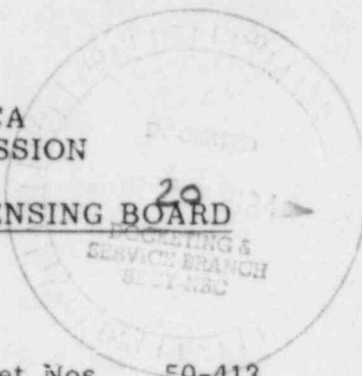


A-77
12/1/83

UNITED STATES OF AMERICA
NUCLEAR REGULATORY COMMISSION

BEFORE THE ATOMIC SAFETY AND LICENSING BOARD



In the Matter of)

DUKE POWER COMPANY, et al.)

(Catawba Nuclear Station,)
Units 1 and 2))

Docket Nos. 50-413
50-414

TESTIMONY OF RICHARD W. IRBY

1 Q. STATE YOUR NAME AND YOUR WORK ADDRESS.

2 A. Richard W. Irby, Catawba Nuclear Project, P.O. Box 223, Clover,
3 SC 29710.

4 Q. WHAT IS YOUR PRESENT JOB WITH DUKE POWER COMPANY?

5 A. I am a welding inspector - visual, MT, PT for Unit 1.

6 Q. SUMMARIZE YOUR EXPERIENCE AND QUALIFICATIONS, INCLUDING
7 OTHER NON-DUKE JOBS, EDUCATION, CERTIFICATIONS, AND
8 COMPANY SPONSORED COURSES AND TRAINING.

9 A. U. S. Navy retired after 20 years of service primarily in the area
10 of welding related activities. I have been working for Duke since
11 May 1977. I have been a welding inspector at Catawba since May
12 1978. I have a high school diploma, and an Associate Degree in
13 Industrial Management from York Tech in Rock Hill, South Carolina.

14 Q. WHAT OTHER JOB POSITIONS HAVE YOU HELD WITH DUKE POWER
15 COMPANY?

16 A. Welder.

17 Q. ARE YOU FAMILIAR WITH WHAT IS COMMONLY REFERRED TO AS
18 THE WELDING INSPECTOR CONCERNS WHICH WERE EXPRESSED IN
19 LATE 1981/EARLY 1982?

20 A. Yes.

8405240139 841201
PDR ADOCK 05000413
G PDR

1 Q. WHAT IS YOUR UNDERSTANDING OF WHAT THESE CONCERNS
2 WERE?

3 A. Written concerns by welding inspectors of technical and
4 administrative short comings in the QA Program (Catawba Project).

5 Q. DID YOU EXPRESS ANY CONCERNS AS A WELDING INSPECTOR TO
6 ANY OF THE TASK FORCES OR TO DUKE POWER MANAGEMENT?

7 A. Yes.

8 Q. TO WHOM DID YOU EXPRESS YOUR CONCERNS?

9 A. Task Force I, Technical Task Force, and Gail Addis.

10 Q. WERE YOUR CONCERNS WRITTEN?

11 A. Yes.

12 Q. DESCRIBE EACH DOCUMENT WHICH CONTAINS YOUR EXPRESSION
13 OF CONCERNS, AND INDICATE WHO IT WAS SUBMITTED TO.

14 A. My concerns were set forth in three document packages which
15 contained questions and concerns related to resolution of the
16 following three NCIs:

17 (1) Technical concern on resolution to NCI 13165 submitted
18 through QA Technical Recourse.

19 (2) NCI 9092 (defects of Unit 2 dome plate) submitted through Bob
20 Morgan and presented to the Task Force.

21 (3) NCI 12549 (defect in piping, Unit 1) submitted through Bob
22 Morgan and presented to Task Force.

23 Q. DID YOU FEEL FREE TO EXPRESS ALL OF YOUR CONCERNS?

24 A. Yes.

25 Q. DID YOU EXPRESS ALL OF YOUR CONCERNS?

26 A. Yes.

1 Q. HAVE YOU DISCUSSED YOUR CONCERNS WITH ANYONE ELSE?
2 A. Yes, with my supervisor, Beau Ross. My concerns were turned in
3 through the chain of command in the department.
4 Q. HAS ANYONE ELSE CONTACTED YOU AND ASKED YOU TO
5 DISCUSS YOUR CONCERNS?
6 A. Jan Liegnette, "60 Min." staff at home, by phone early July, 1983.
7 Q. DOES THE DOCUMENTS ATTACHED TO YOUR TESTIMONY AS
8 ATTACHMENT A, B AND C REFLECT ALL OF YOUR CONCERNS?
9 A. Yes.
10 Q. ARE ALL OF YOUR CONCERNS INCLUDED IN THESE DOCUMENTS?
11 A. Yes.
12 Q. PLEASE SUMMARIZE AND EXPLAIN WHAT YOU WERE TRYING TO
13 COMMUNICATE BY YOUR CONCERNS.
14 A. I was trying to get specific items corrected that in my judgment
15 was wrong by procedure or by technical nature. Important to me
16 was the inefficient processing of nonconforming items relating to
17 lack of support in the program. Decisions made were some time not
18 conducive to the program and yielded to the needs of an
19 overpowering construction element.
20 Q. WERE YOUR CONCERNS INVESTIGATED BY THE TASK FORCES?
21 A. Yes.
22 Q. DID YOU ATTEND ANY MEETINGS WITH TASK FORCE AND/OR QA
23 MANAGEMENT MEMBERS WHERE THE TASK FORCE FINDINGS,
24 CONCLUSIONS AND RECOMMENDATIONS WERE DISCUSSED?
25 A. Yes. One such meeting was a final meeting with Larry Coggins,
26 David Whitaker over technical concern (resolution) of NCI 13165. I
27 have attended other meetings but don't remember the details.

1 Q. WERE THERE ANY CHANGES MADE IN THE QA PROGRAM AFTER
2 THE WELDING INSPECTOR CONCERNS AND THE TASK FORCE
3 INVESTIGATION OF THESE CONCERNS?
4 A. Yes.
5 Q. DESCRIBE THE CHANGES OF WHICH YOU ARE AWARE IN THE QA
6 PROGRAM.
7 A. There were some changes in procedures and activities which
8 resulted in some improvements in the QA program.
9 Q. TO WHAT EXTENT HAVE THESE CHANGES ADDRESSED ISSUES
10 RAISED BY THE WELDING INSPECTOR CONCERNS? TO WHAT
11 EXTENT HAVE THESE CHANGES ADDRESSED YOUR PARTICULAR
12 CONCERNS?
13 A. In that I am unaware of all the concerns expressed by other
14 inspectors, I do not know how these changes affected their
15 concerns. With respect to my concerns, the task force addressed
16 and resolved each concern.
17 Q. THE WELDING INSPECTOR CONCERNS HAVE BEEN
18 CHARACTERIZED AS CONCERNS ABOUT THE QUALITY AND
19 SAFETY OF CONSTRUCTION AT CATAWBA. DO YOU AGREE OR
20 DISAGREE WITH THAT CHARACTERIZATION?
21 A. Disagree, I think the topic of concerns has been strongly or over
22 characterized. Generally speaking, over a period of time quality
23 has been sacrificed to some degree but not to the point of
24 quality/safety dangers.

1 Q. DID THE EXPRESSION OF YOUR CONCERNS INDICATE YOUR
2 BELIEF THAT THERE WAS A BREAKDOWN IN THE QA PROGRAM
3 OR INDICATE THAT THE QA PROGRAM WAS NO LONGER
4 WORKING?

5 A. There was no breakdown in the QA program so as to affect safety.
6 However, there was a breakdown as it affected the manner in which
7 technical matters and NCI resolutions were handled.

8 Q. DID YOUR CONCERNS REFLECT A BELIEF ON YOUR PART THAT
9 THE CATAWBA PROJECT IS NOT BEING CONSTRUCTED SAFELY?

10 A. No.

11 Q. IN YOUR VIEW, HAS THE QA PROGRAM BEEN EFFECTIVE WHILE
12 YOU HAVE WORKED AS AN INSPECTOR AT CATAWBA?

13 A. Effective, with exceptions which have been listed through different
14 individuals.

15 Q. ARE YOU AWARE OF ANY DEFICIENCIES IN CONSTRUCTION IN
16 THE QA PROGRAM WHICH WOULD CAUSE YOU TO QUESTION
17 WHETHER CATAWBA IS SAFELY BUILT?

18 A. No.

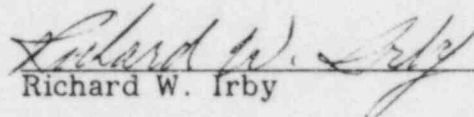
19 Q. IS THERE ANYTHING ELSE YOU WOULD LIKE TO ADD TO YOUR
20 TESTIMONY?

21 A. Yes. I feel that my concerns, each in a unique way, touch a broad
22 level of expertise and management (ranging from Catawba through
23 the Charlotte office). The handling and solutions to my concerns

1 (prior to the task force review) clearly characterize (not a
2 breakdown) but a lack of concern for practical, efficient working
3 solutions.

4
5
6
7 I hereby certify that I have read and understand this document, and
8 believe it to be my true, accurate and complete testimony.

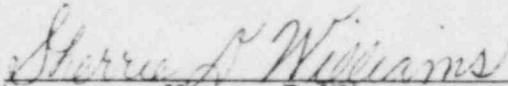
9
10
11
12


Richard W. Irby

13
14

15 Sworn to and subscribed before me
16 this 22nd day of September, 1983.

17
18
19
20


Notary Public

21

22 Commission Expires March 7, 1993

UNIT 21, 22, 23
NONCONFORMING ITEM REPORT
USE BLACK BALL POINT PEN ONLY

CA Required ☒ Yes ☐ No
Condition 1
Date 10-15-81
NC Item ☐ NC Item
Other ☐ Other
Not Filled ☐ Not Filled

Location of Item

FPM. CLASH 187° - 555

Serial No.

13165

Description of Item and Statement of Problem

During nonstop inspection of weld # INV 193-30 on air line was discovered taped in the end of the section being placed (approximately 24") surrounding a rapid cooling process of the welded joint. This process was done without speed control + controlled methods. There is question over the rate of cooling. The molten metal contact of the air + the compressed air addition to the assembly. (An additional 0.1A to additional mold pressure)

Evaluation/Disposition Responsibility

☒ Const☐ Design☐ QA☐ Steam☐ Group

CW

Original

Date

Technical Review

Date

CA Review

Date

10-15-81 10-15-81 10-15-81 10-15-81

Potentially Reportable Under 10CFR21/50.55a

☐ Yes☒ No

If yes, use Form 290.1

Disposition/Justification

2 PART RESOLUTION - IT IS WELDING TECH. SUPPORTS DESIGN THAT THIS IS AN ACCEPTABLE T-MANUE WHEN USED ON STAINLESS STEEL JOINTS SUCH AS THE ONE IN QUESTION. THE AIR FLOW THROUGH THE PIPE HAS A DETRIMENTAL EFFECT ON THE WELD JOINT. NO SPECIAL PROCESS CONTROL IS NECESSARY FOR THE USE OF THIS TECHNIQUE AS IT VIOLATES NO CODE OR PROCEDURE. CONSTRUCTION ENGINEERS SYSTEMS SHALL EVALUATE THIS TECHNIQUE FOR INTERNAL CIRCULATED PROBLEMS AND FOR REPORTABILITY.

(SEE SHEET 2 OF 2 ATTACHED)

Spec/Calc/Dwg Revised As Below

PR-202 Applicable (Design Only) ☐ Yes ☒ No

By

Date

Technical Approval

Date

CA Approval

Date

11-10-81

T.H. Robertson

11/10/81

H.L. HICKS

11/14/81

CORRECTIVE ACTION/INSPECTION REQUIRED

Assigned To

Performed By

Date

SEE SHEET 2 OF 2 ATTACHED

1. INSTRUCT POWERHOUSE MECHANICS NOT TO USE RAW CONSTRUCTION AIR TO BLOW OUT LINES OR VALVES WHICH HAVE BEEN CLEANED. FILTERED AIR OR INSTRUMENT AIR MAY BE USED.
(CONTINUED ON SH. 2 OF 2 ATTACHED 17-54)

PHST.

By Glenn Ginnell

Date

CA Approval

Date

17-15-81

H.L. HICKS

1/4/82

Action/Inspection Exceptions or Remarks

Distribution

GEN. SUPV

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1

Trend Info.

Final QA Review

Date

UNIT = 1, = 2, = 3
NONCONFORMING ITEM REPORT
USE BLACK BALL POINT PEN ONLY

Is Fabricated: ☐ Yes ☐ No
Condition: _____
Date: _____
Identification Method: ☐ G-IB'S ☐ Other ☐ Not Fabricated
CNC I Tape: ☐

Location of Item: _____

Serial No.

13,165

Description of Item and Statement of Problem

The air lines contained oil contaminants were observed during the pipe assembly at this time.
H.W. Smith
10-27-81

Evaluation/Disposition Responsibility

☐ Const ☐ Design ☐ QA ☐ Steam ☐ Group

Original Date: *10-27-81*

Technical Review

Date

QA Review

Date

Potentially Reportable Under 10CFR21/50.55e

☐ Yes ☒ No

If yes, use Form 290.1

10-27-81

Disposition/Justification: *(UN)ACCEPTABLE. OIL CONTAMINANT IN STAINLESS PIPING (IN PARTICULAR, DEMIN. WATER SYSTEMS) IS A VIOLATION OF CNS-1206.00-02-1007, APPENDIX N, PIPING INTER-PIES TO ANY WORK PERFORMED ON A CLEAN SYSTEM. IN ADDITION, INTRODUCTION OF OIL CONTAMINANTS INTO ANY EXISTING PIPING IS A VIOLATION OF N-14. ALTHOUGH THERE APPEARS TO BE NO QA OR CODE REQUIREMENTS AGAINST THE WELDING TECHNIQUE, FOR THE ABOVE REASONS RAW CONSTRUCTION AIR SHOULD NOT BE USED. EITHER FILTERED CONSTRUCTION AIR OR INSTRUMENT AIR MAY BE USED WITH REGARD TO THE GENERAL ASPECTS OF THIS PROBLEM, SAN-ANTS DOCUMENT THAT CONTAMINANTS ARE REMOVED; THIS ELIMINATES CONCERN THAT CONTAMINANTS INTRODUCED INTO PIPING AS A RESULT OF THIS TECHNIQUE MIGHT REMAIN IN PIPING.*

Spec/Calc/Dwg Revised As Below

By: *Alum Connell*

Date

Technical Approver

Date

PR-202 Applicable (Design Only) ☐ Yes ☒ No

QA Approval

Date

CORRECTIVE ACTION/INSPECTION REQUIRED

Assigned To

Performed By

Date

INSTRUCT WELDERS NOT TO USE RAW CONSTRUCTION AIR FOR THIS TECHNIQUE. STRESS IMPORTANCE OF USING EITHER INSTRUMENT OR FILTERED CONSTRUCTION AIR.

PRMR

REMOVE Q-IB TAG

12/4/81

SVTW

Attach a copy of this NCI to the process control.

CEWL

DR Smith 12/4/81
THR

By: *Alum Connell*

Date

QA Approval

Date

Action/Inspection Exceptions or Remarks

Distribution	GEN. SUPT	Sr. Const Engr	Con. Eng	Proj. Eng	QA Eng	WHSE SUPV	QA Div	ANI	NBC
Number Of Copies	Initial								
	Final								
Trend Info.									
Final QA Review								Date	

Additional Resolution to NCI # 13,165

The introduction of air to the internal weld surface solution anneals the weld joint. This actually provides a higher quality weld. This is due to the fact that the weld material spends less time in the 800 - 1600°F range, thus decreasing the amount of sensitization that occurs. As the cooling mechanism was used after deposition of the initial deposition of the initial fill passes, the root had solidified; thus moisture in the air would evaporate and not contaminate the root as it was not in a molten state. Per conversation with Construction Services a statement in will be added in the current revision to L-200, L-300, and L-500. It will state that filtered construction air or instrument air may be used to accelerate cooling when properly authorized.

The weld in question is acceptable and shall remain as is. A copy of this NCI shall be attached to the process control.

DH Kennedy 12/4/81

T.H. Robertson 12/4/81

HL Hines 1/4/82

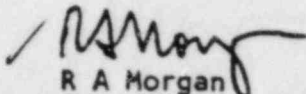
January 11, 1982

J R Wells
L R Davison

Re: Catawba 1-2
Management Procedure 8030-0003
Resolution of Technical Matters

We have an inspector R.W. Irby who has a technical concern on resolution to nonconforming item Serial Number 13165. This nonconformance was evaluated technically by the Catawba Project Technical Support welding group and approved by the QA Technical Group January 4, 1982.

Attached are Mr. Irby's concerns and a copy of Q-1A 13165.


R A Morgan
Project QA Engineer

Attachments

Reasons that I feel the weld in question is rejectable and should be replaced.

Unknown Factors such as - temperature ranges during time of welding and at time of air injection?

Rate of Cooling?

The possible inducement of oil and moisture into the weld joint?

Up setting of the chemical balance of weld deposit and parent metal?

This nonconformance should be addressed entirely from a metallurgy view point and not as a cleanliness problem.

The additional resolution made note of the time factor of the weld deposit and surrounding metal in the critical temperature range (800 - 1600 degrees). This factor is true in respect to sensitization of the metal however accelerated cooling is not an approved method to correct this.

Correct application of the FWDS and following process specification will eliminate the problem of too much time in the critical temperature range. In regard to annealing of the weld joint, this process implies a slow rate of cooling and not an accelerated rate of cooling.

This question may not be technical, but why did the welder apply this method and why do current changes in the process specification (1-4-82) approve of this method that took place on (9-26-81).


R W Irby
Welding Inspector

DUKE POWER COMPANY

ELECTRIC CENTER, P.O. BOX 33189, CHARLOTTE, N.C. 28242

GEORGE W. GRIER
CORPORATE QUALITY ASSURANCE MANAGER

TELEPHONE
(704) 373-4022


February 19, '1982

R W Irby

Re: Catawba 1-2
Resolution of Technical Matters
Your concern dated January 11, 1982

The resolution of the referenced technical concerns from a metallurgical viewpoint is answered in the attached memo to file and will be explained further to you by D E Whitaker, S H Van Malssen, and L M Coggins. The conclusion is that the weld quality is not jeopardized.

As you also know, there was a question as to whether the practice employed was actually quenching, which led to different conclusions regarding whether or not procedures were violated. My feeling is that there was no intent by people resolving the NCI to approve action in violation of the procedure. It is apparent that a better solution would be arrived at by recognizing that the action was not authorized beforehand in the proper manner and, separately, the individuals concerned will be instructed in future resolutions of this type.


G W Grier
Corporate QA Manager

GWG/ph

MEMO TO FILE

SUBJECT: Response to R. W. Irby's request for a 'Resolution of Technical Matters Involving Differences of Opinion' Involving NCI Serial No. 13165
File No. K-1

The 'Description of Item and Statement of Problem' from NCI Serial No. 13165" reads as follows:

"During random inspection of Weld No. INV 193-30, an air hose was discovered taped in the end of the section being joined (approximately 24") providing a rapid cooling process of the welded joint. This process was applied without approved process control and controlled methods. Items in question are the rate of cooling, the moisture and oil content of the air, and the cleanliness. condition of the assembly (see attached QA for additional note) (RWI 10-27)."

Mr. Irby also expressed his concerns in a memo dated January 18, 1982 and in an attachment to a memo from R. A. Morgan to J. R. Wells and L. R. Davison dated January 11, 1982. The concerns are as follows:

January 18, 1982: "My concerns involve specific technical matters and the efficient processing of non-conforming items, relating to lack of support in the program. I would like to point out short comings in decision making and proper research (to specific NCI resolution) that is not conducive to the program and not restricted to Catawba alone."

January 11, 1982:

- "Reason that I feel the weld in question is rejectable and should be replaced.
- Unknown factors such as temperature ranges during time of welding and at time of air injection?
- Rate of cooling?
- Up setting of the chemical balance of weld deposit and parent metal?
- This non-conformance should be addressed entirely from a metallurgy viewpoint and not a cleanliness problem.

- The additional resolution (signed by D. W. Llewellyn, T. H. Robertson, H. L. Atkins) made note of the time factor of the weld deposite and surrounding metal in the critical temperature range (800-1600 degrees). This factor is true in respect to sensitization of the metal; however, accelerated cooling is not an approved method to correct this. Correct application of the FWDS and following process specification will eliminate the problem of too much time in the critical temperature range. In regard to annealing of the weld joint, this process implies a slow rate of cooling and not an accelerated rate of cooling.
- This question may not be technical, but why did the welder apply this method and why do current changes in the process specification (January 4, 1982) approve of this method that took place on September 26, 1981."

This response will cover the technical questions concerning the weld rather than those concerning how the NCI was handled. Also, it is assumed that the concern for cleanliness of the system has been answered satisfactorily.

The rate of cooling of welds can effect material properties by determining temperature gradients, metallurgical structure, and amount of hydrogen retained in the weld. Temperature gradients or change of temperature across a thickness of material coupled with lower yield strength at high temperatures and thermal expansion result in the residual stress. Generally speaking, the higher the thermal gradient the higher the residual stress. For example, residual stresses close to welds where the thermal gradient is the highest are generally considered to be at or close to the yield point. In the postweld heat treatment to relieve stresses, there are rules governing the width to be covered by the blankets and the rate of cooling so that new residual stresses will not be introduced. The Procedure Qualification's Materials tests are used to prove the amount of residual stress induced is not detrimental; with heat input, preheat, interpass temperature and material thickness being the parameters controlling cooling rate. In order to determine whether accelerated cooling of the interior of the pipe affected the integrity of the weld in question, three facts should be taken into account.

First, the weld (a socket weld) was on the opposite wall of the pipe (0.343" thick) from the circulating air. Second, 304 stainless steel is a ductile material with an elongation of 55 percent in the annealed condition. Third, circulating air is not a severe quench as shown in Table 1. A faster cooling rate than circulating air could be produced by an increase in the thickness of the pipe. Thickness is not a limiting factor for fillet welds on P8 material.

	Air	Oil	Water	Brine
No circulation of fluid or agitation of piece	0.02	0.25 to 0.30	0.9 to 1.0	2
Mild circulation (or agitation)		0.30 to 0.35	1.0 to 1.1	2 to 22
Moderate circulation		0.35 to 0.40	1.2 to 1.3	. . .
Good circulation		0.4 to 0.5	1.4 to 1.5	. . .
Strong circulation	0.05	0.5 to 0.8	1.6 to 2.0	. . .
Violent circulation		0.8 to 1.1	4	5

Table 1. Severity of Quench (H) for Various Quenching Media (Grossmann & Bain)

For these reasons, I do not think the properties of the weld were effected due to an increase in residual stress.

The metallurgical structure can also be affected by the cooling rate. The most notable example of this occurs in carbon and low alloy steel where the cooling rate at the time of transition between a Face Center Cubic Structure to that of a Body Center Structure determines whether perlite, bainite or martensite is formed. Type 304 stainless steel is an austenitic material and does not undergo this transformation and is therefore not hardenable by heat treatment. The metallurgical structure of this material is affected by cooling rate due to the formation of chromium carbides between the temperature range of 550°C and 850°C. The formation of carbides is rate dependent allowing sensitization to be avoided by cooling at a fast rate between these temperatures. It should be noted that too fast a cooling rate at high temperature in stabilized stainless steel (Type 321 and 347) can lead to a problem known as knife line attack. I would therefore conclude that the effect of increasing the cooling rate on sensitization would be beneficial.

Quenching metal after welding can increase the probability of hydrogen cracking in carbon and low alloy steel by slowing down the diffusion rate of hydrogen and by adding to the residual stress. This is not a problem with 304 stainless steel which is an austenitic material and not susceptible to hydrogen cracking.

In welding stainless steel joint cleanliness is extremely important. Small amounts of impurities can cause hot cracking or sensitization of the weld metal. Hot cracking is caused by the presence of small amounts of low melting point constituents to the weld metal such as lead or sulfur. Sensitization would be caused by the addition of carbon. Both carbon and sulfur are present in oil but in the case in question the air was not used until after the first pass which sealed the pipe. Another possibility which was looked into was the diffusion of carbon from oil on the inside of the pipe. The idea was discounted or considered superficial due to the short period experienced by the I.D. of the pipe at temperatures which carburizing would take place. Figure 1 and Figure 2 show the relation between time, temperature, percent carbon, and distance below the surface for 1020 during liquid carburizing and 3115 steel during pack carburizing respectively.

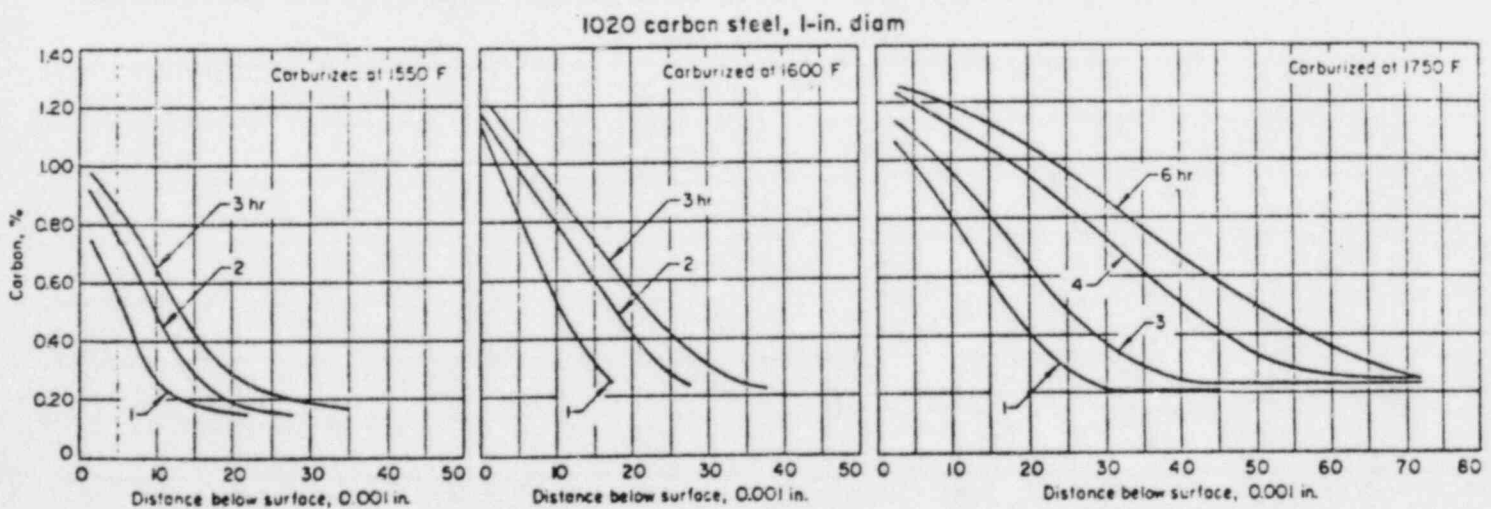


Figure 1. Effect of duration of liquid carburizing on 1020 steel
(ASM Handbook, 8th Edition, Vol. 2)

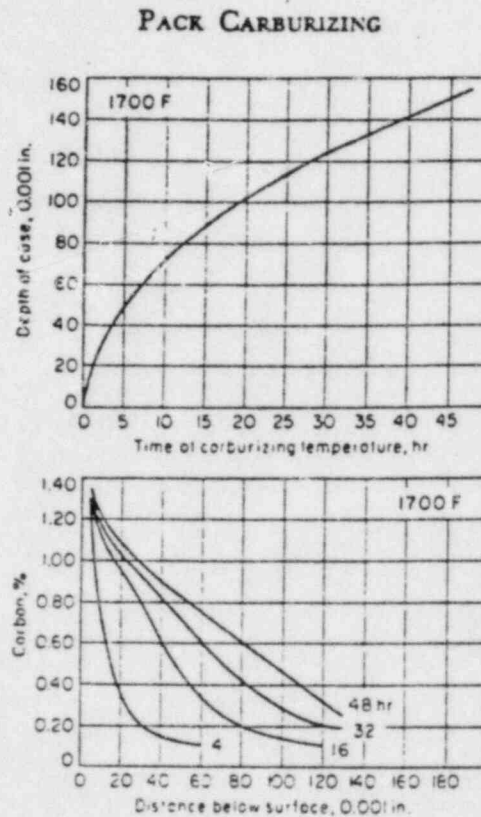


Figure 2 Effect of duration of pack carburizing on 3115 steel
(ASM Handbook, 8th Edition, Vol. 2)

Stating that the weld is technically sound does not mean that Mr. Irby's concerns were not legitimate. I especially agree with his point of view that the FWDS is the vehicle for insuring that sensitization does not occur. Also, I would like to point out that although quenching was not a problem with 304 stainless steel, it could very well be for carbon and low alloy steel. The cooling rate is one of the determining factors for whether preheat or postweld heat treatment is needed for different thickness.

David E. Whitaker
David E. Whitaker
Assistant Engineer

G.O. 373-7602

VERIFICATION-INDIVIDUAL CONCERN

FILE NO. K-1

I concur with the conclusions made by D.E. Whitaker. The following additional points should be made:

1. There was some question as to whether the method being used by the welder was actually "quenching." The use of forced air is quenching; and, therefore, the welder was in violation of the process specification at the time he used the method.
2. Further support that quenching of stainless steel weldments is acceptable is provided by the fact that this method is frequently used to change the nature of residual stresses in pipe welds. In heat sink welding, the root pass is made and then the pipe is filled with water or a jet of water is sprayed on the root ID during subsequent welding in order to change the stresses from tensile to compressive on the root ID, which eliminates the possibility of stress corrosion cracking.

SIGN-OFF

VERIFICATION

PERFORMED BY:

NM Loggins

DATE:

1-15-82

QA/QC INQUIRY

RECORD COPY

SERIAL # 46

STATEMENT OF PROBLEM OR INQUIRY :

During random inspection of weld # INV 193-30 an air hose was discovered taped in the end of the section being joined (approximately 24") providing a rapid cooling process of the weld joint.

By telephone conversation with Rob Atkins (QA Tech) (Charlie Terrell & Billie Smith) at 8:05 AM verbal approval was given to complete the weld & for Q.C. inspector to sign final visual per L-80.

R. Atkins QC welding 9-26-81
INSPECTOR/TECHNICIAN DATE

EVALUATION :

BLOWING AIR THROUGH THE I.D. OF A STAINLESS STEEL SOCKETWELD JOINT DURING THE WELDING PROCESS does NOT VIOLATE THE 200 PROCESS.

"Quenching" AS DESCRIBED & RESTRICTED by the 200 PROCESS REFERS TO ~~THE~~ ACCELERATED COOLING USING A LIQUID COOLING METHOD.

The incident described above IS ACCEPTABLE AS IS

When encountering a similar situation the inspector should assure that ALL cleanliness REQS ARE NOT VIOLATED.

R. Atkins 9/30/81
QA TECH GROUP DATE

[illegible]

CONNECTION ACTION

Observation of beam and Structure C' Problem When called for circumferential inspection
on weld # INC 54-7 it was observed that weld # INC 54-7
(and made visible to the other) also showed penetration
+ cracks in the root pass.

This weld has been accepted by radiography and judged to meet the requirements of NB4424(e) for internal root weld conditions. In addition, the radiographs were reevaluated and judged acceptable by the Level III radiographer. Radiography is the Code specified examination method. Therefore this weld meets Code requirements and shall remain. Future instances of weld interior surfaces becoming accessible when the weld has been examined and accepted by radiography are not required to be visually inspected.

W/IT - (2) SEE ATTACHMENT #3
PR-200 Applications (Design Only) ☐ Yes ☐ No
D. Andrews 8/27/81 Ch. H. Loring 8-27-81 W. Henry 8/27/81

[illegible]

By	Date	Cat Address	Date

Action/Exception/Exception or Remarks

Distribution		DATE	By	Class	Class	Project	OC Item	On Site	Other	OC Item	On Site	Other	AMT	UTC	
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Material <i>NA</i>	Material <i>NA</i>
Class <i>INC</i>	Material <i>NA</i>

DURETOWER COMPANY
STATION/PROJECT *CATAWBA*
UNIT ☒ 1, ☐ 2, ☐ 3
NONCONFORMING ITEM REPORT
USE BLACK BALL POINT PEN ONLY

QA Required <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No	Class <i>A</i>	Identification Method <input checked="" type="checkbox"/> O-18'S <i>2</i> <input type="checkbox"/> NCITape <input type="checkbox"/> Other <input type="checkbox"/> Not Practical
Condition <i>2</i>		

Location of Item <i>RD 1 RBB 80-564</i>	Serial No. <i>12549</i>
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Description of Item and Statement of Problem *when called for clean-up inspection on weld # INC 56-7 it was discovered that weld # INC 56-8 (id made visible by cut out) shows excessive porosity + sugar in the root pass.*

Evaluation/Disposition Responsibility	<input type="checkbox"/> Const	<input type="checkbox"/> Design	<input checked="" type="checkbox"/> QA	<input type="checkbox"/> Steam	<input type="checkbox"/> Group	<i>QT</i>
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Originated <i>DER</i>	Date <i>8-24-81</i>	Technical Review <i>CRB</i>	Date <i>8-25-81</i>	QA Review <i>JC</i>	Date <i>8-26-81</i>
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Potentially Reportable Under 10CFR21/50.55a	<input type="checkbox"/> Yes <input type="checkbox"/> No	If yes, use Form 290.1
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Disposition/Justification

Spec/Calc/Dwg Revised As Below

By	Date	Technical Approval	Date	QA Approval	Date
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CORRECTIVE ACTION/INSPECTION REQUIRED				Assigned To	Performed By	Date
<i>REMOVE G-18 TAG AND CONTINUE INSPECTION ON WELD INC 56-7</i>				<i>SUTW</i>	<i>D.E. R...</i>	<i>8-31-81</i>

By <i>B.L. ...</i>	Date <i>8-28-81</i>	QA Approval <i>JC</i>	Date <i>9-9-81</i>
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Action/Inspection Exceptions or Remarks

Distribution	GEN. SUPT	Sr. Const Eng	Const Eng	Project	QC Supv	QA Eng	WHSE	DESIGN QA Dir	ANI	NEC	Inspector
Number Of Copies	Initial <i>2</i>										
	Final <i>2</i>										
Trend Info.	Final QA Review <i>[Signature]</i> Date <i>9/1/81</i>										

SKIPPED BY MISTAKE (see 2/1/81)

CONSTRUCTION REC'D DATE SEP 10 1981

PROBLEM STATEMENT

EVALUATION

CORRECTION ACTION

②
The radiographs of this weld were reevaluated and the internal surface was also investigated visually. Based on the reevaluation, this weld is judged to be acceptable to the requirements of the Code.

② J. Lander 9/4/81 ② M. Luzzini 9/4/81 ②
② W. J. King 9/4/81

How can RT override a visual insp.

~~judgment was~~

- whether or not the weld in question was subject to oxidation was a judgment call - this should ~~not~~ be backed up by radiograph
- radiography is subject to human error and a number of factors can contribute to a defect being shown, see attachment 1.

* sugar or oxidation that has not completely broken out will not show up on RT

*** the absolute fact is that the defect is still in the pipe

other factors in this case need to be considered - ~~to~~ due to nature & significance of exp.

- possible stress corrosion.
- trap or pocket for radioactive accumulation causing hot spots.
- flow resistance
- possible corrosive action takes place.

*** the weld should be viewed on more practical basis - even with the overriding decision by the Level III radiography the NCI could have had a greater satisfaction by buffing or

5
grinding the ^{internal} surface of the pipe.

after all the joint in question was serviceable.

CONSTRUCTION NEED D

25578 (2-1-80)

Form Q-1A		Revision 10	
RECORD COPY DUKE POWER COMPANY CONSTRUCTION DEPARTMENT PROJECT <u>CATAMBA 1</u> NONCONFORMING ITEM REPORT USE BLACK BALL POINT PEN ONLY			
1. Requisition No.	2. Vendor/Location	3. Documents Violated	4. Serial Number
<u>NA</u>	<u>NEWPORT NEWS</u>	<u>CUS 1144.09-1</u>	<u>9092</u>
5. MFS PO No.	6. Mech/Elec System	7. QA Required	8. Identification Method
<u>NA</u>	<u>NA</u>	<input checked="" type="checkbox"/> Yes <input type="checkbox"/> No	<input type="checkbox"/> Q-18's <input type="checkbox"/> NCI Type
9. Location of Item	10. Description of Item and Statement of Problem	11. Evaluation/Disposition Responsibility	12. Date
<u>RR 2 (ROME)</u>	<u>ROBLINE INSPECTIONS OF CONTAINMENT PLATE (ROME) RRR REVEAL A NUMBER OF PLATES TO BE AILED AND HAVING A ROO SURFACE FINISH. IN GENERAL THE DEFECTS RANGE FROM SMALL SCATTERED PITS (WITH A DEPTH OF 1/32 X 3/4 IN DIA.) TO LARGE CONCENTRATIONS.</u>	<input type="checkbox"/> Const. <input checked="" type="checkbox"/> Design <input type="checkbox"/> QA <input type="checkbox"/> NSSS Div. Culler <input checked="" type="checkbox"/> DC	<u>2-3-80</u>
13. QA Required	14. Evaluation/Disposition Responsibility	15. Senior Eng. Review	16. Date
<input checked="" type="checkbox"/> Yes <input type="checkbox"/> No	<input type="checkbox"/> Const. <input checked="" type="checkbox"/> Design <input type="checkbox"/> QA <input type="checkbox"/> NSSS Div. Culler <input checked="" type="checkbox"/> DC	<u>2-3-80</u>	<u>8-4-80</u>
17. Disposition	18. Report to Management	19. QA Approval	20. Date
<u>AS STATED BELOW</u>	<input type="checkbox"/> Yes <input checked="" type="checkbox"/> No	<u>W. H. H. H.</u>	<u>9/13/81</u>
NOTE: DEFECTS ARE APPARENTLY MAXIMIZING DEFECTS. WORK MAY CONTINUE DURING EVALUATION OF PLATE PLATES 84100 ALL PITS LESS THAN OR EQUAL TO 1/8 INCH IN DEPTH SHALL BE GROUND SMOOTH AND BLENDED INTO ADJACENT MATERIAL. PITS WITH A DEPTH GREATER THAN 1/8 INCH SHALL BE WELD REPAIRED ACCORDING TO ASME PROCEDURES. MT OR PT GROUND AREAS AND WELD REPAIR AREAS. FOR ADDITIONAL EVALUATION SEE ATTACHMENT (1). (SEE ATTACHMENT (2) FOR EVALUATION OF VENDOR QA. NEW 11/1/81) - ALSO FOR S. R. QA <u>R.F. Vance</u> 7-28-81 <u>D.E. DeMark</u> 8-27-81 <u>W. H. H. H.</u> 9/13/81 21. QA Approval Date 22. Action/Inspection Required 23. Assigned To 24. Performed By 25. Date			

CONSTRUCTION REC'D DATE SEP 21 1981

DEC 02 1981

DEC 12 1981

[illegible]

Attachment (1) to NCI 9092

Surface defects are judged not to be significant based on engineering judgement gained by prior experience in containment vessel and pressure vessel design.

Site QA and QA Vendor surveillance shall address and evaluate why defects were not discovered during shop inspection and receiving inspection.

Repairs to be done in accordance with Section III, Subsection NE, of the ASME Code.

D.E. DeKort 8-24-81 R.F. Vause/DED 8-24-81

Attachment (2) to NCI 9092

Response to Attachment (1) to NCI 9092

Vendors supplying safety-related materials or components have an approved QA Program. This program includes QC and inspection that we are confident is satisfactory. Duke Power QA performs surveillance on their program to maintain a good confidence level. The surveillance does not include 100% inspection of the material or component. Minor or extremely small irregularities can go unnoticed depending on inspection or NDE requirements. Shipping damages and normal oxidation are factors to consider in reviewing the containment plate.

JM Carter 9-1-81

say nothing & pass it on to receiving

FAB # W1-3 DESCRIBES THE REQUIRED RECEIVING INSPECTION FOR CONTAINMENT PLATE. THE INSTRUCTIONS state: "IF there is any damage or any question of damage... contact The Const. Engineer Welding." These instructions seem adequate. It appears that these defects were missed due to the small nature of the indications. This does not appear to be a general or recurrent problem. No training or program revisions are required.

HCA/TK 9/21/81
SITE MA

Attachment (3) to NCI 9092

This attachment provides additional guidance to the resolution of original NCI dated 7-28-81.

Surface defects have already been judged not to be significant based on engineering judgement (see attachment (1)). This attachment provides additional criteria for the surface preparation and inspection of pitting and surface roughness less than or equal to 1/8 inch in depth.

- has been RNB 11/17/81 DED 11/17/81 TE 11/17/81*
- The containment dome plate ~~shall be~~ sand blasted to a "white metal surface" in accordance with Surface Preparation Procedure DPSP5-1. This process ~~will~~ *has* removed ~~remove~~ all surface foreign debris, scaling, rusting, etc. to sound metal. *RNB 11/17/81 DED 11/17/81 TE 11/17/81*
- ASTM A20, paragraph 9.2.1.1, requires all imperfections to be removed to sound metal and to be well faired. Procedure MSS SP-55 shall be used as a guide to determine well faired conditions. Type II, Type VII and Type VIII photographs shall be used for representative acceptable surfaces.
- All pits greater than 1/8 inch in depth shall be weld repaired in accordance with ASTM A20, paragraph 9.4.

By:

Richard H. Bengel

11/4/81

RNB 11/9/81

Technical Approval:

D.E. Schast

11/4/81

QA Approval:

TC Roberts

11-7-81

Terms of concern in question is regard to efficient handling in the support & resolution of NC1 9092

we will be
in office &
more of our plates

To be concerned prior to NC1
• external instructions were to follow criteria of
CP-64 which does not apply in full to this problem.
• const. tech. suppl. welding (David Liddell) told me
that if Duke Power representative in New Port News,
via, accepted the plates they were not as far as he
was concerned.

* Attachment 1. to NC1 judged surface defects not to
be significant — to my knowledge no one has
ever casually inspected the plates he asks Rick
Lance (1-12-82 representative from Charlotte office)
18 mos. from NC1 initiation

Attachment 2. relates to engineering judgment based on
prior experience and Duke Power QA surveillance of
welder supply. Minor or extremely small irregularities
can go unnoticed and shipping damages & normal
oxidation are factors to consider.

* * * Everyone writes something in response to NC1 9092
but does not address the point. L. H.

Attachment 3. once again, the surface defects have been judged not to be significant but why is repair work prescribed?

- make decisions to correct the defects but may be questionable.
- all defect removal to sound metal & well faired conditions may be detrimental to plate as far as required thickness.
- procedure 1955 5455 was issued only after NC1 was sent back for further evaluation.
- present surface conditions of some plates exceed the acceptable criterion shown in photographs in 5455

Questions of Support

why did this issue have to be found?

Why an over extended time frame (16 mos) with a questionable resolution 7-31-80 — 12-2-81 ?

why so much correspondence & explanation & no one addresses the problem?

Why did the proper initiative in search & solution not be put forth at the introduction of NC1 9:92?

*** why or how were all decisions made without someone in authority physically making an examination of the plate in question. (2)

why we could not have been removed
immediately or soon after instruction; during
the time of erection while many plates were
still on the ground?

Knowing these questions cannot be answered, ~~but~~ what
I want to point out is the

how it would
write something about it
and say it is of

attitude

This needs to be checked