

# AVERAGE DAILY UNIT POWER LEVEL

DOCKET NO. 50-387

UNIT One

DATE May 9, 1984

COMPLETED BY L.A. Kuczynski

TELEPHONE (717) 542-3759

MONTH April, 1984

DAY	AVERAGE DAILY POWER LEVEL (MWe-Net)
1	<u>980</u>
2	<u>1,057</u>
3	<u>1,059</u>
4	<u>1,057</u>
5	<u>1,051</u>
6	<u>1,058</u>
7	<u>1,053</u>
8	<u>1,008</u>
9	<u>1,058</u>
10	<u>1,059</u>
11	<u>1,057</u>
12	<u>1,055</u>
13	<u>1,053</u>
14	<u>601</u>
15	<u>817</u>
16	<u>1,023</u>

DAY	AVERAGE DAILY POWER LEVEL (MWe-Net)
17	<u>924</u>
18	<u>847</u>
19	<u>844</u>
20	<u>921</u>
21	<u>1,055</u>
22	<u>1,054</u>
23	<u>1,057</u>
24	<u>1,057</u>
25	<u>1,055</u>
26	<u>1,052</u>
27	<u>1,048</u>
28	<u>1,046</u>
29	<u>983</u>
30	<u>1,043</u>
31	<u></u>

## INSTRUCTIONS

On this format, list the average daily unit power level in MWe-Net for each day in the reporting month. Compute to the nearest whole megawatt.

(9/77)

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# OPERATING DATA REPORT

DOCKET NO. 50-387  
 DATE May 9, 1984  
 COMPLETED BY L.A. Kuczynski  
 TELEPHONE (717) 542-3759

## OPERATING STATUS

Unit 1

1. Unit Name: Susquehanna Steam Electric Station
2. Reporting Period: April, 1984
3. Licensed Thermal Power (MWt): 3,293
4. Nameplate Rating (Gross MWe): 1,152
5. Design Electrical Rating (Net MWe): 1,065
6. Maximum Dependable Capacity (Gross MWe): 1,068
7. Maximum Dependable Capacity (Net MWe): 1,032
8. If Changes Occur in Capacity Ratings (Items Number 3 Through 7) Since Last Report, Give Reasons:

None

Notes

9. Power Level To Which Restricted, If Any (Net MWe): None
10. Reasons For Restrictions, If Any: None

	This Month	Yr.-to-Date	Cumulative
11. Hours In Reporting Period	<u>719</u>	<u>2,903</u>	<u>7,872</u>
12. Number Of Hours Reactor Was Critical	<u>719</u>	<u>1,153</u>	<u>4,998.3</u>
13. Reactor Reserve Shutdown Hours	<u>0</u>	<u>0</u>	<u>156.7</u>
14. Hours Generator On-Line	<u>719</u>	<u>1,075.8</u>	<u>4,844.1</u>
15. Unit Reserve Shutdown Hours	<u>0</u>	<u>0</u>	<u>0</u>
16. Gross Thermal Energy Generated (MWH)	<u>2,255,077</u>	<u>3,055,110 *</u>	<u>14,316,771 *</u>
17. Gross Electrical Energy Generated (MWH)	<u>745,490</u>	<u>998,240</u>	<u>4,664,790</u>
18. Net Electrical Energy Generated (MWH)	<u>719,795</u>	<u>960,716</u>	<u>4,497,089</u>
19. Unit Service Factor	<u>100</u>	<u>37.1</u>	<u>61.5</u>
20. Unit Availability Factor	<u>100</u>	<u>37.1</u>	<u>61.5</u>
21. Unit Capacity Factor (Using MDC Net)	<u>97.0</u>	<u>32.1</u>	<u>55.4</u>
22. Unit Capacity Factor (Using DER Net)	<u>94.0</u>	<u>31.1</u>	<u>53.6</u>
23. Unit Forced Outage Rate	<u>0</u>	<u>34.2</u>	<u>18.1</u>
24. Shutdowns Scheduled Over Next 6 Months (Type, Date, and Duration of Each):			

None

25. If Shut Down At End Of Report Period, Estimated Date of Startup:	<u>N/A</u>	
26. Units In Test Status (Prior to Commercial Operation):	Forecast	Achieved
INITIAL CRITICALITY	<u>      </u>	<u>      </u>
INITIAL ELECTRICITY	<u>      </u>	<u>      </u>
COMMERCIAL OPERATION	<u>      </u>	<u>      </u>

\* Updated Figures  
 Better data became available.

(9/77)



# UNIT SHUTDOWNS AND POWER REDUCTIONS

REPORT MONTH April, 1984

DOCKET NO. 50-387

UNIT NAME One

DATE May 9, 1984

COMPLETED BY L.A. Kuczynski

TELEPHONE (717) 542-3759

No.	Date	Type <sup>1</sup>	Duration (Hours)	Reason <sup>2</sup>	Method of Shutting Down Reactor <sup>3</sup>	Licensee Event Report #	System Code <sup>4</sup>	Component Code <sup>5</sup>	Cause & Corrective Action to Prevent Recurrence
3	840413	S	0	H	4	N/A	IC	CONROD	A power reduction from 100% to 60% was initialized to change the control rod pattern. No corrective action is required for this power reduction. It was a planned event.

<sup>1</sup>  
F: Forced  
S: Scheduled

<sup>2</sup>  
Reason:  
A-Equipment Failure (Explain)  
B-Maintenance or Test  
C-Refueling  
D-Regulatory Restriction  
E-Operator Training & License Examination  
F-Administrative  
G-Operational Error (Explain)  
H-Other (Explain)

<sup>3</sup>  
Method:  
1-Manual  
2-Manual Scram.  
3-Automatic Scram.  
4-Other (Explain)

<sup>4</sup>  
Exhibit G - Instructions  
for Preparation of Data  
Entry Sheets for Licensee  
Event Report (LER) File (NUREG-  
0161)

(9/77)

<sup>5</sup>  
Exhibit I - Same Source

UNIT 1  
SUSQUEHANNA STEAM ELECTRIC STATION

Docket Number 50-387      Date May 9, 1984

Completed by L.A. Kuczynski      Telephone (717) 542-3759

Challenges to Main Steam Safety Relief Valves

None.

Changes to the Offsite Dose Calculation Manual

See Attachment.

Major Changes to Radioactive Waste Treatment Systems

None.

ATTACHMENT TO UNIT ONE

April, 1984, Monthly Operating Report

Changes to the  
Offsite Dose Calculation Manual

These revised pages were made effective on January 20, 1984 upon signature by the Manager-Nuclear Support.

Changes have been denoted by revision bars in the right margin. The reasons for the changes are as follows:

- 1) To include setpoints for Service Water and RHR Service Water.
- 2) To include setpoint methodology for Vent Flow Rates and SPING Sample Flow Rates.

PENNSYLVANIA POWER & LIGHT COMPANY  
SUSQUEHANNA STEAM ELECTRIC STATION  
OFFSITE DOSE CALCULATION MANUAL

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Prepared By J.E. Widner Date 1/20/84

Reviewed By K.E. Shank Date 1/20/84

PORC Review Required Yes ( ) No (✓) Date \_\_\_\_\_

Approved By [Signature] Date 1/20/84  
Manager-Nuclear Support

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$$\frac{F + f}{f} = \frac{Y \cdot (A)}{MPC}$$

where  $\frac{F + f}{f}$  = the setpoint dilution factor

The requirements of Equation (2) are then met as follows:

$$Y \cdot (A) = MPC \left( \frac{F + f}{f} \right)$$

Since, by definition,  $Y > X$  and  $Y(A) > X(A)$ , then

$$(c) = X(A) < MPC \left( \frac{F + f}{f} \right)$$

The setpoint concentration (c) can then be converted to a setpoint count rate value by use of the monitor calibration factor.

$$\text{Setpoint (cpm)} = \frac{c \text{ (}\mu\text{Ci/ml)}}{\text{Cal. Factor (}\mu\text{Ci/ml per cpm)}} \quad (3)$$

The setpoint for the dilution water flow (cooling tower blowdown) is 5000 gpm from either cooling tower basin. The setpoint for the LRW discharge flow can then be determined from:

$$\frac{F + f}{f} = \frac{(A)}{MPC} \cdot Y$$

Sample calculations for determining the release concentration limits and setpoints are given in Section A.1.1 of Appendix A.

The Service Water System provides screened water from the cooling tower basin for cooling plant systems and equipment. The Residual Heat Removal (RHR) Service Water System provides water from the Engineered Safeguard Service Water (ESSW) spray pond to the RHR heat exchangers. In post-accident conditions, RHR Service Water can supply water for vessel and containment flooding. The Service Water and RHR Service Water Systems are not normal pathways for liquid effluents. Radiation monitors are in place on these systems to provide indication of leaks across heat exchangers into the service water. The high

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radiation setpoints for these monitors are set at  $2\text{E-}5 \mu\text{Ci/cc}$  cesium-137 equivalent. Considering the radionuclides predominant in SSES liquid effluents, e.g., Co-58, Co-60, Fe-59, Mn-54 and Cr-51, use of a setpoint based on the Cs-137 MPC is conservative based on the following parameters:

- 1) photon abundance (85%)
- 2) magnitude of applicable MPC ( $2\text{E-}5 \mu\text{Ci/cc}$ )

Because Service Water & RHR Service Water are not normal release pathways for liquid effluents, no credit should be taken for possible dilution scenarios. All service water should be maintained below  $2\text{E-}5 \mu\text{Ci/cc}$  Cs-137 equivalent.

## 2.2 GASEOUS EFFLUENT MONITORS

SPECIFICATION 3.3.7.11 - THE RADIOACTIVE GASEOUS EFFLUENT MONITORING INSTRUMENTATION CHANNELS SHOWN IN TABLE 3.3.7.11-1 SHALL BE OPERABLE WITH THEIR ALARM/TRIP SETPOINTS SET TO ENSURE THAT THE LIMITS OF SPECIFICATION 3.11.2.1 ARE NOT EXCEEDED. THE ALARM/TRIP SETPOINTS OF THESE CHANNELS SHALL BE DETERMINED IN ACCORDANCE WITH THE METHODOLOGY AND PARAMETERS IN THE ODCM.

Noble gas activity monitors, iodine samplers, and particulate samplers are present on the reactor building ventilation system (Units 1 and 2), the turbine building ventilation system (Units 1 and 2), and the standby gas treatment system. Effluent system flow rate and sampler flow rate are measured on all of the systems allowing the vent monitor microprocessor to calculate release rates based on measured flow rates. Precautions, limitations, and setpoints applicable to the operation of the SSES gaseous effluent monitors are provided in the applicable plant Procedures. Setpoints are conservatively established for each ventilation effluent monitor so that the instantaneous dose rates corresponding to 10 CFR 20 annual dose limits in unrestricted areas will not be exceeded. Conservatism is to be incorporated into the determination of each setpoint to account for:

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1. All exposure pathways of significance at the critical receptor locations;
2. Dose contributions to critical receptors from multiple release points; and
3. Dose contributions from major radioisotopes expected to be present in gaseous effluents.

The general methodology for establishing plant ventilation gaseous effluent monitor setpoints is based upon vent release rates ( $\mu\text{Ci/sec}$ ) derived from site-specific meteorological dispersion conditions, vent flow rates, and expected radioisotopic mixtures in the gaseous effluents. The vent release rate can then be converted to cpm depending upon the particular monitor's method of operation, sampling rate, and detection efficiency. It is not practical to apply alarm/trip setpoints to integrating radiation monitors sensitive to radioiodines, radioactive materials in particulate form, or radionuclides other than noble gases. Therefore, only the noble gas activity monitors in the five ventilation systems at the SSES will have established setpoints.

The calculated alarm and trip action setpoints for each noble gas ventilation effluent monitor and flow measurement device must satisfy the following equation for whole body dose:

$$Q'_{iv} \leq \frac{500}{(K_1)(X/Q)_v} \quad (4)$$

and by the following equation for skin dose:

$$Q'_{iv} \leq \frac{3000}{(L_1 + 1.1 M_1)(X/Q)_v} \quad (5)$$

JAN 20 1984

where:

- $K_1$  = the whole body dose factor due to gamma emissions for each identified noble gas radionuclide (i) (mrem/yr per  $\mu\text{Ci}/\text{m}^3$ ) from Table 2.
- $Q'_{1v}$  = the release rate of radionuclide (i) from vent (v) which results in an annual dose rate of 500 mrem to the whole body or 3000 mrem to the skin of the critical receptor ( $\mu\text{Ci}/\text{sec}$ ).
- $(X/Q)_v$  = the highest calculated annual average relative concentration for estimating the dose to the critical offsite receptor in an unrestricted area from vent release point (v) ( $\text{sec}/\text{m}^3$ ).
- 500 = the 10 CFR 20 annual whole body dose limit (mrem/yr) to an individual in an unrestricted area.
- $L_1$  = the skin dose factor due to beta emissions for each identified noble gas radionuclide (i) (mrem/yr per  $\mu\text{Ci}/\text{m}^3$ ) from Table 2.
- $M_1$  = the air dose factor due to gamma emissions for each identified noble gas radionuclide (i) (mrad/yr per  $\mu\text{Ci}/\text{m}^3$ ) from Table 2 (conversion constant of 1.1 converts air dose-mrad to skin dose-mrem).
- 3000 = the 10 CFR 20 annual skin dose limit (mrem/yr) to an individual in an unrestricted area.

Xenon-135 should be the principal noble gas radionuclide released from the reactor building vents and the standby gas treatment system vent while Xenon-133 should be the principal noble gas radionuclide released from the turbine building vent due to the offgas holdup system. It is appropriate that these noble gas radionuclides be used as the reference isotopes for establishing the particular monitor setpoints. The whole body dose will be the most limiting and the release rate limit is calculated by substituting the appropriate values in Equation 4. After the release rate limit is determined for each vent, the corresponding vent concentration limits can be calculated based on normal vent flow rates:

$$\text{Setpoint } \frac{\mu\text{Ci}}{\text{cc}} = \frac{Q'_{1v} (\mu\text{Ci}/\text{sec})}{\text{Flow rate (cc/sec)}} \quad (6)$$

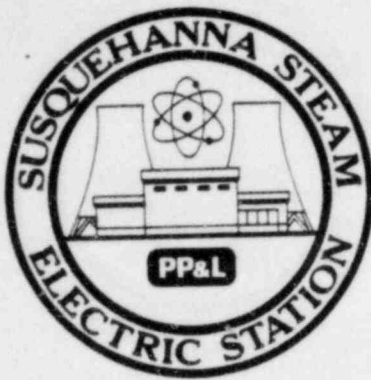
JAN 20 1984

Sample calculations for determining release limits for the whole body dose and the skin dose are given in Section A.1.2 of Appendix A. Also, typical values for flow rates and calibration factor are given for determining the setpoint of the Unit 1 turbine building vent gaseous effluent monitor.

Vent flow rates and sample flow rates are monitored and recorded for each of the five SSES release points. The measured flow rates are used to calculate vent concentrations and release rates. Flow channel setpoints are set at 10% and 90% of the calibrated sensor ranges to provide indication of possibly abnormal flow rates.

JAN 20 1984





# AVERAGE DAILY UNIT POWER LEVEL

DOCKET NO. 50-388

UNIT Two

DATE May 9, 1984

COMPLETED BY L.A. Kuczynski

TELEPHONE (717) 542-3759

MONTH April, 1984

DAY AVERAGE DAILY POWER LEVEL  
(MWe-Net)

1	<u>0</u>
2	<u>0</u>
3	<u>0</u>
4	<u>0</u>
5	<u>0</u>
6	<u>0</u>
7	<u>0</u>
8	<u>0</u>
9	<u>0</u>
10	<u>0</u>
11	<u>0</u>
12	<u>0</u>
13	<u>0</u>
14	<u>0</u>
15	<u>0</u>
16	<u>0</u>

DAY AVERAGE DAILY POWER LEVEL  
(MWe-Net)

17	<u>0</u>
18	<u>0</u>
19	<u>0</u>
20	<u>0</u>
21	<u>0</u>
22	<u>0</u>
23	<u>0</u>
24	<u>0</u>
25	<u>0</u>
26	<u>0</u>
27	<u>0</u>
28	<u>0</u>
29	<u>0</u>
30	<u>0</u>
31	<u>0</u>

## INSTRUCTIONS

On this format, list the average daily unit power level in MWe-Net for each day in the reporting month. Compute to the nearest whole megawatt.





# OPERATING DATA REPORT

DOCKET NO. 50-388  
 DATE May 9, 1984  
 COMPLETED BY L.A. Kuczynski  
 TELEPHONE (717) 542-3759

## OPERATING STATUS

Unit 2

1. Unit Name: Susquehanna Steam Electric Station
2. Reporting Period: April, 1984
3. Licensed Thermal Power (MWt): 3,293
4. Nameplate Rating (Gross MWe): 1,152
5. Design Electrical Rating (Net MWe): 1,065
- \*6. Maximum Dependable Capacity (Gross MWe): -
- \*7. Maximum Dependable Capacity (Net MWe): -

### Notes

\* To be determined.  
 Fuel load completed  
 April 13, 1984.

8. If Changes Occur in Capacity Ratings (Items Number 3 Through 7) Since Last Report, Give Reasons:

None

9. Power Level To Which Restricted, If Any (Net MWe): 0

10. Reasons For Restrictions, If Any: License restriction to 5% full power (164.6 MWt).

Turbine generator will not be synchronized at or below 5% power.

	This Month	Yr.-to-Date	Cumulative
11. Hours In Reporting Period	<u>0</u>	<u>0</u>	<u>0</u>
12. Number Of Hours Reactor Was Critical	<u>0</u>	<u>0</u>	<u>0</u>
13. Reactor Reserve Shutdown Hours	<u>0</u>	<u>0</u>	<u>0</u>
14. Hours Generator On-Line	<u>0</u>	<u>0</u>	<u>0</u>
15. Unit Reserve Shutdown Hours	<u>0</u>	<u>0</u>	<u>0</u>
16. Gross Thermal Energy Generated (MWH)	<u>0</u>	<u>0</u>	<u>0</u>
17. Gross Electrical Energy Generated (MWH)	<u>0</u>	<u>0</u>	<u>0</u>
18. Net Electrical Energy Generated (MWH)	<u>0</u>	<u>0</u>	<u>0</u>
19. Unit Service Factor	<u>N/A</u>	<u>N/A</u>	<u>N/A</u>
20. Unit Availability Factor	<u>N/A</u>	<u>N/A</u>	<u>N/A</u>
21. Unit Capacity Factor (Using MDC Net)	<u>N/A</u>	<u>N/A</u>	<u>N/A</u>
22. Unit Capacity Factor (Using DER Net)	<u>N/A</u>	<u>N/A</u>	<u>N/A</u>
23. Unit Forced Outage Rate	<u>N/A</u>	<u>N/A</u>	<u>N/A</u>

24. Shutdowns Scheduled Over Next 6 Months (Type, Date, and Duration of Each):

Maintenance Outage, 10/27/84, 7 weeks

25. If Shut Down At End Of Report Period, Estimated Date of Startup:

26. Units In Test Status (Prior to Commercial Operation):

INITIAL CRITICALITY  
 INITIAL ELECTRICITY  
 COMMERCIAL OPERATION

Forecast

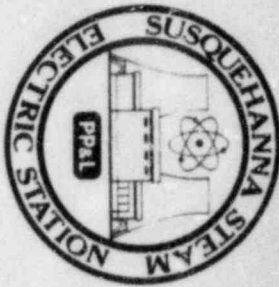
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05/09/84

05/08/84

06/07/84

12/31/84



# UNIT SHUTDOWNS AND POWER REDUCTIONS

REPORT MONTH April, 1984

DOCKET NO. 50-388  
 UNIT NAME Two  
 DATE May 9, 1984  
 COMPLETED BY L.A. Kuczynski  
 TELEPHONE (717) 542-3759

No.	Date	Type <sup>1</sup>	Duration (Hours)	Reason <sup>2</sup>	Method of Shutting Down Reactor <sup>3</sup>	Licensee Event Report #	System Code <sup>4</sup>	Component Code <sup>5</sup>	Cause & Corrective Action to Prevent Recurrence
None									

1 F: Forced  
S: Scheduled

2 Reason:  
A-Equipment Failure (Explain)  
B-Maintenance of Test  
C-Refueling  
D-Regulatory Restriction  
E-Operator Training & License Examination  
F-Administrative  
G-Operational Error (Explain)  
H-Other (Explain)

3 Method:  
1-Manual  
2-Manual Scram.  
3-Automatic Scram.  
4-Other (Explain)

4 Exhibit G - Instructions for Preparation of Data Entry Sheets for Licensee Event Report (LER) File (NUREG-0161)

5 Exhibit I - Same Source (9/77)

UNIT 2  
SUSQUEHANNA STEAM ELECTRIC STATION

Docket Number 50-386      Date May 9, 1984

Completed by L.A. Kuczynski      Telephone (717)542-3759

Challenges to Main Steam Safety Relief Valves

None.

Changes to the Offsite Dose Calculation Manual

None.

Major Changes to Radioactive Waste Treatment Systems

None.



# Pennsylvania Power & Light Company

Two North Ninth Street • Allentown, PA 18101 • 215 / 770-5151

Bruce D. Kenyon  
Vice President-Nuclear Operations  
215/770-7502

**MAY 11 1984**

Director, Data Automation &  
Management Information Division  
Attention: Mr. M. R. Beebe  
Management Information Branch  
Office of Resource Management  
U.S. Nuclear Regulatory Commission  
Washington, D.C. 20555

SUSQUEHANNA STEAM ELECTRIC STATION  
MONTHLY OPERATING REPORT  
ER 100450 FILE 841  
PLA-2195

Docket Nos. 50-387  
50-388

Dear Mr. Beebe:

The April 1984 monthly operating reports for Susquehanna SES Units 1 and 2 are attached.

Very truly yours,

B. D. Kenyon  
Vice President-Nuclear Operations

Attachment

cc: Dr. Thomas E. Murley  
Regional Administrator-Region I  
U.S. Nuclear Regulatory Commission  
631 Park Avenue  
King of Prussia, PA 19406

INPO Records Center  
Suite 1500  
1100 Circle 75 Parkway  
Atlanta, Georgia 30339

Director  
Office of Inspection and Enforcement  
U.S. Nuclear Regulatory Commission  
Washington, D.C. 20555  
Attn: Document Control Desk (12 copies)

Mr. Thomas E. Pollog  
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Resources  
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P.O. Box 2063  
Harrisburg, PA 17120

Mr. R. H. Jacobs - NRC  
Mr. R. L. Perch - NRC

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