

Donald F. Schnell
Senior Vice President
Nuclear

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U.S. Nuclear Regulatory Commission
Attn: Document Control Desk
Mail Station P1-137
Washington, D.C. 20555

ULNRC- 2551

Gentlemen:

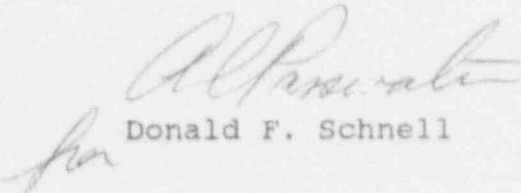
DOCKET NUMBER 50-483
CALLAWAY PLANT - CYCLE 5
CORE OPERATING LIMITS REPORT

- References: 1) ULNRC-2323 dated November 14, 1990
2) ULNRC-2360 dated January 31, 1991
3) ULNRC-2379 dated March 19, 1991
4) ULNRC-2513 dated November 13, 1991
5) ULNRC-2532 dated December 12, 1991

Reference 1 transmitted the Callaway Plant Cycle 5 Core Operating Limits Report (COLR). Attached please find Revision 6 to Sections 2.4.1, 2.5 and Figure 7 of the COLR. Revision 6 modifies the Axial Flux Difference (AFD) target band and corresponding W(Z) values to +12%, -7% for Normal Operation. The revised AFD target bands are applicable through the end of Cycle 5.

Should you have any questions concerning this information, please contact us.

Very truly yours,


Donald F. Schnell

WEK/dls

Attachment

ADD 11

cc: T. A. Baxter, Esq.
Shaw, Pittman, Potts & Trowbridge
2300 N. Street, N.W.
Washington, D.C. 20037

Dr. J. O. Cermak
CFA, Inc.
18225-A Flower Hill Way
Gaithersburg, MD 20879-5334

R. C. Knop
Chief, Reactor Project Branch 1
U.S. Nuclear Regulatory Commission
Region III
799 Roosevelt Road
Glen Ellyn, Illinois 60137

Bruce Bartlett
Callaway Resident Office
U.S. Nuclear Regulatory Commission
RR#1
Steedman, Missouri 65077

L. R. Wharton (2)
Office of Nuclear Reactor Regulation
U.S. Nuclear Regulatory Commission
1 White Flint, North, Mail Stop 13E21
11555 Rockville Pike
Rockville, MD 20852

Manager, Electric Department
Missouri Public Service Commission
P.O. Box 360
Jefferson City, MO 65102

bcc: D. Shafer/A160.761
/QA Record (CA-758)

Nuclear Date
E210.01
DFS/Chrono
D. F. Schnell
J. E. Birk
J. V. Laux
M. A. Stiller
G. L. Randolph
R. J. Irwin
P. Barrett
C. D. Naslund
A. C. Passwater
D. E. Shafer
W. E. Kahl (2)
S. Wideman (WCNOC)
R. C. Slovic (Bechtel)
T. P. Sharkey
NSRB (Sandra Dale)

Westinghouse Proprietary Class 2

Callows, Cycle 5

Rev ⁶1.4 Axial Flux Difference (Specification 3.2.1)

2.4.1 The Axial Flux Difference (AFD) target bands are,

- a. ~~$\pm 8\%$~~ ^{$\pm 12\%$} , -7% for Normal Operation
- b. $\pm 3\%$ for Restricted AFD Operation

2.4.2 The Acceptable Operation Limits are shown in Figure 3.

2.4.3 The minimum allowable power level for Restricted AFD Operation, APLND, is 90% of RATED THERMAL POWER.

Callaway Cycle 5

Rev. 6

2.5 Heat Flux Hot Channel Factor - $F_Q(Z)$
(Specification 3.2.2)

$$F_Q(Z) \leq \frac{F_Q^{RTP}}{P} * K(Z) \quad \text{for } P > 0.5$$

$$F_Q(Z) \leq \frac{F_Q^{RTP}}{0.5} * K(Z) \quad \text{for } P \leq 0.5$$

where: $P = \frac{\text{THERMAL POWER}}{\text{RATED THERMAL POWER}}$

$$2.5.1 \quad \frac{F_Q^{RTP}}{Q} = 2.50$$

2.5.2 $K(z)$ is provided in Figure 4.

2.5.3 The $W(z)$ functions that are to be used in Technical Specifications 4.2.2.2, 4.2.2.3, and 4.2.2.4 for F_Q surveillance are shown in Figures 5 through 8.

Because significant margin exists between the analytically determined maximum $F_Q(z) * P_{rel}$ values and their limit, Restricted Axial Flux Difference (RAFDO) operation is not expected to be required for Cycle 5. For this reason, no $W(z)$ values are supplied for Cycle 5.

RAFDO

The Normal Operation $W(z)$ values, $W(z)_{NO}$, were originally determined for three specific burnups in Cycle 5, assuming Cycle 5 operates with the CAOC strategy and uses a +3%, -12% delta-I band about the target flux difference. This permits determination of $W(z)$ at any cycle burnup through the use of three point interpolation. The end of cycle $W(z)$ value has been revised based on CAOC operation with a +12, -7% delta-I band about the target flux difference. Use of this $W(z)$ value for Cycle 5 burnups from 16000 MWD/MTU until end of cycle is conservative. Interpolation with the +3%, -12% $W(z)$ values from earlier burnups should not be performed. Also included is a $W(z)_{NO}$ function that bounds the $W(z)$ curves based on a +3%, -12% delta-I band for all Cycle 5 burnups. This is not appropriate to use for delta-I bands other than +3%, -12% about the target flux difference.

Rev. 6

INCORE Point	Height (Feet)	W(Z) 16000.	INCORE Point	Height (Feet)	W(Z) 16000.
Top 1.	0.00000	* 1.0000	37.	6.0000	1.1974
2.	0.16700	* 1.0000	38.	6.1670	1.2033
3.	0.33300	* 1.0000	39.	6.3330	1.2076
4.	0.50000	* 1.0000	40.	6.5000	1.2104
5.	0.66700	* 1.0000	41.	6.6670	1.2116
6.	0.83300	* 1.0000	42.	6.8330	1.2112
7.	1.0000	* 1.0000	43.	7.0000	1.2089
8.	1.1670	* 1.0000	44.	7.1670	1.2056
9.	1.3330	* 1.0000	45.	7.3330	1.2032
10.	1.5000	* 1.0000	46.	7.5000	1.2030
11.	1.6670	* 1.0000	47.	7.6670	1.2045
12.	1.8330	1.1629	48.	7.8330	1.2057
13.	2.0000	1.1585	49.	8.0000	1.2055
14.	2.1670	1.1536	50.	8.1670	1.2047
15.	2.3330	1.1483	51.	8.3330	1.2044
16.	2.5000	1.1426	52.	8.5000	1.2037
17.	2.6670	1.1365	53.	8.6670	1.2016
18.	2.8330	1.1300	54.	8.8330	1.1982
19.	3.0000	1.1228	55.	9.0000	1.1958
20.	3.1670	1.1162	56.	9.1670	1.1953
21.	3.3330	1.1125	57.	9.3330	1.1964
22.	3.5000	1.1149	58.	9.5000	1.1977
23.	3.6670	1.1205	59.	9.6670	1.1998
24.	3.8330	1.1250	60.	9.8330	1.1995
25.	4.0000	1.1300	61.	10.000	1.1998
26.	4.1670	1.1360	62.	10.167	1.2007
27.	4.3330	1.1421	63.	10.333	* 1.0000
28.	4.5000	1.1476	64.	10.500	* 1.0000
29.	4.6670	1.1523	65.	10.667	* 1.0000
30.	4.8330	1.1562	66.	10.833	* 1.0000
31.	5.0000	1.1597	67.	11.000	* 1.0000
32.	5.1670	1.1622	68.	11.167	* 1.0000
33.	5.3330	1.1646	69.	11.333	* 1.0000
34.	5.5000	1.1715	70.	11.500	* 1.0000
35.	5.6670	1.1813	71.	11.667	* 1.0000
36.	5.8330	1.1900	72.	11.833	* 1.0000
			73.	12.000	* 1.0000

Figure 7

Callaway Unit 1 Cycle 5

W(z) at 16000 MWD/MTU
NOApplicable for Delta-I bands of +12%, -7%
For burnups from 16000 MWD/MTU until end of cycle

* Top and Bottom 15% Excluded as per Tech Spec 4.2.2.2G

Callaway Cycle 5

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Rev. 8~~be gained by using the burnup dependent $W(z)_{NQ}$ values.~~

The $W(z)$ values are provided for 73 axial points assuming the core height boundaries of 0 and 12 feet and intervals of .167 feet between the core boundaries.

2.6 Nuclear Enthalpy Rise Hot Channel Factor - $F_{\Delta H}^N$ (Specification 3.2.3)

$$F_{\Delta H}^N \leq F_{\Delta H}^{RTP} [1 + PF_{\Delta H}(1-P)]$$

where: THERMAL POWER
 $P = \frac{\text{.....}}{\text{RATED THERMAL POWER}}$

$$2.6.1 \quad F_{\Delta H}^{RTP} = 1.59$$

$$2.6.2 \quad PF_{\Delta H} = 0.3$$

2.7 Refueling Boron Concentration (Specification 3.9.1)

2.7.1 The refueling boron concentration to maintain $k_{eff} \leq 0.95$ shall be ≥ 2000 ppm.