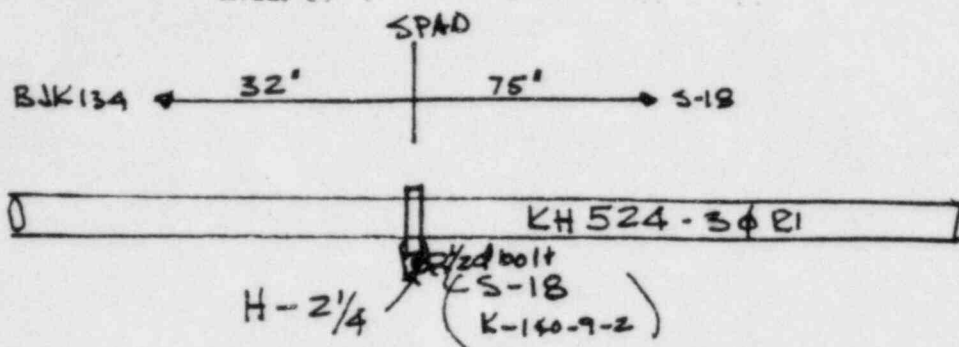


SPANS

73"-to S-20 UP { KH035 - 1φ - R.I.
KH036 - 1φ - R.I.
KHT63 - 1φ - R.I. } 72" to S202 DU.

R.V. Montero
GC. STA. ELEC
DCPP

APPROVED BY								9-7-42	
REV.		DATE		DESCRIPTION		GM		DWN. CHKD. SUPV. APVC	
GM				<p>"As BUILT"</p> <p>K-100-11-40</p> <p>S-243</p> <p>Wall Mounted</p> <p>PACIFIC GAS AND ELECTRIC COMPANY</p> <p>SAN FRANCISCO, CALIFORNIA</p>		B/M			
SUPV.						DWG. LIST			
DSGN.						SUPSDS			
DWN.						SUPSD BY			
CHKD.						SHEET NO.		SHEETS	
O.K.				DRAWING NUMBER		REV.			
DATE		SCALE							

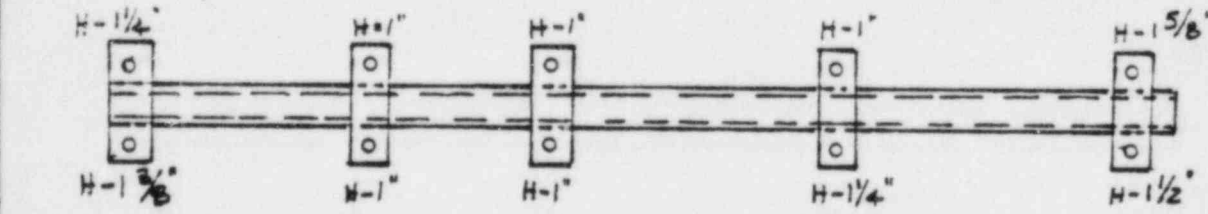
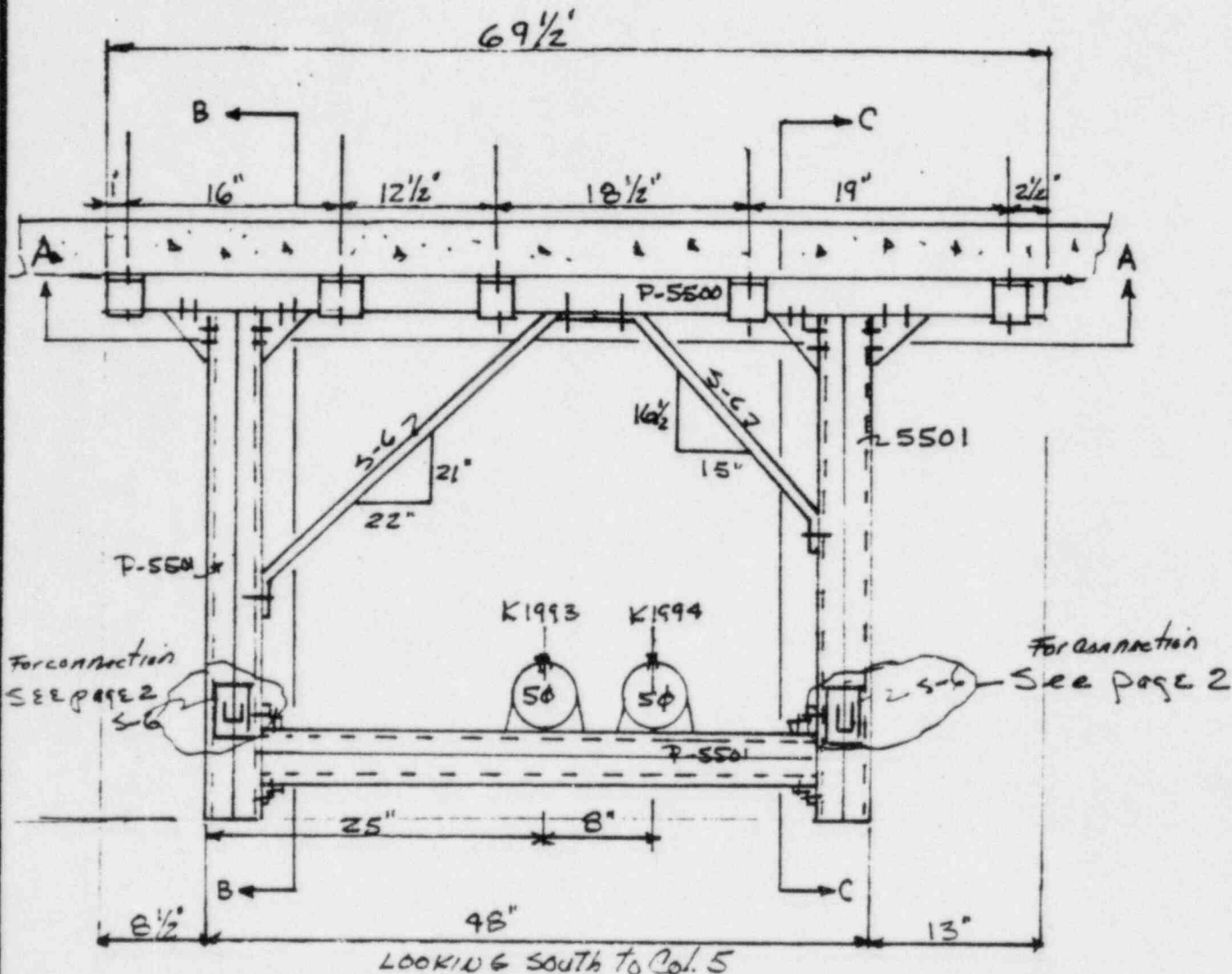


RV. Montrose
GC. STA. Elec
DCPP
9-7-82

APPROVED BY											
		REV.	DATE	DESCRIPTION			GM	DWN.	CHKD.	SUPV.	APVD.
GM		<p>"AS BUILT"</p> <p>K-140-9-2</p> <p>S-18</p> <p>WALL MOUNTED</p> <p>PACIFIC GAS AND ELECTRIC COMPANY</p> <p>SAN FRANCISCO, CALIFORNIA</p>						B/M			
SUPV.								DWG. LIST			
DSGN.								SUPSDS			
DWN.								SUPD BY			
CHKD.								SHEET NO.			
O.K.						DRAWING NUMBER				REV.	
DATE	SCALE										

NOTE: ALL BOLTS $\frac{1}{2}" \phi \times 3\frac{3}{4}"$ Hilti

PAGE 1 of 2



Section A-A

R.V. Montenegro
GC. STA. ELEC

DEPP 9-8-81

APPROVED BY											
REV.		DATE		DESCRIPTION				GM		DWN. CHKD. SUPV. APVD	
GM				<p>"AS BUILT"</p> <p>G-140-B-1023 B</p> <p>3-48</p> <p>Mounted At Ceiling</p> <p>PACIFIC GAS AND ELECTRIC COMPANY</p> <p>SAN FRANCISCO, CALIFORNIA</p>				B/M			
SUPV.								DWG. LIST			
DSGN.								SUPSDS			
DWN.								SUPSD BY			
CHKD.								SHEET NO.		SHEETS	
O.K.				DRAWING NUMBER		REV.					
DATE		SCALE									

MINOR VARIATION REPORT

12.

IDENTIFICATION	Location Diablo Canyon	Unit No. 2	Reference Spec. No. 8837	Page 1 of 3
Organization Endurance Metal Products	Contractor's Report No.		PGandE MVR No. C-1354	
Send Copy to Contractor <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No		Name H. P. Foley Company		

DESCRIPTION OF DISCREPANCY

Item	Supports for Class I Electrical Panels
Explanation	Non Class I - Beams supporting Class I electrical panels were found to have deficient bolted connections as indicated on the attached pages.

Initiated By <i>R. D. Kohler</i>	Date 1/17/84
DISPOSITION REJECT - Rework in accordance with SMF-0605 attached.	

Additional Concurrence, When Required	Name	Date
Senior Site Representative	<i>Lawrence M. Rumer</i>	Date 1/17/84
R E V I E W	This Minor Variation Report (1) <input checked="" type="checkbox"/> Is Not Reportable; <input type="checkbox"/> May be Reportable (Per Title 10 CFR, Part 21)	
	(2) <input checked="" type="checkbox"/> Is Not a Nonconformance	
	Quality Control	Date 1/18/84
	Senior Site Representative	Date 1/17/84

DISPOSITION ACCOMPLISHED

Remarks

Inspected By	Date
Quality Control	Date

☒ ATTACHMENTS 1) SMF-0605 (3 sheets)

PRIORITY 400

PGand E
General Construction
77G-101 10/82

MINOR VARIATION REPORT

5 IDENTIFICATION	Location Diablo Canyon	Unit No. 182 *	Reference Spec. No. 8837	Page 1 of 8
Organization Endurance Metal Products			Contractor's Report No.	PGand E MVR No. C-1338
Send Copy to Contractor <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No		Name H.P. Foley Company		

DESCRIPTION OF DISCREPANCY

Item
Supports for Class I Electrical Panels

Explanation
Non Class I - beams supporting Class I electrical panels were found to have deficient bolted connections as indicated on the attached pages.

Initiated By *R.D. Kohler* Date 12/1/83

DISPOSITION
Pending Engineering Evaluation

Additional Concurrence, When Required		Name		Date
Senior Site Representative <i>Forrest M. Runner</i>		Date		12/5/83
R E V I E W	This Minor Variation Report (1) <input checked="" type="checkbox"/> Is Not Reportable; (2) <input checked="" type="checkbox"/> Is Not a Nonconformance		<input type="checkbox"/> May be Reportable (Per Title 10 CFR, Part 21)	
	Quality Control <i>J.R. Bratt</i>		Date 12/13/83	
	Senior Site Representative <i>Forrest M. Runner</i>		Date 12/5/83	

DISPOSITION ACCOMPLISHED

Remarks

Inspected By _____ Date _____

Quality Control _____ Date _____

☐ ATTACHMENTS

PRIORITY 450

MINOR VARIATION REPORT

IDENTIFICATION	Location DIABLO CANYON	Unit No. 1&2	Reference Spec. No. 8837	Page 1 of 8
Organization Endurance Metal Products			Contractor's Report No.	PGandE MVR No. C-1338 R
Send Copy to Contractor <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No		Name H.P. Foley Company		

DESCRIPTION OF DISCREPANCY

Item
Supports for Class I Electrical Panels

Explanation
Non Class I - beams supporting Class I electrical panels were found to have deficient bolted connections as indicated on the attached pages.

Initiated By **R.D. Kohler** Date **12/1/83**

DISPOSITION

REJECT-REWORK in accordance with SMF-0605 attached.

Additional Concurrence, When Required		Name	Date
Senior Site Representative		Forrest M. Russell	1/14/84
R E V I E W	This Minor Variation Report (1) <input checked="" type="checkbox"/> Is Not Reportable; <input type="checkbox"/> May be Reportable (Per Title 10 CFR, Part 21)		
	(2) <input checked="" type="checkbox"/> Is Not a Nonconformance		
	Quality Control		Date
Senior Site Representative		Deek Bell	1/17/84
		Forrest M. Russell	1/14/84

DISPOSITION ACCOMPLISHED

Remarks

Inspected By	Date
Quality Control	Date

☒ ATTACHMENTS 1) SMF-0605

PRIORITY

1'-8"

W10 (TYP.)

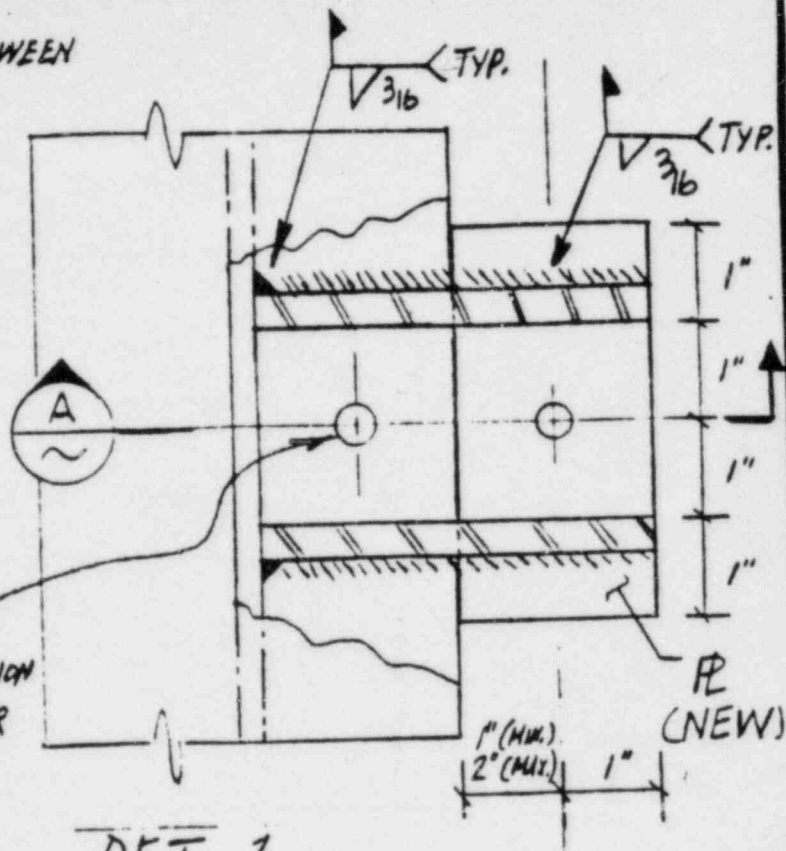
TYP.
PROCESS
CONTROL &
PROTECTION
PANELS

N

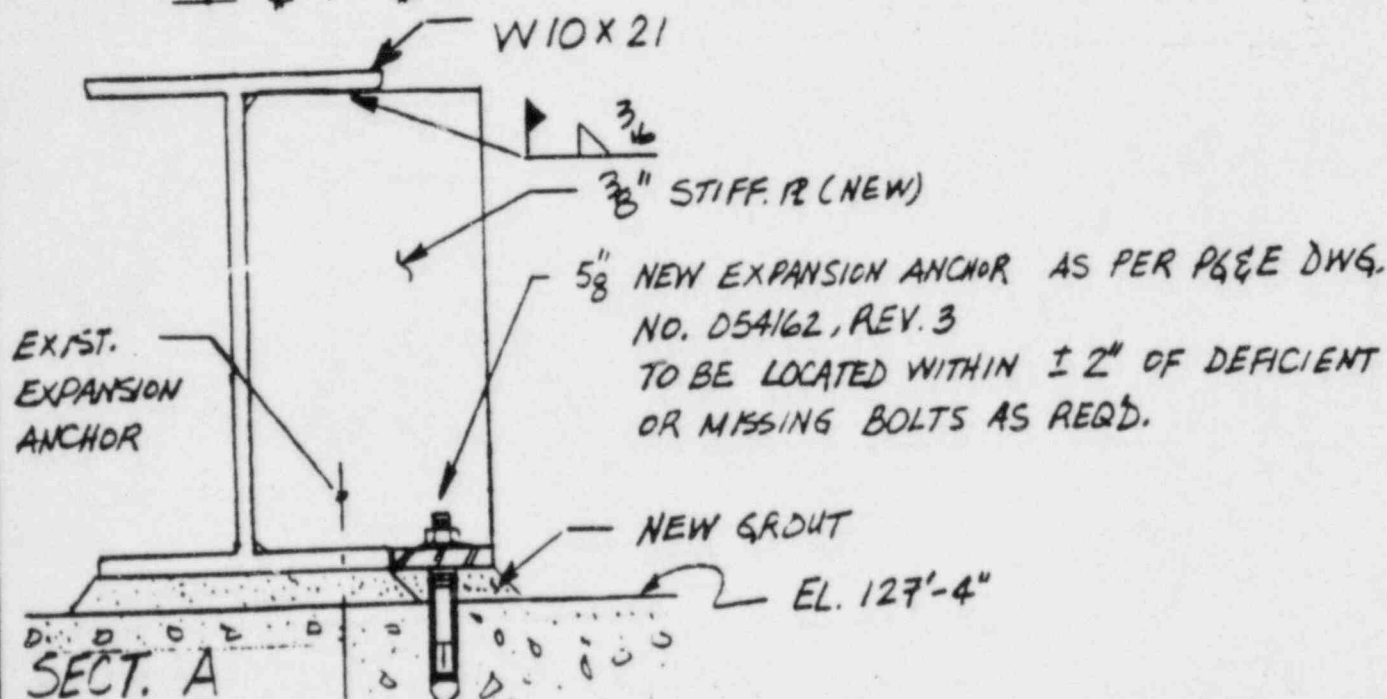
1'-8"

DET.

E
E
A



DET. 1



SECT. A

[illegible]

MINOR VARIATION REPORT

IDENTIFICATION	Location Diablo Canyon	Unit No. 1	Reference Spec. No. #837	Page 1 of 6
Organization Endurance Metal Products			Contractor's Report No. N/A	PGandE MVR No C-1338 R2
Send Copy to Contractor <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No		Name H. P. Foley Company		
DESCRIPTION OF DISCREPANCY				

Item	Supports for Class I Electrical Panels
Explanation	Non Class I - beams supporting Class I electrical panels were found to have deficient bolted connections as indicated on the attached pages.

Initiated By <u>R. D. Kohler</u>	Date <u>1-17-84</u>
----------------------------------	---------------------

DISPOSITION	Pending Engineering evaluation.
-------------	---------------------------------

Rev. 1: REJECT - Rework in accordance with SMF-0605 attached.

Rev. 2: Revised to indicate Unit One only. Refer to IWR #C-1354 for Unit Two portion.

Additional Concurrence, When Required	Name	Date
Senior Site Representative	<i>Sam R...</i>	Date 1-17-84

R E V I E W	This Minor Variation Report		(1) <input checked="" type="checkbox"/> Is Not Reportable;	<input type="checkbox"/> May be Reportable (Per Title 10 CFR, Part 21)
			(2) <input checked="" type="checkbox"/> Is Not a Nonconformance	
	Quality Control	<i>Derek Bell</i>		Date <i>1/17/84</i>
	Senior Site Representative	<i>Lawrence R. Bunker</i>		Date 1-17-84

DISPOSITION ACCOMPLISHED

Remarks

Inspected By	Date
--------------	------

Quality Control	Date
-----------------	------

 ATTACHMENTS 1) SHF-0605 (3 sheets)

PRIORITY 450R

TO 4/28
H. L. L. L.

TO: Mr. D.A. Rockwell
Assistant Project Superintendent
Pacific Gas and Electric Company

DESCRIPTION OF PROBLEM:

PAGE 1 OF 7

THE LINE BEAMS IN THE CSP 20' SPAN (UNITS I & II)
ARE A COMBINATION OF METAL & WOOD & ELECTRICAL
BOLTS HAVE THE FOLLOWING DEFICIENCIES:

- 1) INSUFFICIENT THREAD ENGAGEMENT (IN MANY CASES)
- 2) 90% OF ALL THE BOLTS ARE EXCESSIVELY OUT OF ALIGN-
MENT (BOLTED)
- 3) MANY OF THE BOLTS DO NOT HAVE NUTS.
- 4) IN MANY CASES OF ANCHOR BARS DRILLED (ANALOGOUS)
(PAP) AND NO BOLTS EVER INSERTED. SEE PAGE 2

LOCATION: CSP Elevation 124' Col = Line

DATE: 10-7-83

REVISION BY

[Signature]
EST: 1731

PLEASE CONTACT ME AT THE OFFICE.
A QUICK RESPONSE TO THIS MATTER WOULD
BE APPRECIATED. THANK YOU.

EARL D. BLANK

TO: Mr. D.A. Rockwell
 Assistant Project Superintendent
 Pacific Gas and Electric Company

PAGE 2 OF 7

DESCRIPTION OF PROBLEM:

5.) SEVERAL OF THE BOLTS HAVE BEEN FOUND TO
 HAVE EXCESSIVE INTERFERENT ELEMENTS ONE PARTICULAR
 BOLT WAS NOTED TO SLIGHTLY BOW THE SURFACE
 OF THE BOTTOM SECTION OF THE BEAM IN SUCH A
 MANNER THE NUT COULD NOT BE ATTACHED.

6.) ONE 1/2" DIA. BOLT WAS USED IN PLACE OF THE
 REQUIRED 3/4" DIA. BOLT WITH STATED YOU'LL
 FIND COPIES OF PICTURES REFLECTING THESE
 PROBLEMED AREAS ALONG WITH A LIST OF AFFECTED
 CLASS E PANELS.

LOCATION:

CSR

Elevation 127' Vol. Line

DATE: 10-7-83

REPORT BY

[Signature]

INVESTIGATING DISPOSITION TO MVA NOV 1998

INSURANCE INVESTIGATION REPORT

TO: Mr. D.A. Rockwell

TO: Mr. D.A. Rockwell

Assistant Project Superintendent

Pacific Gas and Electric Company

PAGE 3 OF 7

DESCRIPTION OF WORK:

SINCE THE ELECTRICAL PANELS HAVE BEEN
REMOVED (H. DEF-150) AND THE
FLOOR MEETS CIRCUIT REQUIREMENTS, THE
BEAMS SHOULD ALSO MEET THE SAME OR SIMILAR
CIRCUIT REQUIREMENTS. THE TOTAL NUMBER
OF DEFICIENT FLOOR BEAMS AND NUTS INSTALLED
SHOULD BE DETERMINED TO BE THE SUB-FLOOR
BEAMS DATE BEING IN GOOD CONDITION BACK IN PLACE.

LOCATION: CSR

Elevation

127

Column Line

ORIGINAL PICTURES WILL BE SUPPLIED

UPON REQUEST

DATE: 10-7-82

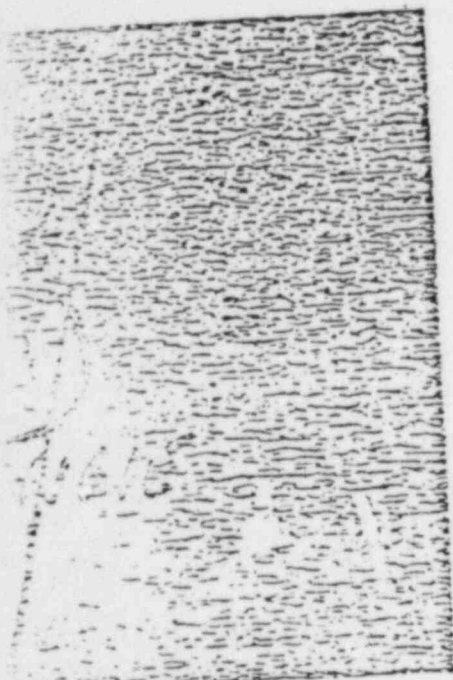
REPORT BY

Bob R. [Signature]

ANELS AFFECTED

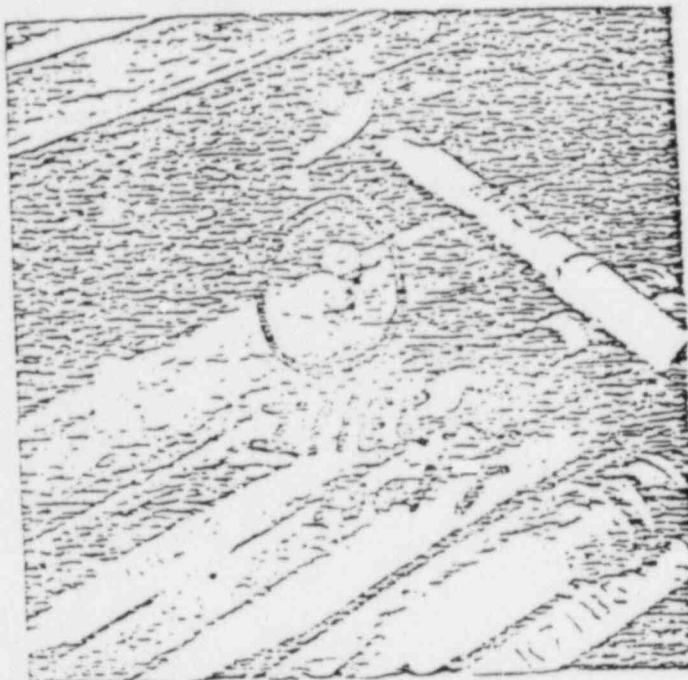
<u>PROTECTION</u>	<u>SET</u>
- A	
1 - B	
1 - C	
1 - D	
1 - E	
<u>CONT.</u>	<u>SET</u>
1 - A	
1 - B	
1 - C	
1 - D	
<u>PROTECTION</u>	<u>SET</u>
2 - A	
2 - B	
2 - C	
2 - D	
2 - E	
<u>CONT.</u>	<u>SET</u>
2 - A	
2 - B	
2 - C	
2 - D	
<u>PROTECTION</u>	<u>SET</u>
3 - A	
3 - B	
3 - C	

<u>CONT.</u>	<u>SET</u>
RND3 - A	
RND3 - B	
RND3 - C	
<u>CONT.</u>	<u>SET</u>
RND4 - A	
RND4 - B	
RND4 - C	
RND4 - D	
RND4 - E	
<u>PROTECTION</u>	<u>SAFE</u>
<u>SET</u>	<u>GUARDS</u>
RNP4 - A	
RNP4 - B	
RNP4 - C	
<u>SAFE</u>	<u>RELAY</u>
<u>GUARDS</u>	<u>RELAY</u>
RNP4 - A	
RNP4 - B	
<u>RELAY</u>	<u>RELAY</u>
RNP4 - A	
RNP4 - B	



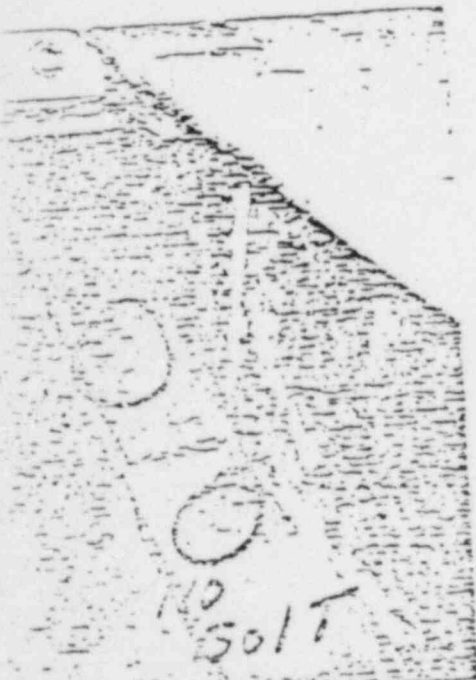
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UNIT I



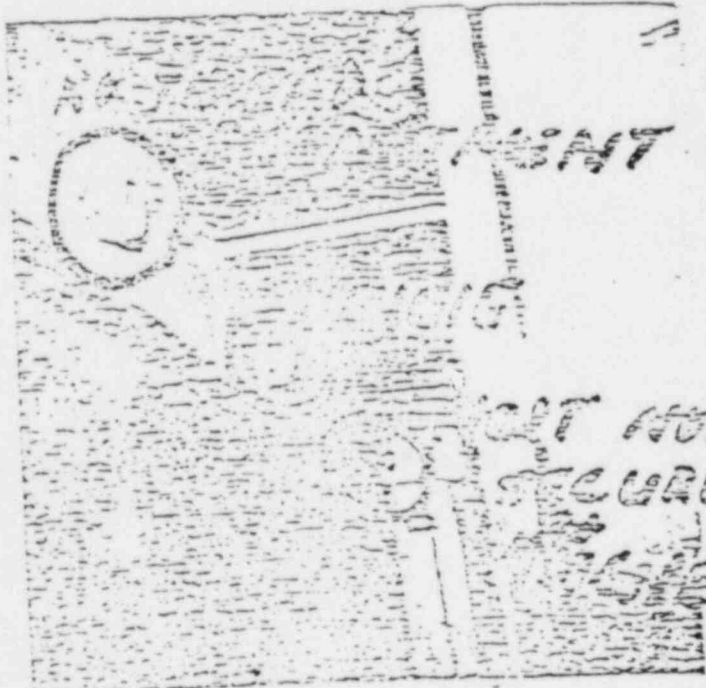
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UNIT II



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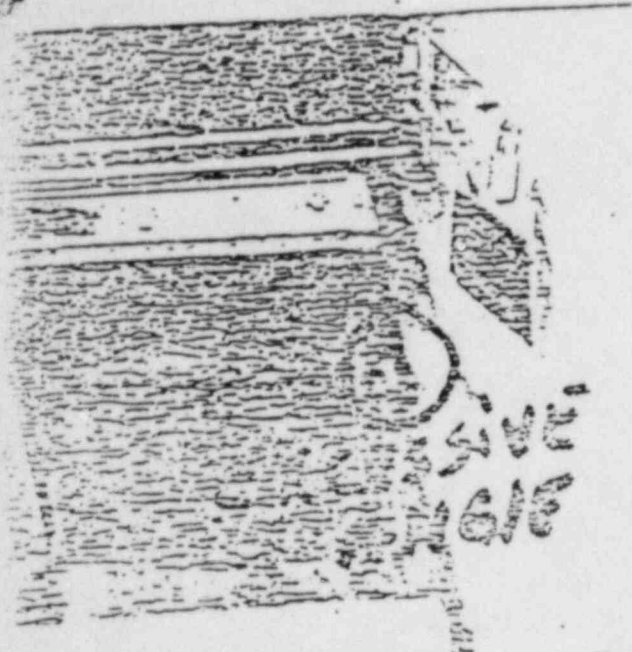
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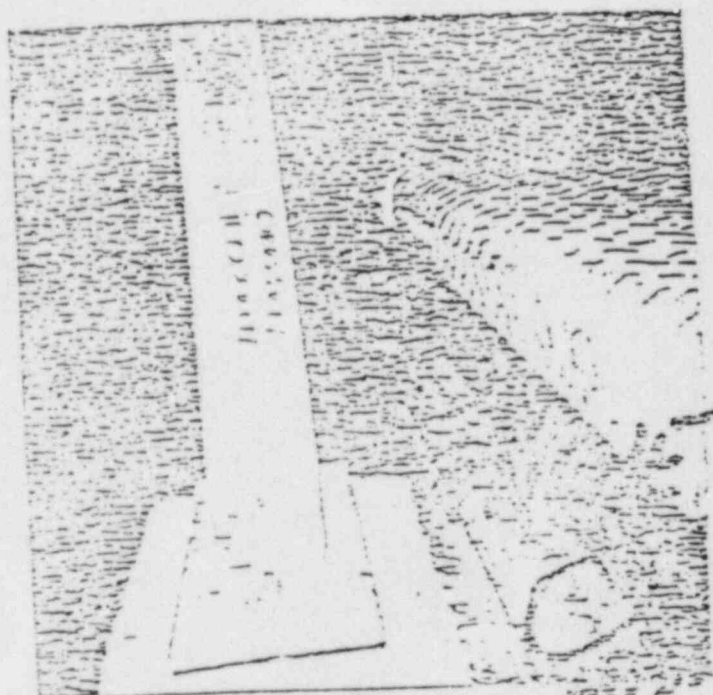
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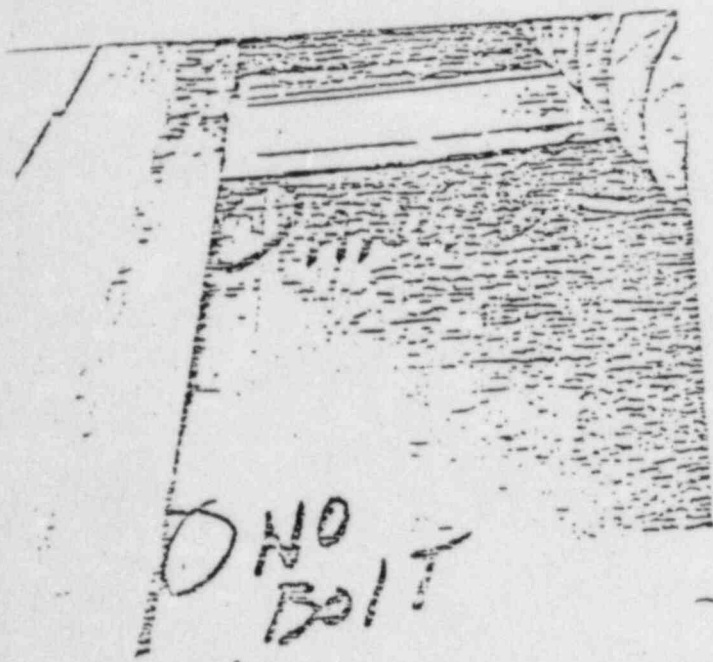
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SN # 006

006

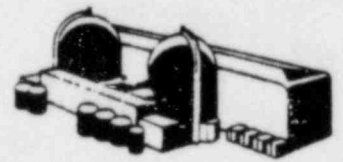


NO
BOLT

SN # 007
u = II

INTEROFFICE MEMORANDUM

Diablo Canyon Project



PACIFIC GAS AND ELECTRIC COMPANY
BECHTEL POWER CORPORATION

To F.M. RUSSELL, GENERAL CONSTRUCTION

Date

From F.A. MORSY

File No. 912

Of ONSITE PROJECT ENGINEERING GROUP

Subject Requested OPEG/CIVIL response
to document # MVR C-1338
UNIT - 1

At JOBSITE Extension (805)595-7351
x3137

SUBJECT:

MVR C-1338

LOCATION:

AREA "H", EL. 128'-3" (CSR)

DRAWING NO.:

59658

DESCRIPTION OF SUBJECT:

SEE MVR C-1338

DATE OF REPLY:

11 JAN. 84

OPEG/CIVIL RESPONSE:

SEE ATTACHED SKETCH

Joe O'Connor

SIGNED

Fathy Morsy

SMF -0605

ENGINEERING DISPOSITION TO MVR NO. C1338

- 1) INSPECT EXPANSION ANCHORS OF PROCESS CONTROL AND PROTECTION PANELS IN ACCORDANCE TO THE FOLLOWING ANCHOR BOLT SCHEDULE:

<u>TOTAL NUMBER OF PANELS / GROUP</u>	<u>TOTAL NUMBER OF ANCHORS REQUIRED FOR EACH SUPPORT BEAM WITHIN 20' OF E.S.</u>
4	10
5	12
6	15
8	19

- 2) ALL EXPANSION ANCHORS MUST BE INSTALLED PER PG&E DWG. NO. 054162.
REV. 3

- (3) WHERE INSUFFICIENT NUMBER OF EXPANSION ANCHORS OR DEFICIENT EXPANSION ANCHORS EXIST, INSTALL NEW ANCHORS PER THE FOLLOWING OPTIONS :

OPTION 1 : REPLACE DEFICIENT ANCHORS AND INSTALL ADDITIONAL ANCHORS AS REQUIRED TO MEET MINIMUM NUMBER PER PG8E DWG. NO. 054162, REV. 3

OPTION 2: INSTALL NEW EXPANSION ANCHORS PER DETAIL "I"
OF DWG. NO. SKJT-EPA-9-1. REV. 0.

[illegible]

COPY

PACIFIC GAS AND ELECTRIC COMPANY

PG&E +

77 BEALE STREET, SAN FRANCISCO, CALIFORNIA 94106

TELEPHONE (415) 781-4211

February 7, 1984

PGandE Letter No: DCL-84-047

Mr. John B. Martin, Regional Administrator
U. S. Nuclear Regulatory Commission, Region V
1450 Maria Lane, Suite 210
Walnut Creek, CA 94596-5368

Re: Docket No. 50-275, OL-DPR-76
Docket No. 50-323
Diablo Canyon Units 1 and 2
Welding in the Cable Spreading Room

Dear Mr. Martin:

As a result of the recent NRC investigations into the allegations listed in SSER 21, the Staff has raised questions regarding the installation of class I equipment on class II material in the cable spreading room. The enclosure to this letter provides the PGandE response to these questions.

Kindly acknowledge receipt of this material on the enclosed copy of this letter and return it in the enclosed addressed envelope.

Sincerely,

J. O. Schuyler

by J. D. Shiffer

Enclosure

cc: T. W. Bishop
D. G. Fleischhut
E. Schierling

8402090256-840207
PDR ADOCK 05000275
E PDR

DIST. RE TEAM LEE

BOO!
1/1

Feb 9 1984 13.

ENCLOSURE

USE OF NON-CLASS I MATERIAL TO SUPPORT
SAFETY-RELATED EQUIPMENT IN THE CABLE SPREADING ROOMS

Background

The NRC has requested additional information based on their review of the use of non-Class I steel to support safety-related equipment in the cable spreading rooms. The information requested is:

1. Show qualification for the materials and installation.
2. Explain why resolution of the problem has not been accomplished in a more timely manner.
3. Why wasn't the problem discovered by the IDVP or the ITP?
4. Address generic implications, including late identification of the issue as a nonconformance.

Resolution

The following discussion provides a response to each question.

1. Show qualification for the materials and installation.

The non-Class I steel beams used in this installation have been tested to determine chemical and physical properties. The steel was found to have ASTM A-36 properties as required by the design drawings. The beam installations and equipment attachments to the beams have been as-built. Calculations have been performed which show qualification of the as-built installation. Refer to Attachment 1 for details.

2. Explain why resolution of the problem has not been accomplished in a more timely manner.

On October 6, 1983, H.P. Foley Company identified to PGandE a concern regarding the adequacy of anchor bolt installations which fix the steel beams in place. This initial concern was broadened to include the issue of non-Class I material in Class I installations. Resolution has required preparation of additional as-built drawings, material removal for testing and analysis, and design reanalysis. Although resolution has taken approximately four months, when considering the complexity of the issue, we find the duration to closure to be reasonable.

3. Why wasn't the problem discovered by the Independent Design Verification Program (IDVP) or the Internal Technical Program (ITP)?

The IDVP was based on a sampling approach. This installation was not included in their sample. However, their review did identify a generic concern for adequacy of equipment supports. As a result of this generic concern, the equipment attached to the cable spreading room platforms was reviewed by the ITP. The welds from the equipment to the steel beams were found to require modification for structural reinforcement. In addition, the design of the cable spreading room platforms was reviewed by the ITP. The design of the

platform consisted of steel beams installed in a grid pattern fixed to the floor by closely spaced anchor bolts. A senior engineer reviewed this design and judged that margin exists in the design such that as-built and detailed reanalysis was not warranted. The steel was specified as ASTM A-36, but no certification was required. Since A-36 is a standard commercial grade steel and no welding problems were apparent, the material was judged adequate. The review described above was completed prior to identification of the NRC questions.

Therefore, this installation was reviewed, weld modifications specified, and the remainder judged adequate by the Diablo Canyon Project. Subsequently, the more detailed January 30, 1984 structural analysis and material testing has confirmed the judgments made in the earlier review. Refer to Question 1 for details.

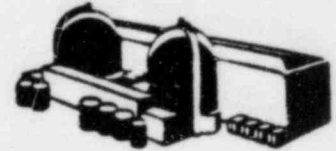
4. Address generic implications, including late identification of the issue as a nonconformance.

The unique nature of the steel-frame raised-floor configuration led to the acceptance of the design and material without the detailed type of as-built and analysis that was performed for the other structures. This type of configuration exists only in the cable spreading rooms. All other platforms which support Class I equipment have been thoroughly analyzed. Therefore, this installation is not a generic issue. The Nonconformance Report (NCR) associated with this issue will be completed by February 17, 1984.

The Project has initiated a separate NCR to assess the adequacy of the steps taken in addressing timely identification of this issue as a nonconformance. This NCR will establish cause, investigate generic implications, determine corrective action to prevent recurrence, and review reportability.

INTEROFFICE MEMORANDUM

Diablo Canyon Project

PACIFIC GAS AND ELECTRIC COMPANY
BECHTEL POWER CORPORATION

To D. Rockwell/M. Leppke

Date January 30, 1984

From J. K. McCall

File No. 52.19

Of Civil Engineering - Unit 1

Subject Supports for Class I
Electrical Panels in the Cable
Spreading Room - El. 127
Unit 1

At 45/23/B35 Extension 8-1414

Reference: Minor Variation Report - MVR No. C-1338
Non-Conformance Report - NCR No. DCL-84-SC-N001

Engineering has evaluated the above referenced reports and following is our engineering disposition:

A. 10WF21 Supporting Beams

1. Structural Evaluation: Based on as-built information from the field and new panel loads furnished by Westinghouse, supporting beams are found to be structurally adequate when subjected to Hosgri/DDE earthquake.
2. Material: Our calculations are based on the material conforming to ASTM A-36 which requires a minimum yield strength of 36ksi. It has been confirmed that the material does meet the requirements of ASTM A-36 by the mechanical and chemical tests performed on coupons taken from the supporting beams. The test report will be available upon request.

Based upon the above information, existing supporting beams are considered acceptable and, therefore, use as is. The portion of the beams where the coupons were taken shall be ground smooth to remove any irregularities and sharp notches. The cut out portion need not be welded back.

B. Concrete Expansion Anchors

Based on as-built information from the field and new panel loads furnished by Westinghouse, all expansion anchors are found to be structurally adequate when subjected to the Hosgri/DDE earthquake. The capacity of expansion anchors are based on the report "Use of Concrete Expansion Anchors at Diablo Canyon" contained in PGandE Letter No. DCL-84-031 which accounts for embedment and angularity. All existing expansion anchors are acceptable and therefore, use as is.

042507

D. Rockwell/M. Lappke

- 2 -

January 30, 1984

For your reference, the calculation number for the above is EPA-9, Rev. 2 and filed in 52.19.

If there are any questions, please call Ali Vanek at Ext. 8-5953.

J. K. McCall
J. K. McCALL

slp
AVanek:slp

Response Required: No.

cc: HFriend
GEMoore
WHWhite
LERosetta
FRussell
FMorsy
WOShah
BSarkar
AVanek
KTawney

[MISC10020]

MINOR VARIATION REPORT

14.

IDENTIFICATION	Location Diablo Canyon	Unit No. I	Reference Spec. No. 8802	Page 1 of 1
Organization PTGC Electrical	Contractor's Report No.		PG&E M.V.R. No. E-2773	
Send Copy to Contractor <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No		Name N/A		

DESCRIPTION OF DISCREPANCY

Class I Electrical Raceway Supports attached to Non-Class I steel
 Explanation
 NRC field inspection has revealed Class I Electrical Raceway Supports attached to the
 Non-Class I steel supporting the diamond plate in the cable spreading room, elevation
 127'. Example: CSR-127-3-634 detail S-415
 CSR-127-3-573 detail S-235

Initiated By *[Signature]* Date January 17, 1984
 DISPOSITION
 Refer to Engineering for disposition.

Additional Concurrence, When Required Name Date
 Senior Site Representative *[Signature]* Date January 17, 1984

REVIEW
 This Minor Variation Report (1) ☒ Is Not Reportable; ☐ May be Reportable (Per Title 10 CFR, Part 21)
 (2) ☒ Is Not a Nonconformance
 Quality Control Date
 Senior Site Representative *[Signature]* Date January 17, 1984

DISPOSITION ACCOMPLISHED

Remarks
 Inspected By Date
 Quality Control Date

☐ ATTACHMENTS

DCM No. C-15 Revision 3
Date March 1, 1983
File No. 52.7.11.2 x 40.2.4

PACIFIC GAS AND ELECTRIC COMPANY

DESIGN CRITERIA MEMORANDUM

Structure, System, or Component: Diablo Canyon PP - Electrical Raceway Supports

Prepared by: Michael K. Yan *Michael K. Yan* Date 3/23/83

Group Leader/Supervisor Review J. K. McCall *J. K. McCall* Date 3/23/83
N. O. Shah (Discipline)
N. O. Shah

Reviewed by Interfacing Disciplines:

Group Leader/Supervisor S. Auer *S. Auer* Date 3-23-83

Electrical Group Leader/Supervisor C. M. Hazari *C. M. Hazari* Date 3/23/83

Group Leader/Supervisor _____ Date _____

Approved by:

Department Chief: R. V. Bettinger *R. V. Bettinger*

Date: 3-31-83

Approved for Project use:

Project Engineer: G. H. Moore
G. V. Cranston *G. V. Cranston*

Date: 4/6/83

Page 2 through 14 attached; describing design inputs. Other attachments as indicated below.
with Attachment A thru H

cc:

☐ Approving Discipline Chief(s)

FOR INFORMATION ONLY

☐ Chief, Engineering Quality Control

☐ Project Engineer

☐ Discipline Group Leader(s)/Supervisor(s)

☐ Manager, Steam Generation

Others _____

DESIGN CRITERIA FOR SEISMIC REVIEW
OF CLASS 1E ELECTRICAL RACEWAY SUPPORTS
AT DIABLO CANYON POWER PLANT

1. Introduction

- A. This set of design criteria is applicable to design review of Class 1E electrical cable tray, conduit and pull box supports at Diablo Canyon Power Plant. Design of conduits, cable trays, pull boxes and other raceway system components is not included. Design of these supports shall be assumed to conform to the configuration and general and special notes shown on PG&E Drawing 050030, Rev.29 (generic condition), except as modified by as-built data.
- B. Loads to be considered are:
- (1) Dead loads of conduits, trays, and weight of insulated copper conductors (see Attachment A -- letter dated 10-29-81 Herrera/Vahlstrom to Bettinger); applicable dead load of support shall also be included.
 - (2) Seismic loads are:
 - a) The current floor response spectra for the Hosgri Earthquake event contained in DCM C-17
 - b) The current floor response spectra of the Double Design Earthquake (DDE) contained in DCM C-30.
- The review shall be based on 7% damped floor response spectra.
- C. In determining the amount of dead load which is tributary to a support, the assumption shall be made that supports are spaced at the maximum allowed by the drawing and that the number of cable trays and conduits allowed by the drawing are present on the support (generic condition), unless as-built data indicates otherwise.

2. Seismic Response Calculation

- A. Response acceleration in horizontal direction

Total response acceleration in either north-south or east-west horizontal direction shall be computed as follows:

For north-south horizontal motion:

$$A_T^{NS} = A^{NS} + \phi^{NS} \cdot X/g$$

For east-west horizontal motion:

$$A_T^{EW} = A^{EW} + \phi^{EW} \cdot Y/g$$

where:

A_T^{NS} = Total north-south response acceleration

A_T^{EW} = Total east-west response acceleration

A^{NS} = Translational spectral acceleration due to north-south ground motion

A^{EW} = Translational spectral acceleration due to east-west ground motion

ϕ^{NS} = Torsional spectral acceleration due to north-south ground motion

ϕ^{EW} = Torsional spectral acceleration due to east-west ground motion

X = East-west distance from center of mass

Y = North-south distance from center of mass

g = Gravitational constant

Separate calculations of A_T shall be made for Blume and for Newmark spectra. The greater of these shall be used in subsequent calculation of seismic loads.

The above method of calculating response acceleration including effects of structure torsional acceleration is applicable only to structures for which torsional response spectra have been provided. (Torsional effects of Hosgri Earthquake in the Turbine Building have been included in the translational response spectra for that building)

B. Response acceleration in vertical direction

(1) The vertical response acceleration for Hosgri Earthquake shall be obtained from the vertical response spectra in DCM C-17.

(2) The vertical response acceleration for DDE shall be 0.36g. | 3

C. Transverse Seismic Loading

In determining the transverse seismic loading on an electrical raceway support, the more severe of the two horizontal acceleration components described in Sec. 2A shall be assumed acting transverse to the raceway support unless the support is being evaluated based on as-built conditions, in which case, the appropriate horizontal component may be used.

D. Longitudinal Seismic Loading

(1) In the longitudinal direction, conduits and supports shall be considered as systems. The systems shall be analyzed in one of the two ways.

(a) For systems that have a first mode frequency in the longitudinal direction of not less than 33 Hz, equivalent static analysis is used. The total seismic load in the longitudinal direction is calculated using the zero period acceleration (ZPA) of the appropriate floor response spectra. The total seismic load is distributed among the supports proportionally to their longitudinal stiffnesses.

(b) Alternatively, dynamic analysis is used to determine seismic load on each support of the system from the appropriate floor response spectrum applied in the longitudinal direction.

(2) Cable trays have been provided with separate longitudinal supports and do not require seismic review of transverse-type supports in the longitudinal direction. The longitudinal-type seismic tray supports shall be reviewed for their tributary longitudinal spans.

E. In determining the spectral acceleration, the spectral ordinate corresponding to the calculated natural period of the raceway support shall be used with the following exception:

If the support is being evaluated for its generic condition and if the calculated natural period is greater than the period corresponding to 75% of the peak, the peak value shall be used. See Figure 1

F. Wherever more than one set of response spectra at a particular floor level has been provided, the spectra located closest to the support location shall be used (without interpolating).

G. Interpolating between the spectra at different floor levels to derive spectra at intermediate elevations is permissible and shall be done in accordance with DCM C-17 and DCM C-30.

H. For floor response spectra at Elevation 85' or below, ground response spectra shall be used (see Hosgri Evaluation Report).

3. Load Combinations

All raceway supports shall be evaluated for the transverse seismic loading and the longitudinal seismic loading separately. For each seismic loading condition, the load combination shall be as follows:

Maximum stress or member force at each critical location in the support shall be calculated, separately, for seismic loads in the maximum horizontal direction and in the vertical direction. The resulting stresses or member forces due to loads in the maximum horizontal direction shall be combined with the stresses or member forces due to vertical loads by absolute sum. Stress or member force due to dead loads shall be added to the results described above to get total stress/force.

The above paragraph may be expressed symbolically, thus:

$$U = D + DA_H (\text{max hor}) + DA_V$$

where: D = Stress due to dead load of applicable support weight plus tributary weight of raceways spans adjacent to the support.

DA_V = Absolute stress due to applicable vertical seismic load.

DA_H = Absolute stress due to applicable horizontal seismic load.

U = Total stress due to seismic loads in horizontal and vertical directions, and dead load.

4. Design Specification

Applicable design specifications for this purpose, adapted to reflect the approach described above, are:

- A. For hot-rolled steel members, AISC 1969 Specification for the Design, Fabrication and Erection of Structural Steel for Buildings.
- B. For cold-formed steel members, AISI Specification of Design of Cold-Formed Steel Structural Members, 1968 edition.

5. Material Properties

- A. Structural steel (ASTM A-36) used in these raceway supports has a yield point of 36 ksi.
- B. Cold formed steel (ASTM A570, Grade 33) used in these raceway supports has an average yield point, F_{ya} , as shown in Table A for each cold-formed channel section. Virgin yield point, F_y , is 33 ksi. Ultimate strength, F_{ult} is 52 ksi.

- C. Concrete strength, based on test reports, varies throughout the plant. When applying acceptance criteria, the designer shall use the applicable concrete strength as shown in Attachment E (Table 4-3 of the Hosgri Evaluation Report).

6. Acceptance Criteria

- A. Member stress shall not exceed the following acceptance criteria.

- (1) Acceptance criteria for hot-rolled steel members.

The provisions of Part 1 of the AISC Specification for the Design Fabrication and Erection of structural steel for Buildings are applicable with the following modification: allowable stresses may be increased by 60% for acceptance limits applicable to load combinations which include seismic. Reference: NRC Standard Review Plan Sec. 3.8.4.

Minor local yielding may be permitted if it can be demonstrated that local yielding does not affect the member strength or its function.

- (2) Acceptance criteria for cold-formed steel members

- (a) Bending about major axis (ksi)

$$F_b = F_{ya} - \frac{F_{ya}^2}{4.05\pi^2 EC_b} \cdot \frac{L^2}{d} \cdot \frac{S_{xc}}{I_{yc}}$$

where: F_{ya} = average yield point, ksi
(see Table A)
 E = elastic modulus, ksi
 C_b = bending coefficient; conservatively
 $C_b = 1.0$ (see AISI Sec. 3.3)
 d = section depth, inches
 L = unbraced length, inches
 S_{xc} = compression-side section modulus of
entire section about centroidal axis
perpendicular to loading plane,
inches³
 I_{yc} = moment of inertia of compression
portion of section about its
centroidal axis parallel to the
loading plane, inches⁴

For particular Unistrut (or equivalent) profiles, the above formula reduces to: | 3

$$P1000, F_b = 41 - .0028 L^2$$

$$P1001, F_b = 41 - .0010 L^2$$

$$P3300, F_b = 45 - .0096 L^2$$

$$P5000, F_b = 33 - .0011 L^2 \text{ See Note}$$

$$P5001, F_b = 33 - .0008 L^2 \text{ See Note}$$

$$P5500, F_b = 39 - .0012 L^2$$

$$P5501, F_b = 39 - .0009 L^2$$

NOTE: When Unistrut P5000 and P5001 or their equivalents are used as beams, the acceptance limits shown above have been reduced by 12.5% to avoid local buckling of the compression flange.

Conduits and cable trays which are attached to cold-formed channel members and are continuous across the support may be considered as lateral bracing of the member.

(b) Bending about minor axis (ksi)

$$F_b = F_{ya}$$

(c) Shear (ksi)

$$F_v = 0.6 F_y$$

NOTE: Use F_y here, not F_{ya} .

(d) Axial tension (ksi)

$$F_t = F_{ya} \text{ on net section}$$

(e) Axial compression (pounds)

Refer: Column Load Table, Unistrut General Engineering Catalog No. 9 (1978 edition), page 120, and Super Strut Framing Channel and Pipe Hangers Catalog No. 3 - Revision 3, Table III. (See AISC Steel Manual, Table C1.8.1, for advice on selecting K values.)

$$\text{If } \frac{KL}{r_{\min}} \leq 118, P_a = 1.33 \times \text{Column Load in Table}$$

HISTORY OF CONTROLLED DOCUMENT
DISTRIBUTION FOR P-149, P-126, B-75

12/15/83

<u>DOCUMENTS</u>	<u>ISSUED</u>	<u>RETURN RECEIPT REC'D</u>
P-149, P-126		
Rev 8	8/83	9/1/83
Rev 9	11/18	Not Returned As of Yet
 B-75		
M 46 - 1	4/15	4/28
Complete manual	4/21	5/2
w/o criteria		
M 42 - 4	4/25	4/28
M 46 - 2	5/18	6/1
M 46 - 3	6/2	6/7
M 46 - 4	8/15	8/18
M 46 - 5	10/3	10/7
M 46 - 6	11/1	11/8
M 58 - 0	5/2	5/10
M 58 - 1	6/20	7/29
M 58 - 2	8/3	8/5
M 58 - 3	8/24	8/29
M 58 - 4	9/20	9/27
M 58 - 5	10/20	10/28
P 11 -4	5/26	6/1
P 11 - 5	8/31	9/6
P 11 - 6	10/20	11/8
P 33 - 0	5/23	6/1
P 33 - 1	7/7	7/15
P 34 - 0	7/26	8/5
P 27 - 3	10/20	11/8

B - 75 CONTINUED

	<u>ISSUED</u>	<u>RETURN RECEIPT REC'D</u>
I 29 - 1	9/15	9/22
I 41 - 0	7/1	7/12
I 42 - 0	7/1	7/12
I 42 - 1	9/30	10/5
I 50 - 0	8/2	8/5
I 50 - 1	8/12	8/18
I 50 - 2	8/23	8/30
I 50 - 3	9/28	10/6
I 50 - 4	10/27	10/30

If $\frac{KL}{r_{min}} > 118$, $P_a = 1.0 \times \text{Column Load in Table}$

$\frac{KL}{r_{min}}$ shall not exceed 200

- B. Acceptance limit stress on fillet welds on cold-formed steel members shall be 60% greater than given in Section 4.2.1 of AISI specification of Design of Cold-Formed Steel Structural Members. Effective size of a fillet weld shall not exceed the thickness of the thinnest element to which the weld is applied.

- C. When axial and flexural stresses occur simultaneously at a critical location in a cold-formed steel member, the following interaction formula is applicable:

$$p_a/P_a + f_b/F_b \leq 1.0$$

where p_a is the calculated axial load, f_b is the calculated flexural stress, P_a is the acceptance limit axial load, and F_b is the acceptance limit flexural stress.

- D. Loads on Unistrut (or equivalent) bolts shall not exceed 90% of the proof loads (i.e., shall not exceed 2.7 times manufacturer's allowable loads). Interaction of pullout and slip loads shall be evaluated by the following formula:

$$P \leq (P_u/S_u) (S_u^2 - S^2)^{\frac{1}{2}} \quad \text{Ref. Commentary on AISC Spec. 1.6.3}$$

where: P , S are interaction limit values of pullout and slip loads, respectively, for load combinations including seismic. P_u , S_u are three times manufacturer's allowable pullout and slip loads, respectively.

Neither P nor S shall individually exceed 2.7 times manufacturer's allowable load. For load combinations not including seismic, P_u , S_u shall be 1.0 times manufacturer's allowable loads.

- E. Loads on Unistrut (or equivalent) concrete inserts shall not exceed 2.7 times manufacturer's allowable loads in pullout or slip. For evaluating interaction of pullout and slip, use same formula as for Unistrut bolts, above.

- F. Design loads for Unistrut (or equivalent) channel connections shall not exceed 2.25 times the manufacturer's allowable loads.

- G. Loads on Unitstrut (or equivalent) conduit clamps shall not exceed the values shown in Table B.
- H. Loads on concrete expansion anchors shall not exceed twice the allowable pullout and shear loads specified in PG&E Engineering Standard Drawing 054162 - Rev. 3. Interaction of pullout and shear loads shall be evaluated according to Section A2.9 of Dwg 054162.
- I. If a support detail shows loads applied in such a way that more severe stress conditions would occur if the loads were shifted to another location on the support, the designer should check as-built conditions unless the worst position of loads can be accommodated. See Figure 2.
- J. Vertical supports using vertical rods are not horizontal seismic supports.
- K. Unbraced joints made of angle fittings (e.g. P1331, P2626) shall be checked for rotation and fatigue resistance. No checking is necessary for a braced joint. See Figure 3.

The Moment versus Rotation curve and The Fatigue Curves of various combination of angle fittings have been derived from test data and are provided in Attachment G and H respectively. | 3

The fatigue resistance of an angle fitting shall be checked with the following equation:

$$\frac{5n_{EQ}}{N_{DE}} + \frac{n_{EQ}}{N_{HOSGRI}} \leq 1.0 \quad \text{Ref. IEEE Standard 344-1975}$$

or

$$\frac{5n_{EQ}}{N_{DE}} + \frac{n_{EQ}}{N_{DDE}} \leq 1.0$$

where: n_{EQ} = total number of load/stress cycle per earthquake
 $n_{EQ} = 10$ Ref: NRC Standard Review Plan Sec. 3.7.3.

N_{DE} = allowable number of load/stress cycles per DE event

N_{HOSGRI} = allowable number of load/stress cycles per HOSGRI event

N_{DDE} = allowable number of load/stress cycles per DDE event

7. Evaluation Procedures

Step No. 1

1. Use spectra with appropriate damping given in Section 1.
2. Use acceptance criteria given in Section 6.
3. Use weights cited in Attachment A.
4. Compute R, ratio of acceptance criterion to corresponding computed stress or force, for each critical location in the support assembly.
5. If any R-value is less than 1.0, go to Step No. 2.

Step No. 2.

1. Use spectra with appropriate damping given in Section 1.
2. Use acceptance criteria given in Section 6.
3. Use as-built data obtained from field (General Construction Department).
4. Compute R for each critical location in the support assembly.
5. If any R-value is less than 1.0, go to Step No. 3

Step No. 3

1. Provide design modification.
2. Repeat Step No. 2 on as-modified configuration.

Table A
AVERAGE YIELD STRENGTH
OF COLD-FORMED STEEL MEMBERS
BASED ON AISI SPECIFICATION, SEC. 3.1.1

<u>UNISTRUT</u>	<u>F_{ya} (ksi)</u>
P1000	41
P1001	41
P3300	45
P5000	38
P5001	38
P5500	39
P5501	39

TABLE B
UNISTRUT CLAMPS - ACCEPTANCE LIMITS
Reference: Unistrut Corp. Test Reports C-13-H, C-36-A
(dated 10-6-77 and 5-13-77, respectively).
Limits shown are 90% of test ultimate loads (pounds)

CONDUIT SIZE	PIPE CLAMP NO.	PULL OUT	TRANSVERSE SLIP	LONG. SLIP
1/2"	P-1111B	1620	315	180
3/4"	P-1112B	2340	335	315
1"	P-1113B	2585	605	560
1-1/4"	P-1114B	2160	405	315
1-1/2"	P-1115B	3150	380	270
2"	P-1117B	3780	470	270
2-1/2"	P-1118B	3510	855	495
3"	P-1119B	3780	945	875
3-1/2"	P-1120	4725	990	920
4"	P-1121	5355	1665	1485
5"	P-1123	4455	855	630
6"	P-1124	4320	1190	830

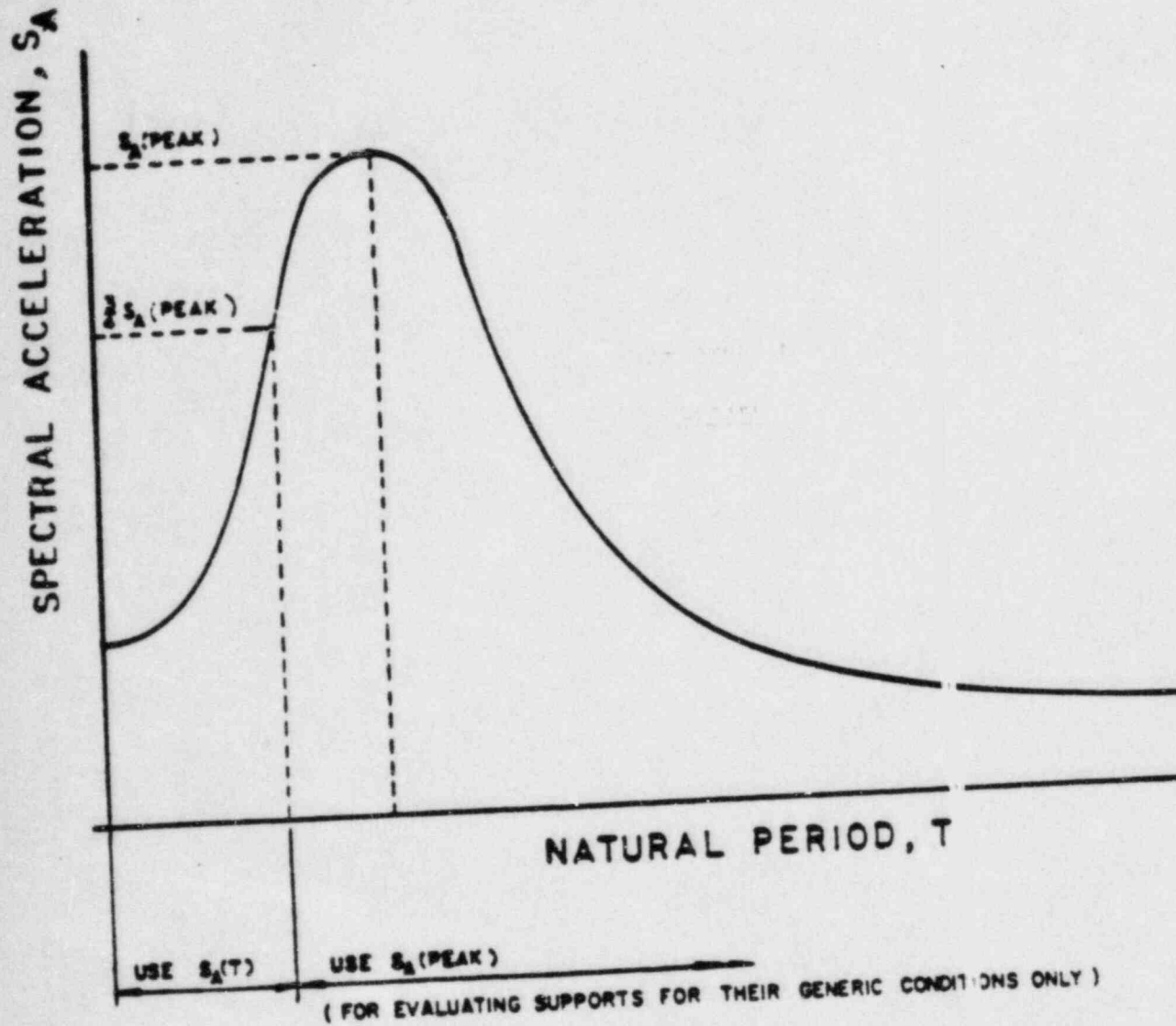
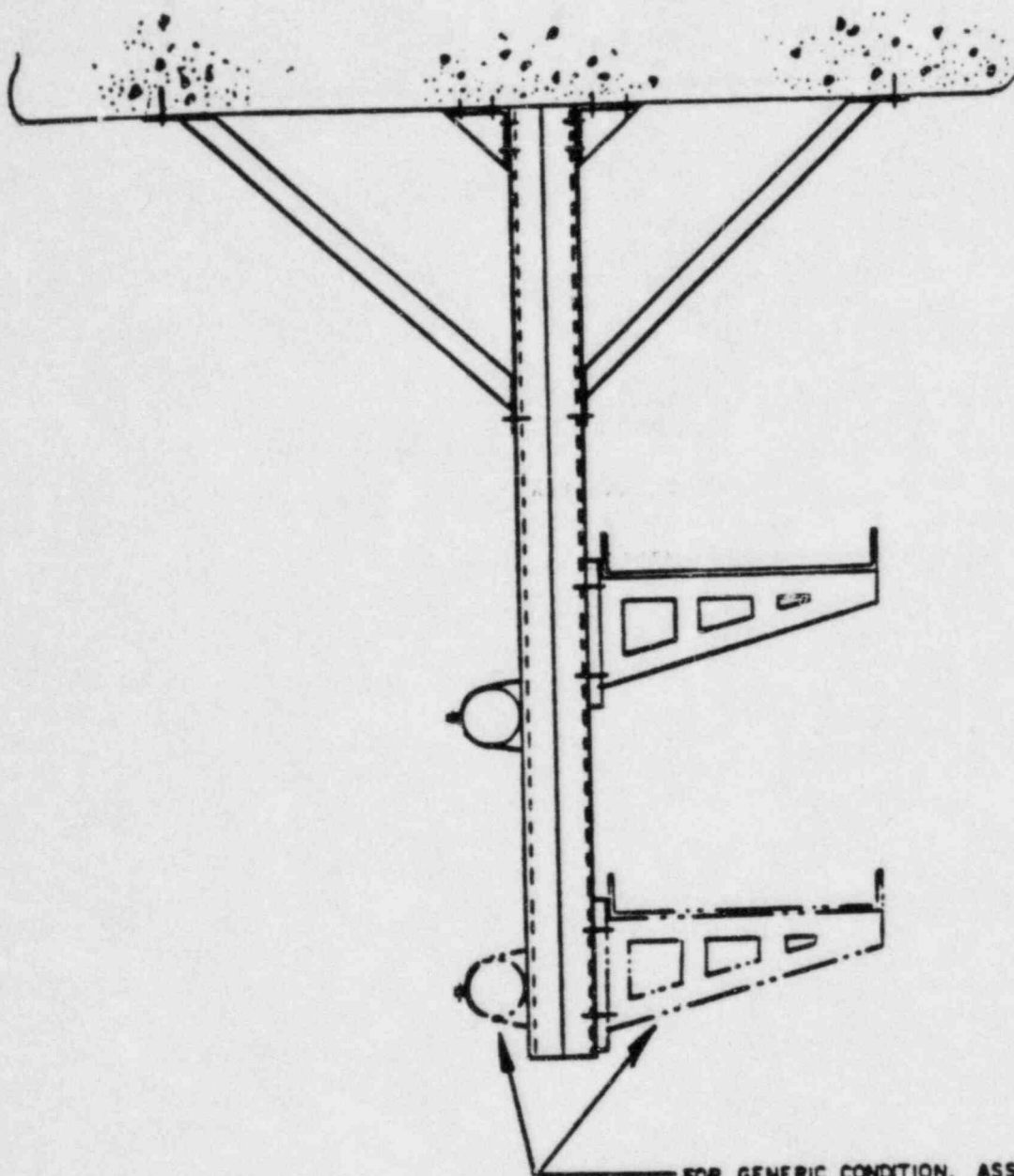
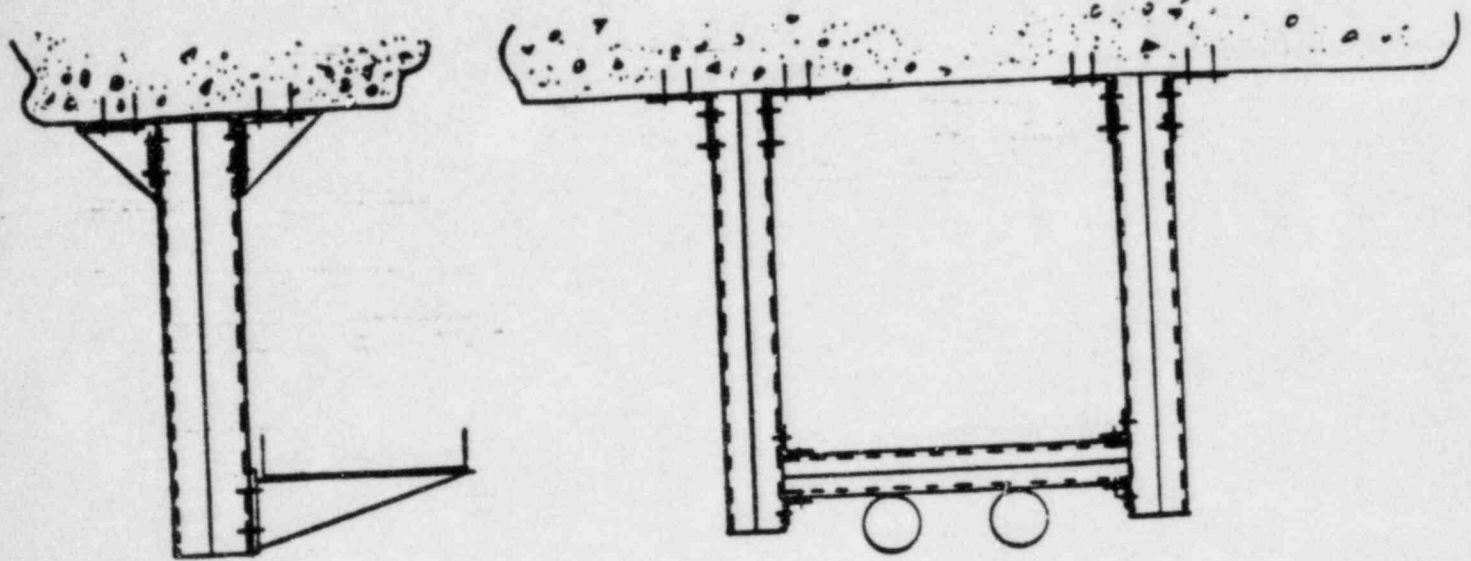


FIGURE 1

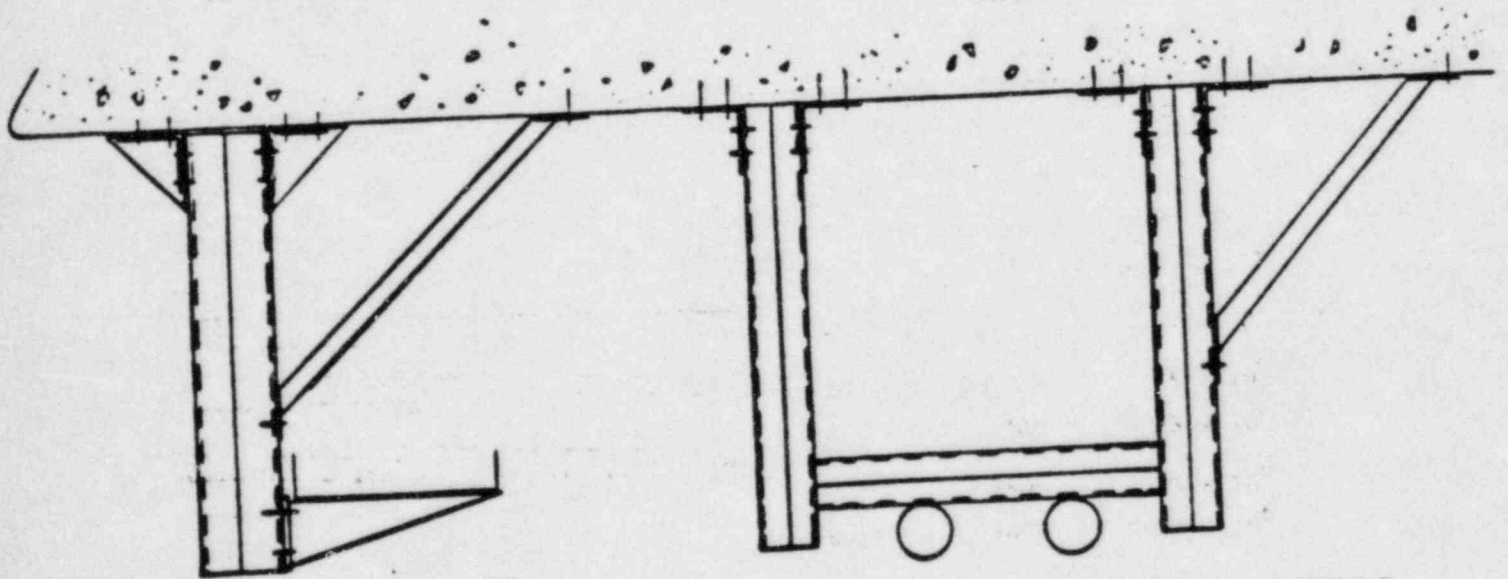


FOR GENERIC CONDITION, ASSUME RACEWAYS ARE
LOCATED IN POSITIONS THAT GIVE MAX. STRESS
UNLESS AS BUILT CONDITION INDICATED
OTHERWISE

FIGURE 2



EXAMPLES OF SUPPORTS THAT REQUIRE CHECKING FOR JOINT ROTATION AND FATIGUE.



EXAMPLES OF SUPPORTS THAT DO NOT REQUIRE CHECKING FOR JOINT ROTATION AND FATIGUE

FIGURE 3

ATTACHMENT

DCM C-15
Rev. 3

PG-E

FOR INTRA-COMPANY USE

A

From Division of
Department ELECTRICAL ENGINEERING

FILE NO.

RE LETTER OF

SUBJECT Diablo Canyon
Cable Tray & Conduit Weights

To Division of
Department

October 29, 1981

MR. R. V. BETTINGER:

Here are weights which should be used in designing supports for cable trays and conduits:

CONDUIT

Size (Dia. in.)	1/2	3/4	1	1-1/4	1-1/2	2	2-1/2	3	4	5	6
Wt (lbs/ft)	1.0	1.4	2.1	3.1	4.1	6.0	8.6	12.5	19.0	28.1	39.7

TRAY

Size (Width, in.)	6	9	12	18	24
Wt (lbs/ft)	12.5	18.8	25.0	37.5	50.0

These weights are based on the following considerations:

Conduit

- assumed to be filled to the maximum (42% by area) with insulated copper conductors.
- conduit assumed to be rigid iron.

Cable Tray

- tray assumed to be NEMA Class II (3 inches high).
- filled weights assumed to be 25 pounds per square foot of tray bottom. These weights are approximately equal to values calculated assuming maximum fill (32% by area) of insulated copper conductors.

General

- these weights will provide very conservative values since average actual weights are about 30% less.

J. R. HERRERA

By W. Vahlstrom
W. VAHLSTROM

WV(1214):ds
cc: JWCowell, FJDan

ATTACHMENT B

DELETED

ATTACHMENT C

DELETED

ATTACHMENT D

DELETED

TABLE 4-3

Average Concrete Strength and Modulus of Elasticity

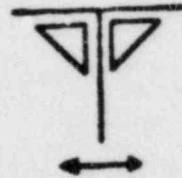
<u>Structure and Component</u>	<u>Concrete Mix*</u>	<u>Average f_c^1 (test value) (psi)</u>	<u>E_c (psi)</u>
Containment Structure			
Base Slab to Elevation 87'	A	6330	4.53×10^6
Skin Pour at Elevation 89'	A	6330	4.53×10^6
Interior	A	6330	4.53×10^6
Skin Pour	B	3850	3.54×10^6
Soldier Beams	B	3850	3.54×10^6
Exterior Walls	B	3850	3.54×10^6
Dome	B	3850	3.54×10^6
Auxiliary Building			
Skin Pour	B	3920	3.57×10^6
Walls and Slabs Below Elevation 85'	B	3920	3.57×10^6
Slabs 4 Feet and Thicker at Elevation 85'	B	3920	3.57×10^6
Columns Below Elevation 85'	C	5650	4.28×10^6
Walls and Slabs Above Elevation 85'	C	5650	4.28×10^6
Slabs Less Than 4 Feet Thick at Elevation 85'	C	5650	4.28×10^6
Columns Above Elevation 85'	C	5650	4.28×10^6
East Walls Above Elevation 115'	C	5650	4.28×10^6
Other Exposed Walls	C	5650	4.28×10^6
Exterior Slabs at Elevation 140'	C	5650	4.28×10^6
Other Roof Slabs	C	5650	4.28×10^6
Turbine Building			
Slab at Elevation 140'	A	6590	4.63×10^6
Skin Pour	B	3870	3.55×10^6
Slabs Except at Elevation 140', Columns and Pedestal	B	3870	3.55×10^6
Exterior Walls Above Elevation 85'	B	3870	3.55×10^6
Except Shear Wall Along Line (1) & (35)	B	3870	3.55×10^6
Shear Wall Along Line (1) and (35)	C	5500	4.23×10^6
Shear Walls Along Lines (5), (17), (19), and (31)	C	5500	4.23×10^6
Remainder	B	3870	3.55×10^6
Intake Structure			
	B	3630	3.43×10^6

*Reference 1

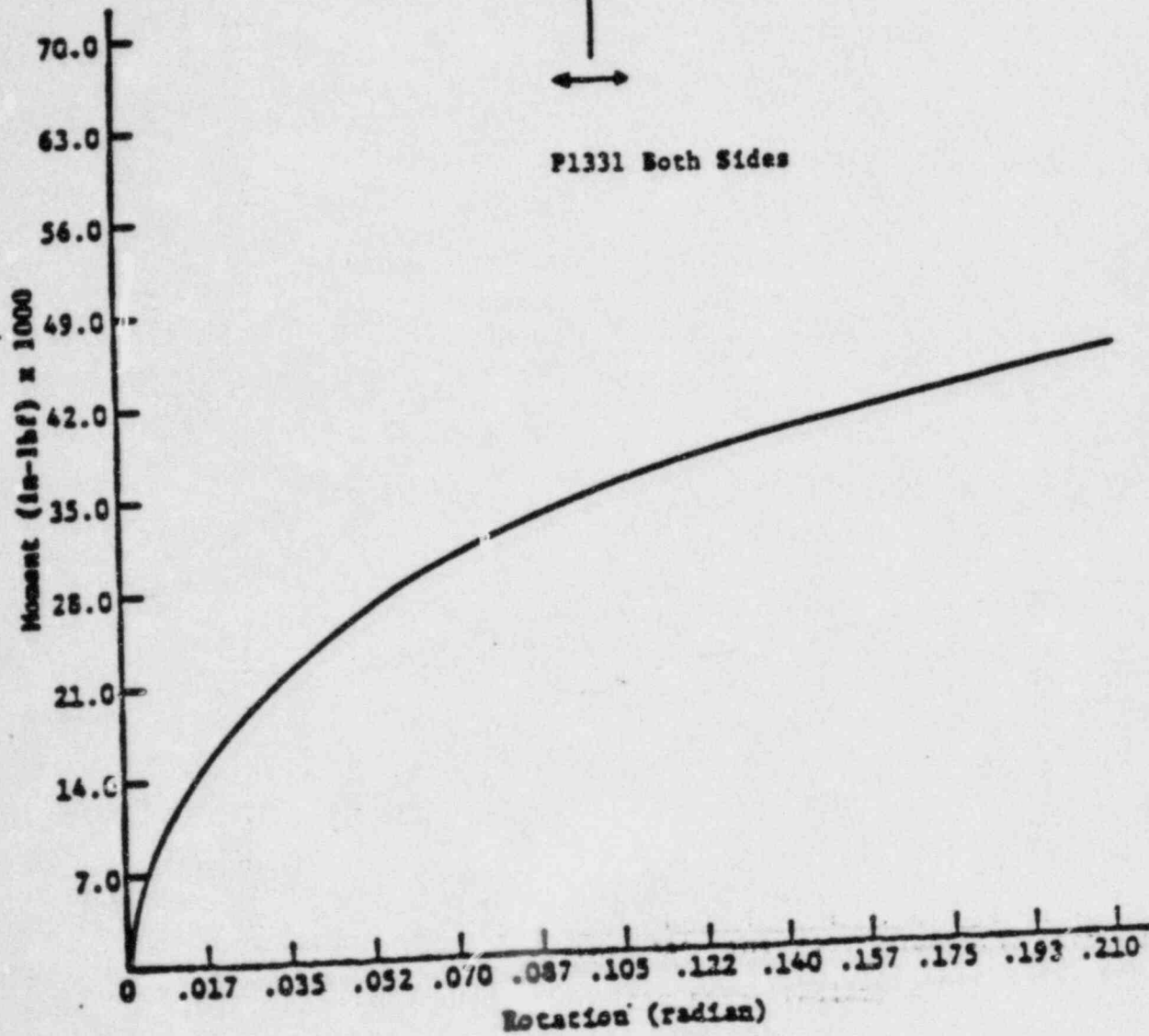
ATTACHMENT F

DELETED

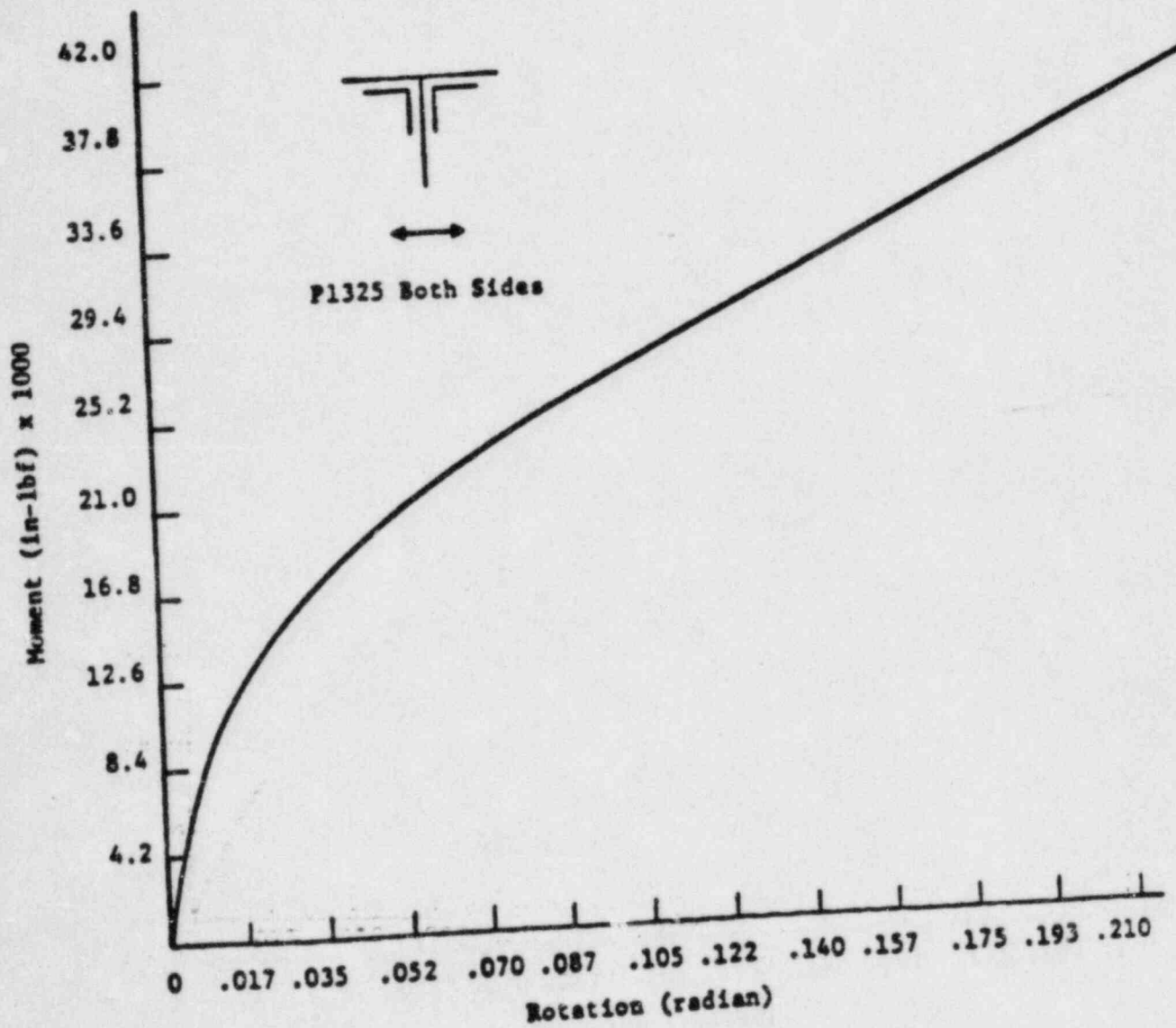
Attachment G.
Moment Versus Rotation



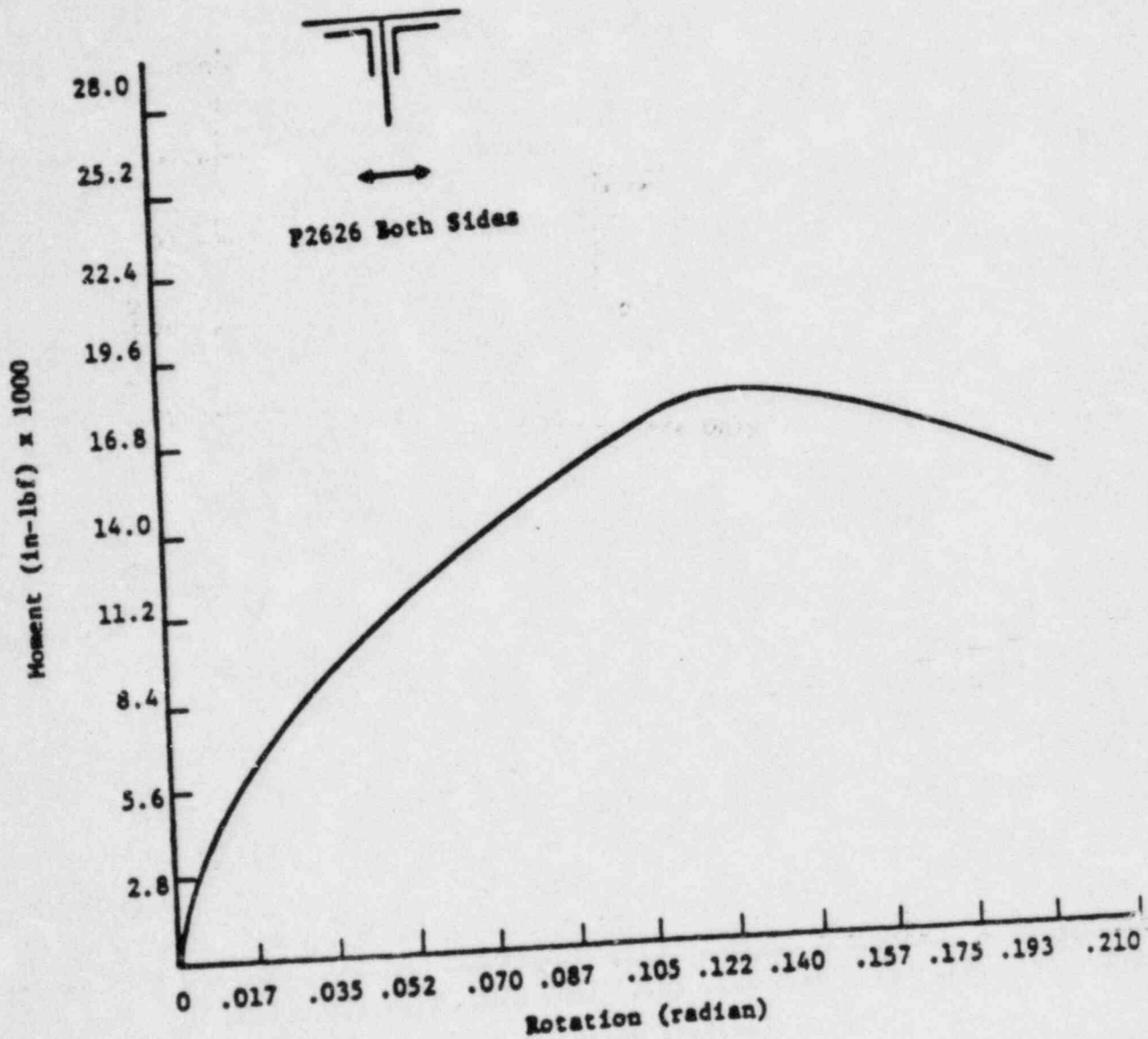
P1331 Both Sides



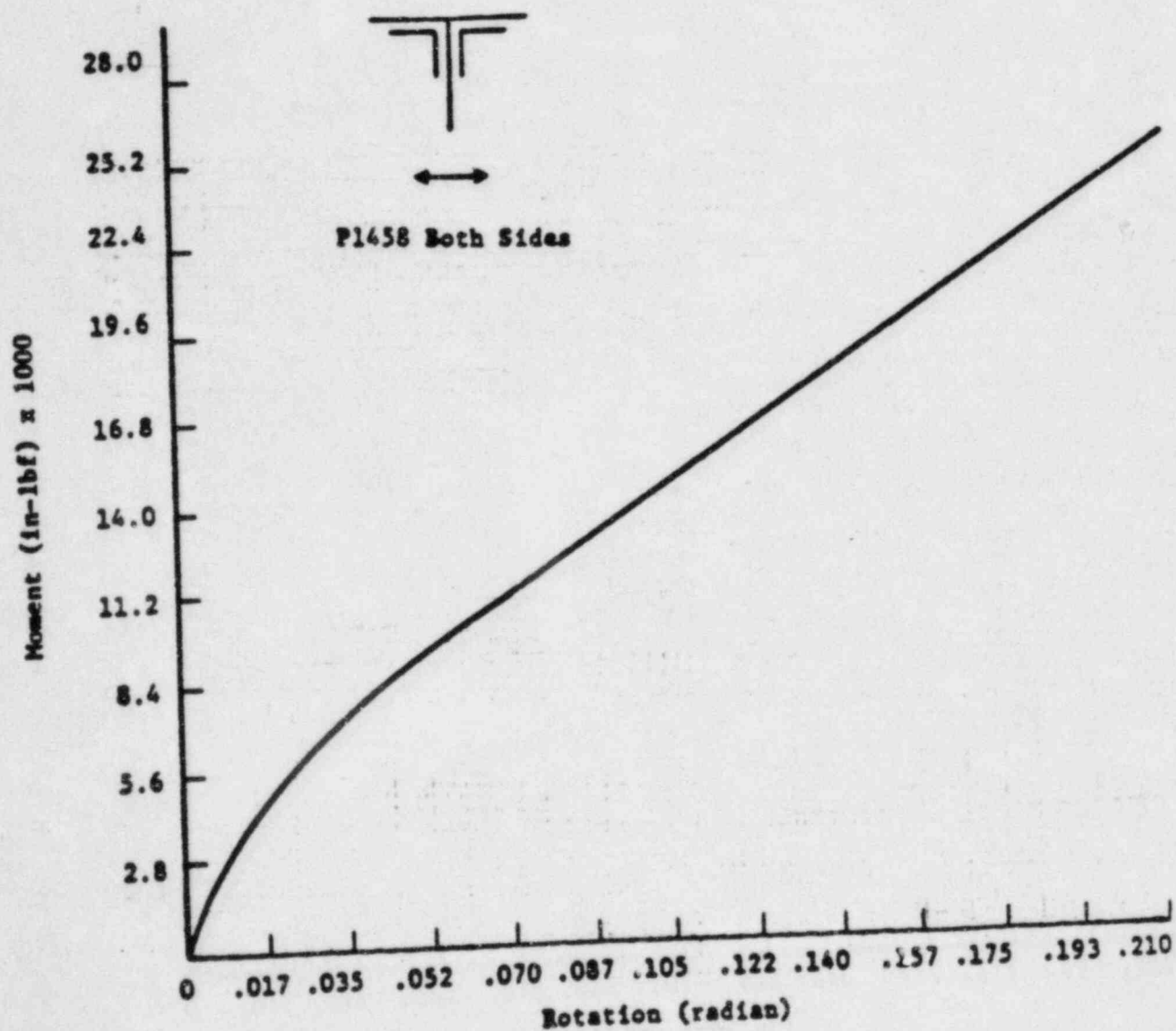
Attachment G.
Moment Versus Rotation



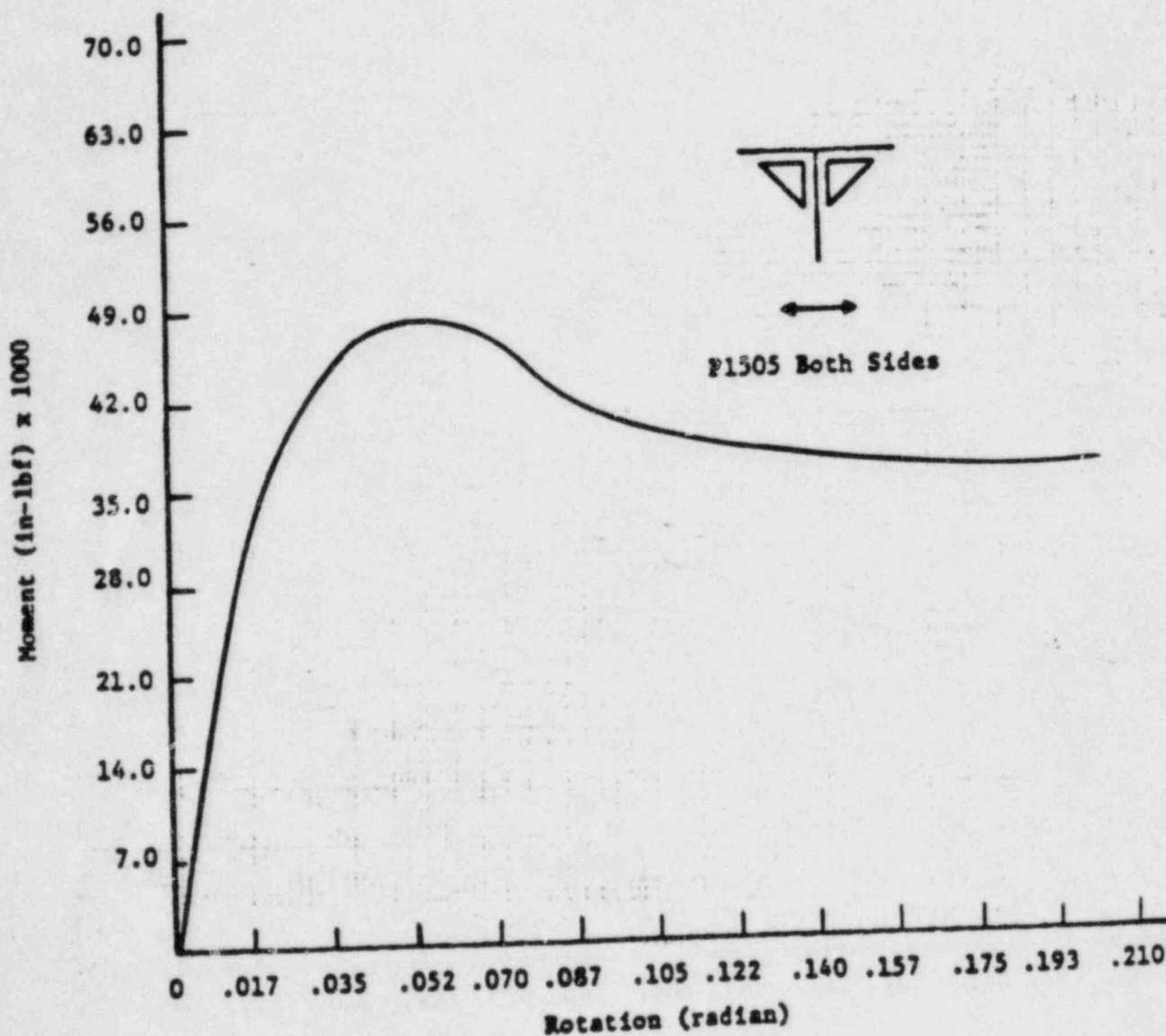
Attachment G.
Moment Versus Rotation



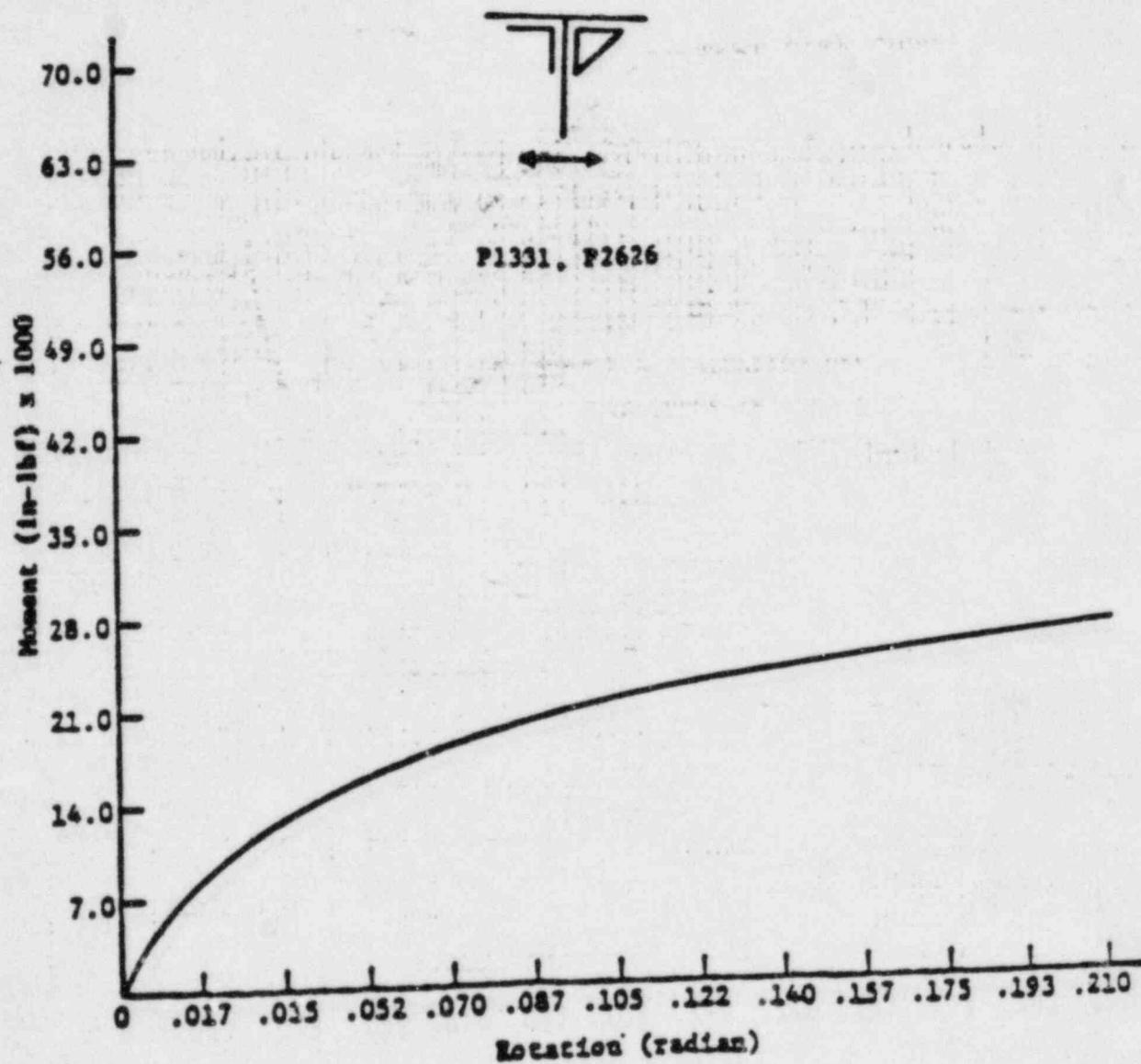
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Moment Versus Rotation



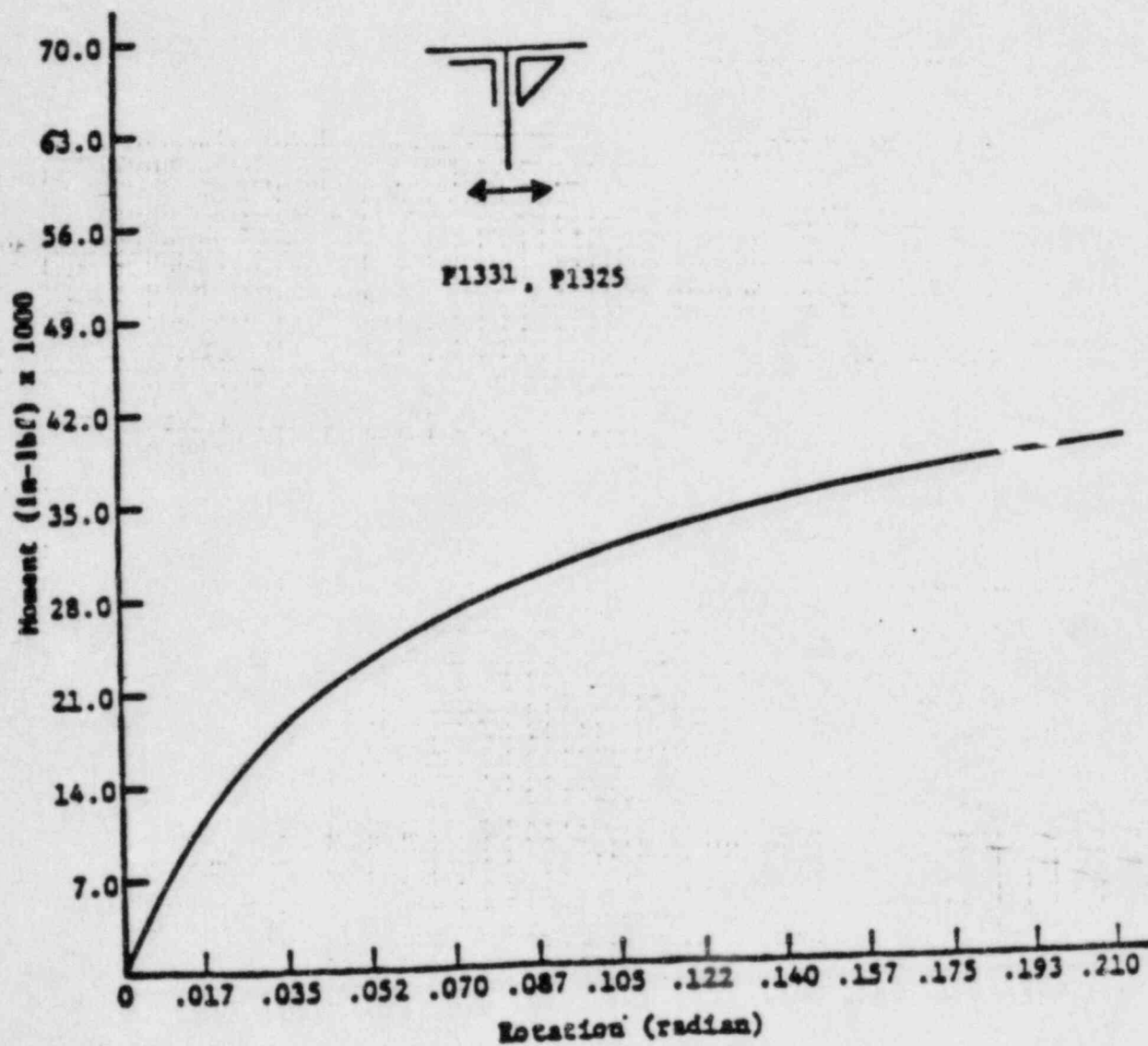
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Moment Versus Rotation



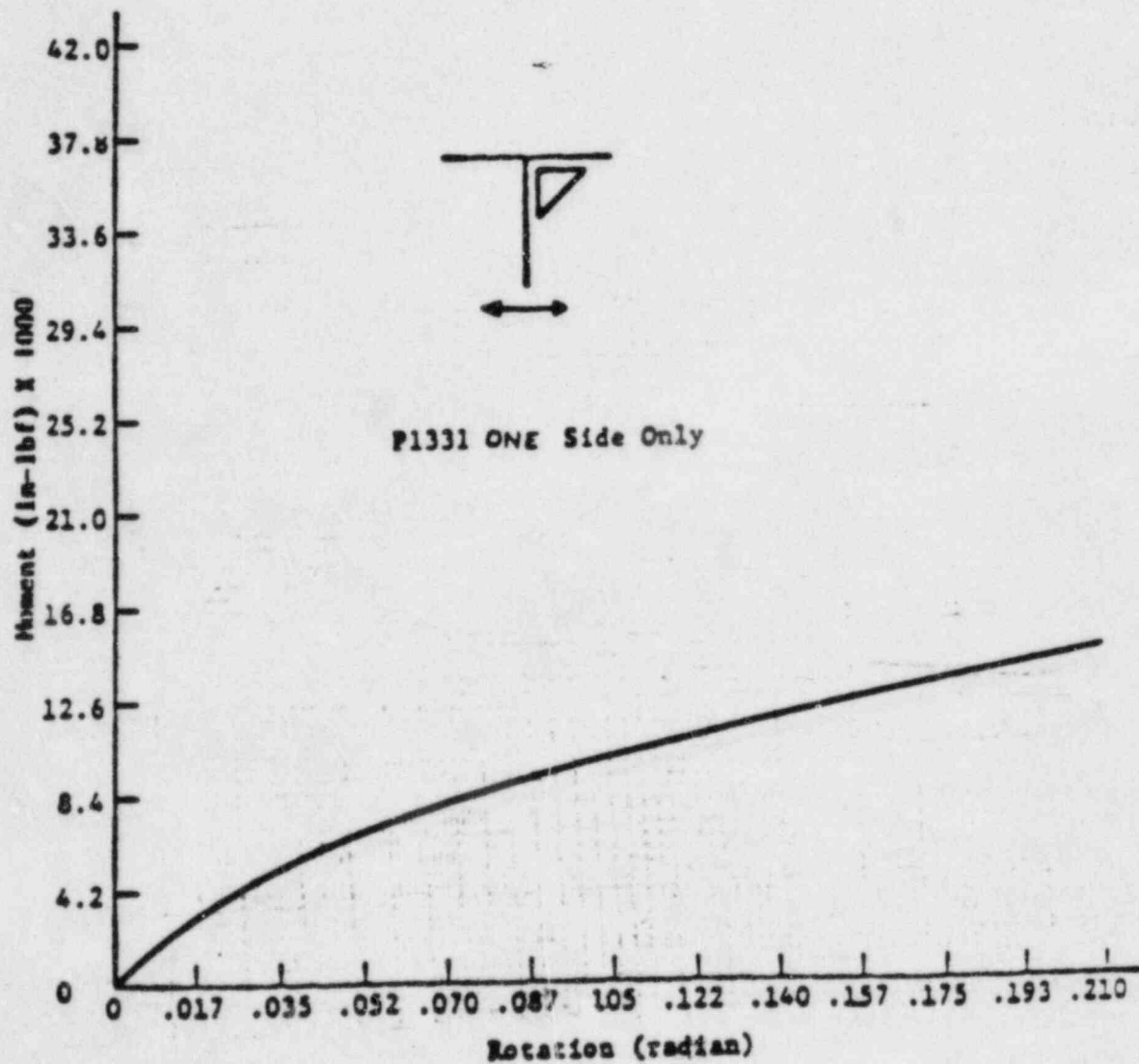
Attachment G.
Moment Versus Rotation



Attachment C.
Moment Versus Rotation

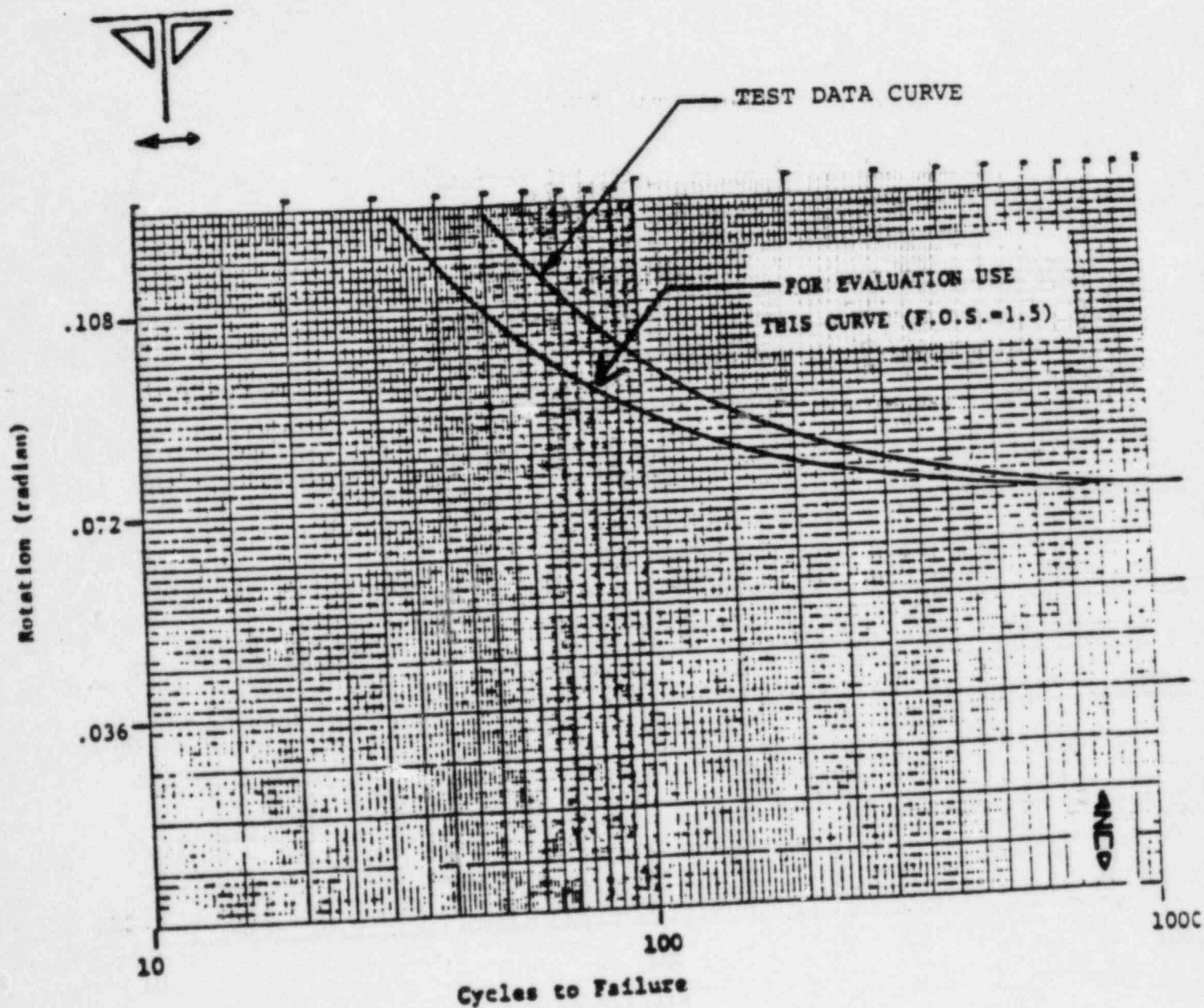


Attachment G.
Moment Versus Rotation



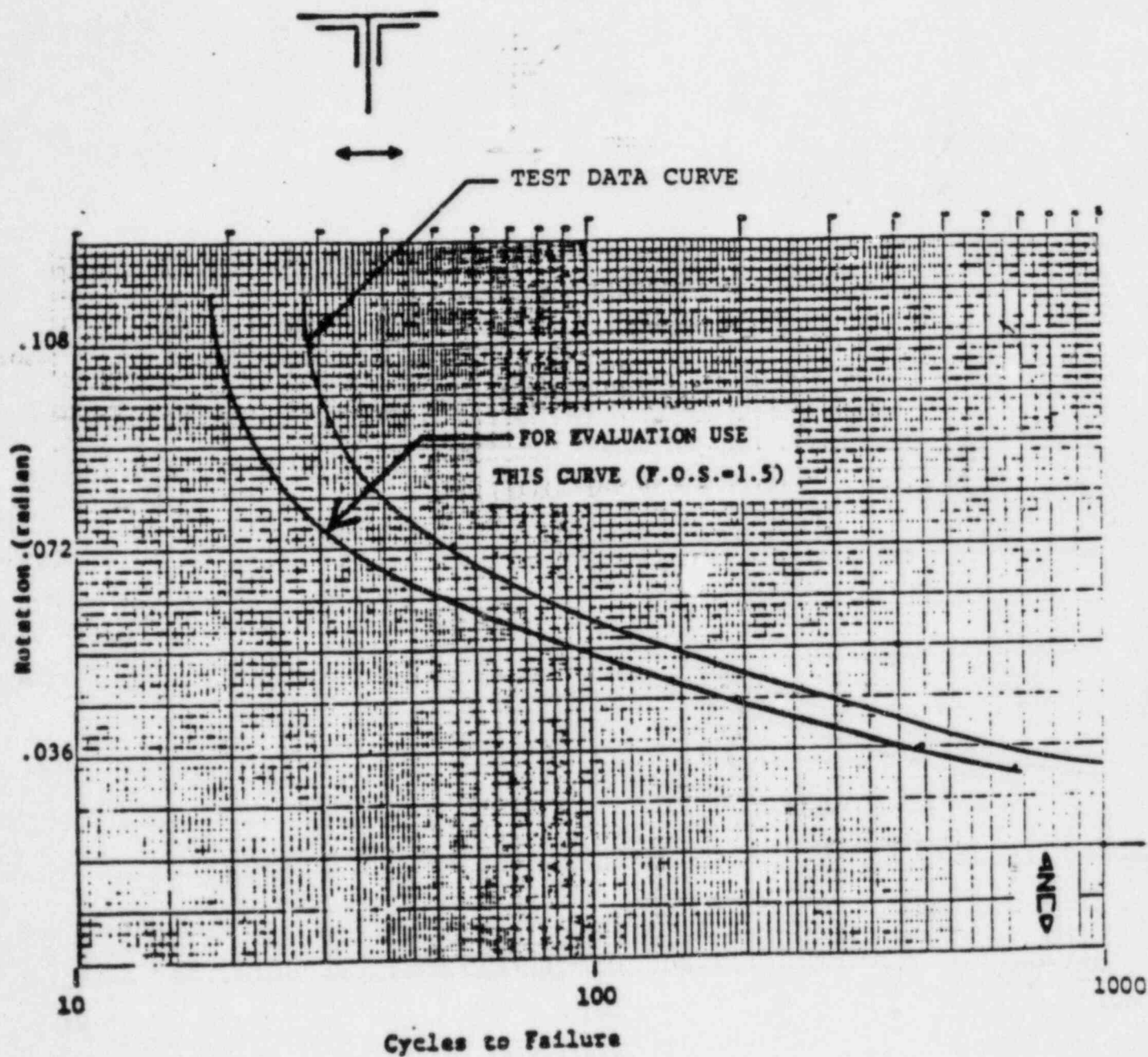
Attachment H.
Rotation Versus Cycles

P1331 Both Sides



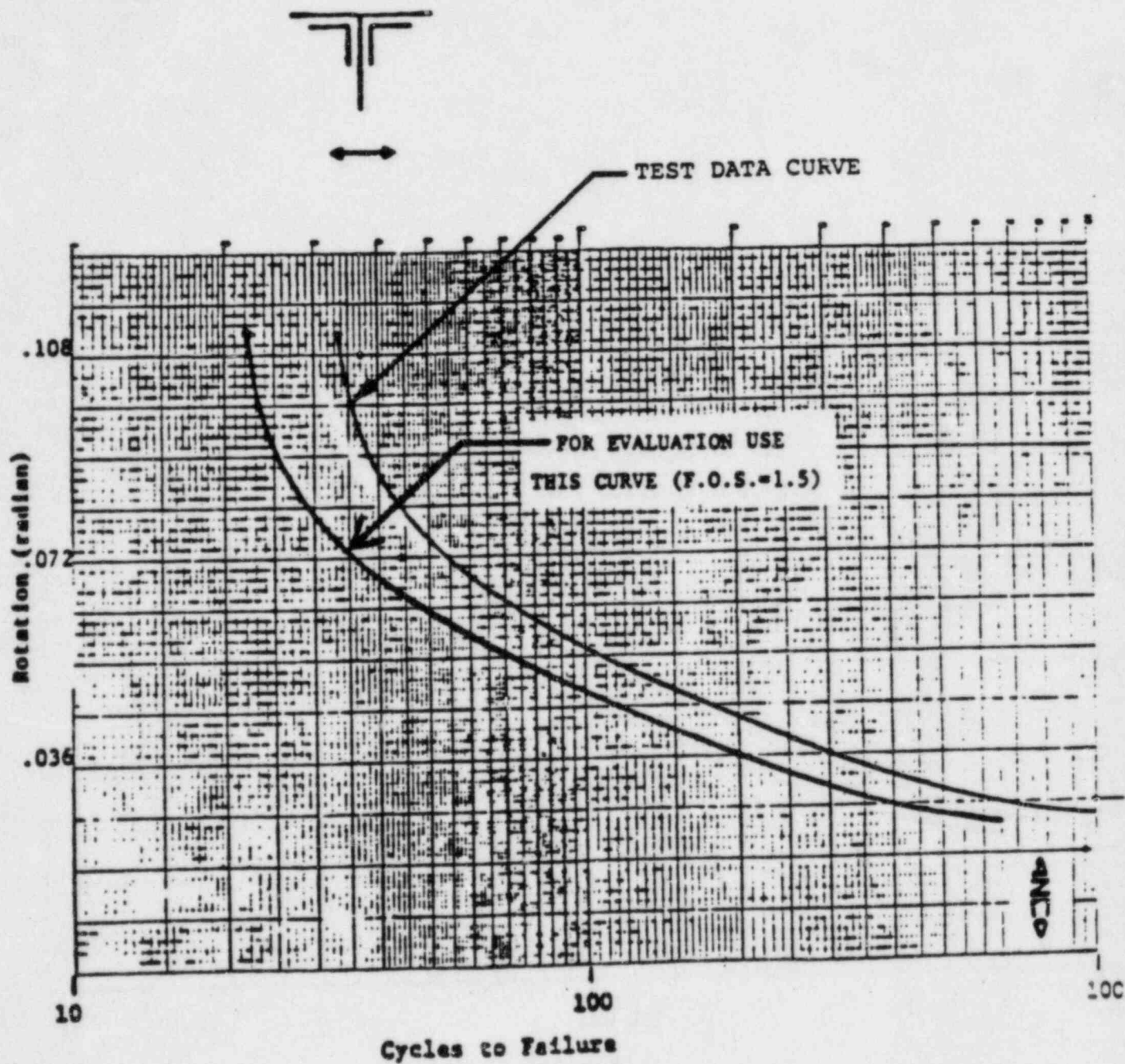
Attachment N.
Rotation Versus Cycles

P1325 Both Sides



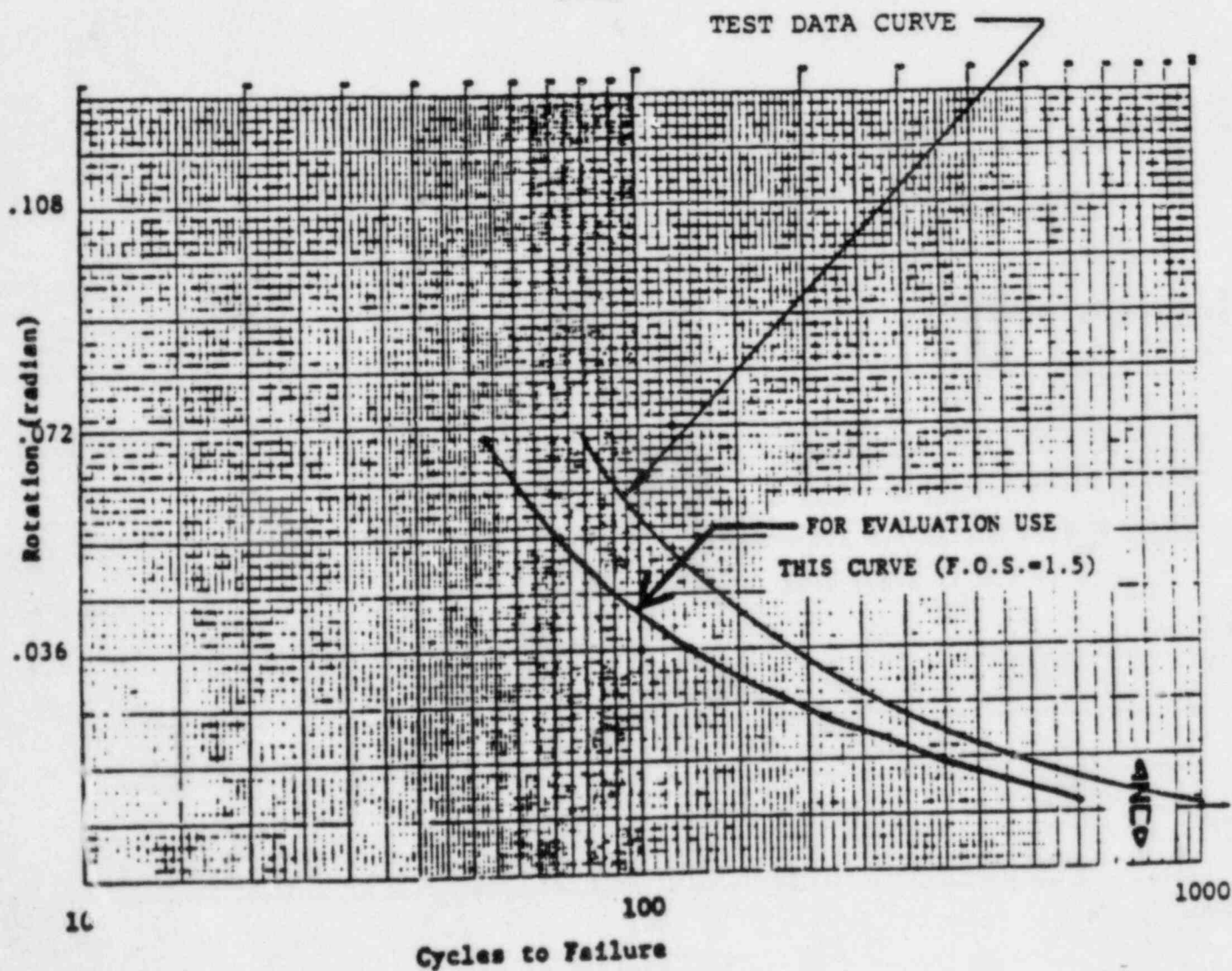
Attachment H.
Rotation Versus Cycles

P2626 Both Sides



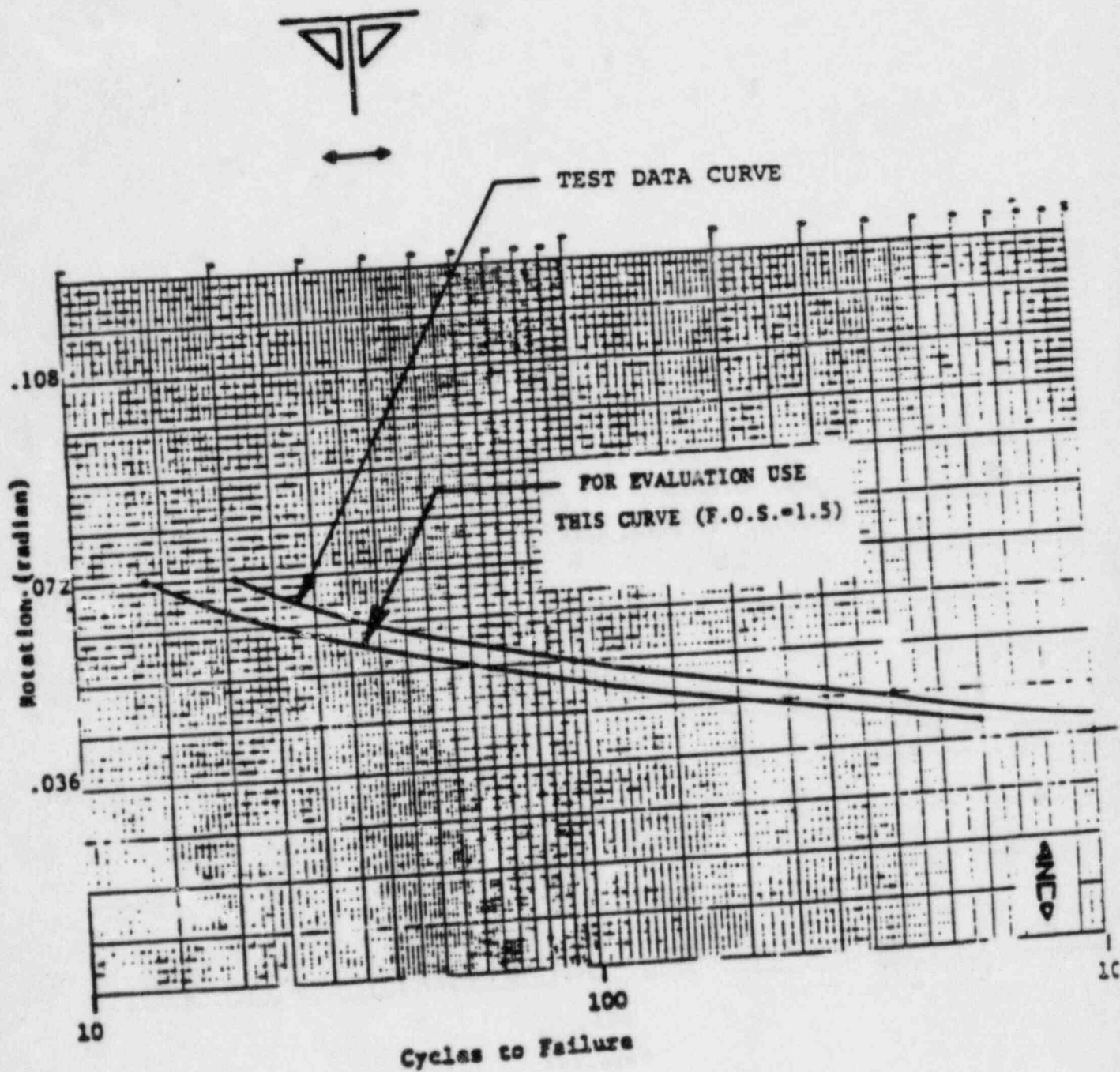
Attachment B.
Rotation Versus Cycles

P1458 Both Sides

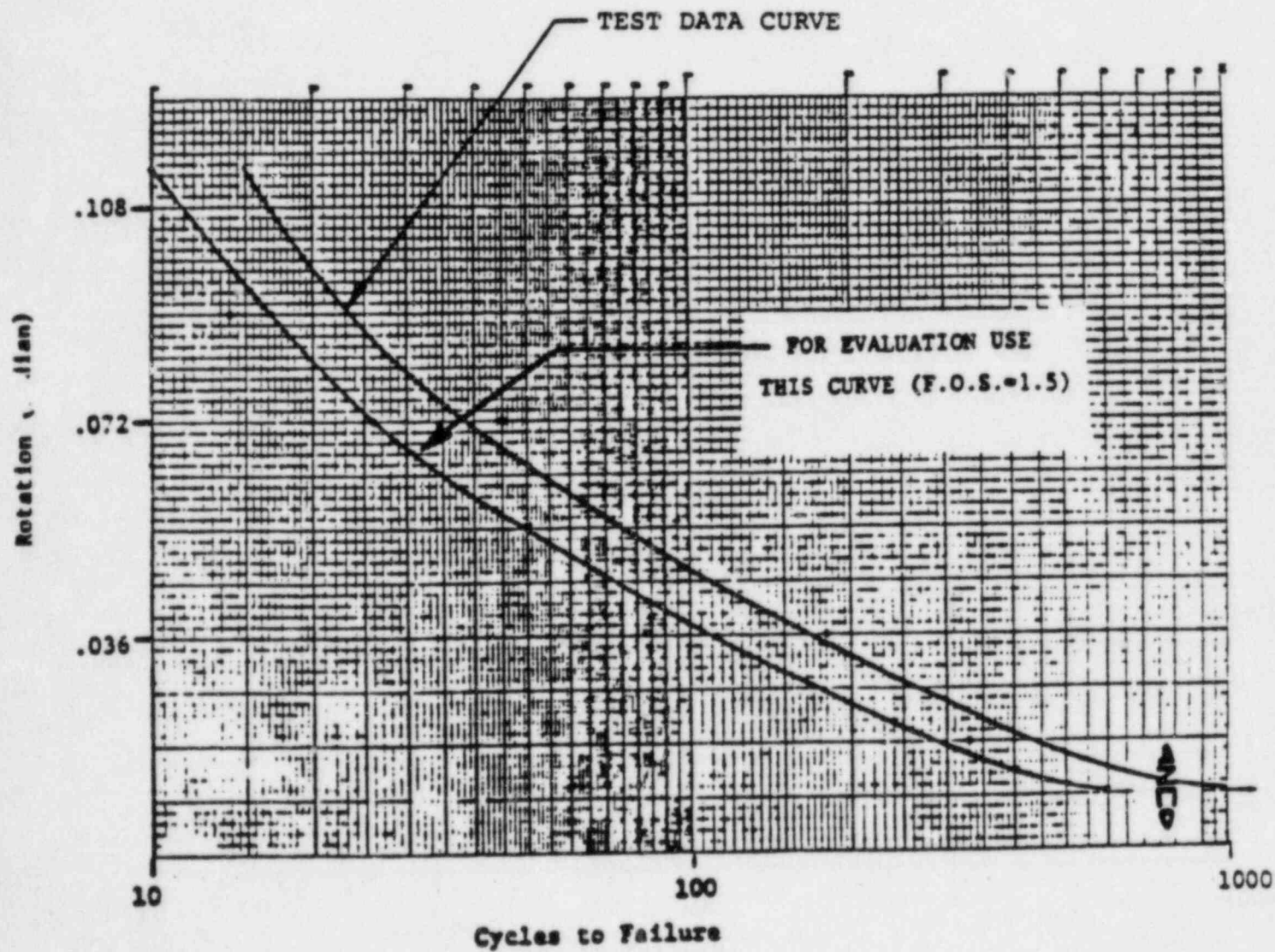


Attachment B.
Rotation Versus Cycles

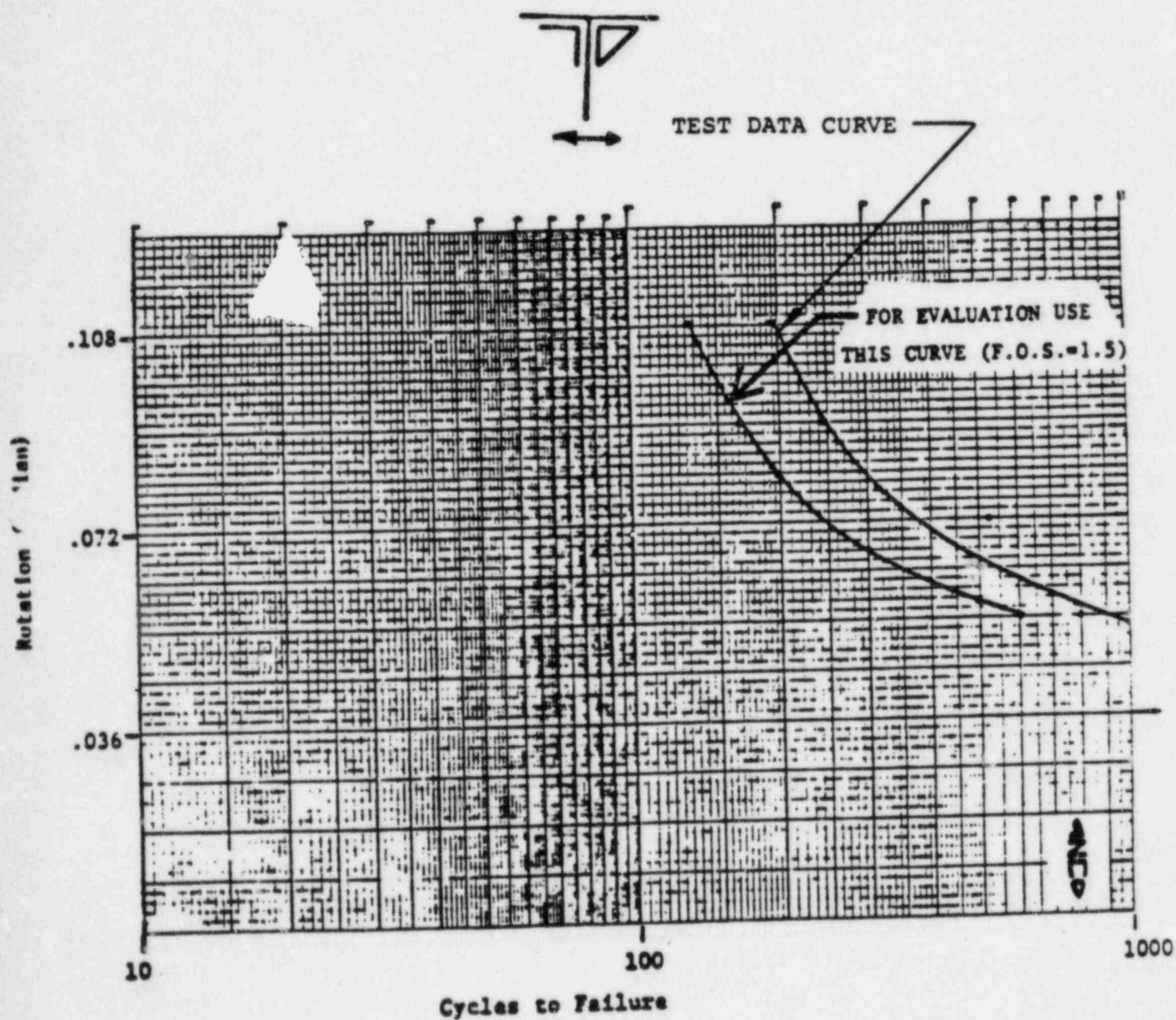
P1505 Both Sides



Attachment E.
Rotation Versus Cycles
P2626 AND P1331



Attachment H.
Rotation Versus Cycles
P1325 AND P1331



PROCEDURE FOR INSPECTION
OF EXISTING CONCRETE EXPANSION ANCHORS
IN HANGER INSTALLATIONS

REV. 0

REV. 1

2-14-77

Mike

DIABLO CANYON NUCLEAR POWER PLANT
UNITS I & II
QAI 96

PREPARED BY

TITLE

J. P. Rung *Field Eng* DATE *1/21/77*

C. G. Samuel *Chief Field Eng* DATE *1-21-77*

APPROVED BY

TITLE

M. J. Fisher *PESE* DATE *1/21/77*

William Hallock *John W. Ryan* DATE *1/21/77*

FOR INFORMATION
ONLY

PROCEDURE INDEX

1. PURPOSE
2. SCOPE
3. REFERENCES
4. PERSONNEL
5. DISCUSSION
6. PROCEDURE
7. DOCUMENTATION
8. SURVEILLANCE

FOR INFORMATION
ONLY

1.0 PURPOSE

- 1.1 To provide instruction to personnel performing inspections of existing concrete expansion anchors.

2.0 SCOPE

- 2.1 Inspection of all accessible concrete anchors as defined and outlined by the M. W. Kellogg program for inspection of existing concrete anchors.

3.0 REFERENCE MATERIAL

- 3.1 The following reference material will be used in providing instruction and for performing inspections of installed concrete anchors.
- 3.1.1 Anchor Manufacturer data and instructions.
 - 3.1.2 P.G. & E. and M. W. Kellogg hanger drawings.
 - 3.1.3 M. W. Kellogg program for inspection of existing concrete expansion anchors.

4.0 PERSONNEL

- 4.1 Personnel performing and documenting anchor inspections shall meet the following requirements.
- 4.1.1 Pass visual acuity test as outlined in M. W. Kellogg procedure E.S.D. 256.
 - 4.1.2 Have a general mechanical or engineering background sufficient to understand and comply with the requirements of this procedure.
 - 4.1.3 Have received sufficient instruction on this procedure to develop an understanding of the apparatus and procedures required to complete the requirements outlined herein. They will not determine the final disposition of the anchors.

5.0 DISCUSSION

- 5.1 Random inspections of installed expansion anchors have indicated that some existing installations do not meet minimum requirements. Recognizing this, we have performed an anchor failure analysis test to determine to what extent an anchor can deviate from perfect and still meet design requirements. Because of these findings a complete inspection will be performed. Anchors found to be outside the criteria defined herein will be evaluated and, if required, repairs made to assure compliance with design requirements.

FOR INFORMATION
ONLY

5.0 PROCEDURE

6.1 HILTI ANCHORS (See Attachment # 1)

6.1.1 These anchors are designed to develop maximum strength when installed as shown in steps 1, 2 & 3 of attachment # 1.

- a. The hole must be drilled to the proper depth and size. The depth being the length of the anchor. (Steps # 1)
- b. The hole should then be cleaned to remove any remaining chips or powdered concrete. (Steps # 2)
- c. The anchor is then placed in the hole, the plug inserted, small end first, and driven to expand the anchor inside the concrete. (Step # 3) This is accomplished with the proper sized setting tool, shown at the bottom of sheet, Attachment # 1.

6.1.2 A perfect installation would be one that leaves the anchor flush, to not more than 1/8" below the surface of the concrete and has the plug driven where the small end is flush with the back of the anchor, and the angle of the anchor is perpendicular to the surface of the concrete.

6.2 PHILLIPS ANCHORS (See Attachment # 2)

6.2.1 These anchors are designed to develop maximum strength when installed as shown in attachment # 2.

- a. The anchor itself is used, in a machine designed for installing these anchors, to drill the hole. The hole should be not greater than 1/16" - 1/8" deeper than the length of the anchor. (Step # 1)
- b. After the hole is drilled the anchor is removed and the hole cleaned. Care should be taken to assure that the core is removed from the center of the hole. (See Step # 2)
- c. After the hole is cleaned the expansion plug is inserted, small end first, into the back end of the anchor (Step 2.a), placed in the hole and, unlike the Hilti, the anchor is driven down on the plug to expand it.

6.2.2 A perfect installation would be one that leaves the anchor flush to not more than 1/8" below the concrete surface and has the anchor driven where the back, large end, of the plug is flush with the back of the anchor, and the angle of the anchor is perpendicular to the surface of the concrete.

6.3 Inspection and Documentation

FOR INFORMATION
ONLY

6.3.1 All Accessible anchors will be inspected and findings recorded as follows.

6.3.1.1 Prepare an Anchor Inspection Check List.
(Attachment # 3)

6.3.1.2 Record the hanger symbol, area and elevation.
Line " A "

6.3.1.3 Sketch the base plate and bolt pattern.
Line " B "

6.3.2 Number each bolt in the pattern. Facing the plate start with number 1 in the top left corner, and proceed clockwise. If the plate is floor or ceiling mounted consider North as the top of the plate. Mark the number adjacent to each bolt with a permanent, easily identifiable marker. If a support has more than one base plate, identify each plate using letters A, B, etc. Record the number on the check list Line " B ": complete Line " C ".

6.3.3 Remove each accessible bolt in the hanger installation. Record the type and size on the "Check List". IE: $\frac{1}{2}$ " H or $\frac{1}{2}$ " P. "H" being Hilti and "P" being Phillips. Line " D "

NOTE: Hilti plugs are unpainted and dark grey.
Phillips are either "red" anodized or painted.
Occasionally a rusted Hilti may appear to be red.

Remove only one bolt at a time unless it can be determined that the hanger will not move if more than one bolt is removed. If, for any reason, the hanger moves during the inspection it shall be noted in the "Remarks" section of the "Check List" and the "Review Required" box checked.

If there is reason to believe that the bolt or anchor will be damaged during bolt removal, other bolts may be loosened to relieve binding. If the bolt still binds and cannot be removed leave as is and note it on the check list, circle the notation, and check the "Rework Required" box.

If any or all bolts cannot be removed because of interference or accessibility note it on the check list and check the "Review Required" box.

6.3.4 After the bolt has been removed, visually examine the anchor for obvious irregularities such as: oversize holes in the concrete or loose anchors, stripped threads or anchors with the wrong type expansion plug. If any of these or other obvious irregularities exist note it in the remarks section of the check list and check the "Review Required" box.

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ONLY

6.3.4 If there is evidence that an anchor has been cut off on the thread end; determine the number of remaining threads and record it on the check list. Line "E"

NOTE: Unmodified Hilti anchors have a 45° internal chamfer on the shoulder. Unmodified Phillips anchors will have a rough shoulder caused by breaking off the driving portion of the anchor after it has been set. The number of remaining threads shall be determined by fully inserting the anchor test gauge and counting the number of turns required to remove it. If the remaining number of threads is greater than the number in the chart below it can be recorded as "All" threads remaining.

SIZE	NUMBER THREADS	
	HILTI	PHILLIPS
1/2	8	9
5/8	9	9
3/4	13	11
7/8	-----	12

6.3.5 Check the depth of the anchor below the surface of the concrete. If it is not possible to measure the anchor depth, estimate the depth and note that the measurement has been estimated. If the depth is greater than 1" record the depth in the entry space and circle the entry, Line "F". Check the "Review Required" box.

6.3.6 Check for Angular Misalignment as follows:

1. Insert the test tool (See Attachment # 4) into the anchor.
2. Measure the angle between the hammer plate and the test tool.
3. If the angular misalignment is greater than 5° from perpendicular to the plane of the plate, record the degree of deviation in the entry space, Line "G", and check the "Review required" box.
4. Remove the test tool.

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- 6.3.7 Check the bolt for length and thread damage. The length must be sufficient to assure at least 4 full threads engagement in the anchor.

If bolts are found to be short or have thread damage, discard them and after completion of the inspection install new bolts. It is not necessary to record this on the check list.

If bolt threads are stripped and it is determined that contact with the base plate is the reason, leave the bolt out and note the condition in the remarks section of the check list. Check the "Rework Required" box.

- 6.3.8 Using the appropriate type and size driving tool, the fitter, will drive the plug or anchor to assure it is fully driven. Caution should be exercised to prevent over driving.

Visually examine the hole to determine if the plug is below the bottom thread. If not, measure the length of the exposed remaining thread from the top of the plug to the edge of the anchor, record this dimension and note that the dimension was measured without the use of the test gauge.

If the bottom thread is visible above the plug, and the thread end is not cut off, measure with a depth gauge the distance from the top of the anchor to the plug. Record the reading on the check list, Line "H" (See Typ Inspection Aid Attached to Form 110).

NOTE: Anchor test gauge (Attachment #5) is to be used for all inspections where the thread end of the anchor is cut off.

If the alternate gauge (Attachment #6) is used so indicate on the check list and add 2" to the readings below.

NOTE: The anchor test gauges will be checked for excessive wear at periodic intervals not to exceed 1 week. When there is evidence of wear the worn gauge will be replaced by a new one.

If the readings are outside the ranges given below circle the entry and check the "Review Required" box.

FIELD Q.A. ACCEPTANCE CRITERIA

MEASURED WITH GAUGE

HILTI			PHILLIPS		
SIZE	MIN.	MAX.	SIZE	MIN.	MAX.
1/2	2 22/32	3 3/32	1/2	2 17/32	2 31/32
5/8	3 3/32	3 19/32	5/8	3 1/32	3 20/32
3/4	3 17/32	4 5/32	3/4	3 17/32	4 6/32
7/8	-----	-----	7/8	3 17/32	4 14/32

MEASURED WITHOUT GAUGE

HILTI			PHILLIPS		
SIZE	MIN.	MAX.	SIZE	MIN.	MAX.
1/2	3 1/32	1 12/32	1/2	2 1/32	1 16/32
5/8	1 3/32	1 19/32	5/8	25/32	1 18/32
3/4	1 14/32	2 4/32	3/4	1 5/32	1 29/32
7/8	-----	-----	7/8	1 12/32	2 12/32

FOR INFORMATION
ONLY

6.3.9 After all measurements have been recorded replace the bolts except where it is obvious that repairs must be made. Then spray a spot of orange paint on the hanger plate to indicate that the hanger has been inspected.

6.3.9.1 If the "Review Required" or Rework Required" box is checked on the check list, the inspector will hang a red flag on the hanger adjacent to the base plate.

7.0 DOCUMENTATION

7.1 Upon completion of an inspection the inspector shall review the inspection check list to assure that all required entries are made. Then sign and date the sheet.

7.2 During the shift the check lists will be collected by Q.C. surveillance for review and or rework scheduling as required.

8.0 AUDITS

8.1 The M. W. Kellogg Q.A. Department will perform audits of the inspection program. This will be performed by auditors who will randomly observe the inspection teams to assure that all inspection requirements are met, that measurements are accurate and that the inspection check lists are properly documented.

8.2 When an auditor observes an inspection he will initial the check list as an indication that he has observed that inspection and that it was performed correctly.

8.3 If he finds that inspections are being performed or documented incorrectly he will have the inspection team reinspect all previous suspect work.

Repeated discrepancies by an inspection team will be cause for retraining of the individuals or reassignment.

FOR INFORMATION
ONLY



1. Set depth gauge to length of anchor (adding carbide tip length).

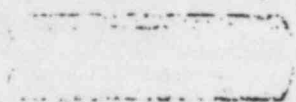


2. Drill and clean hole, insert anchor.



3. Fit setting tool into check and expand anchor, or use hammer and hand setting tool.

Available in all popular sizes



1/4" NC

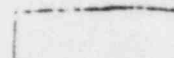


Note: This snap on the 1/4 to 3/8 sizes prevents the plug from jamming before the anchor is fully expanded.

3/8-3/4" NC



1/2" Plug

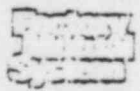


5/8 & 1 1/4" Plug

Description	Catalog Number	Bolt Size	Drill Bit Dia.	Bit Color Code	Usable Thread Length	Qty. Per Box	Average Pullout & Shear Strength Measurements			
							2000 PSI Concrete Pullout	2000 PSI Concrete Shear	4000 PSI Concrete Pullout	4000 PSI Concrete Shear
HD1 1/4"	5450000	1/4"	3/16"	Yellow	7/16"	100	1001	1700	2051	1761
HD1 3/8"	5450001	3/8"	1/2"	Blue	1"	50	3174	3970	4040	4225
HD1 1/2"	5450002	1/2"	5/8"	White	1 1/16"	50	3997	5870	6701	6224
HD1 3/4"	5450002	3/4"	27/32"	Black	1 1/2"	25	5540	8840	9990	12205
HD1 1"	5450000	1"	1"	Maroon	1 3/4"	25	8967	15195	10004	17000

Made in U.S.A.

UL listed and



Approved

All sizes I.C.D.O. approved.

NOTE: Maximum working loads should not exceed 11 of the average values for a concrete anchor size. Actual factor of safety to be used depends on the application. For comprehensive information, consult Laboratory Pullout and Shear data for each anchor size. See also I.C.D.O. Bulletin T-1000, "Primary Bolts" and I.C.D.O. Bulletin T-1000, "Anchor Test Program."

Setting Tools

For use with all anchors, the following tools are recommended:

TESD FOR TORNA 755

TESD FOR TORNA 755

TESD FOR TE-17

HSD (Hand Setting Tool)

	Machine Setting				Manual Setting	
	Torna 755		TE 17		Desc.	Cat. No.
	Desc.	Cat. No.	Desc.	Cat. No.		
HD1 1/4"			TESD 6	5451500	HSD 6	5454501
HD1 3/8"			TESD 10	5451515	HSD 10	5454520
HD1 1/2"			TESD 12	5454524	HSD 12	5454523
HD1 3/4"	TESD 13	5455056			HSD 13	5454538
HD1 1"	TESD 15	5455060			HSD 15	5454540



Conventional undercut expansion can cause stress concentrations in the concrete and a possible failure.

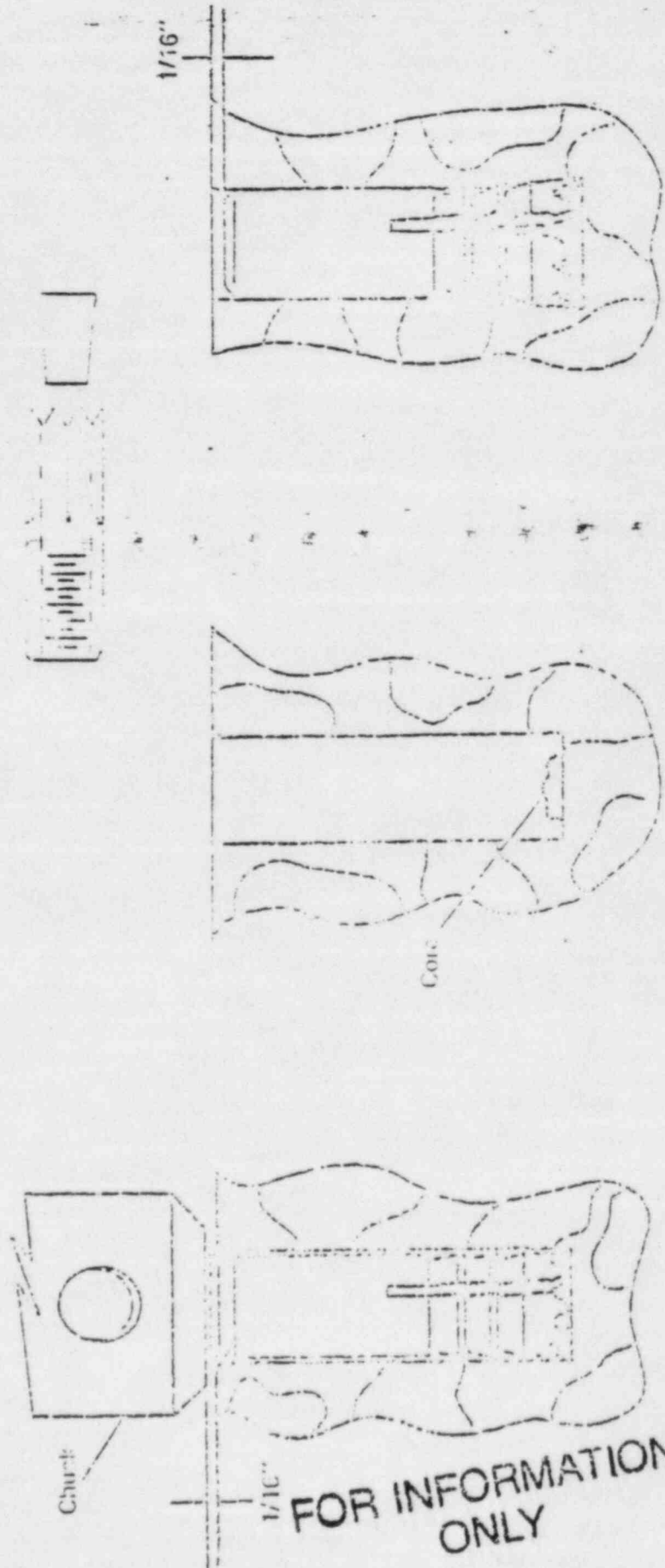
Special expansion provides uniform stress distribution and resistance against pull out of hole.

FOR INFORMATION ONLY

375 HING, C. J. HING
One Commercial Road, North
Shore, Conn. 06460

- (2) Holes drilled with SFS (5/8") of larger anchors may have a piece of concrete core in bottom which should be broken up with a rock drill, sand or other tool. Clean all castings from the hole.

(2.1)



PAGE 11 OF 14

ATTACHMENT # 3

ANCHOR INSTALLATION CHECK LIST

PAGE ____ OF ____

(A)

HANGER SYMBOL _____ AREA & ELEV. _____

CONFINEMENT _____

SKETCH OF ANCHOR PATTERN ON PLATE

☐
☐
☐

INSTALLATION ACCEPTABLE
REWORK
REVIEW REQUIRED

FOR INFORMATION ONLY

(B)

(C)	REFERENCE NUMBER	_____	_____	_____	_____	_____	_____	_____	_____	_____
(D)	SIZE & TYPE	_____	_____	_____	_____	_____	_____	_____	_____	_____
(E)	Ø OF THREADS REMAINING (IF LESS THAN 4, CIRCLE)	_____	_____	_____	_____	_____	_____	_____	_____	_____
(F)	ANCHOR DEPTH (IF MORE THAN 1/2)	_____	_____	_____	_____	_____	_____	_____	_____	_____
(G)	ANGULAR MISALIGNMENT (IF GREATER THAN 5°)	_____	_____	_____	_____	_____	_____	_____	_____	_____
(H)	AS LEFT PLUG DEPTH (DIM. A)	_____	_____	_____	_____	_____	_____	_____	_____	_____
	MINUS (DIM. B)	_____	_____	_____	_____	_____	_____	_____	_____	_____
	EQUALS (DIM. C)	_____	_____	_____	_____	_____	_____	_____	_____	_____

REMARKS: _____

DATA CHECK BY/DATE _____

REVIEWED BY _____

DIMENSION CHECK WITHOUT GAUGE

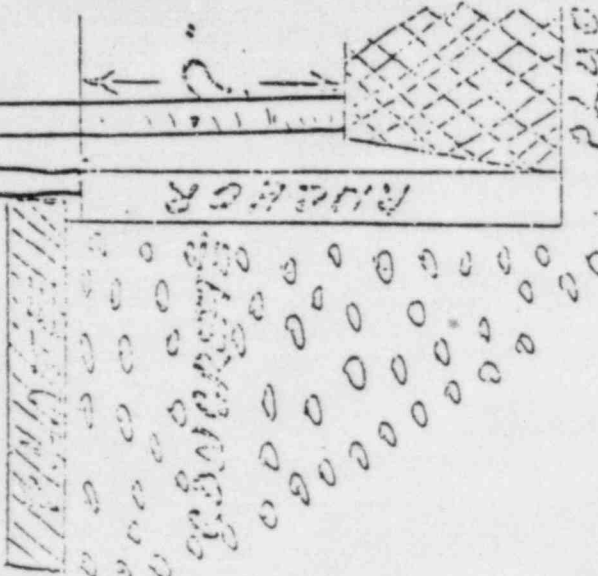
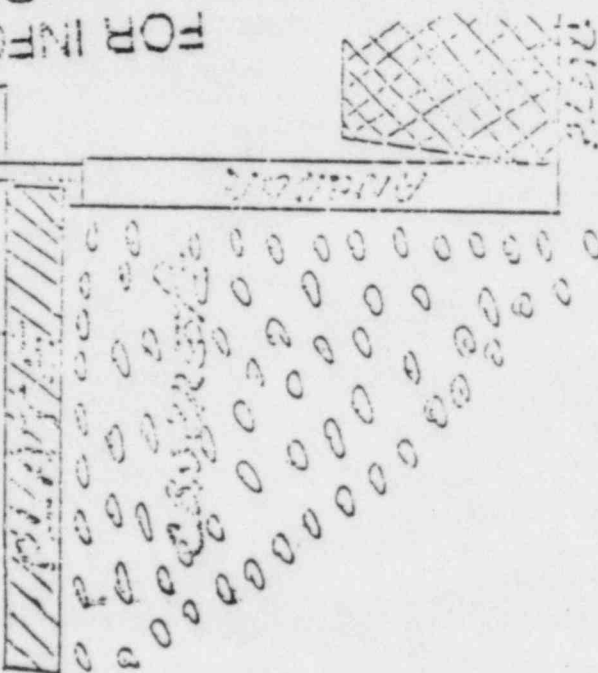
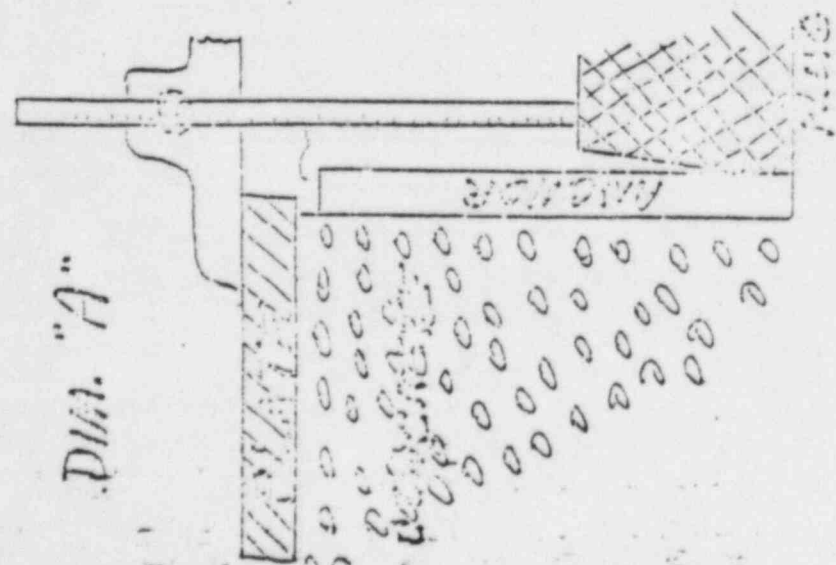
Note: Dimension "C" may be measured directly with the modified gauge shown below

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DIM. "A"

DIM. "B"

DIM. "C"



DIMENSION "A"

MIXED DIMENSIONS "B"

DIM. "C"

Dim. A 1.125"

Example

ATTACHMENT #4

ANCHOR MISALIGNMENT TEST TOOL

ANCHOR SIZE

TOOL DIA. "A"

1/2

15/32

5/8

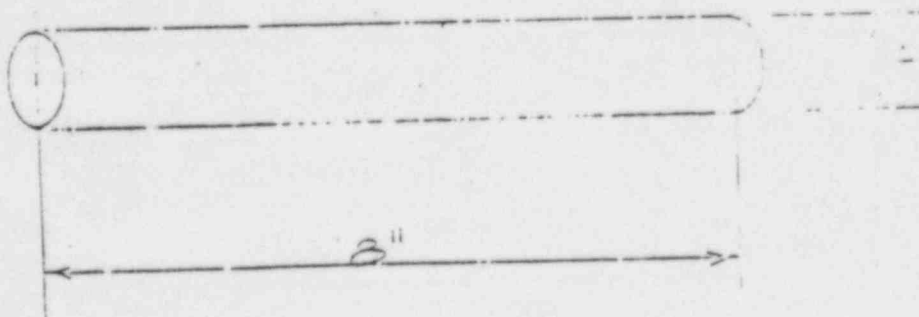
15/32

3/4

27/32

7/8

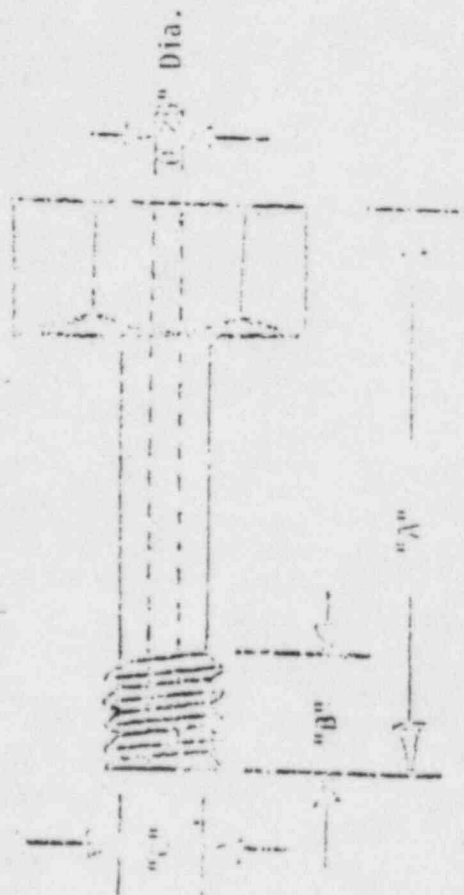
27/32



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ONLY

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MAJOR TEST GAUGE

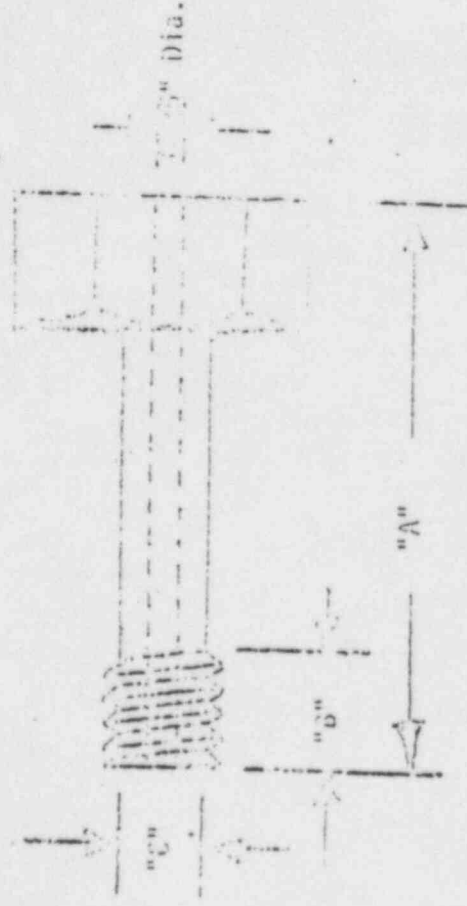


SALT SIZE	THREADS/IN.	DIMENSION "A"	DIMENSION "B"	DIMENSION "C"
1/2"	12	2.50"	4 FULL THREADS	MINOR DIAMETER
5/8"	11	3.00"	4 FULL THREADS	MINOR DIAMETER
3/4"	10	3.50"	4 FULL THREADS	MINOR DIAMETER
7/8"	9	3.50"	4 FULL THREADS	MINOR DIAMETER

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ALTERNATE

SECTION 15-6000



BOLT SIZE	THREADS/IN.	DIMENSION "A"	DIMENSION "B"	DIMENSION "C"
1/2"	13	4.50"	4 FULL THREADS	MINOR DIAMETER
5/8"	11	5.00"	5 FULL THREADS	MINOR DIAMETER
3/4"	10	5.50"	6 FULL THREADS	MINOR DIAMETER
7/8"	9	5.50"	7 FULL THREADS	MINOR DIAMETER