

# WMA C Performance Assessment (PA) Updates to Hydrogeologic Model, Numerical Model Construction and Parameterization

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# Updates to Hydrogeologic Model, Numerical Model Construction and Parameterization

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# Update to Hydrogeologic Framework

- **Development of Alternative Geological Models based on:**
  - WMA C Alternative I (DOE Interpretation)
  - WMA C Alternative II (Nez Perce Interpretation)
- **Basis for new Interpretations: Geophysical and Geologic data:**
  - 70 dry wells
  - 50 direct pushes
  - 22 Groundwater wells
- **New Geologic Report – RPP-RPT-56356, Rev. 0, *Development of Alternative Geologic Models of Waste Management Area C***

# Developing a 3-Dimensional Grid

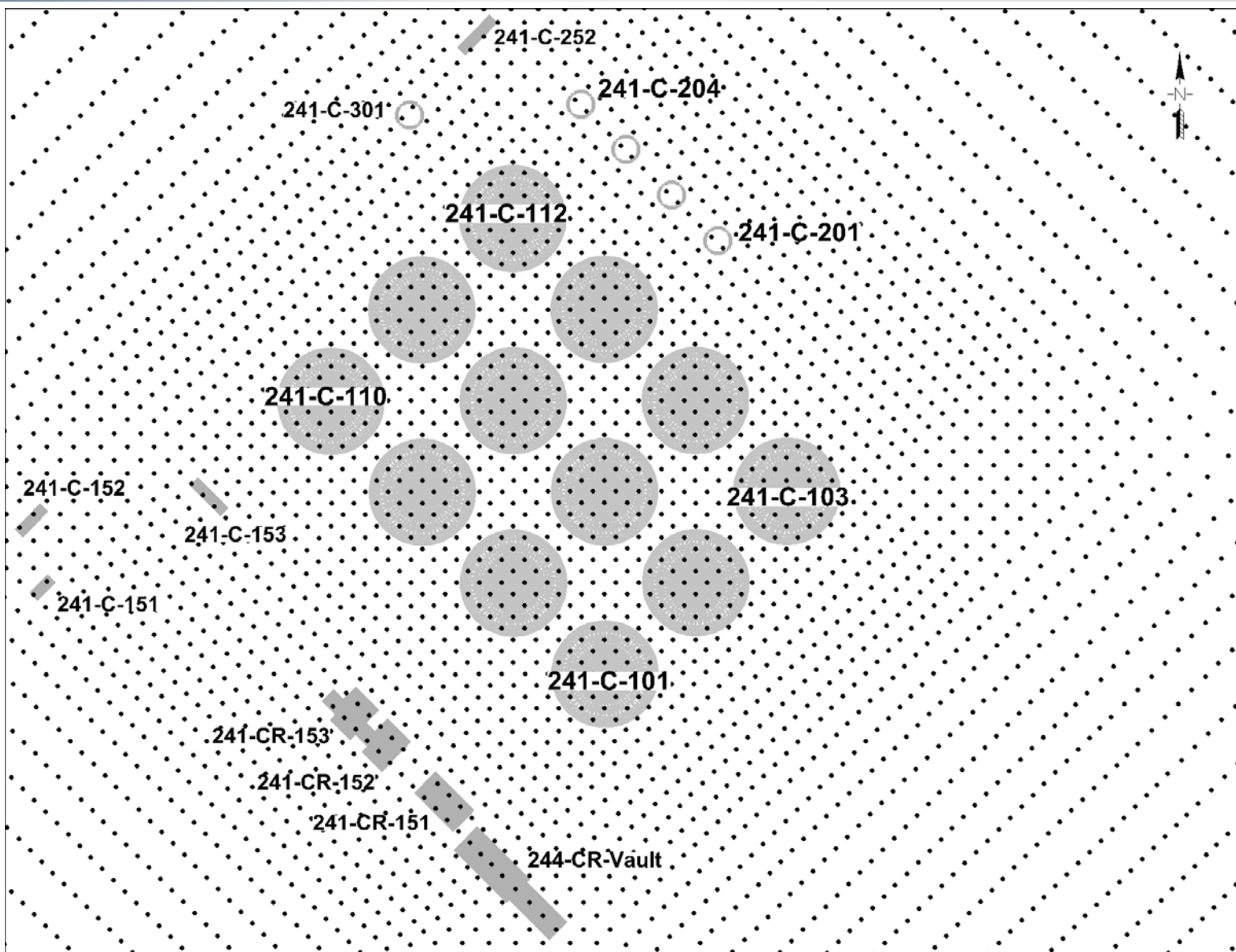
**The objective is to represent the natural and engineered systems**

- The vertical spacing
  - must address the contacts between the different geologic units
  - must address tanks and ancillary structures
- The node horizontal spacing must represent the tanks and ancillary structures

# Plan View of WMA C Tanks and STOMP Grid

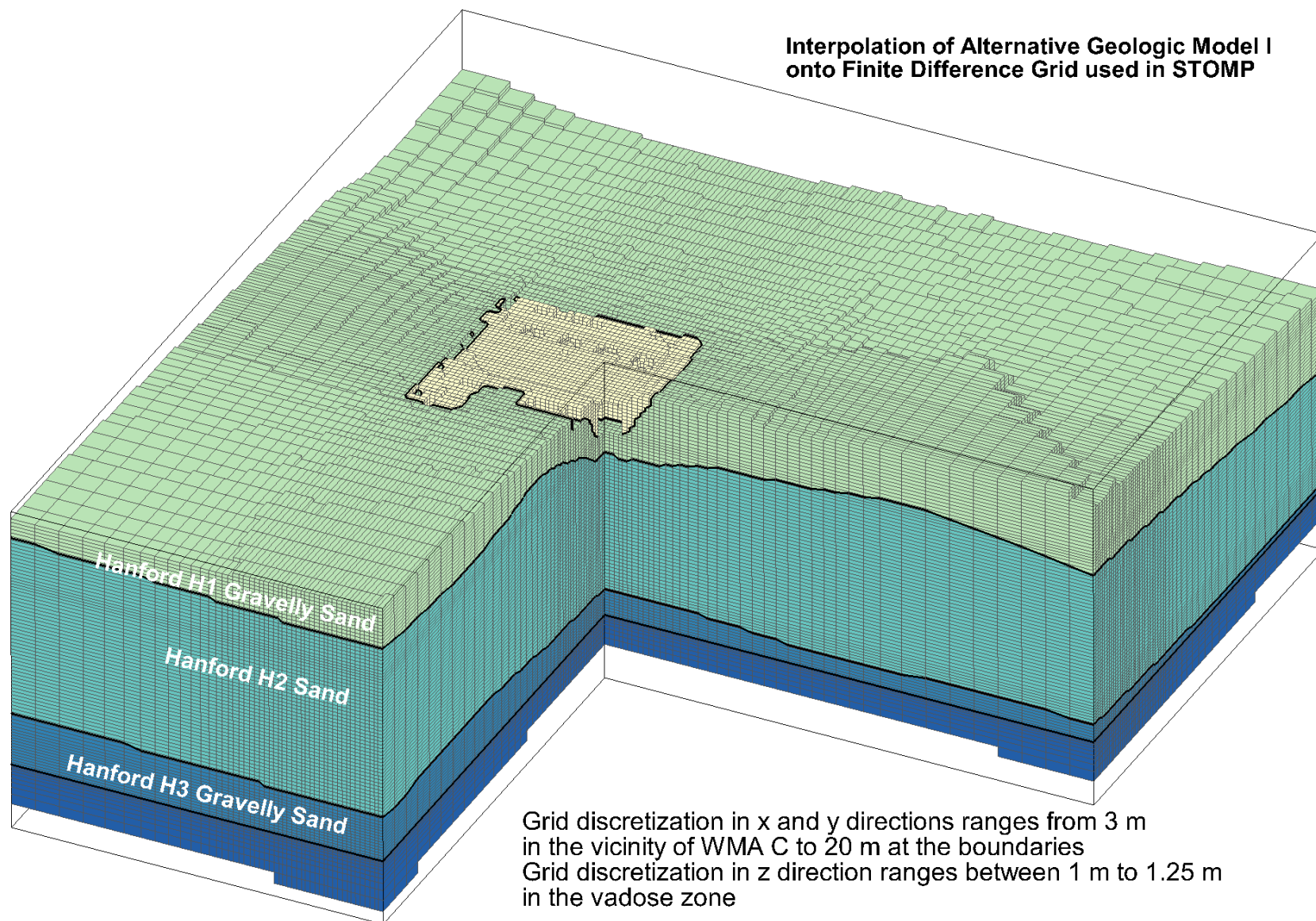
Black =  
grid node

Gray =  
tank or vault  
outline



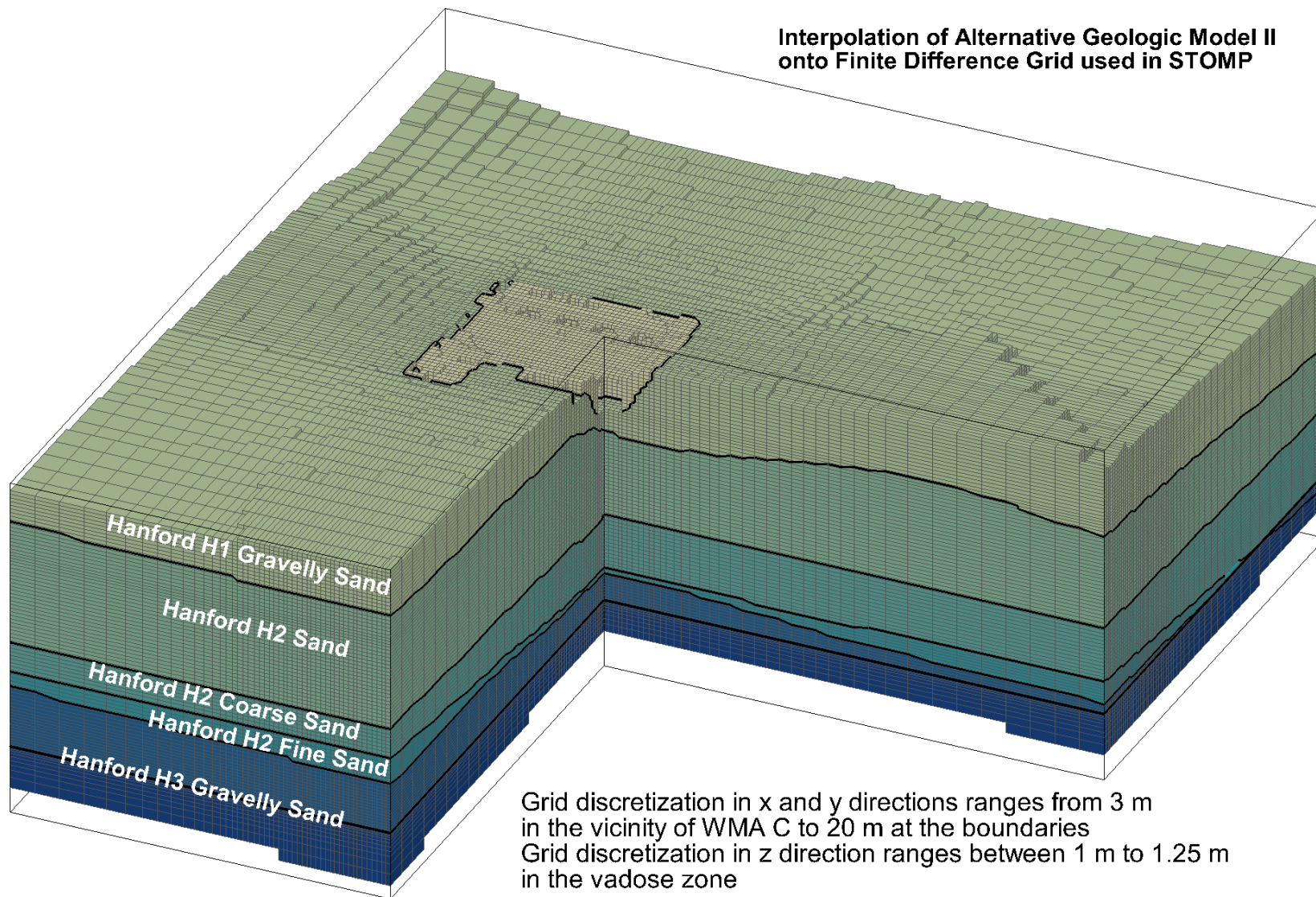
# WMA C Alternative Model I

Interpolation of Alternative Geologic Model I  
onto Finite Difference Grid used in STOMP



# WMA C Alternative Model II

Interpolation of Alternative Geologic Model II  
onto Finite Difference Grid used in STOMP



# Surface Conditions of WMA C Model



# Recharge Rates of WMA C Model

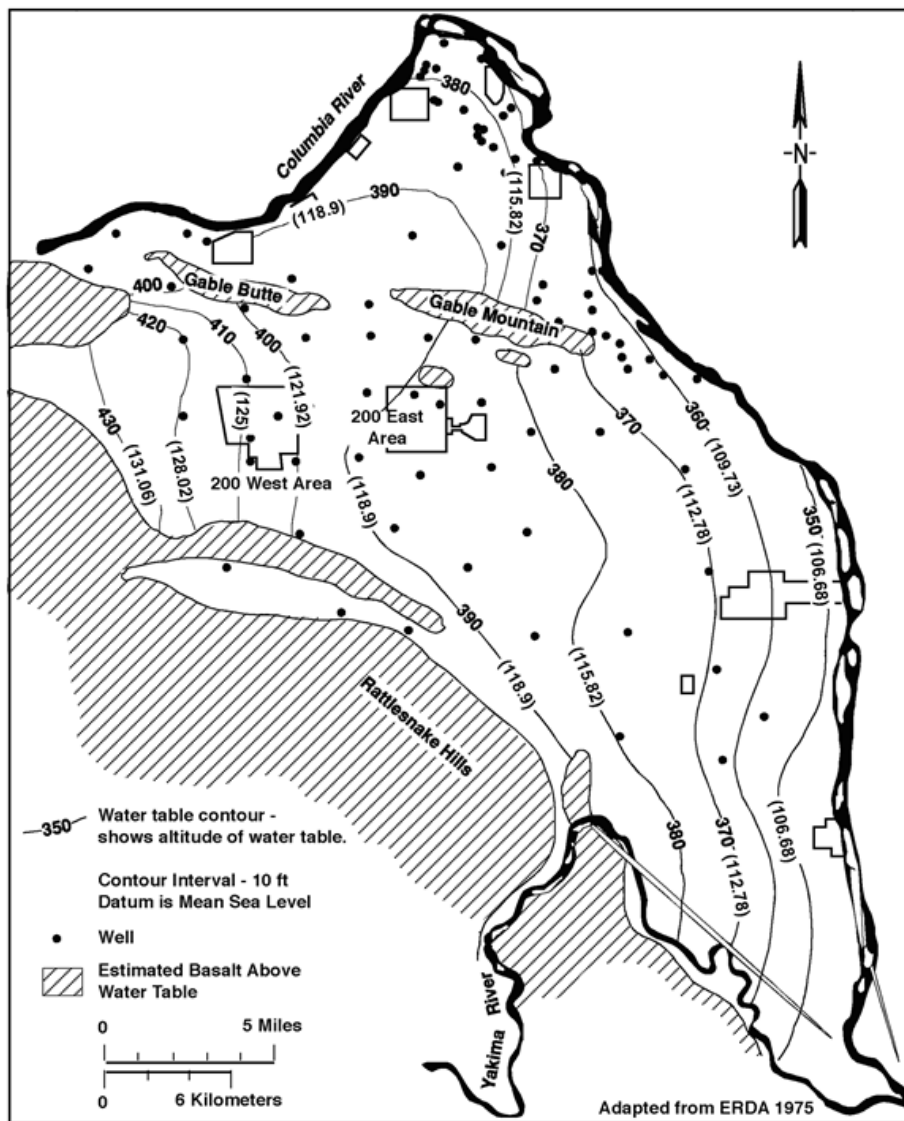
Barrier Status	Pre-Hanford (mm/yr)	Operational Period (mm/yr)	Institutional Control (100 yr) (mm/yr)	Barrier design life (500 yr after closure) (mm/yr)	End of Barrier Design life (mm/yr)
Denominator Case	3.5	100	0.5	0.5	3.5
Sensitivity Case 1	3.5	100	0.5	0.5	1.0
Sensitivity Case 2	3.5	40	0.5	0.5	1.0
Sensitivity Case 3	3.5	140	0.5	100	100

# Aquifer Conditions of WMA C Model

Current conditions show groundwater flow in the WMA C area is generally to the south and southeast.

Slowly returning to pre-operational Hanford Site conditions

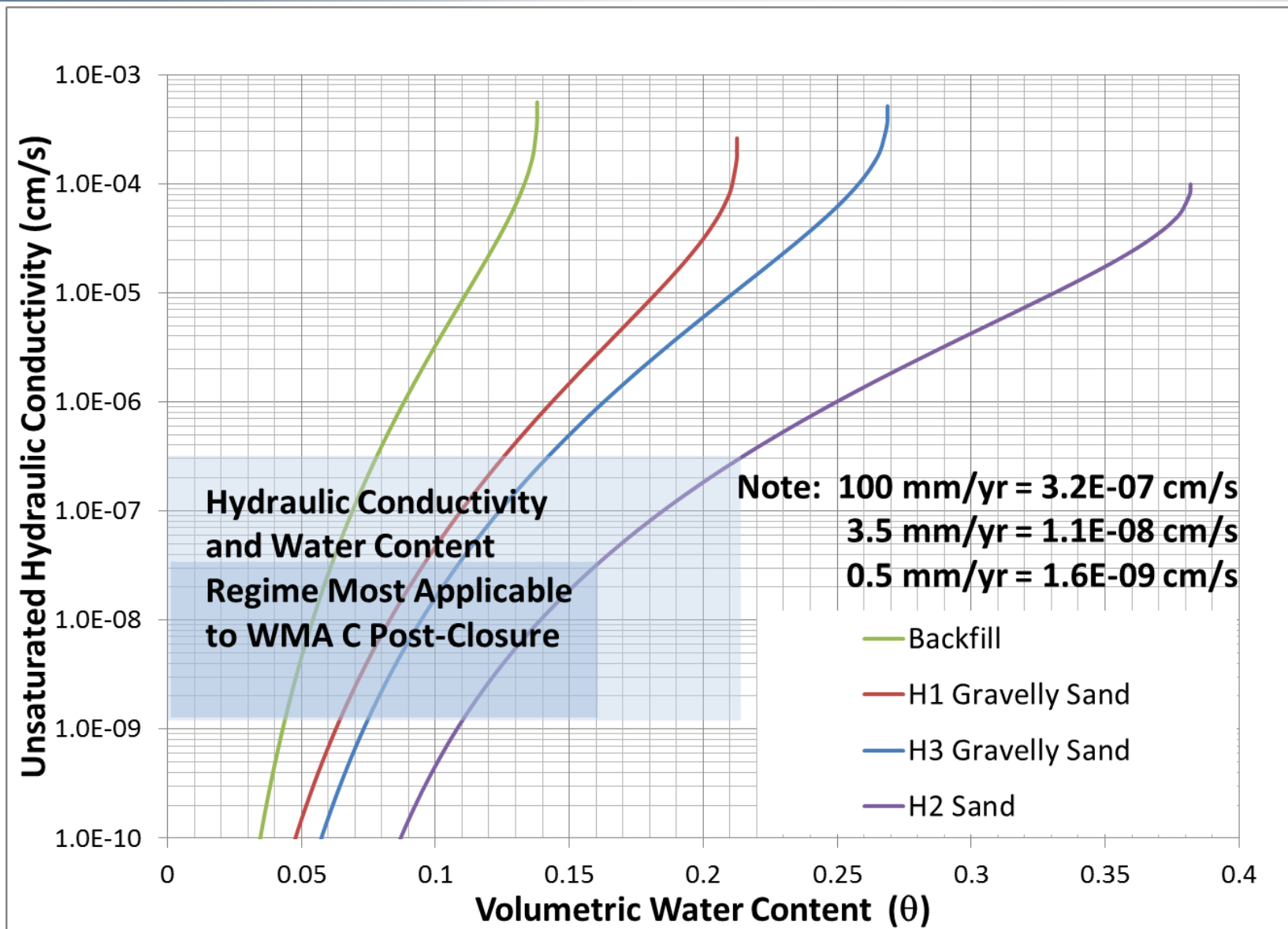
Hindcast Water Table Map of the Hanford Site, January 1944



# Aquifer Hydraulic Properties of WMA C Model

Property	Denominator Case	Minimum	Maximum
Hydraulic Conductivity (m/d)	3000	100	7000
Effective Porosity (-)	0.25 (Hanford gravel)	NC	NC
Hydraulic Gradient (-)	$10^{-5}$	$2 \times 10^{-6}$	$10^{-4}$

# Hydraulic Properties of WMA C Model



# Field Test Results from Tracer Injection

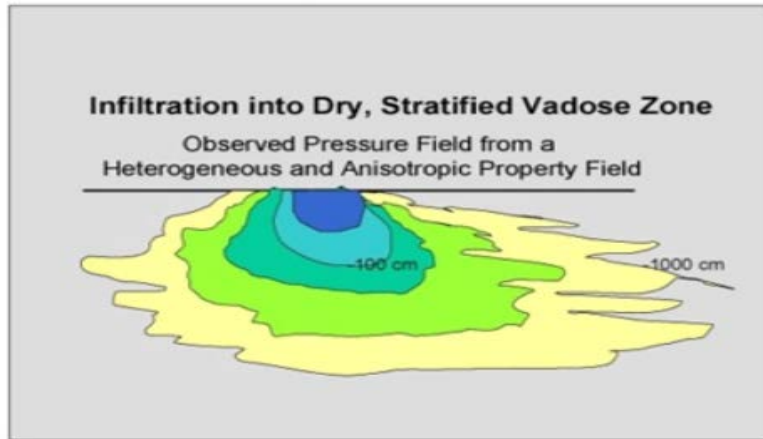


Media **heterogeneity** (and the resulting variability in unsaturated K) induces variable **moisture-dependent anisotropy** in the field

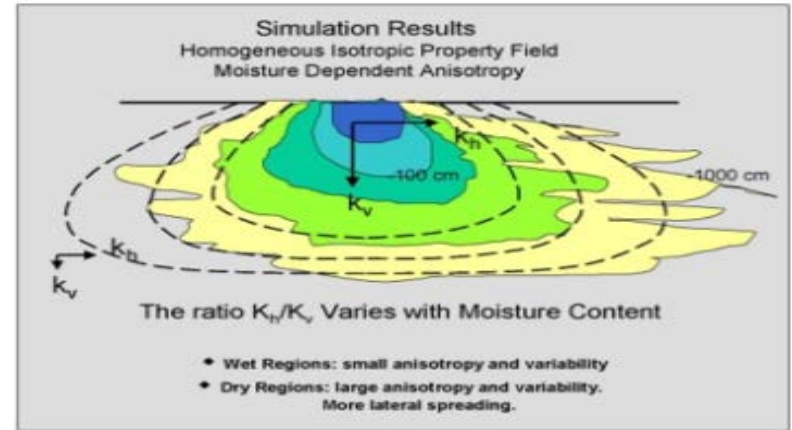


# Moisture Dependent Anisotropy

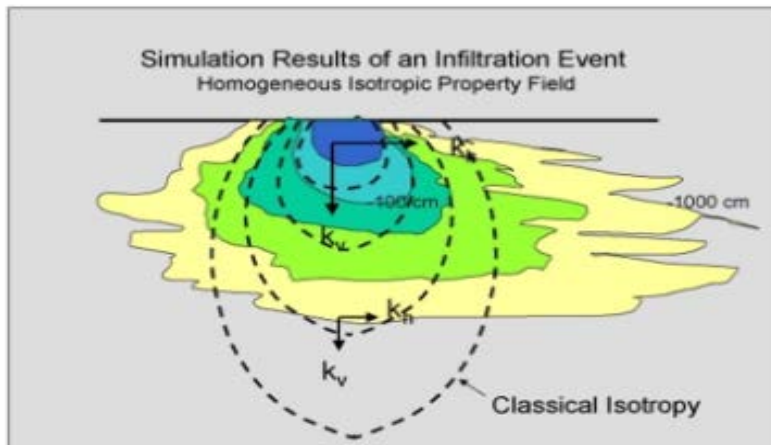
## Schematic Illustrations



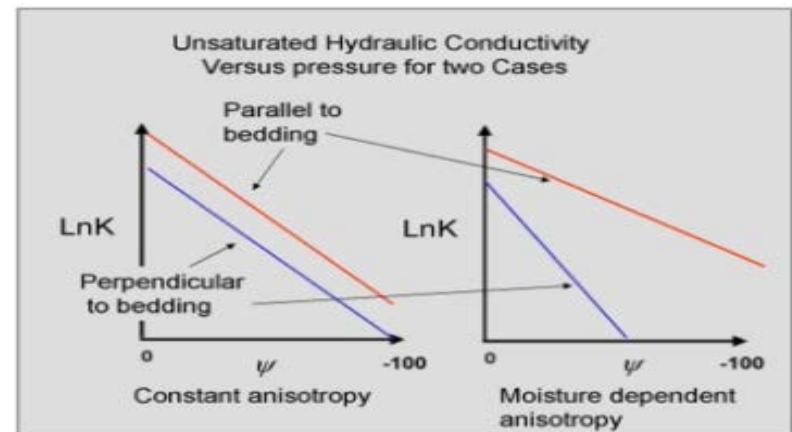
(a)



(c)



(b)



(d)

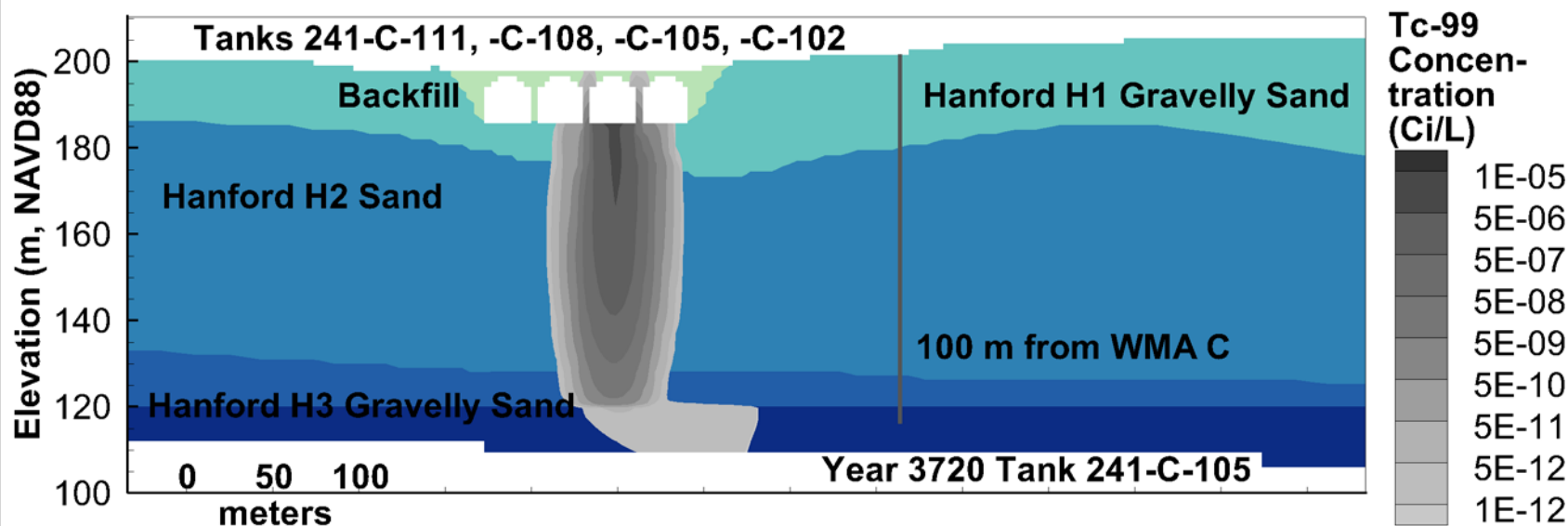
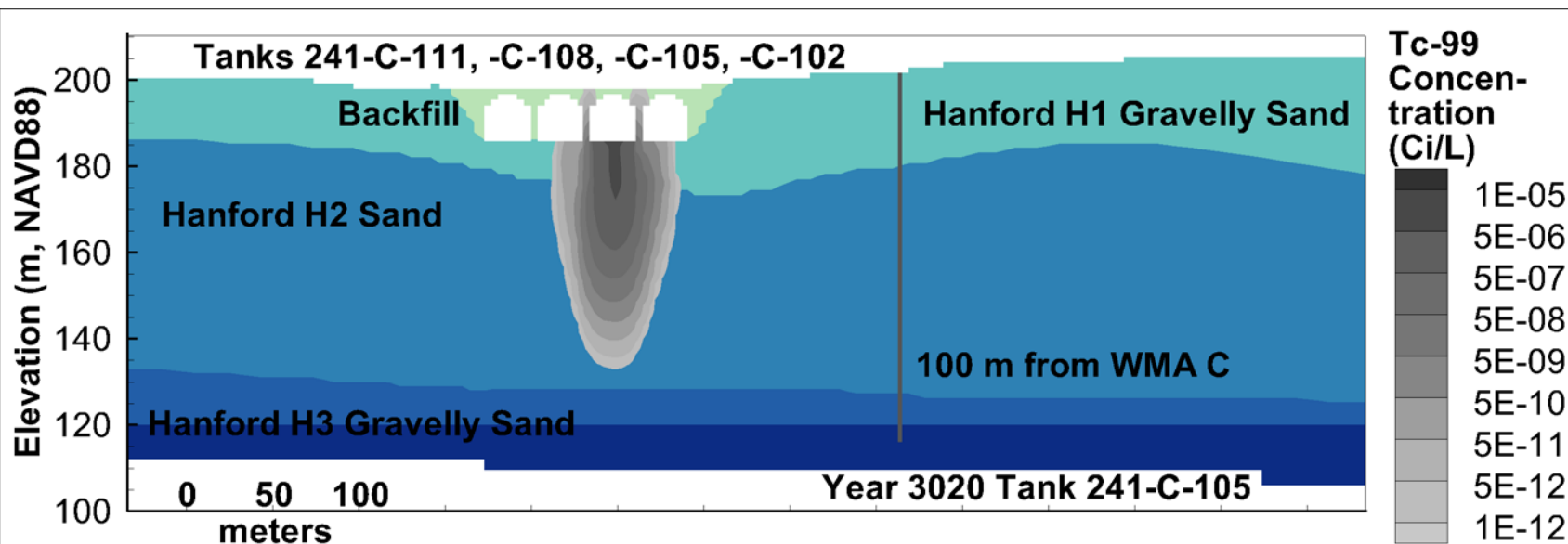
# Local-scale Model Development & Testing

- Two alternative hydrogeologic models implemented using STOMP
- Evaluation of model domain, design, and discretization completed
- Model simulations using unit source inventories and different combinations of hydraulic properties and recharge rates have been initiated.
- Preliminary runs using a variety of recharge conditions to support model abstraction of flow into GoldSim System Model have been initiated.

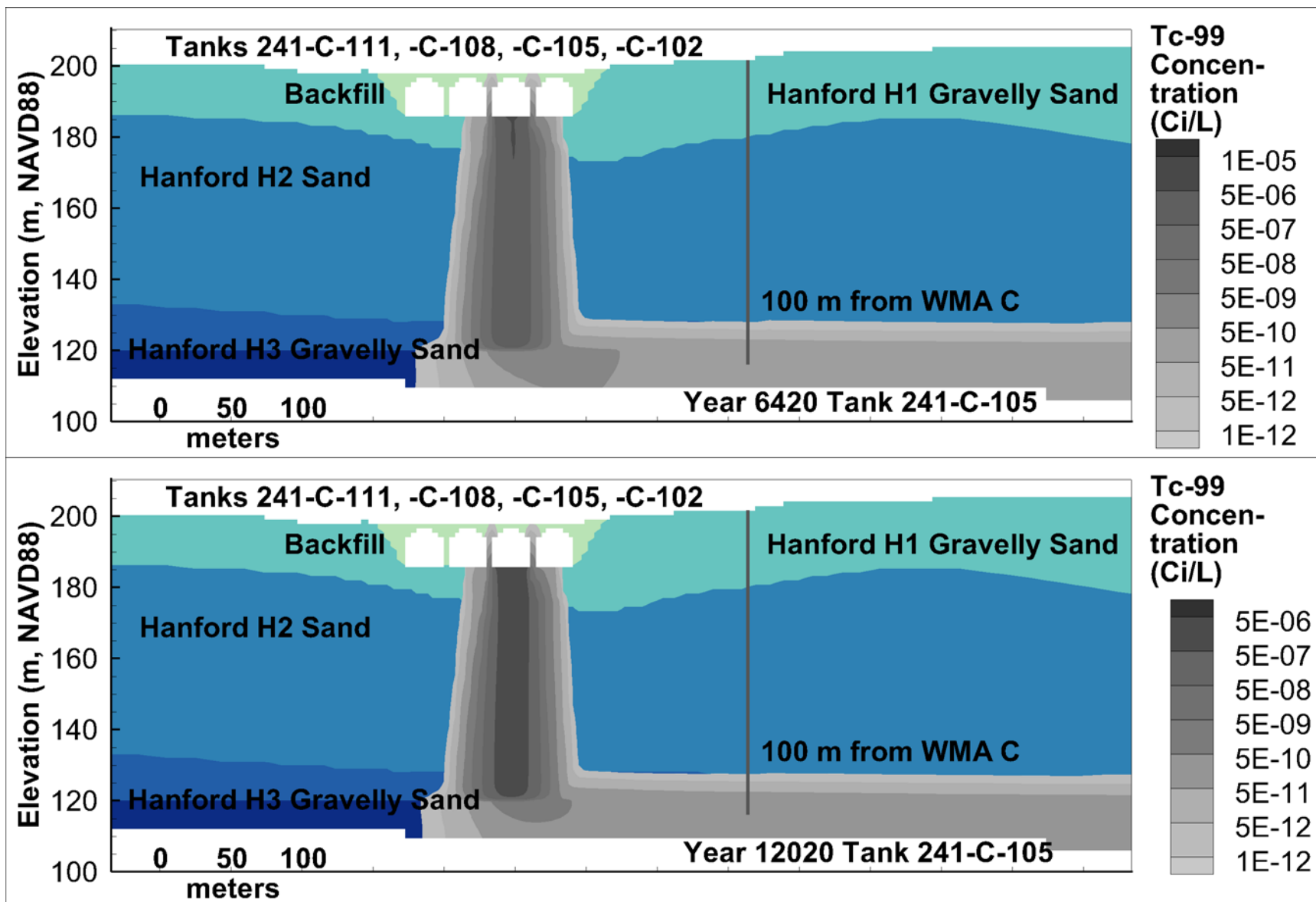
# Sample Model Results

- Diffusive release of 1 Ci of Tc-99 from C-105
- Breakthrough curves presented at 100 m points of calculation
- Spatial distribution of Tc-99 in groundwater at time of peak concentration
- Superposition of concentration from diffusive releases from additional tanks.

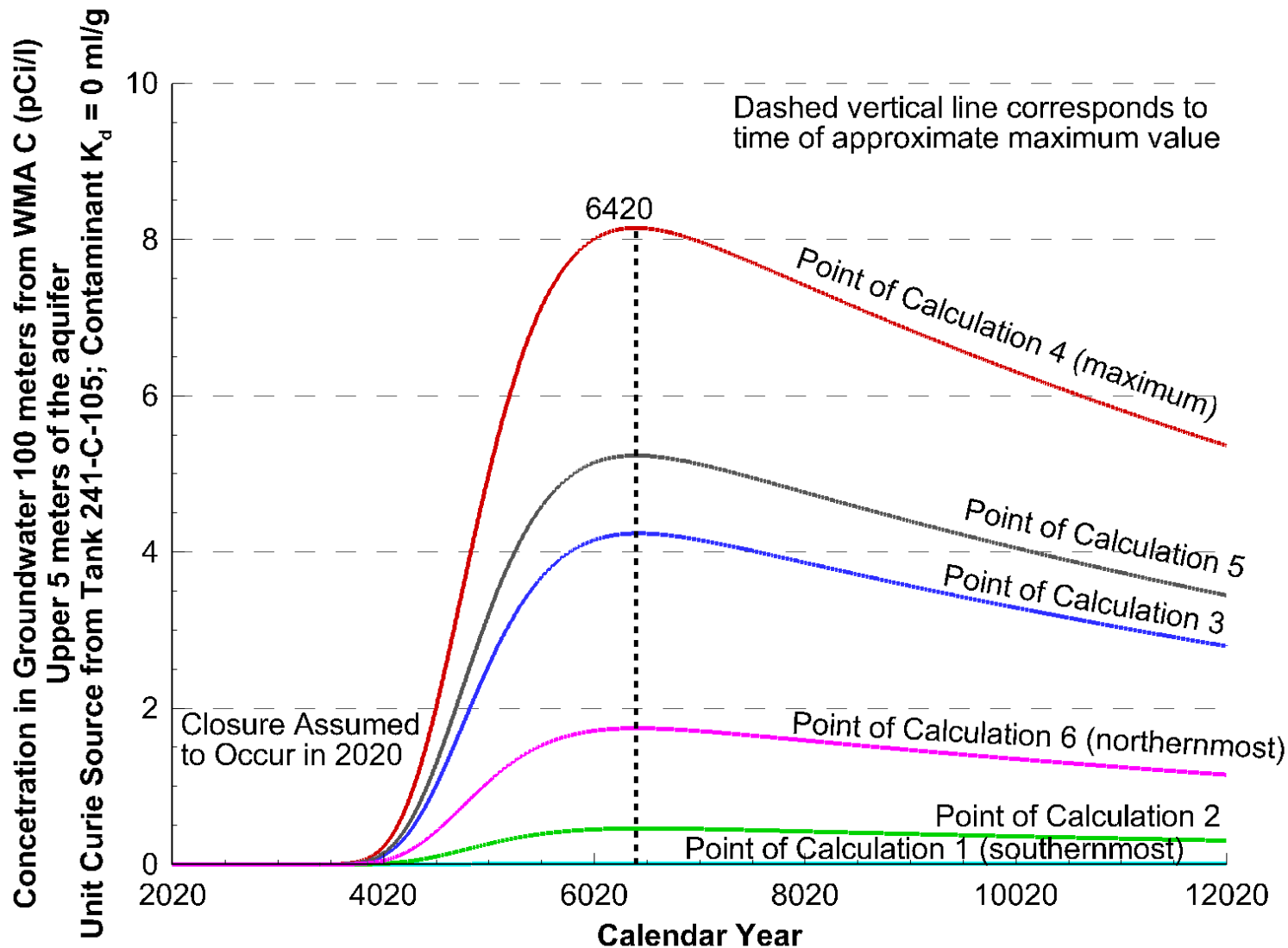
# WMA C Alternative Model I



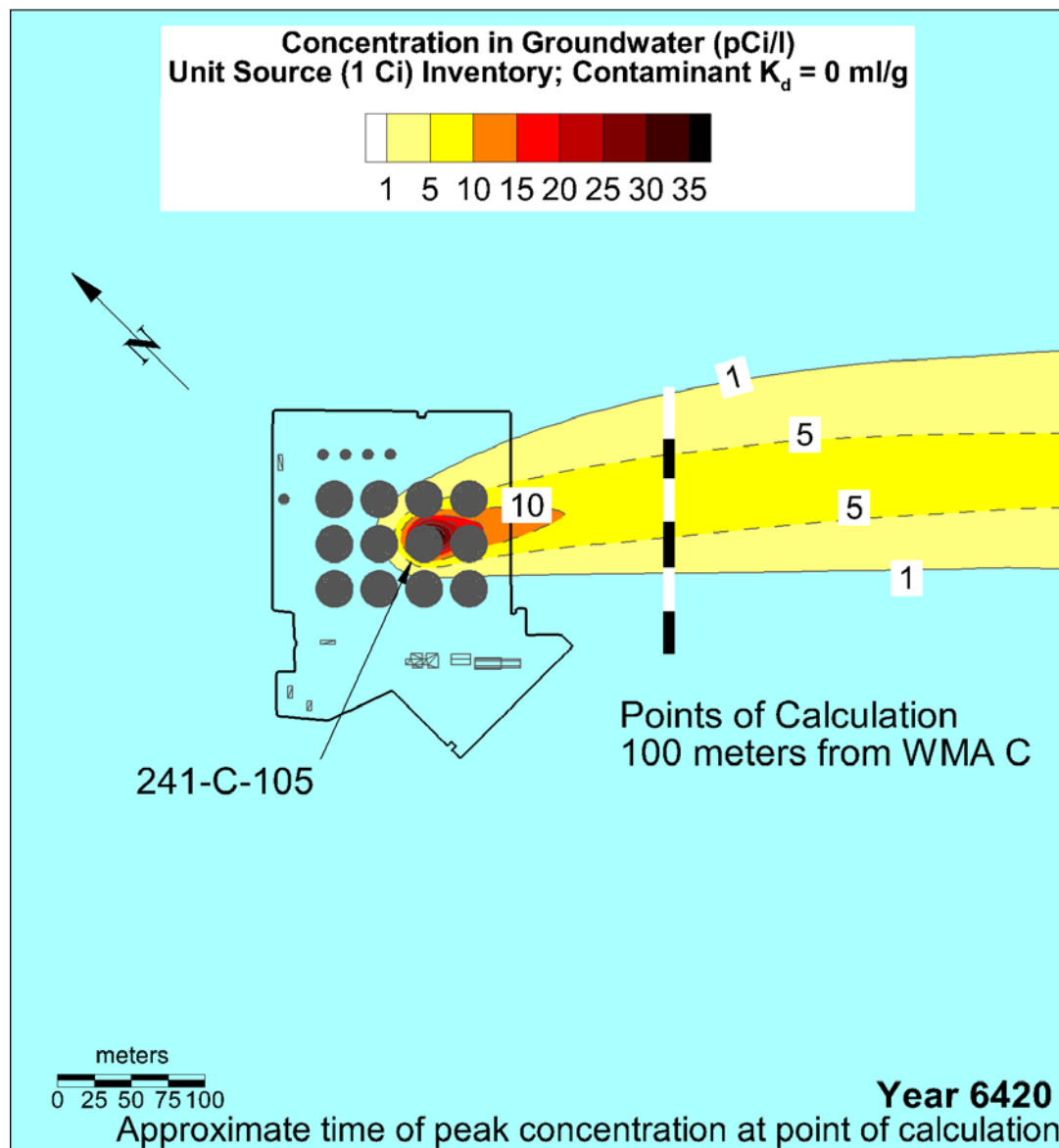
# WMA C Alternative Model I



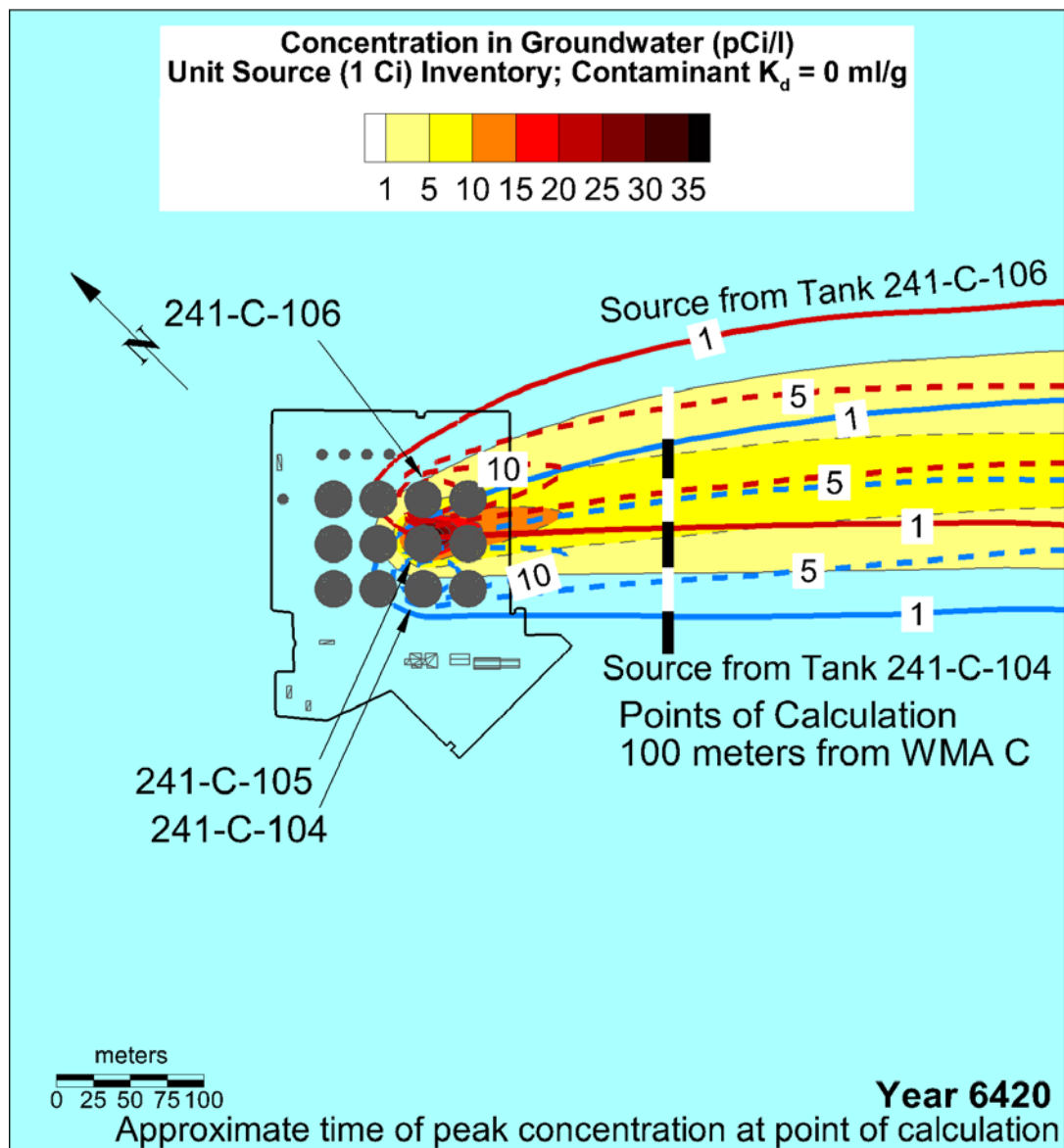
# Breakthrough Curves for Tank 241-C-105 Residual Waste Unit Source (1 Ci) Inventory; Contaminant $K_d = 0$ ml/g



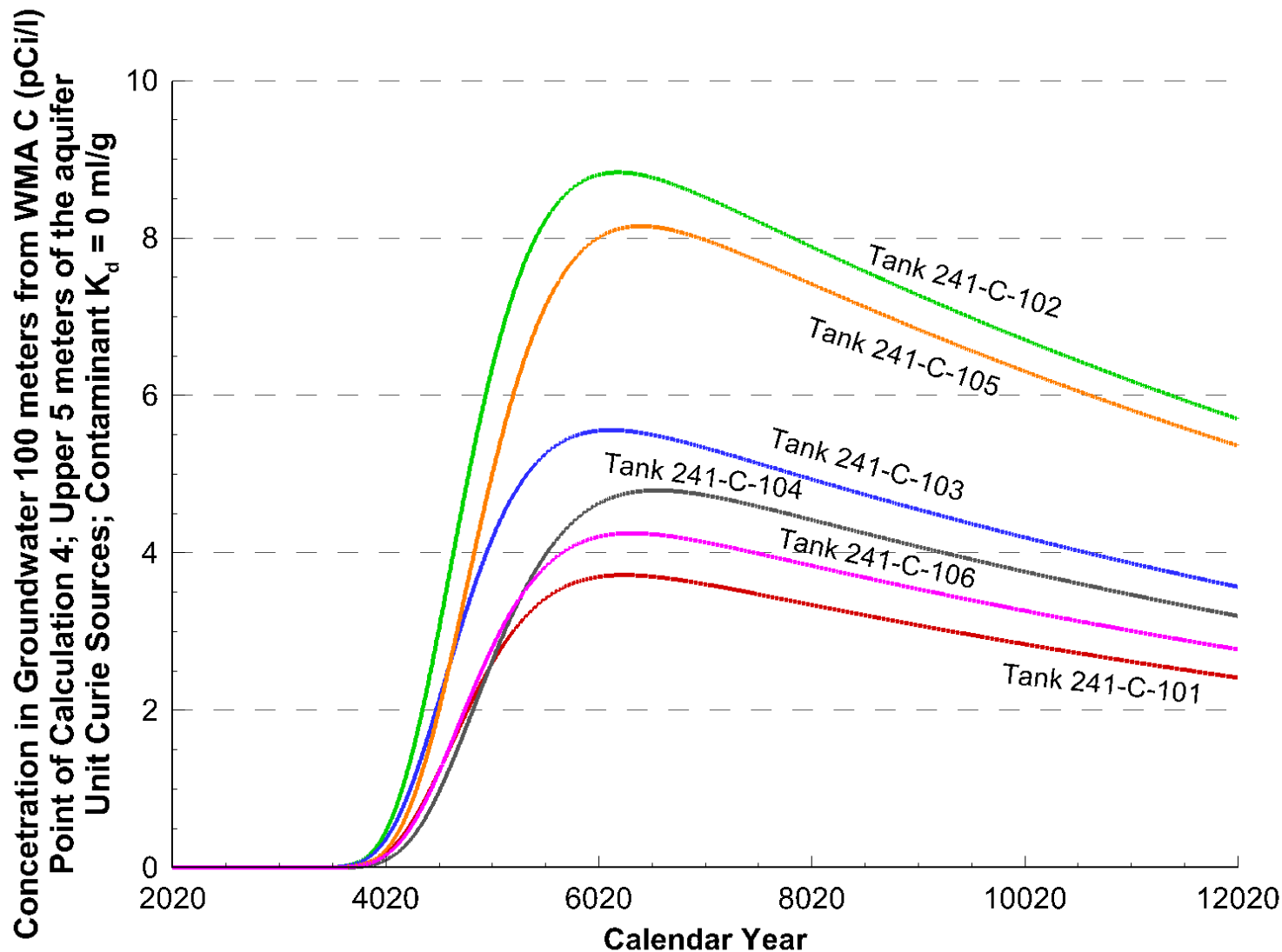
# Plan View of Tank 241-C-105 Residual Waste Fate and Transport Model Results



# Plan View of Fate and Transport Model Results: Plume Interaction



## Breakthrough Curves at Point of Calculation 4 Residual Waste Unit Sources (1 Ci); Contaminant $K_d = 0$ ml/g



## Contaminant Inventory and Mobility Arrival Time Evaluation

Which contaminants in the WMA C inventory are sufficiently mobile to impact groundwater within the 1,000 year and 10,000 year timeframes?

“Sufficiently mobile” = low enough distribution coefficient  $K_d$  value

### Long-Term Recharge Rates Associated With the Different Modeling Periods Used in the Arrival Time Evaluation

Period	Duration	Surface Condition of WMA C	Arrival Time Analysis Recharge Rate (mm/yr)
Pre-WMA C Construction	Steady state	Undisturbed natural conditions	5.2
WMA C Operational Period	1945.5 – 2020	Disturbed bare gravel surface	140
WMA C Post-Closure Period (500 Years)	2020 – 2520	Evapotranspiration (ET) surface barrier	1
WMA C Post-Closure Period (after 500 Years)	2520 – 12020	ET barrier reverts to natural conditions	5.2

Vadose Zone Properties Assigned the Maximum Transport Values Developed for the Uncertainty Analysis

## Contaminant Inventory and Mobility Arrival Time Evaluation Results

	Years to First Arrival					
	Distribution Coefficient $K_d$ (ml/g)					
Location	0.1	0.2	0.3	0.6	2.0	3.0
Water Table	547	975	1430	2740	8750	DNA
100 meters from WMA C	695	1080	1575	3029	9680	DNA

Contaminant Transport Starts Year 2030

Contaminant Release Concludes Year 2031

DNA = Did Not Arrive in 10,000 years.