

# CASE

(CITIZENS ASSN. FOR SOUND ENERGY)

March 29, 1984

RELATED CORRESPONDENCE

1426 S. Polk  
Dallas, Texas 75224

214/946-9446

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BRANCH

David R. Pigott, Esq.  
Orrick, Herrington, & Sutcliffe  
600 Montgomery Street  
San Francisco, California 94111

Dear Mr. Pigott:

SUBJECT: In the Matter of  
Texas Utilities Electric Company, et al.  
(Comanche Peak Steam Electric Station,  
Units 1 and 2)  
Docket No. 50-445 and 50-446

Request for Additional Information

In reviewing Cygna's answers in preparation for next month's hearings, Messrs. Walsh and Doyle have some additional information which they need from Cygna, as discussed on the attached sheets.

Sincerely,

CASE (Citizens Association for Sound Energy)

*Juanita Ellis*  
(Mrs.) Juanita Ellis  
President

Attachments

Service List - see attached

8404030093 840329  
PDR ADOCK 05000445  
G PDR

DS03

Doyle #4:

Please provide documentation from which the answer provided by Cygna was derived.

Doyle #8:

Please provide a copy of the drawing of the rear bracket in question, which indicates the 1-1/4" radius.

Doyle #15:

Please provide the math model used, as well as the input for the finite analysis.

Doyle #18:

Please provide the source and document(s) for the information contained in tables 1 and 2 on enclosure D18-1.

Walsh #7:

(a) Please refer to CASE Exhibit 889, especially pages 140-143. An analysis is done to determine the equivalent K for a column. The analysis shows the K value should be 1.2. The designer chose to use .8, and he stated the reason why; one of the reasons he stated is that the base plate is not actually a pin connection but instead is a fixed connection. If the designer chose to use the fixed connection so that the frame does not fail due to column buckling, the frame should have been analyzed from the beginning as a fixed connection (i.e., able to resist moments at the base plate).

When the designer decided to use the .8 value for K, the stress ratio became .991, as shown on a previous sheet within CASE's Exhibit 889. The AISC code does not allow columns to have a  $Kl/r$  greater than 200. Utilizing a K value of .8, the  $Kl/r$  is 173. Utilizing the calculated K value which is shown on pages 140-143 of Exhibit 889, = 259, this would make the support insufficient in regards to the code.

(b) In reviewing the calculations for bending stresses within the channels that are in direct contact with the cable trays (i.e., the C4X7.25), there has been no reduction in the section modulus for the hole where the bolts go through the channel flange. Due to the hole, the cross-sectional area of the flange is reduced by more than 50%. Also, the hole that is made through the flange is in violation of the AISC code requirements for an edge distance. Further, the calculations have neglected to consider the torsional effects within the channel due to the cable tray's not loading the channel through the shear center.

UNITED STATES OF AMERICA  
NUCLEAR REGULATORY COMMISSION

BEFORE THE ATOMIC SAFETY AND LICENSING BOARD

In the Matter of

TEXAS UTILITIES GENERATING  
COMPANY, et al.

(Comanche Peak Steam Electric Station  
Station, Units 1 and 2)

Docket Nos. 50-445 and  
50-446

CERTIFICATE OF SERVICE

By my signature below, I hereby certify that true and correct copies of  
CASE's 3/29/84 letter to Cygna with attachments, Request for Additional  
Information

have been sent to the names listed below this 29th day of March, 1984,  
by: Express Mail where indicated by \* and First Class Mail elsewhere.

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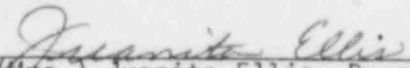
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