

QUAD-CITIES NUCLEAR POWER STATION

UNITS 1 AND 2

MONTHLY PERFORMANCE REPORT

SEPTEMBER 1983

COMMONWEALTH EDISON COMPANY

AND

IOWA-ILLINOIS GAS & ELECTRIC COMPANY

NRC DOCKET NOS. 50-254 AND 50-265

LICENSE NOS. DPR-29 AND DPR-30

1E24

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I. INTRODUCTION

Quad-Cities Nuclear Power Station is composed of two Boiling Water Reactors, each with a Maximum Dependable Capacity of 769 MWe net, located in Cordova, Illinois. The Station is jointly owned by Commonwealth Edison Company and Iowa-Illinois Gas & Electric Company. The Nuclear Steam Supply Systems are General Electric Company Boiling Water Reactors. The Architect/Engineer was Sargent & Lundy, Incorporated, and the primary construction contractor was United Engineers & Constructors. The condenser cooling method is a closed cycle spray canal, and the Mississippi River is the condenser cooling water source. The plant is subject to license numbers DPR-29 and DPR-30, issued October 1, 1971, and March 21, 1972, respectively, pursuant to Docket Numbers 50-254 and 50-265. The date of initial reactor criticalities for Units 1 and 2 respectively were October 18, 1971, and April 26, 1972. Commercial generation of power began on February 18, 1973 for Unit 1 and March 10, 1973 for Unit 2.

This report was compiled by Becky Brown and Alex Misak, telephone number 309-654-2241, extensions 127 and 194.

II. SUMMARY OF OPERATING EXPERIENCE

A. UNIT ONE

September 1-7: Unit One began the month operating at 600 MWe due to low Service Water pressure as a result of high cooling canal temperature. This load was maintained until 0930 hours on September 4 when a normal load increase was initiated. The load increase was terminated at 0645 hours on September 5 with the load at 775 MWe.

September 8-14: Unit One dropped load to minimum Recirculation pump speed at 2200 hours on September 8 in preparation for beginning one Recirculation pump operation. At 0050 hours on September 9, the 1A Recirculation Pump Motor-Generator Set was tripped, and at 0250 hours the unit increased load with one Recirculation pump. The load increase was terminated at 0405 hours at 442 MWe. At 1405 hours the Station began open cycle cooling operation, and at 2210 hours the unit began dropping load to 390 MWe in order to achieve 50 percent thermal power. At 2315 hours the Station terminated open cycle cooling operation. At 2115 hours on September 14, the unit began dropping load in preparation for a scheduled Maintenance Outage.

September 15-22: At 0010 hours, on September 15, the Turbine was tripped, and at 0029 hours, the Reactor was manually scrammed as the unit was shutdown for maintenance. The unit was shutdown until 0555 hours on September 21 when the Reactor became critical. At 1355 hours the Reactor scrammed due to HI-HI IRM indication caused by the injection of cold Feedwater into the vessel for maintaining water level. The Reactor was critical again at 1751 hours, and the Generator was placed on line at 0814 hours on September 22. At 0815 hours, a normal load increase was initiated.

September 23-30: Unit One continued a normal load increase until 0900 hours on September 26 when the unit achieved full power with a load of 809 MWe. The unit maintained full power for the remainder of the month.

B. UNIT TWO

Unit Two began the month derated to approximately 350 MWe due to End of Cycle Fuel Depletion. The unit operated at this level until 0800 hours on September 4 when the unit dropped load in preparation for a scheduled Refueling and Maintenance Outage. The Generator was taken off line at 1202 hours and the Reactor was shutdown at 1505 hours. Unit Two remained shutdown for the remainder of the month.

III. PLANT OR PROCEDURE CHANGES, TESTS, EXPERIMENTS, AND SAFETY
RELATED MAINTENANCE

A. Amendments to Facility License or Technical Specifications

There were no amendments to the Facility License or Technical Specifications.

B. Facility or Procedure Changes Requiring NRC Approval

There were no Facility or Procedure changes requiring NRC approval for the reporting period.

C. Tests and Experiments Requiring NRC Approval

There were no Tests or Experiments requiring NRC approval for the reporting period.

D. Corrective Maintenance of Safety Related Equipment

The following represents a tabular summary of the major safety related maintenance performed on Unit One and Unit Two during the reporting period. This summary includes the following headings: Work Request Numbers, LER Numbers, Components, Cause of Malfunctions, Results and Effects on Safe Operation, and Action Taken to Prevent Repetition.

UNIT ONE MAINTENANCE SUMMARY

W.R. NUMBER	LER NUMBER	COMPONENT	CAUSE OF MALFUNCTION	RESULTS & EFFECTS ON SAFE OPERATION	ACTION TAKEN TO PREVENT REPETITION
Q25864		1B Off-Gas Suction Valve 1-5401-B	The valve sticks in the "open" position.	The valve serves as isolation of Condenser vacuum pump. The pump is normally isolated with a manual valve.	The valve was dis- assembled & the valve guides were repaired.
Q25865		1A Off-Gas Suction Valve 1-5401-A	The valve sticks in the "open" position.	The valve serves as auto-isolation for Condenser vacuum pump. This pump is normally isolated with a manual valve.	The valve was dis- assembled & the guides were repaired.
Q26655	83-24/03L	Vacuum Breaker 1-1601-33F, Division 2, Indication was Replaced.	The position in- dication switch malfunctioned.	The valve indication showed dual indication when the Operator attempted to close it. The Drywell/Torus Separation Test was run successfully; thus, the valve was actually closed.	The switch was replaced.
Q27700		LPRM 24-33A	Failed operational amplifier.	The LPRM was spiking high, and in bypass. The other LPRMs were working.	The operational amplifier was replaced on the LPRM circuit.
Q28026		Main Steamline Hi Flow Switch DPIS-1-261-2R had the Barton Switch Replaced.			

UNIT ONE MAINTENANCE SUMMARY

W.R. NUMBER	LER NUMBER	COMPONENT	CAUSE OF MALFUNCTION	RESULTS & EFFECTS ON SAFE OPERATION	ACTION TAKEN TO PREVENT REPETITION
Q28302	83-34/03L	1A Recirculation Pump Discharge Valve 1-202-5A	Cabling to the valve in the Dry- well was shorted- out.	The valve was declared inoperable. The 1A Recirculation pump was shutdown, and the unit was operated with one Recirculation pump. All required surveil- lances & limit adjustments were performed.	The cable was replaced during the dual unit outage.
Q28326		1-2301-48 Valve, HPCI Cooling Water	The motor came loose from the valve.	This valve is not required for HPCI to be operable.	The motor was replaced.
Q28204		HPCI Controller 1-2340-1	A resistor (R-5) on board 2-A amplifier failed.	HPCI was not declared inoperable. It was still capable of meeting all require- ments.	The resistor was replaced like-for-like.
Q28232		1-1001-23B Back-up Containment Spray Valve	Two motor bolts were broken & the torque switch was out of adjustment.	The valve would not open from the Control Room. It was moved off the seat by hand and then opened from the Control Room & stroked three times and worked properly.	The motor bolts were replaced and the torque switch was adjusted during the dual unit outage (9-14 through 9-20). Also, the valve was successfully stroked three times & timed.

UNIT ONE MAINTENANCE SUMMARY

W.R. NUMBER	LER NUMBER	COMPONENT	CAUSE OF MALFUNCTION	RESULTS & EFFECTS ON SAFE OPERATION	ACTION TAKEN TO PREVENT REPETITION
Q28233		1-1001-7D Suppression to 1D RHR Pump Suction Valve	Limit switches were out of adjustment.	The valve went full- closed twice and only part closed four times out of six. Because the safe position for this valve is OPEN, and no problem was encountered opening the valve, the valve was inoperable.	The limit switches were adjusted and the pump start interlocks were adjusted. The valve was then stroked and timed.
Q28485	83-35/03L	1-203-3A Target Rock Safety Relief Valve	The seal on the pilot valve was worn, preventing immediate seating.	The unit was scrambled. This event occurred during a planned shut- down.	The valve was replaced.
Q28584		M0-1-220-1 Main Steamline Drain Valve	The disk and seat were worn.	This valve's leak rate put the total, as found leakage, over the Local Leak Rate limit.	A high spot on the guide was filed down. See Work Requests Q28594 and Q28637.
Q28594		Main Steamline Drain Valve 1-220-2	The seat and disk were worn.	The volume bounded by 1-220-2 & 1-220-1 leaked enough to put the total local leakage over the Tech Spec limit.	The seat and disk were machined and the valves were leak rate tested.
Q28637		Main Steamline Drain Valve 1-220-1	The seat and disk were worn.	The volume bounded by 1-220-2 & 1-220-1 leaked enough to put the leakage over the Tech Spec limit.	The seat and disk were machined and the valves were leak rate tested. See Work Requests Q28594 & Q28584.

UNIT ONE MAINTENANCE SUMMARY

W.R. NUMBER	LER NUMBER	COMPONENT	CAUSE OF MALFUNCTION	RESULTS & EFFECTS ON SAFE OPERATION	ACTION TAKEN TO PREVENT REPETITION
Q28658	83-36/03L	1D Main Steamline Penetration to 'D' Heater Bay (MK-110)	Deterioration of penetration boot material.	The Secondary Containment Integrity Test was successfully performed before discovery of the crack, so the safety consequences were minimal.	The boot was replaced and sealed.

UNIT TWO MAINTENANCE SUMMARY

W.R. NUMBER	LER NUMBER	COMPONENT	CAUSE OF MALFUNCTION	RESULTS & EFFECTS ON SAFE OPERATION	ACTION TAKEN TO PREVENT REPETITION
Q27841		Core Spray Suction Valve MO 2-1402-3B	Auxiliary contacts were bad.	The valve would not open after being closed. It was opened by hand and left there. Unit was in refueling outage.	New auxiliary contacts were installed.
Q28320		Unit 2 24 VDC 2A1 Battery Charger	One of the battery cells failed by shorting, thus causing charger voltage to drop.	The charger voltage dropped. Consequently, a half-scam was received when IRMs 11, 12, 13 & 14 and SRMs went inoperable.	The failed battery was replaced.

IV. LICENSEE EVENT REPORTS

The following is a tabular summary of all licensee event reports for Quad-Cities Units One and Two occurring during the reporting period, pursuant to the reportable occurrence reporting requirements as set forth in Sections 6.6.B.1. and 6.6.B.2. of the Technical Specifications.

<u>UNIT ONE</u>		
<u>Licensee Event Report Number</u>	<u>Date</u>	<u>Title of Occurrence</u>
83-32/03L	9-1-83	Secondary Containment Test Failure
83-34/03L	9-8-83	1A LPCI Loop Inoperable
83-35/03L	9-15-83	Target Rock, 1-203-3A, Stuck Open
83-36/03L	9-20-83	Secondary Containment Broken
83-37/03L	9-23-83	Unit One Not Inerted Within 24 Hours
<u>UNIT TWO</u>		
83-13/03L	9-1-83	CRD 10-39 Overtravel
83-14/03L	9-6-83	2A MSIV Failed Local Leak Rate Test
83-15/03L	9-12-83	Containment Leakage Exceeded 0.6 LA
83-16/03L	9-12-83	HPCI High Temperature 2370D & 2371D

V. DATA TABULATIONS

The following data tabulations are presented in this report:

- A. Operating Data Report
- B. Average Daily Unit Power Level
- C. Unit Shutdowns and Power Reductions

OPERATING DATA REPORT

DOCKET NO. 50-254

UNIT ONE

DATE October 7

COMPLETED BY Alex L. Misak

TELEPHONE 309-654-2241x194

OPERATING STATUS

0000 090183

1. Reporting period: 2400 093083 Gross hours in reporting period: 720

2. Currently authorized power level (MWt): 2511 Max. Depend capacity (MWe-Net): 769* Design electrical rating (MWe-Net): 789

3. Power level to which restricted (if any) (MWe-Net): NA

4. Reasons for restriction (if any):

	This Month	Yr. to Date	Cumulative
5. Number of hours reactor was critical	<u>566.6</u>	<u>6170.2</u>	<u>81361.4</u>
6. Reactor reserve shutdown hours	<u>0.0</u>	<u>0.0</u>	<u>3421.9</u>
7. Hours generator on line	<u>543.9</u>	<u>6075.4</u>	<u>78162.1</u>
8. Unit reserve shutdown hours.	<u>0.0</u>	<u>0.0</u>	<u>909.2</u>
9. Gross thermal energy generated (MWH)	<u>1063390</u>	<u>13693423</u>	<u>159906414</u>
10. Gross electrical energy generated (MWH)	<u>340808</u>	<u>4132301</u>	<u>51554182</u>
11. Net electrical energy generated (MWH)	<u>315945</u>	<u>4165133</u>	<u>47994041</u>
12. Reactor service factor	<u>78.7</u>	<u>94.5</u>	<u>81.5</u>
13. Reactor availability factor	<u>78.7</u>	<u>94.5</u>	<u>84.9</u>
14. Unit service factor	<u>75.5</u>	<u>92.7</u>	<u>78.3</u>
15. Unit availability factor	<u>75.5</u>	<u>92.7</u>	<u>79.2</u>
16. Unit capacity factor (Using MDC)	<u>56.9</u>	<u>82.6</u>	<u>62.5</u>
17. Unit capacity factor (Using Des. MWe)	<u>55.4</u>	<u>80.5</u>	<u>60.9</u>
18. Unit forced outage rate	<u>3.3</u>	<u>2.3</u>	<u>6.4</u>

19. Shutdowns scheduled over next 6 months (Type, Date, and Duration of each):

20. If shutdown at end of report period, estimated date of start up NA

*The MDC may be lower than 769 MWe during periods of high ambient temperature due to the thermal performance of the spray canal.

#UNOFFICIAL COMPANY NUMBERS ARE USED IN THIS REPORT

OPERATING DATA REPORT

DOCKET NO. 50-265

UNIT TWO

DATE October 7

COMPLETED BY Alex L. Misak

TELEPHONE 309-654-2241x194

OPERATING STATUS

0000 090183

1. Reporting period: 2400 093083 Gross hours in reporting period: 720

2. Currently authorized power level (MWt): 2511 Max. Depend capacity (MWe-Net): 769* Design electrical rating (MWe-Net): 789

3. Power level to which restricted (if any) (MWe-Net): NA

4. Reasons for restriction (if any):

	This Month	Yr. to Date	Cumulative
5. Number of hours reactor was critical	<u>87.1</u>	<u>5654.1</u>	<u>77917.5</u>
6. Reactor reserve shutdown hours	<u>0.0</u>	<u>0.0</u>	<u>2985.6</u>
7. Hours generator on line	<u>84.0</u>	<u>5621.7</u>	<u>75209.8</u>
8. Unit reserve shutdown hours	<u>0.0</u>	<u>0.0</u>	<u>702.9</u>
9. Gross thermal energy generated (MWH)	<u>98588</u>	<u>10790594</u>	<u>155382088</u>
10. Gross electrical energy generated (MWH)	<u>28418</u>	<u>3398245</u>	<u>49435780</u>
11. Net electrical energy generated (MWH)	<u>19888</u>	<u>3157729</u>	<u>46341296</u>
12. Reactor service factor	<u>12.1</u>	<u>86.3</u>	<u>78.8</u>
13. Reactor availability factor	<u>12.1</u>	<u>86.3</u>	<u>81.8</u>
14. Unit service factor	<u>11.7</u>	<u>85.8</u>	<u>76.0</u>
15. Unit availability factor	<u>11.7</u>	<u>85.8</u>	<u>76.7</u>
16. Unit capacity factor (Using MDC)	<u>3.9</u>	<u>62.8</u>	<u>60.9</u>
17. Unit capacity factor (Using Des. MWe)	<u>3.8</u>	<u>61.2</u>	<u>59.4</u>
18. Unit forced outage rate	<u>0.0</u>	<u>1.8</u>	<u>8.6</u>

19. Shutdowns scheduled over next 6 months (Type, Date, and Duration of each):

20. If shutdown at end of report period, estimated date of startup 1-8-84

*The MDC may be lower than 769 MWe during periods of high ambient temperature due to the thermal performance of the spray canal.

#UNOFFICIAL COMPANY NUMBERS ARE USED IN THIS REPORT

APPENDIX B
AVERAGE DAILY UNIT POWER LEVEL

DOCKET NO. 50-254

UNIT ONE

DATE October 7

COMPLETED BY Alex L. Misak

TELEPHONE 309-654-2241x194

MONTH September 1983

DAY AVERAGE DAILY POWER LEVEL
(MWe-Net)

1.	<u>549.3</u>
2.	<u>562.2</u>
3.	<u>546.5</u>
4.	<u>618.1</u>
5.	<u>726.4</u>
6.	<u>724.4</u>
7.	<u>741.2</u>
8.	<u>730.7</u>
9.	<u>414.3</u>
10.	<u>354.8</u>
11.	<u>345.8</u>
12.	<u>339.5</u>
13.	<u>367.6</u>
14.	<u>317.5</u>
15.	<u>-13.7</u>
16.	<u>-10.6</u>

DAY AVERAGE DAILY POWER LEVEL
(MWe-Net)

17.	<u>-8.9</u>
18.	<u>-8.2</u>
19.	<u>-9.4</u>
20.	<u>-11.2</u>
21.	<u>-11.5</u>
22.	<u>255.0</u>
23.	<u>552.6</u>
24.	<u>586.3</u>
25.	<u>666.4</u>
26.	<u>755.2</u>
27.	<u>761.9</u>
28.	<u>745.5</u>
29.	<u>754.4</u>
30.	<u>773.5</u>

INSTRUCTIONS

On this form, list the average daily unit power level in MWe-Net for each day in the reporting month. Compute to the nearest whole megawatt.

These figures will be used to plot a graph for each reporting month. Note that when maximum dependable capacity is used for the net electrical rating of the unit, there may be occasions when the daily average power level exceeds the 100% line (or the restricted power level line). In such cases, the average daily unit power output sheet should be footnoted to explain the apparent anomaly.

APPENDIX B
AVERAGE DAILY UNIT POWER LEVEL

DOCKET NO. 50-265

UNIT TWO

DATE October 7

COMPLETED BY Alex L. Misak

TELEPHONE 309-654-2241x194

MONTH September 1983

DAY AVERAGE DAILY POWER LEVEL
(MWe-Net)

1.	<u>319.9</u>
2.	<u>313.8</u>
3.	<u>314.5</u>
4.	<u>122.3</u>
5.	<u>-15.6</u>
6.	<u>-6.4</u>
7.	<u>-9.3</u>
8.	<u>-8.0</u>
9.	<u>-7.0</u>
10.	<u>-8.3</u>
11.	<u>-8.3</u>
12.	<u>-8.4</u>
13.	<u>-8.3</u>
14.	<u>-8.0</u>
15.	<u>-9.2</u>
16.	<u>-7.6</u>

DAY AVERAGE DAILY POWER LEVEL
(MWe-Net)

17.	<u>-7.6</u>
18.	<u>-7.5</u>
19.	<u>-7.5</u>
20.	<u>-7.9</u>
21.	<u>-7.6</u>
22.	<u>-6.7</u>
23.	<u>-4.6</u>
24.	<u>-3.3</u>
25.	<u>-2.4</u>
26.	<u>-2.2</u>
27.	<u>-2.6</u>
28.	<u>-1.9</u>
29.	<u>-2.3</u>
30.	<u>-2.8</u>

INSTRUCTIONS

On this form, list the average daily unit power level in MWe-Net for each day in the reporting month. Compute to the nearest whole megawatt.

These figures will be used to plot a graph for each reporting month. Note that when maximum dependable capacity is used for the net electrical rating of the unit, there may be occasions when the daily average power level exceeds the 100% line (or the restricted power level line). In such cases, the average daily unit power output sheet should be footnoted to explain the apparent anomaly.

ID/5A

APPENDIX D
UNIT SHUTDOWNS AND POWER REDUCTIONS

QTP 300-S13

Revision 6

August 1982

DOCKET NO. 050-254

UNIT NAME Quad-Cities Unit One

COMPLETED BY Alex Misak

DATE October 3, 1983

REPORT MONTH SEPTEMBER 1983

TELEPHONE 309-654-2241

NO.	DATE	TYPE F OR S	DURATION (HOURS)	REASON	METHOD OF SHUTTING DOWN REACTOR	LICENSEE EVENT REPORT NO.	SYSTEM CODE	COMPONENT CODE	CORRECTIVE ACTIONS/COMMENTS
83-59	830908	S	0.0	B	5		CB	VALVEX	Reduced load to test 1-202-5A valve
83-60	830908	F	0.0	D	5		CB	VALVEX	Reduced load to 50% thermal power for one Recirculation loop operation
83-61	830915	S	157.8	B	1		CB	VALVEX	Unit shutdown for maintenance on the 1-202-5A valve
83-62	830921	F	18.3	G	3		IA	INSTRU	Unit scrammed during startup due to Hi-Hi IRM indication caused by the injection of cold feedwater into the vessel for maintaining water level
83-63	830924	S	0.0	H	5		RC	FUELXX	Reduced load to change control rod pattern

APPROVED

AUG 16 1982

ID/5A

APPENDIX D
UNIT SHUTDOWNS AND POWER REDUCTIONSQTP 300-S13
Revision 6
August 1982

DOCKET NO. 050-265

UNIT NAME Quad-Cities Unit Two

COMPLETED BY Alex Misak

DATE October 3, 1983

REPORT MONTH SEPTEMBER 1983

TELEPHONE 309-654-2241

NO.	DATE	TYPE F OR S	DURATION (HOURS)	REASON	METHOD OF SHUTTING DOWN REACTOR	LICENSEE EVENT REPORT NO.	SYSTEM CODE	COMPONENT CODE	CORRECTIVE ACTIONS/COMMENTS
83-65	830904	S	0.0	H	5		RC	FUELXX	Load reduced in preparation for End of Cycle Six Refueling Outage
83-66	830904	S	636.0	C	1		RC	FUELXX	Unit shutdown for End of Cycle Six Refueling Outage

APPROVED
AUG 16 1982

VI. UNIQUE REPORTING REQUIREMENTS

The following items are included in this report based on prior commitments to the commission:

A. MAIN STEAM RELIEF VALVE OPERATIONS

Relief valve operations during the reporting period are summarized in the following table. The table includes information as to which relief valve was actuated, how it was actuated, and the circumstances resulting in its actuation.

<u>UNIT</u>	<u>DATE</u>	<u>VALVES ACTUATED</u>	<u>NO. & TYPE ACTUATIONS</u>	<u>PLANT CONDITIONS</u>	<u>DESCRIPTION OF EVENTS</u>
2	9-04-83	2-203-3A 2-203-3B 2-203-3C 2-203-3D 2-203-3E	1 Manual 1 Manual 1 Manual 1 Manual 1 Manual	Rx Press 972	Surveillance T.S. 4.5.D.1.b
1	9-15-83	1-203-3A	1 Manual	Rx Press 920	Surveillance T.S. 4.5.D.1.b (stuck open to 360 psig)
1	9-22-83	1-203-3A	1 Manual	Rx Press 910	Surveillance T.S. 4.5.D.1.b (Post- Maintenance; Replaced Valve)
1	9-22-83	1-203-3B 1-203-3C 1-203-3D 1-203-3E	1 Manual 1 Manual 1 Manual 1 Manual	Rx Press 910	Surveillance T.S. 4.5.D.1.b (Post- Maintenance; Replaced Pilot Valve)

B. CONTROL ROD DRIVE SCRAM TIMING DATA FOR UNITS ONE AND TWO

The basis for reporting this data to the Nuclear Regulatory Commission are specified in the surveillance requirements of Technical Specifications 4.3.C.1 and 4.3.C.2.

The following table is a complete summary of Units One and Two Control Rod Drive Scram Timing for the reporting period. All scram timing was performed with Reactor pressure greater than 800 psig.

PERFORMED ON UNIT 1 CONTROL

DATE	NUMBER OF RODS	AVERAGE TIME IN SECONDS AT % INSERTED FROM FULLY WITHDRAWN				Max. Time For 90% Insertion	DESCRIPTION
		5	20	50	90		
		0.375	0.900	2.00	3.5		
9-14	88	0.28	0.65	1.40	2.50	2.96 (G-10)	Technical Specification 3.3.C.1 & 3.3.C.2 (Average Scram Insertion Time) Unit One Hot Scram Time "A" Sequence

VII. REFUELING INFORMATION

The following information about future reloads at Quad-Cities Station was requested in a January 26, 1978, licensing memorandum (78-24) from D. E. O'Brien to C. Reed, et al., titled "Dresden, Quad-Cities, and Zion Station--NRC Request for Refueling Information", dated January 18, 1978.

QUAD-CITIES REFUELING
INFORMATION REQUEST

QTP 300-S32
Revision 1
March 1978

- *
1. Unit: Q1 Reload: 6 Cycle: 7
2. Scheduled date for next refueling shutdown: 9-6-82
3. Scheduled date for restart following refueling: 12-18-82
4. Will refueling or resumption of operation thereafter require a technical specification change or other license amendment: Yes
5. Scheduled date(s) for submitting proposed licensing action and supporting information: 8-19-82: Tech. Spec. changes submitted to the NRC.
6. Important licensing considerations associated with refueling, e.g., new or different fuel design or supplier, unreviewed design or performance analysis methods, significant changes in fuel design, new operating procedures:
- a) All 7x7 fuel assemblies will be removed from the core.
 - b) MAPLHGR curves for fuel types in the core are being extended to 40,000 MWD/ST.
 - c) MCPR limits will be determined by GE's ODYN computer code.
 - d) The vessel pressure safety limit is being modified to accommodate the potential for higher reactor pressures as calculated by ODYN.
7. The number of fuel assemblies.
- a. Number of assemblies in core: 724
 - b. Number of assemblies in spent fuel pool: 800
8. The present licensed spent fuel pool storage capacity and the size of any increase in licensed storage capacity that has been requested or is planned in number of fuel assemblies:
- a. Licensed storage capacity for spent fuel: 3657
 - b. Planned increase in licensed storage: 0
9. The projected date of the last refueling that can be discharged to the spent fuel pool assuming the present licensed capacity: 2003

APPROVED

APR 20 1978

Q. C. O. S. R.

QUAD-CITIES REFUELING
INFORMATION REQUEST

QTP 300-S32
Revision 1
March 1978

- *
1. Unit: Q2 Reload: 6 Cycle: 7
2. Scheduled date for next refueling shutdown: 9-5-83
3. Scheduled date for restart following refueling: 11-12-83
4. Will refueling or resumption of operation thereafter require a technical specification change or other license amendment:
No, however, a change to the Technical Specifications is being submitted (see below).
5. Scheduled date(s) for submitting proposed licensing action and supporting information:
June 14, 1983 (Scheduled)
6. Important licensing considerations associated with refueling, e.g., new or different fuel design or supplier, unreviewed design or performance analysis methods, significant changes in fuel design, new operating procedures:
a) All new fuel assemblies will be of barrier design; MAPLHGR curves will be re-labeled to include the barrier designation.
b) The use of improved assumptions in the load reject without bypass analysis resulted in a much improved MCPR operating limit. Technical Specifications are being changed to provide this additional operating margin.
7. The number of fuel assemblies.
a. Number of assemblies in core: 724
b. Number of assemblies in spent fuel pool: 204
8. The present licensed spent fuel pool storage capacity and the size of any increase in licensed storage capacity that has been requested or is planned in number of fuel assemblies:
a. Licensed storage capacity for spent fuel: 3897
b. Planned increase in licensed storage: 0
9. The projected date of the last refueling that can be discharged to the spent fuel pool assuming the present licensed capacity: 2003

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VIII. GLOSSARY

The following abbreviations which may have been used in the Monthly Report, are defined below:

ACAD/CAM	-	Atmospheric Containment Atmospheric Dilution/Containment Atmospheric Monitoring
ANSI	-	American National Standards Institute
APRM	-	Average Power Range Monitor
ATWC	-	Anticipated Transient Without Scram
BWR	-	Boiling Water Reactor
CRD	-	Control Rod Drive
EHC	-	Electro-Hydraulic Control System
EOF	-	Emergency Operations Facility
GSEP	-	Generating Stations Emergency Plan
HEPA	-	High-Efficiency Particulate Filter
HPCI	-	High Pressure Coolant Injection System
HRSS	-	High Radiation Sampling System
IPCLRT	-	Integrated Primary Containment Leak Rate Test
IRM	-	Intermediate Range Monitor
ISI	-	Inservice Inspection
LER	-	Licensee Event Report
LLRT	-	Local Leak Rate Test
LPCI	-	Low Pressure Coolant Injection Mode of RHRS
LPRM	-	Local Power Range Monitor
MAPLHGR	-	Maximum Average Planar Linear Heat Generation Rate
MCPR	-	Minimum Critical Power Ratio
MFLCPR	-	Maximum Fraction Limiting Critical Power Ratio
MPC	-	Maximum Permissible Concentration
MSIV	-	Main Steam Isolation Valve
NIOSH	-	National Institute for Occupational Safety and Health
PCI	-	Primary Containment Isolation
PCOMR	-	Preconditioning Interim Operating Management Recommendations
RBCCW	-	Reactor Building Closed Cooling Water System
RBM	-	Rod Block Monitor
RCIC	-	Reactor Core Isolation Cooling System
RHRS	-	Residual Heat Removal System
RPS	-	Reactor Protection System
RWM	-	Rod Worth Minimizer
SBGTS	-	Standby Gas Treatment System
SBLC	-	Standby Liquid Control
SDC	-	Shutdown Cooling Mode of RHRS
SDV	-	Scram Discharge Volume
SRM	-	Source Range Monitor
TBCCW	-	Turbine Building Closed Cooling Water System
TIP	-	Traversing Incore Probe
TSC	-	Technical Support Center



Commonwealth Edison

Quad Cities Nuclear Power Station
22710 206 Avenue North
Cordova, Illinois 61242
Telephone 309/654-2241

NJK-83-350

October 3, 1983

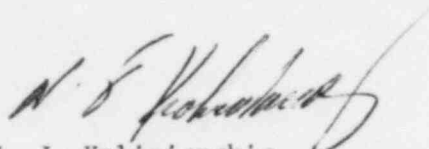
Director, Office of Inspection & Enforcement
United States Nuclear Regulatory Commission
Washington, D. C. 20555
Attention: Document Control Desk

Gentlemen:

Enclosed for your information is the Monthly Performance Report covering the operation of Quad-Cities Nuclear Power Station, Units One and Two, during the month of September 1983.

Very truly yours,

COMMONWEALTH EDISON COMPANY
QUAD-CITIES NUCLEAR POWER STATION


N. J. Kalivianakis
Station Superintendent

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Enclosure

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