LIMITING CONDITIONS FOR OPERATION

3.7.A Primary Containment (Cont'd.)

2. Primary containment integrity shall be maintained at all times when the reactor is critical or when the reactor water temperature is above 212° F and fuel is in the the reactor vessel except while performing "open vessel" physics tests at power levels not to exceed 5 Mw (t).

3. If the primary containment integrity is breached when it is required by 3.7.A.2, that integrity shall be re-established within 24 hours hours or the reactor placed in a cold shutdown condition within 24 hours.

SURVEILLANCE REQUIREMENTS

4.7.A Primary Containment (Cont't.)

2. Integrated Leak Rate Testing

   a. Integrated leak rate tests (ILRT's) shall be performed to verify primary containment integrity. Primary containment integrity is confirmed if the leakage rate does not exceed the equivalent of 0.5 percent of the primary containment volume per 24 hours at 49.1 psig.

   b. Integrated leak rate tests may be performed at either 49.1 psig or 25 psig, the leakage rate test period, extending to 24 hours of retained internal pressure. If it can be demonstrated to the satisfaction of those responsible for the acceptance of the containment structure that the leakage rate can be accurately determined during a shorter test period, the agreed-upon shorter period may be used.

   Prior to initial operation, integrated leak rate tests must be performed at 49.1 and 25 psig (with the 25 psig test being performed prior to the 49.1 psig test) to establish the allowable leak rate (in percent of containment volume per 24 hours) at 25 psig as the lesser of the following values:

   (L_a is 0.5 percent)

   $$L_t = 0.5 \frac{L_{tm}}{L_{am}}$$

LIMITING CONDITIONS FOR OPERATION	SURVEILLANCE REQUIREMENTS
3.7.A Primary Containment (Cont'd.)	4.7.A Primary Containment (Cont'd.)

where

L_{tm} = measured ILR at 25 psig (P_t)

L_{am} = measured ILR at 49.1 psig (P_a), and

$\frac{L_{tm}}{L_{am}} \leq$ 0.7, otherwise

$$L_t = 0.5 \left(\frac{P_t}{P_a}\right)^{\frac{1}{2}}$$

where

P_a = peak accident pressure (psig)

P_t = appropriately measured test pressures (psig)

c. The ILRT's shall be performed at the following minimum frequency:

1. Prior to initial unit operation.

2. After the preoperational leakage rate tests, a set of three Type A tests shall be performed at approximately equal intervals during each 10 year service period. These intervals may be extended up to eight months if necessary to coincide with refueling outage.

d. The allowable leakage rates, L_{tm} and L_{am} , shall be less than 0.75 L_t and 0.75 L_a for the reduced pressure tests and peak pressure tests, respectively.

LIMITING CONDITIONS FOR OPERATION	SURVEILLANCE REQUIREMENTS
3.7.A Primary Containment (Cont'd.)	4.7.A Primary Containment (Cont'd.)

e. Except for the initial ILRT, all ILRT's shall be performed without any preliminary leak detection surveys and leak repairs being performed between the containment inspection and the performance of the ILRT.

While performing an ILRT, if excessive leakage is identified which will interfere with satisfactory completion of the test or result in the ILRT not meeting the acceptance criteria as specified in Section 4.7.A.2.d, either of the following methods for determining the "as found" and "as left" condition of primary containment shall be used.

(1) If an ILRT cannot be satisfactorily completed due to excessive leakage through identified leakage paths, those leakage paths may be isolated provided the leakage through such paths can be determined by a local leak rate test. The ILRT shall be completed with the leakage paths isolated and the "as found" ILRT shall be declared a failure.

For each leakage path isolated during the ILRT, local leakage rates shall be measured and recorded before and after repairs are made to each leakage path. The pre-repair local leakage rates shall be added to the ILRT leakage rate, measured with the leak-paths isolated, and this shall be used to determine

LIMITING CONDITIONS FOR OPERATION	SURVEILLANCE REQUIREMENTS
3.7.A Primary Containment (Cont'd.)	4.7.A Primary Containment (Cont'd.)

the "as found" condition of of primary containment. The post-repair local leakage rates shall be added to the ILRT leakage rate, measured with the leakage paths isolated, and this sum shall be used to determine the "as left" condition of primary containment.

(2) If an ILRT is completed with all identified leakage paths in service, but the acceptance criteria of Section 4.7.A.2.d is not satisfied, the "as found" ILRT shall be declared a failure, any identified leakage paths shall be isolated provided the leakage through such paths can be determined by a local leak rate test, and another ILRT shall be conducted with the leakage paths isolated.

After repairs are made, local leakage rates shall be measured for each of those leakage paths isolated. The post-repair leakage rates shall be added to the ILRT leakage rate, measured with the leakage paths isolated, and this sum shall be used to determine the "as left" condition of primary conment.

LIMITING CONDITIONS FOR OPERATION	SURVEILLANCE REQUIREMENTS
3.7.A <u>Primary Containment</u> (Cont'd.)	4.7.A <u>Primary Containment</u> (Cont'd.)
	f. Local leak rate tests (ILRT's) shall be performed on the primary containment testable penetrations and isolation valves at a pressure of 49.1 psig (except for the main steam isolation valves, see below) each operating cycle, but in no case at intervals greater than two years. Bolted double-gasketed seals shall be tested whenever the seal is closed after being opened and at least once per operating cycle, but in no case at intervals greater than two years. The Main Steamline isolation valves shall be tested at a pressure of 25 psig for leakage during each refueling outage, but in no case at intervals greater than two years. If a total leakage rate of 11.5 scf/hr for any one main steamline isolation valve is exceeded, repairs and retest shall be performed to correct the condition.
	g. <u>Continuous Leak Rate Monitor</u> When the primary containment is inerted, the containment shall be continuously monitored for gross leakage by review of the inerting system makeup requirements. This monitoring system may be taken out-of-service for maintenance but shall be returned to service as soon as practicable.

LIMITING CONDITIONS FOR OPERATION

3.7.A Primary Containment (Cont'd)

3. Pressure Suppression Chamber - Reactor Building Vacuum Breakers

a. Except as specified in 3.7.A.3.b below , two pressure suppression chamber-reactor building vacuum breakers shall be operable at all times whem primary containment integrity is required. The setpoint of the differential pressure instrumentation which actuates the pressure suppression chamber-reactor building vacuum breakers shall be 0.5 $\pm$ 0.25 psid.

b. From and after the date that one of the pressure suppression chamber-reactor building vacuum breakers is made or found to be inoperable for any reason, reactor operation is permissible only during the succeeding seven days unless such vacuum breaker is sooner made oeprable, provided that the repair procedure does not violate primary containment integrity.

4. Drywell-Pressure Suppression Chamber Vacuum Breakers

a. When primary containment is required, all drywell-suppression chamber vacuum breakers shall be operable and positioned in the fully closed position (except during testing) except as specified in 3.7.A.4.b and c, below.

b. One drywell-suppression chamber vacuum breaker may be non-fully closed so long as it is deter-

SURVEILLANCE REQUIREMENTS

4.7.A Primary Containment (Cont'd)

h. Drywell Surfaces

The interior surfaces of the drywell and torus shall be visually inspected each operating cycle for evidence of deterioration. In addition, the external surfaces of the torus below the water level shall be inspected on a routine basis for evidence of torus corrosion or leakage.

3. Pressure Suppression Chamber - Reactor Building Vacuum Breakers

a. The pressure suppression iated instrumentation including setpoint shall be checked for proper operation every refueling outage.

4. Drywell-Pressure Suppression Chamber-Vacuum Breakers

a. Each drywell-suppression chamber vacuum breaker shall be exercised through an opening-closing cycle once a month.

b. When it is determined that a vacuum breaker valve is inoperable for opening at a time when

TABLE 3.7.2

TESTABLE PENETRATIONS WITH DOUBLE O-RINGS SEALS

Pen No.		Notes
N-1	Equipment Access Hatch	(1)(2)(4)(6)
N-2	Equipment Access and Personnel Lock	(1)(4)(8)
N-4	Drywell Head Access Hatch	(1)(2)(4)(6)
N-6	CRD Removal Hatch	(1)(2)(4)(6)
N-25	AO-2520 (Unit #2); AO-3520 (Unit #3) Purge System Valves	(1)(2)(4)(6)
N-26	AO-2506 (Unit #2); AO-3506 (Unit #3) Purge System Valves	(1)(2)(4)(6)
N-35-A through N-35-G	TIP System	(1)(2)(4)(6)
N-200A&B	Suppression Chamber Access Hatch	(1)(2)(4)(6)
N-205B	AO-2521B (Unit #2); AO-3521B (Unit #3) [Purge System Valves]	(1)(2)(4)(6)
	AO-2502A (Unit #2); AO-3502A (Unit #3) [Purge System Valves]	(1)(2)(4)(6)
N-205A	AO-2502B (Unit #2); AO-3502B (Unit #3) [Purge System Valves]	(1)(2)(4)(6)
N-212	Stop Check 13-9 (RCIC Stop Check)	(1)(2)(4)(6)
N-213A&B	Construction Drain	(1)(2)(4)(6)
N-214	Stop Check 23-12" (HPCI Stop Check)	(1)(2)(4)(6)

TABLE 3.7.3

TESTABLE PENETRATIONS WITH TESTABLE BELLOWS

Pen No.		Notes	Pen No.		Notes
N-7A	Primary Steam Line 'A'	(1)(2)(4) (6)	N-13A	RHR Pump Discharge	(1)(2)(4) (6)
N-7B	Primary Steamline 'B'	(1)(2)(4) (6)	N-13B	RHR Pump Discharge	(1)(2)(4) (6)
N-7C	Primary Steamline 'C'	(1)(2)(4) (6)	N-14	Reactor Water Cleanup Line	(1)(2)(4) (6)
N-7D	Primary Steamline 'D'	(1)(2)(4) (6)	N-16A	Core Spray Pump Discharge	(1)(2)(4) (6)
N-9A	Feedwater Line 'A'	(1)(2)(4) (6)	N-16B	Core Spray Pump Discharge	(1)(2)(4) (6)
N-9B	Feedwater Line 'B'	(1)(2)(4) (6)	N-17	RPV Head Spray	(1)(2)(4) (6)
N-11	Steam Line to HPCI Turbine	(1)(2)(4) (6)	N-201A through N-201H	Suppression Chamber to Drywell Vent Line	(1)(2)(4) (6)
N-12	RHR Shutdown Pump Supply	(1)(2)(4) (6)			

TABLE 3.7.4

PRIMARY CONTAINMENT TESTABLE ISOLATION VALVES

Pen No.		NOTES
7A to D	AO-2-80A to D	1,2,3,4,5
	AO-2-86A to D	1,2,3,4,5
8	MO-2-74	1,2,4,5,9,10
	MO-2-77	1,2,4,5
9A	MO-23-19; MO-2-38A	1,2,4,5
	Check Valves 2-28A and 2-96A	1,2,4,5
9B	MO-13-21; MO-2-38B; MO-12-68	1,2,4,5
	Check Valves 2-28B and 2-96B	1,2,4,5
10	MO-13-15	1,2,4,5,9,10
	MO-13-16	1,2,4,5
11	MO-23-15	1,2,4,5,9,10
	MO-23-16	1,2,4,5
	AO-4807 (Unit #2)	1,2,4,5
12	MO-10-18;	1,2,4,5,9,10
	MO-10-17	1,2,4,5
13A	MO-10-25B; AO-10-46B; AO-10-163B*	1,2,4,5
13B	MO-10-25A; AO-10-46A; AO-10-163A*	1,2,4,5
14	MO-12-15	1,2,4,5,9,10
	MO-12-18	1,2,4,5
16A	MO-14-12B; AO-14-13B; AO-14-15B*, **	1,2,4,5
16B	MO-14-12A; AO-14-13A; AO-14-15A*, **	1,2,4,5
17	MO-10-32	1,2,4,5,9,10
	MO-10-33	1,2,4,5
18	AO-20-82	1,2,4,5,9,11
	AO-20-83	1,2,4,5
19	AO-20-94	1,2,4,5,9,11
	AO-20-95	1,2,4,5
21	Service Air System Inner Globe Valve	1,2,4,5,9,11
	Service Air System Outer Globe Valve	1,2,4,5

* Effective following the next Refueling Outage on Unit Nos. 2 & 3.
**Effective following the next Refueling Outage subsequent to the completion of modifications on Unit 3 approved by Amendment No.

TABLE 3.7.4

PRIMARY CONTAINMENT TESTABLE ISOLATION VALVES

Pen No.		NOTES
22	AO-2969A (Unit #2); AO-3969A (Unit #3)	1,2,4,5
	Check Valve	1,2,4,5
23	MO-2373 (Unit #2); MO-3373 (Unit #3)	1,2,4,5
24	MO-2374 (Unit #2); MO-3374 (Unit #3)	1,2,4,5
25,	AO-2502A (Unit #2); AO-3502A (Unit #3)	1,2,4,5,9
205B	AO-2505 (Unit #2); AO-3505 (Unit #3)	1,2,4,5
	AO-2519 (Unit #2); AO-3519 (Unit #3)	1,2,4,5
	AO-2520 (Unit #2); AO-3520 (Unit #3)	1,2,4,5,9,12
	AO-2521A (Unit #2); AO-3521A (Unit #3)	1,2,4,5
	AO-2521B (Unit #2); AO-3521B (Unit #3)	1,2,4,5,9,12
	AO-2523 (Unit #2); AO-3523 (Unit #3)	1,2,4,5
	Check Valve 9-26A; Two Check Valves	1,2,4,5
26	AO-2506 (Unit #2); AO-3506 (Unit #3)	1,2,4,5,9,12
	AO-2507 (Unit #2); AO-3507 (Unit #3)	1,2,4,5
	AO-2509 (Unit #2); AO-3509 (Unit #3)	1,2,4,5,9,11
	AO-2510 (Unit #2); AO-3510 (Unit #3)	1,2,4,5
	AO-4235 (Unit #2); AO-5235 (Unit #3)	1,2,4,5
	SV-2671G (Unit #2); SV-3671G (Unit #3)	1,2,4,5
	SV-2978G (Unit #2); SV-3978G (Unit #3)	1,2,4,5
	SV-4960B (Unit #2); SV-5960B (Unit #3)	1,2,4,5
	SV-4961B (Unit #2); SV-5961B (Unit #3)	1,2,4,5
	SV-4966B (Unit #2); SV-5966B (Unit #3)	1,2,4,5
	SV-8100 (Unit #2); SV-9100 (Unit #3)	1,2,4,5
	SV-8101 (Unit #2); SV-9101 (Unit #3)	1,2,4,5
32C, D	ILRT System Two Globe Valves	1,2,4,5,13
35A to E	TIP Ball Valves	1,2,4,5
35F	SV-7-113; Check Valve	1,2,4,5
38	CV-3-32A; CV-3-32B; CV-3-33	1,2,4,5
	CV-3-35A; CV-3-35B; CV-3-36	1,2,4,5
39A	MO-10-31B	1,2,4,5,9,10
	MO-10-26B	1,2,4,5
	SV-4949B (Unit #2); SV-5949B (Unit #3)	1,2,4,5
	Check Valve	1,2,4,5
39B	MO-10-31A	1,2,4,5,9,10
	MO-10-26A	1,2,4,5
	SV-4949A (Unit #2); SV-5949A (Unit #3)	1,2,4,5
	Check Valve	1,2,4,5
41	AO-2-39	1,2,4,5,9,11
	AO-2-40	1,2,4,5

TABLE 3.7.4

PRIMARY CONTAINMENT TESTABLE ISOLATION VALVES

Pen No.		NOTES
42	Check Valve 11-16; XV-14A,B	1,2,4,5
47	SV-8130B (Unit #2); SV-9130B (Unit #3)	1,2,4,5
	Check Valve	1,2,4,5
51A	SV-2671E (Unit #2); SV-3671E (Unit #3)	1,2,4,5
	SV-2978E (Unit #2); SV-3978E (Unit #3)	1,2,4,5
51B	SV-2671D (Unit #2); SV-3671D (Unit #3)	1,2,4,5
	SV-2978D (Unit #2); SV-3978D (Unit #3)	1,2,4,5
51C	SV-2671C (Unit #2); SV-3671C (Unit #3)	1,2,4,5
	SV-2978C (Unit #2); SV-3978C (Unit #3)	1,2,4,5
	SV-4960C (Unit #2); SV-5960C (Unit #3)	1,2,4,5
	SV-4961C (Unit #2); SV-5961C (Unit #3)	1,2,4,5
	SV-4966C (Unit #2); SV-5966C (Unit #3)	1,2,4,5
	SV-8101 (Unit #2); SV-9101 (Unit #3)	1,2,4,5
51D	SV-2980 (Unit #2); SV-3980 (Unit #3)	1,2,4,5
	Check Valve	1,2,4,5
52F	AO-2969B (Unit #2); AO-3969B (Unit #3)	1,2,4,5
	Check Valve	1,2,4,5
53	MO-2201B (Unit #2); MO-3201B (Unit #3)	1,2,4,5
54	MO-2200B (Unit #2); MO-3200B (Unit #3)	1,2,4,5
55	MO-2200A (Unit #2); MO-3200A (Unit #3)	1,2,4,5
56	MO-2201A (Unit #2); MO-3201A (Unit #3)	1,2,4,5
57	AO-2-316	1,2,4,5,9,11
	AO-2-317	1,2,4,5
102B	Breathing Air System - 2 Gate Valves (Unit #3)	1,2,4,5,9
	SV-8130A (Unit #2); SV-9130A (Unit #3)	1,2,4,5
	Check Valve	1,2,4,5
203	SV-2671B (Unit #2); SV-3671B (Unit #3)	1,2,4,5
	SV-2978B (Unit #2); SV-3978B (Unit #3)	1,2,4,5
	SV-4960D (Unit #2); SV-5960D (Unit #3)	1,2,4,5
	SV-4961D (Unit #2); SV-5961D (Unit #3)	1,2,4,5
	SV-4966D (Unit #2); SV-5966D (Unit #3)	1,2,4,5
	SV-8101 (Unit #2); SV-9101 (Unit #3)	1,2,4,5
205A	AO-2502B (Unit #2); AO-3502B (Unit #3)	1,2,4,5,9,12
	Check Valve 9-26B	1,2,4,5

TABLE 3.7.4

PRIMARY CONTAINMENT TESTABLE ISOLATION VALVES

Pen No.		NOTES
210A	MO-10-34B	1,2,4,5,9,11
210B	MO-10-34A	1,2,4,5,9,11
211A	MO-10-38B	1,2,4,5,9,11
	MO-10-39B; MO-10-34B; Check Valve	1,2,4,5
	SV-4951B (Unit #2); SV-5951B (Unit #3)	1,2,4,5
211B	MO-10-38A	1,2,4,5,9,11
	MO-10-39A; MO-10-34A; Check Valve	1,2,4,5
	SV-4951A (Unit #2); SV-5951A (Unit #3)	1,2,4,5
212,	AO-4240 (Unit #2); AO-5240 (Unit #3)	1,2,4,5,9,11
214,	AO-4241 (Unit #2); AO-5241 (Unit #3)	1,2,4,5
217B	AO-4247 (Unit #2); AO-5247 (Unit #3)	1,2,4,5,9,11
	AO-4248 (Unit #2); AO-5248 (Unit #3)	1,2,4,5
	MO-4244 (Unit #2); MO-5244 (Unit #3)	1,2,4,5,14
	MO-4244A (Unit #2); MO-5244A (Unit #3)	1,2,4,5,14
	Check Valve 13-50; Check Valve 23-65	1,2,4,5
218A	AO-2968 (Unit #2); AO-3968 (Unit #3)	1,2,4,5
	Check Valve	1,2,4,5
218B	SV-2671A (Unit #2); SV-3671A (Unit # 3)	1,2,4,5
	SV-2978A (Unit #2); SV-3978A (Unit #3)	1,2,4,5
218C	ILRT System-Two Globe Valves	1,2,4,5,13
219	AO-2511 (Unit #2); AO-3511 (Unit #3)	1,2,4,5,9,12
	AO-2512 (Unit #2); AO-3512 (Unit #3)	1,2,4,5
	AO-2513 (Unit #2); AO-3513 (Unit #3)	1,2,4,5,9,11
	AO-2514 (Unit #2); AO-3514 (Unit #3)	1,2,4,5
	SV-2671F (Unit #2); SV-3671F (Unit #3)	1,2,4,5
	SV-2978F (Unit #2); SV-3978F (Unit #3)	1,2,4,5
	SV-4960A (Unit #2); SV-5960A (Unit #3)	1,2,4,5
	SV-4961A (Unit #2); SV-5961A (Unit #3)	1,2,4,5
	SV-4966A (Unit #2); SV-5966A (Unit #3)	1,2,4,5
	SV-8101 (Unit #2); SV-9101 (Unit #3)	1,2,4,5
221	Check Valve 13-38	1,2,4,5
223	Check Valve 23-56	1,2,4,5
225	MO-14-71; MO-13-39	1,2,4,5
227	MO-23-57	1,2,4,5

NOTES FOR TABLES 3.7.2 THROUGH 3.7.4

(1) Minimum test duration for all valves and penetrations listed is one hour.

(2) Test pressures shall be at least 49.1 psig for all valves and penetrations except MSIV's which are tested at 25 psig.

(3) MSIV's acceptable leakage is 11.5 scfh/valve of air.

(4) The total acceptable leakage for all valves and penetrations other than the MSIV's is 0.60 La. MSIV leakage is excluded from this total.

(5) Local leak tests on all testable isolation valves shall be performed at intervals no greater than 2 years.

(6) Local leak tests on all testable penetrations shall be performed at intervals no greater than 2 years.

(7) Deleted.

(8) The personnel air locks are tested at 49.1 psig.

(9) Identifies isolation valves that are tested by applying pressure between the inboard and outboard valves.

(10) Gate valve tested in reverse direction. Test acceptable since the normal force between the seat and the disc generated by stem action alone is greater than ten (10) times the normal force induced by test differential pressure. This applied to the following valves:

MO-2-74	MO-10-31A, B
MO-13-15	MO-10-18
MO-23-15	MO-12-15
MO-10-32	

NOTES FOR TABLES 3.7.2 THROUGH 3.7.4 (Cont'd)

(11) Globe valve tested in reverse direction. Test acceptable since test pressure is applied under the valve seat. This applies to the following valves:

AO-4240 (5240)	AO-20-94
AO-4247 (5247)	AO-2509 (3509)
MO-10-38A and B	AO-2-39
MO-10-34A and B	AO-2-316
AO-20-82	AO-2513 (3513)

Inner manual valve on penetration N-21.

(12) Butterfly valve tested in reverse direction. Test acceptable since valve is equipped with inflatable seals which provide equivalent bi-directional sealing. This applies to the following valves:

AO-2520 (3520)	AO-2506 (3506)
AO-2511 (3511)	AO-2521B (3521B)
AO-2502A and B (3502A and B)	

(13) Manual globe valves tested in reverse direction. This applies to valves on the following penetrations:

N-32C	(two valves)
N-218C	(two valves)
N-32D	(two valves)

(14) Gate valve utilized for containment isolation in both directions. Test performed only in one direction. Valve normal force ratio is 17.9. Leakage path is between separate torus penetrations only.

The primary containment leak rate test frequency is based on maintaining adequate assurance that the leak rate remains within the specification. The leak rate test frequency is based on the NRC guide for developing leak rate testing and surveillance of reactor containment vessels.

The method for correcting measured containment integrated leakage rates based upon local leakage measurements, taken before and after repairs are made to identified excessive leakage paths, provides a conservative assessment of containment leakage by satisfying two objectives. First, by ensuring that the containment integrated leakage rate satisfies the acceptance criteria of 10 CFR 50, Appendix J, once the testing is complete. Second, by ensuring that the "as found" condition of primary containment, i.e. before repairs are made, is determined for the purpose of establishing the subsequent test frequency in accordance with Appendix J.

The penetration and air purge piping leakage test frequency, along with the containment leak rate tests, is adequate to allow detection of leakage trends. Whenever a bolted double-gasketed penetration is broken and remade, the space between the gaskets is pressurized to determine that the seals are performing properly. It is expected that the majority of the leakage from valves, penetrations and seals would be into the reactor building. However, it is possible that leakage into other parts of the facility could occur. Such leakage paths that may affect significantly the consequences of accidents are to be minimized.

The Main Steamline Isolation Valves (MSIV's) are angled in the main steam lines in order to afford better sealing in the direction of accident pressure. This being the case, local leak rate testing at a reduced pressure of 25 psig results in a conservative determination of the actual leakage through these valves. The 11.5 scf/hr acceptance criteria is effective and reliable in determining the status of the MSIV's and in verifying that substantial degradation of these valves has not occurred since the last Integrated Leakage Rate Test (ILRT). The 11.5 scf/hr criteria is likewise conservative because of the reduced test pressure. Additionally, the leakage path through the MSIV's is included during an ILRT; and therefore, the effect of this leakage on containment integrity is taken into account. For these reasons, the leakage through the MSIV's is excluded from the limit of 0.6 La for the combined leakage rate for penetrations and valves subject to local leak rate tests.

Table 3.7.4 identifies certain isolation valves that are tested by pressurizing the volume between the inboard and outboard isolation valves. This results in conservative test results since the inboard valve, if a globe valve, will be tested such that the test pressure is tending to lift the globe off its seat.

The primary containment pre-operational test pressures are based upon the calculated primary containment pressure response in the event of a loss-of-coolant accident. The peak drywell pressure would be about 49.1 psig which would rapidly reduce to 27 psig following the pipe break. Following the pipe break, the suppression chamber pressure rises to 27 psig, equalizes with drywell pressure and therefore, rapidly decays with the drywell pressure decay. The design pressure of the drywell and suppression chamber is 56 psig. Based on the calculated containment pressure response discussed above, the primary containment pre-operational test pressures were chosen. Also, based on the primary containment pressure response and the fact that the drywell and suppression chamber function as a unit, the primary containment will be tested as a unit rather than the individual components separately.