

UNITED STATES OF AMERICA
NUCLEAR REGULATORY COMMISSION

BEFORE THE ATOMIC SAFETY AND LICENSING BOARD

In the Matter of

TEXAS UTILITIES GENERATING
COMPANY, et al.

(Comanche Peak Steam Electric Station
Station, Units 1 and 2)

Docket Nos. 50-445-1
and 50-446-1

CASE'S ANSWER TO APPLICANTS' STATEMENT OF MATERIAL FACTS
AS TO WHICH THERE IS NO GENUINE ISSUE REGARDING THE EFFECTS OF
GAPS ON STRUCTURAL BEHAVIOR UNDER SEISMIC LOADING CONDITIONS

in the form of

AFFIDAVIT OF CASE WITNESS MARK WALSH

1. Applicants state:

"All bolts in multiple bolt, bearing-type connections will react imposed shear loads within at most the distance of the bolt hole tolerances. (Iotti, Finneran Affidavit at 8 /1/.)"

I disagree with this statement (and with some of the statements in the Affidavit). At the point all bolts begin to react the shear loads (that is, when the last bolt will have received a 1 lb. shear load), the first bolt that has reacted the shear load may have the shear load of 1,000 lbs., and this may have exceeded the allowable shear capacity of the bolt. This is assuming that the first bolt that reacted the shear load has not failed when the last bolt begins to resist the shear load.

/1/ I believe that the actual citation should be at 4-5.

One of Applicants' primary arguments which is contained in the back-up Iotti/Finneran Affidavit is regarding the definition of "oversized" bolt holes. This is addressed in detail in answer 2. following.

One example of statements with which I disagree which is made in the Affidavit of Dr. Iotti and Mr. Finneran is found on page 5 of the Affidavit (last paragraph, continuing on page 6), wherein they cite "Structural Design Guide to AISC Specifications for Buildings," by Paul F. Rice and Edward S. Hoffman (Attachment B to Affidavit).

Although the one page (268) from that document which Applicants have attached appears to be accurate /2/, their discussion and the portion cited (which is out of context) are very misleading. (See Attachment A, pages 264 through 271 of the Rice/Hoffman text.) In the portion attached by Applicants, Messrs. Rice and Hoffman are only talking about connections that receive static loads (i.e., loads that do not change direction) because the yielding stress criteria is not applicable in friction-type connections, as will be discussed later. The connections referenced by Messrs. Rice and Hoffman specifically exclude the supports that have dynamic loads (as will be shown below) such as most of those supports at CPSES. In addition, the inelastic deformation in bearing-type connections is recognized by the AISC Code at 1.5.2.2, where the allowable bearing stress is $1.35 F_y$.

Therefore, the Applicants' statements are lacking reference to the

/2/ It should be noted that I have not reviewed the entire text of the other reference cited by Applicants, "Plastic Design of Steel Frames," and cannot state whether or not it is taken out of context.

specific amount of inelastic deformation allowed by the AISC Code for a non-dynamically loaded structure.

On pages 265-266 of the Rice/Hoffman text, following a discussion of AISC and ASTM specifications, it is stated (the numbers Messrs. Rice and Hoffman have placed in parentheses refer to sections from AISC or ASTM):

"The use of ordinary (A307) bolts is limited by a number of Specification requirements. The allowable stresses are low: tension $F_t = 20$ ksi on the threaded area; and shear $F_v = 10$ ksi (1.5.2.1). The slip before full bearing is achieved on a group of ordinary bolts effectively rules out the sharing of stress in a mixed connection. Holes are to be taken as $1/16$ in. larger than the nominal diameter (1.23.4), and the ordinary bolt does not expand to fill out the hole like a driven rivet nor can it be used for dependable friction. Stress sharing may not be assumed between ordinary bolts and rivets or welds (1.15.10; 1.15.11). In addition, low-strength bolts are not permitted in important field connections including . . . connections subject to vibration, impact, or stress reversal (1.15.12) . . . " (Emphases added.)

As discussed above, according to Messrs. Rice and Hoffmar (Applicants' own chosen authority), A307 bolts are not permitted in connections subject to vibration, such as those at Comanche Peak.

Applicants have admitted that the connections at Comanche Peak are subject to vibration. Applicants' witness Finneran stated, in regard to the support which Jack Doyle and I noticed that had failed during hydrotesting (Tr. 4793/15-4794/4):

"Q: (By Mr. Reynolds) Would you render an opinion on why the paint that Mr. Doyle talked about may have flaked during the flow of fluid through the pipe?

"BY WITNESS FINNERAN:

"A. I would say that possibly vibration may have been a cause for paint coming off of the deformed area during flow of fluid during the pipe; one possible cause.

"Q. Yes. So what you are saying is that it could have been that when the deformation was caused during construction, the paint cracked but remained on, and then when vibration occurred due to hydrostatic flow, the paint chipped off?

"BY WITNESS FINNERAN:

"A. It's a possibility. I couldn't say if that's exactly what happened." (Emphases added.)

And at Tr. 5002/24-5003/9, Mr. Finneran further testified:

"Q: (By Mr. Walsh) Is vibration a common occurrence at Comanche Peak?

"BY WITNESS FINNERAN:

"A. I think all piping systems that have fluids in them or flowing to them are possibly subject to some vibration.

"Q: How about other pipes, main steam? Will they have vibrating effects?

"BY WITNESS FINNERAN:

"A. Quite possibly there will be vibration in the main steam piping." (Emphases added.)

The ASME Code requires the Applicants to minimize vibration where it states:

"NF-3112.2 Design Mechanical Loads. . . . The requirements of (a), (b), and (c) below shall apply.

". . . (c) Component supports shall be designed to minimize vibration."

In addition, according to Messrs. Rice and Hoffman (Applicants' own chosen authority), Applicants are also barred from using A307 bolts because of stress reversal.

As indicated above, Messrs. Rice and Hoffman cited the AISC code (to which the Applicants are committed through Specification MS-46A), Section 1.15.12, which states, in part:

"Field Connections

"Rivets, high strength bolts or welds shall be used for the following connections:

". . . Connections for supports of running machinery, or of other live loads which produce impact or reversal of stress.

"In all other cases field connections may be made with A307 bolts." (Emphases added.)

CASE requested, through discovery on the issue of Applicants' Motion for Summary Disposition regarding generic stiffnesses, the drawings which the Applicants used in their Motion. Of the 60 supports which the Applicants provided (I count 59, but this is immaterial to this point), 52 had reversible loads which is a reversal of stress on the supporting connection. (See Attachment B, the referenced 59 drawings.) On the drawings, the reversal of loads is shown in the block listing the loads and the direction of the load is indicated as + or - . Of the 7 supports which do not contain reversible loads (CT-1-013-006-S22S, CT-1-013-004-S32S, MS-1-001-002-C72S, MS-1-01-001-C72S, CT-1-013-002-C42S, CC-2-011-719-A53R, CT-1-013-011-S22R), 5 are spring cans and 2 are rigid-type supports. Based on this random sample, 88% of these supports require high strength bolts due to the requirement of a reversal of stress (load) /3/, according to the AISC Code (to which the Applicants are committed in design specification MS-46A).

It is also obvious from the preceding discussions that Applicants are in violation of ANSI N45.2.11, 3. DESIGN INPUT REQUIREMENTS, 3.2 Requirements, which states, in part:

"The design input requirements should include the following where applicable:

"(9) Mechanical requirements such as vibration, stress, shock and reaction forces." (Emphases added.)

/3/ Stress is equal to the load divided by the cross-sectional area of the item under consideration.

2. Applicants state:

"Applicants' specifications for bolt hole tolerances are 1/16" for up to 1" diameter bolts and 1/8" for 1" and greater diameter bolts. (Iotti, Finneran Affidavit at 7.)"

I agree that this appears to be Applicants' current practice (although Applicants have not provided copies of the specifications themselves with their Motion for Summary Disposition). However, I do not agree with the implication, which is obviously that Applicants' specifications are acceptable. I maintain that Applicants' practice (or specifications) is contrary to applicable codes and NRC regulations.

One of Applicants' primary arguments which is contained in the back-up Iotti/Finneran Affidavit is regarding the definition of "oversized" bolt holes. This is a crucial argument for Applicants, because according to their own statement (bottom of page 6, Iotti/Finneran Affidavit):

"The 8th Edition of the AISC Manual of Steel Construction is quite instructive on this point. At page 5-58 of the Manual, Paragraph 1.23.4.3 (Attachment C) states 'Oversized holes may be used in any or all plies of friction-type connections, but they shall not be used in bearing-type connections.'" (Emphasis added.)

Applicants claim (Affidavit, page 7) that they use more stringent tolerances than defined by the AISC Code (to which Applicants are committed, according to their Design Specification MS-46A). A claim the Applicants make in the Iotti/Finneran Affidavit (page 7) is:

"AISC defines 'oversized' as $d + 3/16$ " for bolts up to and including 7/8" diameter, $d + 1/4$ " for 1" bolts, and $d + 5/16$ " for bolts greater than or equal to 1 1/8" (sic) diameter."

I do not agree with Applicants' representation as to AISC's definition of "oversized." A point which the Applicants fail to make is as shown in Attachment C to their Affidavit, AISC Table 1.23.4, "Maximum Sizes of Fastener Holes, Inches" (emphasis added) -- that is, that these are the maximum size of holes. For a 1" diameter bolt, the maximum size hole for a standard hole is 1-1/16". If the hole is greater than 1-1/16" up to and including 1-1/4" for a 1" diameter bolt, the hole is considered oversized.

It is apparent that the Applicants do utilize an oversized hole for the 1" and greater bolts. As stated previously, paragraph 1.23.4.3 of Attachment C of the Applicants' affidavit (from 8th Edition, AISC Manual of Steel Construction, page 5-58), states:

"Oversized holes may be used in any or all plies of friction type connections, but they shall not be used in bearing type connections." (Emphasis added.)

It can be seen from what is shown above that bearing type connections can only be used with standard size holes. If the hole is greater than a standard size hole, bearing connections are not allowed. Therefore, the Applicants are not in compliance with the AISC Code to which they are committed (according to their design specification MS46-A).

On page 7 of Applicants' affidavit, they state:

"Thus, Applicants' specifications for bolt hole tolerances can definitely not be called 'oversized,' as that term is generally used in the construction industry."

Although the Applicants have not sized their bolt holes to the maximum allowed for an oversized condition, the bolt hole is still an

oversized hole (as discussed above). And, as the term is generally used in the construction industry, holes are considered to be oversized if they are over a standard sized hole, up to and including the maximum oversized hole allowed. Contrary to what Applicants state (Affidavit, page 7), they are not in compliance with standard industry practice.

There are several aspects of this matter of which the Board should be aware. One of the most important is whether or not Applicants even attempt to determine the size of bolt holes and, if so, how? During the 6/6/84 telephone conference call between Applicants/NRC Staff/and me, I requested documentation (original and all revisions of procedures or whatever other documentation exists) showing that QC inspectors inspect the whole tube steel base plates prior to inserting the bolt (which is the only way QC could be certain when inspecting that there were no oversize holes). (See 6/6/84 conference call Tr. 74-76.)

In Applicants' 7/15/84 letter to CASE President Juanita Ellis (received by CASE 7/16/84), Applicants' counsel stated (page 2, second full paragraph):

"Second were materials concerning Applicants' practice regarding the inspection of bolt holes in base plates, which relates to the motion concerning the effect of gaps. This information is attached. Copies of an example of the Material Identification Log, and the associated hanger drawing, for support H-BR-2-5B-001-009-3 are provided. This log is filled out by the QC inspector prior to release of materials, including base plates, from the fabrication shop. Although not separately called out on the log, one of the attributes of base plates the QC inspector examines is bolt hole size." (First emphasis in the original; second emphasis added.)

I agree with the statement of Applicants' counsel that the

inspection of base plates for bolt hole size is not separately called out on the Material Identification Log, and in reviewing these documents (see Attachment C), I see no reference to the QC inspectors' verifying the hole size.

There is additional information which indicates that QC inspectors do not inspect for oversize bolt holes. In the sworn affidavit of Howard J. "Robbie" Robinson (sent to the Board and parties with CASE's 11/28/83 Answer to Board's 10/25/83 Memorandum (Procedure Concerning Quality Assurance)), Mr. Robinson stated (page 7):

"My duties as general foreman over the fab shop consisted of fabricating items such as pipe hangers, cable tray hangers, and Q miscellaneous steel assemblies for subsequent installation in the field. . . I did, over a period of about three years, engage in an ongoing argument with one of the foremen within the steel hanger department whose duty was to install hangers in the field where he challenged the practice in the fab shop of drilling 1" holes in base plates to the code allowable of 1-1/16" diameter for a 1" bolt. His stand had been that we were allowed to overdrill the hole to a 1-1/8" diameter. . . he . . . made the statement to me that he had been drilling them oversize all along and intended to continue to. If he in fact did drill these holes oversize, and I believe that he did, one must assume that any subsequent QC inspection failed to identify this." (Emphases added.)

(See also discussion under answer 2. preceding.)

Further confirmation of what I believe to be the truth of this matter is to be found in a document concerning an investigation conducted by Applicants into allegations which had been made. (See Attachment D, 3/9/84 TUGCO Office Memorandum to Distribution from Jerry C. Walker, Subject: Resolution of QAI-0001, and the attached 2/22/84 TUGCO Office Memorandum from Boyce Grier to Antonio Vega, Subject: Investigation of Allegations QAI #0001.) Item 3, page 2, of the

2/22/84 Memorandum discusses allegations of an alleged that an oversize hole (1-1/2") had been drilled for a 1-1/4" Hilti bolt in a hanger base plate (i.e., a hole 1/4" larger in diameter than the bolt). Mr. Grier states that he subsequently identified the support in question as CC-2-070-002-A33R (copy of the as-built drawing for the support is Attachment F to his report). He further states:

"There is nothing in the documentation package for this pipe support to indicate a requirement for or the approval of an oversize hole. I reviewed the reports of the QC inspections for the Hilti installation for this support. These are contained in the following:

"IRMH-19682, dated 7/1/81
"IRMH-53200, dated 2/15/83
"IRMH-53257, dated 2/22/83

"These reports do not indicate any nonconforming or unsatisfactory conditions. (Blacked-out) stated during his interview that he had no knowledge of oversize holes ever being drilled for Hilti bolts.

"I made inquiry of pipe support engineering (Jay Ryan) as to whether an oversize hole for a Hilti bolt in the support in question would be of concern. I was told that it would not be a problem.

"The allegation that an oversize hole had been drilled for a Hilti bolt could neither be confirmed or dismissed. It appears that physical inspection of the holes for the support in question would be the only way to resolve this matter. In view of the response from Engineering regarding the significance of this matter, it does not appear necessary to pursue the matter further." (Emphases added.)

Thus, the investigator reviewed the documentation packages and saw no indication of an oversize hole or of a requirement for or the approval of an oversize hole. He reviewed the reports of the QC inspections, which did not include the Material Identification Log which Applicants' counsel referenced as being the documentation I

requested regarding Applicants' practice for the inspection of bolt holes in base plates. When he checked with pipe support engineering (Jay Ryan), he was told that the 1/4" oversize bolt hole would be no problem, although no basis is given in the report for Jay Ryan's disposition of the problem. Based on Jay Ryan's position, the investigator ceased his investigation -- even though he admitted that he could neither confirm or dismiss the allegation.

Therefore, as demonstrated above, Applicants' statement that they have no oversize holes (including those greater than the 1/8" criteria Applicants claim to use) is without substance.

3. Applicants state:

"Test data indicate that bolts of the kind Applicants use have margins of safety for shear displacements equal to the maximum bolt hole tolerances ranging from 5.6 (1 1/4" super kwick Hilti) to 3.2 (1 1/4" Richmond Inserts). (Iotti, Finneran Affidavit at 8-9.)"

I agree with this statement, but I do not see where it is material to the Board. This statement discusses displacements only. For the Applicants to be in compliance with IE Bulletin 79-02, the factor of safety must be based on ultimate load, not displacement.

Using the test data shown in Attachment A to Applicants' testimony in September 1982 (Applicants' Exhibit 142D, admitted at Tr. 4794, Attachment B), for a 3/4" diameter Hilti bolt loaded in shear, the load at 1/8" displacement is 10,000 lbs. The allowable load as listed in the PSE Manual (see Attachment E, PSE Manual, Section V, Hilti Concrete Anchor Bolts, Rev. 0, 1/8/82, page 8 of 10, Figure 6) is 3,693 lbs. for

a 3/4" diameter Hilti with 9-1/4" embedment. Therefore at 1/8" displacement, the Hilti bolt has exceeded its allowable by $10,000/3,693 = 2.71$.

The same philosophy can be used for the Richmond insert. Referring to Applicants' Exhibit 142D, Attachment C, sheet labeled 5, at a displacement of .125" (1/8"), the shear load is approximately $(14 + 16) / 2 = 15$ kips. The capacity for a 1" diameter A307 bolt is 7.85 kips. Therefore, the load in the bolt has exceeded the established allowable by $15/7.85 = 1.91$.

In addition, in the design of pipe supports at CPSES, the designer assumes the support is rigid at the bolted connections and does not move, and determines the stiffness of the support or determines the deflection for the support based on this assumption (that is, that the bolted connections don't move). Now the Applicants are stating that the bolted connections by themselves will move 1/8". It would appear that the Applicants are not utilizing appropriate design assumptions. Only if the Applicants were utilizing friction type connections, would their assumptions be proper.

At this time it would be appropriate to bring to the Board's attention what I believe Applicants are up to. The Applicants, in this Motion for Summary Disposition, are addressing the consequences of gaps in bearing type connections. The Applicants have claimed to this Board on the record (for example, Tr. 5154/18-5154/15, 5161/7-25, and 5208/1-17) that they utilize bearing type connections in the design of base

plates utilizing Hilti bolts. But in response to one of Cygna's questions in regards to Hilti bolts, the Applicants informed Cygna that they are designed as friction type connections and will not move because they are pretorqued. See Attachment F (copy of the 4/19/84 letter, with relevant attachments, from L. M. Popplewell, Project Engineering Manager, TUGCO, to Ms. Nancy Williams, Project Manager, Cygna Energy Services), wherein Applicants state (bottom of page 9):

"Using our design approach, the Hilti joints, since they are pretorqued, would perform as a friction joint within their working loads." (Emphasis added.)

This is a complete reversal of philosophy by the Applicants, not presented to the Licensing Board before. At Tr. 5208/1-7, Dr. Chang states that the loads due to pretorquing are to set the wedges and the pretorque value used is too small to be considered sufficient as a friction-type connection.

It is apparent that the Applicants are singing a different song in their response to Cygna. There is no indication within the Phase 3 Cygna Report that Cygna investigated whether or not the Hilti bolts are torqued sufficiently to be considered as a friction-type connection.

One must consider whether or not the statement made to Cygna is true (i.e., the pretorque provided to the Hilti bolts is sufficient to consider them as friction connections). The allowable shear force assuming a safety factor of 2 can be calculated by the following formula modified from the Applicants' Motion for Summary Disposition on cinched-up U-bolts, page 14 of Affidavit, modified to accommodate the shear force requirement:

$$V = (T/K \times D)(.4)/FS$$

where V = the allowable shear capacity

.4 = the coefficient of friction between concrete and steel

K = torque coefficient = .3

D = diameter of bolt (say, a 3/4" diameter)

T = the applied torque

FS = factor of safety = 2

The Brown & Root procedures shown in CASE Exhibit 669B (Attachment to Deposition/Testimony of CASE Witness Jack Doyle), sheet 10P, for a 3/4" diameter bolt has a required torque of 150 foot-lbs.

The allowable shear value is thus

$$1/2 ((150)(12) / (.3)(.75)) (.4) = 1,600 \text{ lbs.}$$

The allowable listed in the PSE Manual for a 3/4" diameter Hilti bolt is 3,693 lbs. or a $(3693/1600)(100) = 231\%$ difference.

The above analysis does not include creep effects on the concrete; these effects will decrease the pretorqued value. The coefficient of friction between the nut and the Hilti bolt was assumed to be .3. Therefore, my analysis is on the very liberal side, and the Applicants' statement to Cygna that the Hilti bolt connection is a friction connection is lacking proper consideration.

In addition, when Brown & Root tested the Hilti bolts for compliance to IE Bulletin 79-02 and compared pretorque to ultimate load, they neglected to consider an important factor. This factor is that Brown & Root did not measure the load induced into the bolt due to

pretorquing, but rather the ultimate load due to pretorquing in a tension test. To have measured the pretorqued value would have required Brown & Root to measure the displacement of the bolt due to an applied load. When the bolt first begins to displace is when the pretorqued value is determined.

4. Applicants state:

"Consideration of all bolts in multiple bolt, bearing connections, with bolt hole tolerances equivalent to those used by Applicants, to react shear loads equally is accepted industry practice and is premised on the fact that the inelastic localized deformations that could result from self-limiting stresses do not unacceptably reduce the ultimate bolt capacity. (Iotti, Finneran Affidavit at 5-7.)"

I disagree with this statement. As already discussed above, accepted industry practice does not allow bearing-type connections when the bolt hole is greater than the maximum standard sized hole. The inelastic localized deformations that the Applicants are relying on have limitations that the Applicants failed to address, as shown above; i.e., allowable bearing stresses and when bearing connections can and cannot be used. Therefore, the conclusion that the Applicants have attempted to make is not complete and violates established code allowables and industry practice.

5. Applicants state:

"The report CASE relied on (CASE Exhibit 1001) to support its contention that at most two bolts may be considered to react shear loads in multiple bolt, bearing connections addressed connections in which bolt hole tolerances from 1.33 times bolt diameter, up to 1/2" for 1" bolts, may be present.

"These conditions could result in a safety factor for shear displacement of only 1.1. (Iotti, Finneran Affidavit at 9-10)."

I disagree with the first sentence. As stated above, the inelastic deformations that occur with the Applicants' position will exceed established code allowables (i.e. allowables based on load, not displacement) with these oversized holes the Applicants use. What Dr. Fisher (referenced in the Iotti/Finneran Affidavit) was addressing was a warning to engineers and designers of the new Code provisions; i.e., an allowance for excessively oversize holes in column base plates where tensile forces are not commonly seen, and the shear force is accommodated by the compressive load of the column. With the old Code (i.e., the 7th Edition), no oversize hole was allowed with A307 bolts to resist a shear load. But the new Code not only allows the oversize hole but the hole can be larger because, as Dr. Fisher states, columns are generally not experiencing tensile loads. Therefore, Dr. Fisher provides methods to accommodate connections for columns that do not contain sufficient compressive loads.

I partially agree with the second sentence, to the extent that it is correct when one considers displacement only, and not allowable stress, for a nuclear power plant.

6. Applicants state:

"In a seismic event, only the first quarter cycle loading could cause preferentially loaded bolts to deflect in shear.

"For the remainder of the cycles the bolts will equally react the loading (Iotti, Finneran Affidavit at 13.)"

I agree with the first and second sentences; however, they are not reflective of the true extent of the problem, as discussed in the following.

The Applicants' example and position is demonstrated in Figure 1 below. At the end of the first quarter cycle loading on a two-bolt base plate, the bolt that reacts first may deform at the peak of the cycle, as shown in Figure 1b below, as the Applicants state. And as shown in Figure 1c, the bolt is permanently deformed. In addition to this, Applicants have another flaw in their presentation. They assume that the bolt is behaving in a ductile manner, under a shear load. This assumption is not consistent with the following statement from NRC Regulatory Guide 1.124 ("Service Limits and Loading Combinations for Class 1 Linear-Type Component Supports," admitted at Tr. 5901, page 1.124-2, B.1.b.):

"The increase permitted by NF-3231.1 and F-1370(a) of Section III for shear stresses or shear stress range should not be more than 1.5 times the level A service limits because of the potential for non-ductile behavior." (Emphasis added.)

Nowhere in ASME NF are the level A service limits or the AISC Code for shear stress allowed to exceed the yield strength of the material. Therefore, the Applicants are in violation of the ASME code, as well as the AISC Code, when they allow the bolts to exceed the yield strength in shear and deform.

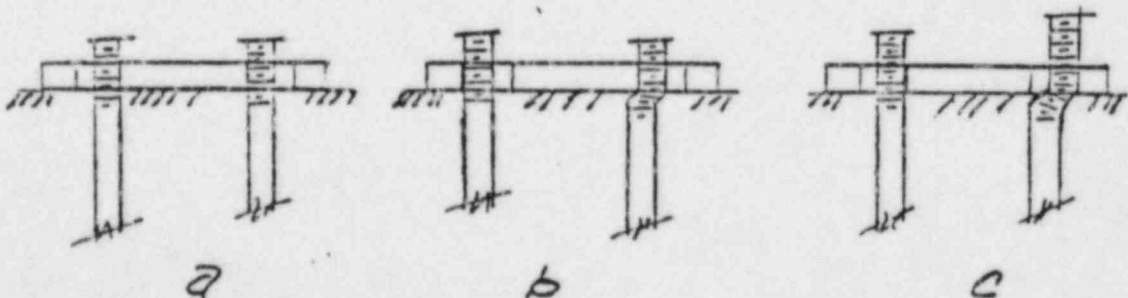


FIGURE 1

The above example consisted of a stiff plate and a flexible bolt. Another condition can also occur, and that is a stiff bolt and a flexible plate, as shown in Figure 2 following.

As shown in Figure 2b, at the end of a 1/4 cycle the original circular hole for bolt A has deformed into an elliptical type of configuration. At the end of the 1/2 cycle, there is now a gap on both sides of bolt A, as shown in Figure 2c below, and there is no bearing between bolt A and the plate. At the end of the 3/4 cycle, the hole for bolt B has now deformed into an elliptical type of configuration, as shown in Figure 2d. At the end of the first full cycle, as shown in Figure 2e below, there are now two permanently elliptical-type holes with gaps twice as large as before the cyclic motion began, and neither bolt A or B is in bearing. If the original gap for a 1" diameter bolt was 1/8", the gap now is 1/4", and this would definitely be considered an oversized hole in that particular direction. This is not allowed for bearing type connections, as Applicants should agree.

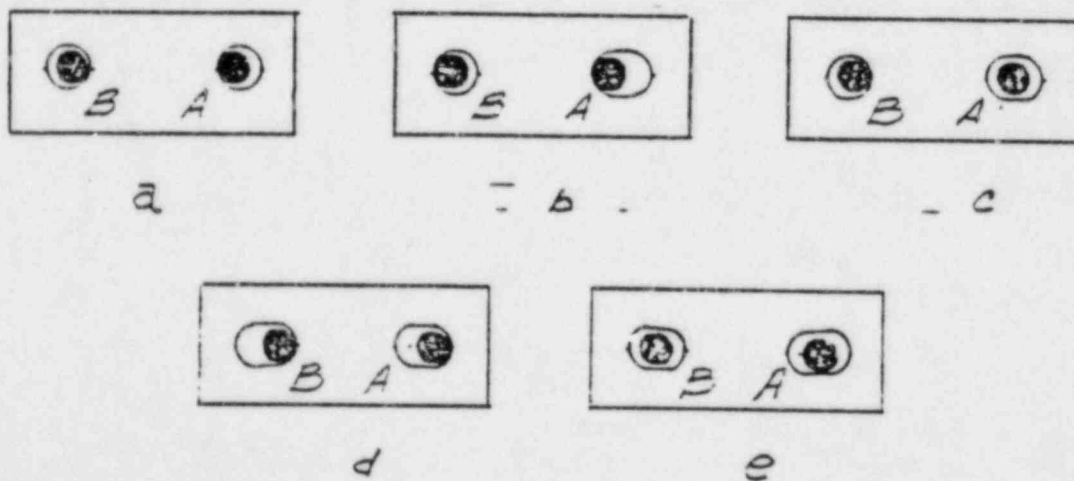


FIGURE 2

The deformation discussed in example 2 is possible since the AISC Code at 1.5.2.2 allows the bearing stress of the plate to exceed the yield strength of the plate in the bearing type connection. The deformation discussed in example 1 (the condition which the Applicants cite) is possible, but would conflict with Regulatory Guide 1.124. And nowhere in the AISC Code is the bolt stress allowed to exceed the yield strength in shear.

Example 2 is realistic when one considers the A307 bolt/tube steel/Richmond insert condition. When the axial force from the tube steel member is transferring this axial load to the bolt by means of shear, the NRC Special Inspection Team (SIT) (as well as the Applicants) claimed that approximately 85% of the axial force being transferred as shear is in the flange of the tube steel member closest to the concrete. The thickness of the tube steel is at most 1/2" thick and the bolt is 1-1/2" diameter (minimum) for supports within the containment. The bolt is designed for an allowable stress value equal to 10 ksi (from Table 1.5.2.1 of the AISC Code, 7th Edition), yet the allowable bearing stress of this thin tube steel member has an allowable of 48.6 ksi for yield strength equal to 36 ksi. The allowable capacity for a 1-1/2" diameter bolt is equal to 17.67 kips. Due to the high allowable for bearing stress, the allowable force for the tube steel member is equal to 36.45 kips. This high allowable will permit deformations for the bearing type connections when cyclic loads are not a consideration. For this reason, example 2 shown above is more realistic for the supports at Comanche Peak than the Applicants' example and position. In either case, the gap is an unacceptable

condition for a dynamically loaded structure, and is not permitted under the AISC Code, Section 1.15.12 discussed in item 1, page 3, of this affidavit.

7. Applicants state:

"The effect of gaps in seismic analyses cannot be defined in absolute terms. The effect is dependent on many factors, including the nature of the excitation (magnitude and distribution of frequencies), and the size, orientation and number of gaps. (Iotti, Finneran Affidavit at 13-14.)"

As indicated on page 14 of the Applicants' Affidavit, the existence of gaps in bearing type connections is a very complicated issue by the fact that non-linearities introduce additional impact loadings, as well as impact damping, and as the Applicants stated:

"Clearly, consideration of such effects would require complex analyses which depart from accepted practices." (Page 14 of Affidavit.) Not only do I agree with this statement, but the AISC Code has recognized the complexity of the gap in bearing type connections due to cyclic loads. Paragraph 1.15.12 Field Connections requires high strength bolts for supports which produce impact or reversal of stress, as discussed above in Answer 1, page 3 of this Affidavit.

Therefore, the complexity to which the Applicants refer is their own doing. The Applicants decided to use bearing type connections with low strength bolts, and consequently are now attempting to justify their erroneous decision. The Applicants have resorted to crying on the Board's shoulder about how complex it would be if they were required to analyze the supports as they now exist.

8. Applicants state:

"Impact damping also occurs in seismic events where gaps are present.

"To account for this damping, however, would require consideration of effects that require complex analyses which depart from accepted design practices. (Iotti, Finneran Affidavit at 14.)"

I agree with the first sentence.

I agree with the second sentence, as discussed above in answer 7.

However, I disagree with their back-up statement on page 14 of the Iotti/Finneran Affidavit, that the impact damping values would be greater than those specified by Regulatory Guide 1.61, for the following reasons: If the Applicants' position is that a higher damping value would be allowed for bearing type connections, it is obvious that Regulatory Guide 1.61 does not allow bearing type connections for cyclic loads, or it would have been listed as a specific item, with a higher damping value. But since bearing-type connections are not common industry practice for seismically qualified supports, Regulatory Guide 1.61 did not list it. Therefore, the Applicants' conclusion that a higher damping value should be allowed due to the bearing type connection would conflict with Regulatory Guide 1.61, as well as the AISC Code (to which Applicants are committed.)

9. Applicants state:

"Material damping will take place as the gap is transversed without a corresponding feed of energy from the seismic event.

"This is a beneficial effect for the seismic response of the system. (Iotti, Finneran Affidavit at 14-15.)"

I agree with the first sentence, as far as it goes, and if one is not concerned with the inelastic behavior and unpredictable behavior of the connection.

I disagree with the second sentence, because you lose the ability to predict the response of the system; you do not know where supports will be moving due to the bearing type connection; you do not know which supports will have the inelastic deformations of the bolts.

10. Applicants state:

"Each of the factors discussed in Findings 7-9 cannot be accounted for in the typical linear response spectrum analyses, as are used at Comanche Peak. (Iotti, Finneran Affidavit at 15.)"

I agree with this sentence, but that does not necessarily mean that the Applicants' position is a correct one. To begin with, IE Bulletin 79-02 required the Applicants to perform tests on expansion anchor bolts. The Applicants neglected to measure the amount of displacement that occurs at the allowable shear value. This is the Applicants' own negligence.

Another important factor which the Applicants were negligent on is the use of the Richmond insert/A307 bolt/tube steel connection. 10 CFR 50.34(a)(2) states:

"50.34 Contents of applications; technical information

"(a) Preliminary safety analysis report. Each application for a construction permit shall include a preliminary safety analysis report. The minimum information to be included shall consist of the following: . . .

"(2) A summary description and discussion of the facility, with special attention to design and operating characteristics, unusual or novel design features, and principal safety considerations." (Emphasis added.)

This Richmond insert/A307 bolt/tube steel connection is not mentioned in the Applicants PSAR, although it is unusual and novel, as I have stated and the Applicants' own witnesses have admitted. (See Walsh, Tr. 3145/6-3146/8; Krishnan, Finneran, Scheppele, Reedy, and Chang, Tr. 5061/18-5065/8.)

In addition, during the 7/3/84 meeting in Bethesda between the NRC Staff and Cygna Energy Services regarding the Cygna Phases 1 and 2 Independent Assessment Program, during a discussion between the Staff's Mr. Terao and Cygna's Ms. Williams, Mr. Terao also indicates that he recognizes that this is an unusual and novel design and points out the importance of the design organization's (such as Gibbs & Hill) having followed ANSI N45.2.11, Section 6.2, which states:

"The extent of the design verification required is a function of the importance of the safety of the item under construction, the complexity of the design, the degree of standardization, the state of the art, and the similarity with previously proven designs."

Mr. Terao discusses examples of an unconventional design, then states (7/3/84 Meeting Tr. 57):

"I don't really see that there's a problem with Richmond inserts, just like there is no problem with the modeling of dual function restraints, in other words, just the Richmond inserts alone, taken by themselves, there's no problem."

"But it has to do with the design considerations that go along with it. And one of design considerations is the use of the tube steel with the holes in it as anchorage for the Richmond insert."

(See full discussion, 7/3/84 Staff/Cygna meeting Tr. 50-57.)

11. Applicants state:

"Each of the factors discussed in Findings 7-9 can only be accounted for with difficulty by performing nonlinear time history analyses. (Iotti, Finneran Affidavit at 15.)"

I agree with this statement. Based upon this statement by itself, it would seem reasonable that the Board require the Applicants to either perform the non-linear time-history analysis which they reference above or utilize a friction-type connection in the supports that are already constructed. But, as discussed in answer 12. below, the utilization of a friction-type connection would validate the assumptions the designers used in their original analysis.

12. Applicants state:

"Identifying the effects of gaps by comparison of the results of nonlinear time history (with gaps) and response spectrum (without gaps) analyses is difficult and one may not discern whether particular results are attributable to differences in individual variables or assumptions or the analytical techniques themselves. (Iotti, Finneran Affidavit at 15-16.)"

I agree with this statement. From what the Applicants have just stated, it would appear that they must be required to install at all supporting connections a friction-type connection to validate their original assumptions, and to have them fabricated as friction-type connections. The Applicants may, in the future, state that their being required to redesign their supports for friction-type connections would be costly (in the hopes that the Board will give them yet a third chance), but as stated above in the previous answers, the Applicants should have done it right to begin with.

13. Applicants state:

"Comparison of the results obtained by response spectra analyses and nonlinear time history analyses which simulate actual gaps in systems show that

- "a) the seismic response spectrum method, which ignores the nonlinearities, is more conservative than the non-linear time domain method (which includes gaps), and
- "b) the effect of gaps on reduction of response frequency is negligible due to the transient nature of the seismic acceleration loading."

"(Iotti, Finneran Affidavit at 16-17.)"

I disagree with Applicants' statements, because if what Applicants state were true, the AISC Code would allow bearing type connections in dynamically loaded structures and supports -- it does not. If the Applicants wish to use the nonlinear time domain method (which includes gaps) to be less conservative than the response spectra method, that would be their option; but as stated above in answer 12, this is not realistic.

In summary, I believe that the Applicants did not properly consider the effects of gaps in the initial or final (i.e., vendor certified) design of pipe supports. The AISC Code does not allow bearing type connections in supports where there is a cyclic type load. The Applicants, on the majority of their supports, have cyclic type loads. They utilize bearing type connections and are therefore in conflict with the AISC Code (to which they are committed). The Applicants rely on references to inelastic deformations to justify their position but omit the consideration of full cyclic loads in the inelastic deformation discussions. They depend on damping factors that are not recognized by the NRC in Regulatory Guide 1.61 for a

justification, after the fact, of their negligence. Because of these gaps, the Applicants are not able to predict how these systems will react to imposed loadings.

If they planned to use this unusual and unique design, Applicants should have initially included it in their PSAR -- they did not. They freely admit that it would be difficult to properly analyze the as-built condition of the supports as they now exist. And finally, Applicants state that the gaps that do exist at Comanche Peak in pipe supports (which I believe are in violation of the AISC Code) are more conservative than the Code requires the Applicant to comply with. In essence, Applicants are trying to convince the Board that not complying with the AISC Code is conservative. I do not agree.

Attachments:

Attachment A -- "Structural Design Guide to AISC Specifications for Buildings," by Paul F. Rice and Edward S. Hoffman, pages 264 through 271 -- (see answer 1, page 2)

Attachment B -- 59 drawings (received on discovery re: Applicants' Motion for Summary Disposition regarding generic stiffnesses), demonstrating reversible loads -- (see answer 1, page 5)

Attachment C -- Copies of an example of the Material Identification Log and associated hanger drawing for support H-BR-2-5B-001-009-3, regarding Applicants' practice re: inspection of bolt holes in base plates -- (see answer 2, pages 8-9)

Attachment D -- 3/9/84 TUGCO Office Memorandum to Distribution from Jerry C. Walker, Subject: Resolution of QAI-0001, and attached 2/22/84 TUGCO Office Memorandum from Boyce Grier to Antonio Vega, Subject: Investigation of Allegations QAI #0001, regarding allegations of oversize bolt hole -- (see answer 2, pages 9-10)

Attachment E -- PSE Manual, Section V, Hilti Concrete Anchor Bolts, Rev. 0, 1/8/82, page 8 of 10, Figure 6, re: allowable load for Hilti bolt -- (see answer 3, pages 11-12)

Attachment F -- 4/19/84 letter with relevant attachments, from L. M. Popplewell, Project Engineering Manager, TUGCO, to Ms. Nancy Williams, Project Manager, Cygna Energy Services, advising Cygna that Hilti joints perform as a friction joint -- (see answer 3, page 13)

The preceding CASE's Answer to Applicants' Statement of Material Facts As To Which There Is No Genuine Issue was prepared under the personal direction of the undersigned, CASE Witness Mark Walsh. I can be contacted through CASE President, Mrs. Juanita Ellis, 1426 S. Polk, Dallas, Texas 75224, 214/946-9446.

My qualifications and background are already a part of the record in these proceedings. (See CASE Exhibit 841, Revision to Resume of Mark Walsh, accepted into evidence at Tr. 7278; see also Board's 12/28/83 Memorandum and Order (Quality Assurance for Design), pages 14-16.)

I have read the statements therein, and they are true and correct to the best of my knowledge and belief. I do not consider that Applicants have, in their Motion for Summary Disposition, adequately responded to the issues raised by CASE Witness Jack Doyle and me; however, I have attempted to comply with the Licensing Board's directive to answer only the specific statements made by Applicants.

Mark Walsh
(Signed) Mark Walsh

STATE OF TEXAS

On this, the 12 day of August, 1984, personally appeared Mark Walsh, known to me to be the person whose name is subscribed to the foregoing instrument, and acknowledged to me that he executed the same for the purposes therein expressed.

Subscribed and sworn before me on the 12 day of August, 1984.

Samuel W. Nestor
Notary Public in and for the
State of Texas
SAMUEL W. NESTOR
My Commission Expires
1-31-85

My Commission Expires: _____

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Structural Design Guide to AISC Specifications for Buildings

Paul F. Rice
Edward S. Hoffman



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This book is intended to provide designs with the specifications for steel and joist construction.

Each new AISC Specification language for safe structural plastic design, each new economy of material with design calculations.

The increasing complexity for design. Computer, however, and computer.

This Guide does not replace the Manual of Steel Construction, shows how to use the Manual. It converts specifications to direct design. It provides design.

Tables 3-1 and 3-2 provide AISC equations for all beam section, or solution about three minutes.

Specification requirements have been assembled for frames, composite construction based on structural steel discussed to aid the structural specifications.

It is assumed that use as well as the terms and requirements in the or

5

CONNECTIONS

General

The latest AISC Specifications permit a wide variety of connections. The basic requirement, appropriate with the sophisticated combinations of different types of steel to be connected, different design requirements of connections, and different means of connections, is a performance requirement consistent with the overall development of the Specifications. This requirement states simply "... that the design of connections be consistent with the assumptions as to the type of construction..." (1.2). Each of the detailed requirements for the design of connections simply builds upon this basic requirement. By implicitly or explicitly requiring that the design of a particular type of connection be consistent with the design assumptions as to the type and amount of force to be transmitted, and rotation capacity (or rigidity) consistent with the rotation assumed necessary to develop the connection forces, the basic performance requirement is completed (1.2).

The Specifications explicitly recognize inelastic behavior in connections of members designed as elastic: "virtually unchanged" angles at the joints in rigid frames, "non-elastic" deformation of parts of connections in Type 2 and 3 construction, and "inelastic rotation" for wind connections with Type 2 construction (1.2). Elastic behavior in the connections of members under plastic design is implicitly recognized (2.1).

Scope

For the purposes of this Chapter, connections are most conveniently considered as classified on two bases; (1) materials used (rivets, bolts, pins, or welds), and (2) the assumed behavior of the connection (design requirements: rigid, semi-rigid, or plastic for moment; shear transmission only; tensile or compressive force only; or combinations). In addition to forming joints between two or more steel members or parts of members, connections are required to elements composed of other structural materials. For composite action with concrete elements not bonded by encasement, shear connections are required (1.11.1). Shear connections may utilize specially designed shear connectors or standard welded stud connectors (1.11.4; 1.4.6). For connection of steel column bases to transmit any direct tension or shear, anchor bolts are required (1.22).

It is not intended in the *AISC Handbook*, presentation of a wide search in this area. (See explanations and illustrations overlooked or troublesome interpretations to the extension of such interpretations been desirable to extend plate connections were design to cover an applicable Code. During the interim revised to agree with the

Rivets, Pins, and Bolts

Rivets and Pins. The requirements have been directed toward there has been little change the requirements for, as in little need for interpretation available under ASTM are given in Table 1.5. (1.14.2); computed as $\frac{1}{16}$ diameter of the rivet hole.

The use of pin connections in modern steel building, requiring special design. The requirements have remained unchanged from previous editions.

Perhaps the most useful alterations or additions to construction, bearing-type connections (1.15.10). If used in connections strengthening existing connections to place loads, and the new

Bolts. Bolts may be classified as A325, for $F_t = 40$ ksi, and A307 bolts are usable. They may be designed for either

The use of ordinary bolts. The allowable stresses are 10 ksi (1.5.2.1). The specification rules out the $\frac{1}{16}$ in. larger than the nominal fill out the hole like a plug. In addition, low-strength column splices in all cases where width/height < 4

It is not intended in this chapter to duplicate the design aids, detail data, and examples in the *AISC Handbook*, Part 4, Connections. Equally, space limitations do not permit presentation of a wide range of examples to illustrate even the recently published research in this area. (See "Selected References".) Rather, the purpose here is limited to explanations and illustrations of all applicable Specification requirements that might be overlooked or troublesome in routine work. This aim will include indication of reasonable interpretations to resolve apparent conflicts or ambiguities in the Specifications, and extension of such interpretations where the Specifications seem to have omissions. It has been desirable to extend this aim somewhat in that design aids for bearing plate and base plate connections were included as well as an extension of concrete bearing connection design to cover an apparent gap between the AISC Specifications and the ACI Building Code. During the interim between preparation and publication, AISC specifications were revised to agree with the latest ACI Building Code.

Rivets, Pins, and Bolts

Rivets and Pins. The requirements for the use of rivets and pins were established many years ago and were in many AISC Specifications. Since most of the late research has been directed toward welded, and more recently high-strength bolted connections, there has been little change in the Specifications for the use of rivets. Familiarity with the requirements for, and a sharply reduced use of, rivets in building construction results in little need for interpretations of these Specifications. Rivets of Grades 1 and 2 are available under ASTM A502 (1.4.2). Allowable stresses (for tension and bearing only) are given in Table 1.5.2.1 (1.5.2.1). Net sections for tension members must be used (1.14.2); computed as prescribed (1.14.3); and allowance of $\frac{1}{16}$ in. made plus the nominal diameter of the rivet holes (1.14.5).

The use of pin connections, originally popular in truss construction, has declined in modern steel building, and is usually encountered only for very special situations requiring special design. The general requirements for the use of pins are brief and essentially unchanged from previous Specifications (1.14.6).

Perhaps the most used application of these Specification requirements today will be in alterations or additions to existing buildings in which rivets or pins were used. For new construction, bearing-type connections can not be assumed to share stress with welds (1.15.10). If used in combination, the welds must be designed for the entire stress. In strengthening existing construction, bearing connections can be assumed to carry the in-place loads, and the new welds designed only for the additional stress (1.15.10).

Bolts. Bolts may be classified by strength as (1) low, A307, for $F_t = 20$ ksi; and (2) high, A325, for $F_t = 40$ ksi, and A490, for $F_t = 54$ ksi . . . (1.5.2.1). The ordinary low strength (A307) bolts are usable only in bearing connections (1.5.2.2). The high strength bolts may be designed for either bearing or friction connections (1.5.2.1).

The use of ordinary (A307) bolts is limited by a number of Specification requirements. The allowable stresses are low: tension $F_t = 20$ ksi on the threaded area; and shear $F_v = 10$ ksi (1.5.2.1). The slip before full bearing is achieved on a group of ordinary bolts effectively rules out the sharing of stress in a mixed connection. Holes are to be taken as $\frac{1}{16}$ in. larger than the nominal diameter (1.23.4), and the ordinary bolt does not expand to fill out the hole like a driven rivet nor can it be used for dependable friction. Stress sharing may not be assumed between ordinary bolts and rivets or welds (1.15.10; 1.15.11). In addition, low-strength bolts are not permitted in important field connections including column splices in all buildings with $H \geq 200$ ft., and where width/height < 0.25 ; also where width/height < 0.40 , for $H \geq 100$ ft.; beam-column or column-bracing connections

where $H > 125$ ft.; frames carrying cranes with more than five-ton capacity; and connections subject to vibration, impact, or stress reversal (1.15.12); nor for flange-to-web nor cover plate-to-flange connections of built-up girders (1.10.4).

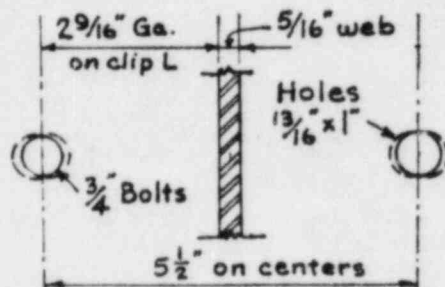
High strength bolts (1.16.1) and welds are considered essentially equivalent as connections, and, for friction-type joints assembled prior to the welding, the high-strength bolts may be assumed to share stress with welds in a mixed connection (1.15.10) or with rivets (1.15.11). Gross sections may be used for the design of compression members (1.14.2), and for the flanges of both built-up and rolled-shape girders provided the area of holes is equal to or less than fifteen percent of gross flange area (1.10.1). For tension members net section area is the basis of design (1.14.2). In friction-type joints resisting direct tension, the shear stress permitted with high strength bolts must be reduced (1.6.3).

Slotted Holes for Bolted Shear Connections. The use of short-slotted holes is permitted under 1974 AISC Specification for "Structural Joints Using ASTM A-325 or A-490 Bolts," Section 3, subject to the approval of the designer. They can be used in either friction-type or bearing-type connections, provided a washer is installed over the hole.

The normal hole size for a $\frac{3}{4}$ " ϕ bolt is $\frac{13}{16}$ ", whereas a short-slotted hole is $\frac{13}{16}$ " deep by 1" long (or $\frac{3}{16}$ " longer in the horizontal dimension). While the Specifications state that the hole can be either vertical or horizontal, the authors suggest only the horizontal slotted method be used. End clip holes only would be slotted, not the holes in the connection beam or column. See sketch, a full scale view of the end clip holes and bolt relationship for a typical $\frac{5}{16}$ " thick web.

The advantages to this system are many, several of which are:

1. Greater erection speed with less field burning of misaligned holes.
2. The use of one size clip angle with a set gauge will accommodate web thickness from $\frac{3}{16}$ " to $\frac{9}{16}$ ".
3. The reduction in sizes of clips to fabricate and stock should help reduce costs.
4. The speed of erection (and elimination of mill web thickness tolerance problems) should help reduce cost.



Short-slotted holes layout for clip \angle - shear connection

Welds

General. Full penetration groove-welds can be designed for full development, same stress as the base metal (1.5.2.1), by selection of the specified matching electrode and welding process (1.17.2). For all fillet, plug, and slot welds, and partial penetration groove-welds, reduced permissible stresses upon the effective throat area (1.14.7) are specified (1.5.2.1). In no case may the stresses exceed that for the base metal, or if different, the weaker base metal (1.5.2.1).

Special Considerations. A number of minor special considerations arise in the specification of welding. Generally, net sections are not a consideration except for plug and slot welds in which the gross area of the holes is deducted to check the fifteen percent maximum allowed (1.10.1; 1.14.3). The Specifications require preheating for various conditions, including all work when the temperatures are below 32°F (1.23.6). Except for single- and double-angle or similar minor members, welds are to be laid out to avoid eccentric axial force or such eccentricity must be considered in the design of the connection

and the member connected to accommodate the need and the selection of the connection.

As previously noted, welds are required as a mixed connection required prior to the weld also important, though not generated in the operation strained, leave corresponding local inelastic yielding, but warping and lamellar tearing caution of a specified sequence avoid warping. Even after to retain adverse residual stresses, stress relief by heat service is not provided unless.

The use of a proper sequence same can also be specified. Particularly with thicker members restrained and the result should be given to the practicable sequence as strains without developing the entire connection design economical to specify a

Connection Design

Classification. In addition connections, certain are established. All connections support not less than shear in flexural members, all at allowable members are to be designed (1.15.2). These minimum of light members such as members are required to meet the minimum six kips strength of the member truss in which the minimum load for open web steel design stress or half the Joists; Examples.)

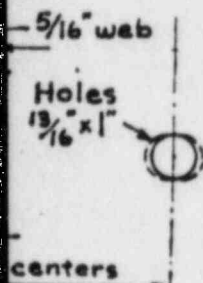
As noted previously, method or the design the transmission of shear members connected and tra

*"Commentary on Highly 1973.

capacity; and connection for flange-to-web nor

equivalent as connection with high-strength bolts (1.15.10) or with rivets on members (1.14.2), and the area of holes is reduced. For tension members joints resisting direct shear are reduced (1.6.3).

Drilled holes is permitted in A-325 or A-490 bolts can be used in either shear or tension over the hole. The hole is $\frac{1}{16}$ " deep by Specification state that only the horizontal distance between the holes in the connection and bolt re-



Holes layout
shear connection

development, same matching electrode and partial penetration heat area (1.14.7) are base metal, or if dif-

fer in the specification for plug and slot fifteen percent maximum for various connections (1.23.6). Except for layout to avoid eccentricity of the connection

and the member connected (1.15.3). For the usual shear connection requiring flexibility to accommodate the necessary simple-end rotations assumed, the locations of the welds and the selection of the connection elements must be coordinated (1.15.4).

As previously noted, where welding at high-strength bolted friction-type joints is required as a mixed connection with shared stress, the final tightening of the bolts is required prior to the welding. The *sequence* of completing purely welded connections is also important, though not explicitly covered by the Specifications (1.23.6). The heat generated in the operations of welding creates intense shrinkage strains which, if restrained, leave corresponding residual stresses (1.23.6). These stresses can be relieved by local inelastic yielding, but where local inelastic yielding is also restrained or limited, warping and lamellar tearing* may result. For many welded assemblies, the simple precaution of a specified *sequence* of welding may be employed to balance the strains and to avoid warping. Even after this precaution, certain complex assemblies may be expected to retain adverse residual stresses. For cases where this condition is anticipated or suspected, stress relief by heating must be specified by the Engineer (1.23.6). (Note: this service is not provided unless it has been specified and will normally be an added cost.)

The use of a proper *sequence* to avoid creation of shrinkage stresses or to minimize same can also be specified in many connections where lamellar tearing might occur. Particularly with thicker sections, where both the direction of the shrinkage is completely restrained and the resulting stress is normal to the surface of the section, consideration should be given to the welding sequence. If the condition can not be eliminated by a practicable sequence as a first choice for a solution, it may be possible to relieve the strains without developing large stresses by use of soft wire "cushions" or by revision of the entire connection detail. At least for simple cases it should, of course, be more economical to specify a particular welding sequence. (See Examples this chapter.)

Connection Design

Classification. In addition to the general requirements previously cited for the design of connections, certain arbitrary minimum design requirements for connections have been established. All connections for members carrying calculated stress must be "designed to support not less than six kips" (except lacing, sag bars, and girts), presumably six kips shear in flexural members, six kips tension in ties, and six kips bearing in compression members, all at allowable stress levels (1.15.1). Eccentric connections of axially loaded members are to be designed to transmit the resulting moments as well as the axial force (1.15.2). These minimum requirements naturally become most significant in the design of light members such as axially loaded members in trusses. Connections for such members are required to meet an additional requirement that they transmit the design load or the minimum six kips, whichever is larger, and develop at least half of the effective strength of the member (1.15.7). Note: joists are regarded as a special very limited-size truss in which the minimum connection capacity is simply specified as twice the design load for open web steel joists (4.5); or for the longspan and deep longspan joists, as the design stress or half the allowable strength of the member (103.5b). (See Chapter 4: Joists; Examples.)

As noted previously, connection types may be classified on the basis of the connection method or the design function. Broadly, connections may be described as *flexible* (for the transmission of shear only, 1.15.4), or *rigid* (maintaining the angle between the members connected and transmitting full moment capacity of the most flexible element at the

*"Commentary on Highly Restrained Welded Connections," *Engineering Journal*, AISC, 10, No. 3, 1973.

joint as well as the shear, 1.15.5), or *semi-rigid* (transmitting a pre-determined fraction of the full moment capacity as a rigid joint and further loads in shear as a flexible joint with corresponding angle change to supply rotation for the additional loads, 1.15.5; 1.2).

Flexible Connections. "Flexible" connections are designed to transmit shear without exceeding allowable unit stresses on the connectors as a group or the connection as a whole. The use of an average capacity for each of several connector elements sharing the total load is justified by allowing self-limiting localized stresses determined by an elastic joint analysis to exceed the yield point and create inelastic localized deformations of the connector materials, or by inelastic deformations of the connection elements (1.15.4). The simplest examples of localized deformation occur in the assembly of bearing-type bolted connections where the cumulative tolerances permitted exist on (1) out-of-round in the bolts, (2) oversize holes ($\frac{1}{16}$ "), and (3) center-to-center location of the holes in the different elements connected. The extreme degree of such inelastic action occurs with a two-bolt bearing-type connection where one bolt is loosely fitted and one is very tight. Until the material of the connected element surrounding the loaded bolt or the bolt yields and deforms ($+\frac{1}{16}$ "), the load is not shared and a 50 percent adjustment will be developed as the load increases. For larger (and thus more important) members, more bolts or rivets will be required and the degree of adjustment required on each will be less. Lesser adjustments are required for a long line of bolts or rivets intended to share stress equally. Even if perfectly fitted, yielding and inelastic deformations occur, maximum at and beginning at the first loaded bolt or rivet, and decreasing to a minimum at the last. (See Figs. 5-1

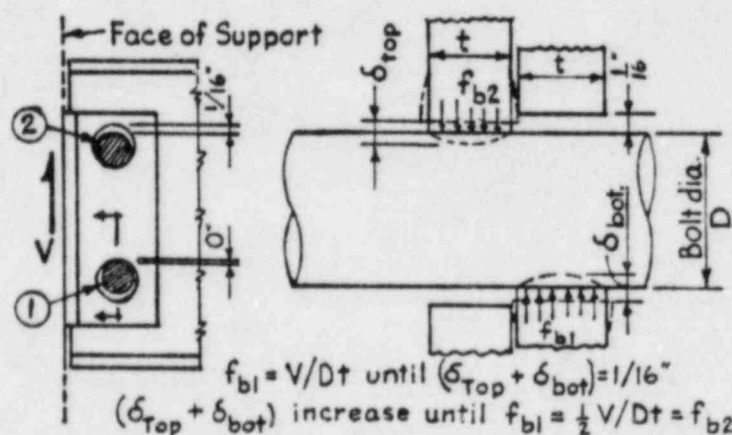
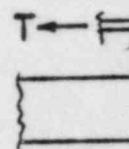


FIG. 5-1 Self-Limiting, Localized Deformations—Two Bolts.

and 5-2.) After this localized inelastic adjustment in the connectors for shear transmission, consider the inelastic adjustments that occur to reduce the "elastic theory" moments.

Inelastic deformation in the connection elements, typically angles, will occur and reduce the restraint which would transmit moment. The common double-angle shear bearing connection is extremely stiff longitudinally for the transmission of shear, and it depends upon the minor inelastic bearing deformations around each fastener to equalize the shear stresses in the fasteners. The same double-angle member is relatively flexible and will twist to permit a relatively large angular rotation reducing moment transmission. (See Fig. 5-3.)

Experience and tests confirm the practical assumptions of shear transfer only and the



Inelastic
plates
ginning
tinning
s₂ s₃
in all

FIG. 5-2 Self-Limiting.



FIG. 5-3 Self-Limiting Angles.

use of an average stress served in one series limits corresponding to the same for Figure 5-4 presents reported from these "s" (see Fig. 5-3) support. Coping and required angle deep connections.

For Type 2 constant design drawings; all capacity for the section designed for one half

¹"Moment-Rotation" Engineering Journal, AISC

e-determined fraction of
ar as a flexible joint with
oads, 1.15.5; 1.2).

transmit shear without
or the connection as a
tor elements sharing the
etermined by an elastic
ed deformations of the
tion elements (1.15.4).
sembly of bearing-type
ist on (1) out-of-round
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d bolt or the bolt yields
ment will be developed
rs, more bolts or rivets
be less. Lesser adjust-
re stress equally. Even
mum at and beginning
he last. (See Figs. 5-1



Inelastic deformations occur successively in the plates at each fastener and in the fasteners, beginning and largest at the first loaded, and continuing until the elastic strains in the spaces s_1 , s_2 , s_3 , and s_4 become proportional to equal stress in all fasteners.

FIG. 5-2 Self-Limiting Deformations—Axial Stress on Line of Separate Fasteners.

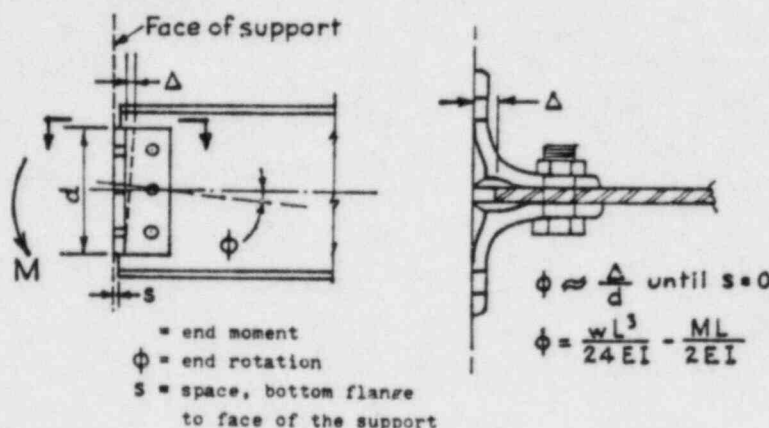


FIG. 5-3 Self-Limiting Deformation (Twist) in the Connection Elements (□□) Two Angles.

use of an average shear stress per unit weld or separate fastener. The actual rotations observed in one series range from 0.84 to 0.97 times Φ_0 , the "simple beam rotation." These limits corresponding to moments ranging from three to sixteen percent were approximately the same for a single end plate connector or the common double-angle connector.¹ Figure 5-4 presents the usual device for an approximate analysis. An additional caution reported from these tests is that the moment stiffness increases abruptly when the space "s" (see Fig. 5-3) closes and the lower flange transmits compression to the face of the support. Coping the bottom flange where a quick analysis of the proportions of depth and required angle change show the usual clearance to be inadequate may be desirable for deep connections.

For Type 2 construction (flexible connections) all the reactions should be shown on the design drawings; alternatively, only those exceeding one half the tabulated uniform load capacity for the sections used, together with a general note that connections shall be designed for one half the capacity unless otherwise noted, should be shown.

¹"Moment-Rotation Characteristics of Shear Connections," Kennedy, October, 1969, 6, No. 4, *Engineering Journal*, AISC.

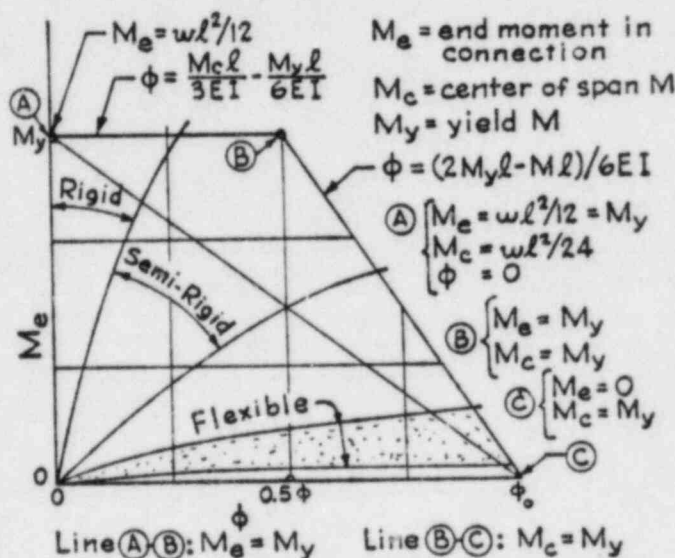
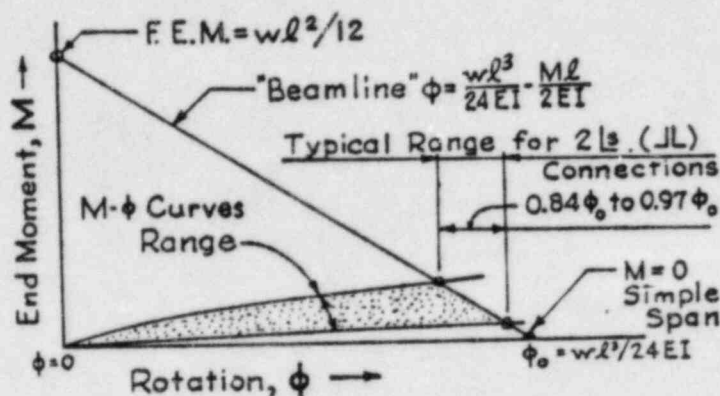


FIG. 5-4 Uniformly Loaded Elastic Beam Line—Rotations at Connection.

Rigid Connections (Type 1 Construction). The AISC Specifications requirement is quite realistic: that rigid connections hold the original angles "virtually" unchanged (1.2). This requirement in elastic design is usually satisfied by connections designed to develop the full section of the flexural member or the full moment at yielding of the more flexible member connected. It will be noted from Fig. 5-4 that the rigid frame analysis ($\Phi = 0$ at the allowable stress) may be satisfied by such a connection which would have a very small rotation at 0.66 to $0.60F_y$, but would be capable of a significant rotation at yielding of the flexural member (line A-B).

A diagram similar to Fig. 5-4 but with point A representing an end moment, $M_e = M_p$, and point C, a center span moment, $M_c = M_p$, can be prepared for plastic design. Connections capable of achieving full collapse load (hinges at both ends and center of span) would be required to reach $\Phi = 0.5\Phi_0$, point B. The simpler concept of "plastic redesign," where only end hinges are required to form at the factored load, would require connections with a somewhat less rotation capacity, along line A-B. See Fig. 5-5.

Semi-Rigid Connections (Type 3 Construction). (See Fig. 5-4.) Ideally, the semi-rigid connections for Type 3 construction will behave elastically between the $\Phi = 0$ ordinate

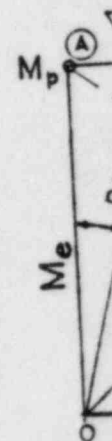


FIG. 5-5

and the "rigid" condition determined end moments to develop the yield moment. In practical cases where required, the excess hinges only will form more rotation capacity.

Masonry Bearing

General. The AISC Specifications on masonry and regulations (1.5.5) low allowable stress block, and hollow materials. Values specified are therefore and brick laid in of the masonry rotational association AISC Specifications fractions of the economy.** The codes. For design recommend the use of

Beam Bearing beam bearing p

*All mortars until
**Supplement N

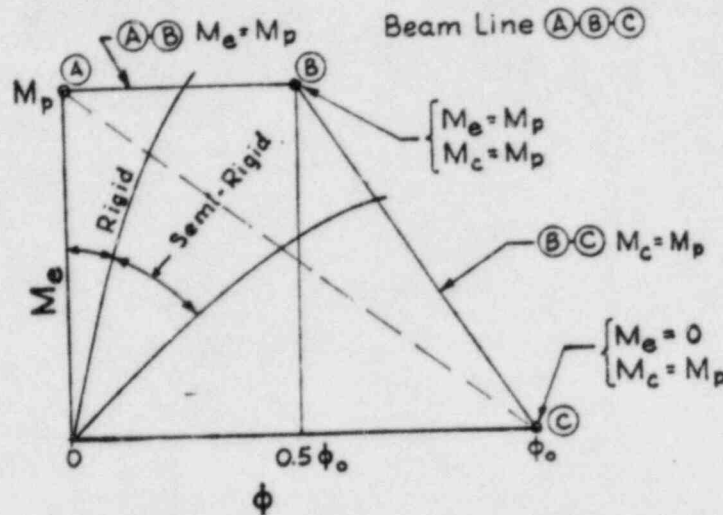


FIG. 5-5 Uniformly Loaded Plastic or Rotations at Connection.

and the "rigid" connection up to a predetermined end moment. Upon reaching this predetermined end moment (M_y for the connection), a rotation capacity sufficient to develop the yield moment at the center of the span, $M_c = M_y$, should be available. In practical cases where the nearest available rolled section will be above the design capacity required, the excess capacity will be provided at the midspan. As in plastic redesign, end hinges only will form at the full design load. Since these hinges are designed for $M_e = M_y$, more rotation capacity is required (to cross line B-C).

Masonry Bearing Connections

General. The AISC Specifications provide very conservative allowable stresses for bearing on masonry and concrete which apply in the absence of Code (statutory Building Code) regulations (1.5.5). For all masonry laid up in mortar, most statutory codes also provide low allowable stresses. Usually, codes distinguish among solid masonry units, bricks or block, and hollow units as well as among different classes of mortar and masonry materials. Values so prescribed range in general from 50 psi to 400 psi. The AISC Specification is therefore seldom applicable since it includes only stone masonry, $F_p = 0.400$ ksi, and brick laid in "cement" mortar, $F_p = 0.250$ ksi (1.5.5). *The authors recommend use of the masonry bearing values prescribed in local Codes or those recommended by national associations dealing with masonry products.* For bearing stresses on concrete, the AISC Specifications, $F_p = 0.35f'_c$ on the full area and $F_p = 0.35f'_c \sqrt{A_2/A_1} \leq 0.70f'_c$ on fractions of the area, utilize recent ACI Building Code (ACI 318-71) refinements for economy.** The ACI Building Code is of course usually applicable under local statutory codes. *For beam-bearing plates and column base plates on concrete, the authors recommend the use of bearing values prescribed by the ACI Building Code.*

Beam Bearing Plates. The approved design (Chapter 2, pp. 82-83, *AISC Handbook*) for beam bearing plates is the formula:

$$t = \sqrt{3 f_p (n)^3 / F_b}$$

(Continued on page 274)

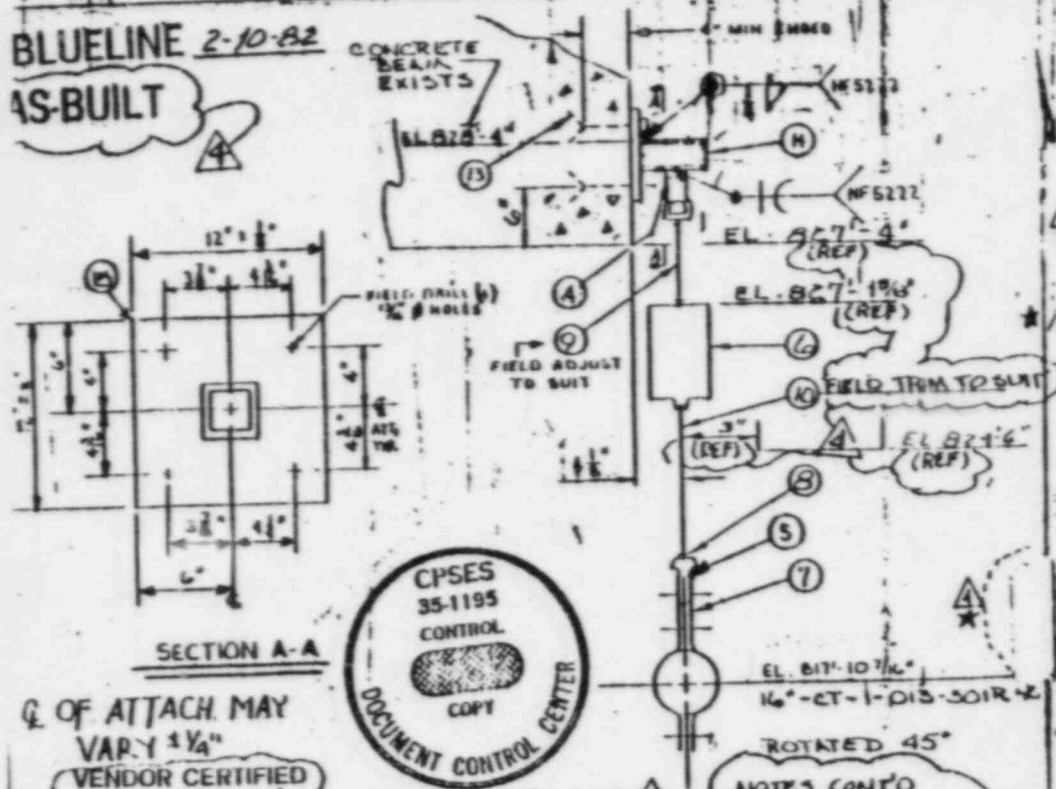
*All mortars utilize cementitious materials and the term "cement" can be quite properly applied to all.
**Supplement No. 3, 1974.

RECEIVED

280
ALT
67
26

FOR OFFICE AND
ENGINEERING USE

BLUELINE 2-10-82
AS-BUILT



Q. OF ATTACH. MAY VARY ± 1/4"

VENDOR CERTIFIED DRAWING REV. NO. 4

BY 1/2 DATE 1/15/82

BRHL 150-CT-1-58-08 R.1

I.P.B. Iss. CT-1-58-08 R.1

Date Print 2-11-82

Pipe Mat'l 2A-33A-CL-10254

Insul. 814g. 5

NOTES

4) BY ISSUE OF REV. 2 OF THIS DRAWING, THE FOLLOWING DOCUMENTS ARE VOIDED:

CMC 33089

REV	DATE	BY	CHK	APP	DESCRIPTION
1	1/15/82	1/2			REV AS NOTED REF RMHS R.1
2	1/15/82	1/2			REV AS NOTED REF RMHS R.1
3	1/15/82	1/2			REV AS NOTED REF RMHS R.1
4	1/15/82	1/2			REV AS NOTED REF RMHS R.1

MOVEMENTS	
X	+0.202 / -0.041
Y	+0.796 / -0.131
Z	+0.070 / -0.450



THIRD PARTY INSPECTION

CODE CLASS: ASME-III-C1

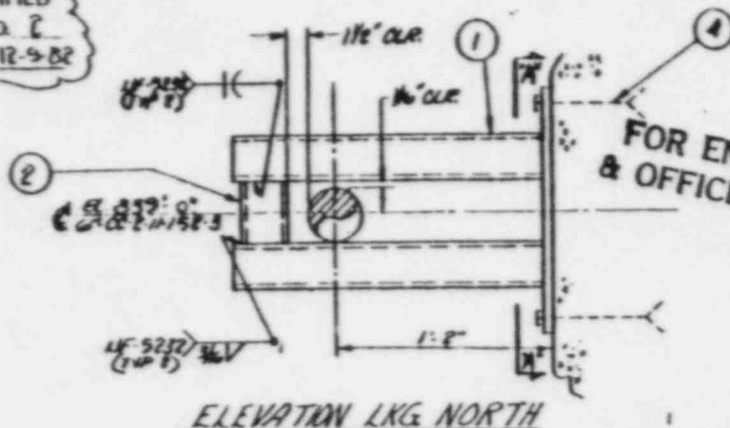
FOR OFFICE AND

ITEM NO.	MATERIALS & OPERATIONS	QUAN	SHIP	PBS	CS	PM	ME	PA
1	HANGER ASSEMBLY CONSISTING OF:	ONE						
2	MATERIALS LIST							
3	Carbon Steel (SA515 GR 65 or SA 36) Plate	1						
4	Detail A, TH-14							
5	2 1/2" x 1/2" High Rivet Concrete Anchors, TH-24	4						
6	Hex (SA 36) 1/2" x 3 1/2" Long, TH-14	1						
7	1/4" Filw. 66N W/Load Pin Steel Attachment	1						
8	1/4" Filw. 290N Eye Nut	2						
9	1/2" Filw. 98N W/Travel Stops (Hot Load)	1						
10	1/4" Filw. Cold Load (Hot Load)	1						
11	1/4" Filw. 140N W/Thread Full Length	1						
12	1/4" Filw. 140N W/1/2" Thread Both	1						
13	Ends							
14	HANGER ASSEMBLY SKETCH AND ENGINEERING BUNDLE AND TAG	1						
15	MARK # CT-1-013-002-5475							
16	16" UT N.D.E./PAR 2.5.1 of the Unit Price Structure							
17	Apply one coat of Carbor Zinc All for above m't'l except th'ds which shall be coated w/a rust preventative							
18	W x F x L (SA 36)	1						
19	W x F x L (SA 36)	1						
20	W x F x L (SA 36)	1						
21	W x F x L (SA 36)	1						
22	W x F x L (SA 36)	1						
23	W x F x L (SA 36)	1						
24	W x F x L (SA 36)	1						
25	W x F x L (SA 36)	1						

FO. MATERIALS AND OPERATIONS SEE SKETCH NO. 1		SHEE. OF	
REV	DATE	BY	CHK
1	1/15/82	1/2	
2	1/15/82	1/2	
3	1/15/82	1/2	
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5	1/15/82	1/2	
6	1/15/82	1/2	
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20	1/15/82	1/2	
21	1/15/82	1/2	
22	1/15/82	1/2	
23	1/15/82	1/2	
24	1/15/82	1/2	
25	1/15/82	1/2	

AS-BUILT

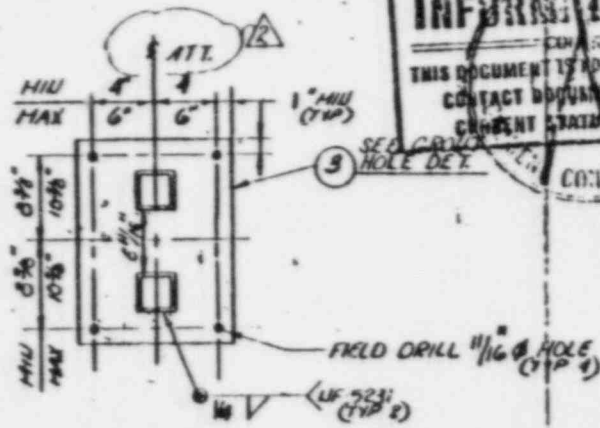
VENDOR CERTIFIED
DRAWING REV. NO. 2
BY BH DATE 12-9-82



FOR ENGINEERING
& OFFICE USE ONLY

ELEVATION LKG NORTH

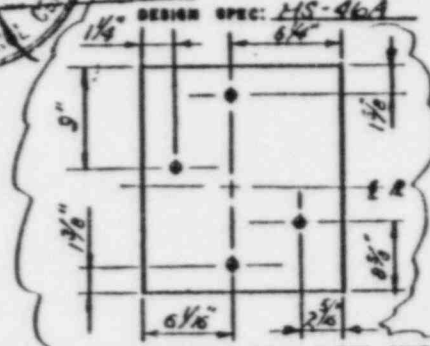
NOTE:
1. LOCKING DEVICES FOR
HIGH STRENGTH BOLTS
ARE NOT REQUIRED
PER DCA 7602



SECTION "A-A"

INFORMATION COPY

THIS DOCUMENT IS FOR INFORMATION ONLY.
CONTACT DOCUMENT CONTROL FOR NAME CODE EDITION: 1974
CURRENT STATUS AND DESIGN ADDRESS: WINTER
DESIGN SPEC: HS-46A



GROUT HOLE DET. PROB. ABT. (L&R) LOCATION PLAN

ITEM NO.	QTY REQ'D	MATERIAL DESCRIPTION	P.B.S.	L.C.S.	M.C.S.	B.C.S.	A.I.S.C.
1	2	5/8 X 1/2 X 1/2" TUBE 1500 G.P.B.		X	X	X	
2	1	5/8 X 1/2 X 1/2" TUBE 1500 G.P.B.		X	X	X	
3	1	1/2" SECT. A-A (SA-515 GR. 65)		X	X	X	
4	4	5/8 X 6" HRT. BRK. CONCRETE ANCHORS		X	X	X	
APPLY OILY MNT. OF 6" TO 3/4" FILL TO ABOVE HMT. EXCEPT THREADS WHICH SHALL BE TREATED WITH A RUST PREVENTATIVE.							
REV	DESCRIPTION	DATE	OWN	CHG.	APPV.		
1	REV'D AS-BUILT PER DCA 7602 TO	12/9/82	TEH	Q	CBP		
2	VENDOR CERTIFICATION, LTRW 59790						

DATA PT	SUPPORT	LOADS (LBS)	PIPE	REF.	BRHL	REV	MECHANICAL	REV	ELECTRICAL	REV	REV	DESCRIPTION	DATE	OWN	CHG.	APPV.
2082	DESIGN	DESIGN	DESIGN	DESIGN	CC-2-AB-031	0	HI-0702	0	EI-0702	0	1	REV ALNTD; REF DCA 7607 (SEE REF) W/NO	5/21/81	TEH	Q	CBP
VERT	—	—	—	—	FAB 130	REV	STRUCTURAL	REV	H.V.A.C	REV	2	REV ALNTD; REF DCA 7607 (SEE REF) W/NO	5/21/81	TEH	Q	CBP
E-S	—	—	—	—	CC-2-AB-031	0	S-0718	0	HI-0755	0	0	REV ALNTD; REF DCA 7607 (SEE REF) W/NO	5/21/81	TEH	Q	CBP
E-W	—	—	—	—												
NOTE	AUTHORIZED NUCL. INSP. YES <input checked="" type="checkbox"/> NO <input type="checkbox"/>															
ASME CODE CLASS	3															

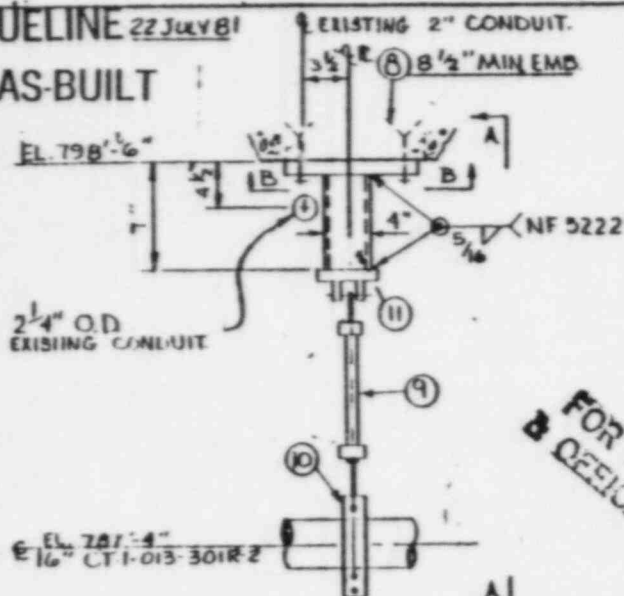
Brown & Root, Inc.
HOUSTON, TEXAS

CLIENT T.U.S.I.
PLANT COMANCHE PEAK
JOB NO. K323

SUPPORT NO. CC-2-AB-719-A23P
SHEET 1 OF 1 REV. 2

FOR OFFICE AND

AS-BUILT



VENDOR CERTIFIED
DRAWING REV. NO. 4
BY W.D. DATE 11/11/83



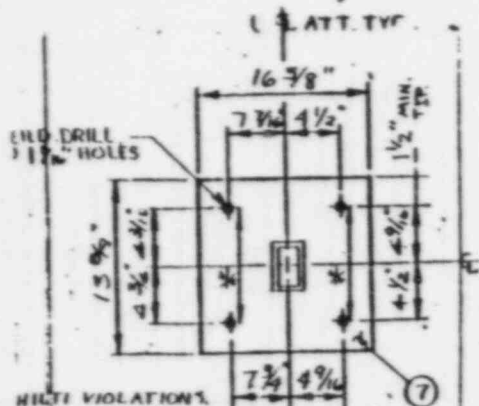
FOR ENGINEERING
OFFICE USE ONLY

CPSES
33-1195
CONTROLS INFORMATION DIV
THIS DOCUMENT IS NOT CONTROL FOR
CURRENT STATUS AND REVISION.
DOCUMENT CONTROL CENTER

NOTES: *

4) Locking devices for high strength bolts are not required per DCA 7607

SEE BRNL FOR
HOR. LOC.



SECTION B-B

CTR LINE OF ATTACH MAY VARY $\pm \frac{1}{4}$ "

BRHL Iso. CT-1-SB-08 Rev. 1
B.R.P. Iso. CT-1-SB-8 Rev. 3
Data Point 250/PROB. 18-1-32 R.O.
Pipe Mat'l. SA 358 & 1-TP 304
Insul. — Bldg. SA


T.O. 4802

ITEM NO.	MATERIALS & OPERATIONS	QUAN	SHIP		P&S	L	CRS	WEL	PAINT	ALC
7	1/4" C.S. B. Per Sec. B-B (BASIS SRS-65 OR SA 30)	1			X			X		
8	1-12" HILTI RWIR CONC. ANCHOR	4						X		
9	SRS-20-80 SWAY STRUT 2'-0" Bx10"	1						X		
10	SRS-20-160 PIPE CLAMP	1						X		
11	3/4" 1 1/2" 1/4" L.O. 5 3/4" LONG. STRUCTURAL TUBING (A-500 Gr.B)	1				X			X	

[illegible]

MARK # CT-1-013-011:522R
PAINT: CARBO ZINC # 11

FOR MATERIALS AND OPERATIONS SEE SKETCH NO. 1 SHEET OF 1


BROWN & ROOT, INC.
 ENGINEERS & CONSTRUCTORS

REF. DRAWING NUMBERS

PIPE: MI-0611a Plan 11 ELECT: EI-0600 R. 11
STEEL: SI-0600 Rev. 12 H.V.A.G.: MI-0630 R. 11

REV	DATE	OWN	CNK	APP	DESCRIPTION
△	5-9-80	B	W	W	ISSUED FOR CONST.
△	5-11-80	C	W	W	REVISED AS NOTED
△	5-11-80	C	W	W	12K ITT REV. 1
△	5-11-80	C	W	W	REV'D AS NOTED REFLITING
△	5-11-80	C	W	W	CME 53215, F.M.H.S.
△	5-11-80	C	W	W	REV'D AS NOTED REFLITING
△	5-11-80	C	W	W	PCA 7001 (REV'D 1) 11/11/80

CUSTOMER Page Utilities Service, Inc.
ORDER OR CONT. NO. CP-0048
JOB NAME Commons Park 102
MARK NO. CT-1-013-011-523R
SKETCH NO. _____
SHEET OF _____ REV. 1

FOR OFFICE AND

THIRD PARTY INSPECTION
CODE CLASS: ASME III-2

REV	DATE	BY	CHK	APP	DESCRIPTION
1	11-18-80	BS	BS	BS	ISSUED FOR CONST. REF.
2	11-18-80	BS	BS	BS	FIELD MODIFIED - WINDS ETC.
3	11-18-80	BS	BS	BS	REVISION FOR ON-11-18-80
4	11-18-80	BS	BS	BS	REVISION FOR ON-11-18-80
5	11-18-80	BS	BS	BS	REVISION FOR ON-11-18-80
6	11-18-80	BS	BS	BS	REVISION FOR ON-11-18-80
7	11-18-80	BS	BS	BS	REVISION FOR ON-11-18-80
8	11-18-80	BS	BS	BS	REVISION FOR ON-11-18-80
9	11-18-80	BS	BS	BS	REVISION FOR ON-11-18-80
10	11-18-80	BS	BS	BS	REVISION FOR ON-11-18-80
11	11-18-80	BS	BS	BS	REVISION FOR ON-11-18-80
12	11-18-80	BS	BS	BS	REVISION FOR ON-11-18-80
13	11-18-80	BS	BS	BS	REVISION FOR ON-11-18-80
14	11-18-80	BS	BS	BS	REVISION FOR ON-11-18-80
15	11-18-80	BS	BS	BS	REVISION FOR ON-11-18-80
16	11-18-80	BS	BS	BS	REVISION FOR ON-11-18-80

PIPELINE 1-13-BK

VENDOR CERTIFIED
DRAWING REV. NO. 5
BY BS DATE 23 NOV 83



STEEL SUPPLIED WITH
MK. #MS-1-01-001-C72S,
NPS #137, THIS PROB.

AS-BUILT

T.O.S. EL. 905'-7"
B.O.S. EL. 902'-9"

EXIST WHIP RESTRAINT
(A 500 G.A.)

STEEL SUPPLIED WITH
MK. #MS-1-01-001-C72S,
NPS #137, THIS PROB.

SEE DETAIL-D

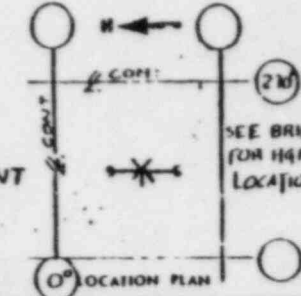
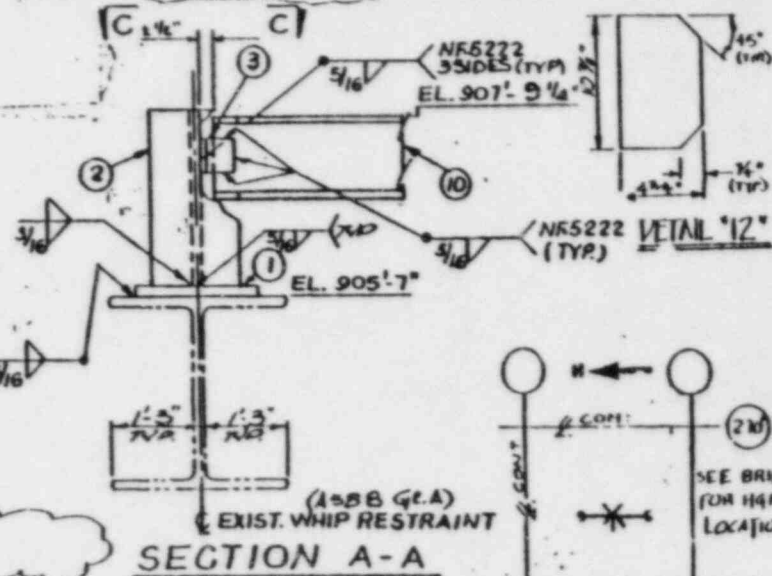
NOTES:

- 1) THERM. UPSET MWTS.
PER UCA 7002,
V = 2.032" UP
S = 1.126"
W = 2.046"

N + PLAN

SECT. C-C

ITEM NO.	NO. REQ'D.	DESCRIPTION	WT.	ASME OR ASME	ASME	ASME	ASME
1	1	FP 1" x 14" x 1' 2" LG.		SA-36			
2	1	W12 x 58		SA-36			
3	4	L 4" x 4" x 3/8" x 8' LG.		SA-36			
4	1	SMA-35-RO					
5	1	MECHANICAL SNUBBER		SA-36			
6	1	SPC-24-320 PIPE CLAMP		SA-36			
7	1	FP 3/4" x 10 1/2" x 8' LG. (SEE DETAIL-6)		SA-36			
8	1	W12 x 58		SA-36			
9	1	FP 1" x 11" x 11' LG.		SA-36			
10	4	FB 4 1/2" x 12" x 10 1/2" LG. (SEE DETAIL-9)		SA-36			
11	1	W12 x 58		SA-36			
12	1	ASME III NAME PLATE					
13	5	FB 1/2" x 4 1/2" x 10 1/2" LG. (SEE DETAIL-12)		SA-36			
14	1	SE 1" x 7" x 11		SA-36			
15	1	FP 3/4" x 10 1/2" x 8'		SA-36			
16	2	PCSR 6" x 8" (FIELD CUT TO SUIT)		SA-36			



BI SUPP'T. 150 NPSI-MS-1-RB-02				DRAWN		DATE		CHK'D		DATE		APPV'D		DATE	
ELECTRICAL				REV. 8		11-18-80		REV. 8		11-25-80		REV. 8		11-26-80	
STRUCTURAL				REV. 2		11-18-80		REV. 2		11-25-80		REV. 2		11-26-80	
H.V.A.C.				REV. 5		11-18-80		REV. 5		11-25-80		REV. 5		11-26-80	
PAINT				REV. 1		11-18-80		REV. 1		11-25-80		REV. 1		11-26-80	
ZONE				REV. 1		11-18-80		REV. 1		11-25-80		REV. 1		11-26-80	
OWNER				TEXAS UTILITIES SERVICES INC.		PRODUCTION ORDER		SERIAL NUMBER		SHEET		10F3		REV. 5	
PROJECT				COMANCHE PEAK UNITS NO. 1 & 2		310		MX. NO. MS-1-01-001-C72K		REV. 5					
ENGINEER				GIBBS & HILL INC.											

FOR OFFICE AND
ENGINEERING USE ONLY

1947

FOR OFFICE AND
ENGINEERING USE ONLY

$$6'' \quad 10^{15/16}'' \quad 1'-2'' \quad 1'-2''$$

EXIST. STL
WHIP RESTRAINT
REF. DWG. 2325-SI-0583
DET. M-17
A532 GR. A

Locking devices for high strength bolts are not required per DCA 7607.

VENDOR CERTIFIED
DRAWING REV. NO. 6
BY: H. H. H. H. DATE: 5-2-54

N-PLAN TO. 3401

Exposure at 100 ft per second plotted on S.I.C. Card	0x	0Y	0Z
ABNORMAL MAXIMUM	+ .006	+ .006	+ .006
NORMAL MINIMUM	- .205	- .150	- .131
NORMAL OPERATING M.C.	- .205	- .150	- .126

$$\begin{aligned} V &= 1.926 \text{ u} \\ S &= 1.643 \\ W &= 2.897 \end{aligned}$$

N

CONT

SEE BRILL. FOR HGR. LOC.

270

0°

LOCATION PLAN

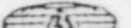
REV	DATE	INITIALS	CHK	2P	DESCRIPTION
△	12/28/83	AK	OK	OK	REV'D VENDOR CERT.
△	1/1/84	T	OK	OK	REV'D VENDOR CERT.

91	SUPP'T 150.	NPSI-MS-I-RB-02
----	-------------	-----------------

[illegible]

REFERENCE DRAWINGS	S.P.H.L. 150.	REV	1 PIPING
	MS-1-RB-002	2	2.2.3-W-C-22
	PAB. ISOMETRIC	REV	STRUCTURAL
	MS-1-RB-02	A	23.3-31-0532
OWNER TEXAS UTILITIES SERVICES INC.			
PROJECT COMANCHE PEAK UNITS NO. 1 & 2			
ENGINEER			

REV	ELECTRICAL	REV	COLOR/CLASS	5/2	DRAWN	DATE	CHK'D	DATE	APP'D	DATE
1	2323-EL-0502	1	PAINT	ACR	BS	12-1-80	DP	12-4-80	g.m.t.	12-10-80
REV	H.V.A.C.	2	ONE		P.O. NO.	CF-G048A-1	MFG. REL.			
2	2323-MI-0552	5								


Brown & Root, Inc.
 ENGINEERS AND CONSTRUCTORS
 HOUSTON, TEXAS

PRODUCTION ORDER	SERIAL NUMBER	SHEET
		1075

309 11-1-80 MS-1-001-006-C72K REV. 6

THIS EQUIPMENT IS INTENDED FOR OFFICE USE ONLY.
CONTACT SUPPLY FOR CATALOG FOR CURRENT
STATUS AND PRICING.

FOR ENGINEERING
& OFFICE USE ONLY

FOR OFFICIAL USE ONLY

AS-BUILT

(MATERIAL SUPPLIED WITH)
 MK. # CT-1-137-701-525R
 (REF)

CHINA CO. MADE
BY CHINA

TOP OF CONCRETE @
ELEV. 785'-6"

(PIPE @ ELEV. 789'-9 1/2")

VENDOR CERTIFIED
DRAWING REV. NO. 1
DATE 3-10-83

ITEM	QTY.
NO.	REQ'D

MATERIAL	DESCRIPTION
1	...
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SRS-20-FC SHAW STRUT: C-C = 4'-7 3/4"
WITH SRS-20-100 PIPE CLAMP (SA-36)
1" THK. CARBON STEEL RATE (A-36)
(SEE SECTION "A-A")
1" x 12" LONG SUPER HILT KWIK BOLT
1/2" (2 3/4" MIN. EMB.)

PAINT: CARBO-ZINC # 11

REV

[illegible]

DATE	TIME	TEST
------	------	------

W	C
---	---

APR 2001

1	2	3
4	5	6

ASME CODE EDITION:

ADDENDUM:

DESIGN SPECI

THIS SUPPORT REPLACES
SUPPORT #
CT-1-137-E02-925R

NOTES:

1) Locking devices for
high strength bolts
are not required
per DCA 7607

LOCATION PLAN

T.O. # 4102

SECTION "A-A"

STENT ROTATED FOR CLARITY

IN PT	SUPPORT LOADS (lbs)				POE
DESIGN	SERVICE LEVEL LIMITS				WYTS
	A	B	C	D	INCHES
INT.	-1000	-1907	-2948		-9.004
	-958	+359	+5500		19.018
F-B					0.031
					9.4002
	+1095	-46	-6366		
	+1179	+2519	+29410		
ASME, SECTION VIII, DIVISION 2	AUTHORIZED MULL. ASME CODE CLASS			INSP. YES	NO

REF. DNGS.		ORIG. I.D.	REV.	MECHANICAL	REV.	ELECTRICAL	REV.	REV.	DESCRIPTION	DATE	OWN.	CHKD.	APPROV.
CT-1-SB-002		1	REV.	MT 06156	11	ET 06155	2	1	REV'D AS MT 06156; REV'D DNG 6679783	11/0/5	1	7EH	Q
FAB. NO.		REV.	STRUCTURAL	REV.	H.V.A.C.	REV.	FOOT	1	DCA 7607 (MT 11); ASBUILT VEHICLE	~	~	~	~
CT-1-SB-003		5	REV.	31 0600	17	MT 0650	6	-	CERTIFICATION CPD 26082	~	~	~	~



Brown & Root, Inc.

HOUSTON, TEXAS

CLIENT I.U.S.I.

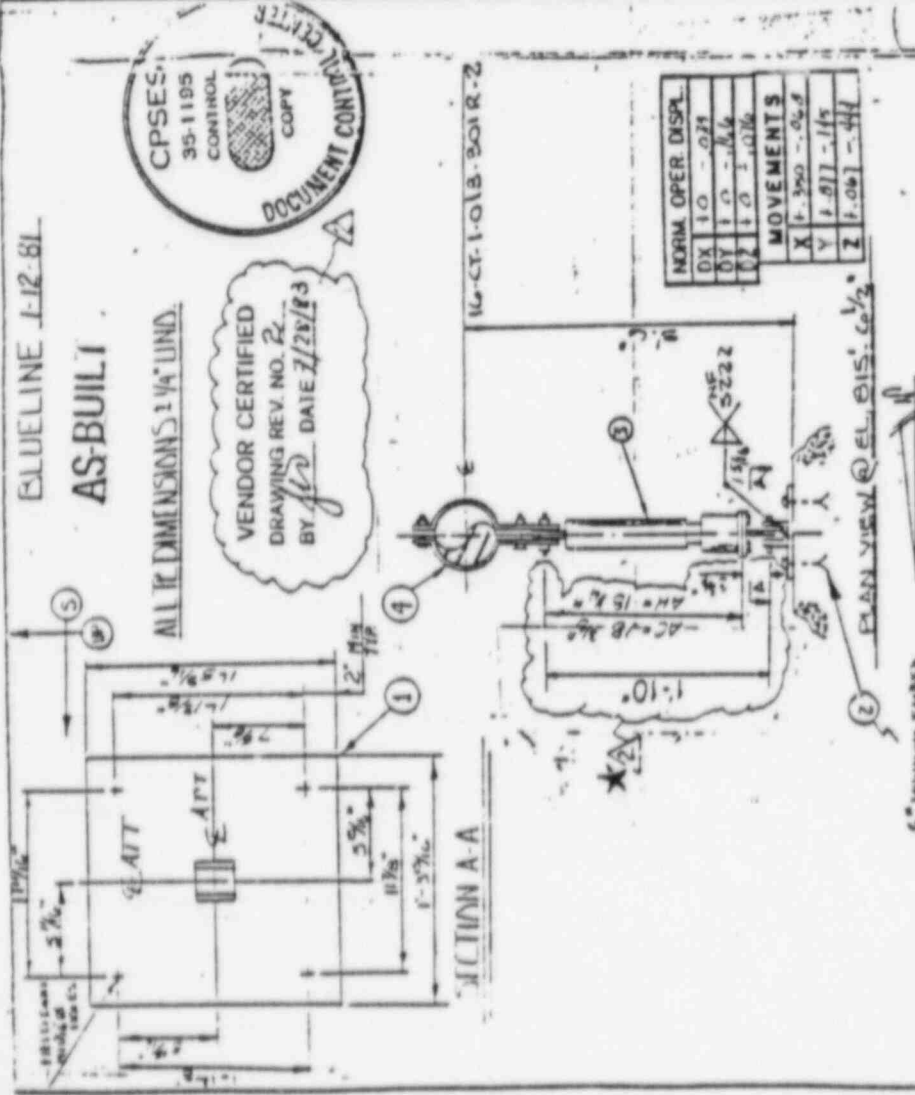
PLANT COMANCHE PEAK

JOB NO. 2323

SUPPORT NO. CT-1137-702 925R

SHEET 1 OF 1 REV. 1

FOR OFFICE AND



locking devices for
high strength bolts
are not required
per DCA 7607

★ CHANCE NOT MADE
BY CMC

Page: FO 01-50-0 R1
 BPP Iso. CV-1-50-0-05A B
 Issue Point 260/000 M1 H10
 Pipe Mat'l. SA 35B Cl. 1-10-20A
 Insul. Bldg. 5B

THIRD PARTY INSPECTION

CODE CLASS: ASSESSMENT - 2

ITEM NO.	NO REQD	PART CALL-OUT	DESCRIPTION	MATERIAL	MIC. NO.	WT.
1	4	C.S. 1/4" THK	(SEE DET. A-A)	SA-36		
2	1	OSA-1-12	(SEE DET. A-A)			
3	1	SME-10-80	SNIBBLER			
4	1	SPC-13-100	PIPE CLAMP	SA-36		
5	1	ASME 15-100	PIPE CLAMP			

ITEM NO.	NO REQD	PART CALL-OUT	DESCRIPTION	MATERIAL	MIC. NO.	WT.
1	1	SEISMIC ASSEMBLY SKETCH AND ENGINEERING BUNDLE AND TAG				
2	1	MARK # CT-1-013-019-542K				

Apply one coat of CARBO-ZINC #11110 above mat'l except in'ds which shall be coated w/a rust preventative.

FOR OFFICE AND ENGINEERING USE ONLY

REV	DATE	OWN	CHK	APP	DESCRIPTION
A	11-24-61	MD	R		REV'D. SUPPLY CLERK, R. E. G. NCR # 73105

Approved By: R. E. G.
Date: 6-20-79

QUAN	SHIP

[illegible][illegible]

INFORMATION COPY

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CONTACT DISTRICT CONTROL FOR CURRENT
PROJECT AND DESIGN.

FOR ENGINEERING
OFFICE USE ONLY

FOR OFFICE AND
ENGINEERING USE ONLY

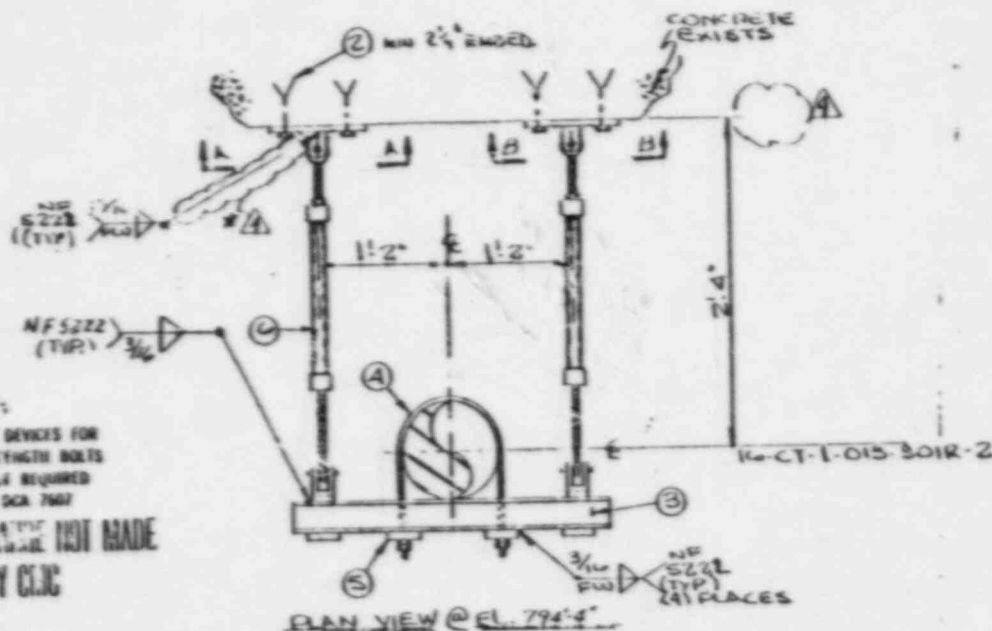
IE LINE 11-19-80

BUILT

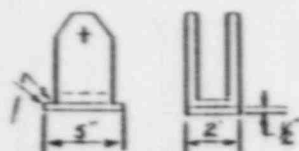
FOR CERTIFIED

REV. NO. 4

DATE 3/23/83



IE:
ING DEVICES FOR
STRENGTH BOLTS
E N/A REQUIRED
PER DCA 7007
CREATIVE TEST MADE
BY CJC



DETAIL 1
T/04802

MARK NO. CT-1-013-014-532R
BPP ISO. CT-1-013-014-532R

Paint: 253A
Pipe But'l. SA 350 CL 1 TP 204

MOVEMENTS	
X	0.016/0.007
Y	0.016/0.007
Z	



THIRD PARTY INSPECTION
CODE CLASS: ASME III - G

ITEM NO.	MATERIALS & OPERATIONS	QUAN	SHIP	PBS	CSS	PRIN	SEC	AISC
1	R 1" x 1 1/2" x 9 1/2" (SA-36)	1		X		X		
2	BSA-12- 5/2 CONC. ANCHORS	2			X	X		
3	C 4 x 5.4 x 3" B 3/4" (SA-36) P-R 3/4" x 1"	2			X	X		
4	ANS-160 STD (1-BOLT (SA-36) L=14 1/2	1			X	X		
5	RWP-07 (SA-36)	4			X	X		
6	SAS-04- BA SWAY STAIT C.C. 3 1/2"	2			X	X		
7	R 1/2" x 2" x 5" (SA-36) SEE RETAIL-T.	4		X		X		
8	R 1" x 9 1/4" x 10 3/8" (SA-36)	1		X		X		

REV	DATE	OWN	CHG	APP	DESCRIPTION
1	3/23/83				REVISED VENDOR CERTIFICATION

MARK # CT-1-013-014-532R
PAINT: CARBO ZINC # 11

Approved By: C.E.C.
Date: 6-20-83

FOR MATERIALS AND OPERATIONS SEE SKETCH NO. SHEET OF

Brown & Root, Inc.		CONDITIONS	Fx	Fy	Fz	Mx	My	Mz
REF. DRAWING NUMBERS		DESIGN						
PIPE: M1 0602 REV 1 ELECT: 01 0601		NORMAL & VIBET						
STEEL: 01 0602 REV 12 HV.A.C: 01 0601		EMERGENCY						
		FAULTED						

REV	DATE	OWN	CHG	APP	DESCRIPTION	CUSTOMER
1	11-19-80				SSOE FOR CONSY, REF FIELD BOWING	Texas Utilities Service, Inc.
2	11-19-80				HAIRER SWITCHING/REPAIRS	ORDER OR CONT. NO. CP-0046
3	11-19-80				REV AS NOTED. REF CMC 48246	JOB NAME
4	11-19-80				DCA 307 (SEE NOTE 1) AS C-11	MARK NO. CT-1-013-014-532R
5	11-19-80				REPAIR OF FIELD BOWING, E.T.T.	SKETCH NO.
6	11-19-80				REPAIR OF FIELD BOWING	SHEET 1 OF 2

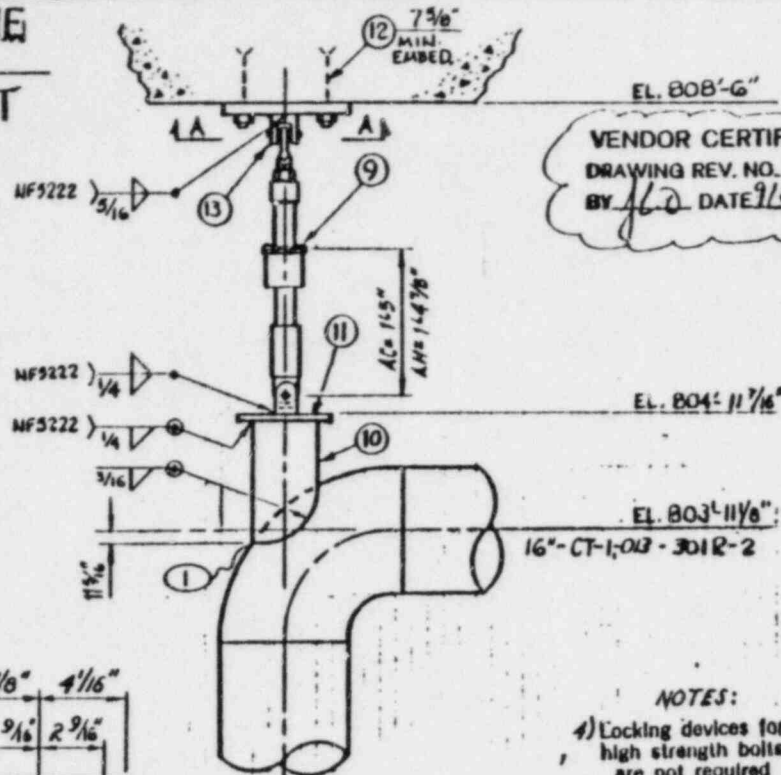
FOR OFFICE AND

ENGINEERING USE ONLY

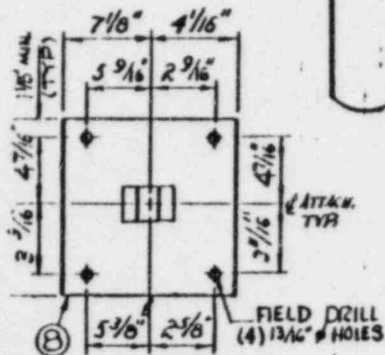
UCLINE

16.81

BUILT



VENDOR CERTIFIED
DRAWING REV. NO. 4
BY 162 DATE 9/6/80



SECTION A-A

BRHL Iso. CT-1-SB-00BR.1
I.P.D. Iso. CT-1-SB-B Rev.3
Data Point 1253/PROB. AB-1-32 R.O
Pipe Mat'l. SA358 TP304
Insul. ~ Bldg. SB

T.O. 4802

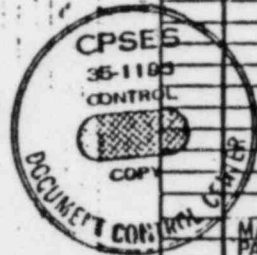
NOTES:
1) Locking devices for high strength bolts are not required per DCA 7607 /

NORM. OPER. DISPL.	
DX	+ .085
DY	+ .090
DZ	- .051

MYTS	
X	+ .342
Y	+ .46
Z	+ .074
	- .22



THIRD PARTY INSPECTION
CODE CLASS: ASME III-2



ITEM NO.	MATERIALS & OPERATIONS	QUAN	SHIP	PBS	L	CSS	PRIM	SEC	AISC
8	CS PLATE, 7/8" THK, PER SECT A-A (SA358/SA358GR69)	1							
9	SMA-3-50 SNIPPER	1							
10	8" SCH 40S PIPE STANCHION H.T. B.B. (1" 1/8" DIA) (CAST TP304)	1							
11	CS PLATE, 3/4" x 12" x 12" (SA358/SA358GR69)	1							
12	3/4" x 10" HILTI-KWIK CONC. ANCHORS	4							
13	NRB-10 BEAR BRACKET (AGRD/SA358)	2							

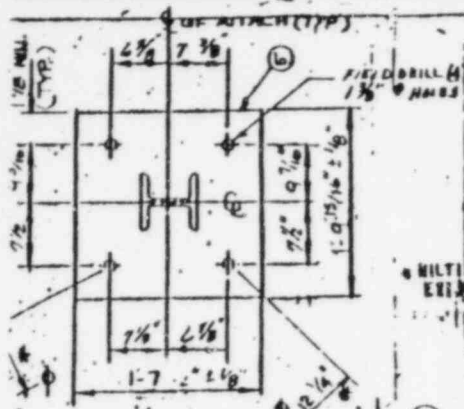
FOR OFFICE AND ENGINEERING USE ONLY

MARK # CT-1-013-013-S32K
PAINT: CARBO ZINC # 11

REV	DATE	OWN	CNA	APP	DESCRIPTION
1	9/6/80	Q	162	162	VENDOR CERTIFICATION LEFT GTH # 62726

FOR MATERIALS AND OPERATIONS SEE SKETCH NO. SHEET OF

BROWN & ROOT, INC. ENGINEERS & CONSTRUCTORS		CONDITIONS	Fx	Fy	Fz	Mx	My	Mz
REF. DRAWING NUMBERS		DESIGN						
PIPE: MI-0405 Rev.14 ELECT: EI-0401 R9		NORMAL & UPSET						
STEEL: 81-0502 Rev.12 HV.A.C.: MI-0401 R6		EMERGENCY						
		FAULTED						
REV	DATE	OWN	CNA	APP	DESCRIPTION	CUSTOMER Texas Utilities Service, Inc.		
1	9/6/80	Q	162	162	ISSUE FOR CONST. R.O. TITR.1	ORDER OR CONT. NO. CP-0046		
2	9/6/80	Q	162	162	REV'D AS NOTED. REF. FAHS. MK # WAS CT-1-013-013-S32K	JOB NAME Comanche Peak 1A 2		
3	9/6/80	Q	162	162	REV'D AS NOTED. REF. MK # WAS CT-1-001-013-S32K	MARK NO CT-1-013-013-S32K		
4	9/6/80	Q	162	162	REV'D AS NOTED. REF. MK # WAS DCA 7607. SEE NR 4 AS BUILT	SKETCH NO.		
						SHEET 1 OF 1 REV. 4		



BLUELINE 27 JULY 81

AS-BUILT

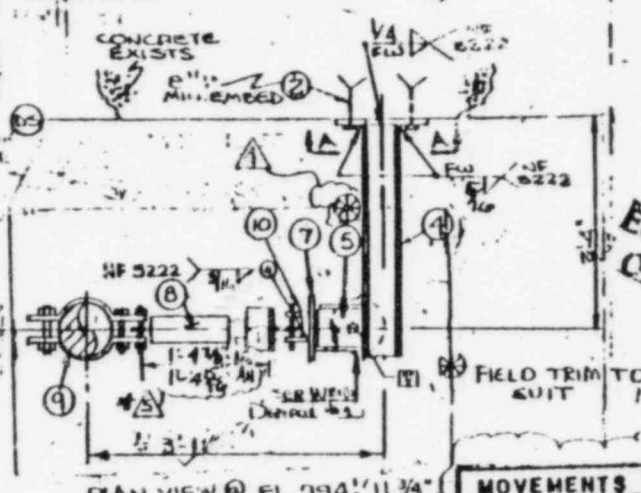
VENDOR CERTIFIED

DRAWING REV. NO. 5

BY 11/18/81 DATE 11/18/81

NOTE:
4) Locking devices for high strength bolts are not required per DCA 7607

MULTI VIOLATION: 1 1/2 HRS
EXT. PER MK# CT-1-010-007-522K



MOVEMENTS

X +.235 -.062
Y +.281 -.049
Z 1.003 -.015

NORM. OPER. DISPL.

DX .071
DY .056
DZ -.008

DETAIL 1



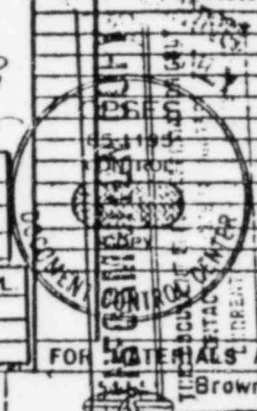
SEE BRHL FOR HGR LOCATION

THIRD PARTY INSPECTION
CODE CLASS: ASME III-2

ITEM NO.	MATERIALS & OPERATIONS	QUAN	SHIP	PBS	L	CSS	PRIM	SEC	AISC
2	1 1/4" X 12" MULTI KWIK CONC. ANCHORS (1144)	4							
4	W 8 X 12 (SA-36) 2'-6 1/2" LONG	1							
5	W 6 X 12 (SA-36) 0'-6 5/8" LONG SEE DET 1	1							
6	1" C.S. R. Per Sec. A-A (SA-515 Gr. 65 or SA-36)	1							
7	1/2" X 8" X 0" B.L.G. C.S. TE (SA-36 or SA-515 Gr. 65)	1							
8	SMF-3-SO SHUBBER C-C 1'-6 1/2" L x 2"	1							
9	SFC-10-160 PIPE CLAMP (SA-36)	1							
10	XRB-10 RLR BRACKET (ALU-B-D/SA36)	1							

SEISMIC ASSEMBLY SKETCH AND ENGINEERING
BUNDLE AND TAG
MARK # CT-1-013-012-532K

Apply one coat of Garbo Binc #11 to above mat #1 except th'ds which shall be coated w/ a rust preventative.



REV	DATE	OWN	CNA	APP
1	7/28/81	TE	TE	TE
2	8/1/81	Q	Q	Q

DESCRIPTION

REV'D AS NOTED, REF. CMC L 5614
REV'D AS NOTED, REF. CMC L 5614
VENDOR CERTIFICATION.
REF. CMC L 5614

Approved By: C.E.C.

Date: 6-20-79

QUAN SHIP

FOR MATERIALS AND OPERATIONS SEE SKETCH NO.

Brown & Root, Inc.

REF. DRAWING NUMBERS

PIPE: 14" O.D. CMC, REV. 14 ELECT. 14
STEEL: 14" O.D. CMC, REV. 14 ELECT. 14

REV	DATE	OWN	CNA	APP	DESCRIPTION
1	5/8/80	Q	Q	Q	ISSUE FOR CONST.
2	6/1/80	Q	Q	Q	BASE PLATE ONLY
3	6/1/80	Q	Q	Q	REVISED AS NOTED PER
4	6/1/80	Q	Q	Q	ITT DWG
5	6/1/80	Q	Q	Q	REVISED AS NOTED PER
6	6/1/80	Q	Q	Q	REVISED AS NOTED PER

CONDITIONS

DESIGN

NORMAL & UPSET

EMERGENCY

FAULTED

SHEET OF

Mx My Mz

CUSTOMER: Ingham Utilities Service, Inc.

ORDER OR COM. NO. CP-0046

JOB NAME: Cap-moche Peak 1 & 2

MARK NO. CT-1-013-012-532K

SKETCH NO.

SHEET 1 OF 1 REV. 5

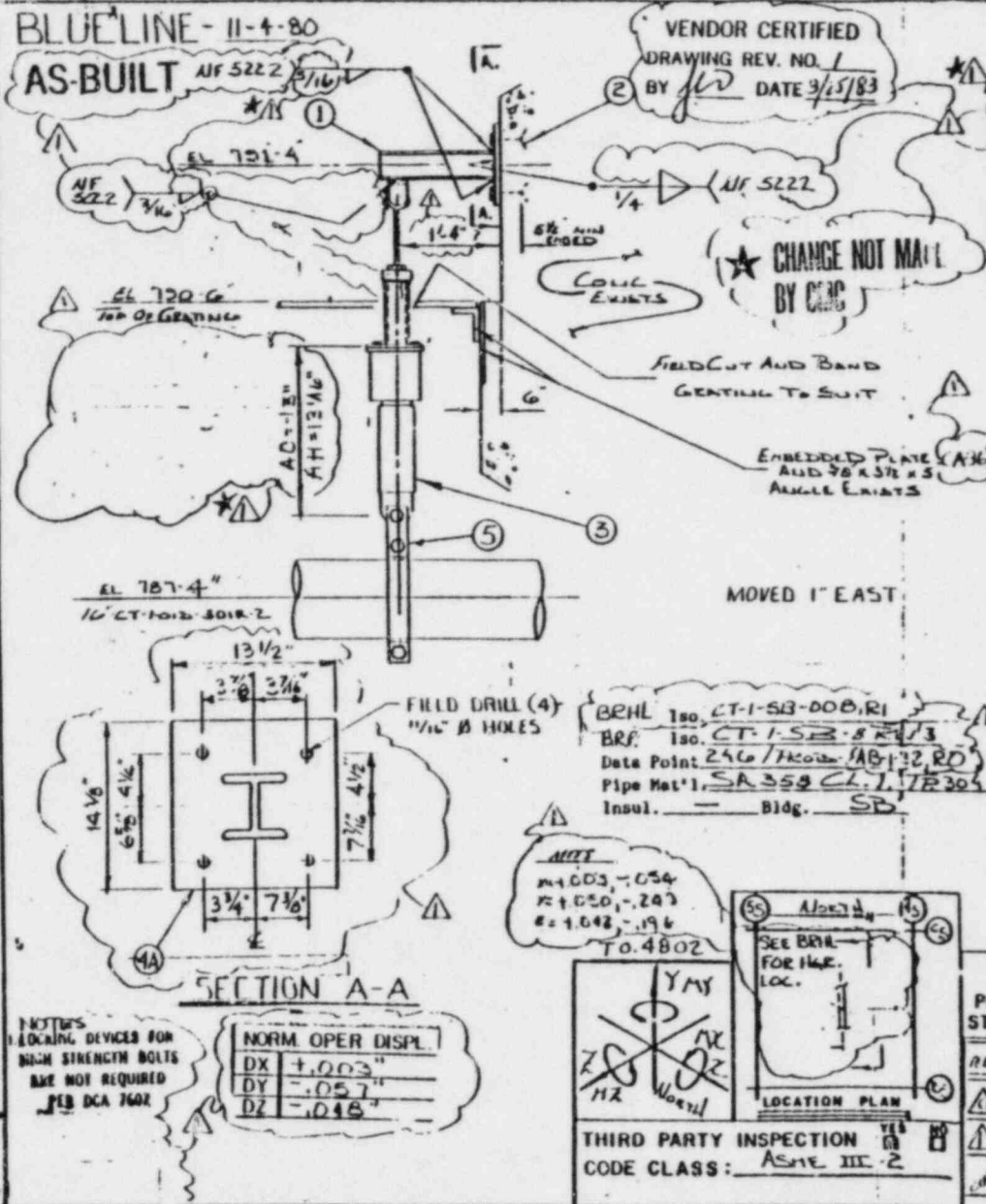
NOT CHANGED BY CMC

BRHL 150. CT-1-58-008 REV. 1
BRHL 150. CT-1-58-008 REV. 2
Data Point 53/PROB# 10-1-32 Rev. 0
Pipe Mat'l. SA 350. Q 1. TP 804
Insul. Bldg. S.B.

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 STATUS AND REVISION.

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**FOR OFFICE AND
 ENGINEERING USE ONLY**



ITEM NO.	NO REQD	PART CALL-OUT	DESCRIPTION	MATERIAL	MIC. NO.	WT.	PBS	L	CSB	PRIED	SEC	AISC
1	1	WAXIEXI-376		SA 36		17		X	X			
2	4	BSA SB-R12	(BY FIELD)					X	X			
3	1	SMA-1 RD	SNUBBER	C-2-SMA-1		11		X	X			
4	1	SHFT K-100	TRANSITION KIT									
5	1	SPC DB-160	PIPE CLAMP	SA 36		47		X				
1	1	PROVIDE TEMPORARY SPACE	C-2A-SMA-1			10						

SEISMIC ASSEMBLY SKETCH AND ENGINEERING BUNDLE AND TAG
MARK # CT-1-013-009-S22K

Apply one coat of Carbo Line #11 to above cat #1 except in areas which shall be coated with rust preventative.

Approved By: C.E.L.
 Date: 6-20-79

FOR MATERIALS AND OPERATIONS SEE SKETCH NO. 1
Brown & Root, Inc.

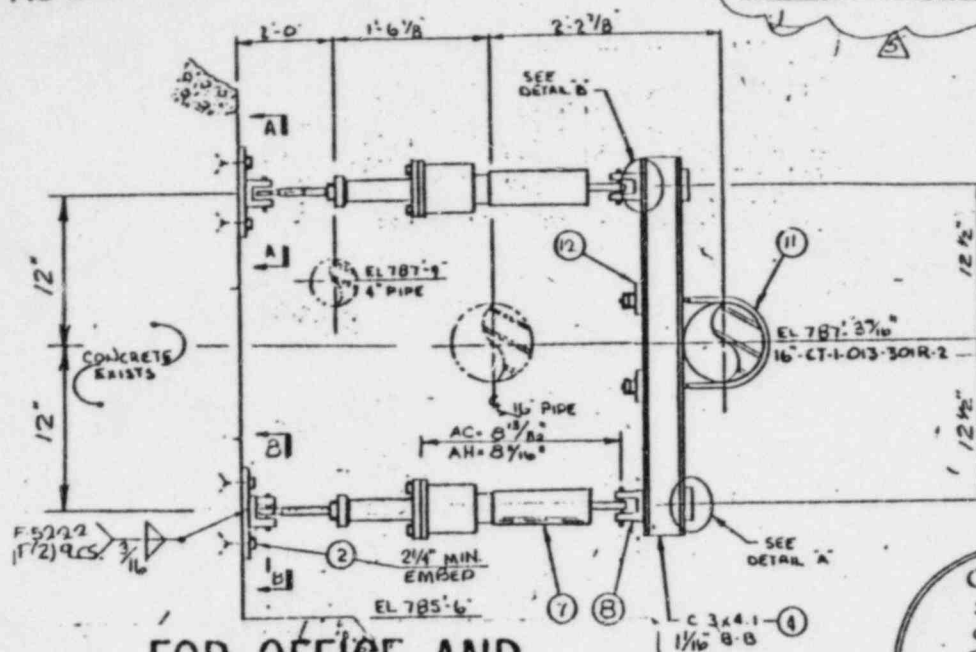
CONDITIONS	Fx	Fy	Fz	Mx	My	Mz
DESIGN						
NORMAL & UPSET		329				
EMERGENCY		499				
FAULTED						

REF. DRAWING NUMBERS
PIPE: 11-0006-2-13 **ELECT:** 11-0002-2-13
STEEL: 11-0002-2-13 **HV.A.C.:** 11-0002-2-13

REV	DATE	OWN	CHK	APP	DESCRIPTION
1	11-4-80	M	W		ISSUE FOR CONST. REF. (11-0002-2-13)
2	5-25-80	V	TA		REV AS NOTED REF. CH. 59159-2
3	6-23-80	V	TA		REVISIONS "AS BUILT"
4	6-23-80	V	TA		VENDOR CERTIFICATION
5	6-23-80	V	TA		REG. 11-4-21210

CUSTOMER Texas Instruments Service, Inc.
ORDER OR CONT. NO. CP-0046
JOB NAME Conanche Peak 1 & 2
MARK NO. CT-1-013-009-S22K
SKETCH NO.
SHEET 1 OF 1 **REV. 1**

AS-BUILT



FOR OFFICE AND
ENGINEERING USE ONLY

NCTL

- 14) LOCKING DEVICES FOR
HIGH STRENGTH BOLTS
ARE NOT REQUIRED
PER DCA 7607

BRUL Iso. CF-1-58-000/R.1
B.R.P. Iso. CF-1-58-8 REV.3
Data Point 44/PS20 = 2B-1-52/R.0
Pipe Mat'l. SA. 358 CL. 1, 79309
Insul. ~ bldg. 58

VENDOR CERTIFIED
DRAWING REV. NO. 5
BY BU DATE 3-15-94

ITEM NO.	MATERIALS & OPERATIONS				QUAN.	SHIP.	P&S	L	CSS	PRIM.	SEC.																		
	SEISMIC MECHANICAL SHOCK SUPPRESSOR																												
	CONSISTING OF:				ONE																								
	MATERIAL EXISTS																												
1	3/8"x8" Carbon Steel (SA-515 GR-65 or SA-36) Plate 0' 8" Long, TW-14#				2		X																						
2	1/2"x5 1/2" Hilti Kwik Concrete Anchors (11141)				8																								
3	# 1/2, 2 1/2" Stroke, Fig. 307N Mechanical Shock Suppressor, W-31.5 3/4", Cold Setting, 1 1/4", Hot Setting, 1 1/4" W/Additional Rear Bracket, Load=2. Ordered In Pairs				2			X																					
4	C3x4.1 (SA-36) 2' - 5" Long TW-18#				2			X																					
5	7/8" Fig. 60N Washer Plate				4				X																				
6	7/8"x16" Fig. 137N U Bolt, D-1' 1 1/2", Developed Length=4' 5 3/4"				1																								
7	EMA 1/2-GO SANDPAPER				2																								
8	XRB-06 PEAR BRACKET (ALAD/SA36)				4				X																				
	SEISMIC ASSEMBLY SKETCH AND ENGINEERING BUNDLE AND TAG				1																								
	MARK # CT-1-013-007-S22K				1																								
9	1/2" C.S. R. FER SECT "A-1" (SA-36) 1-515, GR-65				1		X																						
10	1/2" C.S. R. FER SECT "B" (SA-36) 1-515, GR-65				1		X																						
11	FIS-11.0 U-BOLT B=1 1/4" (SA-36)				1				X																				
12	RWD-07 WASHER PL. (SA-36)				4				X																				
	Apply one coat of Carbo Zinc #11 to above mat'l except th'ds which shall be coated w/a rust preventative.																												
13	ASME NAMEPLATE				1																								
14	1/2" THK. PL 2' x 2" (SA-36)				2																								
<table><tr><th>REV</th><th>DATE</th><th>OWN</th><th>CNK</th><th>APL</th><th>DESCRIPTION</th></tr><tr><td>A</td><td>8-17-83</td><td>PE</td><td>Q</td><td>CS</td><td>REV'D AS-BUILT VENDOR CERTIFIED</td></tr><tr><td>A</td><td>3-15-84</td><td>PE</td><td>E</td><td>CS</td><td>REV'D VENDOR CERT, LIT CMB-47275</td></tr></table>												REV	DATE	OWN	CNK	APL	DESCRIPTION	A	8-17-83	PE	Q	CS	REV'D AS-BUILT VENDOR CERTIFIED	A	3-15-84	PE	E	CS	REV'D VENDOR CERT, LIT CMB-47275
REV	DATE	OWN	CNK	APL	DESCRIPTION																								
A	8-17-83	PE	Q	CS	REV'D AS-BUILT VENDOR CERTIFIED																								
A	3-15-84	PE	E	CS	REV'D VENDOR CERT, LIT CMB-47275																								
						QUAN.	SHIP.	P&S	L	CSS	PRIM.																		

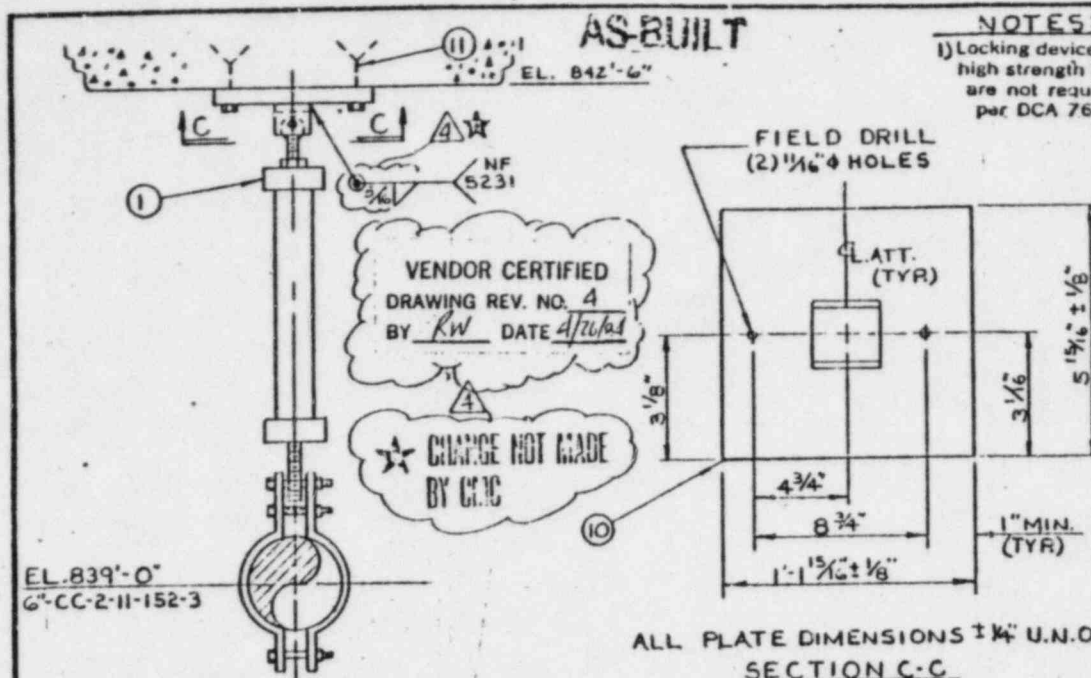
FOR MATERIALS AND OPERATIONS SEE SKETCH NO.

SHEET OF

 Brown & Root, Inc. <small>DESIGNERS AND ENGINEERS</small>		CONDITIONS	Fx	Fy	Fz	Mx	My	Mz
<u>REF. DRAWING NUMBERS</u> PIPE : MI-0604 REV 13 ELECT: EI-0600 REV 12 STEEL: SI-0600 REV 17 HV.A.C.: MI-0600 REV 16		DESIGN						
		NORMAL & UPSET			+F11			
		EMERGENCY			+F13			
		FAULTED						

REV	DATE	OWN	CHK	APP	DESCRIPTION	CUSTOMER	70443 Utilization Service.
1	5-10-73	OK	N/A	1/1	ISSUED FOR CONST.	ORDER OR CONT. NO.	CP-0048
2	5-10-73	OK	N/A	1/1	BASE PLAN & 1/1	JOB NAME	Comanche Peak 1 & 2
3	5-10-73	OK	N/A	1/1	REVISED - 1/1	DRAWING NO.	CT-1-613-007-522K
4	5-10-73	OK	N/A	1/1	REVISED - 1/1	SKETCH NO.	~
5	5-10-73	OK	N/A	1/1	REVISED - 1/1	SHEET 1 OF 2	REV. 1

FOR OFFICE AND



NOTES:
1) Locking devices for high strength bolts are not required per DCA 7607

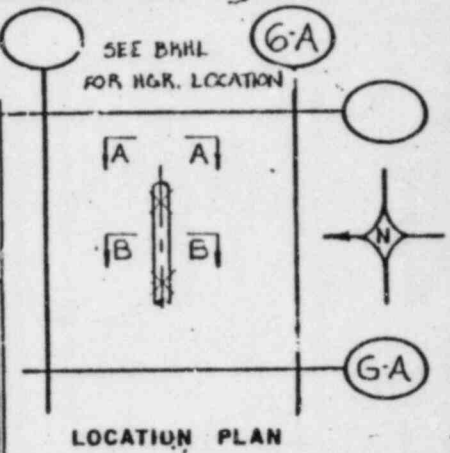
ITEM NO.	QTY REQ'D	MATERIAL	DESCRIPTION	P.B.	ISS.	PREP.	SEC.	AISC
1	1	SRS-08-PC SWAY STRUT	WI		X			
2	1	SPC-08-060 PIPE CLAMP						
3	1	SRS-03-PC SWAY STRUT	WI		X			
4	1	SPC-08-060 PIPE CLAMP						
5	1	1" THK PL. PER SECT E (SA-36/SA-515 GR.B)		X				
6	1	T.S. 1/4" X 4" X 4" X 4" 1 1/2" LG. (A-500 GR.B)		X	X			
10	1	CSR 1" THK PER SECT C-C	SA-36 OR SA-515 GR.B	X			X	
11	2	5/8" X 8 1/2" HILTI KWIK CONCRETE ANCHORS			X			
12	4	1" X 12" SUPER HILTI CONCRETE ANCHORS						

APPLY ONE COAT OF CADNO ZINC #11 TO
BOTH MAT'L EXCEPT THREADS WHICH SHALL
BE TREATED WITH A RUST PREVENTATIVE

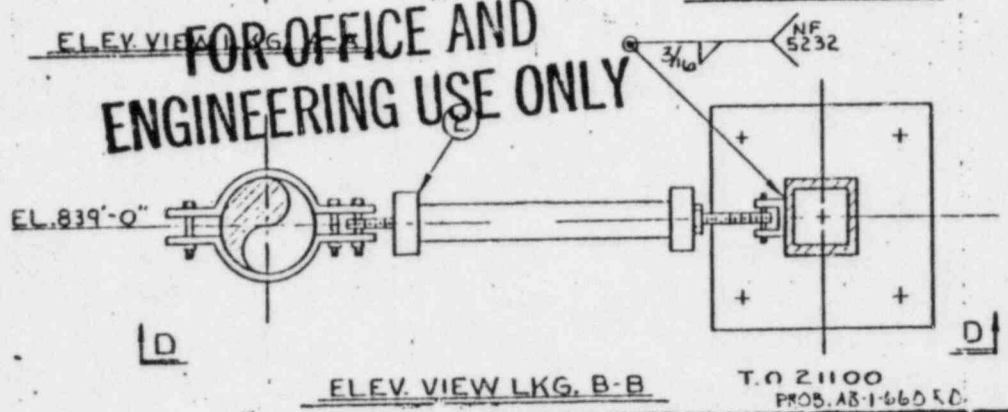
DESCRIPTION	DATE	C.H.	CHKD.	APP'D.
1 VENDOR CERTIFICATION, REF. 59790	4/26/68	TEH	CEH	CEH
2 REV VENDOR CERTIFICATION 9264	11/25/68	VM	R.G.	AP.H
3 REV'D VENDOR CERT.	4/27/68	WAR	CEH	AP.H

ASME CODE EDITION: 1974
ADDENDA: WINTER
DESIGN SPEC: MS-46A

DATA PT.	SUPPORT	LOADS (Lb)	PIPE MVTS (INCHES)
1088	DESIGN	SERVICE LEVEL LIMITS	
		A B C D	
VERT.			
N-S		-30 -201 -1058	
E-W		1103 1954 1111	
2088	DESIGN	SERVICE LEVEL LIMITS	
		A B C D	
VERT.			
N-S		-1024 -1175 -2249	
E-W		1036 1524 741	



**FOR OFFICE AND
ENGINEERING USE ONLY**



DESCRIPTION	DATE	DWN	CHKD.	APP'D.
1 IEC	11-20/67	11-20/67	11-20/67	11-20/67
2 IEC	11-20/67	11-20/67	11-20/67	11-20/67
3 IEC	11-20/67	11-20/67	11-20/67	11-20/67

NOTE
+N,E,UP
-S,W,DN

AUTHORIZED NUCL. INSP. YES ☒ NO ☐

ASME CODE CLASS 3

Brown & Root, Inc.
ENGINEERS AND CONSTRUCTORS
HOUSTON, TEXAS

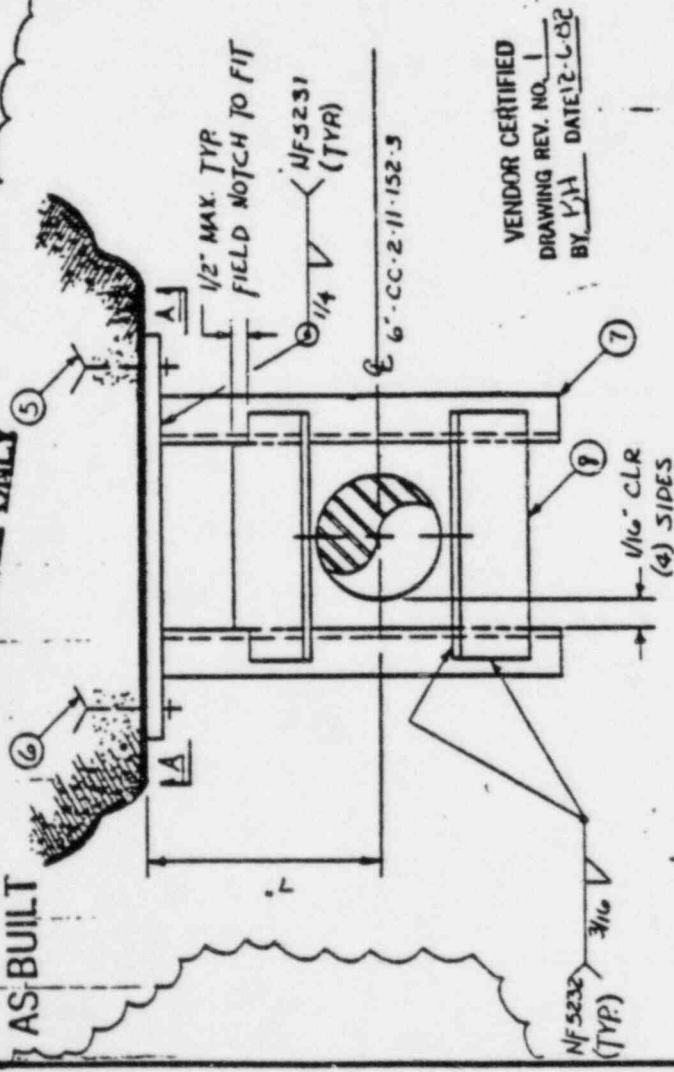
CLIENT T.U.S.I.
PLANT COMANCHE PEAK
JOB NO. 2323

SUPPORT NO. CC-2-011-716-A53R
SHEET 1 OF 2 REV. 4

**FOR OFFICE AND
ENGINEERING USE ONLY**

FOR ENGINEERING
OFFICE USE ONLY

AS BUILT



PLAN VIEW

@ ELEV. 839'-9"

MVT'S	
Y	10.025 -0.152

NOTES:
1) Locking devices for high strength bolts are not required per DCA 7602

FIELD DRILL
(4) 13/16" Ø HOLES

SECTION A-A

VENDOR CERTIFIED
DRAWING REV. NO. 1
BY V/A DATE 12-1-82

ITEM NO.	QTY	REMARKS	MATERIAL	DESCRIPTION
1	1		5/8" THK CS PL	PER SECT. A-A (S.A.36)
2	1		3/4" HT. HILTI KWIK CONCRETE ANCHORS	
3	3		3/4" x 10" HILTI KWIK BOLT	
4	2		1/4" x 3 1/2" x 1/4" LG. (S.A.36)	
5	2		1/4" x 3 1/2" x 1/2" LG. (S.A.36)	

INFORMATION COPY

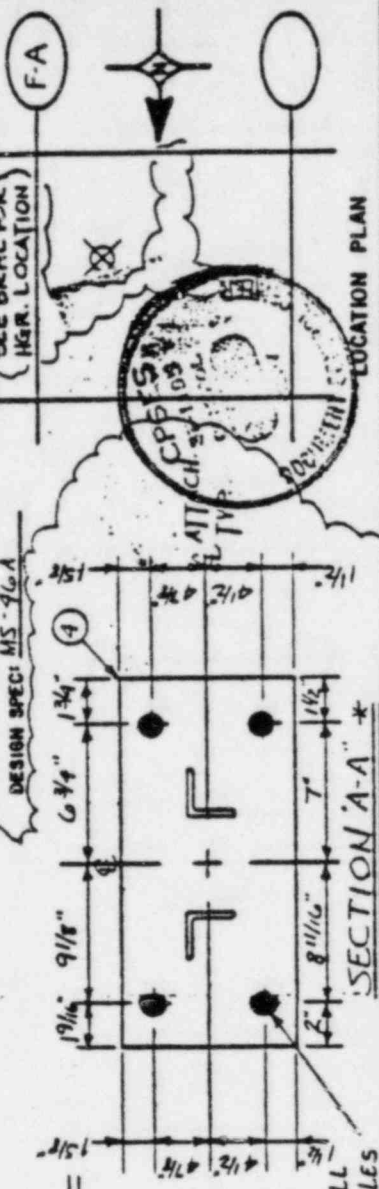
THIS DOCUMENT IS FOR INFORMATION ONLY
CONTACT: ROOM 2211 FOR INFORMATION
STATUS: FOR DESIGN

PAINT: CARBORING #11
PROBLEM: PAB-1-66-REV.0

REV	DESCRIPTION	DATE	BY	CHKD	APPD
1	AS BUILT VENDOR CERTIFICATION	12/1/82	V/A		

* QTR. LINE OF ATT. MIN VAR ± 1/8"

ASME CODE EDITION 1974
ADDENDUM 1 WINTER
DESIGN SPEC: MS-96A



LOCATION PLAN

DATE	REV	DESCRIPTION	DATE	REV	DESCRIPTION
12/1/82	1	REV'D AS NOTED PER DCA 7602	12/1/82	1	REV'D AS NOTED PER DCA 7602
12/1/82	2	REV'D AS NOTED PER DCA 7602	12/1/82	2	REV'D AS NOTED PER DCA 7602
12/1/82	3	REV'D AS NOTED PER DCA 7602	12/1/82	3	REV'D AS NOTED PER DCA 7602
12/1/82	4	REV'D AS NOTED PER DCA 7602	12/1/82	4	REV'D AS NOTED PER DCA 7602
12/1/82	5	REV'D AS NOTED PER DCA 7602	12/1/82	5	REV'D AS NOTED PER DCA 7602

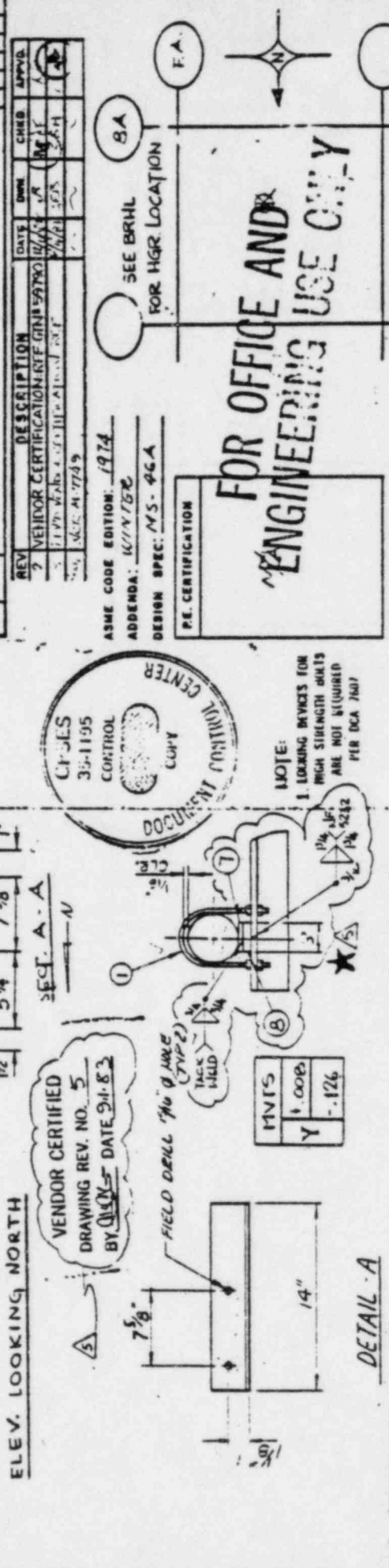
Brown & Root, Inc.

HOUSTON, TEXAS

CLIENT: U.S.I.
PLANT: COMANCHE PEAK
JOB NO. 2323

SUPPORT NO. CC-2-011-710-A53R
SHEET 1 OF 1 REV. 1

FOR OFFICE AND
ENGINEERING USE ONLY



PROB. # AB-1-66C REV O

SECTION "B-B"

TO # 21101

CHANGE NOT MADE BY CMC

LOCATION PLAN

APPROV

CHKD

APPROV

DESIGN	SUPPORT	LOADS	PIPE	STRESS	ISO	REV	MECHANICAL	REV	ELECTRICAL	REV	REV	DESCRIPTION	DWN	CHKD	APPROV
2110G	DESIGN	SERVICE	LEVEL	2	UNIT	N	M-0702	A	E-0701	9	O	IFC	11/30/79	DM	11/1/80
VERT	DESIGN	SERVICE	LEVEL	2	UNIT	N	STRUCTURAL	REV	H V A C	REV	1	REV'D AS NOTED IN F.C.M.C. 3-42 REV 5, P.H. P.C. 1-1	1-1	RE	1-1
E-W	DESIGN	SERVICE	LEVEL	2	UNIT	N	5-0721	1	M-0756	5	5	REV'D AS NOTED IN F.C.M.C. 3-42 REV 5, P.H. P.C. 1-1	1-1	RE	1-1
NOTE	DESIGN	SERVICE	LEVEL	2	UNIT	N	CC-2 AB-032	1	M-0756	5	5	REV'D AS NOTED IN F.C.M.C. 3-42 REV 5, P.H. P.C. 1-1	1-1	RE	1-1

CLIENT T. U. S. I.

PLANT COMANCHE PEAK

JOB NO 2323

SUPPORT NO. CC-2-11-709-AG3R

SHEET 1 OF 1 REV. 5

Brown & Root, Inc.

ENGINEERS AND CONSTRUCTORS

HOUSTON, TEXAS

CPSES

35-1193

PIPE

WTS

UNCHNG

REF

DWGS

DESIGN

SUPPORT

LOADS

PIPE

WTS

UNCHNG

REF

DWGS

DESIGN

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DESIGN

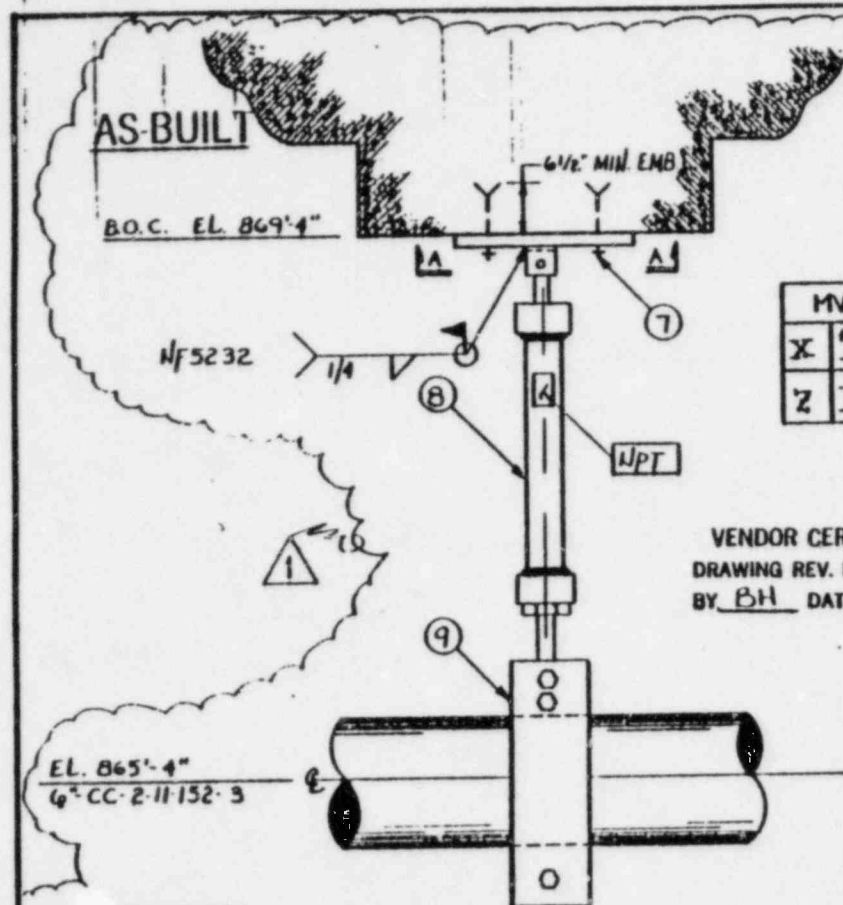
SUPPORT

LOADS

PIPE

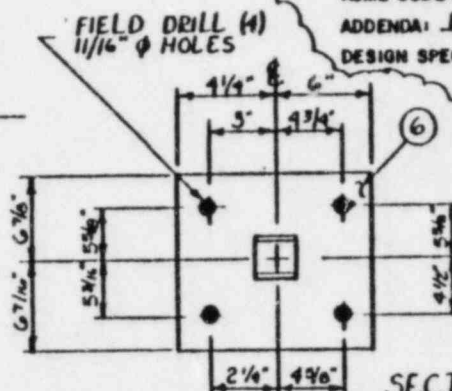
WTS

UNCHNG



MVTs	
X	0.006 -0.019
Z	-0.009 -0.012

VENDOR CERTIFIED
DRAWING REV. NO. 1
BY BH DATE 12-6-82



ITEM NO.	QTY. REQD.	MATERIAL DESCRIPTION	REV.	DATE	DWN.	CHKD.	APPVD.
6	1	3/4" THK. CS PL. PER SECT. A-A (SA36/SA515GR60)					
7	4	3/8" x 8 1/2" HILTI KWIK ANCHOR BOLTS					
8	1	SPS-10-RD SWAY STRUT CC-2-110 3/4"					
9	1	SPC-10-060 PIPE CLAMP					

INFORMATION
THIS DOCUMENT IS
CONTACT DOCUMENT
STATUS: *12/6/82*

FOR ENGINEERING
& OFFICE USE ONLY

PREP. AB-1-66C

ASME CODE EDITION 1974
ADDENDA: WINTER
DESIGN SPEC: MS-46-A



SEE BRHL FOR
HGR. LOCATION

LOCATION PLAN

NOTES:
Locking devices for
high strength bolts
are not required
per DCA 7607

ELEV. LKG. SOUTH

T.O. # 21101

DATA PT	SUPPORT	LOADS (lbs)	PIPE MVTs (INCHES)
2110	DESIGN	1265	1125
VERT.			
N-S			
E-W			

STRESS ISO.	REV.	MECHANICAL	REV.	ELECTRICAL	REV.	DESCRIPTION	DATE	DWN.	CHKD.	APPVD.
M2-3231-36	A	MI-0701	6	E1-0710-01	7	ISSUED FOR CONSTRUCTION	12/6/82			
(BRILL) ISO.	REV.	STRUCTURAL	REV.	H.V.A.C.	REV.	REV. AS NTD. REF. CMC 19812	12/6/82			
CC-2 AB-032	1	S-0735	2	MI-0758	4	DCA 7607 (SEE NT 1) 1/2" DIA	12/6/82			

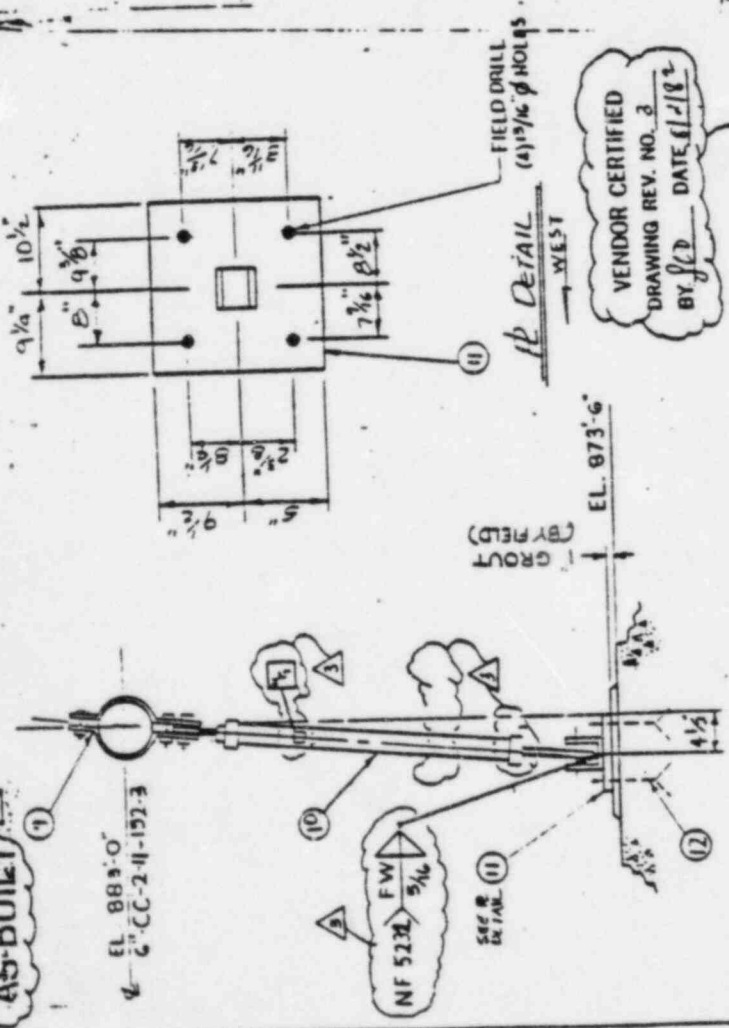
Brown & Root, Inc.
ENGINEERS AND CONSTRUCTORS
HOUSTON, TEXAS

CLIENT T.U.S.I.
PLANT COMANCHE PEAK
JOB NO. 2323

SUPPORT NO. CC-2-011-705-A63R
SHEET 1 OF 1 REV. 1

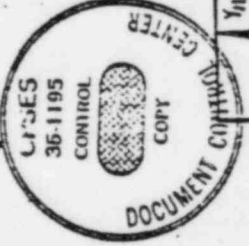
FOR OFFICE AND
FIELD USE ONLY

AS-BUILT



ELEVATION LOOKING EAST

VENDOR CERTIFIED
DRAWING REV. NO. 3
BY JED DATE 6/1/82



NOTE
4) TACKLING DRIFTS FOR
HIGH 21" HIGH BOLTS
ARE NOT REQUIRED
PER DCA 2601

BRHL ISO. CC-2 AD 50-R 1
J.P.D. Insp. CC-2 AD 50-R 1
Unit Point 1152 AD 144-R 1
Pipe Mat'l. 5106-0-0-0
Insul. 1/2" Blkg. A

To: 2100

THIRD PARTY INSPECTION
CODE CLASS: ASME III-2

ITEM NO	MATERIALS & OPERATIONS	QUANTITY	SHIP																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																														
1	SEISMIC SWAY STRUT ASSEMBLY CONSISTING OF SWS (SWAY STRUT CLAMP) N85PC-1-060 SRS (SWAY STRUT) TYP P, SIZE 1/4"	ONE																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																															
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3	1/2" THK. C. PLATE 158-36 OR SA315 68, 65																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																
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5	3/4" x 10' LONG. MULTI KWINK BOLT CONCRETE	4																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																															
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8	SEISMIC ASSEMBLY SKETCH AND ENGINEERING BUNDLE AND TAG MARK # CC-2-011-0006-A73R	1																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																															
9	Apply Carbo-Zinc fill to above but except the area which shall be treated with a rust preventative																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																
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OA	52	6/1/82	JED			REV FOR NIS/REV OA	53	6/1/82	JED			REV FOR NIS/REV OA	54	6/1/82	JED			REV FOR NIS/REV OA	55	6/1/82	JED			REV FOR NIS/REV OA	56	6/1/82	JED			REV FOR NIS/REV OA	57	6/1/82	JED			REV FOR NIS/REV OA	58	6/1/82	JED			REV FOR NIS/REV OA	59	6/1/82	JED			REV FOR NIS/REV OA	60	6/1/82	JED			REV FOR NIS/REV OA	61	6/1/82	JED			REV FOR NIS/REV OA	62	6/1/82	JED			REV FOR NIS/REV OA	63	6/1/82	JED			REV FOR NIS/REV OA	64	6/1/82	JED			REV FOR NIS/REV OA	65	6/1/82	JED			REV FOR NIS/REV OA	66	6/1/82	JED			REV FOR NIS/REV OA	67	6/1/82	JED			REV FOR NIS/REV OA	68	6/1/82	JED			REV FOR NIS/REV OA	69	6/1/82	JED			REV FOR NIS/REV OA	70	6/1/82	JED			REV FOR NIS/REV OA	71	6/1/82	JED			REV FOR NIS/REV OA	72	6/1/82	JED			REV FOR NIS/REV OA	73	6/1/82	JED			REV FOR NIS/REV OA	74	6/1/82	JED			REV FOR NIS/REV OA	75	6/1/82	JED			REV FOR NIS/REV OA	76	6/1/82	JED			REV FOR NIS/REV OA	77	6/1/82	JED			REV FOR NIS/REV OA	78	6/1/82	JED			REV FOR NIS/REV OA	79	6/1/82	JED			REV FOR NIS/REV OA	80	6/1/82	JED			REV FOR NIS/REV OA	81	6/1/82	JED			REV FOR NIS/REV OA	82	6/1/82	JED			REV FOR NIS/REV OA	83	6/1/82	JED			REV FOR NIS/REV OA	84	6/1/82	JED			REV FOR NIS/REV OA	85	6/1/82	JED			REV FOR NIS/REV OA	86	6/1/82	JED			REV FOR NIS/REV OA	87	6/1/82	JED			REV FOR NIS/REV OA	88	6/1/82	JED			REV FOR NIS/REV OA	89	6/1/82	JED			REV FOR NIS/REV OA	90	6/1/82	JED			REV FOR NIS/REV OA	91	6/1/82	JED			REV FOR NIS/REV OA	92	6/1/82	JED			REV FOR NIS/REV OA	93	6/1/82	JED			REV FOR NIS/REV OA	94	6/1/82	JED			REV FOR NIS/REV OA	95	6/1/82	JED			REV FOR NIS/REV OA	96	6/1/82	JED			REV FOR NIS/REV OA	97	6/1/82	JED			REV FOR NIS/REV OA	98	6/1/82	JED			REV FOR NIS/REV OA	99	6/1/82	JED			REV FOR NIS/REV OA	100	6/1/82	JED			REV FOR NIS/REV OA
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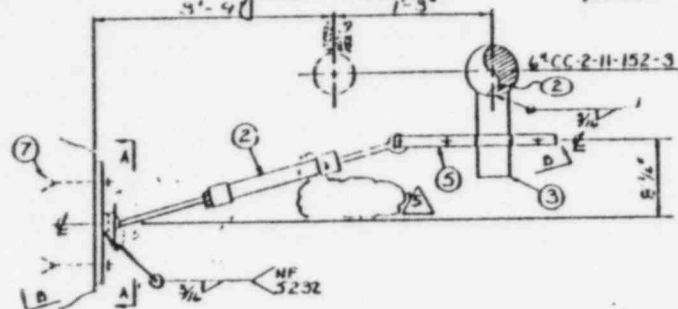
FOR OFFICE AND

FOR OFFICE AND

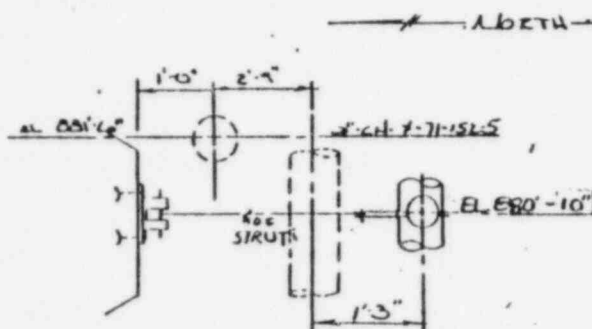
CUSTOMER Texas Utilition Service,
ORDER OR CONT. NO. CP-0018
JOB NAME Comanche Peak 1 & 2
MARK NO. CC-2-011-0006-A73R
SKETCH NO.
SHEET 1 OF 1 REV. 5

FOR OFFICE AND ENGINEERING USE ONLY

BLUELINE
AS-BUILT
VENDOR CERTIFIED
DRAWING REV. NO. 5
BY *[Signature]* DATE 7/19/83
NOTE: 1) Locking devices for high strength bolts are not required per DCA 7607

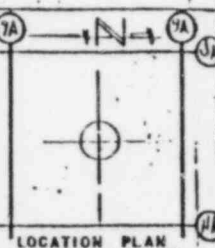


PLAN VIEW



SECTION B-B

SEE BRILL FOR
HGR. LOCATION



THIRD PARTY INSPECTION
CODE CLASS: ASME III-3

PARH ISO CC-2-AB-050 R.1
I.P.D. Iso. CC-2-AB-050 R.1
Data Point: 2131 ABTLLC R.1
Pipe Mat'l: SA106C GR.B
Insul: 1/2" EMDP A

ITEM NO.	NO REQD	PART CALL-OUT	DESCRIPTION	MATERIAL	MIC NO.	WT.	POS	L	CSS	PRIM	SEC	AISC
1	1	ISA 12-512	FRONT ANCHORS									
2	1	ERS DR RD	SWAY STRUT									
3	1	SAE 5/16-11-152-3										
4	1	SAE 5/16-11-152-3										
5	1	SAE 5/16-11-152-3										
6	1	SAE 5/16-11-152-3										
7	1	SAE 5/16-11-152-3										

NO ABT'L BY GRINDING

SEISMIC ASSEMBLY SKETCH AND ENGINEERING
BUNDLE AND TAG -
MARK # CC-2-011-005-A73R

Apply Carso-Zinc #11 to above
mat'l except in as which shall
be treated with a rust
preventative

CPSES
35-1193
CONTROL


FOR OFFICE AND ENGINEERING USE ONLY

REV	DATE	OWN	CNA	APP	DESCRIPTION
1	7/19/83	BY	Q	BY	REV. AS NOTED REF. CAC 43587 DCA-7607 LEE NT-4 AS BUILT VENDOR CERTIFICATE; REF GTU #9770
2	7/19/83	BY	Q	BY	REV. VENDOR CERT.

QUAN SHIP

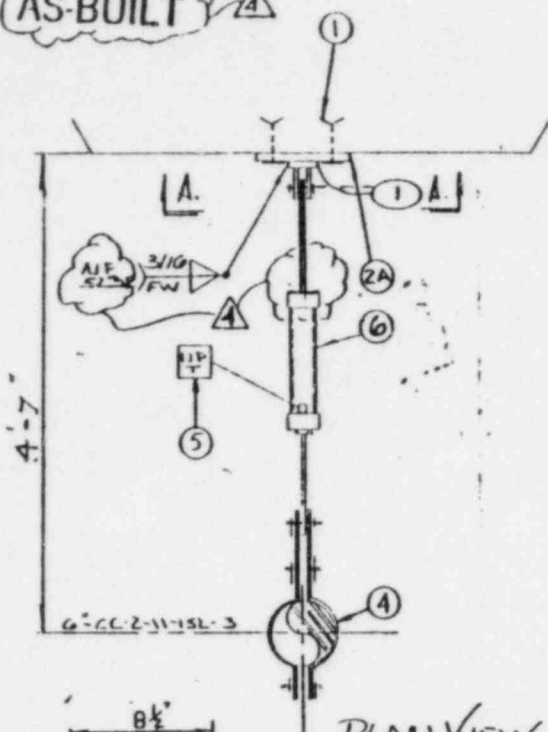
FOR MATERIALS AND OPERATIONS SEE SKETCH NO.

(SHEET OF

 Brown & Root, Inc. <small>DESIGNERS AND ENGINEERS</small>					CONDITIONS					Fx	Fy	Fz	Mx	My	Mz
REF. DRAWING NUMBERS PIPE: MI-0103-01 R/O ELECT: MI-0104-01 STEEL: S-0135 E012 HV.A.C: MI-0137 E1					DESIGN		NORMAL & UPSET		-262	—	-6	—	—	—	
					EMERGENCY		—		-262	—	-6	—	—	—	
					FAULTED		—		-262	—	-6	—	—	—	
REV	DATE	OWN	CNA	APP	DESCRIPTION	CUSTOMER Foxan Utilities Service, Inc									
1	6-5-71	JW	BY	BY	ISSUE FOR CONST. FW 1-2	ORDER OR CONT. NO. CP-0046									
2	2-20-80	RY	BY	BY	REV. PER NPS1 REV CA	JOB NAME Oronoke Peak 2 & 2									
3	1-15-81	XC	BY	BY	REV. AS NOTED REF. CAC 3106 R1	MARK NO. CC-2-011-005-A73R									
4	11-30-81	BY	BY	BY	REV. AS NOTED REF. CAC 3350 R1 PHDP 1134 R1	SKETCH NO.									
						SHEET 1 OF 1 REV. 5									

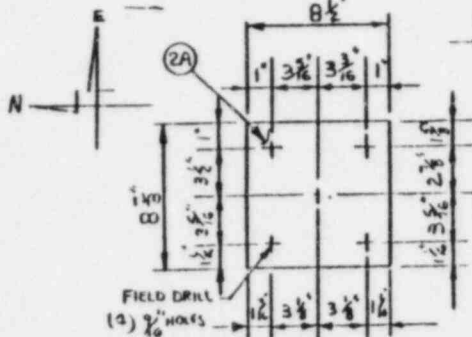
OTFSCONT-
CKING DEVICES FOR
IN STRENGTH BOLTS
ARE NOT REQUIRED
PER DCA 7607

AS-BUILT



PLAN VIEW
@ EL 8'7'-10"

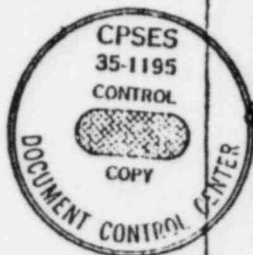
NORTH



SECTION 'A-A'

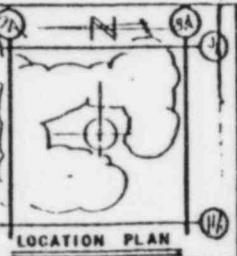
TO 21K10

VENDOR CERTIFIED
DRAWING REV. NO. 4
BY JCD DATE 2/1/82



BRHL ISO. CC-2-AB-50 REV. 1
I.P.D. ISO. CC-2-AB-36-1.0
Data Point 21291 PAB14CRO
Pipe Hat'l. SDRG GLE
Insul. YL Rldg. A

SEE BRHL FOR
HGR. LOCATION



THIRD PARTY INSPECTION YES NO
CODE CLASS: ASME III-B

ITEM NO.	NO REQD	PART CALL-OUT	DESCRIPTION	MATERIAL	MIC NO.	WT.	PBS	L	CSS	PRIM	SEC	AISC
1	4	BSA 12-512	CONC ANCHORS									
2	1	2 3/4\" x 2 3/4\" SWS CL-400	SWAY BRACE	SA 36	670	20						
3	1	SA 36 CL-400	PIPE CLAMP	SA 36		1/4						
4	1	DRG 2078A	ASME III PLATE	SA 36								
5	1	2 1/2\" x 8\" x 1/4\"	CS PLATE	SA 36								
6	1	SWS-DL-RD	SWAY BRACE G.C. 3-8"									

NO DATA BY GRUNNELL

SEISMIC ASSEMBLY SKETCH AND ENGINEERING
BUNDLE AND TAG
MARK # CC-2-011-004-A73R

Apply Carbo-Zinc 211 to above
mat'l except th'ds which shall
be treated with a rust
preventative

FOR ENGINEERING
OFFICE USE ONLY

~~THIS DRAWING IS FOR INFORMATION ONLY.
CONTACT ENGINEERING CONTROL FOR
CURRENT STATUS AND REVISIONS.~~

REV	DATE	OWN	CHK	APP	DESCRIPTION
1	1-14-81	PJB	JP		REV. AS NOTED REF DCA 7607 X-ENT. 4, SMC 766 BGR PHHP 324-DLETED NT '31-3 (AS BUILT)
2					VENDOR CERTIFICATION REF. GTN 4 59790

QUAN SHIP

FOR MATERIALS AND OPERATIONS SEE SKETCH NO. 4 SHEET OF



Brown & Root, Inc.

REF. DRAWING NUMBERS

PIPE: MI-0705-01.R.D ELECT: 17-0704 R.3
STEEL: SC755 R.2 HV.A.C: MI-0167 R.4

REV	DATE	OWN	CHK	APP	DESCRIPTION
1	6-3-79	JW	PJM		ISSUE FOR CONST
2	2-21-80	PJ	PJM	JW	REV. PER NIST REV CA
3	4-26-80	RS	PJM	ES	REV. AS NOTED REF CC 324

CONDITIONS	Fx	Fy	Fz	Mx	My	Mz
DESIGN			405			
NORMAL & UPSET			1420			
EMERGENCY			950			
FAULTED			1960			

CUSTOMER Texas Utilities Service, Inc.
ORDER OR CONT. NO. CP-0046
JOB NAME Comanche Fork 1 & 2
MARK NO. CC-2-011-004-A73R
SKETCH NO.
SHEET 1 OF 1 REV. 4

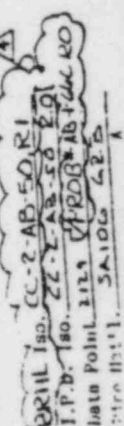
FOR OFFICE AND

ENGINEERING USE ONLY

THIS DOCUMENT IS FOR INFORMATION ONLY.
CONTACT DOCUMENT CONTROL FOR CURRENT
STATUS AND REVISION.

BY Ar DATE 1/29/83

ARE NOT REQUIRED



ITEM NO.	NO. REQD.	PART CALL-OUT	DESCRIPTION	MATERIAL	MIC. NO.	WT.	PBS	CSB	PRIN	SEC	AISC
1	1	BR 12-512	1016 AN 1016'S	SA 36	170 20	3					
2	1	RE 12-512	1016 AN 1016'S	SA 36	170 20	3					
3	1	SA 36	1016 AN 1016'S	SA 36	170 20	3					
4	1	CS 512	1016 AN 1016'S	SA 36	170 20	3					
5	1	CS 512	1016 AN 1016'S	SA 36	170 20	3					
6	1	CS 512	1016 AN 1016'S	SA 36	170 20	3					
7	1	CS 512	1016 AN 1016'S	SA 36	170 20	3					
8	1	CS 512	1016 AN 1016'S	SA 36	170 20	3					
9	1	CS 512	1016 AN 1016'S	SA 36	170 20	3					
10	1	CS 512	1016 AN 1016'S	SA 36	170 20	3					
11	1	CS 512	1016 AN 1016'S	SA 36	170 20	3					
12	1	CS 512	1016 AN 1016'S	SA 36	170 20	3					
13	1	CS 512	1016 AN 1016'S	SA 36	170 20	3					
14	1	CS 512	1016 AN 1016'S	SA 36	170 20	3					
15	1	CS 512	1016 AN 1016'S	SA 36	170 20	3					
16	1	CS 512	1016 AN 1016'S	SA 36	170 20	3					
17	1	CS 512	1016 AN 1016'S	SA 36	170 20	3					
18	1	CS 512	1016 AN 1016'S	SA 36	170 20	3					
19	1	CS 512	1016 AN 1016'S	SA 36	170 20	3					
20	1	CS 512	1016 AN 1016'S	SA 36	170 20	3					
21	1	CS 512	1016 AN 1016'S	SA 36	170 20	3					
22	1	CS 512	1016 AN 1016'S	SA 36	170 20	3					
23	1	CS 512	1016 AN 1016'S	SA 36	170 20	3					
24	1	CS 512	1016 AN 1016'S	SA 36	170 20	3					
25	1	CS 512	1016 AN 1016'S	SA 36	170 20	3					
26	1	CS 512	1016 AN 1016'S	SA 36	170 20	3					
27	1	CS 512	1016 AN 1016'S	SA 36	170 20	3					
28	1	CS 512	1016 AN 1016'S	SA 36	170 20	3					
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30	1	CS 512	1016 AN 1016'S	SA 36	170 20	3					
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91	1	CS 512	1016 AN 1016'S	SA 36	170 20	3					
92	1	CS 512	1016 AN 1016'S	SA 36	170 20	3					
93	1	CS 512	1016 AN 1016'S	SA 36	170 20	3					
94	1	CS 512	1016 AN 1016'S	SA 36	170 20	3					
95	1	CS 512	1016 AN 1016'S	SA 36	170 20	3					
96	1	CS 512	1016 AN 1016'S	SA 36	170 20	3					
97	1	CS 512	1016 AN 1016'S	SA 36	170 20	3					
98	1	CS 512	1016 AN 1016'S	SA 36	170 20	3					
99	1	CS 512	1016 AN 1016'S	SA 36	170 20	3					
100	1	CS 512	1016 AN 1016'S	SA 36	170 20	3					

FOR ENGINEERING
& OFFICE USE ONLY

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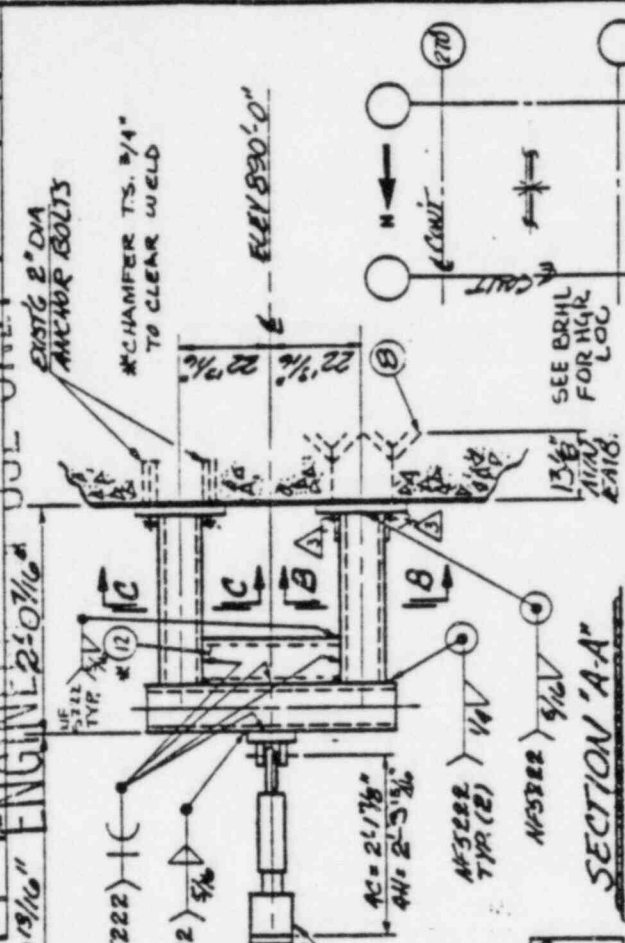
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REVISIONS

BLUELINE 1-13-81
AS-BUILT

VENDOR CERTIFIED
DRAWING REV. NO. 3
REVISED DATE 10-18-83

ITEM NO.	DESCRIPTION	QTY	UNIT	ALIAS OR ALIAS	REV.	MISC.
1	SMA-35-50 HEX. NUTS	1				
2	SMA-35-50 PIPE CLAMP	1				
3	ASME III NAME PLATE	1				
4	SMA-35-50 HEX. NUTS	1				
5	SMA-35-50 PIPE CLAMP	1				
6	ASME III NAME PLATE	1				
7	SMA-35-50 HEX. NUTS	1				
8	SMA-35-50 PIPE CLAMP	1				
9	ASME III NAME PLATE	1				
10	SMA-35-50 HEX. NUTS	1				
11	SMA-35-50 PIPE CLAMP	1				
12	ASME III NAME PLATE	1				
13	SMA-35-50 HEX. NUTS	1				
14	SMA-35-50 PIPE CLAMP	1				
15	ASME III NAME PLATE	1				
16	SMA-35-50 HEX. NUTS	1				
17	SMA-35-50 PIPE CLAMP	1				
18	ASME III NAME PLATE	1				
19	SMA-35-50 HEX. NUTS	1				
20	SMA-35-50 PIPE CLAMP	1				
21	ASME III NAME PLATE	1				
22	SMA-35-50 HEX. NUTS	1				
23	SMA-35-50 PIPE CLAMP	1				
24	ASME III NAME PLATE	1				
25	SMA-35-50 HEX. NUTS	1				
26	SMA-35-50 PIPE CLAMP	1				
27	ASME III NAME PLATE	1				
28	SMA-35-50 HEX. NUTS	1				
29	SMA-35-50 PIPE CLAMP	1				
30	ASME III NAME PLATE	1				



REV	DESCRIPTION	DATE	CHK'D	DATE	APP'D	DATE
1	REVISED	10-18-83				
2	REVISED	10-18-83				
3	REVISED	10-18-83				
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29	REVISED	10-18-83				
30	REVISED	10-18-83				

REV	DESCRIPTION	DATE	CHK'D	DATE	APP'D	DATE
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28	REVISED	10-18-83				
29	REVISED	10-18-83				
30	REVISED	10-18-83				

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INFORMATION COPY

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CONTACT PROJECT ENGINEER FOR CURRENT
STATUS AND REVISIONS.

FOR ENGINEERING
OFFICE USE ONLY

FOR OFFICE AND
ENGINEERING USE ONLY

BLUELINE EXEMPT

AS-BUILT

VENDOR CERTIFIED

DRAWING REV. NO. 1

DATE 3-10-83

MATERIAL SUPPLIED WITH
MK. # CT-137-702-S25R
(REF.)

10" CT-137-301 R.5

ELEV. 789.93

1" GROUT

ELEV. LKG. NORTH

CHANGES NOT MADE
BY CMC

FIELD DRILL (4)
1 1/4" HOLES

SECTION "A-A" STEEL SHOWN ROTATED FOR CLARITY

ASME CODE EDITION: ---
ADDENDA: ---
DESIGN SPEC: MS-46B

NOTES:

1) THIS SUPPORT
REPLACES SUPPORT
CT-137-E02-S25R

2) To keep the new hot
bracket, the bolts
are not required
per LRA 7007

ITEM NO.	QTY.	MATERIAL	DESCRIPTION	PS	CS	MS	AL	SS
1	1	SWAY STRUT SRS-20-PC	CC=3'-7 1/2"					
2	1	WITH SPC-20-100 PIPE CLAMP (SAB)						
3	4	1" THK CARBON STEEL PLATE (A36)	(SEE SECTION "A-A")					
4	1	1" x 12" LG. SUPER HILTI KWIK BOLT						
5	1	TUBE STEEL 4" x 1/2" x 17' 1/2" LG.	(A500GRB)					

REV.	DESCRIPTION	DATE	DWN.	CHKD.	APPVD.
1	ISSUED FOR CONSTRUCTION	3/10/83	YLM	WMP	WJL
2	CONF. BELOW				

PAINT: CARBO-ZINC #11

FIELD CUT TO SUIT

PROB # AB-132-RC

SEE BRILL
FOR HGR.
LOC.

CS

LOCATION PLAN

REV	SUPPORT LOADS (lbs)					PIPE
DESIGN	SERVICE LEVEL LIMITS				MVTS (INCHES)	
	A	B	C	D		
1	3352	5271	6293		10.000	
2	72	16247	12473		10.000	
3					10.000	
4					10.000	
5	2961	4655	5553		10.000	
6	13	11631	12739		10.000	
AUTHORIZED NUCL. INSP					YES <input type="checkbox"/> NO <input checked="" type="checkbox"/>	
ASME CODE CLASS					AS-1	

REV.	DESCRIPTION	DATE	DWN.	CHKD.	APPVD.
1	BRILL 180.				
2	CT-137-003				
3	MECHANICAL				
4	MI-0626				
5	STRUCTURAL				
6	SI 0600				
7	CT-137-003				
8	REV.				
9	REV.				
10	REV.				
11	REV.				
12	REV.				
13	REV.				
14	REV.				
15	REV.				
16	REV.				
17	REV.				
18	REV.				
19	REV.				
20	REV.				

REV.	DESCRIPTION	DATE	DWN.	CHKD.	APPVD.
1	REV. AS NTD: REF: CMC				
2	REV. AS NTD: REF: CMC				
3	REV. AS NTD: REF: CMC				
4	REV. AS NTD: REF: CMC				
5	REV. AS NTD: REF: CMC				
6	REV. AS NTD: REF: CMC				
7	REV. AS NTD: REF: CMC				
8	REV. AS NTD: REF: CMC				
9	REV. AS NTD: REF: CMC				
10	REV. AS NTD: REF: CMC				
11	REV. AS NTD: REF: CMC				
12	REV. AS NTD: REF: CMC				
13	REV. AS NTD: REF: CMC				
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17	REV. AS NTD: REF: CMC				
18	REV. AS NTD: REF: CMC				
19	REV. AS NTD: REF: CMC				
20	REV. AS NTD: REF: CMC				

REV.	DESCRIPTION	DATE	DWN.	CHKD.	APPVD.
1	REV. AS NTD: REF: CMC				
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3	REV. AS NTD: REF: CMC				
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7	REV. AS NTD: REF: CMC				
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20	REV. AS NTD: REF: CMC				



Brown & Root, Inc.
ENGINEERS AND CONSTRUCTORS
HOUSTON, TEXAS

CLIENT: T.U.S.I.
PLANT: COMANCHE PEAK
JOB NO.: 2323

SUPPORT NO.: CT-137-701-S25R
SHEET 1 OF 1 REV. 1

FOR OFFICE USE

THIS DOCUMENT CONTAINS DESIGN CHANGES

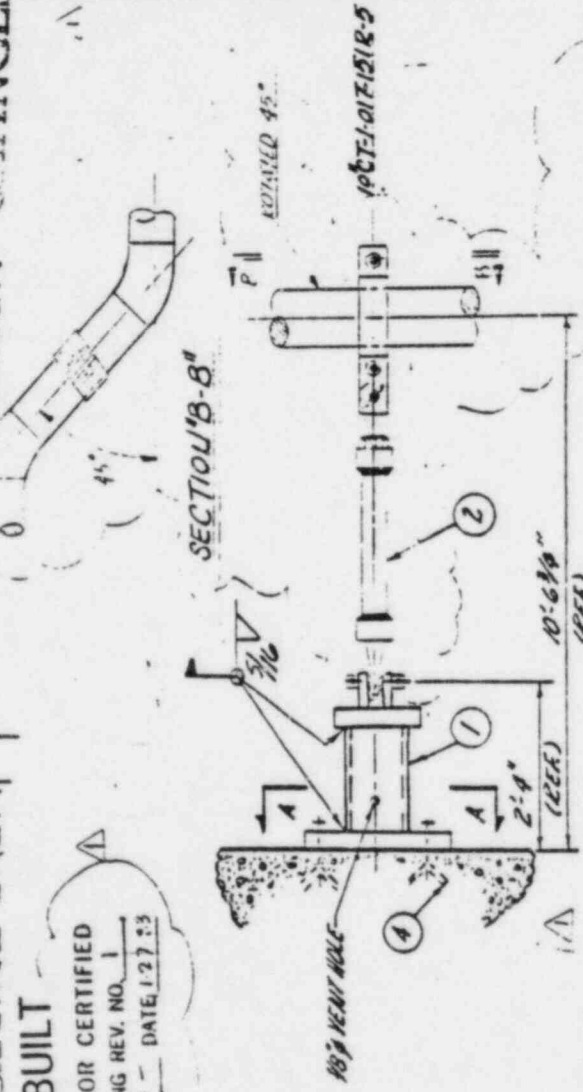
BLUELINE EXEMPT
AS-BUILT

VENDOR CERTIFIED
DRAWING REV. NO. 1
BY 111 - DATE 1/27/83

DESIGN CHANGES

ITEM NO.	QTY. REQD.	MATERIAL	DESCRIPTION
1	1	7.5 3/4" x 200' x 2" PLG AND 2 SUPP. A. 3002B	
2	1	3/4" x 200' x 2" PLG AND 2 SUPP. A. 3002B	
3	1	3/4" x 200' x 2" PLG AND 2 SUPP. A. 3002B	
4	4	3/4" x 200' x 2" PLG AND 2 SUPP. A. 3002B	
		1/4" x 12" SUPER HILTI WIRE CONC. AUGER 1002	
		(MIN. ENDS = 3 1/2')	

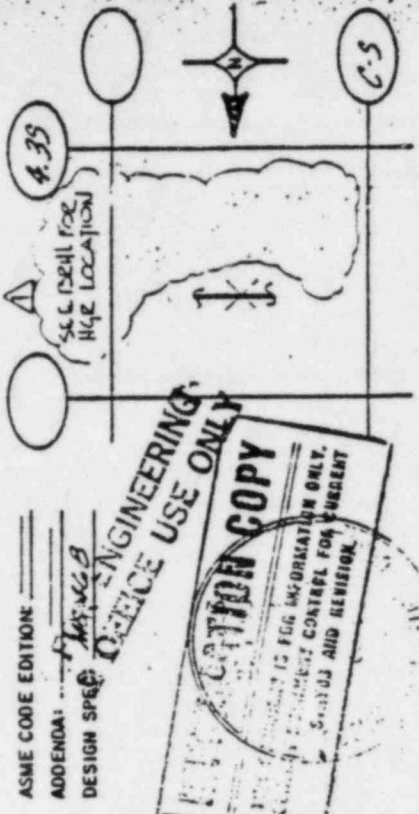
REV.	DESCRIPTION	DATE	CHKD.	APPROV.
1	1/4" x 12" SUPER HILTI WIRE CONC. AUGER 1002			
2	1/4" x 12" SUPER HILTI WIRE CONC. AUGER 1002			
3	1/4" x 12" SUPER HILTI WIRE CONC. AUGER 1002			
4	1/4" x 12" SUPER HILTI WIRE CONC. AUGER 1002			



PLAN VIEW @ EL. 108' 6" (REF.)

NOTES:
1) Locking devices for high strength bolts are not required per DCA 7607

SEE CPGA # 14919
FOR E' NUMBER INFORMATION
10' 4802



LOCATION PLAN

DATA PT.	SUPPORT	LOADS	UNIT	TYPE	NO.
DESIGN	DESIGN	SERVICE	LEVEL	LIMITS	INCHES
VERT.	VERT.	VERT.	VERT.	VERT.	VERT.
N-S	N-S	N-S	N-S	N-S	N-S
E-W	E-W	E-W	E-W	E-W	E-W

REV.	DESCRIPTION	DATE	CHKD.	APPROV.
1	1/4" x 12" SUPER HILTI WIRE CONC. AUGER 1002			
2	1/4" x 12" SUPER HILTI WIRE CONC. AUGER 1002			
3	1/4" x 12" SUPER HILTI WIRE CONC. AUGER 1002			
4	1/4" x 12" SUPER HILTI WIRE CONC. AUGER 1002			

REV.	DESCRIPTION	DATE	CHKD.	APPROV.
1	1/4" x 12" SUPER HILTI WIRE CONC. AUGER 1002			
2	1/4" x 12" SUPER HILTI WIRE CONC. AUGER 1002			
3	1/4" x 12" SUPER HILTI WIRE CONC. AUGER 1002			
4	1/4" x 12" SUPER HILTI WIRE CONC. AUGER 1002			

Brown & Root, Inc.

PLANT COMANCHE PEAK
JOB NO. 2323

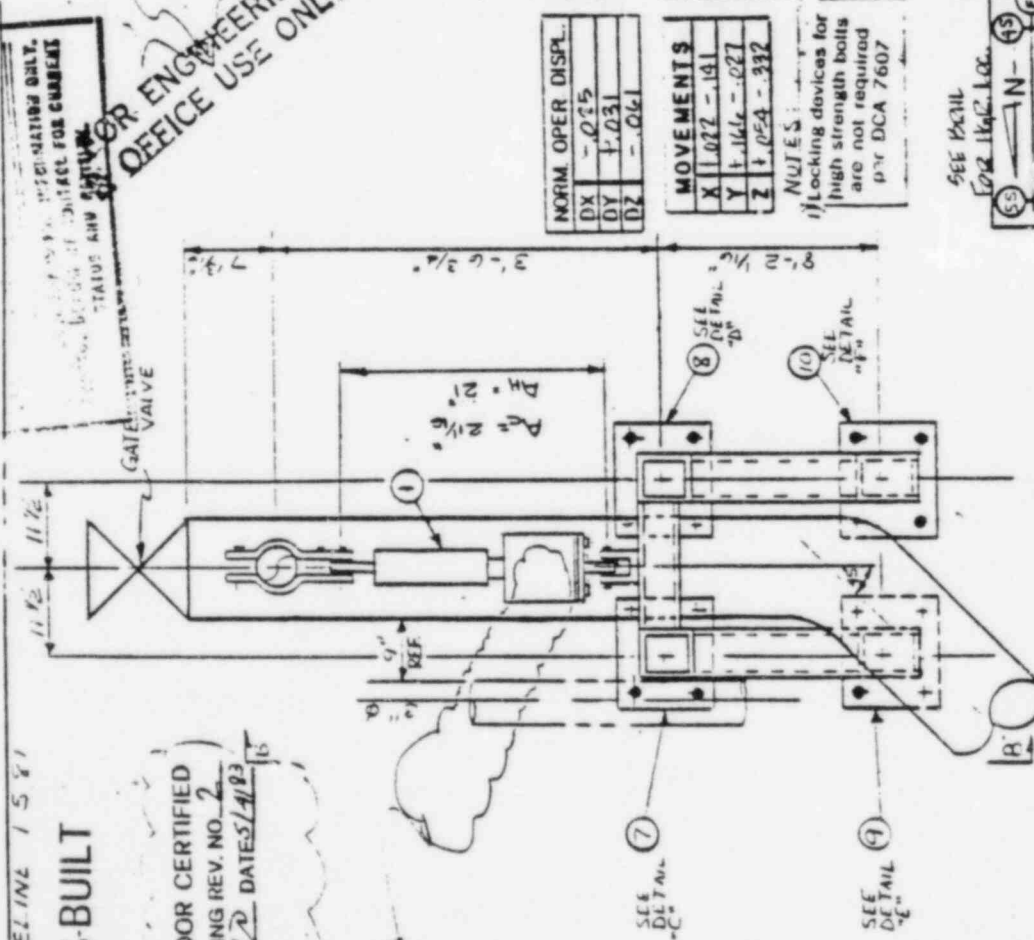
SUPPORT NO. C-1017-104-5222
SHEET 1 OF 1 REV. 1

ENCLOSURE

AS-BUILT

8

FOR ENGINEERING
OFFICE USE ONLY



To #4802 PLAN VIEW @ EL 818'-0"

2431 Iso. 251-58-0321
P.D. Iso. CTISO 8 REV 5
Data Point 251-58-0321
Pipe Mat'l. SA 358 CL 1 JD 304
Bldg. SR

THIRD PARTY INSPECTION
CODE CLASS: ASME III-2

[illegible]

FOR MATERIALS AND OPERATIONS SEE SKETCH NO. SHEET OF

[illegible]

ONLY ABOVE

FOR OFFICE AND ENGINEERING USE ONLY

BLUELINE 1-16-BL
AS-BUILT

VENDOR CERTIFIED
DRAWING REV. NO. 3
BY 17 DATE 9/18/83

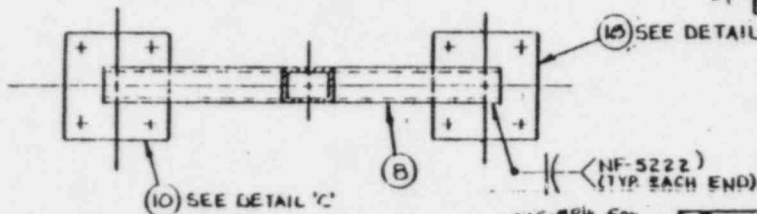
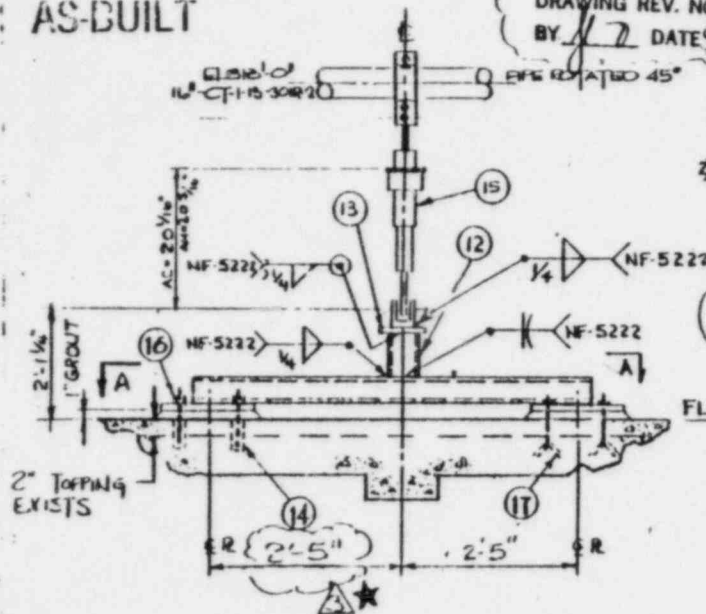
NOTE:
1) PIPE MOVEMENT IS
YELUP $\frac{3}{8}$ " WHEN HOT.
2) LOCKING BOLTS FOR
HIGH STRENGTH BOLTS
ARE NOT REQUIRED
PER DCA 7507

★ CHANGE NOT MADE
BY CMC

FLR. EL. 810'-6"

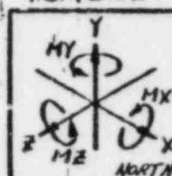
NORM. OPER. DISPL.	
DX	+0.23
DY	+1.54
DZ	-0.04

MOVEMENTS	
X	+1.37/-0.09
Y	+7.14/-1.17
Z	+0.07/-0.51



SECTION A-A

615 BRK FOR
HGR. LOG.
T.O. 4802



DRILL 150 C.F. 1-16-BL 0006/1
I.P.D. No. CT-1-02-B-REVS
Data Point: G2/PBQB A-1-31 R.O.
Pipe Mat. 1-2A 350 CL. 1-TP-204

THIRD PARTY INSPECTION
CODE CLASS: ASME III-2

ITEM NO.	MATERIALS & OPERATIONS	QUAN	SHIP	PS	CS	PR	SEC	ATSC
	SEISMIC MECHANICAL SHOCK SUPPRESSOR CONSISTING OF:							
1	10'-6" STROKE, FIG. 307N MECHANICAL SHOCK SUPPRESSOR, W/1-1/2" 16" O.D. PIPE, CARBON STEEL, LOAD=15000	1						
2	T.S. 3/4" x 6" x 4" x 5" B.L.G. (A500 GR.B)	1						
3	C.S. R 1" x 1/2" x 1/2" x 1/2" / DETAIL 'B' (SA 36/SA 515 GR.B)	1						
4	C.S. R 1" x 1/2" x 1/2" x 1/2" / DETAIL 'C' (SA 36/SA 515 GR.B)	1						
5	1/2" x 10" WELT W/IN CONG. ANCHOR	1						
6	T.S. 3/4" x 4" x 1" B.L.G. (A500 GR.B)	1						
7	C.S. R 3/4" x 0" x 5" x 0" 7/4" (SA 36/SA 515 GR.B)	1						
8	1/2" x 10" THREADED ROD FOR RICHMOND INSERT (FIELD CUT TO LENGTH) (SA 36)	1						
9	SMA R.P.C. 1" x 1/2" x 1/2" x 1/2" / DETAIL 'B' (SA 36/SA 515 GR.B)	1						
10	W/SR-14-100 RUBBER W/ PIPE CLAMP	1						
11	SEISMIC ASSEMBLY SKETCH AND ENGINEERING BUNDLE AND TAG	1						
12	MARK # CT-1-013-020-542K	1						
13	FXN-1/2" HEX NUTS	8						
14	1/4" x 18" SUPER MULTI KWIK BOLTS -#13/8" MILL ERB.	4						
15	1" C.S.R. (PER DETAIL 'B') SA 36	1						
	Apply one coat of Carbo Zinc #11 to above mat'l except th'ds which shall be coated w/a rust preventative.							
REV	DATE	DWN	CNK	APP	DESCRIPTION			
1	9/18/83	VM	R	H	REV'D VENDOR CERT			
Approved By: J. FC					QUAN S.I.P.			
Date: 9-30-79								

FOR MATERIALS AND OPERATIONS SEE SKETCH NO.

SHEET OF

Brown & Root, Inc.					CONDITIONS	Fx	Fy	Fz	Mx	My	Mz
REF. DRAWING NUMBERS					DESIGN						
PIPE: M1-0617-REV.3 ELECT: 2-REV.9					NORMAL & UPSET		15050				
STEEL: S1-0608-REV.4 HVAC: 1-REV.1					EMERGENCY		1911				
					FAULTED						
REV	DATE	DWN	CNK	APP	DESCRIPTION		CUSTOMER				
1	9/18/83	VM	R	H	ISSUED FOR CONST.		Tough Construction Co., Inc.				
2	9/18/83	VM	R	H	REF. NPSI R.O.D.		ORDER JR CONT. NO. CT-0-15				
3	9/18/83	VM	R	H	REV AS NYD: REF FIELD MODIFIED NUMBER		JG9 NAME CONG OF 1982 1 & 2				
4	9/18/83	VM	R	H	REV AS NYD: REF FIELD MODIFIED NUMBER		MARK NO. CT-1-013-020-542K				
5	9/18/83	VM	R	H	REV AS NYD: REF FIELD MODIFIED NUMBER		SKETCH NO.				

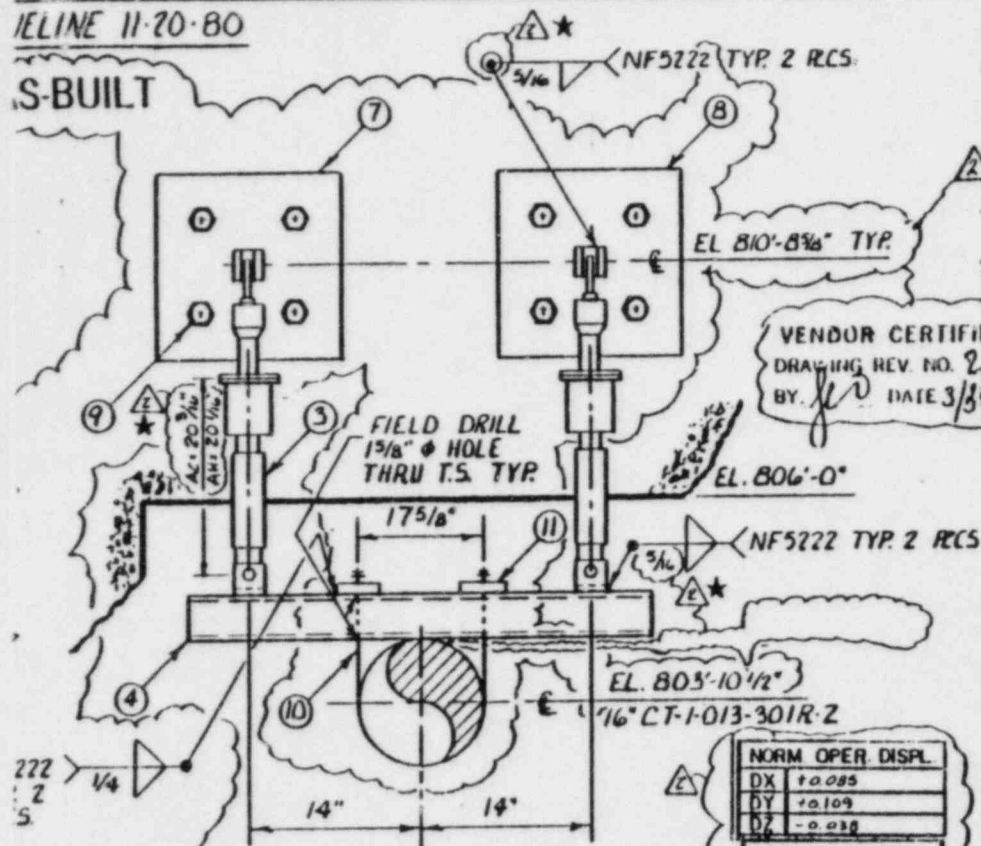
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CONTACT JMWAVE/CONTROL FOR CURRENT
STATUS AND REMOVAL

FOR ENGINEERING
OFFICE USE ONLY

FOR OFFICE AND

THE ONLY


S-BUILT



OTES:

Locking devices for high strength bolts are not required per DCA 7607

★ CHANGE NOT MADE
BY CLIC

BRIL Iso. CT-1-SB-008/R.1 
I.P.D. Iso. CT-1-SB-8 REV. 9
Data Point 256/PROB. #AB-1-32/R.O
Pipe Mat'l. SA-358-CL1 TP304
Insul. Bldg. SB

T.O.# 4802



THIRD PARTY INSPECTION
CODE CLASS: ASME III-2

ITEM NO.	MATERIALS & OPERATIONS	QUAN.	SHIP.	PAS	L	CSS	PRIM.	SEC.	AISC.
3	SM-10 BA SNUBBER (C-C-5-T)	2							
4	1.5" 3/4" x 4" x 4" 2-10" LG. A500GRB	1							
5	1" C.S. R PER DETAIL A SA36 OR SA515GR65	1							
6	1" C.S. R PER DETAIL B SA36 OR SA515GR65	1							
7	1 1/2" Ø x 12" SUPER MULTI KWIK BOLT	8							
10	1 1/2" Ø ROD B-16 3/4" 11-5 1/2"	1							
11	DEVELOPED (LNG. H. 4'-11") SA36	2							
	5/8" C.S. R 4" x 4" W/ 1 1/4" Ø HOLE @ CENTER								
	SA36								

REV	DATE	OWN	CHK	APP	DESCRIPTION
1	7/2/80	JTN	WJ	(Signature)	ISSUED FOR CONST. - REF. ITT, H-1 - BASE PLATE ONLY
2	11/20/80	WJ	WJ	(Signature)	ISSUED FOR CONST. REF FIELD MODIFIED HANGER SKETCH & REF ITT H-2 & DELETED NOTE 1-3 & ADDED INT 2 OF 4

MARK # C-1015-016-5378

PAINT: CARBO ZINC # 11

FOR MATERIALS AND OPERATIONS SEE SKETCH NO. _____ SHEET OF _____

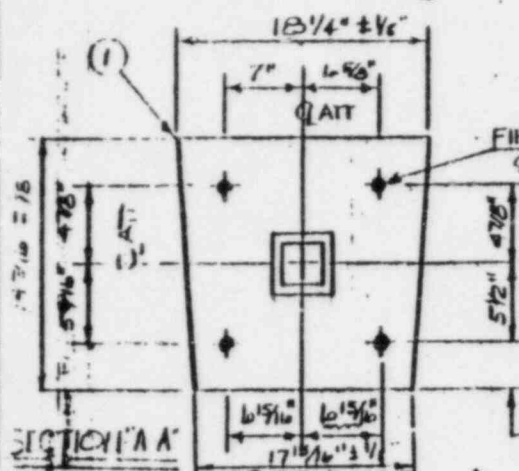
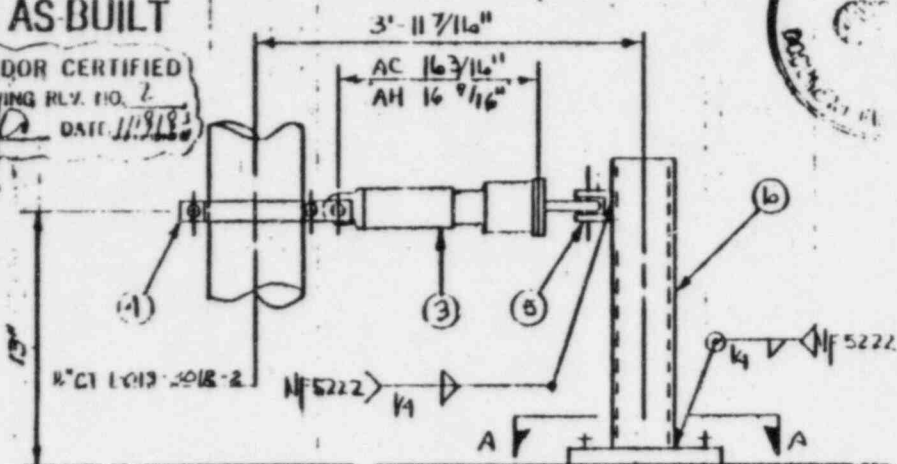
 BROWN & ROOT, INC. ENGINEERS & CONSTRUCTORS		CONDITIONS Fx Fy Fz Mx My Mz
REF. DRAWING NUMBERS REV. 9		DESIGN NORMAL   5577
DE: M1-0604 R.14 EL: 510602 R.12	ELECT: E1-060-01 HV.A.C: M1-0651 R2	EMERGENCY FAULTED

KEY	DATE	OWN	CNR	APP	DESCRIPTION	CUSTOMER
A	830	GL	BB	Q	REV'D. AS NT'D. REF: CMC 4/10/92.7 DKA 7607 NT 4 AS SURT VENDOR CERTIFICATION, REF: GTN G2726	Texas Utilities Service, Inc. ORDER OR CONT. NO. CP-0046 JOB NAME Comanche Peak 182 MARK NO. 77-013-NL-5328 SKETCH NO.

AS-BUILT

TRAINING RLY. NO. 2

DATE 11/2/88



FIELD DRILL (A) 1 K₁₀"
20 H₁₀LES

NOTES:

1) Locking devices for high strength bolts are not required per DCA 7607

CTR LINE OF ART
MAY VARY $\pm 1/4"$

PLAN VIEW @ E. 803' - 10' 711."

MOVEMENTS

X	10	-0.074
Y	13.574	-0.098
Z	10.114	-0.053

100M OPER DISP

DX	10.084
DY	12.42
DZ	11.55

ITEM
NO.

MATERIALS & OPERATIONS

QUANSHIP.

[illegible]

FOR OFFICE USE ONLY

INFORMATION COPY

MARK # CT-1-015-015-553R
PAINT: CARBO ZINC # 11

QUAN SHIP

FOR MATERIALS AND OPERATIONS SEE SKETCH NO.

SHEET OF

BROWN & ROOT, INC.
ENGINEERS & CONSTRUCTORS

REF. DRAWING NUMBERS

PIPE: 11-0604 R19 ELECT: E1-0601-01
STEEL: S1-0602 R12 H.V.A.C.: H1-0651-RI

CONDITIONS

Fa

Fy

F2

A1 x

My

DESIGN

NORMAL
UPSET

EMERGENCY

FAULTED

DESCRIPTION

355R FOR CONSTRUCTION
REF: IIT REV-1 THIS
WEED AS NOTED REORDER
SENT IITMC 355R AS BUILT
VENDOR CERTIFICATION, RE
GTN # 68726

CUSTOMER Texas Utilities Service, Inc.
ORDER OR CONT. NO. CP-0046

JOB NAME Cangocha Park In 2

MARK NO. 1-015-015-533P

SKETCH NO. _____

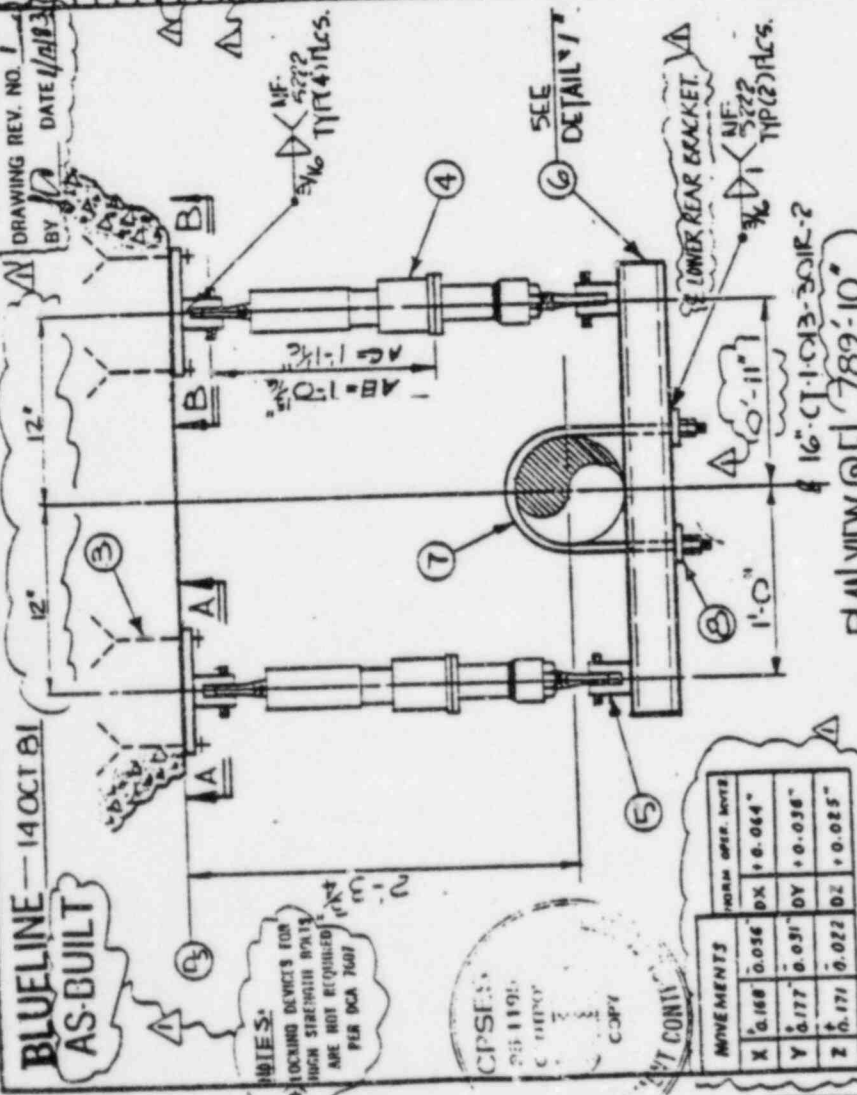
SKR 11.11.11

SHEET 4 OF 5 REV. 2

FOR OFFICE AND

BLUELINE—14 OCT 81
AS-BUILT

VENDOR CERTIFIED
DRAWING REV. NO. 1
BY *10* DATE *1/2/83*



Full view @ 789'-10"

SEE BRNL FOR
HANGER LOCATION

T.O. #4802

—FIELD DELL
1516 BOWLES
THRU T.S.

NETAL-1"

BRHL ISO CT-1-38-008-REV.1
S.P. ISO CT-1-38-0-REV.3
DATA POINT 1246/48-1-32/8.0
TYPE MATL SA-302 CLIPSCA
INCUIL ~ BUDG 2.0

THIRD PARTY INSPECTION
CODE CLASS: A/E/L/W

CODE CLASS: 0-10-10
FOR OFFICIAL USE ONLY

ITEM NO.	MATERIALS & OPERATIONS	QUAN	SHIP
1	1/2" C.S. R PER SECTION 1A (SA 325885)	1	
2	SA 325885	1	
3	1/2" C.S. R PER SECTION 1B (SA 325885)	1	
4	SA 325885	1	
5	1/2" C.S. R PER SECTION 1C (SA 325885)	1	
6	SA 325885	1	
7	1/2" C.S. R PER SECTION 1D (SA 325885)	1	
8	SA 325885	1	
9	1/2" C.S. R PER SECTION 1E (SA 325885)	1	
10	SA 325885	1	
11	1/2" C.S. R PER SECTION 1F (SA 325885)	1	
12	SA 325885	1	
13	1/2" C.S. R PER SECTION 1G (SA 325885)	1	
14	SA 325885	1	
15	1/2" C.S. R PER SECTION 1H (SA 325885)	1	
16	SA 325885	1	
17	1/2" C.S. R PER SECTION 1I (SA 325885)	1	
18	SA 325885	1	
19	1/2" C.S. R PER SECTION 1J (SA 325885)	1	
20	SA 325885	1	
21	1/2" C.S. R PER SECTION 1K (SA 325885)	1	
22	SA 325885	1	
23	1/2" C.S. R PER SECTION 1L (SA 325885)	1	
24	SA 325885	1	
25	1/2" C.S. R PER SECTION 1M (SA 325885)	1	
26	SA 325885	1	
27	1/2" C.S. R PER SECTION 1N (SA 325885)	1	
28	SA 325885	1	
29	1/2" C.S. R PER SECTION 1O (SA 325885)	1	
30	SA 325885	1	
31	1/2" C.S. R PER SECTION 1P (SA 325885)	1	
32	SA 325885	1	
33	1/2" C.S. R PER SECTION 1Q (SA 325885)	1	
34	SA 325885	1	
35	1/2" C.S. R PER SECTION 1R (SA 325885)	1	
36	SA 325885	1	
37	1/2" C.S. R PER SECTION 1S (SA 325885)	1	
38	SA 325885	1	
39	1/2" C.S. R PER SECTION 1T (SA 325885)	1	
40	SA 325885	1	
41	1/2" C.S. R PER SECTION 1U (SA 325885)	1	
42	SA 325885	1	
43	1/2" C.S. R PER SECTION 1V (SA 325885)	1	
44	SA 325885	1	
45	1/2" C.S. R PER SECTION 1W (SA 325885)	1	
46	SA 325885	1	
47	1/2" C.S. R PER SECTION 1X (SA 325885)	1	
48	SA 325885	1	
49	1/2" C.S. R PER SECTION 1Y (SA 325885)	1	
50	SA 325885	1	
51	1/2" C.S. R PER SECTION 1Z (SA 325885)	1	
52	SA 325885	1	
53	1/2" C.S. R PER SECTION 1AA (SA 325885)	1	
54	SA 325885	1	
55	1/2" C.S. R PER SECTION 1AB (SA 325885)	1	
56	SA 325885	1	
57	1/2" C.S. R PER SECTION 1AC (SA 325885)	1	
58	SA 325885	1	
59	1/2" C.S. R PER SECTION 1AD (SA 325885)	1	
60	SA 325885	1	
61	1/2" C.S. R PER SECTION 1AE (SA 325885)	1	
62	SA 325885	1	
63	1/2" C.S. R PER SECTION 1AF (SA 325885)	1	
64	SA 325885	1	
65	1/2" C.S. R PER SECTION 1AG (SA 325885)	1	
66	SA 325885	1	
67	1/2" C.S. R PER SECTION 1AH (SA 325885)	1	
68	SA 325885	1	
69	1/2" C.S. R PER SECTION 1AI (SA 325885)	1	
70	SA 325885	1	
71	1/2" C.S. R PER SECTION 1AJ (SA 325885)	1	
72	SA 325885	1	
73	1/2" C.S. R PER SECTION 1AK (SA 325885)	1	
74	SA 325885	1	
75	1/2" C.S. R PER SECTION 1AL (SA 325885)	1	
76	SA 325885	1	
77	1/2" C.S. R PER SECTION 1AM (SA 325885)	1	
78	SA 325885	1	
79	1/2" C.S. R PER SECTION 1AN (SA 325885)	1	
80	SA 325885	1	
81	1/2" C.S. R PER SECTION 1AO (SA 325885)	1	
82	SA 325885	1	
83	1/2" C.S. R PER SECTION 1AP (SA 325885)	1	
84	SA 325885	1	
85	1		

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THE UNIVERSITY OF CHICAGO

THIS DOCUMENT CONTAINS NEITHER RECOMMENDATIONS NOR
CONCLUSIONS OF THE NATIONAL BUREAU OF STANDARDS
AND IS NOT TO BE USED TO PROMOTE OR VETO ANY
SPECIFIC PRODUCT, TRADE NAME, OR COMPANY

[illegible]

SEE MATERIALS AND OPERATIONS SEE SKETCH NO.

[illegible]

DESCRIPTION

A	10/16	SW	ISSUED FOR CONST. REPLYING, I,
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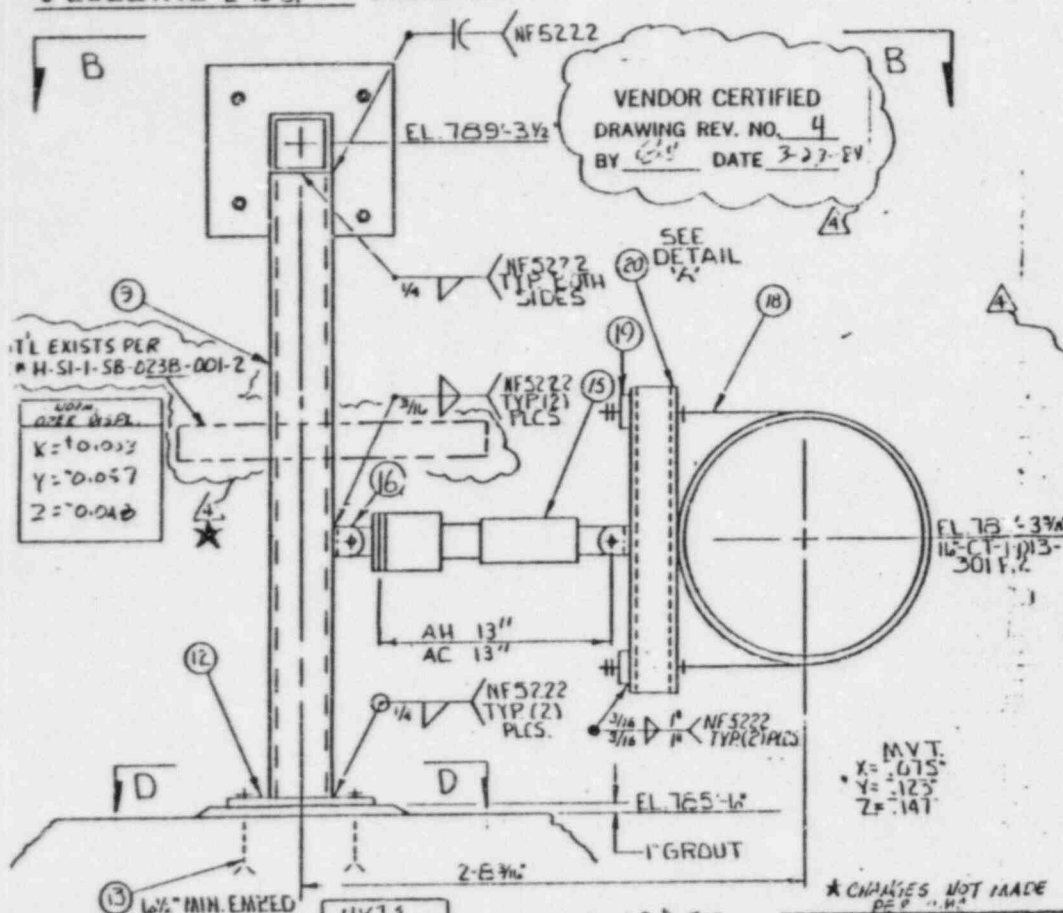
9-6870ND:JA 11111111

[illegible]

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BLUELINE 2-14-81

AS-BUILT

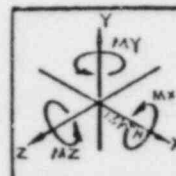


NOTE
Locking devices for high strength bolts are not required per NFCA 7607

COORDINATES	VALUES
X	10.003
Y	2.242
Z	10.043

BRHL Iso. CT-1-SB-002 R.1
B.M.P. Iso. CT-1-SP-5 REV. 5
Data Point 10-1-32 R.G.
Pipe Mat'l. SA-555-CL. TP304
Insul. Bldg. 55

SEE BRHL FOR HORIZ. LOCATION



THIRD PARTY INSPECTION YES ☐ NO ☐
CODE CLASS: ASME III-2

ITEM NO.	MATERIALS & OPERATIONS	QUAN	SHIP	PBS	L	CSS	PRIM	SEC	AISC
1	SEISMIC MECHANICAL SHOCK SUPPORTS FOR ASSEMBLY CONSISTING OF:								
2	SHOCK TEST TABLE	1							
3	1/4" DIA. HANGING SETTING	1							
4	1/4" DIA. SETTING	1							
5	PHS 1/2" U-BOLT (2-2 1/2")	1							
6	SEE DETAIL A	1							
7	TS 4"x4"x3/8" LG (A-500 GR. B)	1							
8	TS 4"x4"x3/8" LG (A-500 GR. B)	1							
9	SEE SECTION C-C (SA-312/SA-516)	1							
10	GR. 60	1							
11	SEE SECTION D-D (SA-312/SA-516)	1							
12	GR. 60	1							
13	3/4"x10" MULTI-KWIK BOLTS	4							
14	3/4"x5/8" MULTI-KWIK BOLTS	4							
15	3/16" I-50 SHIMMER	1							
16	ARA-03 REIN. HARK	2							
17	PHS-160 U-BOLT 8-14"	1							
18	RWP-07 WASHER PL	2							
19	TS 3/8"x3/8"x3/4" PER DETAIL A	1							

REVISIONS: 1. 10-1-80 11. 10-1-80 12. 10-1-80 13. 10-1-80 14. 10-1-80 15. 10-1-80 16. 10-1-80 17. 10-1-80 18. 10-1-80 19. 10-1-80 20. 10-1-80

FOR OFFICE AND ENGINEERING USE ONLY

SEISMIC ASSEMBLY SKETCH AND ENGINEERING BUNDLE AND TAG
MARK # CT-1-013-008-S22K

Apply Carbo Zinc #11 to above mat'l, except threads which shall be treated with a rust preventative

FOR MATERIALS AND OPERATIONS SEE SKETCH NO. SHEET OF

CONDITIONS	Fx	Fy	Fz	Mx	My	Mz
DESIGN						
NORMAL & UPSET	2503					
EMERGENCY	2753					
FAULTED						

REV	DATE	OWN	CHK	APP	DESCRIPTION
1	11-24-80	B	C	H	ISSUE FOR CONST.
2	12-21-80	JTR	M	PH	REVISED HANGING SKETCH, HANGING, ETC.
3	1-14-81	LN	P	PH	REVISED HANGING SKETCH, HANGING, ETC.

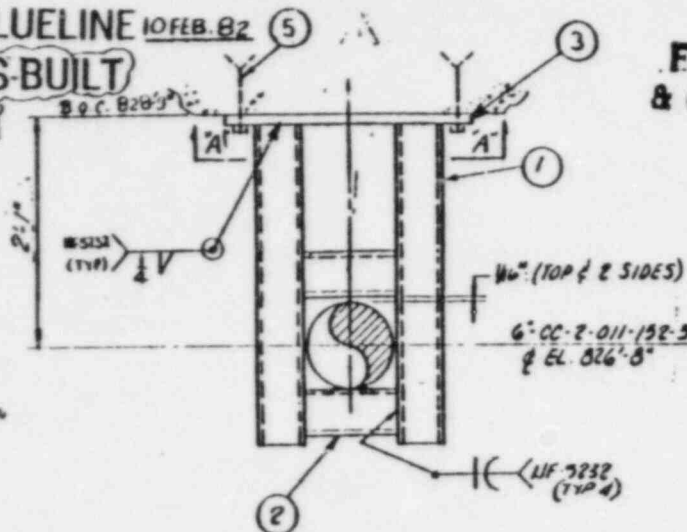
CUSTOMER: TEXAS UTILITIES SERVICE, INC.
ORDER OR CONT. NO. C.P.0046
JOB NAME: COMANCHI PEAK 142
MARK NO. CT-1-013-003-S22K
SKETCH NO.
SHEET 1 OF 2 REV. 4

FOR OFFICE AND

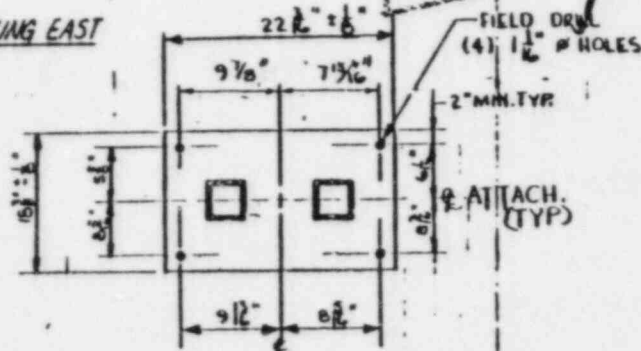
PROCESSED BY: [signature]

BLUELINE 10 FEB. 82
AS-BUILT

FOR ENGINEERING
& OFFICE USE ONLY



ELEVATION LOOKING EAST



SECTION A-A

Q OF ATTACH. MAY VARY ± 1/4"

MVTS
1000L
Z-00

VENDOR CERTIFIED
DRAWING REV. NO. 2
BY BH DATE 12/18/82

NOTE:
Locking devices for
high strength bolts
are not required
per DCA 7607

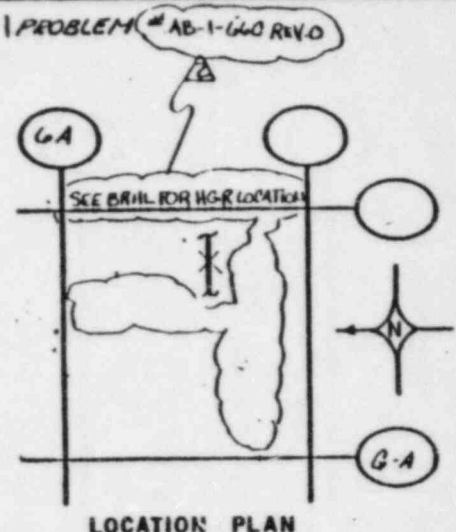
TO # 21101

ITEM NO.	QTY REQ'D	MATERIAL DESCRIPTION	PAS	CS	PRIM	SEC	AISC
1	2	3X3X1/4X2'-7 1/4" TUBE 1500 GR.B.		X	X	X	
2	2	3X3X1/4X 6' TUBE 1500 GR.B.		X	X	X	
3	1	1/2" CSIF SEE SECTION AA 5A36/SAS15GR15	X				
4	4	1" X 9" MULTI-KWIK CONCRETE ANCHORS				X	
5	4	1" X 9" MULTI-KWIK CONCRETE ANCHORS MIN EMB'D				X	

REV	DESCRIPTION	DATE	DWN	CHKD	APPVD
1	AS-BUILT WALL FOR VIBRATION ISOLATION	2-2-82	Z	Z	Z

ASME CODE EDITION: 1974
ADDENDA: WINTER
DESIGN SPEC: MS-46A

RE CERTIFICATION



LOCATION PLAN

DATA PT	SUPPORT	LOADS (LBS)	PIPE	REF	BRW. ISO	REV	MECHANICAL	REV	ELECTRICAL	REV	DESCRIPTION	DATE	DWN	CHKD	APPVD
2075	DESIGN	135	1/2"	CC-2-AB-004	1	1/2"	1/2"	12	1/2"	3	1/2"	1/2"	1/2"	1/2"	1/2"
VERT	135	135	1/2"	FAB. ISO	2	1/2"	1/2"	3	1/2"	6	1/2"	1/2"	1/2"	1/2"	1/2"
N-S	135	135	1/2"	CC-2-AB-004	2	1/2"	1/2"	3	1/2"	6	1/2"	1/2"	1/2"	1/2"	1/2"
E-W	135	135	1/2"												



Brown & Root, Inc.
ENGINEERS AND ARCHITECTS
HOUSTON, TEXAS

CLIENT: T.U.S.I.
PLANT: COMANCHE PEAK
JOB NO. 2323

SUPPORT NO. CC-2-011-721-A132
SHEET 1 OF 1 REV. 12

FOR OFFICE AND

ENGINEERING USE ONLY

BLUELINE
AS-BUILT

11-30-81

FOR ENGINEERING
& OFFICE USE ONLY

MIN. EMBED
5 1/4"

1/2" ALL AROUND

EL. 835'-0"
CC-211-152-3

VENDOR CERTIFIED
DRAWING REV. NO. 2
BY BH DATE 12/7/82

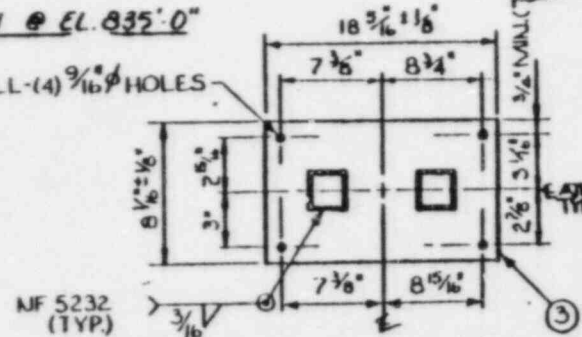
MVTS.
Y 0.006
D.017

NOTE:

(1) LOCKING DEVICES FOR
HIGH STRENGTH BOLTS
ARE NOT REQUIRED
PER DCA 7607

PLAN @ EL. 835'-0"

FIELD DRILL (4) 9/16" HOLES



CTR LINE OF ATTACHMENT MAY VARY ± 1/4 INCH

SECTION 'A-A'

(PROBLEM # AD-166C)

ID # 21101

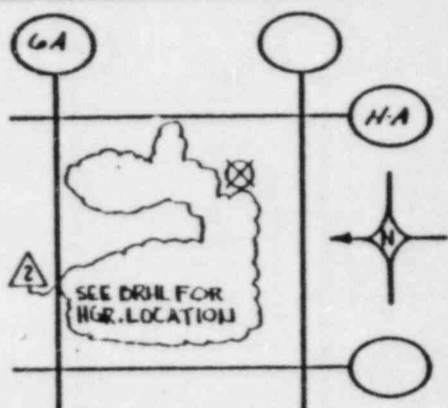


ITEM NO.	QTY REQ'D	MATERIAL	DESCRIPTION	PBS	W	SEC	ASC
1	2	3X3X1/4X 20K TUBE	A500 GR.B.	X	X	X	X
2	2	3X3X1/4X 6W TUBE	A500 GR.B.	X	X	X	X
3	1	1/2" C38 PER SECT. A-A	SAS/13ASIS GR. C5	X	X	X	X
4	4	1/2" X 7" MULTI-RING CONCRETE	ANCHORS	X	X	X	X

REV	DESCRIPTION	DATE	DWN	CHKD	APPVD
1	VENDOR CERTIFICATION REF. QTL # 59740				

ASME CODE EDITION: 1974
ADDENDA: WINTER
DESIGN SPEC: MS-46A

P.E. CERTIFICATION



LOCATION PLAN

DATA PT	SUPPORT	LOADS	LRG	PIPE	REF.	DRG.	REV.	MECHANICAL	REV.	ELECTRICAL	REV.	REV.	DESCRIPTION	DATE	DWN	CHKD.	APPVD.
2000	DESIGN	REVIEW	REVIEW	REVIEW	CC-2-AB-031	REV.	0	MI-702	0	EL-701-02	3	2	Rev. As Bldg, Rev. DCA Note (M. 1) As Bldg	12/7/82	CRH	J	RF
VERI.	1	1	1	1	FAB. 150	REV.	0	STRUCTURAL	3	HVAC	1	0	Rev'd As Mt'd, R.E. F.H.S.	11-30-81			
M-B	1	1	1	1	CC-2-AB-031	REV.	0	8-718	3	MI-753	6	0	I.F.C.	12-27-79			
E-W	1	1	1	1													

NOTE	AUTHORIZED NUCL. INSP. YES <input checked="" type="checkbox"/> NO <input type="checkbox"/>	ASME CODE CLASS 5
------	--	-------------------

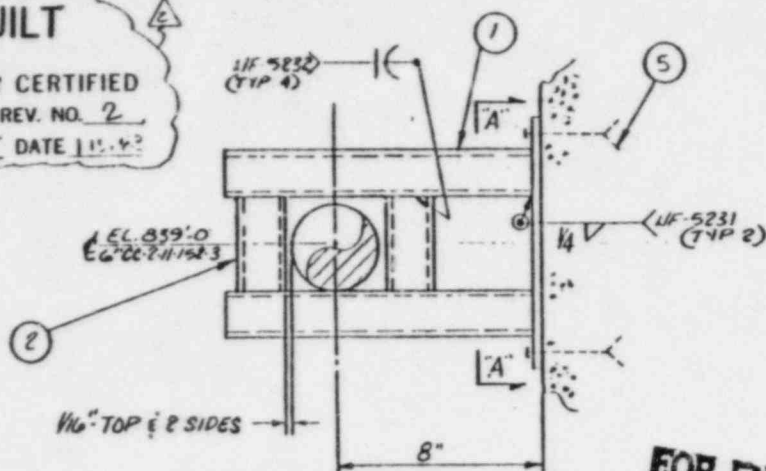
CPSES	Brown & Root, Inc.	CLIENT: T.U.S.L.	SUPPORT NO. CC-2-011-720-A-13R
55-1195	HOUSTON, TEXAS	PLANT: COMANCHE PEAK	SHEET 1 OF 1 REV. 2
		JOB NO. 2323	

FOR OFFICE AND

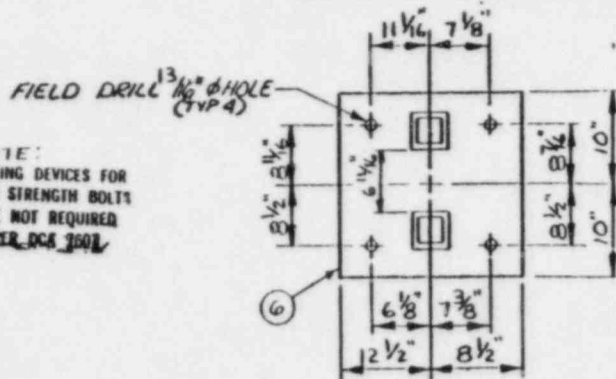
ENGINEERING USE ONLY

AS-BUILT

VENDOR CERTIFIED
DRAWING REV. NO. 2
BY: WLF DATE 11.1.79



ELEVATION LOOKING NORTH



SECTION "A-A"

NOTE:
LOCKING DEVICES FOR
HIGH STRENGTH BOLTS
ARE NOT REQUIRED
PER DCA 3502

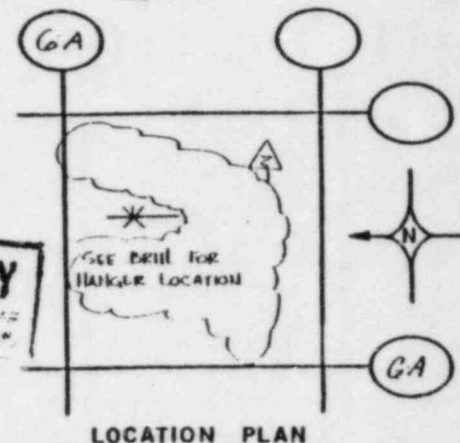
**FOR ENGINEERING
& OFFICE USE ONLY**

ITEM NO.	QTY REQ'D	MATERIAL	DESCRIPTION	PBS	CS	GR	SEC	AS
1	2	3X3X1/4X11.25" TUBE	A500 GR.B.					
2	2	3X3X1/4X10.625" TUBE	A500 GR.B.					
3	1	1/4" SA-36	SEE SECTION "A-A"	X				
4	4	3/4" X 8"	MULTI-KWIK CONCRETE					
5	4	3/4" X 7"	MULTI-KWIK CONC. ANCHOR					
6	1	C.S.R. 3/4" X 20" X 21"	SECT. A-A (SA 36/SA-515 GR 65)	X				

REV	DESCRIPTION	DATE	DWN.	CHKD.	APPVD.
A	VENDOR CERTIFICATION, REF. C.P.P. 8122	1/5/83	GLL	Q	CBD

PROBLEM * AB-1-66C R.O.

ASME CODE EDITION: 1974
ADDENDA: WINTER
DESIGN SPEC: MS-46A



LOCATION PLAN

T.O. 21100

DATA PT	SUPPORT	LOADS (LBS)	PIPE INCHES
208	DESIGN	LEVEL	10"
VERT			
N-S			
E-W			

REF DWGS	BRHL ISO.	REV	MECHANICAL	REV	ELECTRICAL	REV	DESCRIPTION	DATE	DWN.	CHKD.	APPVD.
	CC-2 AB-031	0	MICROZ	0	E10102	0	REV AS BUILT, REF DCA 1607 (SEE N.E.1); WEHS.	6/11/81	DMH		MDL
	FAB. ISO.	REV	STRUCTURAL	REV	H.V.A.C	REV	RECEIVED, CIRC 32932, AS-BUILT				
	CC-2 A2-031	0	SUTB	3	M10155	6	0 LFC.	12-20-79	C.A.T.		M/P



Brown & Root, Inc
ENGINEERS AND ARCHITECTS
HOUSTON, TEXAS

CLIENT T.U.C.L.
PLANT COMMUNIC PEAK
JOB NO. 2323

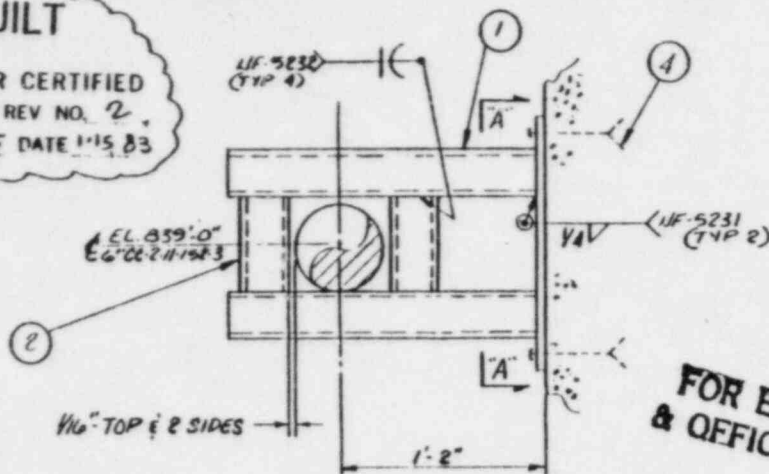
SUPPORT NO. CC-2 011 718 A53R
SHEET 1 OF 1 REV. 2

FOR OFFICE AND

ENGINEERING DEPT 12/24/77

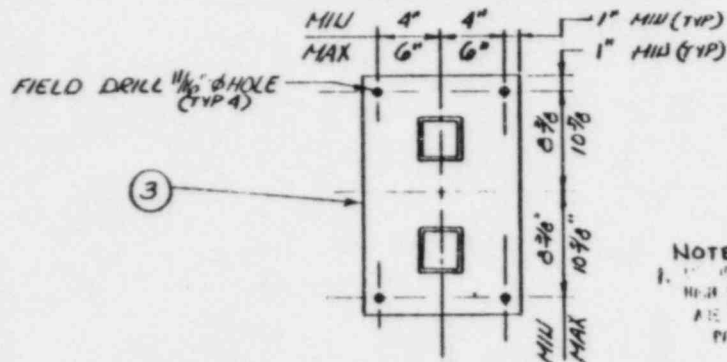
AS-BUILT

VENDOR CERTIFIED
DRAWING REV NO. 2
BY DATE 1-15-83



FOR ENGINEERING
& OFFICE USE ONLY

ELEVATION LOOKING NORTH



SECTION "A-A"

NOTE:
1. ALL DIMENSIONS FOR
HOLE SPACING SHALL
BE NOTED PER
PER 100, 100



ITEM NO.	QTY REQD	MATERIAL DESCRIPTION	PBS	J	CS	PM	SEC	AISC
1	2	3X3X1/4X1'-8 1/4" TUBE A500 GR.B.						
2	2	3X3X1/4X6 1/2" TUBE A500 GR.B.						
3	1	FL 3/8" SA-36 SEE SECTION "A-A"						
4	4	3/8" X 6" MULTI-EMK CONCRETE ANCHORS						

REV	DESCRIPTION	DATE	OWN.	CHKD.	APPVD.
1	VENDOR CERTIFICATION, REF. GTN 59790	1/15/83	GL	Q	CEB

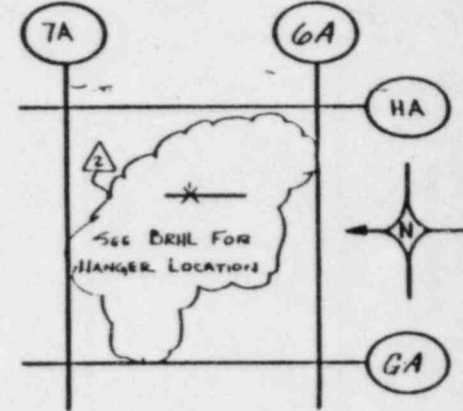
APPLY 1 IF COAT OF CARBON ZINC FIT TO ABOVE LIST EXCEPT THREADS WHICH SHALL BE TREATED WITH A RUST PREVENTATIVE.

PROBLEM # AB-1-66C

ASME CODE EDITION: 1974
ADDENDA: WINTER
DESIGN SPEC: MS-46A

P.E. CERTIFICATION

INFORMATION COPY
THIS DOCUMENT IS FOR INFORMATION ONLY.
CONTACT THE PROJECT ENGINEER FOR ANY
CHANGES OR REVISIONS.



LOCATION PLAN

T.O. 21100

DATA PT	SUPPORT	LOADS (LBS)	PIPE	REF.	BRHL	ISO	REV	MECHANICAL	REV	ELECTRICAL	REV	REV	DESCRIPTION	DATE	OWN	CHKD.	APPVD.
2086	DESIGN	ANALYSIS	LEVEL	LIMITS	CC-2-AB-031	0	0	M-0702	0	E-0702	0	1	REV AS NOTED, REF. DCA 1607 (SEE WT 1); WMS	5/21/81	DMH	JW	CEB
VERT.	—	—	—	—	FAB. ISO.	0	0	STRUCTURAL	0	H.V.A.C.	0	0	FIELD MFG; CHC-32942; AS-BUILT	12-20-79	C.A.T.	W	M.H.
N-S	—	—	—	—	CC-2-AB-031	0	0	SQTAB	0	M-0755	0	0	L.F.C.				
E-W	—	—	—	—													

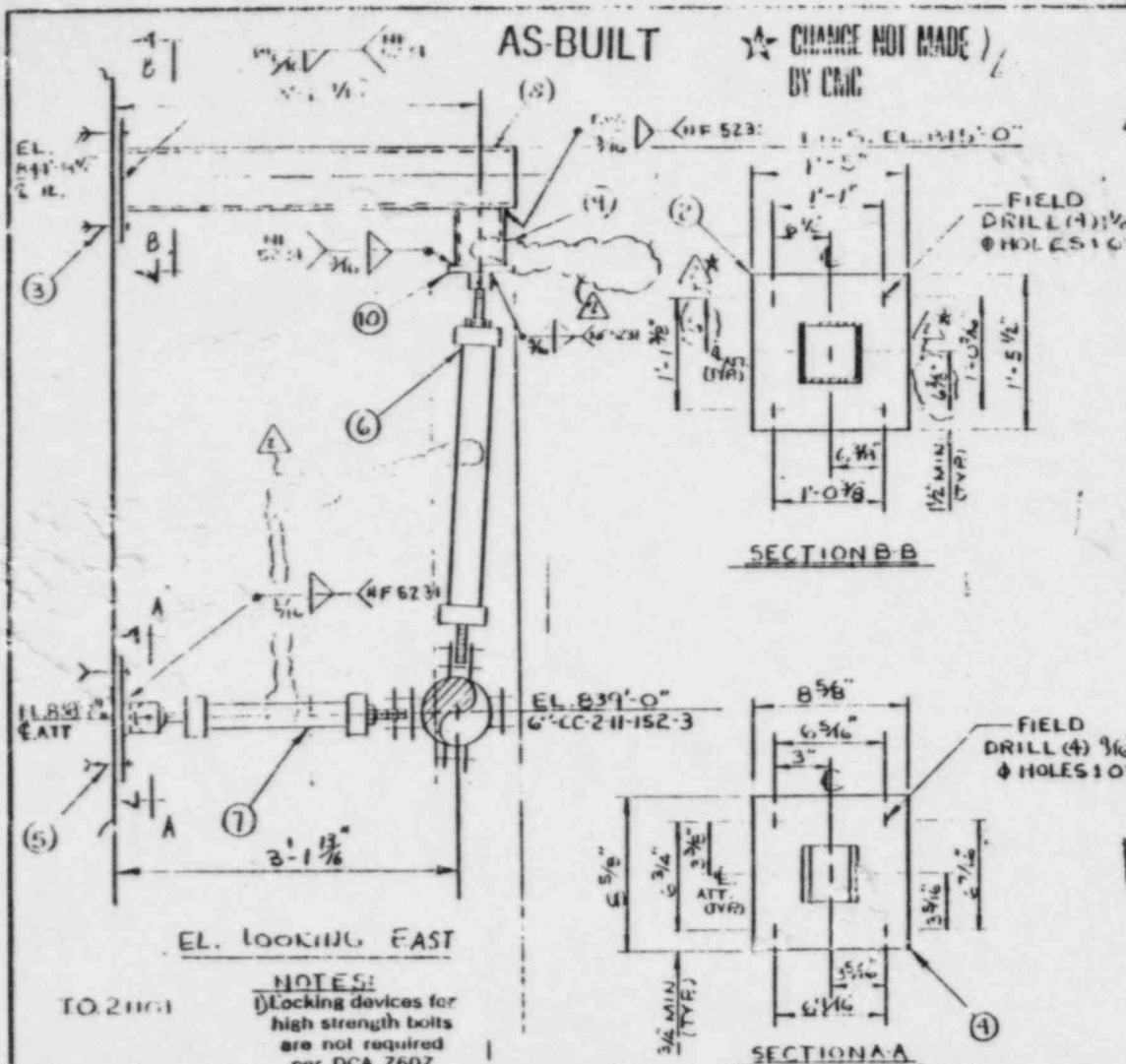
NOTE 1. N, S, UP — S, W, DN	AUTHORIZED NUCL. INSP. YES <input checked="" type="checkbox"/> NO <input type="checkbox"/>	ASME CODE CLASS <u>3</u>	CPSES 35-1193	Brown & Root, Inc. ENGINEERS AND CONSTRUCTORS HOUSTON, TEXAS	CLIENT <u>T.U.S.I.</u> PLANT <u>COMANCHE PEAK</u> JOB NO. <u>2323</u>	SUPPORT NO. <u>CC-2-011-717-A53R</u> SHEET <u>1</u> OF <u>1</u> REV. <u>2</u>
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FOR OFFICE AND






ITEM NO.	QTY	MATERIAL DESCRIPTION	QTY	QTY	QTY
1	1	1" x 1/2" x 1/2" MULTI KWIK CONCRETE ANCHOR			
2	1	1" x 1/2" x 1/2" MULTI KWIK CONCRETE ANCHOR	X		X
3	4	1" x 1/2" x 1/2" MULTI KWIK CONCRETE ANCHOR			X
4	1	1" x 1/2" x 1/2" MULTI KWIK CONCRETE ANCHOR	X		X
5	4	1/2" x 3/4" MULTI KWIK CONCRETE ANCHOR			X
6	1	SRS-08-PC			X
7	1	SRS-08-PC			X
8	1	1" x 1/2" x 1/2" MULTI KWIK CONCRETE ANCHOR	X		
9	1	1" x 1/2" x 1/2" MULTI KWIK CONCRETE ANCHOR			
10	1	1" x 1/2" x 1/2" MULTI KWIK CONCRETE ANCHOR			

VENDOR CERTIFIED
DRAWING REV. NO. 2
BY WWS DATE 7/21/83

PROB: AB-166-REV. 1
ASME CODE EDITION: 1974
ADDENDA: WINTER,
DESIGN SPEC: 11.5 - 46A



REF INVS	STRESS ISO	REF	MECHANICAL
	M2-3231-72	C	111-0702
	BRHL ISO	REF	STRUCTURAL
	CC-2-AB-031	O	S P/B

REV	ELECTRICAL	REV	REV	DESCRIPTION	DATE	BY	CHKD	APPV
8	E1-0702	8	0	IFC	11-30-74			11/30/74
REV	II V A C	REV		REVIS NOTED, RFL QAC 7607, 33422	11/30/74			11/30/74
3	MI-0755	6	End	EDCA 7607, SEE NZ/LAS-BUILT				

CPGB

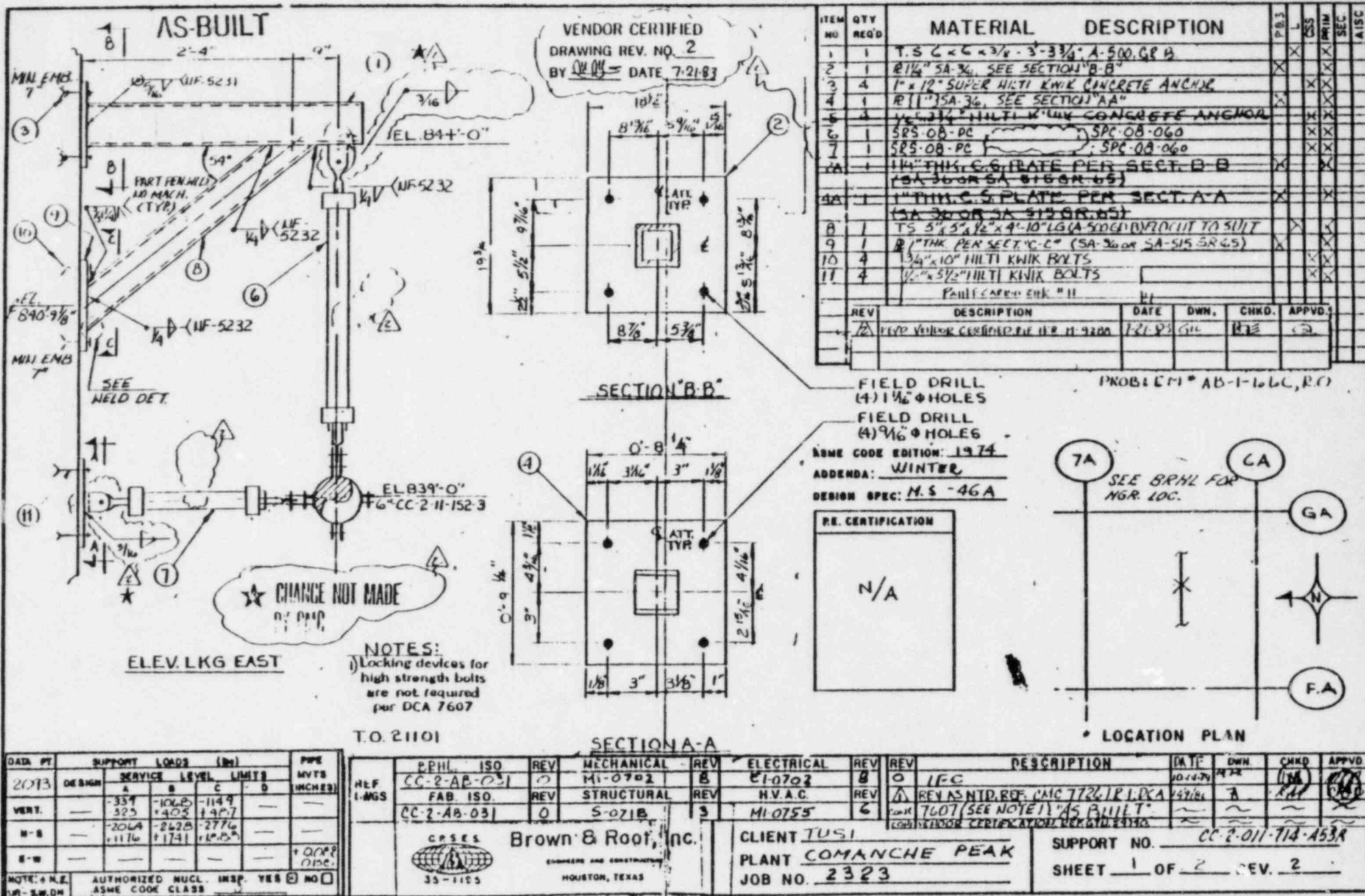


BB-1188

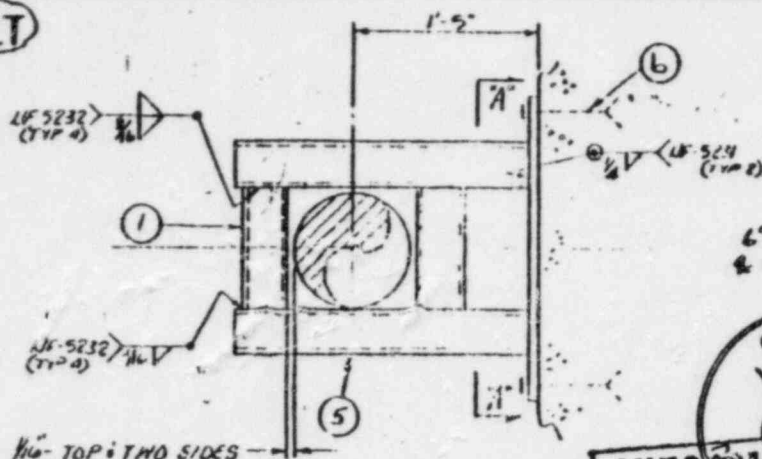
CLIENT T.U.S.I.
PLANT COMANCHE PEAK
JOB NO. 2323

SUPPORT NO. CC-2-011-115-A53R
SHEET 1 OF 1 REV. 2

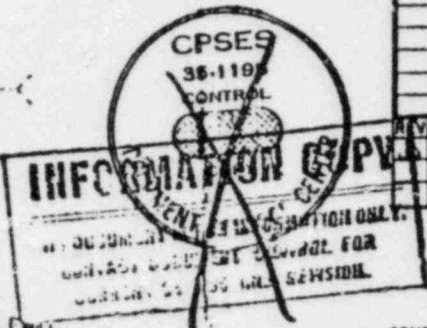
FOR OFFICE AND
ENGINEERING USE ONLY



AS-BUILT



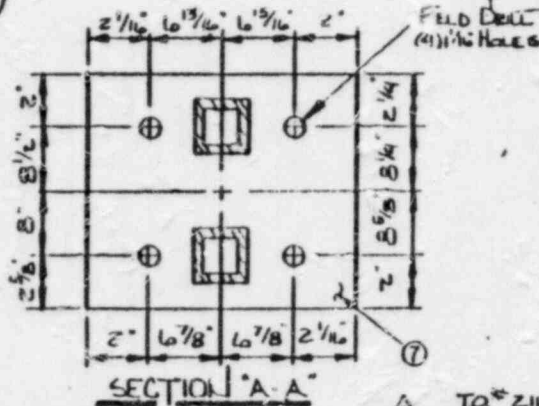
6" CC-2-11-152-3
& EL. 839'-0"



ITEM NO.	QTY REQ'D	MATERIAL DESCRIPTION	POS	UNIT	REMARKS	DATE	CHKD	APP'D
1	2	XXXX 4X0'-6 3/4" WISE AS-BUILT						
2	2	XXXX 4X0'-6 3/4" WISE AS-BUILT						
3	1	XXXX 4X0'-6 3/4" WISE AS-BUILT						
4	1	XXXX 4X0'-6 3/4" WISE AS-BUILT						
5	2	1/4" X 4" X 4" TUBE STEEL 1-11" LG (ASCOGRB)	X	X				
6	9	1" X 12" SUPER HILTS CONCRETE ANCHORS	X	X				
7	1	1X17 1/2" X 21 1/8" CS PLATE (SASISGELS-ASBL)	X	X				

VENDOR CERTIFIED
DRAWING REV. NO. 2
BY BH DATE 12-2-82

ELEVATION LOOKING NORTH

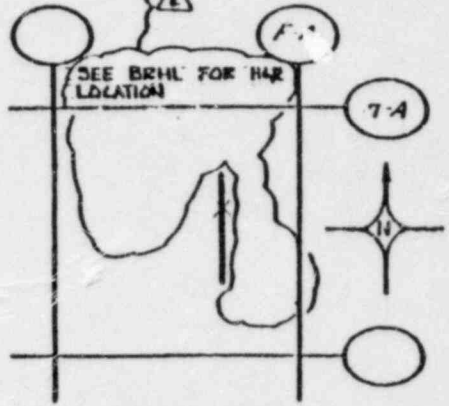


FOR ENGINEERING
& OFFICE USE ONLY

ASME CODE EDITION: 1974
ADDENDA: WINTER
DESIGN SPEC: M-1-16A

RE. CERTIFICATION

PROBLEM = AB-1-66C R-O



LOCATION PLAN

DATA	DESIGN	SUPPORT LOADS (LBS)	PIPE NUTS	REF	BRHL	SO	REV	MECHANICAL	REV	ELECTRICAL	REV	REV	DESCRIPTION	DATE	CHKD	APP'D
191	DESIGN	579	1/4"	CC-2-AB-32	1	11/11/82	1	MECHANICAL	1	11/11/82	1	1	REV AS-BUILT REF 12/2/82 (AS BUILT)	12-2-82	RMD	WIP
191	DESIGN	579	1/4"	CC-2-AB-32	1	11/11/82	1	STRUCTURAL	1	11/11/82	1	1	REV AS-BUILT REF 12/2/82 (AS BUILT)	12-2-82	RMD	WIP
191	DESIGN	579	1/4"	CC-2-AB-32	1	11/11/82	1	MECHANICAL	1	11/11/82	1	1	REV AS-BUILT REF 12/2/82 (AS BUILT)	12-2-82	RMD	WIP



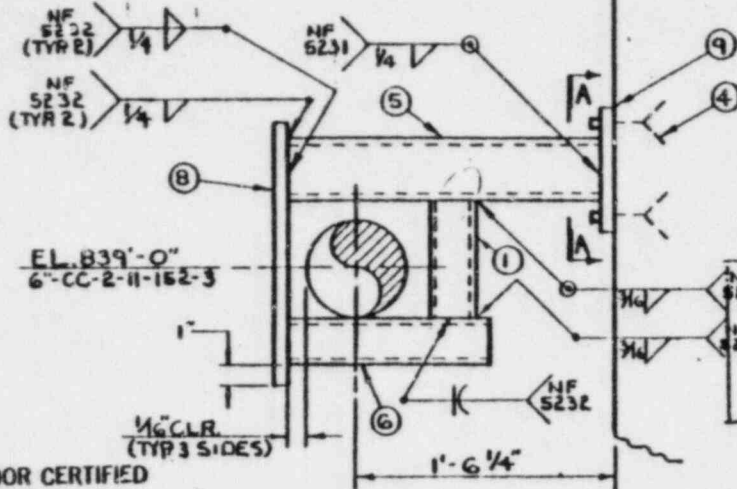
Brown & Root, Inc.
ENGINEERS AND CONSTRUCTORS
HOUSTON, TEXAS

CLIENT: T.V.S.I.
PLANT: COMBUSTION PEAK
JOB NO. 2323

SUPPORT NO. CC-2-01 74-A53R
SHEET 1 OF 1 REV. 2

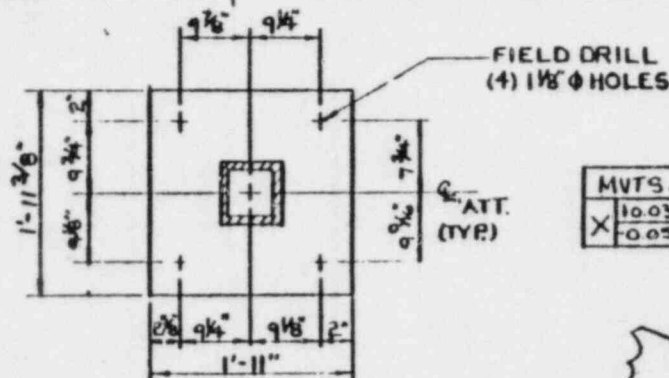
FOR OFFICE AND

AS BUILT



VENDOR CERTIFIED
DRAWING REV. NO. 1
BY: BH DATE 12/6/02

ELEV. VIEW LKG. NORTH



NOTES:

Locking devices for high strength bolts are not required per DCA 7607

T.O. 21100

PROBLEM 18-1-66C/50

SEE BRIL FOR HGR LOCATION


ASME CODE EDITION: 1974
ADDENDA: WINTER
DESIGN SPEC: MS-46A

RE. CERTIFICATION

CPSE9
32-1123
601123

LOCATION PLAN

[illegible]

DATA PT	SUPPORT	LOADS	(LBS)	PIPE	REV	MECHANICAL	REV	ELECTRICAL	REV	REV	DESCRIPTION	DATE	DWN.	CHKD.	APPRD.
2099	DESIGN	REVIEW	REVIEW	UNIT	REV	CC-2-AB-032	2	MI-0702	8	EL-0711	REV	15/10/79	IP	J	AC
VERT		510	1225	1445		FAB 180	REV	STRUCTURAL	REV	H.V.A.C	REV	SEE NIP VENDOR CERTIFICATION CHIT ABOVE			
H-W						CCR-AB-03E	1	S-0121	4	MI-0756	5	12/19/79	C.A.T.	(M)	ALM
NOTE	AUTHORIZED NUCL. INSP. YES <input checked="" type="checkbox"/> NO <input type="checkbox"/>				 Brown & Root, Inc ENGINEERING AND CONSTRUCTION HOUSTON, TEXAS 35-193				CLIENT <u>T.U.S.I.</u> PLANT <u>COMANCHE PEAK</u> JOB NO. <u>2383</u>				SUPPORT NO. <u>CC-2-011-712-A228</u> SHEET <u>1</u> OF <u>1</u> REV. <u>1</u>		

FOR OFFICE AND

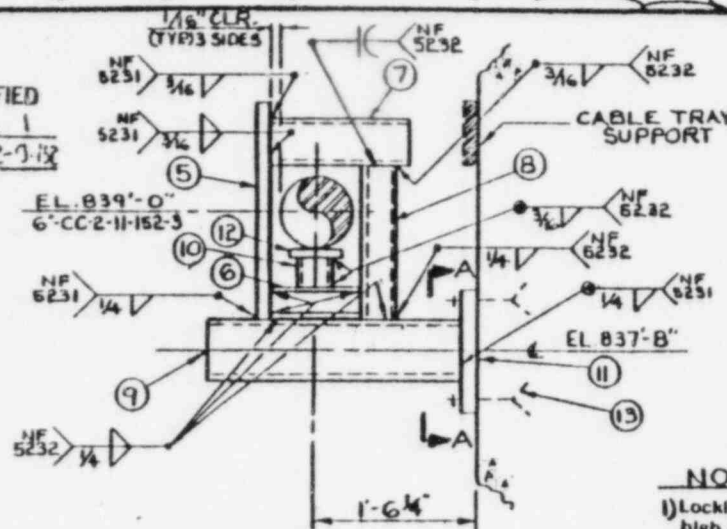
FRANCIS AND JANE

FOR OFFICE AND

FIELD USE ONLY

AS BUILT

VENDOR CERTIFIED
DRAWING REV. NO. 1
BY PJ DATE 12-7-82

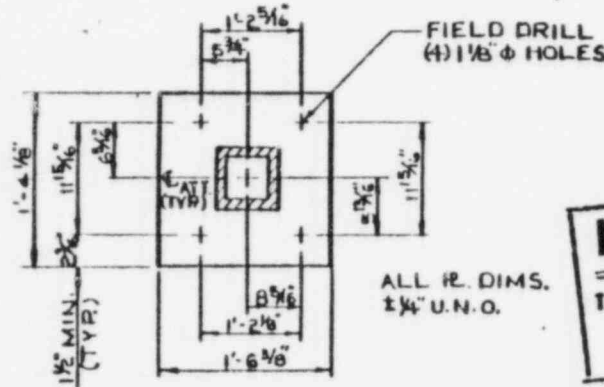


ELEV. LKG NORTH

NOTES

1) Locking devices for high strength bolts are not required per DCA 7607

T.O. 21100



SECTION A-A

ALL R. DIMS.
± 1/4\" U.O.



ITEM NO	QTY REQ'D	MATERIAL DESCRIPTION	PBS	J	MIN	SEC	ABC
5	1	1" x 4 1/2" x 1/8" W.B. C.S.P. (SA-36 OR SA-515, GR. 65)	X				
6	1	W.G.Y. 12 x 0'-6 3/4" L.G. (SA-36)	X				
7	1	T.S. 1/4" x 4" x 4" x 0'-11" L.G. (A-500, GR. B)	X				
8	1	T.S. 1/4" x 4" x 4" x 1'-4 1/8" L.G. (A-500, GR. B)	X				
9	1	T.S. 1/4" x 6" x 6" x 2'-0 1/2" L.G. (A-500, GR. B)	X				
10	1	T.S. 1/4" x 3" x 3" x 0'-2 1/2" L.G. (A-500, GR. B)	X				
11	1	1" THK. C.S.P. / 6ECT. A.A. (SA-36 OR SA-515, GR. 65)	X				
12	1	1" x 4" x 4" L.G. C.S.P. (SA-36 OR SA-515, GR. 65)	X				
13	4	1" x 9" L.G. HILTI KWIK CONCRETE ANCHORS	X				

APPLY ONE COAT OF CARBO-ZINC #11 TO ABOVE MTL EXCEPT THREADS WHICH SHALL BE TREATED WITH A RUST PREVENTATIVE.

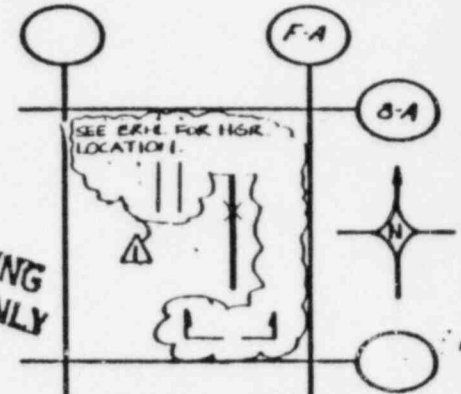
REV	DESCRIPTION	DATE	BY	CHKD	APPD
1	VENDOR CERT. REF. GTN # 52792				

PROB. # AB-1-66C, R-0

ASME CODE EDITION: 1974
APPENDIX: WINTER
DESIGN SPEC: HS-46A

P.E. CERTIFICATION

FOR ENGINEERING
& OFFICE USE ONLY



LOCATION PLAN

DATA PT	SUPPORT	LOADS (LBS)	PIPE	REV	MECHANICAL	REV	ELECTRICAL	REV	REV	DESCRIPTION	DATE	DWR	CHKD	APPD
R101	DESIGN	11,850	11,850	1	MI-0702	3	EL-0711	0	1	REV AS NOTED, REF. CMC	11/11/82	FWY	G	CRD
VERT		5,850	5,850											
H-B		5,850	5,850											
E-W		5,850	5,850											
NOTE	AUTHORIZED NUCL. IMP. YES <input type="checkbox"/> NO <input checked="" type="checkbox"/>													
	ASME CODE CLASS 3													



Brown & Root, Inc.
HOUSTON, TEXAS

CLIENT: T.U.S.I.
PLANT: COMANCHE PEAK
JOB NO.: ESP3

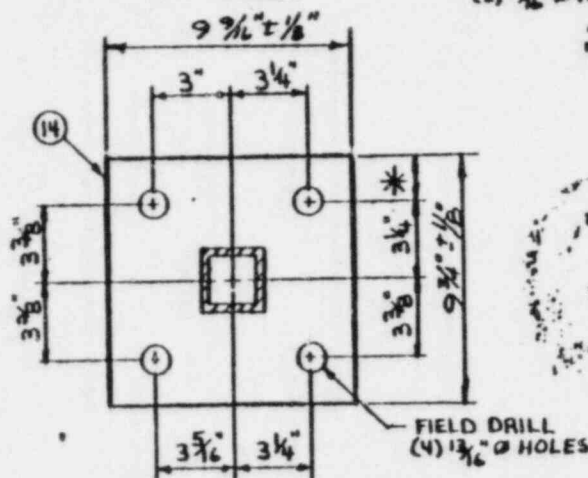
SUPPORT NO.: CC-2-01711-A31R
SHEET 1 OF 1 REV. 1

VENDOR CERTIFIED
DRAWING REV. NO. 2
BY PH DATE 1-1-83

EL. 853'-3"
C'CC-2-11-182-3

EL. 852'-6"

FOR ENGINEERING
& OFFICE USE ONLY



SECTION A-A

FIELD DRILL
(2) 1 1/2" Ø HOLES

SECTION B-B

NOTE:
1. LOCKING DEVICES FOR
HIGH STRENGTH BOLTS
306 NOT REQUIRED

THIS DOCUMENT IS FOR
CONTACT. EIGHT
CURRENT. SIX

ITEM NO.	QTY REQ'D	MATERIAL DESCRIPTION	REV	DESCRIPTION	DATE	OWN	CHKD	APPVD
1	1	ANCHOR BOLT						
2	1	2" x 4" x 1/2" ANGLE 51-36 SEE DETAIL A						
3	1	2" x 4" x 1/2" ANGLE 51-36						
4	1	1/2" x 4" x 1/2" ANGLE 51-36						
5	1	1/2" x 4" x 1/2" ANGLE 51-36						
6	1	1/2" x 4" x 1/2" ANGLE 51-36						
7	1	1/2" x 4" x 1/2" ANGLE 51-36						
8	1	1/2" x 4" x 1/2" ANGLE 51-36						
9	1	1/2" x 4" x 1/2" ANGLE 51-36						
10	1	1/2" x 4" x 1/2" ANGLE 51-36						
11	1	T.S. 4x4 x 1/2" x 10" (A 500 GR.B) TRIM AS REQ'D						
12	1	T.S. 3x3 x 1/2" x 10" (A 500 GR.B)						
13	1	C.S. 1/2" x 4" x 10" (SA-36/SA-515 GR.65)						
14	1	C.S. 1/2" x 4" x 10" (SA-36/SA-515 GR.65)						
15	4	3/4" x 7" HILTI KWIK CONC. ANCHOR						
16	1	PUH-060 U-BOLT						

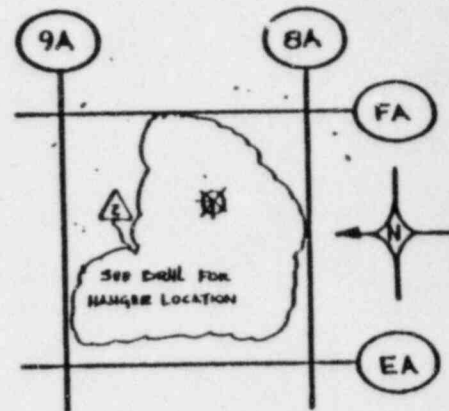
APPLY ONE COAT OF CADDO ZINC #11 TO ABOVE WARE EXCEPT THREADS WHICH SHALL BE TREATED WITH A RUST PREVENTATIVE.

MOBLEM #10-1-CCC R/O

ASME CODE EDITION: 1974
ADDENDA: WINTER
DESIGN SPEC: HS-46A

RE. CERTIFICATION

N/A



LOCATION PLAN

DATA PT	SUPPORT	LOADS (LBS)	PIPE	REF. DMS	BRHL	ISO	REV	MECHANICAL	REV	ELECTRICAL	REV	REV	DESCRIPTION	DATE	OWN	CHKD	APPVD
2107	DESIGN	10000	10000	10000	CC-2-10-032	1	1	H-0701	6	21-0710-01	7	0	IFC	11/20/75	PH	PH	PH
VERT.					FAB. ISO	REV		STRUCTURAL	REV	HV.A.C.	REV	1	REV AS HED. REF. CHC 42611R.2.4	6/11/81	PH	PH	PH
H-W					CC-2-10-032	1	1	S-0728	2	H-0710	4	1	REV AS HED. REF. CHC 42611R.2.4				
E-W													REV AS HED. REF. CHC 42611R.2.4				
NOTE													REV AS HED. REF. CHC 42611R.2.4				
ASME CODE CLASS													REV AS HED. REF. CHC 42611R.2.4				

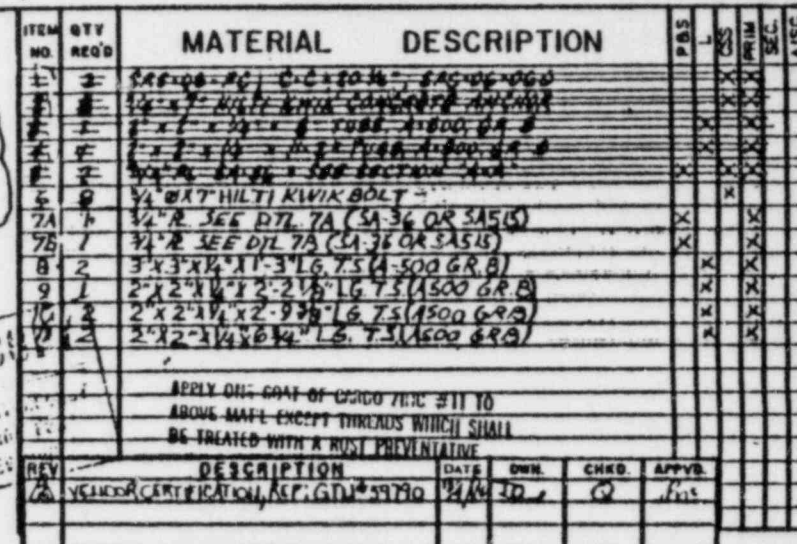


Brown & Root, Inc.
HOUSTON, TEXAS

CLIENT: T.U.S.I.
PLANT: COMANCHE PEAK
JOB NO. 2323

SUPPORT NO. CC-2-011-708-A63A
SHEET 1 OF 1 REV. 2

FOR OFFICE AND
ENGINEERING USE ONLY

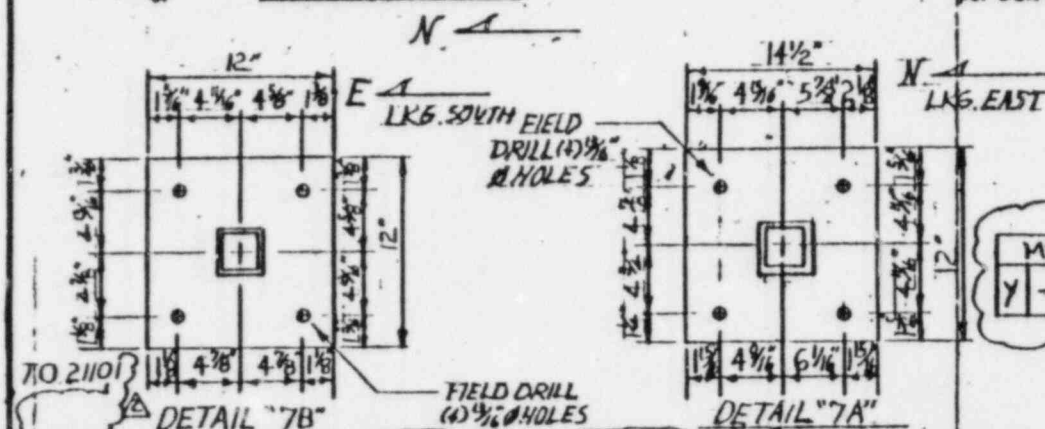
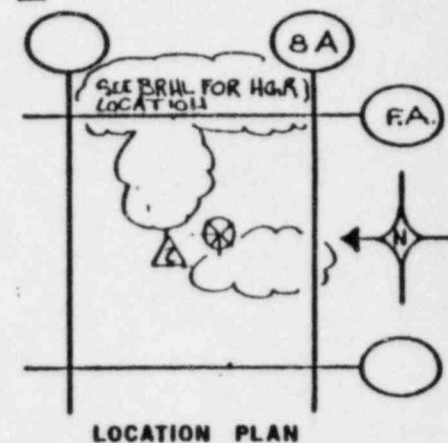


ASMS CODE EDITION: 1974
ADDENDA: WINTER
DESIGN SPEC: MS-46A

RE. CERTIFICATION

N/A


FOR ENGINEERING
& OFFICE USE ONLY



DATA PT	SUPPORT	LOADS	(L&R)	PIPE
2108	DESIGN	SEVERE	LEVEL	HYD
VERT.				INCHES
M-S				
E-W				
NOTE	AUTHORIZED NUCL. INSP. YES <input checked="" type="checkbox"/> NO <input type="checkbox"/>			
10, S, UP	ASME CODE CLASS 3			
7, 8, DN				

PRIL 150	REV	MECHANICAL
CC-2-AB-032	0	M-0701
FAB 150	1	STRUCTURAL
CC-2-AB-032	1	S-0728

CPSEE



35-1198

Brown & Root, Inc
ENGINEERS AND ARCHITECTS
HOUSTON, TEXAS

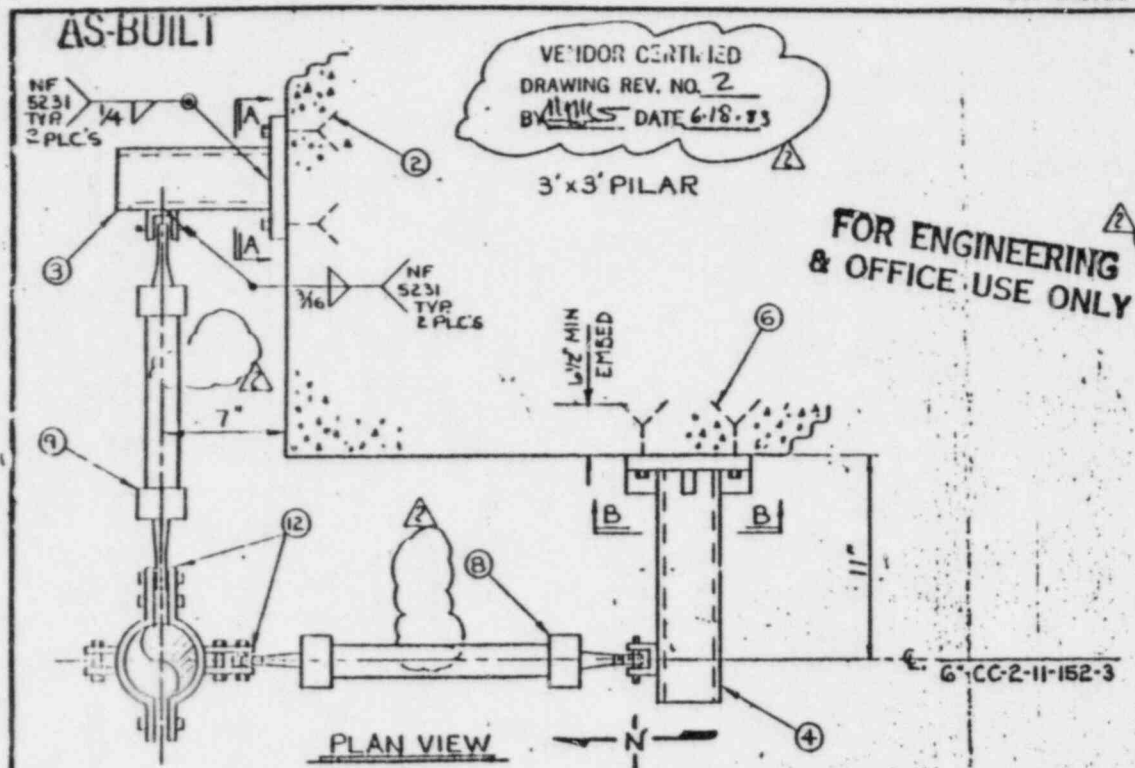
REV	ELECTRICAL	REV	REV	0
G	EL-0710-01	17	Q	IFC 1...
REV	HVA'S	REV	A	REV DAS NOT DEF
2	M1-0758	4	1041	IFC NOT ELCT

CLIENT T.U.S.I.
 PLANT COMANCHE PEAK
 JOB NO. 2323

DESCRIPTION	DWIR	CHER	APPROV
11/5/79 CNC 33446 R1110005 20725 1/1 WEARS (AS BUILT) 1/1	W. L. KAN S. W. L. 1/1	1/1 1/1 1/1	1/1 1/1 1/1
SUPPORT NO. <u>CC-8-011-707-AG3A</u>			
SHEET <u>1</u> OF <u>1</u> REV. <u>2</u>			

**FOR OFFICE AND
EMERGENCY USE ONLY**

FOR OFFICE AND
ENGINEERING USE ONLY



FOR ENGINEERING
& OFFICE USE ONLY

ITEM NO.	QTY REQ'D	MATERIAL DESCRIPTION	PAS	US	MS
2	4	3/4"x7" HILTI KWIK CONCRETE ANCHORS		X	
3	1	T.S. 1/4"x3"x3" X 8 1/4" LG. (A-500-740, GR. B)	X		
4	1	T.S. 1/4"x3"x3"x1'-2 1/4" LG. (A-500-740, GR. B)	X		
6	4	5/8"x8 1/2" HILTI KWIK CONCRETE ANCHORS		X	
7	4	1/2"x4"x3 1/4" LG. STIFFENER PLATE (SA-36 OR SA-515 GR. 65)	X		
8	1	SRF-OB-RO SWAY STRUT		X	
9	1	SRF-OB-RO SWAY STRUT		X	
10	1	3/4" C.S. PLATE PER SECT. A-A (SA-36 OR SA-515 GR. 65)	X		
11	1	3/4" C.S. PLATE PER SECT. B-B (SA-36 OR SA-515 GR. 65)	X		
12	2	SPC-OB-060 C.S. PIPE CLAMP (SA-36 OR SA-515 GR. 65)	X		
		PAINT: CARBO ZINC II			

NOTES:

Locking devices for high strength bolts are not required per DCA 7607

T.O. 21101

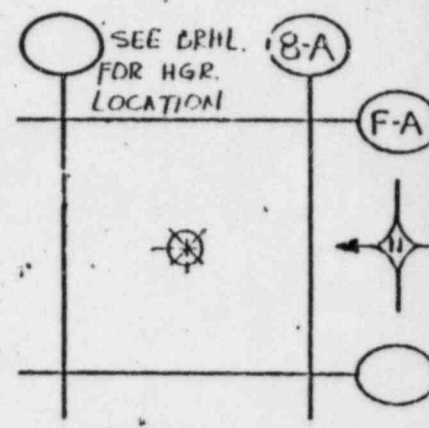


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DO NOT REPRODUCE OR DISTRIBUTE FOR OTHERS.

ASME CODE EDITION: 1974
ADDENDA: WINTER
DESIGN SPEC: MS-46A

P.E. CERTIFICATION
N/A

PROJ# AB-166CRD



LOCATION PLAN

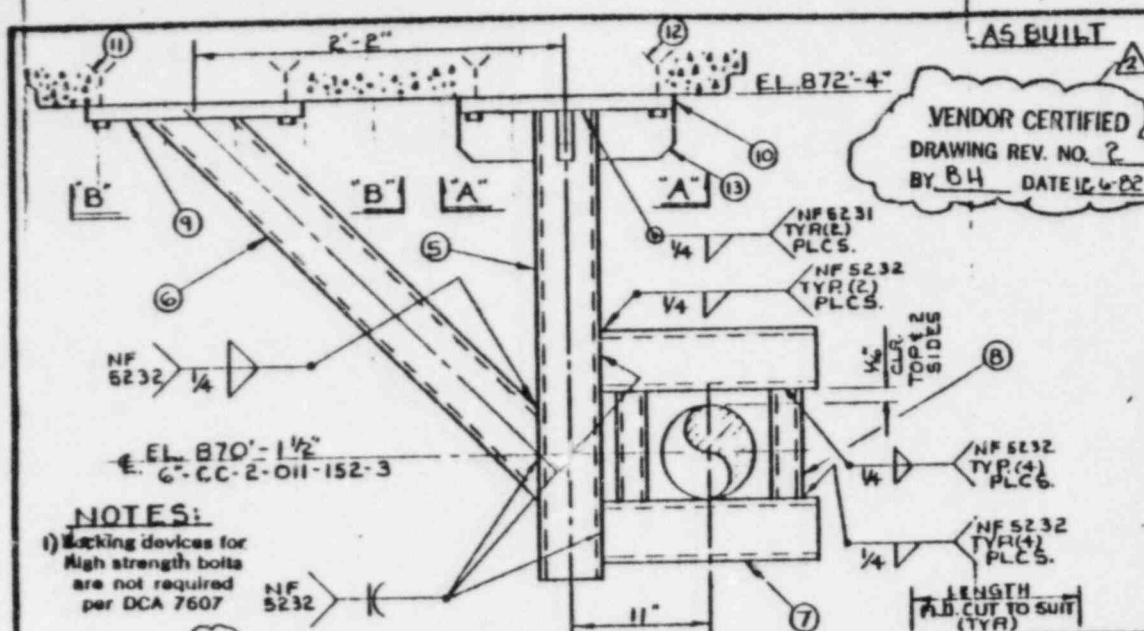
DATA PT	SUPPORT LOADS (LBS)	PIPE NUTS INCHES	REF. DWGS	BRHL ISO.	REV	MECHANICAL	REV	ELECTRICAL	REV	REV	DESCRIPTION	DATE	DWN.	CHKD.	APPD.
2109	DESIGN	3/4" X 1/2"		CC-2-AB-032	1	MI-0701	6	EI-0710-01	7	0	IFC	11-30-74			
VERT.				FAB. ISO.	REV	STRUCTURAL	REV	H.V.A.C.	REV			12-1-74			
N-S				CC-2-AB-032	2	S-0728	2	MI-0758	4			12-1-74			
E-W															
NOTE: AUTHORIZED NUCL. INSP. YES <input checked="" type="checkbox"/> NO <input type="checkbox"/>															
ASME CODE CLASS 3															



Brown & Root, Inc.
ENGINEERING AND CONSTRUCTION
HOUSTON, TEXAS

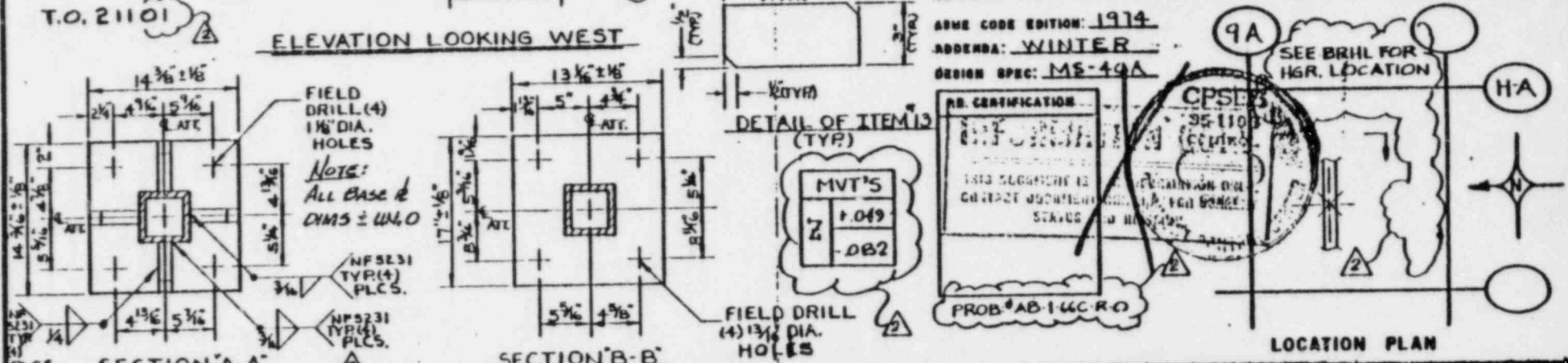
CLIENT: T.U.
PLANT: COMANCHE PEAK
JOB NO.: 2323

SUPPORT NO. CC-2-011-706-A65R
SHEET 1 OF 2 REV. 2



ITEM NO.	QTY REQD	MATERIAL DESCRIPTION	AS BUILT	REV	DATE	BY	CHKD	APPVD
5	1	T.S. 1/4" x 4" x 4" x 2'-9 1/2" LG. (A-500, GR.B)						
6	1	T.S. 1/4" x 4" x 4" x 3'-8" LG. (A-500, GR.B)						
7	2	T.S. 1/4" x 4" x 4" x 1'-2 1/2" LG. (A-500, GR.B)						
8	2	T.S. 1/4" x 2" x 2" x 0'-6 1/4" LG. (A-500, GR.B)						
9	1	3/4" THK. C.S. PLATE PER SECT. B-B (3A-515 GR. 65 OR SA-36)						
10	1	3/4" THK. C.S. PLATE PER SECT. A-A (3A-515 GR. 65 OR SA-36)						
11	4	3/4" x 10" LG. HILTI KWIK CONCRETE ANCHORS						
12	4	1" x 12" LG. HILTI KWIK CONCRETE ANCHORS						
13	4	1/2" THK. C.S. PLATE (SA-36 OR SA-515 GR. 65) x 0'-3" WIDE x LENGTH TO BE FURNISHED BY FIELD						

REV	DESCRIPTION	DATE	OWN	CHKD	APPVD
1	VENDOR CERTIFICATION, REG. NO. 39790	12/6/82	JH	JH	JH



DATA PT	SUPPORT	LOADS (LBS)	PIPE	REF. DIMS	STRESS ISO.	REV	MECHANICAL	REV	ELECTRICAL	REV
2122	DESIGN	462	80	112	M2-3231-3G	A	MI-0701	6	EI-0703	6
VERT.					(DRH) 180	REV	STRUCTURAL	REV	H.V.A.C.	REV
H-B					CC-2-AB-03E	1	S-0735	2	MI-0757	4
E-W										

NOTE	AUTHORIZED NUCL. INSP. YES <input checked="" type="checkbox"/> NO <input type="checkbox"/>
ASME CODE CLASS	3

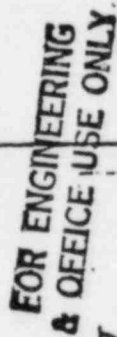
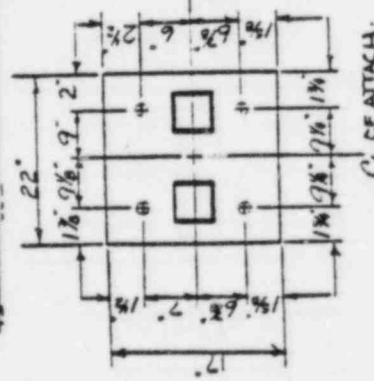
Brown & Root, Inc.	CLIENT T.U.S.I.
HOUSTON, TEXAS	PLANT COMANCHE PEAK
	JOB NO. 2323

SUPPORT NO. CC-2-11-701-A63R
SHEET 1 OF 1 REV. 2

FOR ENGINEERING
OFFICE USE ONLY

ENGINEERING USE ONLY

VENDOR CERTIFIED
DRAWING REV. NO. 2
BY: CH DATE 12-3-81

ELEVATION LOOKING EAST

NOTES:
1) LOCKING DEVICES FOR
HIGH STRENGTH BOLTS
ARE NOT REQUIRED
PER DQA 7607

T.O. 21100

ASME CODE EDITION: 1974
ADDENDA: WINTER
DESIGN SPEC: MS-46A

P.R. CERTIFICATION

--	--

SEE BILL FOR
IGP LOCATION

PROBLEM AB-1-66C-RO

LOCATION PLAN

DATA PT	SUPPORT	LOADS	(LBS)	PIPE
1124	STEEL	STEEL	STEEL	STEEL
VERT	STEEL	STEEL	STEEL	STEEL
H-Z	STEEL	STEEL	STEEL	STEEL


REF	ISQ	MECHANICAL	REV	ELECTRICAL	REV	DESCRIPTION	DATE	OWN	CHNG	APP
CC-2-AB-032	1	MI-0701	6	EI-0703	6	I.E.C.	9-28-79	MAN/KC	1	1
CC-2-AB-033	1	STRUCTURAL	REV	HV.A.C.	1	REVALS. NID. REF. CMC. 45420 R 2	4-10-56	MT		
CC-2-AB-033	1	5-0735	2	MI-0757	4	1. DLT. ENVS. 1-6. DLT. 07/68 (MNH) (A) 1	ONT			

Brown & Root, Inc.

ENGINEERING AND CONSTRUCTION

HOUSTON, TEXAS

CP 358



35-1135

SUPPORT NO. CC-2-11-700-A63A

SHEET 1 **OF** 1 **REV.** 2

CLIENT T.U.S.I.

PLANT COMANCHE PEAK

JOB NO. 2323

DATE 11/24

TIME 1:00

BY J.E.C.

FOR J.E.C.

NOTES

1. DLT. ENVS. 1-6. DLT. 07/68 (MNH) (A) 1

AUTHORIZED NUCL. ENSP. YES ☐ **NO** ☒

ASME CODE CLASS 3

DATE 11/24

TIME 1:00

BY J.E.C.

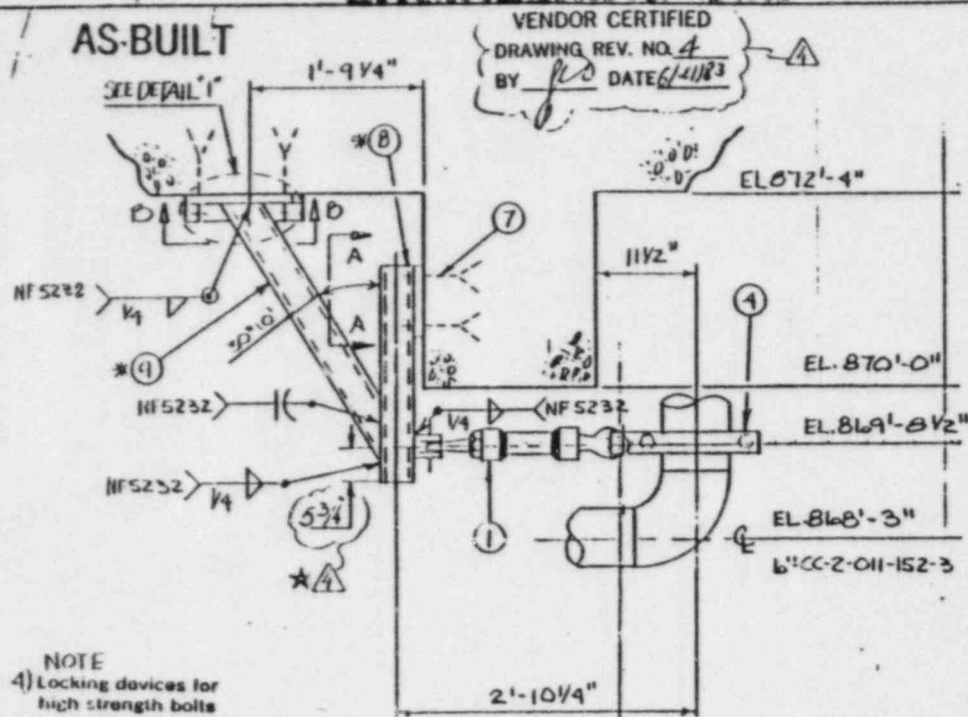
FOR J.E.C.

THE
LIBRARY
OF THE

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JOURNAL
OF
THE
ROYAL
ANTHROPOLOGICAL
INSTITUTE
OF GREAT
BRITAIN
AND IRELAND
PART I
1901

FOR OFFICE AND ENGINEERING USE ONLY

AS-BUILT



NOTE
4) Locking devices for
high strength bolts
are not required
per DCA 7607

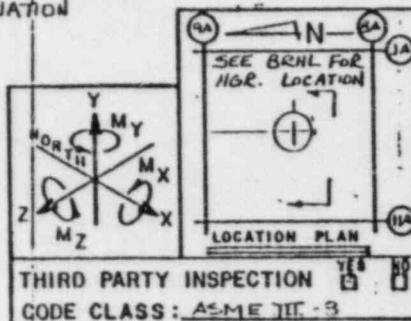
CHANGE NOT MADE
BY GRC

* FIELD TRIM TO SUIT

OBTUSE OR ACUTE
ANGLE WELD NOT
USED FOR ENGR.
EVALUATION

TO #21101

BRILL Iso. CC-2 AB-50 R-1
I.P.D. Iso. CC-2 AB-50-R-0
Data Point 212 TAB 10000
Pipe Mat'l. SA106GR.B
Insul. Y2 Bldg. A



VENDOR CERTIFIED
DRAWING REV. NO. 4
BY *[Signature]* DATE 6/11/83

ITEM NO.	MATERIALS & OPERATIONS	QUAN.	SHIP	P.S.	L	CSS	PRIM.	SEC.
1	DRS-10-RD SWAY STRUT C.C. = 1'-8 1/4"	1						
2	SPC-10-060 PIPE CLAMP SA36	1						
3	3/4" CS IF PER DETAIL A-A SA106GR.B	1						
4	3/4" CS IF PER DETAIL A-A SA106GR.B	1						
5	3/4" CS IF PER DETAIL A-A SA106GR.B	1						
6	3/4" CS IF PER DETAIL A-A SA106GR.B	1						
7	3/4" CS IF PER DETAIL A-A SA106GR.B	1						
8	3/4" CS IF PER DETAIL A-A SA106GR.B	1						
9	3/4" CS IF PER DETAIL A-A SA106GR.B	1						
10	3/4" CS IF PER DETAIL A-A SA106GR.B	1						
11	3/4" CS IF PER DETAIL A-A SA106GR.B	1						
12	3/4" CS IF PER DETAIL A-A SA106GR.B	1						

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& OFFICE USE ONLY

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AND MAINTENANCE
ONLY

REV	DATE	OWN	CHK	APP	DESCRIPTION
1	6/11/83	JW	PK	Q	ADDED SHIT 2 AS BUILT. VED FOR CERTIFICATION. SEE AT 21101 REV'D VENDOR CERTIFICATION REF AISC 21-BOLTS

MARK # CC-2-011-002-AL3R
PAINT: CARBO ZINC # 11

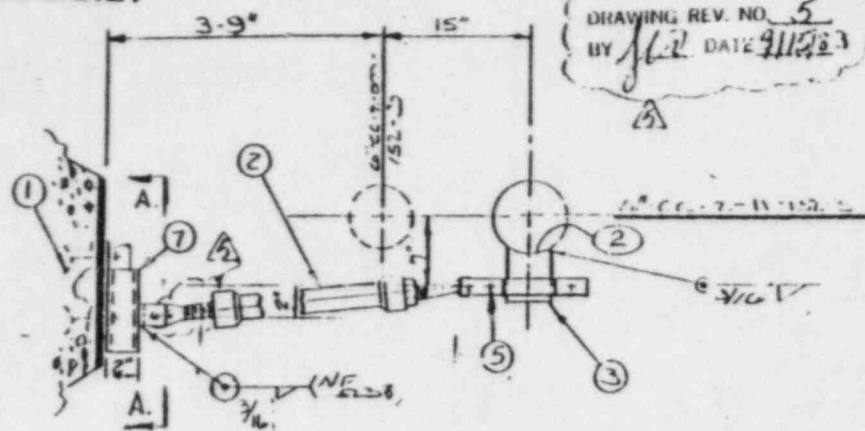
FOR MATERIALS AND OPERATIONS SEE SKETCH NO. SHEET OF

BROWN & ROOT, INC. ENGINEERS & CONSTRUCTORS		CONDITIONS	Fx	Fy	Fz	Mx	My	Mz
REF. DRAWING NUMBERS		DESIGN						
PIPE: MI-0701-R7 ELECT: EL0703-R5		NORMAL & UPSET			15372			
STEEL: S-0735-R2 HV.A.C: MI-0752-R4		EMERGENCY			2069			
		FAULTED			2287			

REV	DATE	OWN	CHK	APP	DESCRIPTION
1	6/11/83	JW	PK	Q	ISSUE FOR CONST. FW 1
2	6/11/83	ER	Q	Q	REV PER NPSI REV OA
3	6/11/83	ER	Q	Q	REV PER NPSI # 326
4	6/11/83	ER	Q	Q	REV PER NPSI # 326
5	6/11/83	ER	Q	Q	REV PER NPSI # 326

CUSTOMER Texas Utilities Service, Inc.
ORDER OR CONT. NO. CP-0046
JOB NAME Comanche Peak 1A 2
MARK NO. CC-2-011-002-AL3R
SKETCH NO.
SHEET 1 OF 2 REV 4

AS-BUILT

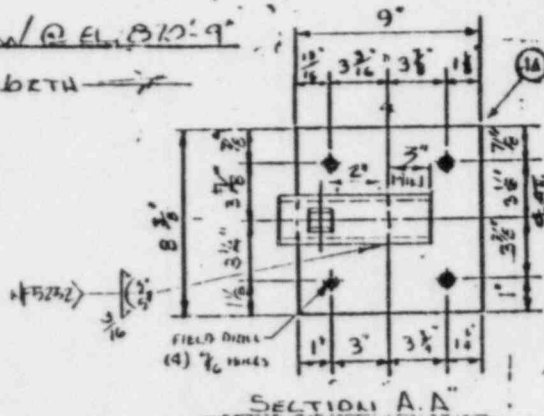


VENDOR CERTIFIED

DRAWING REV. NO. 5

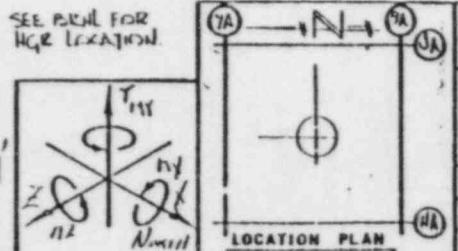
BY J.L. DATE 9/11/83

PLAN VIEW @ EL. 80'-9"



- NOTES:
- LOCKING DEVICES FOR HIGH STRENGTH BOLTS ARE NOT REQUIRED PER ISEA 7107

SEE BRN FOR HGR LOCATION



THIRD PARTY INSPECTION

CODE CLASS: ASME III

ITEM NO.	NO REQD	PART CALL-OUT	DESCRIPTION	MATERIAL	MIC. NO.	WT.	PBS	CSS	PRIN	REC	AISC
1	4	BRN 17-70	COIL ANCHOR								
2	1	BRN 17-70	SWAP STAP		67P	2.0		X			
3	1	1/2" X 40 X 3/4"	STANCHION	A106 GR				X	X		
4	1	1/2" X 40 X 3/4"	C-9 PLATE	A106 GR				X	X		
5	1	1/2" X 40 X 3/4"	PIPE CLAMP	A106 GR				X	X		
6	1	1/2" X 40 X 3/4"	ASME III PLATE					X	X		
7	1	1/2" X 40 X 3/4"	CS PLATE					X	X		
8	1	1/2" X 40 X 3/4"	PIPE STEEL	A106 GR				X	X		

SEISMIC ASSEMBLY SKETCH AND ENGINEERING BUNDLE AND TAG

MARK # CC-2-011-001-A63K

Apply Carbo-Zinc #11 to above mat 1 except th'ds which shall be treated with a rust preventative

NO MAT - BY GRINDING

REV	DATE	OWN	CNK	APP	DESCRIPTION
1	9/11/83	JL			ISSUE FOR CONIT
2	9/11/83	JL			REV FOR NIS/REV CA
3	9/11/83	JL			REV AS UPD REF: CFC-310LZ
4	9/11/83	JL			REV AS UPD REF: CFC-310LZ
5	9/11/83	JL			REV AS UPD REF: CFC-310LZ

APPROVED BY: CFC

DATE: 4-23-79

QUAN SHIP

FOR MATERIALS AND OPERATIONS SEE SKETCH NO.

SHEET OF

FOR OFFICE AND ENGINEERING USE ONLY

BRN ISO CC-2-AD-50 R.1
I.P.D. ISO CC-2-62-50 R.D
Data Point: 12/1/80 12/1/80
Pipe Mat'l: SA106 GR.B
Insul: 7/2 Bldr. A



Brown & Root, Inc.

REF. DRAWING NUMBERS

PIPE: 11-0701-1-1/2" ELECT: 11-0701-1-1/2"
STEEL: 5-0728-1/2" HV.A.C: 11-0701-1-1/2"

REV	DATE	OWN	CNK	APP	DESCRIPTION
1	6/1/83	JL			ISSUE FOR CONIT
2	6/1/83	JL			REV FOR NIS/REV CA
3	6/1/83	JL			REV AS UPD REF: CFC-310LZ
4	6/1/83	JL			REV AS UPD REF: CFC-310LZ
5	6/1/83	JL			REV AS UPD REF: CFC-310LZ

CONDITIONS	Fx	Fy	Fz	Mx	My	Mz
DESIGN						
NORMAL & UPSET	1386	474				
EMERGENCY	1386	474				
FAULTED						

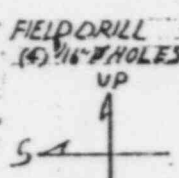
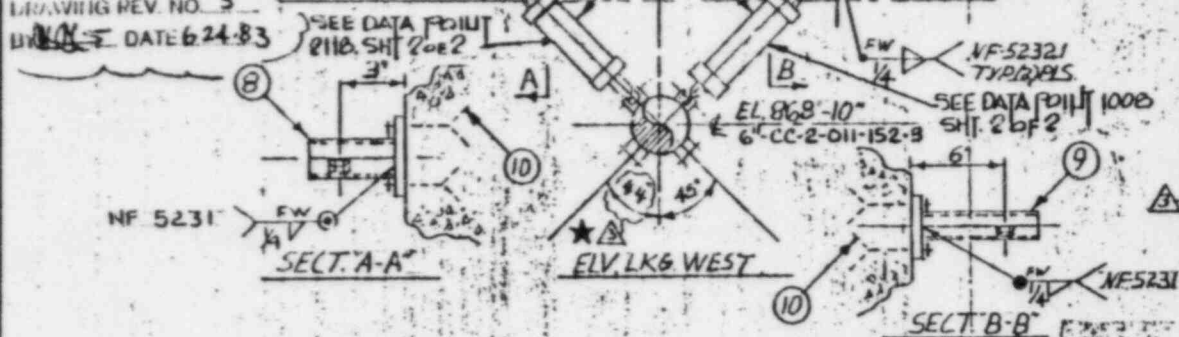
CUSTOMER: Foxess Utilities Service
ORDER OR CONT. NO. CP-0046
JOB NAME: Oconee Peak 2 & 2
MARK NO. CC-2-011-001-A63K
SKETCH NO.
SHEET 1 OF 1 REV. 1

AS-BUILT

VENDOR CERTIFIED

DRAWING REV. NO. 3

DATE 6-24-83



WALL R. FACING WEST

WALL R. FACING WEST

NOTE:
1) Locking devices for high strength bolts are not required per DCA 7807

★ CHANGE NOT MADE BY CMC

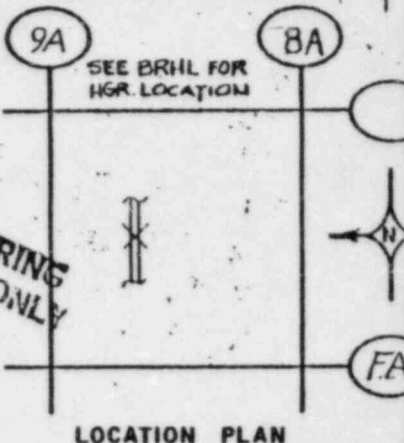
PROBLEM # AB-146C

REV	QTY	MATERIAL	DESCRIPTION	DATE	CHKD	APPROV
5	1	1/2" R.C.S. (SA-515 OR SA-36)				
6	1	1/2" R.C.S. (SA-515 OR SA-36)				
7	2	3/8" OB TYPE RC				
8	1	7/8" 1/4" x 1/2" LG. AS500-74A-GR.B				
9	1	7/8" 1/4" x 1/2" LG. AS500-74A-GR.B				
10	8	HILTI EWIK BOLTS 1/2" x 5 1/2"				

REV	DESCRIPTION	DATE	CHKD	APPROV
1	WELDOR CERTIFICATION, REF. GIL 59790	12/80	BC	ML
2	ADDED SH. 2 CMC 76965			
3	REV'D WELDOR CMC, REF. AICP M-8041	6/83	RM	TS

ASME CODE EDITION: 1974
ADDENDA: WINTER
DESIGN SPEC: MS-76A

RE. CERTIFICATION
FOR ENGINEERING & OFFICE USE ONLY



DATA PT	SUPPORT	LOADS (LBS)	PIPE
DESIGN	SEISMIC	LEVEL	NYTS
VERT.		SEE SHEET 2 OF 2	INCHES
N-S			
E-W			
NOTE	AUTHORIZED NUCL. INSP. YES <input checked="" type="checkbox"/> NO <input type="checkbox"/>		
IN, E, UP	ASME CODE CLASS 3		
8, W, DN			

STRESS ISO.	REV	MECHANICAL	REV	ELECTRICAL	REV
M2-3231-36	A	MI-0701	6	EI-0703	6
ISO.	REV	STRUCTURAL	REV	H.V.A.C	REV
CC-2-AB-032	1	S-0735	2	MI-0757	4



Brown & Root, Inc.
ENGINEERS AND CONSTRUCTORS
HOUSTON, TEXAS

CLIENT: T.U.S.I.
PLANT: COMANCHE PEAK
JOB NO.: 2323

SUPPORT NO. CC-2-011-703-A63R
SHEET 1 OF 2 REV. 3

FOR OFFICE AND
ENGINEERING USE ONLY

AS-BUILT

VENDOR CERTIFIED
DESIGNED BY NO. 3
REV. (W.M.) 6-24-83

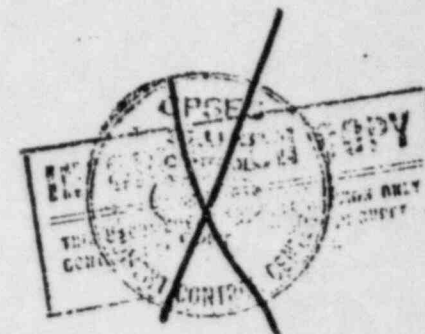
DATA PT.	DESIGN	SERVICE	LEVEL	LIMITS	PIPE MVT'S (INCHES)
2112		A	B	C	D
VERT.		-197	±224	±242	±265
N-S		+215	-354	±240	±261
E-W					
NOTE P.N.E,UP -S.W,DN AUTHORIZED NUCL. INSP. YES <input checked="" type="checkbox"/> NO <input type="checkbox"/> ASME CODE CLASS 3					


DATA PT.	DESIGN	SERVICE	LEVEL	LIMITS	PIPE MVT'S (INCHES)
1008		A	B	C	D
VERT.		-270	±287	±291	±296
N-S		-270	±287	±291	±296
E-W					
NOTE P.N.E,UP -S.W,DN AUTHORIZED NUCL. INSP. YES <input checked="" type="checkbox"/> NO <input type="checkbox"/> ASME CODE CLASS 3					

MVT'S
±.104
- .185

MVT'S
±.103
- .184

FOR ENGINEERING
& OFFICE USE ONLY



DATA PT.	SUPPORT LOADS (lbs)				PIPE MVT'S (INCHES)	REF. DWGS.	STRESS ISO.	REV.	MECHANICAL	REV.	ELECTRICAL	REV.	DESCRIPTION	DATE	OWN.	CHKD.
	DESIGN	SERVICE	LEVEL	LIMITS			M2-3231-36	A		BRHL ISO.		REV.				
VERT.	A	B	C	D			CC-2-AB-032	I					VEHICULAR CERTIFICATION REF. CH# 59790	11/1/82	P	186
N-S													CMC 76965			
E-W													REV'D VENDOR CERTIFICATION REF. CH# 115041	7/1/83	RM	186
NOTE P.N.E,UP -S.W,DN	AUTHORIZED NUCL. INSP. YES <input checked="" type="checkbox"/> NO <input type="checkbox"/> ASME CODE CLASS 3					<div>CPSES</div> <div></div> <div>38-1188</div> <div>Brown & Root, Inc.</div> <div>ENGINEERS AND CONSTRUCTORS</div> <div>HOUSTON, TEXAS</div>					CLIENT T.U.S.I. PLANT COMANCHE PEAK JOB NO. 2323			SUPPORT NO. CC 2-011703-A63R SHEET 2 OF 2 REV. 3		

FOR OFFICE AND

REVISIONS

AS-BUILT

VENDOR CERTIFIED
DRAWING REV. NO. 2
BY BH DATE 12-6-82

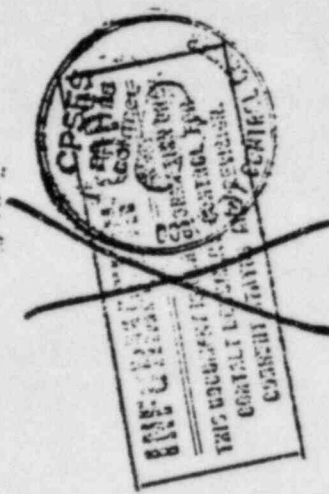


DATA PT		SUPPORT LOADS (lbs)			MUTS	
DEWG	SERVICE LEVEL	C	CH			
ROCK	A	350	350		X	0
VERT.	B	350	350			0
L-S	C	350	350		Y	0
E-W	D	350	350			0
	E	350	350			0
	F	350	350			0
	G	350	350			0
	H	350	350			0
	I	350	350			0
	J	350	350			0
	K	350	350			0
	L	350	350			0
	M	350	350			0
	N	350	350			0
	O	350	350			0
	P	350	350			0
	Q	350	350			0
	R	350	350			0
	S	350	350			0
	T	350	350			0
	U	350	350			0
	V	350	350			0
	W	350	350			0
	X	350	350			0
	Y	350	350			0
	Z	350	350			0

DATA #	SUPPORT LOADS (lbs.)			MVTs
	DESIGN	SERVICE LEVEL	ACTUAL	
2116	A	B	C	0
VERT	-192	-337	132	0
11-5	+225	1394	1174	0
E-W	0	0	0	0
				2
				2125
				214



**FOR ENGINEERING
& OFFICE USE ONLY**



TO* 21101

DATA PT.	SUPPORT	LOADS	(in)	PIPE
DESIGN	SERVICE	LEVEL	LIMITS	WITS
	A			(INCHES)
VERT.				
H-B				
E-W				

REF. DWS.	BRILL. ISO.	MECHANICAL	REV.	ELECTRICAL	REV.	NEW	DESCRIPTION	DATE	DWN.	CHKD.	APP.
CC-2-AB-032	CC-2-AB-032	MI-0701	0	ET-0703	6	6	VALVEOR CERTIFICATION	11/1/73	TPJ	Q	JRS
		STRUTURAL	REV.	H.V.A.C.	REV.	REV.	COMC 76964				
		1 5-0735		MI-0757	2	4					

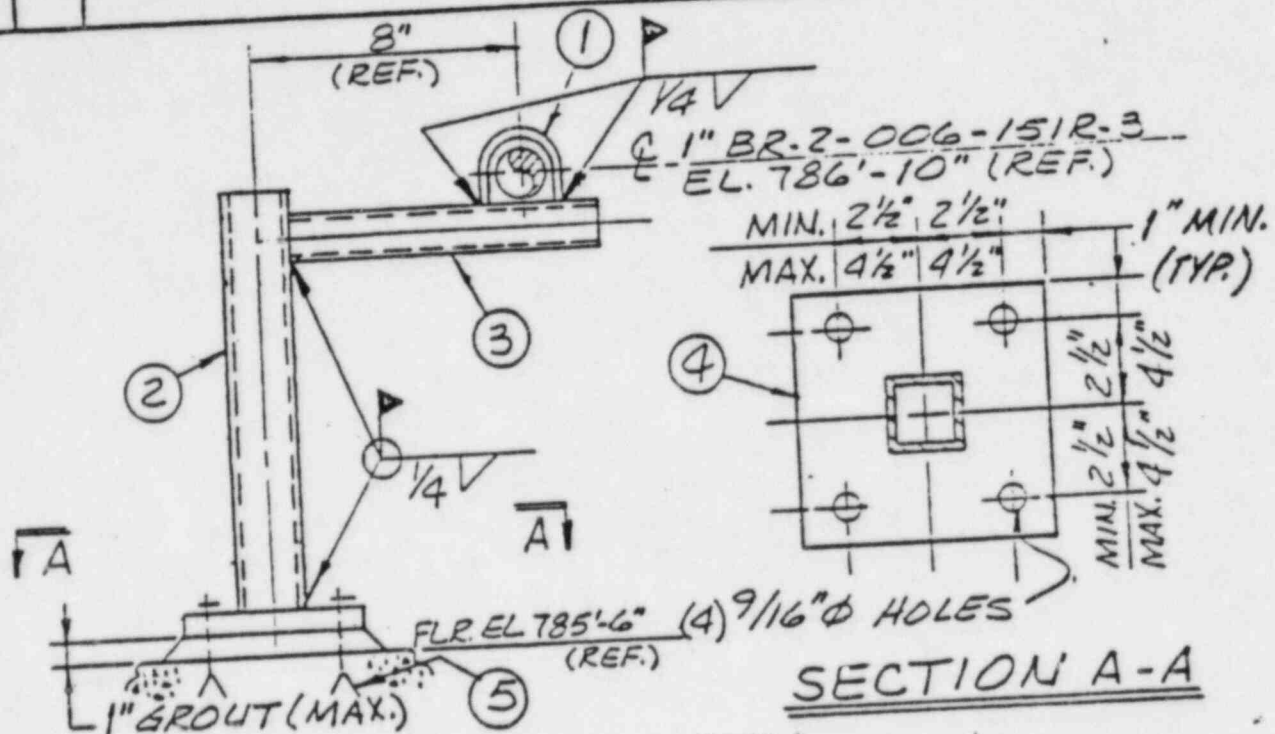
CLIENT	T.U.S.I.
PLANT COMANCHE PEAK	
JOB NO. 2323	

SUPPORT NO.	CC-2-011-704-A63R
SHEET 2 OF 2	REV. 2

DESIGNER	DATE	APP.
JRS	11/1/73	JRS

ITEM NO.	QTY	MATERIAL DESCRIPTION	MATERIAL DESIG.
1	1	WELDED U-GUIDE - PUG - 010	SA-36
2	1	TS. 3 x 3 x .250 x 1'-4 1/2" LG. (CUT TO SUIT)	A500, GR.B
3	1	TS. 2 x 2 x .250 x 1'-1 1/2" LG. (CUT TO SUIT)	A500, GR.B
4	1	PIPE 5 3/4" THK. (SEE SECTION A-A)	SA-36
5	4	1/2" x 9" HILTI-KWIK BOLT (5 1/2" MIN. EMB.)	

FOR OFFICE AND
ENGINEERING USE ONLY



ELEVATION LKG NORTH

NOTE:

FOR GEN. NOTES, SEE CP-AA-001.

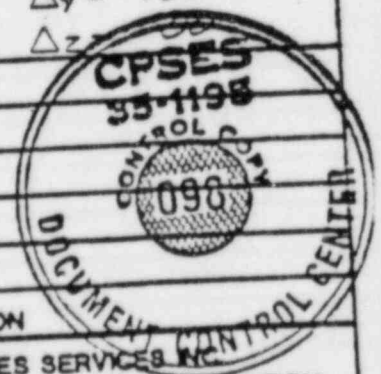
MAX. MVMTS. (IN.)

$\Delta x = -.11$

$\Delta y = .00$

$\Delta z = .00$

0	11.16.83	E.C.	CP	11.16.83	RELEASED FOR CONSTRUCTION	
REV	DATE	DWN	CHKD	APPR	DESCRIPTION	
PROB. #	DATA PT.	DESIGN	LOADS (LBS)	PIPE		
		SERVICE	LEVEL LIMITS	MVMT		
		A	B	C	(INCHES)	
	VERT.	21	34	47	0	
+N,E,UP	N-S				-.10	
-S,W,DN	E-W	5	11	17	0	
TEXAS UTILITIES SERVICES INC.						
COMANCHE PEAK STEAM ELECTRIC STATION						
PIPE SUPPORT ENGINEERING						
DRAWING NO. H-BR-2-SB-001-009-3						
REV. 0						
SHT 1-OF-1						



TEXAS UTILITIES GENERATING COMPANY

OFFICE MEMORANDUM

To 000 DistributionDallas, Texas March 9, 1984Subject Resolution of QAI-0001

'84 AGO 15 P12:15

OFFICE OF SECURITY
SECRETARY
BR

The Quality Assurance Investigation listed above has been resolved to the satisfaction of the Manager, Quality Assurance. No further action is necessary at this time. Please contact the undersigned at 214-979-8890 if there are any questions on this matter.

Thank you.

Jerry C. Walker
Jerry C. Walker

JCW:ln

Distribution: D. N. Chapman/QE File 3
D. L. Andrews/Corporate Security
Boyce Grier/CPSES QA
Initiator (A. Vega)

CONFIDENTIAL

TEXAS UTILITIES GENERATING COMPANY

OFFICE MEMORANDUM

To A. Vega

Glen Rose, Texas February 22, 1984

Subject

Investigation of Allegations

QAI #0001

In response to your request of 12/20/83 I have investigated the allegations forwarded with QAI #0001. This is the report of my findings.

I interviewed the alleged, [REDACTED], at his home to obtain additional information on the matters alleged in his letter to Doug Frankum. A copy of this letter is attached (Attachment A). My report of the interview is contained in Attachment B. During the interview I was given additional allegations as indicated in the interview report. These additional matters have also been investigated where practicable.

In the investigation, I interviewed two persons named by [REDACTED] in his allegations-- a QC inspector, [REDACTED], and a General Foreman, [REDACTED]. My reports of these interviews are contained in Attachment C and Attachment D. I also reviewed various procedures, records and documentation as appropriate. I have summarized the results of these activities and have developed my evaluation and conclusion for each allegation. These are discussed below.

1. Improper Marking of Hilti Bolts

The information regarding improper marking of Hilti bolts provided by [REDACTED] in the interview was essentially the same as that contained in his letter to Frankum. It should be noted that [REDACTED] had no first hand knowledge of this matter but was reporting what he was told. I interviewed [REDACTED] the QC inspector named by [REDACTED] as having received the star stamp found by the laborer, and she told me essentially the same story. She did state that the star stamp found and given to her was different from that used by QC to mark Super Hilti's and she felt if the stamp had been used the different marking would have been noticed on the Hilti. She had never noticed any evidence that the stamp was used by the craft. I interviewed [REDACTED], the General Foreman named by [REDACTED] who knew that a star stamp had been found and turned in to QC but he had not seen the stamp. [REDACTED] stated that he had no knowledge of the star stamp being used by craft personnel under his supervision.

The allegation of a star stamp being found and turned in to QC was confirmed. The allegation of it being used for improper marking of Hilti bolts was not confirmed.

2. Improper Welding

Based on additional information provided by [REDACTED] during the interview, I visited the area and identified the pipe support in question to be

BR-X-056-726-A53A. A copy of the as-built drawing for this support is attached (Attachment D). I reviewed the weld records for the saddle weld in question and found everything in order. This information was reviewed during my interview with [REDACTED]. It should be noted that the welding procedure specified in this case was WPS-18010 which provides for using "heliarc" procedure for the root and hot pass. After these first two passes it is optional whether "heliarc" or "stick" welding is used to complete the weld. Thus completing the entire weld in question using "heliarc" procedure as alleged by [REDACTED] is not improper. This is what was done according to the welding records. The records show the welding was done by [REDACTED]. There is no indication of any involvement by a welder named [REDACTED].

The allegation that the saddle for the pipe hanger in question was welded by heliarc procedure was confirmed and the procedure used was found to be proper. The allegation that the weld was improperly made by [REDACTED] was not confirmed.

3. Oversize Holes for Hilti Bolts

During the interview [REDACTED] made an allegation regarding an oversize hole (1½") being drilled in the floor for a 1½" Hilti bolt in a hanger base plate. Based on information provided I visited the area and identified the support in question as CC-2-070-002-A33R. A copy of the as-built drawing for this support is attached (Attachment F). There is nothing in the documentation package for this pipe support to indicate a requirement for or the approval of an oversize hole. I reviewed the reports of the QC inspections for the Hilti installation for this support. These are contained in the following:

IRMH-19682, dated 7/1/81
IRMH-53200, dated 2/15/83
IRMH-53257, dated 2/22/83

These reports do not indicate any nonconforming or unsatisfactory conditions. [REDACTED] stated during his interview that he had no knowledge of oversize holes ever being drilled for Hilti bolts.

I made inquiry of pipe support engineering (Jay Ryan) as to whether an oversize hole for a Hilti bolt in the support in question would be of concern. I was told that it would not be a problem.

The allegation that an oversize hole had been drilled for a Hilti bolt could neither be confirmed or dismissed. It appears that physical inspection of the holes for the support in question would be the only way to resolve this matter. In view of the response from Engineering regarding the significance of this matter, it does not appear necessary to pursue the matter further.

4. Torqueing of Hilti Bolts in Ceiling

It is my understanding that the allegation regarding QC inspectors relying on craft personnel to check the torqueing of Hilti bolts in places where access is limited has been investigated previously. This matter has been discussed in the Licensing Hearings before the ASLB and is recorded in the transcript for September 14, 1982, on pages 4537-4539 (Attachment G). In view of this, no further investigation of this matter was made.

5. Damaged Threads on 1/2" Hilti Bolt

[REDACTED] did not provide sufficient information on the location of this problem to enable the matter to be investigated. Since it was described as an isolated case, it does not appear that further action is warranted at this time to resolve safety concerns. Of more concern is the alleged deliberate act for fraudulent purposes.

If you have questions or comments regarding any of the above matters or if you wish me to pursue anything further, please let me know.

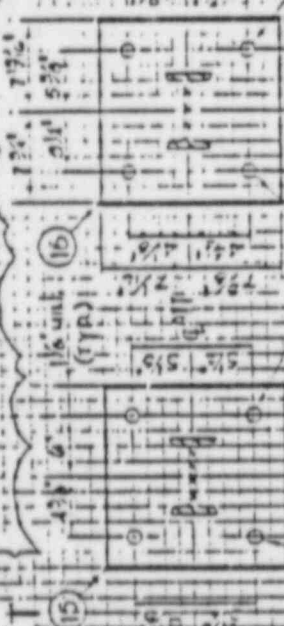
Doyce H. Grier

BHG/b11

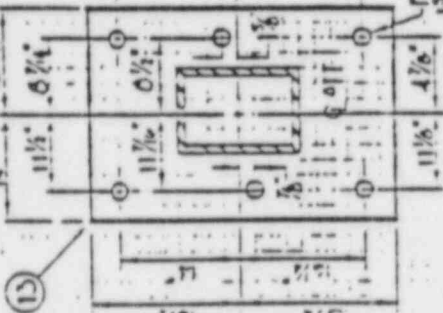
Attachments: A - Letter to Frankum from [REDACTED]
B - Interview with [REDACTED]
C - Interview with [REDACTED]
D - Interview with [REDACTED]
E - Drawing BR-X-056-126-A53A
F - Drawing CC-2-070-002-A33R
G - Hearing Transcript pp. 4537-4539

cc: D. N. Chapman
D. L. Andrews
R. G. Tolson

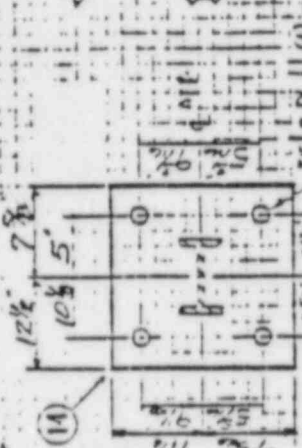
VENDOR CERTIFIED
OF BUYING REV. NO. 2
BY *W. R. FAIG* 4/2/83



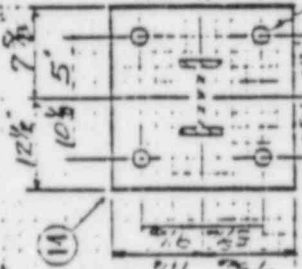
SECTION "F-2"



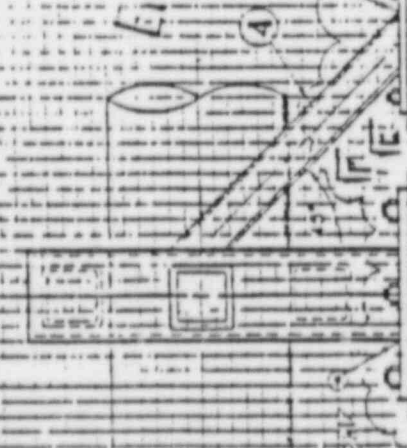
SECTION "C-C"



SECTIONS



FOR OFFICE AND
ENGINEERING USE ONLY



REVOLUTION



BROWN & ROOT, INC.
Engineering • Construction

REF. DRAWING NUMBERS

PIPE: _____
ELECT: _____
HVAC: _____
TECH: _____

CUSTOMER Texas Utilities Service, Inc.

ORDER OR CONT. NO. CP-0046

JOB NAME Comanche Pass 1022
MAIN C C-2-070-002-0550

SKETCH NO. 1

SHEET 2 OF 3 YZS REV. 7

NOV 1 1985

FOR CONST

FEELINGS NOTED. SEE CMC#
31523 E1

11 E 115 44th St / 10th Ave / 01142 Bx 207
Rd 66878207 / 30 10 / 10 10 10 10

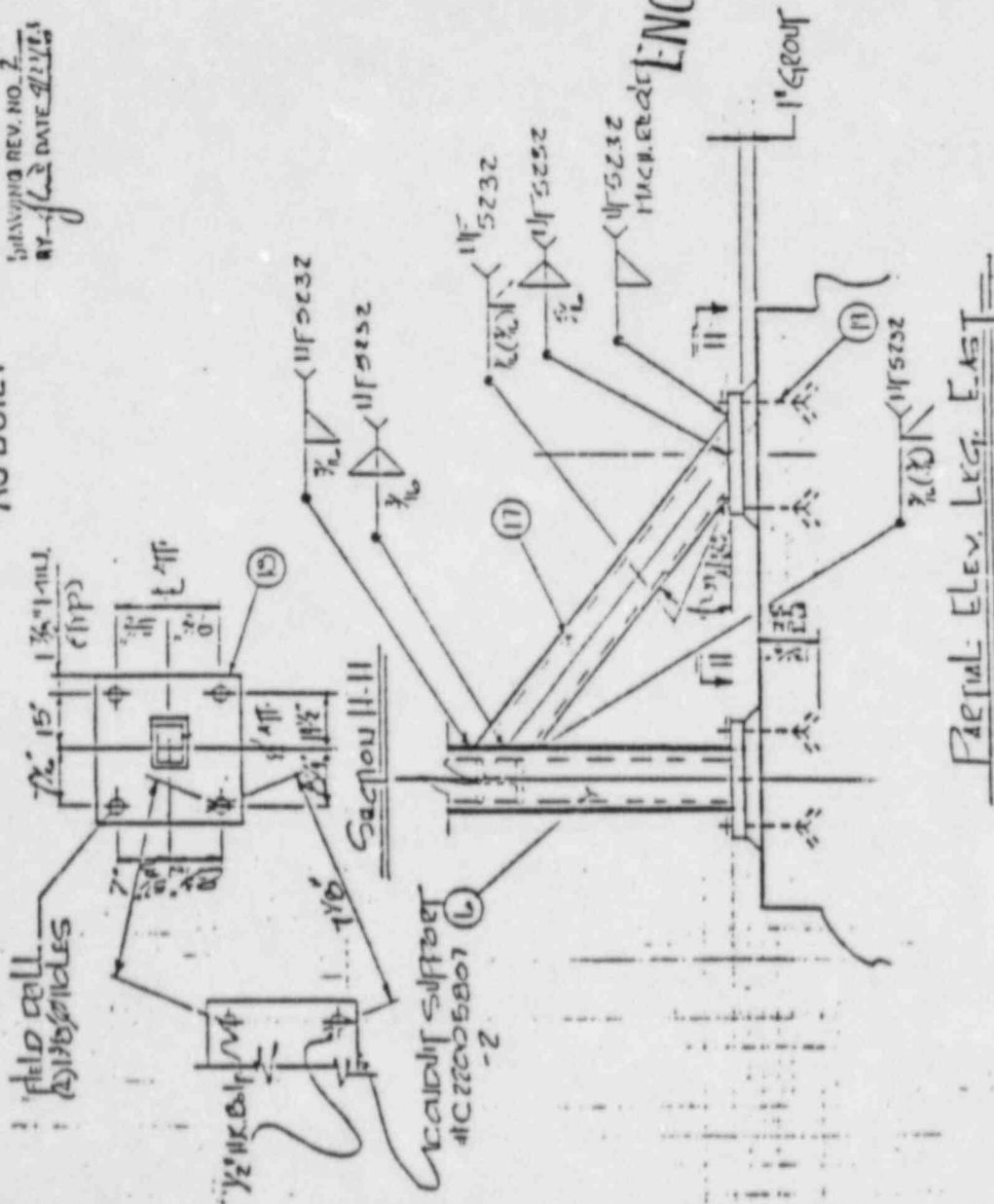
[illegible]

THIRD PARTY INSPECTION

CODE CLASS: ASME III-2

AS-BUILT

VENDOR CERTIFIED
DRAWING REV. NO. 2
DATE 9/1/83



FOR OFFICE AND
ENGINEERING USE ONLY

PARTIAL ELEV. LEG. EAST

BROWN & ROOT, INC. ENGINEERING & CONSTRUCTION	
REF. DRAWING NUMBERS	
PIPE:	ELECT:
STEEL:	HVAC:
CUSTOMER: Texas Utilities Service, Inc.	
ORDER OR CONT. NO.	CP-0046
JOB NAME	Comanche Peak 1B2
MARKING	CC-3-010-002-ASB
SKETCH NO.	
SHEET 3 OF 3	REV. 2

DESCRIPTION			
1	1/2" x 1/2" x 1/2"	1/2" x 1/2" x 1/2"	1/2" x 1/2" x 1/2"
2	1/2" x 1/2" x 1/2"	1/2" x 1/2" x 1/2"	1/2" x 1/2" x 1/2"
3	1/2" x 1/2" x 1/2"	1/2" x 1/2" x 1/2"	1/2" x 1/2" x 1/2"
4	1/2" x 1/2" x 1/2"	1/2" x 1/2" x 1/2"	1/2" x 1/2" x 1/2"
5	1/2" x 1/2" x 1/2"	1/2" x 1/2" x 1/2"	1/2" x 1/2" x 1/2"
6	1/2" x 1/2" x 1/2"	1/2" x 1/2" x 1/2"	1/2" x 1/2" x 1/2"
7	1/2" x 1/2" x 1/2"	1/2" x 1/2" x 1/2"	1/2" x 1/2" x 1/2"
8	1/2" x 1/2" x 1/2"	1/2" x 1/2" x 1/2"	1/2" x 1/2" x 1/2"
9	1/2" x 1/2" x 1/2"	1/2" x 1/2" x 1/2"	1/2" x 1/2" x 1/2"
10	1/2" x 1/2" x 1/2"	1/2" x 1/2" x 1/2"	1/2" x 1/2" x 1/2"

THIRD PARTY INSPECTION
CODE CLASS: ASME III-2

10.21101

[illegible]

SECTION V
FIGURE 6

TEXAS UTILITIES SERVICES INC.
Agent For
DALLAS POWER & LIGHT COMPANY
TEXAS ELECTRIC SERVICE COMPANY
COMANCHE PEAK S.E.S.

ALLOWABLE LOADS FOR HILTI KWIK AND SUPER HILTI KWIK BOLTS
USING 4000 PSI CONCRETE, 5:1 SAFETY FACTOR, A.A. HANKS TESTING LAB REPORT
NO. 873R AND HILTI LETTER DATED OCT. 27, 1980 / CPPA-7419 COVER LETTER

HILTIS

BOLT DIA	EMB. LENGTH	TENSION	SHEAR
1/2"	2 3/4"	1102	1663
	2 3/4"	1440	↓
	3 1/2"	1890	↓
	4 1/2"	2245	2046
	5 1/2"	2410	↓
	6"	2460	↓
5/8"	2 3/4"	1320	2312
	3 1/2"	1820	↓
	4 1/2"	2400	↓
	5 1/2"	2860	3087
	6 1/2"	3200	↓
	7 1/2"	3400	↓
3/4"	3 1/4"	2030	3427
	4"	2680	↓
	5"	3300	↓
	6"	3600	3693
	7"	4200	↓
	8"	4600	↓
1"	4 1/2"	3200	5375
	5"	3780	↓
	6"	4688	↓
	7"	↓	↓
	8"	↓	6898
	9"	↓	↓
1 1/4"	5 1/2"	4600	7136
	6 1/2"	5420	↓
	7 1/2"	6220	↓
	8 1/2"	6920	↓
	9 1/2"	7560	↓
	10 1/2"	8180	↓

SUPER HILTIS

BOLT DIA.	EMB. LENGTH	TENSION	SHEAR
1/2"	3 1/4"	1997	2288
	4 1/4"	2956	↓
	5 1/4"	2956	↓
	6 1/4"	3029	↓
1"	6 1/2"	6993	5507
	8 1/2"	9951	↓
	10 1/2"	9951	↓
1 1/4"	8 1/8"	8540	8296
	10 5/8"	10736	↓
	13 1/8"	12984	↓

TEXAS UTILITIES GENERATING COMPANY

P. O. BOX 1002 · GLEN ROSE, TEXAS 76043

PROJECT FILE

April 19, 1984

DOCKETED
USING

'84 AGO 15 P12:15

Cygn Energy Services
101 California Street
Suite 1000
San Francisco, California 94111

CYGNA	
LOG NO.:	84042
DATE LOGGED:	5/14/84
LOG NO.:	#9
FILE:	2.1.1 Inc. CR
CROSS REF. FILE	2.1.1 Inc. CR

Attention: Ms. Nancy Williams
Project Manager

COMANCHE PEAK STEAM ELECTRIC STATION

Gentlemen:

In response to your handwritten questions provided to TUGCO on March 16, 19, 20, 21 and 22, enclosed is a copy of the questions followed by TUGCO's response. Several questions are still under review and will be answered shortly. In addition, questions asked via telephone to Dave Rencher on March 30, 1984, are presently being reviewed and responses will be forwarded by April 27th.

If there are any further questions or comments, please contact me or George Grace (Site Ext. 500).

Very truly yours,

TEXAS UTILITIES GENERATING COMPANY
ENGINEERING DIVISION

L. M. Popplewell
Project Engineering Manager

LMP/cp

Distributive
NH Williams
J. C. Minchillo
R. Weirgart
C. Wang
M. Schulman
84042 Project File (To Acura)

working range (generally near mid-travel); a minimum $\frac{1}{4}$ " travel exists beyond working range limits to reach a fully extended or retracted position. For most springs, more than $\frac{1}{4}$ " is available. This is sufficient to account for the small seismic displacements. For box frames, the seismic movements for the supports listed were checked against the designs. In all cases, adequate clearance existed to allow combined thermal and seismic displacements.

CYGNA COMMENT:

3. In reviewing certain MS supports, CYGNA has noted instances where beams with small gaps are used to provide stability, instead of tightening U-bolts (supports MS-1-004-003-S72R, for example). In these cases, no analysis is done on the "stability bumpers." CYGNA has performed calculations which show that the load on these "supports" could be quite high, assuming one accepts the instability of this structure during dynamic loading. Has TUSI used this design for any supports with static compressive loads? Also, where is the documentation for the integrity of this support arrangement in general?

TUGCO RESPONSE:

3. The "bumpers" supplied on MS-1-004-003-S72R (in lieu of a snug U-bolt) for stability are designed to take an oscillating, momentary load (for a system at 20Hz, the applied load onto the bumpers will act less than 0.05 seconds). Hence, the nature of the cyclic load assures stability in that there is not sufficient time for a constant applied force to push the bumpers back and allow the pipe to lift up. The calculations which consider a static upward load are therefore erroneous. The stress in the bumper steel stays within its elastic limit under the impact load and hence will return to its original position when the load reverses and pushes down. This design has not been used on any supports which would experience a static compressive load. Structural acceptability of the bumpers is based on the momentary load of less than 0.05 second duration. Size of the members, welds, were judged adequate by inspection.

March 21, 1984

CYGNA COMMENT:

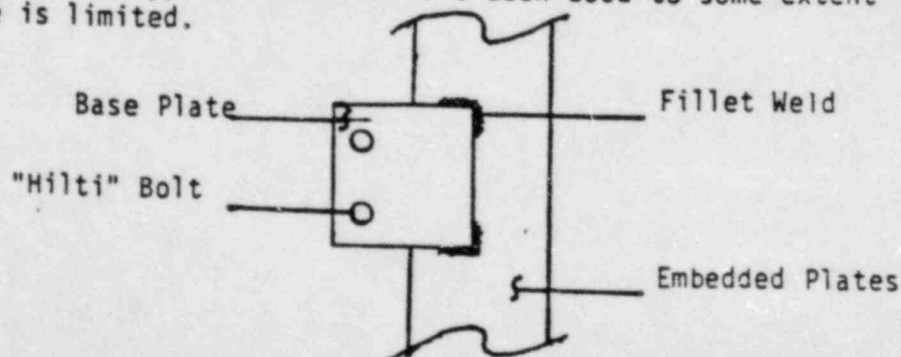
1. In reviewing MS-1-004-001-C72S, CYGNA had the following questions:
 - a) There appears to be a 7/16" flare bevel weld between items 15 and 22. This does not seem possible due to Item 34. Does TUSI have documentation conforming the size and configuration of this weld? Likewise, the weld (5/16") between 26 and 15?

- b) The model uses a fixed point at the embed plates (3, 6, 12, 15 joints). Spec. 2323-SS-30, Rev. 1, requires these to be treated as pin joints, unless the embedment is stiffened. Where is the stiffener in this calc, and has structural accepted this configuration?
- c) Per ASME Appendix XVII, Para. 2442, shear loads on connections with both welds and bolts must be taken by the welds alone. Item 16 is attached to Beam #21 with both welds and Hilti's. The weld sizing calculations done use the bolts to share the shear load. What is TUSI's standard practice in this type of connection? Is this weld acceptable?
- d) The weight of the constant support itself is not included in the support design load for the frame. A #53 constant weighs - 600 lb, or 5% of the design load.

What is TUSI's standard practice for spring anchorage design?

TUGCO RESPONSE:

1. (a) In the NPSI original design, $\frac{1}{2}$ " wall tube steel was used and the $\frac{7}{16}$ " flare bevel weld was possible. Modifications made at the site changed most of the steel members to $\frac{3}{8}$ " wall tube. The weld between items 15 and 22 is a flare bevel weld such that the groove is filled and ground flush to facilitate installation of Item 34. CYGNA is correct in their observation that a $\frac{7}{16}$ " flare bevel weld does not exist, the size was inadvertently not removed during the revision process. The stiffening effect of Item 34 on this joint assures structural acceptability. The $\frac{5}{16}$ " flare bevel weld between items 26 and 15 is an acceptable weld since the tube steel thickness is $\frac{3}{8}$ " (greater than $\frac{5}{16}$ "). Documentation confirming the size of these welds is on file with QC in their inspection package. (b) See comments dated 3/22, response 1. (c) (Editorial: Items 15 and 19 are connected to beam 21, not item 16.) The connection to the beam via embedded plate (i.e., by welding) and via baseplate (i.e., by bolting) is at separate locations. As such, each is capable of resisting shear. It should be noted that Hilti joints are designed using bolt shear allowables based on ultimate test loads divided by 5. This is not the standard engineering approach to design a bearing or friction joint using code allowables for the bearing or friction condition. Using our design approach, the Hilti joints, since they are pre-torqued, would perform as a friction joint within their working loads. At ultimate loads all joints (bearing or friction) would act as bearing joints (i.e., slip would occur in the friction connection). (Following comments, in response to CYGNA's comment on TUSI's standard practice are provided here for information only). Connections of the type shown below have been used to some extent where space is limited.



UNITED STATES OF AMERICA
NUCLEAR REGULATORY COMMISSION

BEFORE THE ATOMIC SAFETY AND LICENSING BOARD

In the Matter of	}}	
	}}	
TEXAS UTILITIES ELECTRIC	}}	Docket Nos. 50-445-1
COMPANY, <u>et al.</u>	}}	and 50-446-1
(Comanche Peak Steam Electric	}}	
Station, Units 1 and 2)	}}	

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CERTIFICATE OF SERVICE

By my signature below, I hereby certify that true and correct copies of
CASE's 8/13/84 Answer to Applicants' Motion for Summary Disposition Regarding
the Effects of Gaps on Structural Behavior Under Seismic Loading Conditions

have been sent to the names listed below this 13th day of August, 1984,
by: Express Mail where indicated by * and First Class Mail elsewhere.

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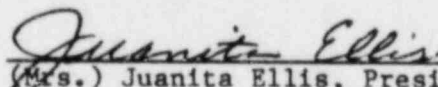
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