

dept. SA - ELECTRICAL
date JULY, 1994
Designed by J AKUS
Approved by _____

PENNSYLVANIA POWER & LIGHT COMPANY
CALCULATION SHEET
PROJECT BATTERY 1D660
LOAD PROFILE EE1

ER No. 741059
EWR
Sh.No. 298 of 324

ATTACHMENT 2

1D660

WORST CASE LOAD PROFILE

BASED ON THE THEORETICAL MAXIMUM

EQUIPMENT THAT

COULD START SIMULTANEOUSLY

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ER No. 741059

Date JULY, 1994

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PROJECT BATTERY 1D660

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LOAD PROFILE

EE1

Using the 1D660 Battery Load Profiles developed in Attachment 1, determine the maximum load profiles that could occur if all equipment that could start simultaneously did in fact start simultaneously for the following time segments. This approach is being used to assure that variations in the timing of the MOVs are enveloped by the Technical Specification.

LOAD SEGMENTS

0 - 60 seconds

1 - 10 minutes

10 - 30 minutes

30 - 240 minutes

1 - 5 minutes (Station Blackout)

5 - 6 minutes (Station Blackout)

6 - 10 minutes (Station Blackout)

The composite 1D660 Battery Load Profile for all modes of operation, including Station Blackout, is shown in Table 7 - 1.

1.0 LARGE BREAK LOCA PROFILE

The Table A2 - 1 shows the maximum possible 1D660 Battery Load Profile for a LARGE BREAK LOCA with all equipment starting simultaneously.

1.1 0 - 60 seconds

The 50 - 50.5 second time segment from Attachment 1 was used to develop the maximum possible 1D660 load due to simultaneous equipment starts since this segment is the heaviest loaded time segment.

During this load segment the following equipment cannot be operated simultaneously with the others loads.

1.11 HV-E41-1F084 inrush amperes are not used since HV-E41-1F084 starts on Reactor Low Pressure (61.2 psig) which occurs after the simultaneous starting of equipment.

1.2 1 - 10 Minute

1.21 HV-E41-1F004 inrush amperes are not used since HV-E41-1F042 must be fully open before HV-E41-1F004 can close. This occurs after the simultaneous equipment start.

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1.3 10 - 30 Minute

All the equipment in this load segment is assumed to operate simultaneously.

1.4 30 - 240 Minute

All the equipment in this load segment is assumed to operate simultaneously.

2.0 LARGE BREAK LOCA HPCI IN PRESSURE CONTROL PROFILE

The Table A2 - 2 shows the maximum possible 1D660 Battery Load Profile for a LARGE BREAK LOCA RCIC IN PRESSURE CONTROL with all equipment starting simultaneously.

2.1 0 - 60 seconds

During this load segment the following equipment cannot be operated simultaneously with the others loads.

2.11 HV-B21-1F019 and HV-G33-1F004 inrush amperes are not use since HV-B21-1F019 and HV-G33-1F004 start on Reactor Low Level-2 signal while the equipment that starts simultaneously starts on High Drywell Pressure.

2.12 1P155B inrush amperes are not used since this motor has a 6 second definite time timer which prevents simultaneous starting with the other equipment.

2.13 HV-E41-1F003 inrush amperes are not used since Reactor Pressure MUST drop to 105.5 psi before HV-E41-1F003 can operate. This occurs after all the equipment in this load segment has started.

2.2 1 - 10 Minute



2.21 HV-E41-1F042 and HV-E41-1F004 inrush amperes are not used since HV-E41-1F042 must be fully open before HV-E41-1F004 can close.

2.3 10 - 30 Minute

All the equipment in this load segment is assumed to operate simultaneously.

2.4 30 - 240 Minute

All the equipment in this load segment is assumed to operate simultaneously.

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3.0 SMALL BREAK LOCA PROFILE

The Table A2 - 3 shows the potential maximum possible 1D660 Battery Load Profile for a SMALL BREAK LOCA with all equipment starting simultaneously.

3.1 0 - 60 seconds

During this load segment the following equipment cannot be operated simultaneously with the others loads.

- 3.11 HV-E41-1F001 inrush amperes are not used since HV-E41-1F001 MUST BE out of Locked Rotor before HV-E41-1F006 can be started.
- 3.12 1P155B inrush amperes are not used since this motor has a 6 second definite time timer which prevents simultaneous starting with the other equipment.
- 3.13 HV-E41-1F012 inrush amperes are not used since HV-E41-1F012 starts on HPCI Turbine High Steam Pressure which occurs after the equipment that starts simultaneously has started.
- 3.14 1P112 inrush amperes are not used since 1P112 does not start until the Main Turbine has slowed down enough to result in low oil pressure. This occurs after the equipment that starts simultaneously has started.

3.2 1 - 10 Minute

All the equipment in this load segment is assumed to operate simultaneously.

3.3 10 - 30 Minute

All the equipment in this load segment is assumed to operate simultaneously.

3.4 30 - 240 Minute

All the equipment in this load segment is assumed to operate simultaneously.



4.0 SMALL BREAK LOCA HPCI IN PRESSURE CONTROL PROFILE

The Table A2 - 4 shows the maximum possible 1D660 Battery Load Profile for a SMALL BREAK LOCA RCIC IN PRESSURE CONTROL with all equipment starting simultaneously.

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4.1 0 - 60 seconds

4.11 1P155B inrush amperes are not used since this motor has a 6 second definite time timer which prevents simultaneous starting with the other equipment.

4.2 1 - 10 Minute

All the equipment in this load segment is assumed to operate simultaneously.

4.3 10 - 30 Minute

All the equipment in this load segment is assumed to operate simultaneously.

4.4 30 - 240 Minute

All the equipment in this load segment is assumed to operate simultaneously.

5.0 STATION BLACKOUT PROFILE

The Table A2 - 5 shows the maximum possible 1D660 Battery Load Profile for a STATION BLACKOUT with all equipment starting simultaneously.

5.1 0 - 60 seconds

During this load segment the following equipment cannot be operated simultaneously with the others loads.

5.11 HV-E41-1F001 inrush amperes are not use since HV-E41-1F001 MUST BE out of Locked Rotor before HV-E41-1F006 can be started.

5.12 HV-E41-1F012 inrush amperes are not used since HV-E41-1F012 starts on HPCI Turbine High Steam Pressure which occurs after the equipment that starts simultaneously has started.

5.13 1P112 inrush amperes are not used since 1P112 does not start until the Main Turbine has slowed down enough to result in low oil pressure. This occurs after the equipment that starts simultaneously has started.

5.2 1 - 5 Minute

All the equipment in this load segment operates simultaneously.

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5.3 5 - 6 Minute

5.31 HV-E41-1F059 inrush amperes are not used since HV-E41-1F059 MUST BE manually opened before the other equipment started in this time segment can start.

5.31 HV-E41-1F011 inrush amperes are not used since HV-E41-1F011 MUST BE manually opened before the other equipment started in this time segment can start.

5.4 6 - 10 Minute

All the equipment in this load segment operates simultaneously.

5.3 10 - 30 Minute

All the equipment in this load segment operates simultaneously.

5.4 30 - 240 Minute

All the equipment in this load segment operates simultaneously.

LARGE BREAK LOCA HPCI IN PPESSURE CONTROL - 1D660 LOAD PROFILE DURING LOCA / HPCI ISOLATION
CURRENTS CALCULATED AT 250 VDC

EC-088-1000
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EQUIPMENT	MCC	0 - 60s	1 - 10 MIN	10-30 MIN	30-240MIN				
HV-E41-1F001	1D264	0	0	0	0				
HV-E41-1F006	1D264	206.1	0	0	0				
HV-E41-1F069	1D264	0	7.8	0	0				
HV-E41-1F075	1D264	0	0	0	0				
HV-E51-1F084	1D264	0	10.3	0	0				
HV-E41-1F012	1D264	0	0	0	0				
HV-E41-1F042	1D264	19.3	2.1	0	0				
HV-E41-1F004	1D264	0	19.3	0	0				
HV-E41-1F003	1D264	0	83.9	0	0				
HV-E41-1F011	1D264	99.6	0	0	0				
1P213	1D274	0	0	0	0				
1P216	1D274	6.2	6.2	6.2	6.2				
HV-B21-1F019	1D274	0	0	0	0				
HV-G33-1F004	1D274	0	0	0	0				
HV-E41-1F008	1D274	123.2	0	0	0				
1P215	1D274	23	11.4	11.4	11.4				
1P125A	1D165	87.1	37.9	37.9	0				
1P155B	1D165	0	4	4	0				
1P112	1D165	340.2	140.1	140.1	0				
1D686	1D166	131	131	131	131				
TOTAL		1035.7	454	330.6	148.6				
1D666		131	131	131	131				
1D165		427.3	182	182	0				
1D264		325	123.4	0	0				
1D274		152.4	17.6	17.6	17.6				

STATION BLACKOUT - 1D660 LOAD PROFILE
CURRENTS CALCULATED AT 250 VDC

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EQUIPMENT	MCC	0 - 60%	1 - 5 MIN	5 - 6 MIN	6 - 10 MIN	10-30 MIN	30-240MIN	
HV-E41-1F001	1D264	18	0	0	0	0	0	
HV-E41-1F006	1D264	206.1	206.1	0	0	0	0	
HV-E41-1F059	1D264	7.8	7.8	0	0	0	0	
HV-E41-1F012	1D264	0	0	38.2	0	0	0	
HV-E41-1F042	1D264	0	0	0	0	0	0	
HV-E41-1F004	1D264	0	0	0	0	0	0	
HV-E41-1F011	1D264	0	0	0	0	0	0	
HV-E41-1F003	1D264	0	0	0	0	0	0	
1P213	1D274	70.8	0	70.8	0	0	0	
1P216	1D274	11.7	6.2	6.2	6.2	6.2	6.2	
HV-B21-1F019	1D274	26.4	0	0	0	0	0	
HV-G33-1F004	1D274	38.2	0	0	0	0	0	
HV-E31-1F008	1D1274	0	0	123.2	0	0	0	
1P215	1D274	0	23	11.4	11.4	11.4	11.4	
1P125A	1D165	87.1	37.9	37.9	37.9	37.9	0	
1P155B	1D165	14.4	4	4	4	4	0	
1P112	1D165	0	140.1	140.1	140.1	140.1	0	
1D666	1D166	131	131	131	131	131	131	
TOTAL		611.5	556.1	562.8	330.6	330.6	148.6	
1D666		131	131	131	131	131	131	
1D165		101.5	182	182	182	182	0	
1D264		231.9	213.9	38.2	0	0	0	
1D274		147.1	29.2	211.6	17.6	17.6	17.6	

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ATTACHMENT 3

1D660

AMPERE-HOURS

10067006

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The AMPERE-HOURS 1D660 is required to deliver are calculated using the load profiles from Attachment 2. This assures variations in the timing of the MOVs are enveloped.

1D660 BATTERY VOLTAGE AT THE END OF 4 HOURS
 AT RATED CURRENT AND VOLTAGE
 LARGE BREAK LOCA

(1) Actual Load (AMPS)	(2) Corrected Load (AMPS) (1) X 1.3875	(3) Elapsed Time (Min)	(4) Total AMP-HRS Removed
864	1199	1	20.0
452	583	10	114.1
331	460	30	267.5
149	207	240	992.0

1D660 BATTERY VOLTAGE AT THE END OF 4 HOURS
 AT RATED CURRENT AND VOLTAGE
 LARGE BREAK LOCA HPCI IN PRESSURE CONTROL

(1) Actual Load (AMPS)	(2) Corrected Load (AMPS) (1) X 1.3875	(3) Elapsed Time (Min)	(4) Total AMP-HRS Removed
1036	1438	1	24.0
454	630	10	118.5
331	460	30	271.9
149	207	240	996.4

* Corrected Load = (Temperature Correction) (Age Correction)
 = (1.11) (1.25) = 1.3875

Temperature Correction = 1.11 for 60°F (From IEEE 485)

Age Correction = 1.25 (IEEE 485)

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**1D660 BATTERY VOLTAGE AT THE END OF 4 HOURS
 AT RATED CURRENT AND VOLTAGE
 SMALL BREAK LOCA**

(1) Actual Load (AMPS)	(2) Corrected Load (AMPS) (1) X 1.3875	(3) Elapsed Time (Min)	(4) Total AMP-HRS Removed
575	798	1	13.3
352	489	10	86.7
331	460	30	240.1
149	207	240	964.6

**1D660 BATTERY VOLTAGE AT THE END OF 4 HOURS
 AT RATED CURRENT AND VOLTAGE
 SMALL BREAK LOCA RCIC IN PRESSURE CONTROL**

(1) Actual Load (AMPS)	(2) Corrected Load (AMPS) (1) X 1.3875	(3) Elapsed Time (Min)	(4) Total AMP-HRS Removed
1036	1438	1	24.0
352	489	10	97.4
331	460	30	250.8
149	207	240	975.3

* Corrected Load = (Temperature Correction) (Age Correction)
 = (1.11) (1.25) = 1.3875

Temperature Correction = 1.11 for 60°F (From IEEE 485)

Age Correction = 1.25 (IEEE 485)

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**1D660 BATTERY VOLTAGE AT THE END OF 4 HOURS
AT RATED CURRENT AND VOLTAGE
STATION BLACKOUT**

(1) Actual Load (AMPS)	(2) Corrected Load (AMPS) (1) X 1.3875	(3) Elapsed Time (Min)	(4) Total AMP-HRS Removed
611	848	1	14.1
550	772	5	65.6
563	781	6	78.7
331	460	30	262.7
149	207	240	987.2

**1D660 BATTERY VOLTAGE AT THE END OF 4 HOURS
AT RATED CURRENT AND VOLTAGE
PROPOSED TECHNICAL SPECIFICATION**

(1) Actual Load (AMPS)	(2) Corrected Load (AMPS) (1) X 1.3875	(3) Elapsed Time (Min)	(4) Total AMP-HRS Removed
1040	1443	1	24.1
575	798	10	143.8
350	486	30	305.8
175	243	240	1156.3

* Corrected Load = (Temperature Correction) (Age Correction)

$$= (1.11)(1.25) = 1.3875$$

Temperature Correction = 1.11 for 60°F (From IEEE 485)

Age Correction = 1.25 (IEEE 485)

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1D660 BATTERY VOLTAGE AT THE END OF 4 HOURS
 AT RATED CURRENT AND VOLTAGE
 EXISTING TECHNICAL SPECIFICATION

(1) Actual Load (AMPS)	(2) Corrected Load (AMPS) (1) X 1.3875	(3) Elapsed Time (Min)	(4) Total AMP-HRS Removed
887	1231	1	20.5
396	550	10	103
366	508	30	441.7
325	451	120	1118.2
187	260	239	1633.9
229	318	240	1639.2

* Corrected Load = (Temperature Correction) (Age Correction)
 = (1.11) (1.25) = 1.3875

Temperature Correction = 1.11 for 60°F (From IEEE 485)

Age Correction = 1.25 (IEEE 485)

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ATTACHMENT 4

1D660

MINIMUM BATTERY TERMINAL

VOLTAGE

9501979007

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1D660
 CALCULATE
 MINIMUM REQUIRED BATTERY TERMINAL VOLTAGE

The minimum required battery terminal voltage is the voltage required at the END OF DISCHARGE to support the connected load per IEEE 485-1978. This voltage is the minimum Technical Specification voltage requirement.

1.0 The Resistance between the Load Center and MCCs are:

Battery to Load Center	=	0.0027 Ω (From E-AAA-255)
Load Center to 1D264	=	0.0147 Ω (From E-AAA-255)
Load Center to 1D274	=	0.0142 Ω (From E-AAA-255)
Load Center to 1D165	=	0.0144 Ω (From E-AAA-255)
Load Center to 1D666	=	0.009 Ω (From E-AAA-255)

1 Determine the voltage at the Load Center while maintaining 210 VDC at the MCCs for the END OF DISCHARGE Load Segment of Battery 1D660 (30 -240 Minutes).

2.1 **1D264**

The Proposed Technical Specification Profile for the 30 - 240 minute segment is 175 amperes. The largest calculated Class 1E load on 1D264 is 0 A (From Attachment 2) and the largest calculated battery load profile is 148.6 amperes (From Attachment 2). The 26.4 ampere differences between the two profiles is added to the Class 1E MCC 1D264.

$$I_{1D264} = 26.4 \text{ A}$$

$$V_{LC} = 210 + V_{DROP} = 210 + (0.0147)(26.4) = 210.4 \text{ V}$$

2.2 **1D274**

The Proposed Technical Specification Profile for the 30 - 240 minute segment is 175 amperes. The largest calculated Class 1E load on 1D274 is 17.6 A (From Attachment 2) and the largest calculated battery load profile is 148.6 amperes (From Attachment 2). The 26.4 ampere differences between the two profiles is added to the Class 1E MCC 1D274.

$$I_{1D274} = (17.6\text{A} + 26.4\text{A}) = 44 \text{ A}$$

$$V_{LC} = 210 + V_{DROP} = 210 + (0.0142)(44) = 210.6 \text{ V}$$

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2.3 1D666

The Proposed Technical Specification Profile for the 30 - 240 minute segment is 175 amperes. The largest calculated load on 1D666 is 131 A (From Attachment 2) and the largest calculated battery load profile is 148.6 amperes (From Attachment 2). The 26.4 ampere differences between the two profiles is added to the 1D666.

$$I_{1D666} = (131A + 26.4A) = 157.4 A$$

$$V_{LC} = 210 + V_{DROP} = 210 + (0.009)(157.4) = 211.4 V$$

2.4 1D165

The Proposed Technical Specification Profile for the 30 - 240 minute segment is 175 amperes. The largest calculated load on 1D165 is 0 A (From Attachment 2) and the largest calculated battery load profile is 148.6 amperes (From Attachment 2). The 26.4 ampere differences between the two profiles is added to the 1D165.

$$I_{1D165} = 26.4 A$$

$$V_{LC} = 210 + V_{DROP} = 210 + (0.0144)(26.4) = 210.4 V$$

3.0 Determine the Battery Terminal Voltage to maintain 210 VDC at the Class 1E MCCs for the END OF DISCHARGE Load Segment of Battery 1D660.

Use the Load Center voltage required to maintain 210 V at 1D666 since this voltage requires the higher battery voltage.

$$V_{BATTERY} = V_{LC} + V_{Drop\ Batt\ to\ LC}$$

$$I = 175 A$$

$$V_{BATTERY} = 211.4 V + (175)(0.0027) \\ = 211.9 V$$

4.0 Determine the Volts per cell that must be used in sizing the Class 1E 120 cell battery in order to maintain a battery voltage of 211.9 at END OF DISCHARGE.

$$VPC = 211.9/120 = 1.766$$

USE 1.77 VPC

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ATTACHMENT 5

INRUSH CURRENT CALCULATION
FOR
1P125A & 1P112

9 2 0 1 9 7 2 0 1 0 1

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ATTACHMENT 5

The purpose of this calculation to the calculate the inrush current for 1P125A and 1P112 with starting resistors based upon speed of the motors when the starting resistors are shorted.

The equations on the following pages were programmed into MicroSoft Excel PC based program.

The only assumption used in this calculation is that the motor Horsepower (HP) is proportional to the square of the speed. This is base upon:

Head is proportional to speed

Flow is proportional to speed

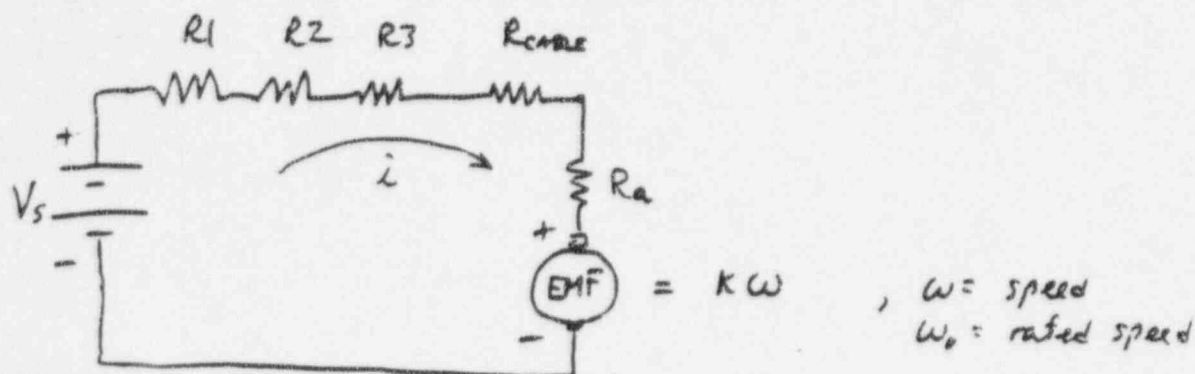
$$HP = (Head)(Flow) = K(Speed^2)$$

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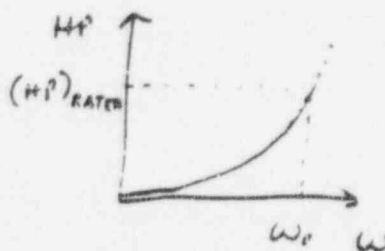
$$746 (\text{HP})_{\text{RATED}} = (V)_{\text{RATED}} (i)_{\text{RATED}} - (i)_{\text{RATED}}^2 R_a$$

$$(R_a)_{\text{CMC}} = \frac{(V)_{\text{RATED}}}{(i)_{\text{RATED}}} - \frac{(\text{HP})_{\text{RATED}} \times 746}{(i)_{\text{RATED}}^2}$$

$$\omega_0 K = (V)_{\text{RATED}} - (i)_{\text{RATED}} (R_a)_{\text{CMC}}$$

$$K = \frac{(V)_{\text{RATED}} - (i)_{\text{RATED}} (R_a)_{\text{CMC}}}{\omega_0}$$

$$\text{HP} = (\text{HP})_{\text{RATED}} \times \left(\frac{\omega}{\omega_0} \right)^2$$



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$$V_s - i R_T = EMF$$

$$R_T = \text{total ckt resist.}$$

$$I \times EMF = I \times KW = 746 \text{ (HP)} = 746 \text{ (HP)}_{\text{RATED}} \times \left(\frac{\omega}{\omega_0} \right)^2$$

$$\therefore L = \frac{746 (\text{HP})_{\text{RATED}} \omega}{K \omega_p^2}$$

$$\omega = \frac{V_s K \omega_o^2}{K^2 \omega_o^2 + 746 (\text{HP})_{\text{RATED}} R_T}$$

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1P125A
D.C. MOTOR STARTING WITH ONE (1) STARTING RESISTOR

EC-088-1006
REV 0
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	A	B	C	D	E	F
1	RATED HP	10.00				
2	RATED VOLTS	240.00				
3	RATED CURRENT (AMPS)	36.00				
4	RATED SPEED (RPM)	3500.00				
5	STARTING R1 (OHMS)	1.8000				
6	STARTING R2 (OHMS)	0.0000				
7	STARTING R3 (OHMS)	0.0000				
8	CABLE RESIST. (OHMS)	0.1600				
9	SOURCE VOLTS	250.00				
10	MEASURED ARMATURE RESIST. (OHMS)	0.0000				
11	ROTOR CONSTANT "K" (VOLTS/RPM)	0.0592				
12	CALC. ARMATURE RESIST. (OHMS)	0.9105				
13						
14		SPEED	ROTOR EMF	CURRENT	MECH. HP	ELEC. HP
15	STEP 1-INRUSH (R1 + R2 + R3)	0.00	0.00	87.09	0.00	0.00
16	STEP 2-RUNNING (R1 + R2 + R3)	2817.49	166.81	28.98	6.48	6.48
17	STEP 3-INRUSH (R2 + R3)	2817.49	166.81	77.71	6.48	17.38
18	STEP 4-RUNNING (R2 + R3)	3560.38	210.80	36.62	10.35	10.35
19	STEP 5-INRUSH (R3)	3560.38	210.80	36.62	10.35	10.35
20	STEP 6-RUNNING (R3)	3560.38	210.80	36.62	10.35	10.35
21	STEP 7-INRUSH (NO STARTING RESIST.)	3560.38	210.80	36.62	10.35	10.35
22	STEP 8-RUNNING (NO STARTING RESIST.)	3560.38	210.80	36.62	10.35	10.35

1P1121
D.C. MOTOR STARTING WITH TWO (2) STARTING RESISTOR

EC-088-1006
REV 0
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	A	B	C	D	E	F
1	RATED HP	40.00				
2	RATED VOLTS	240.00				
3	RATED CURRENT (AMPS)	137.00				
4	RATED SPEED (RPM)	1800.00				
5	STARTING R1 (OHMS)	0.3500				
6	STARTING R2 (OHMS)	0.1900				
7	STARTING R3 (OHMS)	0.0000				
8	CABLE RESIST. (OHMS)	0.0300				
9	SOURCE VOLTS	250.00				
10	MEASURED ARMATURE RESIST. (OHMS)	0.0000				
11	ROTOR CONSTANT "K" (VOLTS/RPM)	0.1210				
12	CALC. ARMATURE RESIST. (OHMS)	0.1620				
13						
14		SPEED	ROTOR EMF	CURRENT	MECH. HP	ELEC. HP
15	STEP 1-INRUSH (R1 + R2 + R3)	0.00	0.00	341.54	0.00	0.00
16	STEP 2-RUNNING (R1 + R2 + R3)	1414.69	171.19	107.67	24.71	24.71
17	STEP 3-INRUSH (R2 + R3)	1414.69	171.19	206.34	24.71	47.35
18	STEP 4-RUNNING (R2 + R3)	1665.80	201.57	126.79	34.26	34.26
19	STEP 5-INRUSH (R3)	1665.80	201.57	252.27	34.26	68.16
20	STEP 6-RUNNING (R3)	1843.43	223.07	140.31	41.95	41.95
21	STEP 7-INRUSH (NO STARTING RESIST.)	1843.43	223.07	140.31	41.95	41.95
22	STEP 8-RUNNING (NO STARTING RESIST.)	1843.43	223.07	140.31	41.95	41.95