

## EMERGENCY PLAN IMPLEMENTING PROCEDURES

## REVISION CONTROL SHEET

Revision No. 13Revision Date 5/25/83

Page/Proc	Date	Rev.	Page/Proc	Date	Rev.	Page/Proc	Date	Rev.
INDEX	3-15-83	6						
1.1	3-1-82	1						
1.2	6/9/82	2						
1.3	1-13-83	0						
2.1	1/15/82	2						
2.2	10/4/82	4						
2.3	12/2/81	0						
3.1	3/1/82	2						
3.2	3/1/82	3						
3.3a	3/11/83	2						
3.3b	4/11/83	2						
4.1	DELETED							
4.2	5/11/81	0						
4.3	10/19/81	1						
4.4	7/30/82	1						
4.5	5/13/82	0						
5.1	11/24/81	1						
5.2	11/24/81	1						
6.1	5/11/81	0						
6.2	5/11/81	0						
6.3	3/1/82	1						
6.4	3/19/83	3						

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3a
INITIAL DOSE PROJECTIONS	Page 1 of 41
	Revision 2
	Date 3/11/83

## 1.0 PURPOSE

This procedure provides instructions for estimating the downwind dose rates resulting from noble gas and radioiodine releases immediately following an emergency at DAEC.

## 2.0 APPLICABILITY

This procedure applies to immediate specific steps to be taken by control room operations personnel during a release of radioactive materials to the environment.

## 3.0 RESPONSIBILITIES

### 3.1 Shift Supervising Engineer

Perform dose projection calculations until the Site Radiation Protection Coordinator arrives or the EOF is manned.

### 3.2 Site Radiation Protection Coordinator

Initially evaluate the results of dose projection calculations.

Initially identify the need for field survey data to backup projected dose calculations.

### 3.3 Emergency Coordinator

Initially advise local and State authorities of the results of dose projection calculations and provide protective action recommendations as required.

## 4.0 INTRODUCTION

The major objective of this procedure is to perform the offsite dose estimate for comparison with protective action guidelines to determine the appropriate emergency action to be taken following an accidental atmospheric release of radioactive material. As a result of this objective the procedure has been developed with four major parts. The first consists of the main body of the procedure and contains general information about the procedure, general instructions for its use and the protective action guidelines. The second part consists of a Data Summary Sheet, Attachment I, which contains all the monitor data necessary for the dose projections. The third part, Attachment II, consists of a summary Table to be completed during the dose estimation procedure. This table contains all the information necessary for comparison with the protective action guidelines. The completion of this table requires a number of calculations to be performed. These calculations are set up in detail on Calculation Sheets which comprise the fourth part of the procedure, Attachment III. The Data Summary Sheet, Summary Table, and the Calculation Sheets are designed to be used together, that is, the Calculation Sheets are required to complete the Summary Table while

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3a
INITIAL DOSE PROJECTIONS	Page 2 of 41
	Revision 2
	Date 3/11/83

information from the Data Summary Sheet and Summary Table is required in many of the calculations performed on the Calculation Sheets. When calculations are required the Summary Table references the appropriate segment of the Calculation Sheets to be completed, likewise when data is required from the Data Summary Sheet and Summary Table the appropriate Data Summary Sheet or Summary Table line number is referenced on the Calculation Sheet.

#### NOTE

A supply of Data Summary Sheets, Summary Tables, and Calculation Sheets are to be maintained in the Control Room and Technical Support Center (TSC) for emergency use.

#### 5.0 INSTRUCTIONS

- 5.1 This simplified method shall be used by operations personnel for determining initial dose estimates only. It should be used until the Site Radiation Protection Coordinator arrives, but not beyond one(1) hour after shutdown. At that time, EPIP 3.3b shall be used.

One (1) hour after shutdown decay factor.

- 5.2 If an accidental atmospheric release of radioactive material has been identified or there is a significant change in the release rate a dose projection is to be performed as follows.

5.2.1 Complete Data Summary Sheet.

5.2.2 Complete Section I of the Summary Table, General Information, using Calculation Sheet I where referenced.

5.2.3 Complete Section II of the Summary Table, Release Information, to determine the total gaseous release rate from the Reactor Building Stacks, the Offgas Stack, and the Turbine Building Roof Exhaust. Use Calculation Sheet II, where referenced, to perform the necessary release rate calculations.

When multiple monitor ranges are available complete the calculations for ONE range ONLY. Use the range which gives a reading nearest mid-scale.

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3a
INITIAL DOSE PROJECTIONS	Page 3 of 41
	Revision 2
	Date 3/11/83

- 5.2.4 Complete Section III of the Summary Table, Dose Information. Use Calculation Sheet III, where referenced, to perform all necessary calculations. Calculation Sheet III is divided into five sections of which only two are to be completed. Section I is always completed and determines, based on the atmospheric stability, which one of the remaining four sections is to be used to perform the dose estimation. The Calculation Sheet subsections referenced in Section III of the Summary Table are those of the appropriate section for dose estimation as determined by Section I. That is, Sections II through V of Calculation Sheet III have the same format only the constants which are dependent on atmospheric stability are different.
- 5.2.5 Report the results of the dose estimation calculations, i.e., supply copies of the Summary Table, to the Emergency Coordinator and/or the Site Radiation Protection Coordinator.
- 5.2.6 The Operations Shift Supervisor shall compare the dose estimates from the Summary Table to the following Protective Action Guidelines and initiate the appropriate action until the Site Radiation Protection Coordinator is available.

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3a
INITIAL DOSE PROJECTIONS	Page 4 of 41
	Revision 2
	Date 3/11/83

### PROTECTIVE ACTION GUIDELINES

#### Projected Exposure to An Individual in the Population

#### Recommended Action

Whole Body = less than 1 Rem or  
Thyroid = less than 5 Rem.

1. No protective action required.
2. Issue an advisory to seek shelter and await further instructions or voluntarily evacuate.
3. Monitor environmental radiation levels.

Whole Body = 1 to 5 Rem or  
Thyroid = 5 to 25 Rem

1. Seek shelter and await further instructions.
2. Consider evacuation, particularly for children and pregnant women.
3. Monitor environmental radiation levels.
4. Control access.

Whole Body = 5 Rem and above or  
Thyroid = 25 Rem and above

1. Conduct evacuation of populations in the predetermined area.
2. Monitor environmental radiation levels and adjust area for evacuation based on these controls.
3. Control access.

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3a
INITIAL DOSE PROJECTIONS	Page 5 of 41
	Revision 2
	Date 3/11/83

## 6.0 REFERENCES

1. Duane Arnold Energy Center Emergency Plan
2. IELP Corporate Emergency Response Plan

## 7.0 ATTACHMENTS

1. Data Summary Sheet
2. Summary Table
3. Calculation Sheets

APPROVED BY: Keith Young DATE: 4/28/83  
Radiation Protection Supervisor

REVIEWED BY: H. S. - George DATE: 4-9-83  
ALARA Coordinator

APPROVED BY: RE Zook for DATE: 4-30-83  
Operations Supervisor

REVIEWED BY: BR York DATE: 4-30-83  
Chairman, Operations Committee

APPROVED BY: BR York for DATE: 4-30-83  
Plant Superintendent - Nuclear



EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3a
INITIAL DOSE PROJECTIONS	Page 7 of 41
	Revision 2
	Date 3/11/83

ATTACHMENT I, DATA SUMMARY SHEET (continued)

- B. Offgas Stack - obtain release concentration from the effluent monitoring system.

Range

1. Offgas Stack Conc.<sup>a</sup> \_\_\_\_\_ uCi/cc    Hi ☐ Int. ☐ Nor. ☐

2. Offgas Stack Flow<sup>c</sup> \_\_\_\_\_ cfm

- C. Turbine Exhaust - obtain release concentration from the effluent monitoring system.

1. Turb. Exhaust Conc.<sup>a</sup> \_\_\_\_\_ uCi/cc    Hi ☐ Int. ☐ Nor. ☐

2. Turb. Exhaust Flow<sup>d</sup> \_\_\_\_\_ cfm

Notes (a-d):

- Data collected from Kaman Effluent Monitoring System see PASAP 6.0 and PCP 10.6A for system operating instructions.
- Data available either from the Kaman Effluent Monitoring System or from Control Room Panel 1C-23.
- Data available either from the Kaman Effluent Monitoring System or from Control Room Panel 1C-02.
- Data available either from the Kaman Effluent Monitoring System or can be estimated by:
  - 18,000 cfm for each fan in slow speed
  - 36,000 cfm for each fan in fast speed

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3a
INITIAL DOSE PROJECTIONS	Page 8 of 41
	Revision 2
	Date 3/11/83

ATTACHMENT I, DATA SUMMARY SHEET (continued)

D. Miscellaneous Data

1. Is Standby Gas Treatment for Offgas Stack Exhaust in operation:

YES ☐ NO ☐

2. Anticipated duration of release \_\_\_\_\_ hours. (If no estimate is available use 1.77 hours.)

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3a
INITIAL DOSE PROJECTIONS	Page 9 of 41
	Revision 2
	Date 3/11/83

## ATTACHMENT II, SUMMARY TABLE

Calculations Performed By: \_\_\_\_\_

### I. GENERAL INFORMATION

1. Calculation Number: \_\_\_\_\_ Date: \_\_\_\_\_ Time: \_\_\_\_\_
2. Time after Shutdown: \_\_\_\_\_ hours
3. Wind Direction: \_\_\_\_\_ deg. (Data Summary Sheet Section I, line 1).
4. Down Wind Direction: \_\_\_\_\_ deg. (180° different from 3 above)
5. Wind Speed \_\_\_\_\_ meters/sec (Calculation Sheet I,A.1)
6.  $\Delta T$ : \_\_\_\_\_ °F, Stability Class: \_\_\_\_\_ (calc. sheet I. sec. B)

### II. RELEASE INFORMATION

1. Exposure Time \_\_\_\_\_ hours (Data Summary Sheet Section II D, line 2).
2. Release rate Reactor Bldg. Stack: \_\_\_\_\_ Ci/sec or  $0.3 \times$  \_\_\_\_\_ Ci/sec.  
= \_\_\_\_\_ actual Ci/sec. (see Note A) (Calc. sheet II, sec. I)
3. Release rate - offgas stack \_\_\_\_\_ Ci/sec a or  $0.3 \times$  \_\_\_\_\_ Ci/sec. =  
\_\_\_\_\_ actual Ci/sec. (see Note A) (Calc. sheet II, sec. II)
4. Release rate - Turbine Bldg. Roof Exhaust: \_\_\_\_\_ Ci/sec  $0.3 \times$  \_\_\_\_\_  
Ci/sec = \_\_\_\_\_ actual Ci/sec. (see Note A) (calc. sheet II, sec. III)
5. Total Gaseous Release Rate: \_\_\_\_\_ Ci/sec (add release rates from previous three lines)

Note A: If the monitor readings were obtained from the intermediate or high range effluent monitor multiply by 0.3 to obtain actual release rates. This corrects for monitor response at 1 hour per P.A.S.A.P. 7.1.

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3a
INITIAL DOSE PROJECTIONS	Page 10 of 41
	Revision 2
	Date 3/11/83

ATTACHMENT II, SUMMARY TABLE (continued)

III. DOSE INFORMATION

1. Cal. sheet III, section number  
for remainder of  
calculations:  
(calc. sheet III, sec. I)

		<u>Distance from Source</u>			
	Site Bdya	Point of max. X/Q for Offgas Stack release <sup>b</sup>	2mi	5mi	10mi
2. Normalized concentration, X/Q, sec/m <sup>3</sup> , Ground level release (calc. sheet III, subsect. A) <sup>c</sup>	_____	_____	_____	_____	_____
3. Normalized concentration, X/Q, sec/m <sup>3</sup> , Elevated release (calc. sheet III, subsect. B) <sup>c</sup>	_____	_____	_____	_____	_____
4. Whole body dose rate, mrem/hr (calc. sheet III, subsect. B) <sup>c</sup>	_____	_____	_____	_____	_____
5. Whole body dose, mrem (calc. sheet III, subsect. C) <sup>c</sup>	_____	_____	_____	_____	_____
6. Thyroid dose commitment <sup>d</sup> , mrem (calc. sheet III, subsect. D) <sup>c</sup>	_____	_____	_____	_____	_____
7. Total plume width, meters(miles) (calc. sheet III, subsect. E) <sup>c</sup>	_____	_____	_____	_____	_____
8. Plume arrival time, hr (calc. sheet III, subsect. F) <sup>c</sup>	_____	_____	_____	_____	_____

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3a
INITIAL DOSE PROJECTIONS	Page 11 of 41 Revision 2 Date 3/11/83

ATTACHMENT II, SUMMARY TABLE (continued)

NOTES:

<sup>a</sup>Assumes wind direction in the ESE sector. For directions in other sectors doses will be lower and plume arrival time and width will be greater.

<sup>b</sup>For stability class FG the distance to the maximum X/Q is greater than 10 miles. In order to limit the dose information to the EPZ a distance of 10 miles is used for class FG.

<sup>c</sup>Calculation sheet subsection refers to the subsection of the Calculation Sheet III section as given in line 1 of Section III of this table.

<sup>d</sup>The thyroid dose commitment given is for an infant, i.e., the worst case. The adult dose commitment is obtained by multiplying by 0.58.

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3a
INITIAL DOSE PROJECTIONS	Page 12 of 41
	Revision 2
	Date 3/11/83

### ATTACHMENT III, CALCULATION SHEET I

#### GENERAL INFORMATION

##### A. Wind Speed

1. Wind Speed \_\_\_\_\_ mph (Data Summary Sheet, Section I, line 2)  $\times 0.447 =$   
\_\_\_\_\_ Meters/sec (to Summary Table sec. I, line 5)

##### B. Stability Class

1.  $\Delta T$  \_\_\_\_\_  $^{\circ}F$  - obtained from Data Summary Sheet, Section I, line 3 (to Summary Table sec. I, line 6)
2. Stability class is determined from the following table as a function of  $\Delta T$ .  
Stability class \_\_\_\_\_ (to Summary Table, sec I, line 6)

$\Delta T$  Range,  $^{\circ}F$

Stability Class

-1.26 or less

AB

-1.26 to -1.11

C

-1.11 to 1.11

DE

1.11 or greater

FG

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3a
INITIAL DOSE PROJECTIONS	Page 13 of 41 Revision 2 Date 3/11/83

# ATTACHMENT III, CALCULATION SHEET II

Page 1 of 3

## RELEASE INFORMATION

### I. Reactor Building Stack Releases

- "A" Stack Conc.<sup>a</sup> \_\_\_\_\_ uCi/cc x "A" Stack Flow<sup>a</sup>  
\_\_\_\_\_ cfm x 472 = \_\_\_\_\_ uCi/sec
- "B" Stack Conc.<sup>a</sup> \_\_\_\_\_ uCi/cc x "B" Stack Flow<sup>a</sup>  
\_\_\_\_\_ cfm x 472 = \_\_\_\_\_ uCi/sec
- "C" Stack Conc.<sup>a</sup> \_\_\_\_\_ uCi/cc x "C" Stack Flow<sup>a</sup>  
\_\_\_\_\_ cfm x 472 = \_\_\_\_\_ uCi/sec
- |                        |                 |
|------------------------|-----------------|
| "A" Stack Release Rate | _____ uCi/sec   |
| "B" Stack Release Rate | _____ uCi/sec   |
| "C" Stack Release Rate | _____ uCi/sec   |
| Total Release Rate     | _____ uCi/sec x |

$$\frac{1 \text{ Curie}}{10^6 \text{ uCi}} = \boxed{\phantom{000000}} \text{ Ci/sec}$$

(To Summary Table, Sec. II, Line 2)

Note:

- Obtain data from Data Summary Sheet, Section II.A, line 2.

### II. Offgas Stack Releases

- Stack Conc.<sup>a</sup> \_\_\_\_\_ uCi/cc x Offgas Stack  
Flow<sup>a</sup> \_\_\_\_\_ cfm x 472 = \_\_\_\_\_ uCi/sec
- Release rate \_\_\_\_\_ uCi/sec x  $\frac{1 \text{ Curie}}{10^6 \text{ uCi}} =$   
 $\boxed{\phantom{000000}} \text{ Ci/sec}$

(To Summary Table, Sec. II, Line 3)

Note:

- Obtain data from Data Summary Sheet, Section II.B.

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3a
INITIAL DOSE PROJECTIONS	Page 14 of 41
	Revision 2
	Date 3/11/83

ATTACHMENT III, CALCULATION SHEET II (continued)

Page 2 of 3

III. Turbine Building Releases

1. Release Conc.<sup>a</sup> \_\_\_\_\_ uCi/cc x Flow<sup>a</sup> \_\_\_\_\_ cfm x 472 =  
 \_\_\_\_\_ uCi/sec

2. Release rate \_\_\_\_\_ uCi/sec x  $\frac{1 \text{ Curie}}{10^6 \text{ uCi}} =$

Ci/sec

(To Summary Table Sec. II, Line 4)

Note:

- a. Obtain data from Data Summary Sheet, Section II.C.

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3a
INITIAL DOSE PROJECTIONS	Page 15 of 41
	Revision 2
	Date 3/11/83

# ATTACHMENT III, CALCULATION SHEET III

Page 3 of 3

## DOSE INFORMATION

- I. Section for the remaining calculations  - Appropriate section is determined from the following table based on the atmospheric stability class. Complete ONLY ONE section.

Stability Class  
(from Summary Table,  
Section I, line 6)

Section

AB

II (page 18 of 41)

C

III (page 22 of 41)

DE

IV (page 28 of 41)

FG

V (page 35 of 41)

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3a
INITIAL DOSE PROJECTIONS	Page 16 of 41
	Revision 2
	Date 3/11/83

ATTACHMENT III, CALCULATION SHEET III (continued)

II. Dose information for atmospheric stability class AB

A. Normalized concentration, Ground Level Release - Results for Summary Table, Section III, Line 2.

1.  $4.0 \times 10^{-5} \div$  \_\_\_\_\_ m/sec<sup>a</sup> =   $\frac{\text{sec}}{\text{m}^3}$  at site boundary
2.  $5.3 \times 10^{-5} \div$  \_\_\_\_\_ m/sec<sup>a</sup> =   $\frac{\text{sec}}{\text{m}^3}$  at point of max  
X/Q for offgas  
stack release
3.  $3.8 \times 10^{-7} \div$  \_\_\_\_\_ m/sec<sup>a</sup> =   $\frac{\text{sec}}{\text{m}^3}$  at 2 miles
4.  $4.0 \times 10^{-8} \div$  \_\_\_\_\_ m/sec<sup>a</sup> =   $\frac{\text{sec}}{\text{m}^3}$  at 5 miles
5.  $7.4 \times 10^{-9} \div$  \_\_\_\_\_ m/sec<sup>a</sup> =   $\frac{\text{sec}}{\text{m}^3}$  at 10 miles

NOTE:

<sup>a</sup>Obtain wind speed from Summary Table, Section I, line 5.

B. Normalized concentration, Elevated Release - Results for Summary Table Section III, line 3.

1.  $2.2 \times 10^{-5} \div$  \_\_\_\_\_ m/sec<sup>a</sup> =   $\frac{\text{sec}}{\text{m}^3}$  at site boundary
2.  $2.4 \times 10^{-5} \div$  \_\_\_\_\_ m/sec<sup>a</sup> =   $\frac{\text{sec}}{\text{m}^3}$  at point of max  
X/Q for offgas  
stack release
3.  $3.5 \times 10^{-7} \div$  \_\_\_\_\_ m/sec<sup>a</sup> =   $\frac{\text{sec}}{\text{m}^3}$  at 2 miles
4.  $3.9 \times 10^{-8} \div$  \_\_\_\_\_ m/sec<sup>a</sup> =   $\frac{\text{sec}}{\text{m}^3}$  at 5 miles
5.  $7.6 \times 10^{-9} \div$  \_\_\_\_\_ m/sec<sup>a</sup> =   $\frac{\text{sec}}{\text{m}^3}$  at 10 miles

NOTE:

<sup>a</sup>Obtain wind speed from Summary Table Section I, line 5.

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3a
INITIAL DOSE PROJECTIONS	Page 17 of 41
	Revision 2
	Date 3/11/83

ATTACHMENT III, CALCULATION SHEET III (continued)

C. Whole body dose rate - Results from Summary Table Section III, line 4.

$$1. \quad \frac{Ci^a}{sec} + \frac{Ci^b}{sec} = \frac{Ci}{sec}$$

$$2. \quad \left[ \frac{Ci}{sec} \text{ (from line 1)} \times 32.0 \right. \\ \left. \text{divided by } \frac{mC}{sec} \right] + \left[ \frac{Ci^d}{sec} \times 11.0^e \right]$$

$$\text{divided by } \frac{mC}{sec} = \boxed{\phantom{000}} \frac{mrem}{hr} \text{ at site boundary}$$

$$3. \quad \left[ \frac{Ci}{sec} \text{ (from line 1)} \times 42.4 \right.$$

$$\text{divided by } \frac{mC}{sec} \left. + \left[ \frac{Ci^d}{sec} \times 12.0^e \right] \right.$$

$$\text{divided by } \frac{mC}{sec} = \boxed{\phantom{000}} \frac{mrem}{hr} \text{ at point of max X/Q for offgas stack release}$$

$$4. \quad \left[ \frac{Ci}{sec} \text{ (from line 1)} \times 0.304 \right.$$

$$\text{divided by } \frac{mC}{sec} \left. + \left[ \frac{Ci^d}{sec} \times 0.280^e \right] \right.$$

$$\text{divided by } \frac{mC}{sec} = \boxed{\phantom{000}} \frac{mrem}{hr} \text{ at 2 miles}$$

$$5. \quad \left[ \frac{Ci}{sec} \text{ (from line 1)} \times 3.20 \times 10^{-2} \right.$$

$$\text{divided by } \frac{mC}{sec} \left. + \left[ \frac{Ci^d}{sec} \times 3.8 \times 10^{-2}^e \right] \right.$$

$$\text{divided by } \frac{mC}{sec} = \boxed{\phantom{000}} \frac{mrem}{hr} \text{ at 5 miles}$$

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3a
INITIAL DOSE PROJECTIONS	Page 18 of 41
	Revision 2
	Date 3/11/83

ATTACHMENT III, CALCULATION SHEET III (continued)

6. 
$$\left[ \frac{\text{Ci}}{\text{sec}} \text{ (from line 1)} \times 5.92 \times 10^{-3} \right]$$
  
divided by  $\frac{\text{m}^{\text{C}}}{\text{sec}}$  +  $\left[ \frac{\text{Ci}^{\text{d}}}{\text{sec}} \times 1.7 \times 10^{-2\text{e}} \right]$   
divided by  $\frac{\text{m}^{\text{C}}}{\text{sec}}$  =  $\boxed{\phantom{000000}} \frac{\text{mrem}}{\text{hr}}$  at 10 miles

NOTES:

<sup>a</sup>Reactor building stack release rate from Summary Table, Section II, line 2.

<sup>b</sup>Turbine building roof exhaust release rate from Summary Table, Section II, line 4.

<sup>c</sup>Wind speed from Summary Table, Section I, line 5.

<sup>d</sup>Offgas stack release rate from Summary Table, Section II, line 3.

<sup>e</sup>If Standby Gas Treatment is in operation (see Data Summary Sheet, Section II D, line 1) multiply this number by 0.662.

D. Whole body dose - Results for Summary Table Section III, line 5.

1.  $\frac{\text{mrem}}{\text{hr}}$  (from line C2) x  $\text{hr}^{\text{a}}$   
=  $\boxed{\phantom{000000}}$  mrem at site boundary

2.  $\frac{\text{mrem}}{\text{hr}}$  (from line C3) x  $\text{hr}^{\text{a}}$   
=  $\boxed{\phantom{000000}}$  mrem at point of max X/Q for offgas stack release

3.  $\frac{\text{mrem}}{\text{hr}}$  (from line C4) x  $\text{hr}^{\text{a}}$   
=  $\boxed{\phantom{000000}}$  mrem at 2 miles

4.  $\frac{\text{mrem}}{\text{hr}}$  (from line C5) x  $\text{hr}^{\text{a}}$   
=  $\boxed{\phantom{000000}}$  mrem at 5 miles

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3a
INITIAL DOSE PROJECTIONS	Page 19 of 41
	Revision 2
	Date 3/11/83

ATTACHMENT III, CALCULATION SHEET III (continued)

5.  $\frac{\text{mrem}}{\text{hr}}$  (from line C6) x  $\text{hra}$   
 =  mrem at 10 miles

NOTE:

<sup>a</sup>Obtain exposure time from Summary Table, Section II, line 1.

E. Thyroid Dose Commitment - Result for Summary Table, Section III, line 6.

1.  $\left( \frac{\text{Ci}}{\text{sec}} + \frac{\text{Cib}}{\text{sec}} \right) \times 0.3 = \frac{\text{Ci}}{\text{sec}}$

2.  $\frac{\text{Ci}}{\text{sec}} \times 0.3^d = \frac{\text{Ci}}{\text{sec}}$

3.  $\frac{\text{Ci}}{\text{sec}}$  (line 1) x  $\frac{\text{sec}}{\text{m}^3}$  (line A.1)  
 +  $\frac{\text{Ci}}{\text{sec}}$  (line 2) x  $\frac{\text{sec}}{\text{m}^3}$  (line B.1)  
 =  $\frac{\text{Ci}}{\text{m}^3}$

4.  $\frac{\text{Ci}}{\text{sec}}$  (line 1) x  $\frac{\text{sec}}{\text{m}^3}$  (line A.2)  
 +  $\frac{\text{Ci}}{\text{sec}}$  (line 2) x  $\frac{\text{sec}}{\text{m}^3}$  (line B.2)  
 =  $\frac{\text{Ci}}{\text{m}^3}$

5.  $\frac{\text{Ci}}{\text{sec}}$  (line 1) x  $\frac{\text{sec}}{\text{m}^3}$  (line A.3)  
 +  $\frac{\text{Ci}}{\text{sec}}$  (line 2) x  $\frac{\text{sec}}{\text{m}^3}$  (line B.3)  
 =  $\frac{\text{Ci}}{\text{m}^3}$

6.  $\frac{\text{Ci}}{\text{sec}}$  (line 1) x  $\frac{\text{sec}}{\text{m}^3}$  (line A.4)  
 +  $\frac{\text{Ci}}{\text{sec}}$  (line 2) x  $\frac{\text{sec}}{\text{m}^3}$  (line B.4)  
 =  $\frac{\text{Ci}}{\text{m}^3}$

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3a
INITIAL DOSE PROJECTIONS	Page 20 of 41
	Revision 2
	Date 3/11/83

ATTACHMENT III, CALCULATION SHEET III (continued)

7.  $\frac{Ci}{sec}$  (line 1) x  $\frac{sec}{m^3}$  (line A.5)  
+  $\frac{Ci}{sec}$  (line 2) x  $\frac{sec}{m^3}$  (line B.5)  
=  $\frac{Ci}{m^3}$
8.  $\frac{Ci}{m^3}$  (line 3) x  $hre$  x  $3.8 \times 10^8$   
=  mrem at site boundary
9.  $\frac{Ci}{m^3}$  (line 4) x  $hre$  x  $3.8 \times 10^8$   
=  mrem at point of max X/Q for offgas stack release.
10.  $\frac{Ci}{m^3}$  (line 5) x  $hre$  x  $3.8 \times 10^8$   
=  mrem at 2 miles
11.  $\frac{Ci}{m^3}$  (line 6) x  $hre$  x  $3.8 \times 10^8$   
=  mrem at 5 miles
12.  $\frac{Ci}{m^3}$  (line 7) x  $hre$  x  $3.8 \times 10^8$   
=  mrem at 10 miles

NOTES:

<sup>a</sup>Reactor building stack release rate from Summary Table, Section II, line 2.

<sup>b</sup>Turbine building roof exhaust release rate from Summary Table, Section II, line 4.

<sup>c</sup>Offgas stack release rate from Summary Table, Section II, line 3.

<sup>d</sup>If Standby Gas Treatment is in operation (See Data Summary Sheet, Section II.D, line 1) use 0.003, otherwise use 0.3.

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3a
INITIAL DOSE PROJECTIONS	Page 21 of 41
	Revision 2
	Date 3/11/83

# ATTACHMENT III, CALCULATION SHEET III (continued)

<sup>e</sup>Obtain exposure time from Summary Table, Section II, line 1.

F. Plume width - The following are the plume widths to be placed in the Summary Table, Section III, line 7.

Site Bdy <sup>a</sup>	Point of maximum X/Q for Offgas Stack release	2mi	5mi	10mi
530	470	3200	6200	11000

G. Plume arrival time - Results for Summary Table Section III, line 8.

1. 0.125 divided by \_\_\_\_\_  $\frac{m^a}{sec} = \boxed{\phantom{000}}$  hr to Site Boundary

2. 0.111 divided by \_\_\_\_\_  $\frac{m^a}{sec} = \boxed{\phantom{000}}$  hr to point of max X/Q for offgas stack release

3. 0.894 divided by \_\_\_\_\_  $\frac{m^a}{sec} = \boxed{\phantom{000}}$  hr to 2 miles

4. 2.23 divided by \_\_\_\_\_  $\frac{m^a}{sec} = \boxed{\phantom{000}}$  hr to 5 miles

5. 4.47 divided by \_\_\_\_\_  $\frac{m^a}{sec} = \boxed{\phantom{000}}$  hr to 10 miles

## NOTE:

<sup>a</sup>Obtain wind speed from Summary Table, Section I, line 5.

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3a
INITIAL DOSE PROJECTIONS	Page 22 of 41
	Revision 2
	Date 3/11/83

ATTACHMENT III, CALCULATION SHEET III (continued)

III. Dose information for atmospheric stability class C.

A. Normalized concentration, Ground level release - Results for Summary Table, Section III, line 2.

1.  $1.8 \times 10^{-4} \div$  \_\_\_\_\_ m/sec<sup>a</sup> =   $\frac{\text{sec}}{\text{m}^3}$  at site boundary
2.  $3.2 \times 10^{-5} \div$  \_\_\_\_\_ m/sec<sup>a</sup> =   $\frac{\text{sec}}{\text{m}^3}$  at point of max X/Q for offgas release
3.  $6.0 \times 10^{-6} \div$  \_\_\_\_\_ m/sec<sup>a</sup> =   $\frac{\text{sec}}{\text{m}^3}$  at 2 miles
4.  $1.2 \times 10^{-6} \div$  \_\_\_\_\_ m/sec<sup>a</sup> =   $\frac{\text{sec}}{\text{m}^3}$  at 5 miles
5.  $3.7 \times 10^{-7} \div$  \_\_\_\_\_ m/sec<sup>a</sup> =   $\frac{\text{sec}}{\text{m}^3}$  at 10 miles

NOTE:

<sup>a</sup>Obtain wind speed from Summary Table Section I, line 5.

B. Normalized concentration, Elevated release - Results for Summary Table, Section III, line 3.

1.  $1.0 \times 10^{-6} \div$  \_\_\_\_\_ m/sec<sup>a</sup> =   $\frac{\text{sec}}{\text{m}^3}$  at site boundary
2.  $3.3 \times 10^{-5} \div$  \_\_\_\_\_ m/sec<sup>a</sup> =   $\frac{\text{sec}}{\text{m}^3}$  at point of max X/Q for offgas stack release
3.  $5.1 \times 10^{-6} \div$  \_\_\_\_\_ m/sec<sup>a</sup> =   $\frac{\text{sec}}{\text{m}^3}$  at 2 miles
4.  $1.2 \times 10^{-6} \div$  \_\_\_\_\_ m/sec<sup>a</sup> =   $\frac{\text{sec}}{\text{m}^3}$  at 5 miles
5.  $3.7 \times 10^{-7} \div$  \_\_\_\_\_ m/sec<sup>a</sup> =   $\frac{\text{sec}}{\text{m}^3}$  at 10 miles

NOTE:

<sup>a</sup>Obtain wind speed from Summary Table, Section I, line 5.

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3a
INITIAL DOSE PROJECTIONS	Page 23 of 41
	Revision 2
	Date 3/11/83

ATTACHMENT III, CALCULATION SHEET III (continued)

C. Whole body dose rate - Results from Summary Table, Section III, line 4.

1.  $\frac{Ci^a}{sec} + \frac{Ci^b}{sec} = \frac{Ci}{sec}$

2.  $\frac{Ci}{sec}$  (from line 1) x 144

divided by  $\frac{mC}{sec} + \frac{Ci^d}{sec} \times 9.30e$

divided by  $\frac{mC}{sec} = \boxed{\phantom{000000}} \frac{mrem}{hr}$  at site boundary

3.  $\frac{Ci}{sec}$  (from line 1) x 25.6

divided by  $\frac{mC}{sec} + \frac{Ci^d}{sec} \times 10.5e$

divided by  $\frac{mC}{sec} = \boxed{\phantom{000000}} \frac{mrem}{hr}$  at point of max X/Q for offgas stack release

4.  $\frac{Ci}{sec}$  (from line 1) x 4.80

divided by  $\frac{mC}{sec} + \frac{Ci^d}{sec} \times 6.50e$

divided by  $\frac{mC}{sec} = \boxed{\phantom{000000}} \frac{mrem}{hr}$  at 2 miles

5.  $\frac{Ci}{sec}$  (from line 1) x 0.960

divided by  $\frac{mC}{sec} + \frac{Ci^d}{sec} \times 1.45e$

divided by  $\frac{mC}{sec} = \boxed{\phantom{000000}} \frac{mrem}{hr}$  at 5 miles

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3a
INITIAL DOSE PROJECTIONS	Page 24 of 41
	Revision 2
	Date 3/11/83

ATTACHMENT III, CALCULATION SHEET III (continued)

6.  $\frac{C_i}{\text{sec}}$  (from line 1)  $\times 0.296$

divided by  $\frac{m^C}{\text{sec}} + \frac{C_i^d}{\text{sec}} \times 0.350^e$

divided by  $\frac{m^C}{\text{sec}} = \boxed{\phantom{0000}} \frac{\text{mrem}}{\text{hr}}$  at 10 miles

NOTES:

- <sup>a</sup>Reactor building stack release rate from Summary Table, Section II, line 2.
- <sup>b</sup>Turbine building roof exhaust release rate from Summary Table, Section II, line 4.
- <sup>c</sup>Wind speed from Summary Table, Section I, line 5.
- <sup>d</sup>Offgas stack release rate from Summary Table, Section II, line 3.
- <sup>e</sup>If Standby Gas Treatment is in operation (see Data Summary Sheet, Section II D, line 1) multiply this number by 0.662.

D. Whole body dose - Results for Summary Table, Section III, line 5.

1.  $\frac{\text{mrem}}{\text{hr}}$  (from line C2)  $\times$   $\text{hr}^a$
- =  $\boxed{\phantom{0000}}$  mrem at site boundary
2.  $\frac{\text{mrem}}{\text{hr}}$  (from line C3)  $\times$   $\text{hr}^a$
- =  $\boxed{\phantom{0000}}$  mrem at point of max X/Q for offgas stack release
3.  $\frac{\text{mrem}}{\text{hr}}$  (from line C4)  $\times$   $\text{hr}^a$
- =  $\boxed{\phantom{0000}}$  mrem at 2 miles
4.  $\frac{\text{mrem}}{\text{hr}}$  (from line C5)  $\times$   $\text{hr}^a$
- =  $\boxed{\phantom{0000}}$  mrem at 5 miles

## ATTACHMENT III, CALCULATION SHEET III (continued)

$$5. \quad \frac{\text{mrem}}{\text{hr}} \text{ (from line C6)} \times \text{hra} = \boxed{\phantom{000000}} \text{ mrem at 10 miles}$$

NOTE:

<sup>a</sup>Obtain exposure time from Summary Table, Section II, line 1.E. Thyroid Dose Commitment - Result for Summary Table, Section III, line 6.

$$1. \quad \left( \frac{C_{ia}}{\text{sec}} + \frac{C_{ib}}{\text{sec}} \right) \times 0.3 = \frac{C_i}{\text{sec}}$$

$$2. \quad \frac{C_{ic}}{\text{sec}} \times 0.3^d = \frac{C_i}{\text{sec}}$$

$$3. \quad \frac{C_i}{\text{sec}} \text{ (line 1)} \times \frac{\text{sec}}{\text{m}^3} \text{ (line A.1)}$$

$$+ \frac{C_i}{\text{sec}} \text{ (line 2)} \times \frac{\text{sec}}{\text{m}^3} \text{ (line B.1)}$$

$$= \frac{C_i}{\text{m}^3}$$

$$4. \quad \frac{C_i}{\text{sec}} \text{ (line 1)} \times \frac{\text{sec}}{\text{m}^3} \text{ (line A.2)}$$

$$+ \frac{C_i}{\text{sec}} \text{ (line 2)} \times \frac{\text{sec}}{\text{m}^3} \text{ (line B.2)}$$

$$= \frac{C_i}{\text{m}^3}$$

$$5. \quad \frac{C_i}{\text{sec}} \text{ (line 1)} \times \frac{\text{sec}}{\text{m}^3} \text{ (line A.3)}$$

$$+ \frac{C_i}{\text{sec}} \text{ (line 2)} \times \frac{\text{sec}}{\text{m}^3} \text{ (line B.3)}$$

$$= \frac{C_i}{\text{m}^3}$$

## ATTACHMENT III, CALCULATION SHEET III (continued)

$$6. \quad \frac{Ci}{sec} \text{ (line 1)} \times \frac{sec}{m^3} \text{ (line A.4)}$$

$$+ \frac{Ci}{sec} \text{ (line 2)} \times \frac{sec}{m^3} \text{ (line B.4)}$$

$$= \frac{Ci}{m^3}$$

$$7. \quad \frac{Ci}{sec} \text{ (line 1)} \times \frac{sec}{m^3} \text{ (line A.5)}$$

$$+ \frac{Ci}{sec} \text{ (line 2)} \times \frac{sec}{m^3} \text{ (line B.5)}$$

$$= \frac{Ci}{m^3}$$

$$8. \quad \frac{Ci}{m^3} \text{ (line 3)} \times \text{ } \text{ hr}^e \times 3.8 \times 10^8$$

$$= \boxed{\phantom{000}} \text{ mrem at site boundary}$$

$$9. \quad \frac{Ci}{m^3} \text{ (line 4)} \times \text{ } \text{ hr}^e \times 3.8 \times 10^8$$

$$= \boxed{\phantom{000}} \text{ mrem at point of max. X/Q for offgas stack release}$$

$$10. \quad \frac{Ci}{m^3} \text{ (line 5)} \times \text{ } \text{ hr}^e \times 3.8 \times 10^8$$

$$= \boxed{\phantom{000}} \text{ mrem at 2 miles}$$

$$11. \quad \frac{Ci}{m^3} \text{ (line 6)} \times \text{ } \text{ hr}^e \times 3.8 \times 10^8$$

$$= \boxed{\phantom{000}} \text{ mrem at 5 miles}$$

$$12. \quad \frac{Ci}{m^3} \text{ (line 7)} \times \text{ } \text{ hr}^e \times 3.8 \times 10^8$$

$$= \boxed{\phantom{000}} \text{ mrem at 10 miles}$$

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EFIP 3.3a
INITIAL DOSE PROJECTIONS	Page 27 of 41
	Revision 2
	Date 3/11/83

# ATTACHMENT III, CALCULATION SHEET III (continued)

## NOTES:

<sup>a</sup>Reactor building stack release rate from Summary Table, Section II, line 2.

<sup>b</sup>Turbine building roof exhaust release rate from Summary Table, Section II, line 4.

<sup>c</sup>Offgas stack release rate from Summary Table, Section II, line 3.

<sup>d</sup>If Standby Gas Treatment is in operation (See Data Summary Sheet, Section II.D, line 1) use 0.003, otherwise use 0.3.

<sup>e</sup>Obtain release duration from Summary Table, Section II, line 1.

F. Plume width - The following are the plume widths to be placed in the Summary Table, Section III, line 7.

Site Bdy	Point of maximum X/Q for Offgas Stack release	2mi	5mi	10mi
310 meters	720	1900	2700	6600

G. Plume arrival time - Results for Summary Table, Section III, line 8.

- 0.125 divided by  $\frac{m^a}{sec}$  =  hr to Site Boundary
- 0.333 divided by  $\frac{m^a}{sec}$  =  hr to point of max X/Q for offgas stack release
- 0.894 divided by  $\frac{m^a}{sec}$  =  hr to 2 miles
- 2.23 divided by  $\frac{m^a}{sec}$  =  hr to 5 miles
- 4.47 divided by  $\frac{m^a}{sec}$  =  hr to 10 miles

## NOTE:

<sup>a</sup>Obtain wind speed from Summary Table, Section I, line 5.

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3a
INITIAL DOSE PROJECTIONS	Page 28 of 41
	Revision 2
	Date 3/11/83

ATTACHMENT III, CALCULATION SHEET III (continued)

IV. Dose information for atmospheric stability class DE.

A. Normalized concentration, Ground level release - Results for Summary Table, Section III, line 2.

1.  $7.3 \times 10^{-4}$  divided by \_\_\_\_\_ m/sec<sup>a</sup> =  $\frac{\boxed{\phantom{00}}}{\boxed{\phantom{00}}} \frac{\text{sec}}{\text{m}^3}$  at site boundary
2.  $2.2 \times 10^{-5}$  divided by \_\_\_\_\_ m/sec<sup>a</sup> =  $\frac{\boxed{\phantom{00}}}{\boxed{\phantom{00}}} \frac{\text{sec}}{\text{m}^3}$  at point of max X/Q for offgas stack release
3.  $3.1 \times 10^{-5}$  divided by \_\_\_\_\_ m/sec<sup>a</sup> =  $\frac{\boxed{\phantom{00}}}{\boxed{\phantom{00}}} \frac{\text{sec}}{\text{m}^3}$  at 2 miles
4.  $7.2 \times 10^{-6}$  divided by \_\_\_\_\_ m/sec<sup>a</sup> =  $\frac{\boxed{\phantom{00}}}{\boxed{\phantom{00}}} \frac{\text{sec}}{\text{m}^3}$  at 5 miles
5.  $2.4 \times 10^{-6}$  divided by \_\_\_\_\_ m/sec<sup>a</sup> =  $\frac{\boxed{\phantom{00}}}{\boxed{\phantom{00}}} \frac{\text{sec}}{\text{m}^3}$  at 10 miles

NOTE:

<sup>a</sup>Obtain wind speed from Summary Table, Section I, line 5.

B. Normalized concentration, Elevated release - Results for Summary Table, Section III, line 3.

1.  $1.6 \times 10^{-11}$  divided by \_\_\_\_\_ m/sec<sup>a</sup> =  $\frac{\boxed{\phantom{00}}}{\boxed{\phantom{00}}} \frac{\text{sec}}{\text{m}^3}$  at site boundary
2.  $7.0 \times 10^{-6}$  divided by \_\_\_\_\_ m/sec<sup>a</sup> =  $\frac{\boxed{\phantom{00}}}{\boxed{\phantom{00}}} \frac{\text{sec}}{\text{m}^3}$  at point of max X/Q for offgas stack release
3.  $6.6 \times 10^{-6}$  divided by \_\_\_\_\_ m/sec<sup>a</sup> =  $\frac{\boxed{\phantom{00}}}{\boxed{\phantom{00}}} \frac{\text{sec}}{\text{m}^3}$  at 2 miles
4.  $4.7 \times 10^{-6}$  divided by \_\_\_\_\_ m/sec<sup>a</sup> =  $\frac{\boxed{\phantom{00}}}{\boxed{\phantom{00}}} \frac{\text{sec}}{\text{m}^3}$  at 5 miles
5.  $2.0 \times 10^{-6}$  divided by \_\_\_\_\_ m/sec<sup>a</sup> =  $\frac{\boxed{\phantom{00}}}{\boxed{\phantom{00}}} \frac{\text{sec}}{\text{m}^3}$  at 10 miles

NOTE:

<sup>a</sup>Obtain wind speed from Summary Table, Section I, line 5.

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3a
INITIAL DOSE PROJECTIONS	Page 29 of 41
	Revision 2
	Date 3/11/83

ATTACHMENT III, CALCULATION SHEET III (continued)

C. Whole body dose rate - Results from Summary Table, Section III, line 4.

1.  $\frac{Ci^a}{sec} + \frac{Ci^b}{sec} = \frac{Ci}{sec}$

2.  $\frac{Ci}{sec}$  (from line 1) x 584  
divided by  $\frac{m^C}{sec} + \frac{Ci^d}{sec} \times 8.00e$   
divided by  $\frac{m^C}{sec} = \boxed{\phantom{000000}} \frac{mrem}{hr}$  at site boundary

3.  $\frac{Ci}{sec}$  (from line 1) x 17.6  
divided by  $\frac{m^C}{sec} + \frac{Ci^d}{sec} \times 8.00e$   
divided by  $\frac{m^C}{sec} = \boxed{\phantom{000000}} \frac{mrem}{hr}$  at point of max X/Q for offgas stack release

4.  $\frac{Ci}{sec}$  (from line 1) x 24.8  
divided by  $\frac{m^C}{sec} + \frac{Ci^d}{sec} \times 9.00e$   
divided by  $\frac{m^C}{sec} = \boxed{\phantom{000000}} \frac{mrem}{hr}$  at 2 miles

5.  $\frac{Ci}{sec}$  (from line 1) x 5.76  
divided by  $\frac{m^C}{sec} + \frac{Ci^d}{sec} \times 5.10e$   
divided by  $\frac{m^C}{sec} = \boxed{\phantom{000000}} \frac{mrem}{hr}$  at 5 miles

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3a
INITIAL DOSE PROJECTIONS	Page 30 of 41
	Revision 2
	Date 3/11/83

ATTACHMENT III, CALCULATION SHEET III (continued)

6.  $\frac{Ci}{sec}$  (from line 1)  $\times 1.92$   
divided by  $\frac{m^C}{sec} + \frac{Ci^d}{sec} \times 2.05^e$   
divided by  $\frac{m^C}{sec} = \boxed{\phantom{000000}} \frac{mrem}{hr}$  at 10 miles

NOTES:

<sup>a</sup>Reactor building stack release rate from Summary Table, Section II, line 2.

<sup>b</sup>Turbine building roof exhaust release rate from Summary Table, Section II, line 4.

<sup>c</sup>Wind speed from Summary Table, Section I, line 5.

<sup>d</sup>Offgas stack release rate from Summary Table, Section II, line 3.

<sup>e</sup>If Standby Gas Treatment is in operation (see Data Summary Sheet, Section II D, line 1) multiply this number by 0.662.

D. Whole body dose - Results for Summary Table, Section III, line 5.

1.  $\frac{mrem}{hr}$  (from line C2)  $\times$   $\phantom{000000}$  hr<sup>a</sup>  
=  $\boxed{\phantom{000000}}$  mrem at site boundary
2.  $\frac{mrem}{hr}$  (from line C3)  $\times$   $\phantom{000000}$  hr<sup>a</sup>  
=  $\boxed{\phantom{000000}}$  mrem at point of max X/Q for offgas stack release
3.  $\frac{mrem}{hr}$  (from line C4)  $\times$   $\phantom{000000}$  hr<sup>a</sup>  
=  $\boxed{\phantom{000000}}$  mrem at 2 miles
4.  $\frac{mrem}{hr}$  (from line C5)  $\times$   $\phantom{000000}$  hr<sup>a</sup>  
=  $\boxed{\phantom{000000}}$  mrem at 5 miles

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3a
INITIAL DOSE PROJECTIONS	Page 31 of 41
	Revision 2
	Date 3/11/83

ATTACHMENT III, CALCULATION SHEET III (continued)

5.  $\frac{\text{mrem}}{\text{hr}}$  (from line C6) x  $\text{hra}$   
 =  mrem at 10 miles

NOTE:

<sup>a</sup>Obtain exposure time from Summary Table, Section II, line 1.

E. Thyroid Dose Commitment - Result for Summary Table, Section III, line 6.

1.  $\left( \frac{Ci^a}{\text{sec}} + \frac{Ci^b}{\text{sec}} \right) \times 0.3 = \frac{Ci}{\text{sec}}$

2.  $\frac{Ci^c}{\text{sec}} \times 0.3d = \frac{Ci}{\text{sec}}$

3.  $\frac{Ci}{\text{sec}}$  (line 1) x  $\frac{\text{sec}}{m^3}$  (line A.1)

+  $\frac{Ci}{\text{sec}}$  (line 2) x  $\frac{\text{sec}}{m^3}$  (line B.1)

=  $\frac{Ci}{m^3}$

4.  $\frac{Ci}{\text{sec}}$  (line 1) x  $\frac{\text{sec}}{m^3}$  (line A.2)

+  $\frac{Ci}{\text{sec}}$  (line 2) x  $\frac{\text{sec}}{m^3}$  (line B.2)

=  $\frac{Ci}{m^3}$

5.  $\frac{Ci}{\text{sec}}$  (line 1) x  $\frac{\text{sec}}{m^3}$  (line A.3)

+  $\frac{Ci}{\text{sec}}$  (line 2) x  $\frac{\text{sec}}{m^3}$  (line B.3)

=  $\frac{Ci}{m^3}$

## ATTACHMENT III, CALCULATION SHEET III (continued)

$$6. \quad \frac{Ci}{sec} \text{ (line 1)} \times \frac{sec}{m^3} \text{ (line A.4)}$$

$$+ \frac{Ci}{sec} \text{ (line 2)} \times \frac{sec}{m^3} \text{ (line B.4)}$$

$$= \frac{Ci}{m^3}$$

$$7. \quad \frac{Ci}{sec} \text{ (line 1)} \times \frac{sec}{m^3} \text{ (line A.5)}$$

$$+ \frac{Ci}{sec} \text{ (line 2)} \times \frac{sec}{m^3} \text{ (line B.5)}$$

$$= \frac{Ci}{m^3}$$

$$8. \quad \frac{Ci}{m^3} \text{ (line 3)} \times \text{hre} \times 3.8 \times 10^8$$

$$= \boxed{\phantom{000000}} \text{ mrem at site boundary}$$

$$9. \quad \frac{Ci}{m^3} \text{ (line 4)} \times \text{hre} \times 3.8 \times 10^8$$

$$= \boxed{\phantom{000000}} \text{ mrem at point of max X/Q for offgas stack release}$$

$$10. \quad \frac{Ci}{m^3} \text{ (line 5)} \times \text{hre} \times 3.8 \times 10^8$$

$$= \boxed{\phantom{000000}} \text{ mrem at . miles}$$

$$11. \quad \frac{Ci}{m^3} \text{ (line 6)} \times \text{hre} \times 3.8 \times 10^8$$

$$= \boxed{\phantom{000000}} \text{ mrem at 5 miles}$$

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3a
INITIAL DOSE PROJECTIONS	Page 33 of 41
	Revision 2
	Date 3/11/83

ATTACHMENT III, CALCULATION SHEET III (continued)

12.  $\frac{Ci}{m^3}$  (line 7) x  $hr^e \times 3.8 \times 10^8$

=  mrem at 10 miles

NOTES:

<sup>a</sup>Reactor building stack release rate from Summary Table, Section II, line 2.

<sup>b</sup>Turbine building roof exhaust release rate from Summary Table, Section II, line 4.

<sup>c</sup>Offgas stack release rate from Summary Table, Section II, line 3.

<sup>d</sup>If Standby Gas Treatment is in operation (See Data Summary Sheet, Section II.D, line 1) use 0.003, otherwise use 0.3

<sup>e</sup>Obtain release duration from Summary Table, Section II, line 1.

F. Plume width - The following are the plume widths to be placed in the Summary Table, Section III, line 7.

Site Bdy	Point of maximum X/Q for Offgas Stack release	2mi	5mi	10mi
190 meters	1400	1100	2400	4300

G. Plume arrival time - Results for Summary Table, Section III, line 8.

1. 0.125 divided by  $\frac{ma}{sec}$  =  hr to Site Boundary

2. 1.11 divided by  $\frac{ma}{sec}$  =  hr to point of max X/Q for offgas stack release

3. 0.894 divided by  $\frac{ma}{sec}$  =  hr to 2 miles

4. 2.23 divided by  $\frac{ma}{sec}$  =  hr to 5 miles

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3a
INITIAL DOSE PROJECTIONS	Page 34 of 41
	Revision 2
	Date 3/11/83

ATTACHMENT III, CALCULATION SHEET III (continued)

5. 4.47 divided by  $\frac{\text{m}^a}{\text{sec}}$  =  hr to 10 miles

NOTES:

<sup>a</sup>Obtain wind speed from Summary Table, Section I, line 5.

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3a
INITIAL DOSE PROJECTIONS	Page 35 of 41
	Revision 2
	Date 3/11/83

ATTACHMENT III, CALCULATION SHEET III (continued)

V. Dose information for atmospheric stability class FG.

A. Normalized concentration, Ground level release - Results for Summary Table, Section III, line 2

1.  $4.0 \times 10^{-3} \div$  \_\_\_\_\_ m/sec<sup>a</sup> =    $\frac{\text{sec}}{\text{m}^3}$  at site boundary
2.  $2.0 \times 10^{-5} \div$  \_\_\_\_\_ m/sec<sup>a</sup> =    $\frac{\text{sec}}{\text{m}^3}$  at point of max X/Q  
for offgas stack release
3.  $2.1 \times 10^{-4} \div$  \_\_\_\_\_ m/sec<sup>a</sup> =    $\frac{\text{sec}}{\text{m}^3}$  at 2 miles
4.  $5.5 \times 10^{-5} \div$  \_\_\_\_\_ m/sec<sup>a</sup> =    $\frac{\text{sec}}{\text{m}^3}$  at 5 miles
5.  $2.0 \times 10^{-5} \div$  \_\_\_\_\_ m/sec<sup>a</sup> =    $\frac{\text{sec}}{\text{m}^3}$  at 10 miles

NOTE:

<sup>a</sup>Obtain wind speed from Summary Table, Section I, line 5.

B. Normalized concentration, Elevated release - Results for Summary Table Section III, line 3.

1.  $0.0 \div$  \_\_\_\_\_ m/sec<sup>a</sup> =    $\frac{\text{sec}}{\text{m}^3}$  at site boundary
2.  $1.7 \times 10^{-4} \div$  \_\_\_\_\_ m/sec<sup>a</sup> =    $\frac{\text{sec}}{\text{m}^3}$  at point of max X/Q  
for offgas stack release
3.  $1.7 \times 10^{-11} \div$  \_\_\_\_\_ m/sec<sup>a</sup> =    $\frac{\text{sec}}{\text{m}^3}$  at 2 miles

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3a
INITIAL DOSE PROJECTIONS	Page 36 of 41
	Revision 2
	Date 3/11/83

ATTACHMENT III, CALCULATION SHEET III (continued)

$$4. \quad 2.2 \times 10^{-7} + \underline{\hspace{2cm}} \text{ m/sec}^a = \boxed{\hspace{2cm}} \frac{\text{sec}}{\text{m}^3} \text{ at 5 miles}$$

$$5. \quad 1.7 \times 10^{-7} + \underline{\hspace{2cm}} \text{ m/sec}^a = \boxed{\hspace{2cm}} \frac{\text{sec}}{\text{m}^3} \text{ at 10 miles}$$

NOTE:

<sup>a</sup>Obtain wind speed from Summary Table, Section I, line 5.

C. Whole body dose rate - Results from Summary Table, Section III, line 4.

$$1. \quad \underline{\hspace{2cm}} \frac{\text{Ci}^a}{\text{sec}} + \underline{\hspace{2cm}} \frac{\text{Ci}^b}{\text{sec}} = \underline{\hspace{2cm}} \frac{\text{Ci}}{\text{sec}}$$

$$2. \quad \underline{\hspace{2cm}} \frac{\text{Ci}}{\text{sec}} \text{ (from line 1)} \times 3.20 \times 10^3$$

$$\text{divided by } \underline{\hspace{2cm}} \frac{\text{m}^c}{\text{sec}} + \underline{\hspace{2cm}} \frac{\text{Ci}^d}{\text{sec}} \times 7.00^e$$

$$\text{divided by } \underline{\hspace{2cm}} \frac{\text{m}^c}{\text{sec}} = \boxed{\hspace{2cm}} \frac{\text{mrem}}{\text{hr}} \text{ at site boundary}$$

$$3. \quad \underline{\hspace{2cm}} \frac{\text{Ci}}{\text{sec}} \text{ (from line 1)} \times 16.0$$

$$\text{divided by } \underline{\hspace{2cm}} \frac{\text{m}^c}{\text{sec}} + \underline{\hspace{2cm}} \frac{\text{Ci}^d}{\text{sec}} \times 3.40^e$$

$$\text{divided by } \underline{\hspace{2cm}} \frac{\text{m}^c}{\text{sec}} = \boxed{\hspace{2cm}} \frac{\text{mrem}}{\text{hr}} \text{ at point of max X/Q for offgas stack release}$$

$$4. \quad \underline{\hspace{2cm}} \frac{\text{Ci}}{\text{sec}} \text{ (from line 1)} \times 168.0$$

$$\text{divided by } \underline{\hspace{2cm}} \frac{\text{m}^c}{\text{sec}} + \underline{\hspace{2cm}} \frac{\text{Ci}^d}{\text{sec}} \times 5.00^e$$

$$\text{divided by } \underline{\hspace{2cm}} \frac{\text{m}^c}{\text{sec}} = \boxed{\hspace{2cm}} \frac{\text{mrem}}{\text{hr}} \text{ at 2 miles}$$

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3a
INITIAL DOSE PROJECTIONS	Page 37 of 41
	Revision 2
	Date 3/11/83

ATTACHMENT III, CALCULATION SHEET III (continued)

5.  $\frac{Ci}{sec}$  (from line 1) x 44.0  
divided by  $\frac{m^C}{sec} + \frac{Ci^d}{sec} \times 4.20^e$   
divided by  $\frac{m^C}{sec} = \boxed{\phantom{000}} \frac{mrem}{hr}$  at 5 miles
6.  $\frac{Ci}{sec}$  (from line 1) x 16.0  
divided by  $\frac{m^C}{sec} + \frac{Ci^d}{sec} \times 3.40^e$   
divided by  $\frac{m^C}{sec} = \boxed{\phantom{000}} \frac{mrem}{hr}$  at 10 miles

NOTES:

- <sup>a</sup>Reactor building stack release rate from Summary Table, Section II, line 2.  
<sup>b</sup>Turbine building roof exhaust release rate from Summary Table, Section II, line 4.  
<sup>c</sup>Wind speed from Summary Table, Section I, line 5.  
<sup>d</sup>Offgas stack release rate from Summary Table, Section II, line 3.  
<sup>e</sup>If Standby Gas Treatment is in operation (see Data Summary Sheet, Section II.D, line 1) multiply this number by 0.662.

D. Whole body dose - Results for Summary Table Section III, line 5.

1.  $\frac{mrem}{hr}$  (from line C2) x  $\phantom{000} hr^a$   
=  $\boxed{\phantom{000}}$  mrem at site boundary
2.  $\frac{mrem}{hr}$  (from line C3) x  $\phantom{000} hr^a$   
=  $\boxed{\phantom{000}}$  mrem at point of max X/Q for offgas stack release

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3a
INITIAL DOSE PROJECTIONS	Page 38 of 41
	Revision 2
	Date 3/11/83

ATTACHMENT III, CALCULATION SHEET III (continued)

3.  $\frac{\text{mrem}}{\text{hr}}$  (from line C4) x  $\text{hra}$

=  $\boxed{\phantom{000}}$  mrem at 2 miles

4.  $\frac{\text{mrem}}{\text{hr}}$  (from line C5) x  $\text{hra}$

=  $\boxed{\phantom{000}}$  mrem at 5 miles

5.  $\frac{\text{mrem}}{\text{hr}}$  (from line C6) x  $\text{hra}$

=  $\boxed{\phantom{000}}$  mrem at 10 miles

NOTE:

<sup>a</sup>Obtain exposure time from Summary Table, Section II, line 1.

E. Thyroid Dose Commitment - Result for Summary Table, Section III, line 6.

1.  $\left( \frac{\text{Ci}^a}{\text{sec}} + \frac{\text{Ci}^b}{\text{sec}} \right) \times 0.3 = \frac{\text{Ci}}{\text{sec}}$

2.  $\frac{\text{Ci}^c}{\text{sec}} \times 0.3^d = \frac{\text{Ci}}{\text{sec}}$

3.  $\frac{\text{Ci}}{\text{sec}}$  (line 1) x  $\frac{\text{sec}}{\text{m}^3}$  (line A.1)

+  $\frac{\text{Ci}}{\text{sec}}$  (line 2) x  $\frac{\text{sec}}{\text{m}^3}$  (line B.1)

=  $\frac{\text{Ci}}{\text{m}^3}$

4.  $\frac{\text{Ci}}{\text{sec}}$  (line 1) x  $\frac{\text{sec}}{\text{m}^3}$  (line A.2)

+  $\frac{\text{Ci}}{\text{sec}}$  (line 2) x  $\frac{\text{sec}}{\text{m}^3}$  (line B.2)

=  $\frac{\text{Ci}}{\text{m}^3}$

## ATTACHMENT III, CALCULATION SHEET III (continued)

5.  $\frac{Ci}{sec} \text{ (line 1)} \times \frac{sec}{m^3} \text{ (line A.3)}$   
+  $\frac{Ci}{sec} \text{ (line 2)} \times \frac{sec}{m^3} \text{ (line B.3)}$   
=  $\frac{Ci}{m^3}$
6.  $\frac{Ci}{sec} \text{ (line 1)} \times \frac{sec}{m^3} \text{ (line A.4)}$   
+  $\frac{Ci}{sec} \text{ (line 2)} \times \frac{sec}{m^3} \text{ (line B.4)}$   
=  $\frac{Ci}{m^3}$
7.  $\frac{Ci}{sec} \text{ (line 1)} \times \frac{sec}{m^3} \text{ (line A.5)}$   
+  $\frac{Ci}{sec} \text{ (line 2)} \times \frac{sec}{m^3} \text{ (line B.5)}$   
=  $\frac{Ci}{m^3}$
8.  $\frac{Ci}{m^3} \text{ (line 3)} \times \text{hre} \times 3.8 \times 10^8$   
=  mrem at site boundary
9.  $\frac{Ci}{m^3} \text{ (line 4)} \times \text{hre} \times 3.8 \times 10^8$   
=  mrem at point of max X/Q for offgas stack release
10.  $\frac{Ci}{m^3} \text{ (line 5)} \times \text{hre} \times 3.8 \times 10^8$   
=  mrem at 2 miles

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3a
INITIAL DOSE PROJECTIONS	Page 40 of 41
	Revision 2
	Date 3/11/83

ATTACHMENT III, CALCULATION SHEET III (continued)

11.  $\frac{C_i}{m^3}$  (line 6) x \_\_\_\_\_ hr<sup>e</sup> x 3.8 x 10<sup>8</sup>  
 =  mrem at 5 miles

12.  $\frac{C_i}{m^3}$  (line 7) x \_\_\_\_\_ hr<sup>e</sup> x 3.8 x 10<sup>8</sup>  
 =  mrem at 10 miles

NOTES:

<sup>a</sup>Reactor building stack release rate from Summary Table, Section II, line 2.

<sup>b</sup>Turbine building roof exhaust release rate from Summary Table, Section II, line 4.

<sup>c</sup>Offgas stack release rate from Summary Table, Section II, line 3.

<sup>d</sup>If Standby Gas Treatment is in operation (See Data Summary Sheet, Section II.D, line 1) use 0.003, otherwise use 0.3.

<sup>e</sup>Obtain release duration from Summary Table, Section II, line 1.

F. Plume Width - The following are the plume widths to be placed in the Summary Table, Section III, line 7.

Site Bdy	Point of maximum X/Q for Offgas Stack release	2mi	5mi	10mi
90 meters	2000	530	970	2000

G. Plume arrival time - Results for Summary Table, Section III, line 8.

1. 0.125 ÷  $\frac{ma}{sec}$  =  hr to Site Boundary

2. 4.47 ÷  $\frac{ma}{sec}$  =  hr to point of max X/Q for offgas stack release

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3a
INITIAL DOSE PROJECTIONS	Page 41 of 41
	Revision 2
	Date 3/11/83

ATTACHMENT III, CALCULATION SHEET III (continued)

$$3. \quad 0.894 \div \underline{\hspace{2cm}} \frac{m^a}{sec} = \boxed{\hspace{2cm}} \text{ hr to 2 miles}$$

$$4. \quad 2.23 \div \underline{\hspace{2cm}} \frac{m^a}{sec} = \boxed{\hspace{2cm}} \text{ hr to 5 miles}$$

$$5. \quad 4.47 \div \underline{\hspace{2cm}} \frac{m^a}{sec} = \boxed{\hspace{2cm}} \text{ hr to 10 miles}$$

NOTE:

<sup>a</sup>Obtain wind speed from Summary Table, Section I, line 5.

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3b
FOLLOW-UP DOSE PROJECTIONS	Page 1 of 94
	Revision 2
	Date 4/11/83

## 1.0 PURPOSE

This procedure provides instructions for estimating the downwind dose rates resulting from noble gas and radioiodine releases during an emergency at DAEC.

## 2.0 APPLICABILITY

This procedure applies to immediate specific steps to be taken by radiological assessment personnel during a release of radioactive material (after the first hour following shutdown) to the environment.

## 3.0 RESPONSIBILITIES

### 3.1 Site Radiation Protection Coordinator

Perform dose projection calculations until the EOF is manned.

Evaluate the results of dose projection calculations.

Initially identify the need for field survey data to backup projected dose calculations.

### 3.2 Emergency Coordinator

Initially advise local and State authorities of the results of dose projection calculations and provide protective action recommendations as required.

### 3.3 IELP Radiological Assessment Coordinator

Perform dose projection calculations.

Provide protective action recommendations as required.

## 4.0 INTRODUCTION

The major objective of this procedure is to perform the offsite dose estimate for comparison with protective action guidelines to determine the appropriate emergency action to be taken following an accidental atmospheric release of radioactive material. As a result of this objective the procedure has been developed with five major parts. The first consists of the main body of the procedure and contains general information about the procedure, general instructions for its use and the protective action guidelines. The second part consists of a Data Summary Sheet, Attachment I, which contains all the monitor data necessary for the dose projections. The third part, Attachment II, consists of a summary Table to be completed during the dose estimation procedure. This table contains all the information necessary for comparison with the protective action guidelines. The completion of this table requires a number of calculations to be performed. These calculations are set up in detail on Calculation Sheets which comprise the fourth part of the procedure, Attachment III. The, Data

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3b
FOLLOW-UP DOSE PROJECTIONS	Page 2 of 94
	Revision 2
	Date 4/11/83

Summary Sheet, Summary Table, and the Calculation Sheets are designed to be used together, that is, the Calculation Sheets are required to complete the Summary Table while information from the Data Summary Sheet and Summary Table is required in many of the calculations performed on the Calculation Sheets. When calculations are required the Summary Table references the appropriate segment of the Calculation Sheets to be completed, likewise when data is required from the Data Summary Sheet and Summary Table the appropriate Data Summary Sheet or Summary Table line number is referenced on the Calculation Sheet. The fifth part, Attachment IV, contains all the figures referenced in the Calculation Sheets.

#### NOTE

A supply of Data Summary Sheets, Summary Tables, and Calculation Sheets are to be maintained in the Technical Support Center (TSC) and Emergency Operations Facility (EOF) for emergency use.

### 5.0 INSTRUCTIONS

- 5.1 If an off-site radiological release has been identified, use the simplified method EPIP 3.3a for the initial dose calculation (within the first hour following shutdown). Subsequent dose calculations shall be made utilizing the methods contained within this procedure.
- 5.2 If an accidental atmospheric release of radioactive material has been identified or there is a significant change in the release rate a dose projection is to be performed as follows.
  - 5.2.1 Complete Data Summary Sheet.
  - 5.2.2 Complete Section I of the Summary Table, General Information, using Calculation Sheet I where referenced.
  - 5.2.3 Complete Section II of the Summary Table, Release Information, to determine the total gaseous release rate from the Reactor Building Stacks, the Offgas Stack, and the Turbine Building Roof Exhaust. Use Calculation Sheet II, where referenced, to perform the necessary release rate calculations.

When multiple monitor ranges are available complete the calculations for ONE range ONLY. Use the range which gives a reading nearest mid-scale.

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3b
FOLLOW-UP DOSE PROJECTIONS	Page 3 of 94
	Revision 2
	Date 4/11/83

- 5.2.4 Complete Section III of the Summary Table, Dose Information. Use Calculation Sheet III, where referenced, to perform all necessary calculations. Calculation Sheet III is divided into five sections of which only two are to be completed. Section I is always completed and determines, based on the atmospheric stability, which one of the remaining four sections is to be used to perform the dose estimation. The Calculation Sheet subsections referenced in Section III of the Summary Table are those of the appropriate section for dose estimation as determined by Section I. That is, Sections II through V of Calculation Sheet III have the same format only the constants which are dependent on atmospheric stability are different.
- 5.2.5 Complete Section IV of the Summary Table if an estimate of the release rate is to be made from a field exposure rate measurement.
- 5.2.6 Report the results of the dose estimation calculations, i.e., supply copies of the Summary Table, to the Emergency Coordinator and/or the Site Radiation Protection Coordinator or the Radiological Assessment Coordinator.
- 5.2.7 The Site Radiation Protection Coordinator or the Radiological Assessment Coordinator shall compare the dose estimates from the Summary Table to the following Protective Action Guidelines and initiate the appropriate action.

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3b
FOLLOW-UP DOSE PROJECTIONS	Page 4 of 94
	Revision 2
	Date 4/11/83

### PROTECTIVE ACTION GUIDELINES

#### Projected Exposure to An Individual In the Population

#### Recommended Action

Whole Body = less than 1 Rem or  
Thyroid = less than 5 Rem.

1. No protective action required.
2. Issue an advisory to seek shelter and await further instructions or voluntarily evacuate.
3. Monitor environmental radiation levels.

Whole Body = 1 to 5 Rem or  
Thyroid = 5 to 25 Rem

1. Seek shelter and await further instructions.
2. Consider evacuation, particularly for children and pregnant women.
3. Monitor environmental radiation levels.
4. Control access.

Whole Body = 5 Rem and above or  
Thyroid = 25 Rem and above

1. Conduct evacuation of populations in the predetermined area.
2. Monitor environmental radiation levels and adjust area for evacuation based on these controls.
3. Control access.

## FOLLOW-UP DOSE PROJECTIONS

## 6.0 REFERENCES

1. Duane Arnold Energy Center Emergency Plan
2. IELP Corporate Emergency Response Plan

## 7.0 ATTACHMENTS

1. Data Summary Sheet
2. Summary Table
3. Calculation Sheets
4. Figures

APPROVED BY:

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Radiation Protection Supervisor

DATE:

5/6/83

REVIEWED BY:

H. S. Linger  
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DATE:

5/9/83

APPROVED BY:

R. S. Cook for  
Operations Supervisor

DATE:

5-9-83

REVIEWED BY:

BR York  
Chairman, Operations Committee

DATE:

5/16/83

APPROVED BY:

BR York for  
Plant Superintendent - Nuclear

DATE:

5/16/83

## ATTACHMENT I, DATA SUMMARY SHEET

Date: \_\_\_\_\_ Recorded By: \_\_\_\_\_  
Time: \_\_\_\_\_ Calculation Number: \_\_\_\_\_

## I. METEROLOGICAL DATA

1. Wind Direction<sup>a</sup> \_\_\_\_\_ (Wind from)
2. Wind speed<sup>a</sup> \_\_\_\_\_ mph
3.  $\Delta T^b$  \_\_\_\_\_ °F
4. Time after shutdown \_\_\_\_\_ (hours)
5. Time release started \_\_\_\_\_ (24 hour clock)

## NOTES:

<sup>a</sup>Obtain wind speed and direction from met panel in control room or Cedar Rapids Flight Service at 9-364-7127.

<sup>b</sup>Obtain from atmospheric  $\Delta T$  recorder readout in control room.

## II. RELEASE DATA

- A. Reactor Building Stacks - Obtain release concentrations from the effluent monitoring system.

Range<sup>e</sup>

1. "A" Stack Conc.<sup>a</sup> \_\_\_\_\_ uCi/cc x \_\_\_\_\_ MRCF(if applicable)= \_\_\_\_\_ corrected uCi/cc  
Hi ☐ Int. ☐ Nor. ☐
2. "B" Stack Conc.<sup>a</sup> \_\_\_\_\_ uCi/cc x \_\_\_\_\_ MRCF(if applicable)= \_\_\_\_\_ corrected uCi/cc  
Hi ☐ Int. ☐ Nor. ☐
3. "A" Stack Conc.<sup>a</sup> \_\_\_\_\_ uCi/cc x \_\_\_\_\_ MRCF(if applicable)= \_\_\_\_\_ corrected uCi/cc  
Hi ☐ Int. ☐ Nor. ☐
4. "A" Stack Flow<sup>b</sup> \_\_\_\_\_ cfm
5. "B" Stack Flow<sup>b</sup> \_\_\_\_\_ cfm
6. "C" Stack Flow<sup>b</sup> \_\_\_\_\_ cfm

## FOLLOW-UP DOSE PROJECTIONS

## ATTACHMENT I, DATA SUMMARY SHEET (continued)

- B. Offgas Stack - obtain release concentration from the effluent monitoring system.

Range<sup>e</sup>

1. Offgas Stack Conc.<sup>a</sup>      uCi/cc x      MRCF (if applicable) =      corrected uCi/cc

Hi ☐ Int. ☐ Nor. ☐

2. Offgas Stack Flow<sup>c</sup>                      cfm

- C. Turbine Exhaust - obtain release concentration from the effluent monitoring system.

1. Turb. Exhaust Conc<sup>a</sup>      uCi/cc x      MRCF (if applicable) =      corrected uCi/cc

Hi ☐ Int. ☐ Nor. ☐

2. Turb. Exhaust Flow<sup>d</sup>                      cfm

Notes (a-e):

- a. Data collected from Kaman Effluent Monitoring System see PASAP 6.0 and PCP 10.6A for system operating instructions.
- b. Data available either from the Kaman Effluent Monitoring System or from Control Room Panel 1C-23.
- c. Data available either from the Kaman Effluent Monitoring System or from Control Room Panel 1C-02.
- d. Data available either from the Kaman Effluent Monitoring System or can be estimated by:  
18,000 cfm for each fan in slow speed  
36,000 cfm for each fan in fast speed
- e. If the high or intermediate range is used, use Fig. 26 to get the Monitor Response Correction Factor (MRCF).

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3b
FOLLOW-UP DOSE PROJECTIONS	Page 8 of 94
	Revision 2
	Date 4/11/83

ATTACHMENT I, DATA SUMMARY SHEET (continued)

D. Miscellaneous Data

1. Is Standby Gas Treatment for Offgas Stack Exhaust in operation:

YES ☐ NO ☐

2. Anticipated duration of release \_\_\_\_\_ hours. (If no estimate is available use 1.77 hours.)

3. Iodine activity to noble gas activity ratio-optional, to be completed only if known to be different than default values(0.3).

3a. \_\_\_\_\_ Reactor Building Stacks and Turbine Building Vent

3b. \_\_\_\_\_ Offgas Stack

III. Field Exposure Rate Information

1. Time of measurement after shutdown \_\_\_\_\_ hours.
2. Distance from release point to measurement location \_\_\_\_\_ meters.
3. Exposure rate \_\_\_\_\_ mR/hr.

## ATTACHMENT II, SUMMARY TABLE

Calculations Performed By: \_\_\_\_\_

## I. GENERAL INFORMATION

1. Calculation Number: \_\_\_\_\_ Date: \_\_\_\_\_ Time: \_\_\_\_\_
2. Time after Shutdown: \_\_\_\_\_ hours
3. Wind Direction (direction wind is blowing from): \_\_\_\_\_ deg.  
(Data Summary Sheet Section I, line 1).
4. Down Wind Direction: \_\_\_\_\_ deg. (Calc. Sheet I, Sec. A, line 1)
5. Wind Speed: \_\_\_\_\_ meters/sec. (Calc. sheet I, Sec. A, line 2)
6.  $\Delta T$ : \_\_\_\_\_ °F, Stability Class: \_\_\_\_\_ (Calc. Sheet I.,  
Sec. B)
7. Down wind Sector \_\_\_\_\_ (Calc. Sheet I, Section A, Line 3)
8. Time release started \_\_\_\_\_ hr. (24 hr. clock).

## II. RELEASE INFORMATION

1. Exposure Time \_\_\_\_\_ hours (Data Summary Sheet, Section II.D,  
line 2).
2. Release rate Reactor Bldg. Stack: \_\_\_\_\_ Ci/sec (Calc. Sheet II,  
Sec. I)
3. Release rate - offgas stack \_\_\_\_\_ Ci/sec (Calc. Sheet II, Sec. II)
4. Release rate - Turbine Bldg. Roof Exhaust: \_\_\_\_\_ Ci/sec (Calc.  
Sheet II, Sec. III.)
5. Total Gaseous Release Rate: \_\_\_\_\_ Ci/sec (add release rates  
from previous three lines)

## ATTACHMENT II, SUMMARY TABLE (continued)

## ATTACHMENT II, SUMMARY TABLE (continued)

## III. DOSE INFORMATION

Cal. sheet III, section number  
for remainder of dose  
calculations:  
(From calc. sheet III, section I)

	Site Bndry	Point of max. X/Q for Offgas Stack release <sup>a,e</sup>	Down Wind Location			Additional Locations <sup>d</sup>		
			2mi	5mi	10mi	No. 1	No. 2	No. 3
1. Distance to location, meters (miles) (Calc. Sheet III, subsection A) <sup>b</sup>	_____	_____	3218 (2)	8045 (5)	16090 (10)	_____	_____	_____
2. Normalized concentration, X/Q, sec/m <sup>3</sup> , Ground level release (Calc. Sheet III, Subsect. B) <sup>b</sup>	_____	_____	_____	_____	_____	_____	_____	_____
3. Normalized concentration, X/Q, sec/m <sup>3</sup> , Elevated release (Calc. Sheet III, Subsect. C) <sup>b</sup>	_____	_____	_____	_____	_____	_____	_____	_____
4. Whole body dose rate mrem/hr (Calc. Sheet III, Subsect. D) <sup>b</sup>	_____	_____	_____	_____	_____	_____	_____	_____
5. Whole body dose, mrem (Calc. Sheet III, Subsect. E) <sup>b</sup>	_____	_____	_____	_____	_____	_____	_____	_____
6. Thyroid dose commitment, <sup>c</sup> mrem (Calc. Sheet III, Subsect. F) <sup>b</sup>	_____	_____	_____	_____	_____	_____	_____	_____
7. Plume width, meters (miles) (Calc. Sheet III, Subsect. G) <sup>b</sup>	_____	_____	_____	_____	_____	_____	_____	_____
8. Plume arrival time, hr (Calc. Sheet III, Subsect. H) <sup>b</sup>	_____	_____	_____	_____	_____	_____	_____	_____

NOTE: a, b, c, d and e -- see next page

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3b
	Page 11 of 94
	Revision 2
FOLLOW-UP DOSE PROJECTIONS	Date 4/11/83

## ATTACHMENT II, SUMMARY TABLE (continued)

### NOTES:

<sup>a</sup>For stability class FG the distance to the maximum X/Q is greater than 10 miles. In order to limit the dose information to the EPZ a distance of 10 miles is used for class FG.

<sup>b</sup>Calculation sheet subsection refers to the subsection of the Calculation Sheet III section as given in the heading of this table and also in Calc. Sheet III, Section I.

<sup>c</sup>The thyroid dose commitment given is for an infant, i.e., the worst case. The adult dose commitment is obtained by multiplying by 0.58.

<sup>d</sup>Additional locations may be added at users discretion.

<sup>e</sup>Maximum X/Q is the location corresponding to the point of maximum ground level X/Q for an offgas stack (elevated) release.

### IV. Release Rate From Exposure Rate (Field Measurement)

Estimated total gaseous release rate \_\_\_\_\_ Ci/sec (Calc. Sheet IV)

Caution: This estimate should be considered to be a lower limit of the release rate.

## FOLLOW-UP DOSE PROJECTIONS

## ATTACHMENT III, CALCULATION SHEET I

## GENERAL INFORMATION

## A. Wind Speed

1. Downwind direction: \_\_\_\_\_ deg. (180° different from wind direction).

2. Wind Speed \_\_\_\_\_ mph (Data Summary Sheet, Section I, line 2)  $\times$  0.447 =

| \_\_\_\_\_ | Meters/sec (To Summary Table Sec. I, line 4)

3. Sector designation

Down Wind Direction, deg.

Sector

348.750 - 11.25

11.25 - 33.75

33.75 - 56.25

56.25 - 78.75

78.75 - 101.25

101.25 - 123.75

123.75 - 146.25

146.25 - 168.75

168.75 - 191.25

191.25 - 213.75

213.75 - 236.25

236.25 - 258.75

258.75 - 281.25

281.25 - 303.75

303.75 - 326.25

326.25 - 348.75

A

B

C

D

E

F

G

H

J

K

L

M

N

P

Q

R

## B. Stability Class

1.  $\Delta T$  | \_\_\_\_\_ | °F - (obtained from Data Summary Sheet, Section I, line 3) (To Summary Table, Sec. I, line 7)

2. Stability class is determined from the following table as a function of  $\Delta T$ .

Stability class | \_\_\_\_\_ | (To Summary Table, Sec I, line 7)

$\Delta T$  Range, °F

Stability Class

-1.26 or less

AB

-1.26 to -1.11

C

-1.11 to 1.11

DE

1.11 or greater

FG

## ATTACHMENT III, CALCULATION SHEET II

Page 1 of 5

## RELEASE INFORMATION

I. Reactor Building Stack Releases

1. "A" Stack Conc.<sup>a</sup> \_\_\_\_\_ uCi/cc x "A" Stack Flow<sup>a</sup>  
                                 cfm x 472 = \_\_\_\_\_ uCi/sec
2. "B" Stack Conc.<sup>a</sup> \_\_\_\_\_ uCi/cc x "B" Stack Flow<sup>a</sup>  
                                 cfm x 472 = \_\_\_\_\_ uCi/sec
3. "C" Stack Conc.<sup>a</sup> \_\_\_\_\_ uCi/cc x "C" Stack Flow<sup>a</sup>  
                                 cfm x 472 = \_\_\_\_\_ uCi/sec
4. "A" Stack Release Rate \_\_\_\_\_ uCi/sec  
    "B" Stack Release Rate \_\_\_\_\_ uCi/sec  
    "C" Stack Release Rate \_\_\_\_\_ uCi/sec  
    Total Release Rate \_\_\_\_\_ uCi/sec x

$$\frac{1 \text{ Curie}}{10^6 \text{ uCi}} = \boxed{\phantom{000000}} \text{ Ci/sec}$$

(To Summary Table, Sec. II, Line 2)

Note:

- a. Obtain data from Data Summary Sheet, Section II.A.

II. Offgas Stack Releases

1. Stack Conc.<sup>a</sup> \_\_\_\_\_ uCi/cc x Offgas Stack  
    Flow<sup>a</sup> \_\_\_\_\_ cfm x 472 = \_\_\_\_\_ uCi/sec
2. Release rate \_\_\_\_\_ uCi/sec x  $\frac{1 \text{ Curie}}{10^6 \text{ uCi}} =$

$$\boxed{\phantom{000000}} \text{ Ci/sec}$$

(To Summary Table, Sec. II, Line 3)

Note:

- a. Obtain data from Data Summary Sheet, Section II.B.

## ATTACHMENT III, CALCULATION SHEET II (continued)

Page 2 of 5

## III. Turbine Building Releases

1. Release Conc.<sup>a</sup> \_\_\_\_\_ uCi/cc x Flow<sup>a</sup> \_\_\_\_\_ cfm x 472 =  
\_\_\_\_\_ uCi/sec

2. Release rate \_\_\_\_\_ uCi/sec x  $\frac{1 \text{ Curie}}{10^6 \text{ uCi}} =$

\_\_\_\_\_ Ci/sec

(To Summary Table Sec. II, Line 4)

## Note:

- a. Obtain data from Data Summary Sheet, Section II.C.

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3b
	Page 15 of 94
	Revision 2
FOLLOW-UP DOSE PROJECTIONS	Date 4/11/83

# ATTACHMENT III, CALCULATION SHEET III

Page 5 of 5

## DOSE INFORMATION

- I. Section for the remaining calculations  - Appropriate section is determined from the following table based on the atmospheric stability class. Complete ONLY ONE section.

Stability Class  
(from Summary Table,  
Section I, line 6)

Section

AB

II (page 16 of 94)

C

III (page 29 of 94)

DE

IV (page 42 of 94)

FG

V (page 54 of 94)

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3b
FOLLOW-UP DOSE PROJECTIONS	Page 16 of 94
	Revision 2
	Date 4/11/83

### ATTACHMENT III, CALCULATION SHEET III (continued)

#### II. Dose information for atmospheric stability class AB

##### A. Variable distance and Xu/Q Values

1. Obtain distance to site boundary and Xu/Q for ground level and elevated releases from following Table using the down wind direction from Summary Table, Section I, line 4.

Distance = \_\_\_\_\_ m       $\frac{X_u}{Q}$  (Ground Level Rel.) = \_\_\_\_\_  $\frac{1}{m^2}$

$\frac{X_u}{Q}$  (Elevated Rel.) = \_\_\_\_\_  $\frac{1}{m^2}$

Down Wind Direction deg.	Distance to Site Bdy, meters	$\frac{X_u}{Q}, \frac{1}{m^2}$	
		Ground Level Rel.	Elevated Rel.
0 - 11.25	1200	$3.8 \times 10^{-6}$	$3.7 \times 10^{-6}$
11.25 - 33.75	1600	$1.9 \times 10^{-6}$	$1.9 \times 10^{-6}$
33.75 - 56.25	700	$1.4 \times 10^{-5}$	$1.2 \times 10^{-5}$
56.25 - 78.75	610	$1.9 \times 10^{-5}$	$1.5 \times 10^{-5}$
78.75 - 101.25	490	$3.2 \times 10^{-5}$	$2.0 \times 10^{-5}$
101.25 - 123.75	450	$4.0 \times 10^{-5}$	$2.2 \times 10^{-5}$
123.75 - 146.25	480	$3.3 \times 10^{-5}$	$2.1 \times 10^{-5}$
146.25 - 168.75	500	$3.0 \times 10^{-5}$	$1.9 \times 10^{-5}$
168.75 - 191.25	460	$3.9 \times 10^{-5}$	$2.2 \times 10^{-5}$
191.25 - 213.75	500	$3.0 \times 10^{-5}$	$1.9 \times 10^{-5}$
213.75 - 236.25	630	$1.8 \times 10^{-5}$	$1.4 \times 10^{-5}$
236.25 - 258.75	720	$1.3 \times 10^{-5}$	$1.2 \times 10^{-5}$
258.75 - 281.25	670	$1.5 \times 10^{-5}$	$1.3 \times 10^{-5}$
281.25 - 303.75	730	$1.3 \times 10^{-5}$	$1.1 \times 10^{-5}$
303.75 - 326.25	980	$6.2 \times 10^{-6}$	$5.8 \times 10^{-6}$
326.25 - 348.75	1300	$3.1 \times 10^{-6}$	$3.0 \times 10^{-6}$
348.75 - 360.00	1200	$3.8 \times 10^{-6}$	$3.7 \times 10^{-6}$

2. Distance to point of maximum  $\frac{X_u}{Q}$  for offgas stack release = 400 m.

## ATTACHMENT III, CALCULATION SHEET III (continued)

## B. Normalized concentration, Ground Level Release - Results for Summary Table, Section III, Line 2.

- 1a.
1.  $\frac{1}{m^2} \div$  \_\_\_\_\_ m/sec<sup>b</sup> =  $\frac{\text{sec}}{m^3}$  at site boundary
  2.  $5.3 \times 10^{-5} \div$  \_\_\_\_\_ m/sec<sup>b</sup> =  $\frac{\text{sec}}{m^3}$  at point of max X/Q for offgas stack release
  3.  $3.8 \times 10^{-7} \div$  \_\_\_\_\_ m/sec<sup>b</sup> =  $\frac{\text{sec}}{m^3}$  at 2 miles
  4.  $4.0 \times 10^{-8} \div$  \_\_\_\_\_ m/sec<sup>b</sup> =  $\frac{\text{sec}}{m^3}$  at 5 miles
  5.  $7.4 \times 10^{-9} \div$  \_\_\_\_\_ m/sec<sup>b</sup> =  $\frac{\text{sec}}{m^3}$  at 10 miles
  6.  $\frac{1^c}{m^2} \div$  \_\_\_\_\_ m/sec<sup>b</sup> =  $\frac{\text{sec}}{m^3}$  at additional location No. 1
  7.  $\frac{1^c}{m^2} \div$  \_\_\_\_\_ m/sec<sup>b</sup> =  $\frac{\text{sec}}{m^3}$  at additional location No. 2
  8.  $\frac{1^c}{m^2} \div$  \_\_\_\_\_ m/sec<sup>b</sup> =  $\frac{\text{sec}}{m^3}$  at additional location No. 3

## NOTE:

<sup>a</sup>Obtain  $\frac{X_u}{Q}$  for ground level release from Section II, Subsection A, line 1.

<sup>b</sup>Obtain wind speed from Summary Table, Section I, line 5.

<sup>c</sup>Obtain ground level release  $\frac{X_u}{Q}$  for additional locations using Figure 1 and appropriate distance from Summary Table, Section III, line 1.

## ATTACHMENT III, CALCULATION SHEET III (continued)

C. Normalized concentration, Elevated Release - Results for Summary Table, Section III, line 3.

$$1. \quad \frac{1^a}{m^2} \div \text{_____} \text{ m/sec}^b = \boxed{\text{_____}} \frac{\text{sec}}{m^3} \text{ at site boundary}$$

$$2. \quad 2.4 \times 10^{-5} \div \text{_____} \text{ m/sec}^b = \boxed{\text{_____}} \frac{\text{sec}}{m^3} \text{ at point of max X/Q for offgas stack release}$$

$$3. \quad 3.5 \times 10^{-7} \div \text{_____} \text{ m/sec}^b = \boxed{\text{_____}} \frac{\text{sec}}{m^3} \text{ at 2 miles}$$

$$4. \quad 3.9 \times 10^{-8} \div \text{_____} \text{ m/sec}^b = \boxed{\text{_____}} \frac{\text{sec}}{m^3} \text{ at 5 miles}$$

$$5. \quad 7.6 \times 10^{-9} \div \text{_____} \text{ m/sec}^b = \boxed{\text{_____}} \frac{\text{sec}}{m^3} \text{ at 10 miles}$$

$$6. \quad \frac{1^c}{m^2} \div \text{_____} \text{ m/sec}^b = \boxed{\text{_____}} \frac{\text{sec}}{m^3} \text{ at additional location No. 1}$$

$$7. \quad \frac{1^c}{m^2} \div \text{_____} \text{ m/sec}^b = \boxed{\text{_____}} \frac{\text{sec}}{m^3} \text{ at additional location No. 2}$$

$$8. \quad \frac{1^c}{m^2} \div \text{_____} \text{ m/sec}^b = \boxed{\text{_____}} \frac{\text{sec}}{m^3} \text{ at additional location No. 3}$$

## NOTE:

<sup>a</sup>Obtain  $\frac{X_u}{Q}$  for elevated release from Section II, Subsection A, line 1.

<sup>b</sup>Obtain wind speed from Summary Table, Section I, line 5.

<sup>c</sup>Obtain elevated release  $\frac{X_u}{Q}$  for additional locations using Figure 2 and appropriate distance from Summary Table, Section III, line 1.

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3b
FOLLOW-UP DOSE PROJECTIONS	Page 19 of 94
	Revision 2
	Date 4/11/83

ATTACHMENT III, CALCULATION SHEET III (continued)

D. Whole body dose rate - Results for Summary Table Section III, line 4.

1.  $\frac{C_1^a}{\text{sec}} + \frac{C_1^b}{\text{sec}} = \frac{C_1}{\text{sec}}$

2a.  $\text{FIM} \times \text{DFID} =$

2b.  $(1 - \text{FIM}) \times \text{DFNG}^e =$

2c.  $(\text{line 2a}) + (\text{line 2b}) = \text{DF}$

3.  $\frac{D_u}{Q}$  for site boundary:

3a.  $\text{FIC} \times \text{DUOQIF}^f \times \text{TCFI}^g =$

3b.  $(1 - \text{FIC}) \times \text{DUOQNG}^h \times \text{TCFNG}^i =$

3c.  $(\text{line 3a}) + (\text{line 3b}) =$

4.  $\frac{D_u}{Q}$  for location of maximum  $\frac{X_u}{Q}$ :

4a.  $\text{FIC} \times 18.0 \times \text{TCFI}^g =$

4b.  $(1 - \text{FIC}) \times 9.20 \times \text{TCFNG}^i =$

4c.  $(\text{line 4a}) + (\text{line 4b}) =$

5.  $\frac{D_u}{Q}$  for 2 miles:

5a.  $\text{FIC} \times 0.360 \times \text{TCFI}^g =$

5b.  $(1 - \text{FIC}) \times 0.250 \times \text{TCFNG}^i =$

5c.  $(\text{line 5a}) + (\text{line 5b}) =$

6.  $\frac{D_u}{Q}$  for 5 miles:

6a.  $\text{FIC} \times 5.00 \times 10^{-2} \times \text{TCFI}^g =$

6b.  $(1 - \text{FIC}) \times 3.40 \times 10^{-2} \times \text{TCFNG}^i =$

6c.  $(\text{line 6a}) + (\text{line 6b}) =$

## ATTACHMENT III, CALCULATION SHEET III (continued)

7.  $\frac{Du}{Q}$  for 10 miles:

7a. \_\_\_\_\_ FIC x  $2.10 \times 10^{-2}$  x \_\_\_\_\_ TCFI<sup>g</sup> = \_\_\_\_\_

7b.  $(1 - \text{_____ FIC}) \times 1.50 \times 10^{-2}$  x \_\_\_\_\_ TCFNG<sup>i</sup> = \_\_\_\_\_

7c. \_\_\_\_\_ (line 7a) + \_\_\_\_\_ (line 7b) = \_\_\_\_\_

8.  $\frac{Du}{Q}$  for additional location No. 1

8a. \_\_\_\_\_ FIC x \_\_\_\_\_ DUOQI<sup>f</sup> x \_\_\_\_\_ TCFI<sup>g</sup> = \_\_\_\_\_

8b.  $(1 - \text{_____ FIC}) \times \text{_____ DUOQNG}^h \times \text{_____ TCFNG}^i = \text{_____}$

8c. \_\_\_\_\_ (line 8a) + \_\_\_\_\_ (line 8b) = \_\_\_\_\_

9.  $\frac{Du}{Q}$  for additional location No. 2

9a. \_\_\_\_\_ FIC x \_\_\_\_\_ DUOQI<sup>f</sup> x \_\_\_\_\_ TCFI<sup>g</sup> = \_\_\_\_\_

9b.  $(1 - \text{_____ FIC}) \times \text{_____ DUOQNG}^h \times \text{_____ TCFNG}^i = \text{_____}$

9c. \_\_\_\_\_ (line 9a) + \_\_\_\_\_ (line 9b) = \_\_\_\_\_

10.  $\frac{Du}{Q}$  for additional location No. 3

10a. \_\_\_\_\_ FIC x \_\_\_\_\_ DUOQI<sup>f</sup> x \_\_\_\_\_ TCFI<sup>g</sup> = \_\_\_\_\_

10b.  $(1 - \text{_____ FIC}) \times \text{_____ DUOQNG}^h \times \text{_____ TCFNG}^i = \text{_____}$

10c. \_\_\_\_\_ (line 10a) + \_\_\_\_\_ (line 10b) = \_\_\_\_\_

11a. \_\_\_\_\_  $\frac{Ci}{\text{sec}}$  (line 1) x \_\_\_\_\_  $\frac{\text{sec}^j}{m^3}$  x \_\_\_\_\_ (line 2) = \_\_\_\_\_

11b. \_\_\_\_\_  $\frac{Ci^k}{\text{sec}}$  x \_\_\_\_\_  $\frac{Du}{Q}$  (line 3) + \_\_\_\_\_  $\frac{m^l}{\text{sec}}$  = \_\_\_\_\_

11c. \_\_\_\_\_ (line 11a) + \_\_\_\_\_ (line 11b)

= \_\_\_\_\_  $\frac{\text{mrem}}{\text{hr}}$  at site boundary

## FOLLOW-UP DOSE PROJECTIONS

## ATTACHMENT III, CALCULATION SHEET III (continued)

$$12a. \quad \frac{Ci}{\text{sec}} (\text{line 1}) \times \frac{\text{sec}^j}{m^3} \times (\text{line 2}) =$$

$$12b. \quad \frac{Cik}{\text{sec}} \times \frac{Du}{Q} (\text{line 4}) + \frac{m^1}{\text{sec}} =$$

$$12c. \quad (\text{line 12a}) + (\text{line 12b})$$

$$= \boxed{\phantom{000000}} \frac{mrem}{hr} \text{ at point of max } \frac{Du}{Q} \text{ for offgas stack release}$$

$$13a. \quad \frac{Ci}{\text{sec}} (\text{line 1}) \times \frac{\text{sec}^j}{m^3} \times (\text{line 2}) =$$

$$13b. \quad \frac{Cik}{\text{sec}} \times \frac{Du}{Q} (\text{line 5}) + \frac{m^1}{\text{sec}} =$$

$$13c. \quad (\text{line 13a}) + (\text{line 13b})$$

$$= \boxed{\phantom{000000}} \frac{mrem}{hr} \text{ at 2 miles}$$

$$14a. \quad \frac{Ci}{\text{sec}} (\text{line 1}) \times \frac{\text{sec}^j}{m^3} \times (\text{line 2}) =$$

$$14b. \quad \frac{Cik}{\text{sec}} \times \frac{Du}{Q} (\text{line 6}) + \frac{m^1}{\text{sec}} =$$

$$14c. \quad (\text{line 14a}) + (\text{line 14b})$$

$$= \boxed{\phantom{000000}} \frac{mrem}{hr} \text{ at 5 miles}$$

$$15a. \quad \frac{Ci}{\text{sec}} (\text{line 1}) \times \frac{\text{sec}^j}{m^3} \times (\text{line 2}) =$$

$$15b. \quad \frac{Cik}{\text{sec}} \times \frac{Du}{Q} (\text{line 7}) + \frac{m^1}{\text{sec}} =$$

$$15c. \quad (\text{line 15a}) + (\text{line 15b})$$

$$= \boxed{\phantom{000000}} \frac{mrem}{hr} \text{ at 10 miles}$$

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3b
FOLLOW-UP DOSE PROJECTIONS	Page 22 of 94
	Revision 2
	Date 4/11/83

ATTACHMENT III, CALCULATION SHEET III (continued)

$$16a. \frac{C_i}{\text{sec}} (\text{line 1}) \times \frac{\text{sec}^j}{\text{m}^3} \times \text{_____} (\text{line 2}) = \text{_____}$$

$$16b. \frac{C_{ik}}{\text{sec}} \times \frac{D_u}{Q} (\text{line 8}) + \frac{\text{m}^1}{\text{sec}} = \text{_____}$$

$$16c. \text{_____} (\text{line 16a}) + \text{_____} (\text{line 16b})$$

$$= \boxed{\text{_____}} \frac{\text{mrem}}{\text{hr}} \text{ at additional location No. 1}$$

$$17a. \frac{C_i}{\text{sec}} (\text{line 1}) \times \frac{\text{sec}^j}{\text{m}^3} \times \text{_____} (\text{line 2}) = \text{_____}$$

$$17b. \frac{C_{ik}}{\text{sec}} \times \frac{D_u}{Q} (\text{line 9}) + \frac{\text{m}^1}{\text{sec}} = \text{_____}$$

$$17c. \text{_____} (\text{line 17a}) + \text{_____} (\text{line 17b})$$

$$= \boxed{\text{_____}} \frac{\text{mrem}}{\text{hr}} \text{ at additional location No. 2}$$

$$18a. \frac{C_i}{\text{sec}} (\text{line 1}) \times \frac{\text{sec}^j}{\text{m}^3} \times \text{_____} (\text{line 2}) = \text{_____}$$

$$18b. \frac{C_{ik}}{\text{sec}} \times \frac{D_u}{Q} (\text{line 10}) + \frac{\text{m}^1}{\text{sec}} = \text{_____}$$

$$18c. \text{_____} (\text{line 18a}) + \text{_____} (\text{line 18b})$$

$$= \boxed{\text{_____}} \frac{\text{mrem}}{\text{hr}} \text{ at additional location No. 3}$$

NOTES:

<sup>a</sup>Reactor building stack release rate from Summary Table, Section II, line 2.

<sup>b</sup>Turbine building roof exhaust release rate from Summary Table, Section II, line 4.

<sup>c</sup>Iodine activity to noble gas activity ratio-obtain from Data Summary Sheet Section IID, line 3b. If unknown use 0.3 unless Standby Gas Treatment is in operation (See Data Summary Sheet, Section II.D, line 1) then use 0.003.

<sup>d</sup>Obtain iodine dose factor (DFI) for time after shutdown (Summary Table, Section I, line 2) from Figure 3.

<sup>e</sup>Obtain noble gas dose factor (DFNG) for time after shutdown (Summary Table, Section I, line 2) from Figure 4.

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3b
	Page 23 of 94
	Revision 2
FOLLOW-UP DOSE PROJECTIONS	Date 4/11/83

ATTACHMENT III, CALCULATION SHEET III (continued)

<sup>f</sup> Obtain  $\frac{Du}{Q}$  for iodine (DUOQI) from Figure 5 using the appropriate distance from Summary Table, Section III, line 1.

<sup>g</sup> Obtain time correction factor for iodine (TCFI) from Figure 6 using time after shutdown (Summary Table, Section I, line 2).

<sup>h</sup> Obtain  $\frac{Du}{Q}$  for noble gas (DUOQNG) from Figure 7 using the appropriate distance from Summary Table, Section III, line 2.

<sup>i</sup> Obtain the noble gas time correction factor (TCFNG) from Figure 8 using time after shutdown (Summary Table, Section I, line 2).

<sup>j</sup> Obtain appropriate  $\frac{X}{Q}$  for ground level release from Summary Table, Section III, line 2.

<sup>k</sup> Obtain offgas stack release rate from Summary Table, Section II, line 3.

<sup>l</sup> Obtain wind speed from Summary Table, Section I, line 5.

<sup>m</sup> Iodine activity to noble gas activity ratio, obtain from Data Summary Sheet, Section II D, line 3a. If unknown use 0.3.

E. Whole body dose - Results for Summary Table Section III, line 5.

1.  $\frac{\text{mrem}}{\text{hr}}$  (from Section IID, line 11c) x  $\text{hr}^a$   
 =  mrem at site boundary

2.  $\frac{\text{mrem}}{\text{hr}}$  (from Section IID, line 12c) x  $\text{hr}^a$   
 =  mrem at point of max X/Q for offgas stack release

3.  $\frac{\text{mrem}}{\text{hr}}$  (from Section IID, line 13c) x  $\text{hr}^a$   
 =  mrem at 2 miles

4.  $\frac{\text{mrem}}{\text{hr}}$  (from Section IID, line 14c) x  $\text{hr}^a$   
 =  mrem at 5 miles

## ATTACHMENT III, CALCULATION SHEET III (continued)

$$5. \frac{\text{mrem}}{\text{hr}} \text{ (from Section IID, line 15c) } \times \text{ } \text{hra} \\ = \text{ } \text{mrem at 10 miles}$$

$$6. \frac{\text{mrem}}{\text{hr}} \text{ (from Section IID, line 16c) } \times \text{ } \text{hra} \\ = \text{ } \text{mrem at additional location No. 1}$$

$$7. \frac{\text{mrem}}{\text{hr}} \text{ (from Section IID, line 17c) } \times \text{ } \text{hra} \\ = \text{ } \text{mrem at additional location No. 2}$$

$$8. \frac{\text{mrem}}{\text{hr}} \text{ (from Section IID, line 18c) } \times \text{ } \text{hra} \\ = \text{ } \text{mrem at additional location No. 3}$$

## NOTE:

<sup>a</sup>Obtain exposure time from Summary Table, Section II, line 1.

F. Thyroid Dose Commitment - Result for Summary Table, Section III, line 6.

$$1. \left( \frac{\text{Ci}^a}{\text{sec}} + \frac{\text{Ci}^b}{\text{sec}} \right) \times \text{ } \text{FIG}^d = \text{ } \frac{\text{Ci}}{\text{sec}}$$

$$2. \frac{\text{Ci}^c}{\text{sec}} \times \text{ } \text{FIE}^e \frac{\text{Ci}}{\text{sec}}$$

$$3a. \frac{\text{Ci}}{\text{sec}} \text{ (line 1) } \times \frac{\text{sec}}{\text{m}^3} \text{ (Sect. IIB, line 1) } = \text{ } \frac{\text{Ci}}{\text{m}^3}$$

$$3b. \frac{\text{Ci}}{\text{sec}} \text{ (line 2) } \times \frac{\text{sec}}{\text{m}^3} \text{ (Sect. IIC, line 1) } = \text{ } \frac{\text{Ci}}{\text{m}^3}$$

$$3c. \text{ } \text{ (line 3a) } + \text{ } \text{ (line 3b) } = \text{ } \frac{\text{Ci}}{\text{m}^3}$$

## FOLLOW-UP DOSE PROJECTIONS

## ATTACHMENT III, CALCULATION SHEET III (continued)

- 4a.  $\frac{Ci}{sec}$  (line 1) x  $\frac{sec}{m^3}$  (Sect. IIB, line 2) =  $\frac{Ci}{m^3}$
- 4b.  $\frac{Ci}{sec}$  (line 2) x  $\frac{sec}{m^3}$  (Sect. IIC, line 2) =  $\frac{Ci}{m^3}$
- 4c. (line 4a) + (line 4b) =  $\frac{Ci}{m^3}$
- 5a.  $\frac{Ci}{sec}$  (line 1) x  $\frac{sec}{m^3}$  (Sect. IIB, line 3) =  $\frac{Ci}{m^3}$
- 5b.  $\frac{Ci}{sec}$  (line 2) x  $\frac{sec}{m^3}$  (Sect. IIC, line 3) =  $\frac{Ci}{m^3}$
- 5c. (line 5a) + (line 5b) =  $\frac{Ci}{m^3}$
- 6a.  $\frac{Ci}{sec}$  (line 1) x  $\frac{sec}{m^3}$  (Sect. IIB, line 4) =  $\frac{Ci}{m^3}$
- 6b.  $\frac{Ci}{sec}$  (line 2) x  $\frac{sec}{m^3}$  (Sect. IIC, line 4) =  $\frac{Ci}{m^3}$
- 6c. (line 6a) + (line 6b) =  $\frac{Ci}{m^3}$
- 7a.  $\frac{Ci}{sec}$  (line 1) x  $\frac{sec}{m^3}$  (Sect. IIB, line 5) =  $\frac{Ci}{m^3}$
- 7b.  $\frac{Ci}{sec}$  (line 2) x  $\frac{sec}{m^3}$  (Sect. IIC, line 5) =  $\frac{Ci}{m^3}$
- 7c. (line 7a) + (line 7b) =  $\frac{Ci}{m^3}$
- 8a.  $\frac{Ci}{sec}$  (line 1) x  $\frac{sec}{m^3}$  (Sect. IIB, line 6) =  $\frac{Ci}{m^3}$
- 8b.  $\frac{Ci}{sec}$  (line 2) x  $\frac{sec}{m^3}$  (Sect. IIC, line 6) =  $\frac{Ci}{m^3}$
- 8c. (line 8a) + (line 8b) =  $\frac{Ci}{m^3}$

## FOLLOW-UP DOSE PROJECTIONS

## ATTACHMENT III, CALCULATION SHEET III (continued)

$$9a. \frac{Ci}{sec} \text{ (line 1)} \times \frac{sec}{m^3} \text{ (Sect. IIB, line 7)} = \frac{Ci}{m^3}$$

$$9b. \frac{Ci}{sec} \text{ (line 2)} \times \frac{sec}{m^3} \text{ (Sect. IIC, line 7)} = \frac{Ci}{m^3}$$

$$9c. \text{ (line 9a)} + \text{ (line 9b)} = \frac{Ci}{m^3}$$

$$10a. \frac{Ci}{sec} \text{ (line 1)} \times \frac{sec}{m^3} \text{ (Sect. IIB, line 8)} = \frac{Ci}{m^3}$$

$$10b. \frac{Ci}{sec} \text{ (line 2)} \times \frac{sec}{m^3} \text{ (Sect. IIC, line 8)} = \frac{Ci}{m^3}$$

$$10c. \text{ (line 10a)} + \text{ (line 10b)} = \frac{Ci}{m^3}$$

$$11. \frac{Ci}{m^3} \text{ (line 3c)} \times \text{ hr}^9 \times 3.8 \times 10^8$$

$$\times \text{ TCFI}^f = \boxed{\phantom{000000}} \text{ mrem at site boundary}$$

$$12. \frac{Ci}{m^3} \text{ (line 4c)} \times \text{ hr}^9 \times 3.8 \times 10^8$$

$$\times \text{ TCFI}^f = \boxed{\phantom{000000}} \text{ mrem at point of max X/Q}$$

$$13. \frac{Ci}{m^3} \text{ (line 5c)} \times \text{ hr}^9 \times 3.8 \times 10^8$$

$$\times \text{ TCFI}^f = \boxed{\phantom{000000}} \text{ mrem at 2 miles}$$

$$14. \frac{Ci}{m^3} \text{ (line 6c)} \times \text{ hr}^9 \times 3.8 \times 10^8$$

$$\times \text{ TCFI}^f = \boxed{\phantom{000000}} \text{ mrem at 5 miles}$$

$$15. \frac{Ci}{m^3} \text{ (line 7c)} \times \text{ hr}^9 \times 3.8 \times 10^8$$

$$\times \text{ TCFI}^f = \boxed{\phantom{000000}} \text{ mrem at 10 miles}$$

## FOLLOW-UP DOSE PROJECTIONS

## ATTACHMENT III, CALCULATION SHEET III (continued)

$$16. \frac{Ci}{m^3} \text{ (line 8c)} \times \text{hr}^9 \times 3.8 \times 10^8$$

$$\times \text{TCFI}^f = \boxed{\phantom{000000}} \text{ mrem at additional location No. 1}$$

$$17. \frac{Ci}{m^3} \text{ (line 9c)} \times \text{hr}^9 \times 3.8 \times 10^8$$

$$\times \text{TCFI}^f = \boxed{\phantom{000000}} \text{ mrem at additional location No. 2}$$

$$18. \frac{Ci}{m^3} \text{ (line 10c)} \times \text{hr}^9 \times 3.8 \times 10^8$$

$$\times \text{TCFI}^f = \boxed{\phantom{000000}} \text{ mrem at additional location No. 3}$$

## NOTES:

<sup>a</sup>Reactor building stack release rate from Summary Table, Section II, line 2.

<sup>b</sup>Turbine building roof exhaust release rate from Summary Table, Section II, line 4.

<sup>c</sup>Offgas stack release rate from Summary Table, Section II, line 3.

<sup>d</sup>Iodine activity fraction for ground level release, obtain from Data Summary Sheet Section IID, line 3a. If unknown use 0.3.

<sup>e</sup>Iodine activity fraction for elevated release-obtain from Data Summary Sheet Section IID, line 3b. If unknown use 0.3 unless Standby Gas Treatment (see Data Summary Sheet, Section II.D, line 1) is in operation then use 0.003.

<sup>f</sup>Obtain TCFI from Figure 9 using time after shutdown (Summary Table, Section I, line 2).

<sup>g</sup>Obtain exposure time from Summary Table, Section II, line 1.

G. Plume width - The following are the plume widths to be placed in the Summary Table, Section III, line 7.

Point of maximum X/Q  
for Offgas Stack release

470  
(0.29)

2mi

3200  
(2.0)

5mi

6200  
(3.9)

10mi

11000 (meters)  
(6.8) (miles)

## NOTE:

Obtain remaining plume widths from Figure 10 using the appropriate distances from Summary Table, Section III, line 1.

## FOLLOW-UP DOSE PROJECTIONS

## ATTACHMENT III, CALCULATION SHEET III (continued)

H. Plume arrival time - Results for Summary Table Section III, line 8.

$$1. \quad 2.78 \times 10^{-4} \times \underline{\hspace{2cm}} \text{ m}^a \div \underline{\hspace{2cm}} \frac{\text{m}^b}{\text{sec}} = \underline{\hspace{2cm}} \text{ hr to Site Boundary}$$

$$2. \quad 0.111 \text{ divided by } \underline{\hspace{2cm}} \frac{\text{m}^b}{\text{sec}} = \underline{\hspace{2cm}} \text{ hr to point of max X/Q for offgas stack release}$$

$$3. \quad 0.894 \text{ divided by } \underline{\hspace{2cm}} \frac{\text{m}^b}{\text{sec}} = \underline{\hspace{2cm}} \text{ hr to 2 miles}$$

$$4. \quad 2.23 \text{ divided by } \underline{\hspace{2cm}} \frac{\text{m}^b}{\text{sec}} = \underline{\hspace{2cm}} \text{ hr to 5 miles}$$

$$5. \quad 4.47 \text{ divided by } \underline{\hspace{2cm}} \frac{\text{m}^b}{\text{sec}} = \underline{\hspace{2cm}} \text{ hr to 10 miles}$$

$$6. \quad 2.78 \times 10^{-4} \times \underline{\hspace{2cm}} \text{ m}^a \div \underline{\hspace{2cm}} \frac{\text{m}^b}{\text{sec}} = \underline{\hspace{2cm}} \text{ hr to additional location No.1}$$

$$7. \quad 2.78 \times 10^{-4} \times \underline{\hspace{2cm}} \text{ m}^a \div \underline{\hspace{2cm}} \frac{\text{m}^b}{\text{sec}} = \underline{\hspace{2cm}} \text{ hr to additional location No.2}$$

$$8. \quad 2.78 \times 10^{-4} \times \underline{\hspace{2cm}} \text{ m}^a \div \underline{\hspace{2cm}} \frac{\text{m}^b}{\text{sec}} = \underline{\hspace{2cm}} \text{ hr to additional location No.3}$$

## NOTES:

<sup>a</sup>Obtain appropriate distance from Summary Table, Section III, line 1.<sup>b</sup>Obtain wind speed from Summary Table, Section I, line 5.

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3b
	Page 29 of 94
FOLLOW-UP DOSE PROJECTIONS	Revision 2
	Date 4/11/83

### ATTACHMENT III, CALCULATION SHEET III (continued)

#### III. Dose information for atmospheric stability class C

##### A. Variable distance and Xu/Q values.

1. Obtain distance to site boundary and Xu/Q for ground level and elevated releases from following table using the down wind direction from Summary Table, Section I, line 4.

Distance \_\_\_\_\_ m  $\frac{X_u}{Q}$  (Ground Level Rel.) \_\_\_\_\_  $\frac{1}{m^2}$

$\frac{X_u}{Q}$  (Elevated Rel.) \_\_\_\_\_  $\frac{1}{m^2}$

Down Wind Direction deg.	Distance to Site Bdy, meters	$\frac{X_u}{Q}, \frac{1}{m^2}$	
		Ground Level Rel.	Elevated Rel.
0 - 11.25	1200	$3.2 \times 10^{-5}$	$1.3 \times 10^{-5}$
11.25 - 33.75	1600	$2.0 \times 10^{-5}$	$1.1 \times 10^{-5}$
33.75 - 56.25	700	$8.2 \times 10^{-5}$	$7.5 \times 10^{-6}$
56.25 - 78.75	610	$1.0 \times 10^{-4}$	$5.0 \times 10^{-6}$
78.75 - 101.25	490	$1.5 \times 10^{-4}$	$2.0 \times 10^{-6}$
101.25 - 123.75	450	$1.8 \times 10^{-4}$	$1.2 \times 10^{-6}$
123.75 - 146.25	480	$1.5 \times 10^{-4}$	$1.8 \times 10^{-6}$
146.25 - 168.75	500	$1.4 \times 10^{-4}$	$2.4 \times 10^{-6}$
168.75 - 191.25	460	$1.7 \times 10^{-4}$	$1.4 \times 10^{-6}$
191.25 - 213.75	500	$1.4 \times 10^{-4}$	$2.4 \times 10^{-6}$
213.75 - 236.25	630	$1.0 \times 10^{-4}$	$5.4 \times 10^{-6}$
236.25 - 258.75	720	$7.8 \times 10^{-5}$	$7.6 \times 10^{-6}$
258.75 - 281.25	670	$8.8 \times 10^{-5}$	$6.7 \times 10^{-6}$
281.25 - 303.75	730	$7.8 \times 10^{-5}$	$7.8 \times 10^{-6}$
303.75 - 326.25	980	$4.6 \times 10^{-5}$	$1.2 \times 10^{-5}$
326.25 - 348.75	1300	$2.8 \times 10^{-5}$	$1.2 \times 10^{-5}$
348.75 - 360.00	1200	$3.2 \times 10^{-5}$	$1.3 \times 10^{-5}$

2. Distance to point of maximum  $\frac{X_u}{Q}$  for offgas stack release = 1200m.

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3b
	Page 30 of 94
FOLLOW-UP DOSE PROJECTIONS	Revision 2
	Date 4/11/83

### ATTACHMENT III, CALCULATION SHEET III (continued)

B. Normalized concentration, Ground level release - Results for Summary Table, Section III, line 2.

$$1. \quad \frac{1^a}{m^2} \div \text{m/sec}^b = \boxed{\phantom{000}} \frac{\text{sec}}{m^3} \text{ at site boundary}$$

$$2. \quad 3.2 \times 10^{-5} \div \text{m/sec}^b = \boxed{\phantom{000}} \frac{\text{sec}}{m^3} \text{ at point of max X/Q for offgas release}$$

$$3. \quad 6.0 \times 10^{-6} \div \text{m/sec}^b = \boxed{\phantom{000}} \frac{\text{sec}}{m^3} \text{ at 2 miles}$$

$$4. \quad 1.2 \times 10^{-6} \div \text{m/sec}^b = \boxed{\phantom{000}} \frac{\text{sec}}{m^3} \text{ at 5 miles}$$

$$5. \quad 3.7 \times 10^{-7} \div \text{m/sec}^b = \boxed{\phantom{000}} \frac{\text{sec}}{m^3} \text{ at 10 miles}$$

$$6. \quad \frac{1^c}{m^2} \div \text{m/sec}^b = \boxed{\phantom{000}} \frac{\text{sec}}{m^3} \text{ at additional location No. 1}$$

$$7. \quad \frac{1^c}{m^2} \div \text{m/sec}^b = \boxed{\phantom{000}} \frac{\text{sec}}{m^3} \text{ at additional location No. 2}$$

$$8. \quad \frac{1^c}{m^2} \div \text{m/sec}^b = \boxed{\phantom{000}} \frac{\text{sec}}{m^3} \text{ at additional location No. 3}$$

NOTE:

<sup>a</sup>Obtain  $\frac{X_u}{Q}$  for ground level release from Section III, Subsection A, line 1.

<sup>b</sup>Obtain wind speed from Summary Table Section 1, line 5.

<sup>c</sup>Obtain ground level release  $\frac{X_u}{Q}$  for additional locations using Figure 11 and appropriate distance from Summary Table, Section III, line 1.

## ATTACHMENT III, CALCULATION SHEET III (continued)

C. Normalized concentration, Elevated release - Results for Summary Table, Section III, line 3.

$$1. \quad \frac{1^a}{m^2} \div \text{m/sec}^b = \boxed{\phantom{000}} \frac{\text{sec}}{m^3} \text{ at site boundary}$$

$$2. \quad 3.3 \times 10^{-5} \div \text{m/sec}^b = \boxed{\phantom{000}} \frac{\text{sec}}{m^3} \text{ at point of max X/Q for offgas stack release}$$

$$3. \quad 5.1 \times 10^{-6} \div \text{m/sec}^b = \boxed{\phantom{000}} \frac{\text{sec}}{m^3} \text{ at 2 miles}$$

$$4. \quad 1.2 \times 10^{-6} \div \text{m/sec}^b = \boxed{\phantom{000}} \frac{\text{sec}}{m^3} \text{ at 5 miles}$$

$$5. \quad 3.7 \times 10^{-7} \div \text{m/sec}^b = \boxed{\phantom{000}} \frac{\text{sec}}{m^3} \text{ at 10 miles}$$

$$6. \quad \frac{1^c}{m^2} \div \text{m/sec}^b = \boxed{\phantom{000}} \frac{\text{sec}}{m^3} \text{ at additional location No. 1}$$

$$7. \quad \frac{1^c}{m^2} \div \text{m/sec}^b = \boxed{\phantom{000}} \frac{\text{sec}}{m^3} \text{ at additional location No. 2}$$

$$8. \quad \frac{1^c}{m^2} \div \text{m/sec}^b = \boxed{\phantom{000}} \frac{\text{sec}}{m^3} \text{ at additional location No. 3}$$

## NOTE:

<sup>a</sup>Obtain  $\frac{X_u}{Q}$  for elevated release from Section III, Subsection A, line 4.

<sup>b</sup>Obtain wind speed from Summary Table, Section I, line 5.

<sup>c</sup>Obtain elevated release  $\frac{X_u}{Q}$  for additional locations using Figure 12 and appropriate distances from Summary Table, Section III, line 1.

D. Whole body dose rate - Results for Summary Table, Section III, line 4.

$$1. \quad \frac{C_i^a}{\text{sec}} \div \frac{C_i^b}{\text{sec}} = \frac{C_i}{\text{sec}}$$

$$2a. \quad \text{FIM} \times \text{DFI}^d =$$

$$2b. \quad (1 - \text{FIM}) \times \text{DFNG}^e =$$

$$2c. \quad (\text{line 2a}) + (\text{line 2b}) =$$

## FOLLOW-UP DOSE PROJECTIONS

## ATTACHMENT III, CALCULATION SHEET III (continued)

3.  $\frac{Du}{Q}$  for site boundary:

3a. \_\_\_\_\_ FIC x \_\_\_\_\_ DUOQIf x \_\_\_\_\_ TCFI9 = \_\_\_\_\_

3b. (1 - \_\_\_\_\_ FIC) x \_\_\_\_\_ DUOQNGh x \_\_\_\_\_ TCFNGi = \_\_\_\_\_

3c. \_\_\_\_\_ (line 3a) + \_\_\_\_\_ (line 3b) = \_\_\_\_\_

4.  $\frac{Du}{Q}$  for location of maximum  $\frac{Xu}{Q}$  for offgas stack release:

4a. \_\_\_\_\_ FIC x 12.0 x \_\_\_\_\_ TCFI9 = \_\_\_\_\_

4b. (1 - \_\_\_\_\_ FIC) x 8.50 x \_\_\_\_\_ TCFNGi = \_\_\_\_\_

4c. \_\_\_\_\_ (line 4a) + \_\_\_\_\_ (line 4b) = \_\_\_\_\_

5.  $\frac{Du}{Q}$  for 2 miles:

5a. \_\_\_\_\_ FIC x 8.30 x \_\_\_\_\_ TCFI9 = \_\_\_\_\_

5b. (1 - \_\_\_\_\_ FIC) x 5.90 x \_\_\_\_\_ TCFNGi = \_\_\_\_\_

5c. \_\_\_\_\_ (line 5a) + \_\_\_\_\_ (line 5b) = \_\_\_\_\_

6.  $\frac{Du}{Q}$  for 5 miles

6a. \_\_\_\_\_ FIC x 1.85 x \_\_\_\_\_ TCFI9 = \_\_\_\_\_

6b. (1 - \_\_\_\_\_ FIC) x 1.30 x \_\_\_\_\_ TCFNGi = \_\_\_\_\_

6c. \_\_\_\_\_ (line 6a) + \_\_\_\_\_ (line 6b) = \_\_\_\_\_

7.  $\frac{Du}{Q}$  for 10 miles

7a. \_\_\_\_\_ FIC x 0.440x \_\_\_\_\_ TCFI9 = \_\_\_\_\_

7b. (1 - \_\_\_\_\_ FIC) x 0.320 x \_\_\_\_\_ TCFNGi = \_\_\_\_\_

7c. \_\_\_\_\_ (line 7a) + \_\_\_\_\_ (line 7b) = \_\_\_\_\_

## FOLLOW-UP DOSE PROJECTIONS

## ATTACHMENT III, CALCULATION SHEET III (continued)

8.  $\frac{Du}{Q}$  for additional location No. 1:

$$8a. \text{_____} FIC \times \text{_____} DUOQI^f \times \text{_____} TCFI^9 = \text{_____}$$

$$8b. (1 - \text{_____} FIC) \times \text{_____} DUOQNG^h \times \text{_____} TCFNG^i = \text{_____}$$

$$8c. \text{_____} (\text{line } 8a) + \text{_____} (\text{line } 8b) = \text{_____}$$

9.  $\frac{Du}{Q}$  for additional location No. 2:

$$9a. \text{_____} FIC \times \text{_____} DUOQI^f \times \text{_____} TCFI^9 = \text{_____}$$

$$9b. (1 - \text{_____} FIC) \times \text{_____} DUOQNG^h \times \text{_____} TCFNG^i = \text{_____}$$

$$9c. \text{_____} (\text{line } 9a) + \text{_____} (\text{line } 9b) = \text{_____}$$

10.  $\frac{Du}{Q}$  for additional location No. 3:

$$10a. \text{_____} FIC \times \text{_____} DUOQI^f \times \text{_____} TCFI^9 = \text{_____}$$

$$10b. (1 - \text{_____} FIC) \times \text{_____} DUOQNG^h \times \text{_____} TCFNG^i = \text{_____}$$

$$10c. \text{_____} (\text{line } 10a) + \text{_____} (\text{line } 10b) = \text{_____}$$

$$11a. \text{_____} \frac{Ci}{\text{sec}} (\text{line } 1) \times \text{_____} \frac{\text{sec}^j}{m^3} \times \text{_____} (\text{line } 2) = \text{_____}$$

$$11b. \text{_____} \frac{Cik}{\text{sec}} \times \text{_____} \frac{Du}{Q} (\text{line } 3c) + \text{_____} \frac{m^1}{\text{sec}} = \text{_____}$$

$$11c. \text{_____} (\text{line } 11a) + \text{_____} (\text{line } 11b)$$

$$= \boxed{\text{_____}} \frac{mrem}{hr} \text{ at site boundary}$$

$$12a. \text{_____} \frac{Ci}{\text{sec}} (\text{line } 1) \times \text{_____} \frac{\text{sec}^j}{m^3} \times \text{_____} (\text{line } 2) = \text{_____}$$

$$12b. \text{_____} \frac{Cik}{\text{sec}} \times \text{_____} \frac{Du}{Q} (\text{line } 4c) + \text{_____} \frac{m^1}{\text{sec}} = \text{_____}$$

$$12c. \text{_____} (\text{line } 12a) + \text{_____} (\text{line } 12b)$$

$$= \boxed{\text{_____}} \frac{mrem}{hr} \text{ at point of max } \frac{Xu}{Q}$$

## FOLLOW-UP DOSE PROJECTIONS

## ATTACHMENT III, CALCULATION SHEET III (continued)

$$13a. \frac{Ci}{sec} (line 1) \times \frac{sec^j}{m^3} \times (line 2) =$$

$$13b. \frac{Cik}{sec} \times \frac{Du}{Q} (line 5c) + \frac{m^1}{sec} =$$

$$13c. (line 13a) + (line 13b)$$

$$= \boxed{\phantom{000000}} \frac{mrem}{hr} \text{ at 2 miles}$$

$$14a. \frac{Ci}{sec} (line 1) \times \frac{sec^j}{m^3} \times (line 2) =$$

$$14b. \frac{Cik}{sec} \times \frac{Du}{Q} (line 6) + \frac{m^1}{sec} =$$

$$14c. (line 14a) + (line 14b)$$

$$= \boxed{\phantom{000000}} \frac{mrem}{hr} \text{ at 5 miles}$$

$$15a. \frac{Ci}{sec} (line 1) \times \frac{sec^j}{m^3} \times (line 2) =$$

$$15b. \frac{Cik}{sec} \times \frac{Du}{Q} (line 7c) + \frac{m^1}{sec} =$$

$$15c. (line 15a) + (line 15b)$$

$$= \boxed{\phantom{000000}} \frac{mrem}{hr} \text{ at 10 miles}$$

$$16a. \frac{Ci}{sec} (line 1) \times \frac{sec^j}{m^3} \times (line 2) =$$

$$16b. \frac{Cik}{sec} \times \frac{Du}{Q} (line 8c) + \frac{m^1}{sec} =$$

$$16c. (line 16a) + (line 16b)$$

$$= \boxed{\phantom{000000}} \frac{mrem}{hr} \text{ at additional location No. 1}$$

$$17a. \frac{Ci}{sec} (line 1) \times \frac{sec^j}{m^3} \times (line 2) =$$

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3b
	Page 35 of 94
FOLLOW-UP DOSE PROJECTIONS	Revision 2
	Date 4/11/83

ATTACHMENT III, CALCULATION SHEET III (continued)

$$17b. \frac{Ci^k}{\text{sec}} \times \frac{Du}{Q} (\text{line } 9c) + \frac{m^1}{\text{sec}} =$$

$$17c. (\text{line } 17a) + (\text{line } 17b) =$$

$$= \frac{\text{mrem}}{\text{hr}} \text{ at additional location No. 2}$$

$$18a. \frac{Ci}{\text{sec}} (\text{line } 1) \times \frac{\text{sec}^j}{m^3} \times (\text{line } 2) =$$

$$18b. \frac{Ci^k}{\text{sec}} \times \frac{Du}{Q} (\text{line } 10c) + \frac{m^1}{\text{sec}} =$$

$$18c. (\text{line } 18a) + (\text{line } 18b)$$

$$= \frac{\text{mrem}}{\text{hr}} \text{ at additional location No. 3}$$

NOTES:

<sup>a</sup>Reactor building stack release rate from Summary Table, Section II, line 2.

<sup>b</sup>Turbine building roof exhaust release rate from Summary Table, Section II, line 4.

<sup>c</sup>Iodine activity to noble gas activity ratio-obtain from Data Summary Sheet Section IID, line 3b. If unknown use 0.3 unless Standby Gas Treatment is in operation (See Data Summary Sheet, Section II.D, line 1) then use 0.003.

<sup>d</sup>Obtain iodine dose factor (DFI) for time after shutdown (Summary Table, Section I, line 2) from Figure 3.

<sup>e</sup>Obtain noble gas dose factor (DFNG) for time after shutdown (Summary Table, Section I, line 2) from Figure 4.

<sup>f</sup>Obtain  $\frac{Du}{Q}$  for iodine (DUOQI) from Figure 13 using the appropriate distance from Summary Table, Section III, line 1.

<sup>g</sup>Obtain time correction factor for iodine (TCFI) from Figure 6 using time after shutdown (Summary Table, Section I, line 2).

<sup>h</sup>Obtain  $\frac{Du}{Q}$  for noble gas (DUOQNG) from Figure 14 using the appropriate distance from Summary Table, Section III, line 1.

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3b
FOLLOW-UP DOSE PROJECTIONS	Page 36 of 94
	Revision 2
	Date 4/11/83

### ATTACHMENT III, CALCULATION SHEET III (continued)

<sup>i</sup> Obtain the noble gas time correction factor (TCFNG) from Figure 8 using time after shutdown (Summary Table, Section I, line 2).

<sup>j</sup> Obtain appropriate  $\frac{X}{Q}$  for ground level release from Summary Table, Section III, line 2.

<sup>k</sup> Obtain offgas stack release rate from Summary Table, Section II, line 3.

<sup>l</sup> Obtain wind speed from Summary Table, Section I, line 5.

<sup>m</sup> Iodine activity to noble gas activity ratio - obtain from Data Summary Sheet, Section IID, line 3a. If unknown use 0.3.

E. Whole body dose - Results for Summary Table Section III, line 5.

1.  $\frac{\text{mrem}}{\text{hr}}$  (from Section IIID, line 11C) x  $\text{hr}^a$   
 =  mrem at site boundary

2.  $\frac{\text{mrem}}{\text{hr}}$  (from Section IIID, line 12C) x  $\text{hr}^a$   
 =  mrem at point of max X/Q for offgas stack release

3.  $\frac{\text{mrem}}{\text{hr}}$  (from Section IIID, line 13C) x  $\text{hr}^a$   
 =  mrem at 2 miles

4.  $\frac{\text{mrem}}{\text{hr}}$  (from Section IIID, line 14C) x  $\text{hr}^a$   
 =  mrem at 5 miles

5.  $\frac{\text{mrem}}{\text{hr}}$  (from Section IIID, line 15C) x  $\text{hr}^a$   
 =  mrem at 10 miles

6.  $\frac{\text{mrem}}{\text{hr}}$  (from Section IIID, line 16C) x  $\text{hr}^a$   
 =  mrem at additional location No. 1

## FOLLOW-UP DOSE PROJECTIONS

## ATTACHMENT III, CALCULATION SHEET III (continued)

$$7. \frac{\text{mrem}}{\text{hr}} \text{ (from Section IIID, line 17C) } \times \text{hr}^a = \boxed{\phantom{000000}} \text{ mrem at additional location No. 2}$$

$$8. \frac{\text{mrem}}{\text{hr}} \text{ (from Section IIID, line 18C) } \times \text{hr}^a = \boxed{\phantom{000000}} \text{ mrem at additional location No. 3}$$

## NOTE:

<sup>a</sup>Obtain exposure time from Summary Table, Section II, line 1.

F. Thyroid Dose Commitment - Result for Summary Table, Section III, line 6.

$$1. \left( \frac{\text{Ci}^a}{\text{sec}} + \frac{\text{Ci}^b}{\text{sec}} \right) \times \text{FIG}^d = \frac{\text{Ci}}{\text{sec}}$$

$$2. \frac{\text{Ci}^c}{\text{sec}} \times \text{FIE}^e = \frac{\text{Ci}}{\text{sec}}$$

$$3a. \frac{\text{Ci}}{\text{sec}} \text{ (line 1) } \times \frac{\text{sec}}{\text{m}^3} \text{ (Sect. IIIB, line 1) } = \frac{\text{Ci}}{\text{m}^3}$$

$$3b. \frac{\text{Ci}}{\text{sec}} \text{ (line 2) } \times \frac{\text{sec}}{\text{m}^3} \text{ (Sect. IIIC, line 1) } = \frac{\text{Ci}}{\text{m}^3}$$

$$3c. \text{ (line 3a) } + \text{ (line 3b) } = \frac{\text{Ci}}{\text{m}^3}$$

$$4a. \frac{\text{Ci}}{\text{sec}} \text{ (line 1) } \times \frac{\text{sec}}{\text{m}^3} \text{ (Sect. IIIB, line 2) } = \frac{\text{Ci}}{\text{m}^3}$$

$$4b. \frac{\text{Ci}}{\text{sec}} \text{ (line 2) } \times \frac{\text{sec}}{\text{m}^3} \text{ (Sect. IIIC, line 2) } = \frac{\text{Ci}}{\text{m}^3}$$

$$4c. \text{ (line 4a) } + \text{ (line 4b) } = \frac{\text{Ci}}{\text{m}^3}$$

$$5a. \frac{\text{Ci}}{\text{sec}} \text{ (line 1) } \times \frac{\text{sec}}{\text{m}^3} \text{ (Sect. IIIB, line 3) } = \frac{\text{Ci}}{\text{m}^3}$$

$$5b. \frac{\text{Ci}}{\text{sec}} \text{ (line 2) } \times \frac{\text{sec}}{\text{m}^3} \text{ (Sect. IIIC, line 3) } = \frac{\text{Ci}}{\text{m}^3}$$

$$5c. \text{ (line 5a) } + \text{ (line 5b) } = \frac{\text{Ci}}{\text{m}^3}$$

## FOLLOW-UP DOSE PROJECTIONS

## ATTACHMENT III, CALCULATION SHEET III (continued)

$$6a. \frac{Ci}{sec} (line 1) \times \frac{sec}{m^3} (Sect. IIIB, line 4) = \frac{Ci}{m^3}$$

$$6b. \frac{Ci}{sec} (line 2) \times \frac{sec}{m^3} (Sect. IIIC, line 4) = \frac{Ci}{m^3}$$

$$6c. (line 6a) + (line 6b) = \frac{Ci}{m^3}$$

$$7a. \frac{Ci}{sec} (line 1) \times \frac{sec}{m^3} (Sect. IIIB, line 5) = \frac{Ci}{m^3}$$

$$7b. \frac{Ci}{sec} (line 2) \times \frac{sec}{m^3} (Sect. IIIC, line 5) = \frac{Ci}{m^3}$$

$$7c. (line 7a) + (line 7b) = \frac{Ci}{m^3}$$

$$8a. \frac{Ci}{sec} (line 1) \times \frac{sec}{m^3} (Sect. IIIB, line 6) = \frac{Ci}{m^3}$$

$$8b. \frac{Ci}{sec} (line 2) \times \frac{sec}{m^3} (Sect. IIIC, line 6) = \frac{Ci}{m^3}$$

$$8c. (line 8a) + (line 8b) = \frac{Ci}{m^3}$$

$$9a. \frac{Ci}{sec} (line 1) \times \frac{sec}{m^3} (Sect. IIIB, line 7) = \frac{Ci}{m^3}$$

$$9b. \frac{Ci}{sec} (line 2) \times \frac{sec}{m^3} (Sect. IIIC, line 7) = \frac{Ci}{m^3}$$

$$9c. (line 9a) + (line 9b) = \frac{Ci}{m^3}$$

$$10a. \frac{Ci}{sec} (line 1) \times \frac{sec}{m^3} (Sect. IIIB, line 8) = \frac{Ci}{m^3}$$

$$10b. \frac{Ci}{sec} (line 2) \times \frac{sec}{m^3} (Sect. IIIC, line 8) = \frac{Ci}{m^3}$$

$$10c. (line 10a) + (line 10b) = \frac{Ci}{m^3}$$

$$11. \frac{Ci}{m^3} (line 3c) \times \text{hr}^9 \times 3.8 \times 10^8$$

$$\times \text{TCFI}^f = \boxed{\phantom{000000}} \text{ mrem at site boundary}$$

$$12. \frac{Ci}{m^3} (line 4c) \times \text{hr}^9 \times 3.8 \times 10^8$$

$$\times \text{TCFI}^f = \boxed{\phantom{000000}} \text{ mrem at point of max X/Q}$$

## FOLLOW-UP DOSE PROJECTIONS

## ATTACHMENT III, CALCULATION SHEET III (continued)

13.  $\frac{Ci}{m^3}$  (line 5c) x  $hr^9 \times 3.8 \times 10^8$   
x  $TCFI^f$  =  mrem at 2 miles

14.  $\frac{Ci}{m^3}$  (line 6c) x  $hr^9 \times 3.8 \times 10^8$   
x  $TCFI^f$  =  mrem at 5 miles

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3b
	Page 40 of 94
FOLLOW-UP DOSE PROJECTIONS	Revision 2
	Date 4/11/83

ATTACHMENT III, CALCULATION SHEET III (continued)

15.  $\frac{Ci}{m^3}$  (line 7c) x  $hr^a$  x  $3.8 \times 10^8$   
x  $TCFI^f$  =  mrem at 10 miles
16.  $\frac{Ci}{m^3}$  (line 8c) x  $hr^a$  x  $3.8 \times 10^8$   
x  $TCFI^f$  =  mrem at additional location No. 1
17.  $\frac{Ci}{m^3}$  (line 9c) x  $hr^a$  x  $3.8 \times 10^8$   
x  $TCFI^f$  =  mrem at additional location No. 2
18.  $\frac{Ci}{m^3}$  (line 10c) x  $hr^a$  x  $3.8 \times 10^8$   
x  $TCFI^f$  =  mrem at additional location No. 3

NOTES:

<sup>a</sup>Reactor building stack release rate from Summary Table, Section II, line 2.

<sup>b</sup>Turbine building roof exhaust release rate from Summary Table, Section II, line 4.

<sup>c</sup>Offgas stack release rate from Summary Table, Section II, line 3.

<sup>d</sup>Iodine activity fraction for ground level release, - obtain from Data Summary Sheet Section IID, line 3a. If unknown use 0.3.

<sup>e</sup>Iodine activity fraction for elevated release - obtain from Data Summary Sheet Section IID, line 3b. If unknown use 0.3 unless Standby Gas Treatment (see Data Summary Sheet, Section II.D, line 1) is in operation then use 0.003.

<sup>f</sup>Obtain TCFI from Figure 9 using time after shutdown (Summary Table, Section I, line 2).

<sup>g</sup>Obtain exposure time from Summary Table, Section II, line 1.

## FOLLOW-UP DOSE PROJECTIONS

## ATTACHMENT III, CALCULATION SHEET III (continued)

- G. Plume width - The following are the plume widths to be placed in the Summary Table, Section III, line 7.

Point of maximum X/Q  
for Offgas Stack release

2mi

5mi

10mi

720 meters  
(0.45)

1900  
(1.2)

2700  
(1.7)

6600 (meters)  
(4.1)(miles)

## NOTE:

Obtain remaining plume widths from Figure 15 using the appropriate distances from Summary Table, Section III, line 1.

- H. Plume arrival time - Results for Summary Table Section III, line 8.

$$1. \quad 2.78 \times 10^{-4} \times \underline{\hspace{2cm}} m^a + \frac{m^b}{\text{Sec}} = \boxed{\hspace{1cm}} \text{ hr to Site Boundary}$$

$$2. \quad 0.333 \text{ divided by } \underline{\hspace{2cm}} \frac{m^b}{\text{Sec}} = \boxed{\hspace{1cm}} \text{ hr to point of max X/Q for offgas stack release}$$

$$3. \quad 0.894 \text{ divided by } \underline{\hspace{2cm}} \frac{m^b}{\text{Sec}} = \boxed{\hspace{1cm}} \text{ hr to 2 miles}$$

$$4. \quad 2.23 \text{ divided by } \underline{\hspace{2cm}} \frac{m^b}{\text{Sec}} = \boxed{\hspace{1cm}} \text{ hr to 5 miles}$$

$$5. \quad 4.47 \text{ divided by } \underline{\hspace{2cm}} \frac{m^b}{\text{Sec}} = \boxed{\hspace{1cm}} \text{ hr to 10 miles}$$

$$6. \quad 2.78 \times 10^{-4} \times \underline{\hspace{2cm}} m^a + \frac{m^b}{\text{Sec}} = \boxed{\hspace{1cm}} \text{ hr to additional location No. 1}$$

$$7. \quad 2.78 \times 10^{-4} \times \underline{\hspace{2cm}} m^a + \frac{m^b}{\text{Sec}} = \boxed{\hspace{1cm}} \text{ hr to additional location No. 2}$$

$$8. \quad 2.78 \times 10^{-4} \times \underline{\hspace{2cm}} m^a + \frac{m^b}{\text{Sec}} = \boxed{\hspace{1cm}} \text{ hr to additional location No. 3}$$

## NOTES:

<sup>a</sup>Obtain appropriate distance from Summary Table, Section III, line 1.

<sup>b</sup>Obtain wind speed from Summary Table, Section I, line 5.

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3b
FOLLOW-UP DOSE PROJECTIONS	Page 42 of 94
	Revision 2
	Date 4/11/83

ATTACHMENT III, CALCULATION SHEET III (continued)

IV. Dose information for atmospheric stability class DE

A. Variable distance and  $X_u/Q$  values.

1. Obtain distance to site boundary and  $X_u/Q$  for ground level and elevated releases from following table using the down wind direction from Summary Table, Section I, line 4.

Distance \_\_\_\_\_ m  $\frac{X_u}{Q}$  (Ground Level Rel.) \_\_\_\_\_  $\frac{1}{m^2}$

$\frac{X_u}{Q}$  (Elevated Rel.) \_\_\_\_\_  $\frac{1}{m^2}$

Down Wind Direction deg.	Distance to Site Bdy, meters	$\frac{X_u}{Q}$ , $\frac{1}{m^2}$ Ground Level Rel.	Elevated Rel.
0 - 11.25	1200	$1.5 \times 10^{-4}$	$3.4 \times 10^{-7}$
11.25 - 33.75	1600	$9.5 \times 10^{-5}$	$1.6 \times 10^{-6}$
33.75 - 56.25	700	$3.5 \times 10^{-4}$	$1.8 \times 10^{-9}$
56.25 - 78.75	610	$4.4 \times 10^{-4}$	$8.0 \times 10^{-10}$
78.75 - 101.25	490	$6.1 \times 10^{-4}$	$2.1 \times 10^{-10}$
101.25 - 123.75	450	$7.3 \times 10^{-4}$	$1.6 \times 10^{-11}$
123.75 - 146.25	480	$6.4 \times 10^{-4}$	$1.6 \times 10^{-10}$
146.25 - 168.75	500	$6.0 \times 10^{-4}$	$2.6 \times 10^{-10}$
168.75 - 191.25	460	$6.9 \times 10^{-4}$	$6.5 \times 10^{-11}$
191.25 - 213.75	500	$6.0 \times 10^{-4}$	$2.6 \times 10^{-10}$
213.75 - 236.25	630	$4.3 \times 10^{-4}$	$9.0 \times 10^{-10}$
236.25 - 258.75	720	$3.4 \times 10^{-4}$	$2.6 \times 10^{-9}$
258.75 - 281.25	670	$3.7 \times 10^{-4}$	$1.2 \times 10^{-9}$
281.25 - 303.75	730	$3.3 \times 10^{-4}$	$3.0 \times 10^{-9}$
303.75 - 326.25	980	$2.1 \times 10^{-4}$	$6.8 \times 10^{-8}$
326.25 - 348.75	1300	$1.3 \times 10^{-4}$	$6.0 \times 10^{-7}$
348.75 - 360.00	1200	$1.5 \times 10^{-4}$	$3.4 \times 10^{-7}$

2. Distance to point of maximum  $\frac{X_u}{Q}$  for offgas stack release = 4000m.

## FOLLOW-UP DOSE PROJECTIONS

## ATTACHMENT III, CALCULATION SHEET III (continued)

B. Normalized concentration, Ground level release - Results for Summary Table, Section III, line 2.

$$1. \frac{1a}{m^2} \div \text{m/sec}^b = \frac{\text{sec}}{m^3} \text{ at site boundary}$$

$$2. 2.2 \times 10^{-5} \div \text{m/sec}^b = \frac{\text{sec}}{m^3} \text{ at point of max X/Q for offgas release}$$

$$3. 3.1 \times 10^{-6} \div \text{m/sec}^b = \frac{\text{sec}}{m^3} \text{ at 2 miles}$$

$$4. 7.2 \times 10^{-6} \div \text{m/sec}^b = \frac{\text{sec}}{m^3} \text{ at 5 miles}$$

$$5. 2.4 \times 10^{-7} \div \text{m/sec}^b = \frac{\text{sec}}{m^3} \text{ at 10 miles}$$

$$6. \frac{1c}{m^2} \div \text{m/sec}^b = \frac{\text{sec}}{m^3} \text{ at additional location No. 1}$$

$$7. \frac{1c}{m^2} \div \text{m/sec}^b = \frac{\text{sec}}{m^3} \text{ at additional location No. 2}$$

$$8. \frac{1c}{m^2} \div \text{m/sec}^b = \frac{\text{sec}}{m^3} \text{ at additional location No. 3}$$

## NOTE:

<sup>a</sup>Obtain  $\frac{Xu}{Q}$  for ground level release from Section IV, Subsection A, line 1.

<sup>b</sup>Obtain wind speed from Summary Table Section I, line 5.

<sup>c</sup>Obtain ground level release  $\frac{Xu}{Q}$  for additional locations using Figure 16 and appropriate distance from Summary Table, Section III, line 1.

C. Normalized concentration, Elevated release - Results for Summary Table, Section III, line 3.

$$1. \frac{1a}{m^2} \div \text{m/sec}^b = \frac{\text{sec}}{m^3} \text{ at site boundary}$$

## FOLLOW-UP DOSE PROJECTIONS

## ATTACHMENT III, CALCULATION SHEET III (continued)

$$2. \quad 7.0 \times 10^{-6} \div \underline{\hspace{2cm}} \text{ m/sec}^b = \underline{\hspace{2cm}} \frac{\text{sec}}{\text{m}^3} \text{ at point of max X/Q for offgas stack release}$$

$$3. \quad 6.6 \times 10^{-6} \div \underline{\hspace{2cm}} \text{ m/sec}^b = \underline{\hspace{2cm}} \frac{\text{sec}}{\text{m}^3} \text{ at 2 miles}$$

$$4. \quad 4.7 \times 10^{-6} \div \underline{\hspace{2cm}} \text{ m/sec}^b = \underline{\hspace{2cm}} \frac{\text{sec}}{\text{m}^3} \text{ at 5 miles}$$

$$5. \quad 2.0 \times 10^{-6} \div \underline{\hspace{2cm}} \text{ m/sec}^b = \underline{\hspace{2cm}} \frac{\text{sec}}{\text{m}^3} \text{ at 10 miles}$$

$$6. \quad \underline{\hspace{2cm}} \frac{1^c}{\text{m}^2} \div \underline{\hspace{2cm}} \text{ m/sec}^b = \underline{\hspace{2cm}} \frac{\text{sec}}{\text{m}^3} \text{ at additional location No. 1}$$

$$7. \quad \underline{\hspace{2cm}} \frac{1^c}{\text{m}^2} \div \underline{\hspace{2cm}} \text{ m/sec}^b = \underline{\hspace{2cm}} \frac{\text{sec}}{\text{m}^3} \text{ at additional location No. 2}$$

$$8. \quad \underline{\hspace{2cm}} \frac{1^c}{\text{m}^2} \div \underline{\hspace{2cm}} \text{ m/sec}^b = \underline{\hspace{2cm}} \frac{\text{sec}}{\text{m}^3} \text{ at additional location No. 3}$$

NOTE:

<sup>a</sup>Obtain  $\frac{X_u}{Q}$  for elevated release from Section IV, Subsection A, line 1.

<sup>b</sup>Obtain wind speed from Summary Table, Section I, line 5.

<sup>c</sup>Obtain elevated release  $\frac{X_u}{Q}$  for additional locations using Figure 17 and appropriate distances from Summary Table, Section III, line 1.

D. Whole body dose rate - Results for Summary Table, Section III, line 4.

$$1. \quad \underline{\hspace{2cm}} \frac{C_{ia}}{\text{sec}} + \underline{\hspace{2cm}} \frac{C_{ib}}{\text{sec}} = \underline{\hspace{2cm}} \frac{C_i}{\text{sec}}$$

$$2a. \quad \underline{\hspace{2cm}} \text{ FIM} \times \underline{\hspace{2cm}} \text{ DFID} = \underline{\hspace{2cm}}$$

$$2b. \quad (1 - \underline{\hspace{2cm}} \text{ FIM} \times \underline{\hspace{2cm}} \text{ DFNG}^e = \underline{\hspace{2cm}})$$

$$2c. \quad \underline{\hspace{2cm}} (\text{line 2a}) + \underline{\hspace{2cm}} (\text{line 2b}) = \underline{\hspace{2cm}}$$

## ATTACHMENT III, CALCULATION SHEET III (continued)

3.  $\frac{Du}{Q}$  for site boundary:

3a. \_\_\_\_\_ FIC x \_\_\_\_\_ DUOQI<sup>f</sup> x \_\_\_\_\_ TCFI<sup>g</sup> = \_\_\_\_\_

3b. (1 - \_\_\_\_\_ FIC) x \_\_\_\_\_ DUOQNG<sup>h</sup> x \_\_\_\_\_ TCFNG<sup>i</sup> = \_\_\_\_\_

3c. \_\_\_\_\_ (line 3a) + \_\_\_\_\_ (line 3b) = \_\_\_\_\_

4.  $\frac{Du}{Q}$  for location of maximum  $\frac{Xu}{Q}$  for offgas stack release:

4a. \_\_\_\_\_ FIC x 11.0 x \_\_\_\_\_ TCFI<sup>g</sup> = \_\_\_\_\_

4b. (1 - \_\_\_\_\_ FIC) x 7.2 x \_\_\_\_\_ TCFNG<sup>i</sup> = \_\_\_\_\_

4c. \_\_\_\_\_ (line 4a) + \_\_\_\_\_ (line 4b) = \_\_\_\_\_

5.  $\frac{Du}{Q}$  for 2 miles:

5a. \_\_\_\_\_ FIC x 11.1 x \_\_\_\_\_ TCFI<sup>g</sup> = \_\_\_\_\_

5b. (1 - \_\_\_\_\_ FIC) x 8.0 x \_\_\_\_\_ TCFNG<sup>i</sup> = \_\_\_\_\_

5c. \_\_\_\_\_ (line 5a) + \_\_\_\_\_ (line 5b) = \_\_\_\_\_

6.  $\frac{Du}{Q}$  for 5 miles

6a. \_\_\_\_\_ FIC x 7.4 x \_\_\_\_\_ TCFI<sup>g</sup> = \_\_\_\_\_

6b. (1 - \_\_\_\_\_ FIC) x 4.1 x \_\_\_\_\_ TCFNG<sup>i</sup> = \_\_\_\_\_

6c. \_\_\_\_\_ (line 6a) + \_\_\_\_\_ (line 6b) = \_\_\_\_\_

7.  $\frac{Du}{Q}$  for 10 miles

7a. \_\_\_\_\_ FIC x 2.6 x \_\_\_\_\_ TCFI<sup>g</sup> = \_\_\_\_\_

7b. (1 - \_\_\_\_\_ FIC) x 1.85 x \_\_\_\_\_ TCFNG<sup>i</sup> = \_\_\_\_\_

7c. \_\_\_\_\_ (line 7a) + \_\_\_\_\_ (line 7b) = \_\_\_\_\_

## FOLLOW-UP DOSE PROJECTIONS

## ATTACHMENT III, CALCULATION SHEET III (continued)

8.  $\frac{Du}{Q}$  for additional location No. 1:

$$8a. \text{_____ FIC} \times \text{_____ DUOQI}^f \times \text{_____ TCFI}^g = \text{_____}$$

$$8b. (1 - \text{_____ FIC}) \times \text{_____ DUOQNGH} \times \text{_____ TCFNG}^i = \text{_____}$$

$$8c. \text{_____ (line 8a)} + \text{_____ (line 8b)} = \text{_____}$$

9.  $\frac{Du}{Q}$  for additional location No. 2:

$$9a. \text{_____ FIC} \times \text{_____ DUOQI}^f \times \text{_____ TCFI}^g = \text{_____}$$

$$9b. (1 - \text{_____ FIC}) \times \text{_____ DUOQNGH} \times \text{_____ TCFNG}^i = \text{_____}$$

$$9c. \text{_____ (line 9a)} + \text{_____ (line 9b)} = \text{_____}$$

10.  $\frac{Du}{Q}$  for additional location No. 3:

$$10a. \text{_____ FIC} \times \text{_____ DUOQI}^f \times \text{_____ TCFI}^g = \text{_____}$$

$$10b. (1 - \text{_____ FIC}) \times \text{_____ DUOQNGH} \times \text{_____ TCFNG}^i = \text{_____}$$

$$10c. \text{_____ (line 10a)} + \text{_____ (line 10b)} = \text{_____}$$

$$11a. \text{_____ } \frac{Ci}{\text{sec}} \text{ (line 1)} \times \text{_____ } \frac{\text{sec}^j}{\text{m}^3} \times \text{_____ (line 2)} = \text{_____}$$

$$11b. \text{_____ } \frac{Ci^k}{\text{sec}} \times \text{_____ } \frac{Du}{Q} \text{ (line 3)} + \text{_____ } \frac{\text{m}^l}{\text{sec}} = \text{_____}$$

$$11c. \text{_____ (line 11a)} + \text{_____ (line 11b)}$$

$$= \boxed{\text{_____}} \frac{\text{mrem}}{\text{hr}} \text{ at site boundary}$$

$$12a. \text{_____ } \frac{Ci}{\text{sec}} \text{ (line 1)} \times \text{_____ } \frac{\text{sec}^j}{\text{m}^3} \times \text{_____ (line 2)} = \text{_____}$$

$$12b. \text{_____ } \frac{Ci^k}{\text{sec}} \times \text{_____ } \frac{Du}{Q} \text{ (line 4)} + \text{_____ } \frac{\text{m}^l}{\text{sec}} = \text{_____}$$

$$12c. \text{_____ (line 12a)} + \text{_____ (line 12b)}$$

$$= \boxed{\text{_____}} \frac{\text{mrem}}{\text{hr}} \text{ at point of max } \frac{Xu}{Q}$$

## FOLLOW-UP DOSE PROJECTIONS

## ATTACHMENT III, CALCULATION SHEET III (continued)

$$13a. \frac{Ci}{\text{sec}} (\text{line 1}) \times \frac{\text{sec}^j}{m^3} \times (\text{line 2}) =$$

$$13b. \frac{Ci^k}{\text{sec}} \times \frac{Du}{Q} (\text{line 5}) + \frac{m^l}{\text{sec}} =$$

$$13c. (\text{line 13a}) + (\text{line 13b})$$

$$= \boxed{\phantom{000000}} \frac{\text{mrem}}{\text{hr}} \text{ at 2 miles}$$

$$14a. \frac{Ci}{\text{sec}} (\text{line 1}) \times \frac{\text{sec}^j}{m^3} \times (\text{line 2}) =$$

$$14b. \frac{Ci^k}{\text{sec}} \times \frac{Du}{Q} (\text{line 6}) + \frac{m^l}{\text{sec}} =$$

$$14c. (\text{line 14a}) + (\text{line 14b})$$

$$= \boxed{\phantom{000000}} \frac{\text{mrem}}{\text{hr}} \text{ at 5 miles}$$

$$15a. \frac{Ci}{\text{sec}} (\text{line 1}) \times \frac{\text{sec}^j}{m^3} \times (\text{line 2}) =$$

$$15b. \frac{Ci^k}{\text{sec}} \times \frac{Du}{Q} (\text{line 7}) + \frac{m^l}{\text{sec}} =$$

$$15c. (\text{line 15a}) + (\text{line 15b})$$

$$= \boxed{\phantom{000000}} \frac{\text{mrem}}{\text{hr}} \text{ at 10 miles}$$

$$16a. \frac{Ci}{\text{sec}} (\text{line 1}) \times \frac{\text{sec}^j}{m^3} \times (\text{line 2}) =$$

$$16b. \frac{Ci^k}{\text{sec}} \times \frac{Du}{Q} (\text{line 8}) + \frac{m^l}{\text{sec}} =$$

$$16c. (\text{line 16a}) + (\text{line 16b})$$

$$= \boxed{\phantom{000000}} \frac{\text{mrem}}{\text{hr}} \text{ at additional location No. 1}$$

## FOLLOW-UP DOSE PROJECTIONS

## ATTACHMENT III, CALCULATION SHEET III (continued)

$$17a. \frac{Ci}{\text{sec}} (\text{line 1}) \times \frac{\text{sec}^j}{m^3} \times (\text{line 2}) =$$

$$17b. \frac{Ci^k}{\text{sec}} \times \frac{Du}{Q} (\text{line 9}) + \frac{m^l}{\text{sec}} =$$

$$17c. (\text{line 17a}) + (\text{line 17b})$$

$$= \boxed{\phantom{000000}} \frac{mrem}{hr} \text{ at additional location No. 2}$$

$$18a. \frac{Ci}{\text{sec}} (\text{line 1}) \times \frac{\text{sec}^j}{m^3} \times (\text{line 2}) =$$

$$18b. \frac{Ci^k}{\text{sec}} \times \frac{Du}{Q} (\text{line 10}) + \frac{m^l}{\text{sec}} =$$

$$18c. (\text{line 18a}) + (\text{line 18b})$$

$$= \boxed{\phantom{000000}} \frac{mrem}{hr} \text{ at additional location No. 3}$$

## NOTES:

<sup>a</sup>Reactor building stack release rate from Summary Table, Section II, line 2.

<sup>b</sup>Turbine building roof exhaust release rate from Summary Table, Section II, line 4.

<sup>c</sup>Iodine activity to noble gas activity ratio - obtain from Data Summary Sheet Section IID, line 3b. If unknown use 0.3 unless Standby Gas Treatment is in operation (See Data Summary Sheet, Section II.D, line 1) then use 0.003.

<sup>d</sup>Obtain iodine dose factor (DFI) for time after shutdown (Summary Table, Section I, line 2) from Figure 3.

<sup>e</sup>Obtain noble gas dose factor (DFNG) for time after shutdown (Summary Table, Section I, line 2) from Figure 4.

<sup>f</sup>Obtain  $\frac{Du}{Q}$  for iodine (DUOQI) from Figure 18 using the appropriate distance from Summary Table, Section III, line 1.

<sup>g</sup>Obtain time correction factor for iodine (TCFI) from Figure 6 using time after shutdown (Summary Table, Section I, line 2).

<sup>h</sup>Obtain  $\frac{Du}{Q}$  for noble gas (DUOQNG) from Figure 19 using the appropriate distance from Summary Table, Section III, line 1.

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3b
	Page 49 of 94
FOLLOW-UP DOSE PROJECTIONS	Revision 2
	Date 4/11/83

### ATTACHMENT III, CALCULATION SHEET III (continued)

<sup>i</sup> Obtain the noble gas time correction factor (TCFNG) from Figure 8 using time after shutdown (Summary Table, Section I, line 2).

<sup>j</sup> Obtain appropriate  $\frac{X}{Q}$  for ground level release from Summary Table, Section III, line 2.

<sup>k</sup> Obtain offgas stack release rate from Summary Table, Section II, line 3.

<sup>l</sup> Obtain wind speed from Summary Table, Section I, line 5.

<sup>m</sup> Iodine activity to noble gas activity ratio - obtain from Data Summary Sheet Section IID, line 3a. If unknown use 0.3.

E. Whole body dose - Results for Summary Table Section III, line 5.

$$1. \frac{\text{mrem}}{\text{hr}} \text{ (from Section IVD, line 11C) } \times \text{ } \text{ hr}^a$$

$$= \text{ } \text{ mrem at site boundary}$$

$$2. \frac{\text{mrem}}{\text{hr}} \text{ (from Section IVD, line 12C) } \times \text{ } \text{ hr}^a$$

$$= \text{ } \text{ mrem at point of max X/Q for offgas stack release}$$

$$3. \frac{\text{mrem}}{\text{hr}} \text{ (from Section IVD, line 13C) } \times \text{ } \text{ hr}^a$$

$$= \text{ } \text{ mrem at 2 miles}$$

$$4. \frac{\text{mrem}}{\text{hr}} \text{ (from Section IVD, line 14C) } \times \text{ } \text{ hr}^a$$

$$= \text{ } \text{ mrem at 5 miles}$$

$$5. \frac{\text{mrem}}{\text{hr}} \text{ (from Section IVD, line 15C) } \times \text{ } \text{ hr}^a$$

$$= \text{ } \text{ mrem at 10 miles}$$

$$6. \frac{\text{mrem}}{\text{hr}} \text{ (from Section IVD, line 16C) } \times \text{ } \text{ hr}^a$$

$$= \text{ } \text{ mrem at additional location No. 1}$$

## FOLLOW-UP DOSE PROJECTIONS

## ATTACHMENT III, CALCULATION SHEET III (continued)

$$7. \quad \frac{\text{mrem}}{\text{hr}} \text{ (from Section IVD, line 17C) } \times \quad \text{hr}^a$$

$$= \quad \boxed{\phantom{000000}} \quad \text{mrem at additional location No. 2}$$

$$8. \quad \frac{\text{mrem}}{\text{hr}} \text{ (from Section IVD, line 18C) } \times \quad \text{hr}^a$$

$$= \quad \boxed{\phantom{000000}} \quad \text{mrem at additional location No. 3}$$

NOTE:

<sup>a</sup>Obtain exposure time from Summary Table, Section II, line 1.F. Thyroid Dose Commitment - Result for Summary Table, Section III, line 6.

$$1. \quad \left( \frac{\text{Ci}^a}{\text{sec}} + \frac{\text{Ci}^b}{\text{sec}} \right) \times \quad \text{FIG}^d = \quad \frac{\text{Ci}}{\text{sec}}$$

$$2. \quad \frac{\text{Ci}^c}{\text{sec}} \times \quad \text{FIE}^e \quad \frac{\text{Ci}}{\text{sec}}$$

$$3a. \quad \frac{\text{Ci}}{\text{sec}} \text{ (line 1) } \times \quad \frac{\text{sec}}{\text{m}^3} \text{ (Sect. IVB, line 1) } = \quad \frac{\text{Ci}}{\text{m}^3}$$

$$3b. \quad \frac{\text{Ci}}{\text{sec}} \text{ (line 2) } \times \quad \frac{\text{sec}}{\text{m}^3} \text{ (Sect. IVB, line 1) } = \quad \frac{\text{Ci}}{\text{m}^3}$$

$$3c. \quad \text{(line 3a) } + \quad \text{(line 3b) } = \quad \frac{\text{Ci}}{\text{m}^3}$$

$$4a. \quad \frac{\text{Ci}}{\text{sec}} \text{ (line 1) } \times \quad \frac{\text{sec}}{\text{m}^3} \text{ (Sect. IVB, line 2) } = \quad \frac{\text{Ci}}{\text{m}^3}$$

$$4b. \quad \frac{\text{Ci}}{\text{sec}} \text{ (line 2) } \times \quad \frac{\text{sec}}{\text{m}^3} \text{ (Sect. IVB, line 2) } = \quad \frac{\text{Ci}}{\text{m}^3}$$

$$4c. \quad \text{(line 4a) } + \quad \text{(line 4b) } = \quad \frac{\text{Ci}}{\text{m}^3}$$

$$5a. \quad \frac{\text{Ci}}{\text{sec}} \text{ (line 1) } \times \quad \frac{\text{sec}}{\text{m}^3} \text{ (Sect. IVB, line 3) } = \quad \frac{\text{Ci}}{\text{m}^3}$$

$$5b. \quad \frac{\text{Ci}}{\text{sec}} \text{ (line 2) } \times \quad \frac{\text{sec}}{\text{m}^3} \text{ (Sect. IVB, line 3) } = \quad \frac{\text{Ci}}{\text{m}^3}$$

$$5c. \quad \text{(line 5a) } + \quad \text{(line 5b) } = \quad \frac{\text{Ci}}{\text{m}^3}$$

## FOLLOW-UP DOSE PROJECTIONS

## ATTACHMENT III, CALCULATION SHEET III (continued)

- 6a.  $\frac{Ci}{sec} (line 1) \times \frac{sec}{m^3} (Sect. IVB, line 4) = \frac{Ci}{m^3}$
- 6b.  $\frac{Ci}{sec} (line 2) \times \frac{sec}{m^3} (Sect. IVB, line 4) = \frac{Ci}{m^3}$
- 6c.  $(line 6a) + (line 6b) = \frac{Ci}{m^3}$
- 7a.  $\frac{Ci}{sec} (line 1) \times \frac{sec}{m^3} (Sect. IVB, line 5) = \frac{Ci}{m^3}$
- 7b.  $\frac{Ci}{sec} (line 2) \times \frac{sec}{m^3} (Sect. IVB, line 5) = \frac{Ci}{m^3}$
- 7c.  $(line 7a) + (line 7b) = \frac{Ci}{m^3}$
- 8a.  $\frac{Ci}{sec} (line 1) \times \frac{sec}{m^3} (Sect. IVB, line 6) = \frac{Ci}{m^3}$
- 8b.  $\frac{Ci}{sec} (line 2) \times \frac{sec}{m^3} (Sect. IVB, line 6) = \frac{Ci}{m^3}$
- 8c.  $(line 8a) + (line 8b) = \frac{Ci}{m^3}$
- 9a.  $\frac{Ci}{sec} (line 1) \times \frac{sec}{m^3} (Sect. IVB, line 7) = \frac{Ci}{m^3}$
- 9b.  $\frac{Ci}{sec} (line 2) \times \frac{sec}{m^3} (Sect. IVB, line 7) = \frac{Ci}{m^3}$
- 9c.  $(line 9a) + (line 9b) = \frac{Ci}{m^3}$
- 10a.  $\frac{Ci}{sec} (line 1) \times \frac{sec}{m^3} (Sect. IVB, line 8) = \frac{Ci}{m^3}$
- 10b.  $\frac{Ci}{sec} (line 2) \times \frac{sec}{m^3} (Sect. IVB, line 8) = \frac{Ci}{m^3}$
- 10c.  $(line 10a) + (line 10b) = \frac{Ci}{m^3}$
11.  $\frac{Ci}{m^3} (line 3) \times \text{hr}^9 \times 3.8 \times 10^8$   
 $\times \text{TCFI}^f = \boxed{\phantom{000000}} \text{ mrem at site boundary}$
12.  $\frac{Ci}{m^3} (line 4) \times \text{hr}^9 \times 3.8 \times 10^8$   
 $\times \text{TCFI}^f = \boxed{\phantom{000000}} \text{ mrem at point of max X/Q}$

## FOLLOW-UP DOSE PROJECTIONS

## ATTACHMENT III, CALCULATION SHEET III (continued)

13.  $\frac{Ci}{m^3}$  (line 5) x  $hr^9$  x  $3.8 \times 10^8$   
 x  $TCFI^f$  =  mrem at 2 miles
14.  $\frac{Ci}{m^3}$  (line 6) x  $hr^9$  x  $3.8 \times 10^8$   
 x  $TCFI^f$  =  mrem at 5 miles
15.  $\frac{Ci}{m^3}$  (line 7) x  $hr^9$  x  $3.8 \times 10^8$   
 x  $TCFI^f$  =  mrem at 10 miles
16.  $\frac{Ci}{m^3}$  (line 8) x  $hr^9$  x  $3.8 \times 10^8$   
 x  $TCFI^f$  =  mrem at additional location No. 1
17.  $\frac{Ci}{m^3}$  (line 9) x  $hr^9$  x  $3.8 \times 10^8$   
 x  $TCFI^f$  =  mrem at additional location No. 2
18.  $\frac{Ci}{m^3}$  (line 10) x  $hr^9$  x  $3.8 \times 10^8$   
 x  $TCFI^f$  =  mrem at additional location No. 3

## NOTES:

<sup>a</sup>Reactor building stack release rate from Summary Table, Section II, line 2.

<sup>b</sup>Turbine building roof exhaust release rate from Summary Table, Section II, line 4.

<sup>c</sup>Offgas stack release rate from Summary Table, Section II, line 3.

<sup>d</sup>Iodine activity fraction for ground level release - obtain from Data Summary Sheet Section IID, line 3a. If unknown use 0.3.

<sup>e</sup>Iodine activity fraction for elevated release - obtain from Data Summary Sheet Section IID, line 3b. If unknown use 0.3 unless Standby Gas Treatment (see Data Summary Sheet, Section II.D, line 1) is in operation then use 0.003.

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3b
FOLLOW-UP DOSE PROJECTIONS	Page 53 of 94
	Revision 2
	Date 4/11/83

# ATTACHMENT III. CALCULATION SHEET III (continued)

<sup>f</sup>Obtain TCFI from Figure 9 using time after shutdown (Summary Table, Section I, line 2).

<sup>g</sup>Obtain exposure time from Summary Table, Section II, line 1.

G. Plume width - The following are the plume widths to be placed in the Summary Table, Section III, line 7.

Point of maximum X/Q for Offgas Stack release	2mi	5mi	10mi
1400 (0.87)	1100 (0.68)	2400 (1.5)	4300 (meters) (2.7)(miles)

NOTE:

Obtain remaining plume widths from Figure 20 using the appropriate distances from Summary Table, Section III, line 1.

H. Plume arrival time - Results for Summary Table Section III, line 8.

1.  $2.78 \times 10^{-4} \times \underline{\hspace{2cm}} m^a + \underline{\hspace{2cm}} \frac{m^b}{\text{sec}} = \underline{\hspace{2cm}} \text{hr to Site Boundary}$
2. 1.11 divided by  $\underline{\hspace{2cm}} \frac{m^b}{\text{sec}} = \underline{\hspace{2cm}} \text{hr to point of max X/Q for offgas stack release}$
3. 0.894 divided by  $\underline{\hspace{2cm}} \frac{m^b}{\text{sec}} = \underline{\hspace{2cm}} \text{hr to 2 miles}$
4. 2.23 divided by  $\underline{\hspace{2cm}} \frac{m^b}{\text{sec}} = \underline{\hspace{2cm}} \text{hr to 5 miles}$
5. 4.47 divided by  $\underline{\hspace{2cm}} \frac{m^b}{\text{sec}} = \underline{\hspace{2cm}} \text{hr to 10 miles}$
6.  $2.78 \times 10^{-4} \times \underline{\hspace{2cm}} m^a + \underline{\hspace{2cm}} \frac{m^b}{\text{sec}} = \underline{\hspace{2cm}} \text{hr to additional location No. 1}$
7.  $2.78 \times 10^{-4} \times \underline{\hspace{2cm}} m^a + \underline{\hspace{2cm}} \frac{m^b}{\text{sec}} = \underline{\hspace{2cm}} \text{hr to additional location No. 2}$
8.  $2.78 \times 10^{-4} \times \underline{\hspace{2cm}} m^a + \underline{\hspace{2cm}} \frac{m^b}{\text{sec}} = \underline{\hspace{2cm}} \text{hr to additional location No. 3}$

NOTES:

<sup>a</sup>Obtain appropriate distance from Summary Table, Section III, line 1.

<sup>b</sup>Obtain wind speed from Summary Table, Section I, line 5.

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3b
	Page 54 of 94
FOLLOW-UP DOSE PROJECTIONS	Revision 2
	Date 4/11/83

# ATTACHMENT III, CALCULATION SHEET III (continued)

## V.. Dose information for atmospheric stability class FG

### A. Variable distance and Xu/Q values.

1. Obtain distance to site boundary and Xu/Q for ground level and elevated releases from following table using the down wind direction from Summary Table, Section I, line 4.

Distance \_\_\_\_\_ m  $\frac{X_u}{Q}$  (Ground Level Rel.) \_\_\_\_\_  $\frac{1}{m^2}$

$\frac{X_u}{Q}$  (Elevated Rel.) \_\_\_\_\_  $\frac{1}{m^2}$

Down Wind Direction deg.	Distance to Site Bdy. meters	$\frac{X_u}{Q}$ , $\frac{1}{m^2}$ Ground Level Rel.	Elevated Rel.
0 - 11.25	1200	$9.5 \times 10^{-4}$	0.0
11.25 - 33.75	1600	$6.2 \times 10^{-4}$	0.0
33.75 - 56.25	700	$2.1 \times 10^{-3}$	0.0
56.25 - 78.75	610	$2.6 \times 10^{-3}$	0.0
78.75 - 101.25	490	$3.6 \times 10^{-3}$	0.0
101.25 - 123.75	450	$4.1 \times 10^{-3}$	0.0
123.75 - 146.25	480	$3.7 \times 10^{-3}$	0.0
146.25 - 168.75	500	$3.5 \times 10^{-3}$	0.0
168.75 - 191.25	460	$3.9 \times 10^{-3}$	0.0
191.25 - 213.75	500	$3.5 \times 10^{-3}$	0.0
213.75 - 236.25	630	$2.5 \times 10^{-3}$	0.0
236.25 - 258.75	720	$2.0 \times 10^{-3}$	0.0
258.75 - 281.25	670	$2.2 \times 10^{-3}$	0.0
281.25 - 303.75	730	$2.0 \times 10^{-3}$	0.0
303.75 - 326.25	980	$1.2 \times 10^{-3}$	0.0
326.25 - 348.75	1300	$8.3 \times 10^{-4}$	0.0
348.75 - 360.00	1200	$9.5 \times 10^{-4}$	0.0

2. Distance to point of maximum  $\frac{X_u}{Q}$  for offgas stack release = 16090m.

## FOLLOW-UP DOSE PROJECTIONS

## ATTACHMENT III, CALCULATION SHEET III (continued)

B. Normalized concentration, Ground level release - Results for Summary Table, Section III, line 2.

$$1. \frac{1^a}{m^2} \div \text{_____} m/sec^b = \frac{\text{_____}}{m^3} \frac{sec}{m^3} \text{ at site boundary}$$

$$2. 2.0 \times 10^{-5} \div \text{_____} m/sec^b = \frac{\text{_____}}{m^3} \frac{sec}{m^3} \text{ at point of max X/Q for offgas release}$$

$$3. 2.1 \times 10^{-4} \div \text{_____} m/sec^b = \frac{\text{_____}}{m^3} \frac{sec}{m^3} \text{ at 2 miles}$$

$$4. 5.5 \times 10^{-5} \div \text{_____} m/sec^b = \frac{\text{_____}}{m^3} \frac{sec}{m^3} \text{ at 5 miles}$$

$$5. 2.0 \times 10^{-5} \div \text{_____} m/sec^b = \frac{\text{_____}}{m^3} \frac{sec}{m^3} \text{ at 10 miles}$$

$$6. \frac{1^c}{m^2} \div \text{_____} m/sec^b = \frac{\text{_____}}{m^3} \frac{sec}{m^3} \text{ at additional location No. 1}$$

$$7. \frac{1^c}{m^2} \div \text{_____} m/sec^b = \frac{\text{_____}}{m^3} \frac{sec}{m^3} \text{ at additional location No. 2}$$

$$8. \frac{1^c}{m^2} \div \text{_____} m/sec^b = \frac{\text{_____}}{m^3} \frac{sec}{m^3} \text{ at additional location No. 3}$$

## NOTE:

<sup>a</sup>Obtain  $\frac{X_u}{Q}$  for ground level release from Section V, Subsection A, line 1.

<sup>b</sup>Obtain wind speed from Summary Table Section I, line 5.

<sup>c</sup>Obtain ground level release  $\frac{X_u}{Q}$  for additional locations using Figure 21 and appropriate distance from Summary Table, Section III, line 1.

## ATTACHMENT III, CALCULATION SHEET III (continued)

C. Normalized concentration, Elevated release - Results for Summary Table, Section III, line 3.

$$1. \frac{1a}{m^2} + \text{_____} m/sec^b = \boxed{\text{_____}} \frac{sec}{m^3} \text{ at site boundary}$$

$$2. 1.7 \times 10^{-4} + \text{_____} m/sec^b = \boxed{\text{_____}} \frac{sec}{m^3} \text{ at point of max X/Q for offgas stack release}$$

$$3. 1.7 \times 10^{-11} + \text{_____} m/sec^b = \boxed{\text{_____}} \frac{sec}{m^3} \text{ at 2 miles}$$

$$4. 2.2 \times 10^{-7} + \text{_____} m/sec^b = \boxed{\text{_____}} \frac{sec}{m^3} \text{ at 5 miles}$$

$$5. 1.7 \times 10^{-6} + \text{_____} m/sec^b = \boxed{\text{_____}} \frac{sec}{m^3} \text{ at 10 miles}$$

$$6. \frac{1c}{m^2} + \text{_____} m/sec^b = \boxed{\text{_____}} \frac{sec}{m^3} \text{ at additional location No. 1}$$

$$7. \frac{1c}{m^2} + \text{_____} m/sec^b = \boxed{\text{_____}} \frac{sec}{m^3} \text{ at additional location No. 2}$$

$$8. \frac{1c}{m^2} + \text{_____} m/sec^b = \boxed{\text{_____}} \frac{sec}{m^3} \text{ at additional location No. 3}$$

## NOTE:

<sup>a</sup>Obtain  $\frac{Xu}{Q}$  for elevated release from Section V, Subsection A, line 1.

<sup>b</sup>Obtain wind speed from Summary Table, Section I, line 5.

<sup>c</sup>Obtain elevated release  $\frac{Xu}{Q}$  for additional locations using Figure 22 and appropriate distances from Summary Table, Section III, line 1.

D. Whole body dose rate - Results for Summary Table, Section III, line 4.

$$1. \frac{Ci^a}{sec} + \text{_____} \frac{Ci^b}{sec} = \text{_____} \frac{Ci}{sec}$$

$$2a. \text{FIM} \times \text{_____} DFID^c = \text{_____}$$

$$2b. (1 - \text{FIM}) \times \text{_____} DFNG^e = \text{_____}$$

$$2c. \text{_____} (\text{line 2a}) + \text{_____} (\text{line 2b}) = \text{_____}$$

## FOLLOW-UP DOSE PROJECTIONS

## ATTACHMENT III, CALCULATION SHEET III (continued)

3.  $\frac{Du}{Q}$  for site boundary:

3a. \_\_\_\_\_ FIC x \_\_\_\_\_ DUOQI<sup>f</sup> x \_\_\_\_\_ TCFI<sup>9</sup> = \_\_\_\_\_

3b. (1 - \_\_\_\_\_ FIC) x \_\_\_\_\_ DUOQNG<sup>h</sup> x \_\_\_\_\_ TCFNG<sup>i</sup> = \_\_\_\_\_

3c. \_\_\_\_\_ (line 3a) + \_\_\_\_\_ (line 3b) = \_\_\_\_\_

4.  $\frac{Du}{Q}$  for location of maximum  $\frac{Xu}{Q}$

4a. \_\_\_\_\_ FIC x 4.2 x \_\_\_\_\_ TCFI<sup>9</sup> = \_\_\_\_\_

4b. (1 - \_\_\_\_\_ FIC) x 3.0 x \_\_\_\_\_ TCFNG<sup>i</sup> = \_\_\_\_\_

4c. \_\_\_\_\_ (line 4a) + \_\_\_\_\_ (line 4b) = \_\_\_\_\_

5.  $\frac{Du}{Q}$  for 2 miles:

5a. \_\_\_\_\_ FIC x 6.8 x \_\_\_\_\_ TCFI<sup>9</sup> = \_\_\_\_\_

5b. (1 - \_\_\_\_\_ FIC) x 4.8 x \_\_\_\_\_ TCFNG<sup>i</sup> = \_\_\_\_\_

5c. \_\_\_\_\_ (line 5a) + \_\_\_\_\_ (line 5b) = \_\_\_\_\_

6.  $\frac{Du}{Q}$  for 5 miles

6a. \_\_\_\_\_ FIC x 5.3 x \_\_\_\_\_ TCFI<sup>9</sup> = \_\_\_\_\_

6b. (1 - \_\_\_\_\_ FIC) x 3.7 x \_\_\_\_\_ TCFNG<sup>i</sup> = \_\_\_\_\_

6c. \_\_\_\_\_ (line 6a) + \_\_\_\_\_ (line 6b) = \_\_\_\_\_

7.  $\frac{Du}{Q}$  for 10 miles

7a. \_\_\_\_\_ FIC x 4.2 x \_\_\_\_\_ TCFI<sup>9</sup> = \_\_\_\_\_

7b. (1 - \_\_\_\_\_ FIC) x 3.0 x \_\_\_\_\_ TCFNG<sup>i</sup> = \_\_\_\_\_

7c. \_\_\_\_\_ (line 7a) + \_\_\_\_\_ (line 7b) = \_\_\_\_\_

8.  $\frac{Du}{Q}$  for additional location No. 1

8a. \_\_\_\_\_ FIC x \_\_\_\_\_ DUOQI<sup>f</sup> x \_\_\_\_\_ TCFI<sup>9</sup> = \_\_\_\_\_

8b. (1 - \_\_\_\_\_ FIC) x \_\_\_\_\_ DUOQNG<sup>h</sup> x \_\_\_\_\_ TCFNG<sup>i</sup> = \_\_\_\_\_

8c. \_\_\_\_\_ (line 8a) + \_\_\_\_\_ (line 8b) = \_\_\_\_\_

## ATTACHMENT III, CALCULATION SHEET III (continued)

9.  $\frac{Du}{Q}$  for additional location No. 2

9a. \_\_\_\_\_  $FIC$  x \_\_\_\_\_  $DUOQI^f$  x \_\_\_\_\_  $TCFI^g$  = \_\_\_\_\_

9b.  $(1 - \text{_____ } FIC)$  x \_\_\_\_\_  $DUOQNG^h$  x \_\_\_\_\_  $TCFNG^i$  = \_\_\_\_\_

9c. \_\_\_\_\_ (line 9a) + \_\_\_\_\_ (line 9b) = \_\_\_\_\_

10.  $\frac{Du}{Q}$  for additional location No. 3

10a. \_\_\_\_\_  $FIC$  x \_\_\_\_\_  $DUOQI^f$  x \_\_\_\_\_  $TCFI^g$  = \_\_\_\_\_

10b.  $(1 - \text{_____ } FIC)$  x \_\_\_\_\_  $DUOQNG^h$  x \_\_\_\_\_  $TCFNG^i$  = \_\_\_\_\_

10c. \_\_\_\_\_ (line 10a) + \_\_\_\_\_ (line 10b) = \_\_\_\_\_

11a. \_\_\_\_\_  $\frac{Ci}{\text{sec}}$  (line 1) x \_\_\_\_\_  $\frac{\text{sec}^j}{m^3}$  x \_\_\_\_\_ (line 2) = \_\_\_\_\_

11b. \_\_\_\_\_  $\frac{Cik}{\text{sec}}$  x \_\_\_\_\_  $\frac{Du}{Q}$  (line 3c) + \_\_\_\_\_  $\frac{m^l}{\text{sec}}$  = \_\_\_\_\_

11c. \_\_\_\_\_ (line 11a) + \_\_\_\_\_ (line 11b)

= \_\_\_\_\_  $\frac{\text{mrem}}{\text{hr}}$  at site boundary

12a. \_\_\_\_\_  $\frac{Ci}{\text{sec}}$  (line 1) x \_\_\_\_\_  $\frac{\text{sec}^j}{m^3}$  x \_\_\_\_\_ (line 2) = \_\_\_\_\_

12b. \_\_\_\_\_  $\frac{Cik}{\text{sec}}$  x \_\_\_\_\_  $\frac{Du}{Q}$  (line 4c) + \_\_\_\_\_  $\frac{m^l}{\text{sec}}$  = \_\_\_\_\_

12c. \_\_\_\_\_ (line 12a) + \_\_\_\_\_ (line 12b)

= \_\_\_\_\_  $\frac{\text{mrem}}{\text{hr}}$  at point of max  $\frac{Xu}{Q}$

13a. \_\_\_\_\_  $\frac{Ci}{\text{sec}}$  (line 1) x \_\_\_\_\_  $\frac{\text{sec}^j}{m^3}$  x \_\_\_\_\_ (line 2) = \_\_\_\_\_

13b. \_\_\_\_\_  $\frac{Cik}{\text{sec}}$  x \_\_\_\_\_  $\frac{Du}{Q}$  (line 5c) + \_\_\_\_\_  $\frac{m^l}{\text{sec}}$  = \_\_\_\_\_

13c. \_\_\_\_\_ (line 13a) + \_\_\_\_\_ (line 13b)

= \_\_\_\_\_  $\frac{\text{mrem}}{\text{hr}}$  at 2 miles

## FOLLOW-UP DOSE PROJECTIONS

## ATTACHMENT III, CALCULATION SHEET III (continued)

$$14a. \frac{Ci}{sec} (line\ 1) \times \frac{sec^j}{m^3} \times (line\ 2) =$$

$$14b. \frac{Cik}{sec} \times \frac{Du}{Q} (line\ 6c) + \frac{m^1}{sec} =$$

$$14c. (line\ 14a) + (line\ 14b)$$

$$= \boxed{\phantom{000000}} \frac{mrem}{hr} \text{ at 5 miles}$$

$$15a. \frac{Ci}{sec} (line\ 1) \times \frac{sec^j}{m^3} \times (line\ 2) =$$

$$15b. \frac{Cik}{sec} \times \frac{Du}{Q} (line\ 7c) + \frac{m^1}{sec} =$$

$$15c. (line\ 15a) + (line\ 15b)$$

$$= \boxed{\phantom{000000}} \frac{mrem}{hr} \text{ at 10 miles}$$

$$16a. \frac{Ci}{sec} (line\ 1) \times \frac{sec^j}{m^3} \times (line\ 2) =$$

$$16b. \frac{Cik}{sec} \times \frac{Du}{Q} (line\ 8c) + \frac{m^1}{sec} =$$

$$16c. (line\ 16a) + (line\ 16b)$$

$$= \boxed{\phantom{000000}} \frac{mrem}{hr} \text{ at additional location No. 1}$$

$$17a. \frac{Ci}{sec} (line\ 1) \times \frac{sec^j}{m^3} \times (line\ 2) =$$

$$17b. \frac{Cik}{sec} \times \frac{Du}{Q} (line\ 9c) + \frac{m^1}{sec} =$$

$$17c. (line\ 17a) + (line\ 17b)$$

$$= \boxed{\phantom{000000}} \frac{mrem}{hr} \text{ at additional location No. 2}$$

## ATTACHMENT III, CALCULATION SHEET III (continued)

$$\begin{aligned}
 18a. & \quad \frac{C_i}{\text{sec}} \text{ (line 1)} \times \frac{\text{sec}^j}{\text{m}^3} \times \text{ (line 2)} = \text{ } \\
 18b. & \quad \frac{C_i^k}{\text{sec}} \times \frac{D_u}{Q} \text{ (line 10c)} + \frac{\text{m}^l}{\text{sec}} = \text{ } \\
 18c. & \quad \text{ (line 18a)} + \text{ (line 18b)} \\
 & = \boxed{\phantom{000}} \frac{\text{mrem}}{\text{hr}} \text{ at additional location No. 3}
 \end{aligned}$$

## NOTES:

- <sup>a</sup>Reactor building stack release rate from Summary Table, Section II, line 2.
- <sup>b</sup>Turbine building roof exhaust release rate from Summary Table, Section II, line 4.
- <sup>c</sup>Iodine activity to noble gas activity ratio - obtain from Data Summary Sheet, Section IID, line 3b. If unknown use 0.3 unless Standby Gas Treatment is in operation (See Data Summary Sheet, Section II.D, line 1) then use 0.003.
- <sup>d</sup>Obtain iodine dose factor (DFI) for time after shutdown (Summary Table, Section I, line 2) from Figure 3.
- <sup>e</sup>Obtain noble gas dose factor (DFNG) for time after shutdown (Summary Table, Section I, line 2) from Figure 4.
- <sup>f</sup>Obtain  $\frac{D_u}{Q}$  for iodine (DUQOI) from Figure 23 using the appropriate distance from Summary Table, Section III, line 1.
- <sup>g</sup>Obtain time correction factor for iodine (TCFI) from Figure 6 using time after shutdown (Summary Table, Section I, line 2).
- <sup>h</sup>Obtain  $\frac{D_u}{Q}$  for noble gas (DUQNG) from Figure 24 using the appropriate distance from Summary Table, Section III, line 1.
- <sup>i</sup>Obtain the noble gas time correction factor (TCFNG) from Figure 8 using time after shutdown (Summary Table, Section I, line 2).
- <sup>j</sup>Obtain appropriate  $\frac{X}{Q}$  for ground level release from Summary Table, Section III, line 2.
- <sup>k</sup>Obtain offgas stack release rate from Summary Table, Section II, line 3.
- <sup>l</sup>Obtain wind speed from Summary Table, Section I, line 5.
- <sup>m</sup>Iodine activity to noble gas activity ratio-obtain from Data Summary Sheet Section IID, line 3a. If unknown use 0.3.

## FOLLOW-UP DOSE PROJECTIONS

## ATTACHMENT III, CALCULATION SHEET III (continued)

E. Whole body dose - Results for Summary Table Section III, line 5.

1. \_\_\_\_\_  $\frac{\text{mrem}}{\text{hr}}$  (from Section VD, line 11C) x \_\_\_\_\_  $\text{hr}^a$

=  mrem at site boundary

2. \_\_\_\_\_  $\frac{\text{mrem}}{\text{hr}}$  (from Section VD, line 12C) x \_\_\_\_\_  $\text{hr}^a$

=  mrem at point of max X/Q

3. \_\_\_\_\_  $\frac{\text{mrem}}{\text{hr}}$  (from Section VD, line 13C) x \_\_\_\_\_  $\text{hr}^a$

=  mrem at 2 miles

4. \_\_\_\_\_  $\frac{\text{mrem}}{\text{hr}}$  (from Section VD, line 14C) x \_\_\_\_\_  $\text{hr}^a$

=  mrem at 5 miles

5. \_\_\_\_\_  $\frac{\text{mrem}}{\text{hr}}$  (from Section VD, line 15C) x \_\_\_\_\_  $\text{hr}^a$

=  mrem at 10 miles

6. \_\_\_\_\_  $\frac{\text{mrem}}{\text{hr}}$  (from Section VD, line 16C) x \_\_\_\_\_  $\text{hr}^a$

=  mrem at additional location No. 1

7. \_\_\_\_\_  $\frac{\text{mrem}}{\text{hr}}$  (from Section VD, line 17C) x \_\_\_\_\_  $\text{hr}^a$

=  mrem at additional location No. 2

8. \_\_\_\_\_  $\frac{\text{mrem}}{\text{hr}}$  (from Section VD, line 18C) x \_\_\_\_\_  $\text{hr}^a$

=  mrem at additional location No. 3

## ATTACHMENT III, CALCULATION SHEET III (continued)

## NOTE:

<sup>a</sup>Obtain exposure time from Summary Table, Section II, line 1.F. Thyroid Dose Commitment - Result for Summary Table, Section III, line 6.

$$1. \left( \frac{Ci^a}{sec} + \frac{Ci^b}{sec} \right) \times \text{FIG}^d = \frac{Ci}{sec}$$

$$2. \frac{Ci^c}{sec} \times \text{FIE}^e \frac{Ci}{sec}$$

$$3a. \frac{Ci}{sec} \text{ (line 1)} \times \frac{sec}{m^3} \text{ (Sect. VB, line 1)} = \frac{Ci}{m^3}$$

$$3b. \frac{Ci}{sec} \text{ (line 2)} \times \frac{sec}{m^3} \text{ (Sect. VC, line 1)} = \frac{Ci}{m^3}$$

$$3c. \text{ (line 3a)} + \text{ (line 3b)} = \frac{Ci}{m^3}$$

$$4a. \frac{Ci}{sec} \text{ (line 1)} \times \frac{sec}{m^3} \text{ (Sect. VB, line 2)} = \frac{Ci}{m^3}$$

$$4b. \frac{Ci}{sec} \text{ (line 2)} \times \frac{sec}{m^3} \text{ (Sect. VC, line 2)} = \frac{Ci}{m^3}$$

$$4c. \text{ (line 4a)} + \text{ (line 4b)} = \frac{Ci}{m^3}$$

$$5a. \frac{Ci}{sec} \text{ (line 1)} \times \frac{sec}{m^3} \text{ (Sect. VB, line 3)} = \frac{Ci}{m^3}$$

$$5b. \frac{Ci}{sec} \text{ (line 2)} \times \frac{sec}{m^3} \text{ (Sect. VC, line 3)} = \frac{Ci}{m^3}$$

$$5c. \text{ (line 5a)} + \text{ (line 5b)} = \frac{Ci}{m^3}$$

$$6a. \frac{Ci}{sec} \text{ (line 1)} \times \frac{sec}{m^3} \text{ (Sect. VB, line 4)} = \frac{Ci}{m^3}$$

$$6b. \frac{Ci}{sec} \text{ (line 2)} \times \frac{sec}{m^3} \text{ (Sect. VC, line 4)} = \frac{Ci}{m^3}$$

$$6c. \text{ (line 6a)} + \text{ (line 6b)} = \frac{Ci}{m^3}$$

## FOLLOW-UP DOSE PROJECTIONS

## ATTACHMENT III, CALCULATION SHEET III (continued)

$$7a. \frac{Ci}{sec} \text{ (line 1)} \times \frac{sec}{m^3} \text{ (Sect. VB, line 5)} = \frac{Ci}{m^3}$$

$$7b. \frac{Ci}{sec} \text{ (line 2)} \times \frac{sec}{m^3} \text{ (Sect. VC, line 5)} = \frac{Ci}{m^3}$$

$$7c. \text{ (line 7a)} + \text{ (line 7b)} = \frac{Ci}{m^3}$$

$$8a. \frac{Ci}{sec} \text{ (line 1)} \times \frac{sec}{m^3} \text{ (Sect. VB, line 6)} = \frac{Ci}{m^3}$$

$$8b. \frac{Ci}{sec} \text{ (line 2)} \times \frac{sec}{m^3} \text{ (Sect. VC, line 6)} = \frac{Ci}{m^3}$$

$$8c. \text{ (line 8a)} + \text{ (line 8b)} = \frac{Ci}{m^3}$$

$$9a. \frac{Ci}{sec} \text{ (line 1)} \times \frac{sec}{m^3} \text{ (Sect. VB, line 7)} = \frac{Ci}{m^3}$$

$$9b. \frac{Ci}{sec} \text{ (line 2)} \times \frac{sec}{m^3} \text{ (Sect. VC, line 7)} = \frac{Ci}{m^3}$$

$$9c. \text{ (line 9a)} + \text{ (line 9b)} = \frac{Ci}{m^3}$$

$$10a. \frac{Ci}{sec} \text{ (line 1)} \times \frac{sec}{m^3} \text{ (Sect. VB, line 8)} = \frac{Ci}{m^3}$$

$$10b. \frac{Ci}{sec} \text{ (line 2)} \times \frac{sec}{m^3} \text{ (Sect. VC, line 8)} = \frac{Ci}{m^3}$$

$$10c. \text{ (line 10a)} + \text{ (line 10b)} = \frac{Ci}{m^3}$$

$$11. \frac{Ci}{m^3} \text{ (line 3c)} \times \text{ hr}^9 \times 3.8 \times 10^8$$

$$\times \text{ TCFI}^f = \boxed{\phantom{000000}} \text{ mrem at site boundary}$$

$$12. \frac{Ci}{m^3} \text{ (line 4c)} \times \text{ hr}^9 \times 3.8 \times 10^8$$

$$\times \text{ TCFI}^f = \boxed{\phantom{000000}} \text{ mrem at point of max X/Q}$$

## ATTACHMENT III, CALCULATION SHEET III (continued)

$$13. \quad \frac{Ci}{m^3} \text{ (line 5c)} \times \text{hr}^9 \times 3.8 \times 10^8$$

$$\times \text{TCFI}^f = \boxed{\phantom{000000}} \text{ mrem at 2 miles}$$

$$14. \quad \frac{Ci}{m^3} \text{ (line 6c)} \times \text{hr}^9 \times 3.8 \times 10^8$$

$$\times \text{TCFI}^f = \boxed{\phantom{000000}} \text{ mrem at 5 miles}$$

$$15. \quad \frac{Ci}{m^3} \text{ (line 7c)} \times \text{hr}^9 \times 3.8 \times 10^8$$

$$\times \text{TCFI}^f = \boxed{\phantom{000000}} \text{ mrem at 10 miles}$$

$$16. \quad \frac{Ci}{m^3} \text{ (line 8c)} \times \text{hr}^9 \times 3.8 \times 10^8$$

$$\times \text{TCFI}^f = \boxed{\phantom{000000}} \text{ mrem at additional location No. 1}$$

$$17. \quad \frac{Ci}{m^3} \text{ (line 9c)} \times \text{hr}^9 \times 3.8 \times 10^8$$

$$\times \text{TCFI}^f = \boxed{\phantom{000000}} \text{ mrem at additional location No. 2}$$

$$18. \quad \frac{Ci}{m^3} \text{ (line 10c)} \times \text{hr}^9 \times 3.8 \times 10^8$$

$$\times \text{TCFI}^f = \boxed{\phantom{000000}} \text{ mrem at additional location No. 3}$$

## NOTES:

<sup>a</sup>Reactor building stack release rate from Summary Table, Section II, line 2.

<sup>b</sup>Turbine building roof exhaust release rate from Summary Table, Section II, line 4.

<sup>c</sup>Offgas stack release rate from Summary Table, Section II, line 3.

<sup>d</sup>Iodine activity fraction for ground level release - obtain from Data Summary Sheet Section IID, line 3a. If unknown use 0.3.

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3b
	Page 65 of 94
FOLLOW-UP DOSE PROJECTIONS	Revision 2
	Date 4/11/83

### ATTACHMENT III, CALCULATION SHEET III (continued)

<sup>e</sup>Iodine activity fraction for elevated release - obtain from Data Summary Sheet Section IID, line 3b. If unknown use 0.3 unless Standby Gas Treatment (see Data Summary Sheet, Section II.D, line 1) is in operation then use 0.003.

<sup>f</sup>Obtain TCFI from Figure 19 using time after shutdown (Summary Table, Section I, line 2).

<sup>g</sup>Obtain exposure time from Summary Table, Section II, line 1.

G. Plume width - The following are the plume widths to be placed in the Summary Table, Section III, line 7.

Point of maximum X/Q for Offgas Stack release	2mi	5mi	10mi
2000 (1.2)	530 (0.33)	970 (0.60)	2000 (meters) (1.2)(miles)

NOTE:

Obtain remaining plume widths from Figure 25 using the appropriate distances from Summary Table, Section III, line 1.

H. Plume arrival time - Results for Summary Table Section III, line 8.

$$1. \quad 2.78 \times 10^{-4} \times \underline{\hspace{2cm}} m^a + \frac{m^b}{\text{sec}} = \boxed{\hspace{1cm}} \text{ hr to Site Boundary}$$

$$2. \quad 4.47 \text{ divided by } \underline{\hspace{2cm}} \frac{m^b}{\text{sec}} = \boxed{\hspace{1cm}} \text{ hr to point of max X/Q for offgas stack release}$$

$$3. \quad 0.894 \text{ divided by } \underline{\hspace{2cm}} \frac{m^b}{\text{sec}} = \boxed{\hspace{1cm}} \text{ hr to 2 miles}$$

$$4. \quad 2.23 \text{ divided by } \underline{\hspace{2cm}} \frac{m^b}{\text{sec}} = \boxed{\hspace{1cm}} \text{ hr to 5 miles}$$

$$5. \quad 4.47 \text{ divided by } \underline{\hspace{2cm}} \frac{m^b}{\text{sec}} = \boxed{\hspace{1cm}} \text{ hr to 10 miles}$$

$$6. \quad 2.78 \times 10^{-4} \times \underline{\hspace{2cm}} m^a + \frac{m^b}{\text{sec}} = \boxed{\hspace{1cm}} \text{ hr to additional location No. 1}$$

## FOLLOW-UP DOSE PROJECTIONS

## ATTACHMENT III, CALCULATION SHEET III (continued)

$$7. \quad 2.78 \times 10^{-4} \times \text{_____ } m^a + \text{_____ } \frac{m^b}{\text{sec}} = \text{_____ } \text{hr to additional location No. 2}$$

$$8. \quad 2.78 \times 10^{-4} \times \text{_____ } m^a + \text{_____ } \frac{m^b}{\text{sec}} = \text{_____ } \text{hr to additional location No. 3}$$

## NOTES:

<sup>a</sup>Obtain appropriate distance from Summary Table, Section III, line 1.

<sup>b</sup>Obtain wind speed from Summary Table, Section I, line 5.

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 3.3b
	Page 67 of 94
FOLLOW-UP DOSE PROJECTIONS	Revision 2
	Date 4/11/83

### ATTACHMENT III, CALCULATION SHEET IV

#### RELEASE RATE FROM FIELD MEASUREMENT

$$\begin{aligned}
 1. & \quad \text{FIA} \times \text{DUOQI}^b \times \text{TCFI}^c \\
 & + (1 - \text{FIA}) \times \text{DUOQNG}^d \times \text{TCFNG}^e \\
 & = \frac{\text{Du}}{\text{Q}} \\
 2. & \quad \text{mR/hr}^f \times \frac{\text{mg}}{\text{sec}} \div \frac{\text{Du}}{\text{Q}} \text{ (line 1)} \\
 & = \boxed{\phantom{000}} \frac{\text{Ci}}{\text{sec}} \text{ Minimum Total Release Rate}
 \end{aligned}$$

\* Assumes measurement taken in plume centerline

#### NOTES:

<sup>a</sup>Iodine activity to noble gas activity ratio. If unknown use 0.3 unless Standby Gas Treatment is in operation (Data Summary Sheet, Section II.D, line 1) then use 0.003.

<sup>b</sup>Obtain  $\frac{\text{Du}}{\text{Q}}$  for iodine (DUOQI) from Figure 5 for atmospheric stability class AB, Figure 13 for class C, Figure 18 for class DE, or Figure 23 for class FG (see Summary Table, Section I, line 6). Use the distance from the release point that the exposure rate measurement was made (Data Summary Sheet, Section III, line 2).

<sup>c</sup>Obtain time correction factor for iodine (TCFI) from Figure 9 using the time of field measurement after shutdown (Data Summary Sheet, Section III, line 1).

<sup>d</sup>Obtain  $\frac{\text{Du}}{\text{Q}}$  for noble gas (DUOQNG) from Figure 7 for atmospheric stability class AB, Figure 14 for class C, Figure 19 for class DE, or Figure 24 for class FG (see Summary Table, Section I, line 6). Use the distance from the release point that the exposure rate measurement was made (Data Summary Sheet, Section III, line 2).

<sup>e</sup>Obtain time correction factor for noble gas (TCFNG) from Figure 8 using the time of the field measurement after shutdown (Data Summary Sheet, Section III, line 1).

<sup>f</sup>Obtain exposure rate from Data Summary Sheet, Section III, line 3.

<sup>g</sup>Obtain wind speed from Summary Table, Section I, line 5.

## FOLLOW-UP DOSE PROJECTIONS

## ATTACHMENT IV, FIGURES

This attachment contains all the figures referenced in this procedure.

FIGURE 1

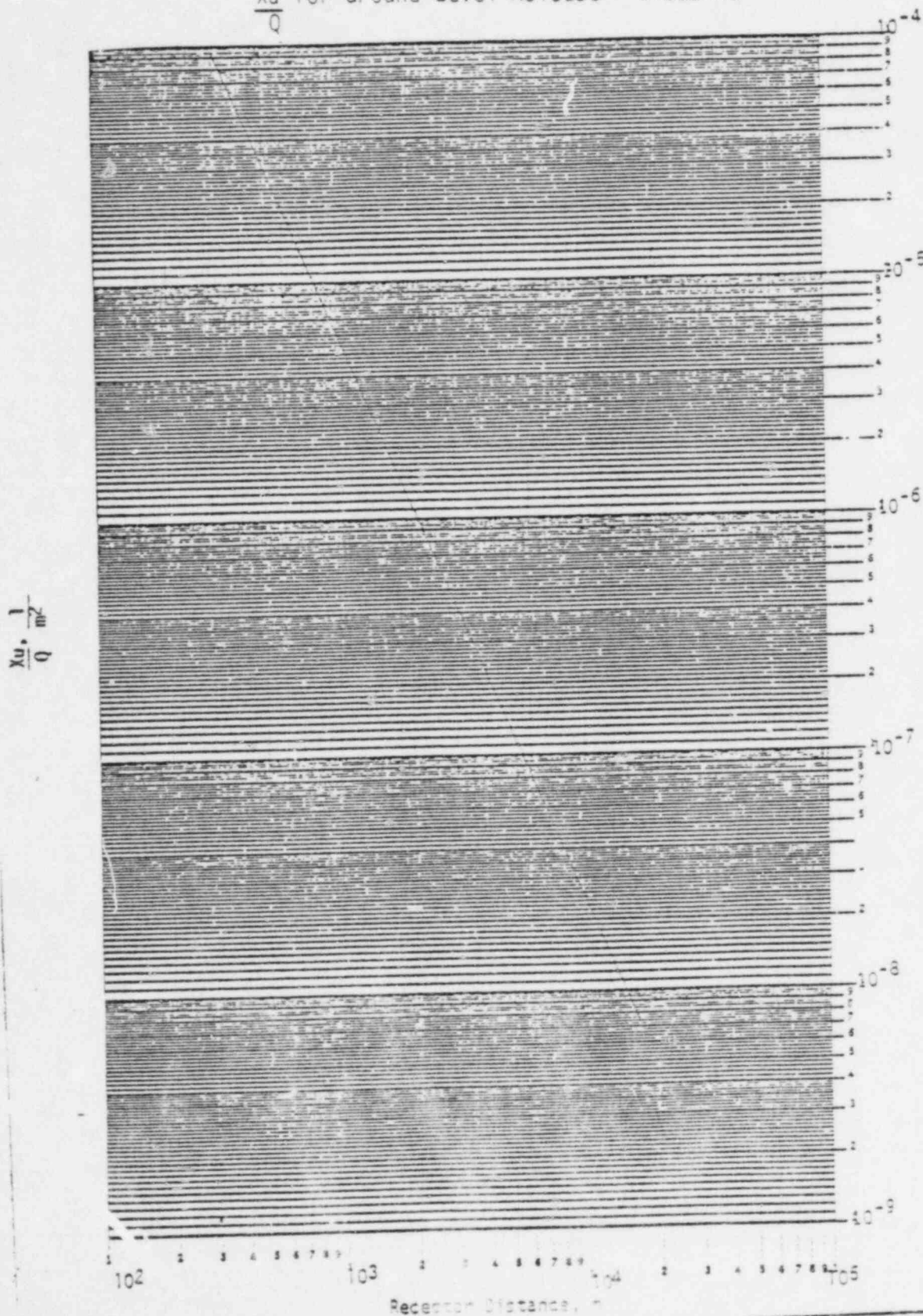
 $\frac{X_u}{Q}$  for Ground Level Release - Class AB

FIGURE 2

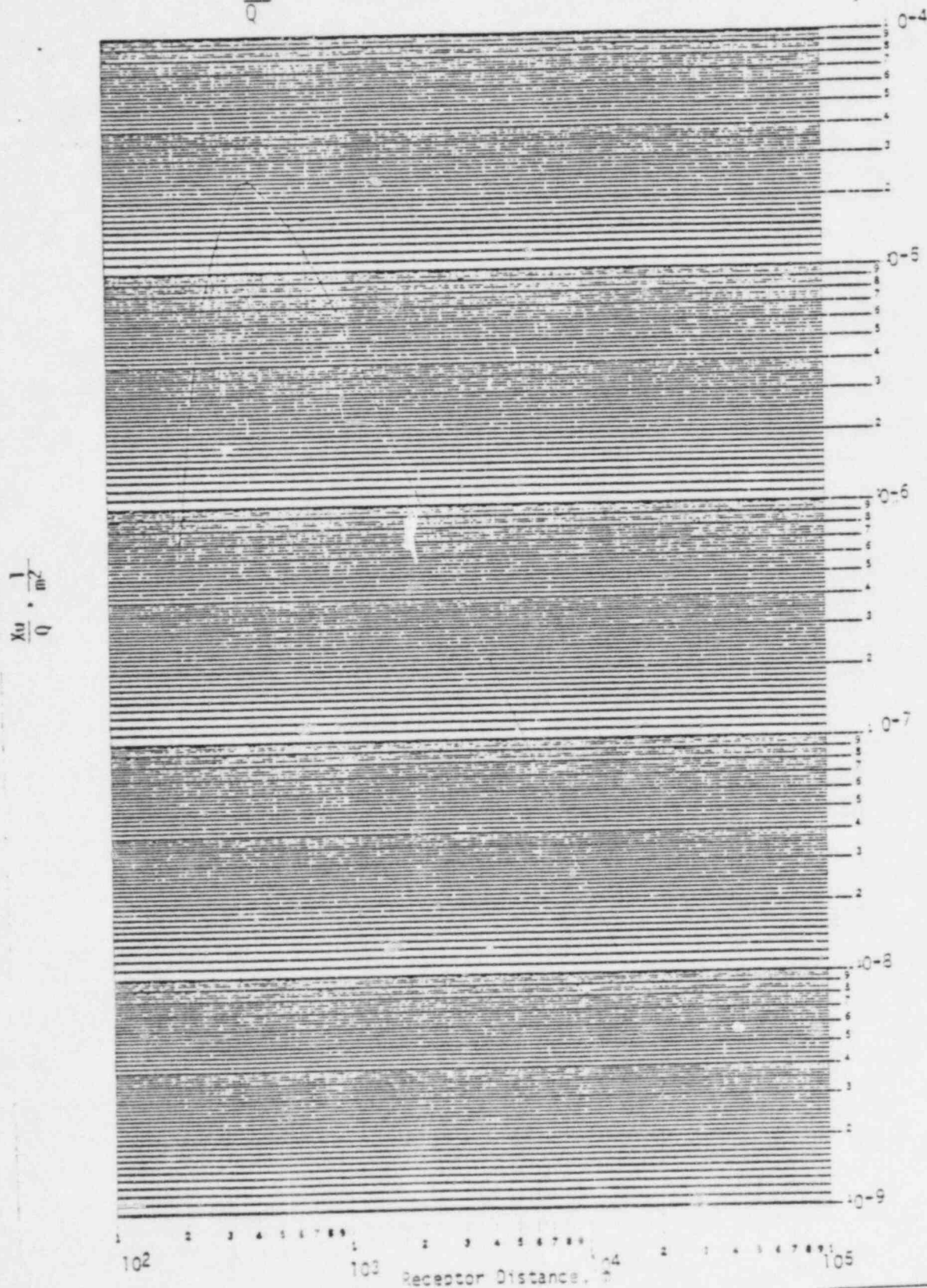
 $\frac{X_u}{Q}$  for Elevated Release - Class AB

FIGURE 3

Whole Body Dose Conversion Factor - Iodine

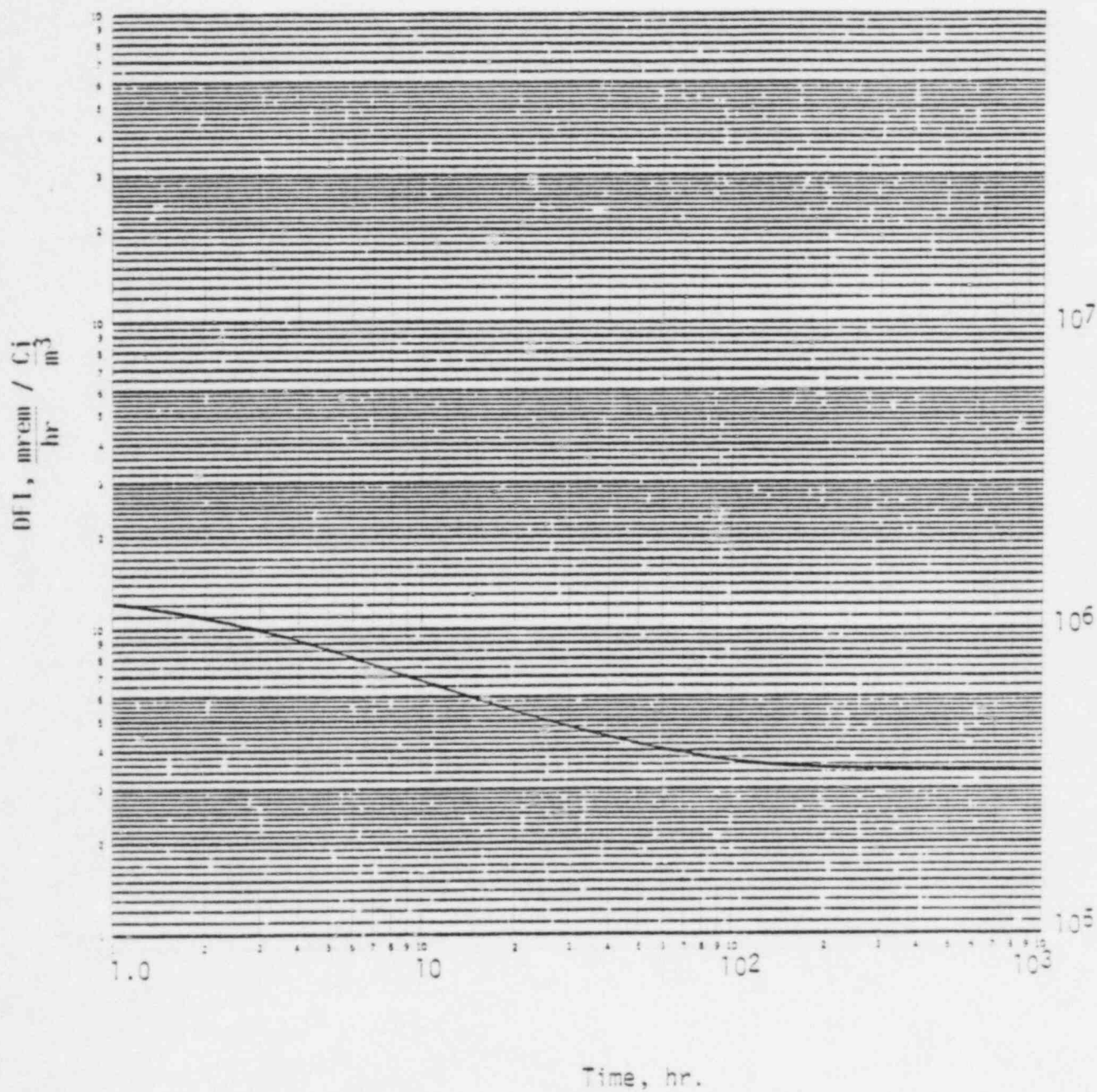


FIGURE 4

Whole Body Dose Conversion Factor - Noble Gas

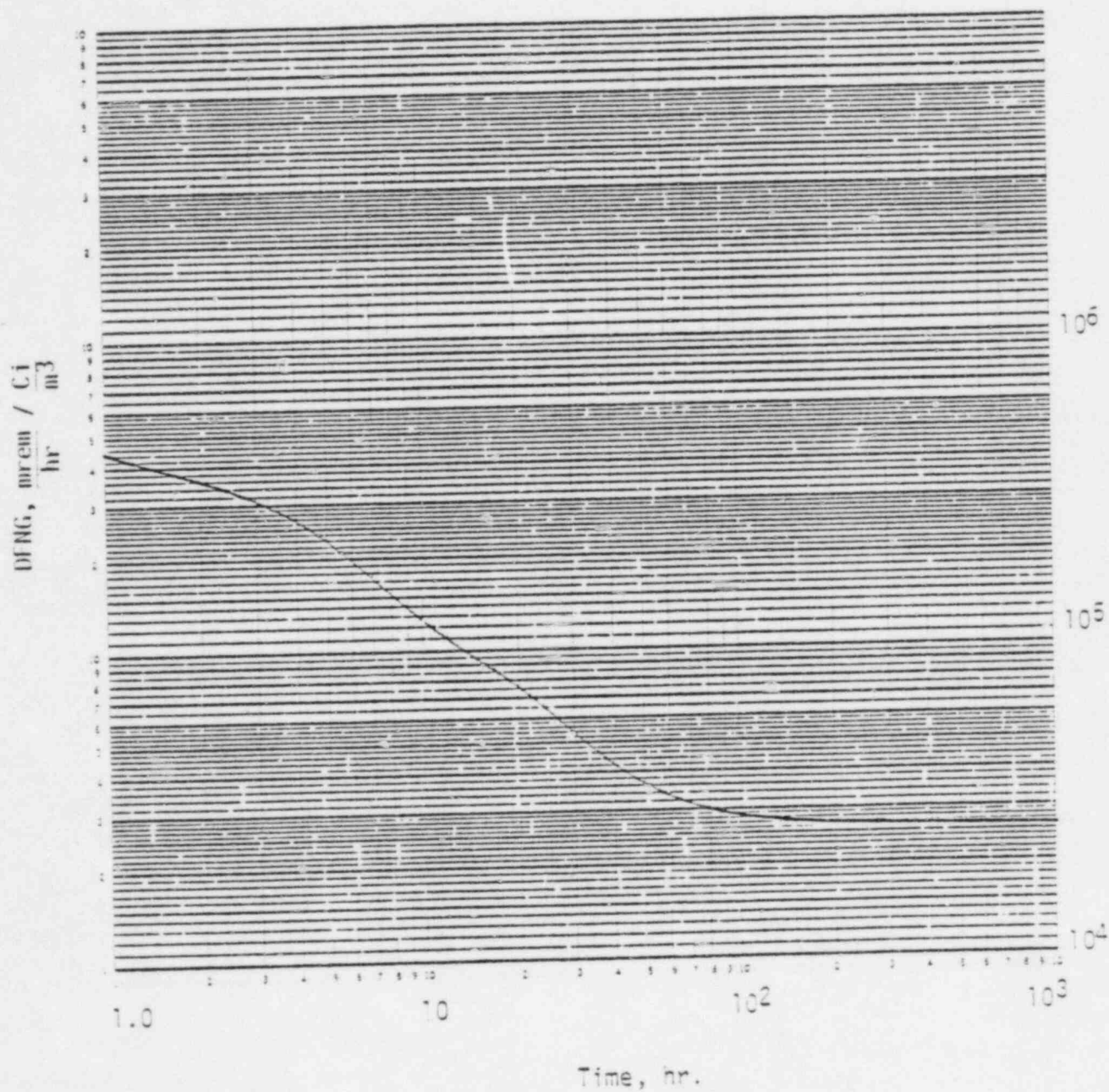


FIGURE 5

$\frac{D_u}{Q}$  for Iodine - Class AB

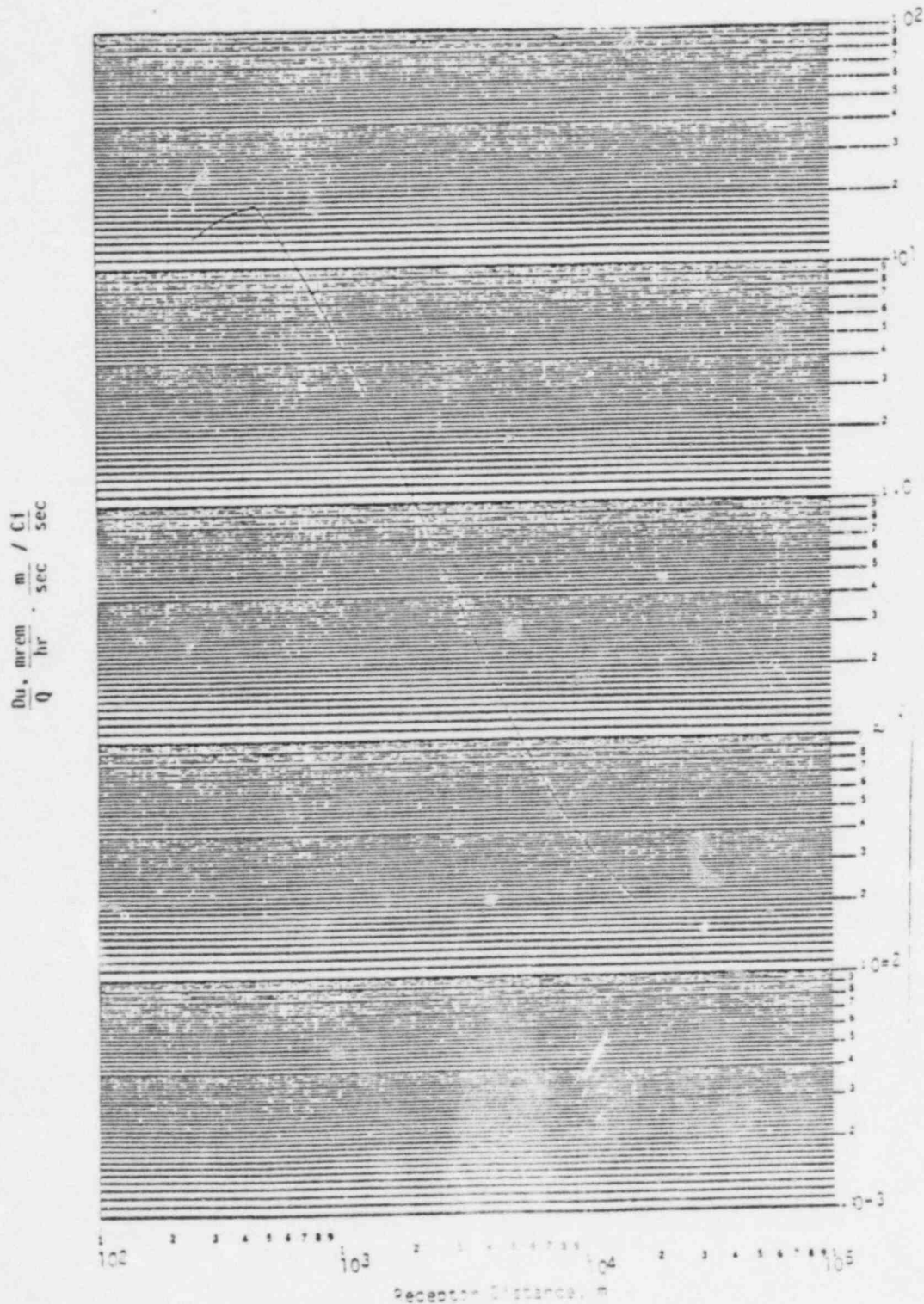


FIGURE 6

Time Correction Factor - Iodine

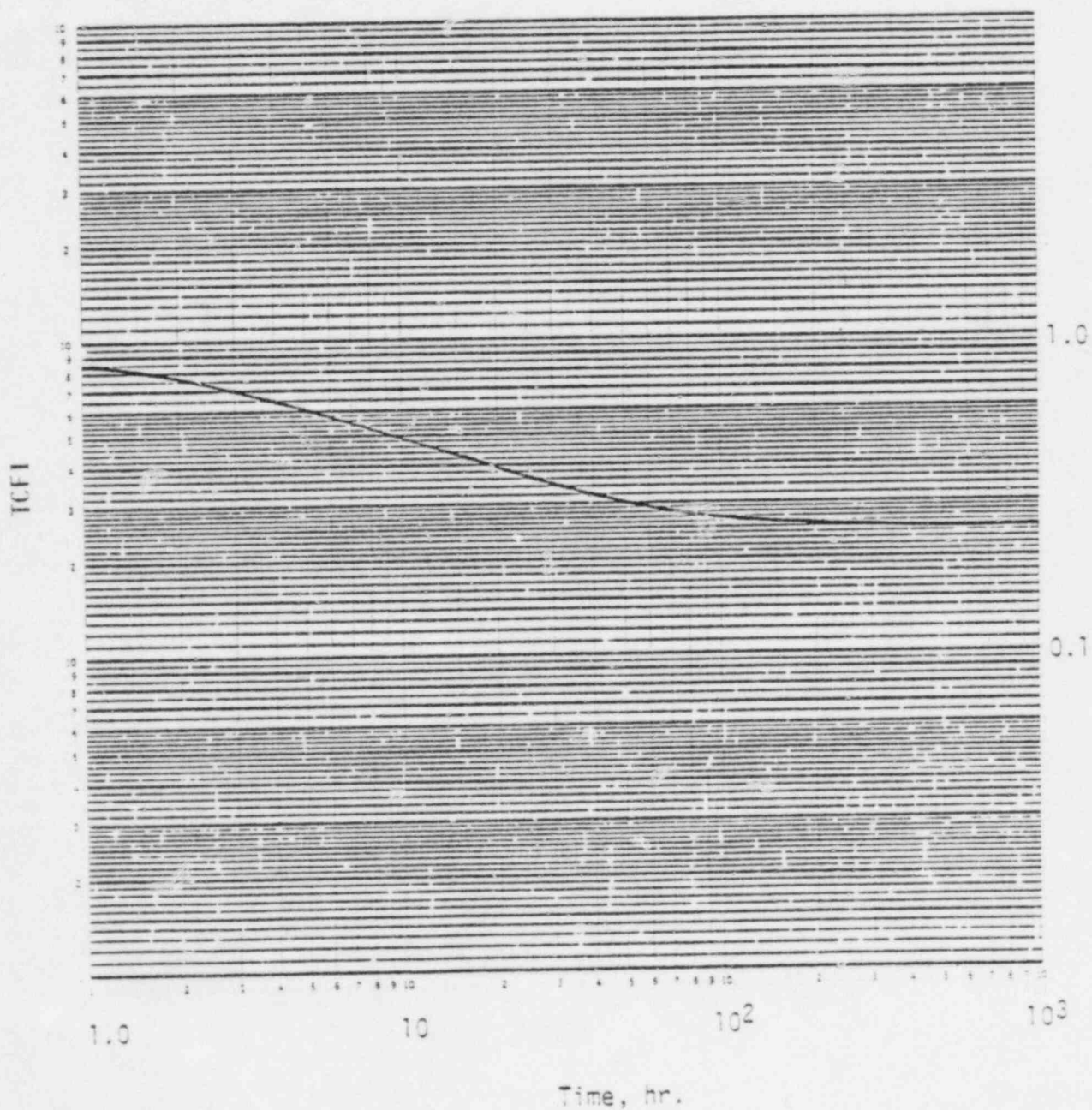


FIGURE 7

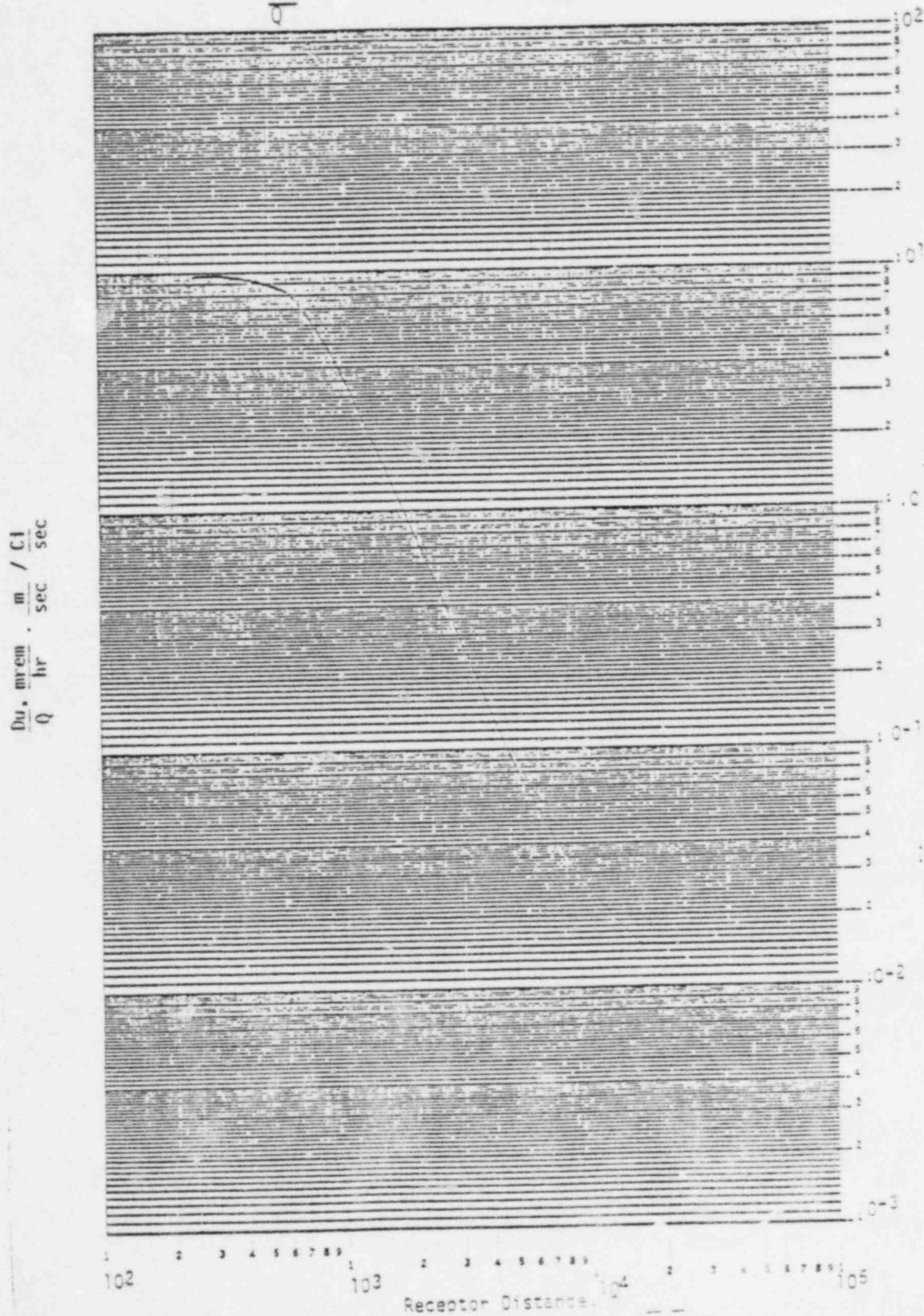
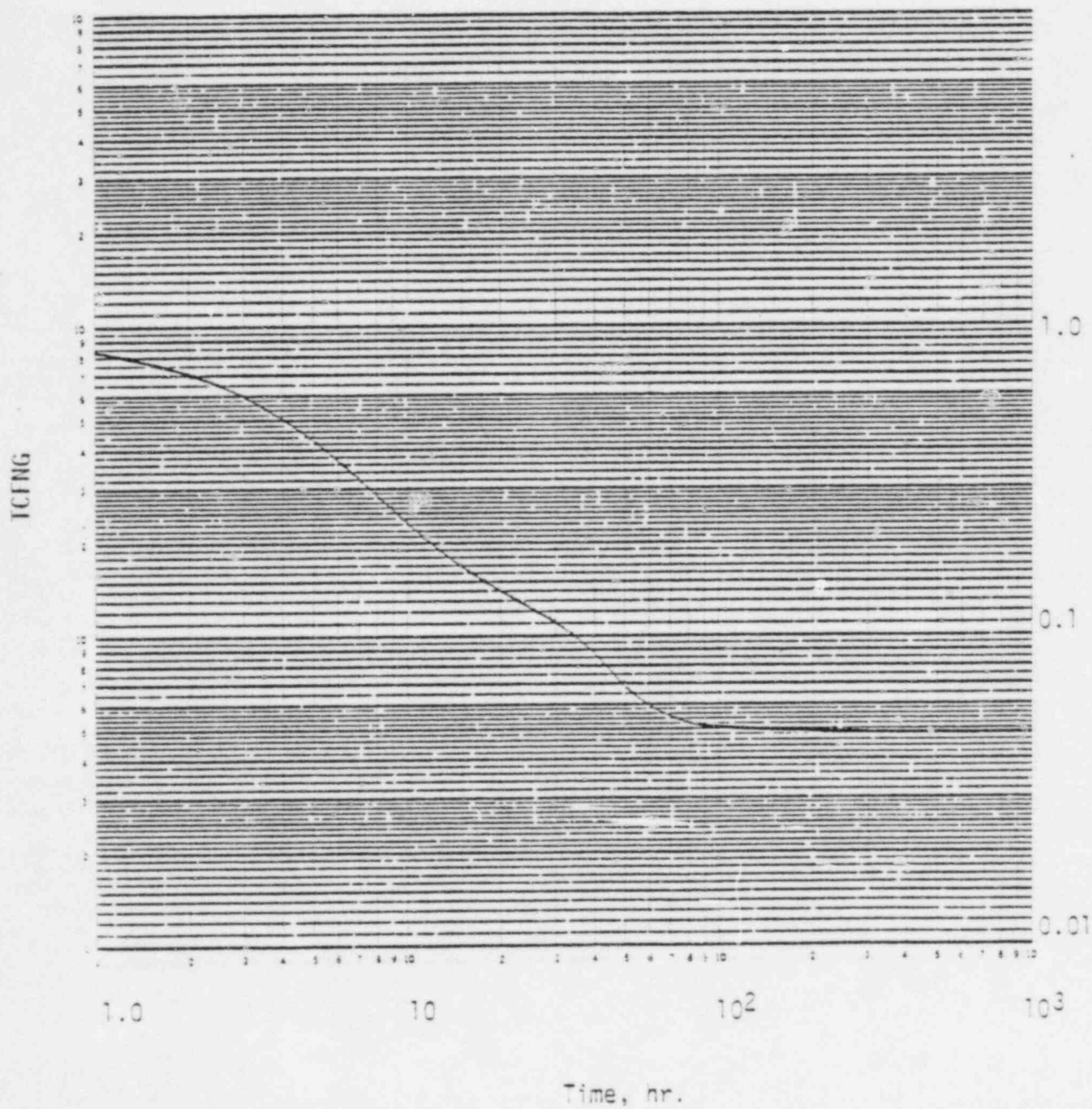
 $\frac{Du}{Q}$  for Noble Gas - Class AB

FIGURE 8

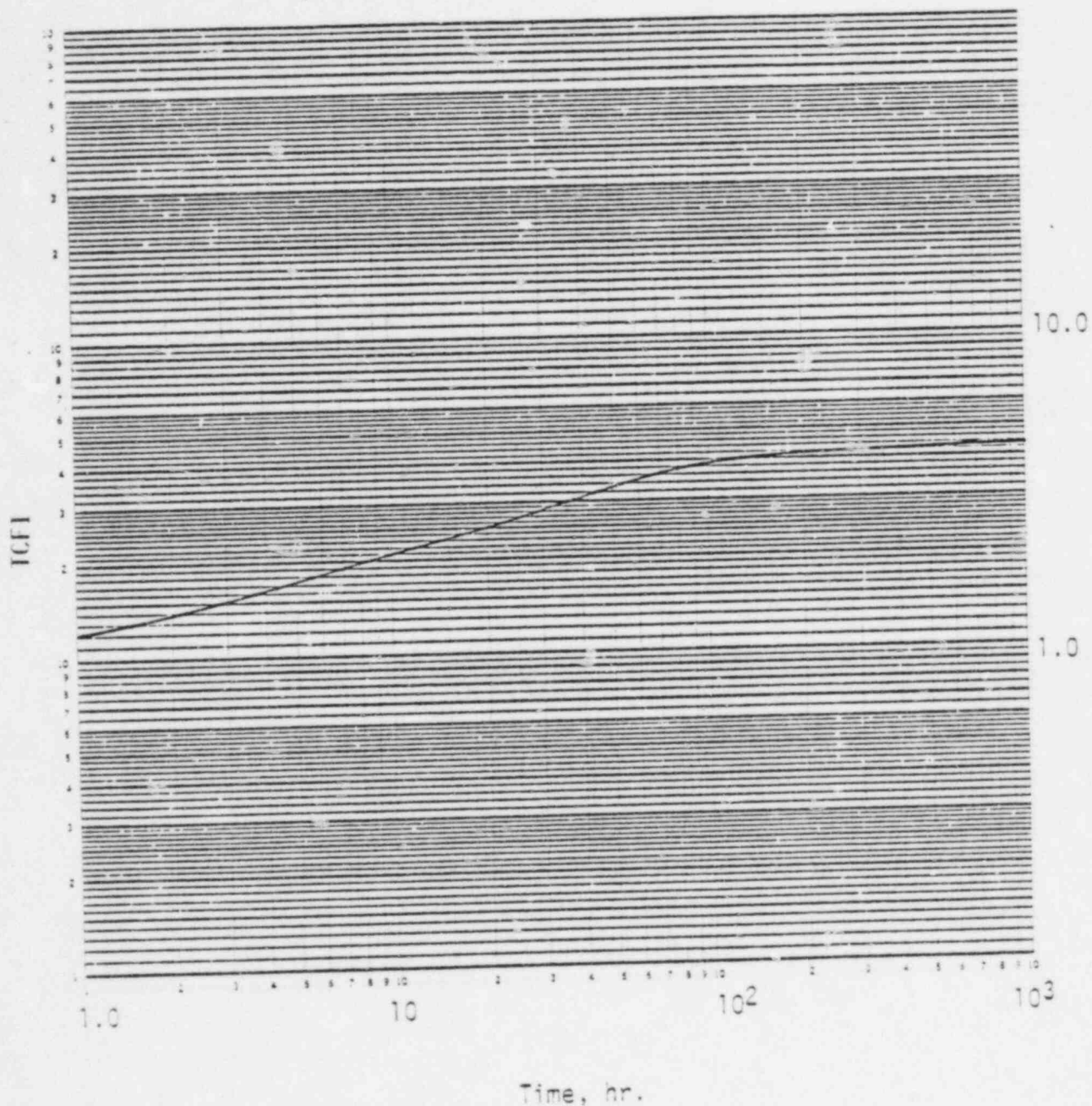
Time Correction Factor - Noble Gas



## FOLLOW-UP DOSE PROJECTIONS

FIGURE 9

Time Correction Factor for Thyroid Dose - Iodine



## FOLLOW-UP DOSE PROJECTIONS

FIGURE 10

Plume Width - Class AB

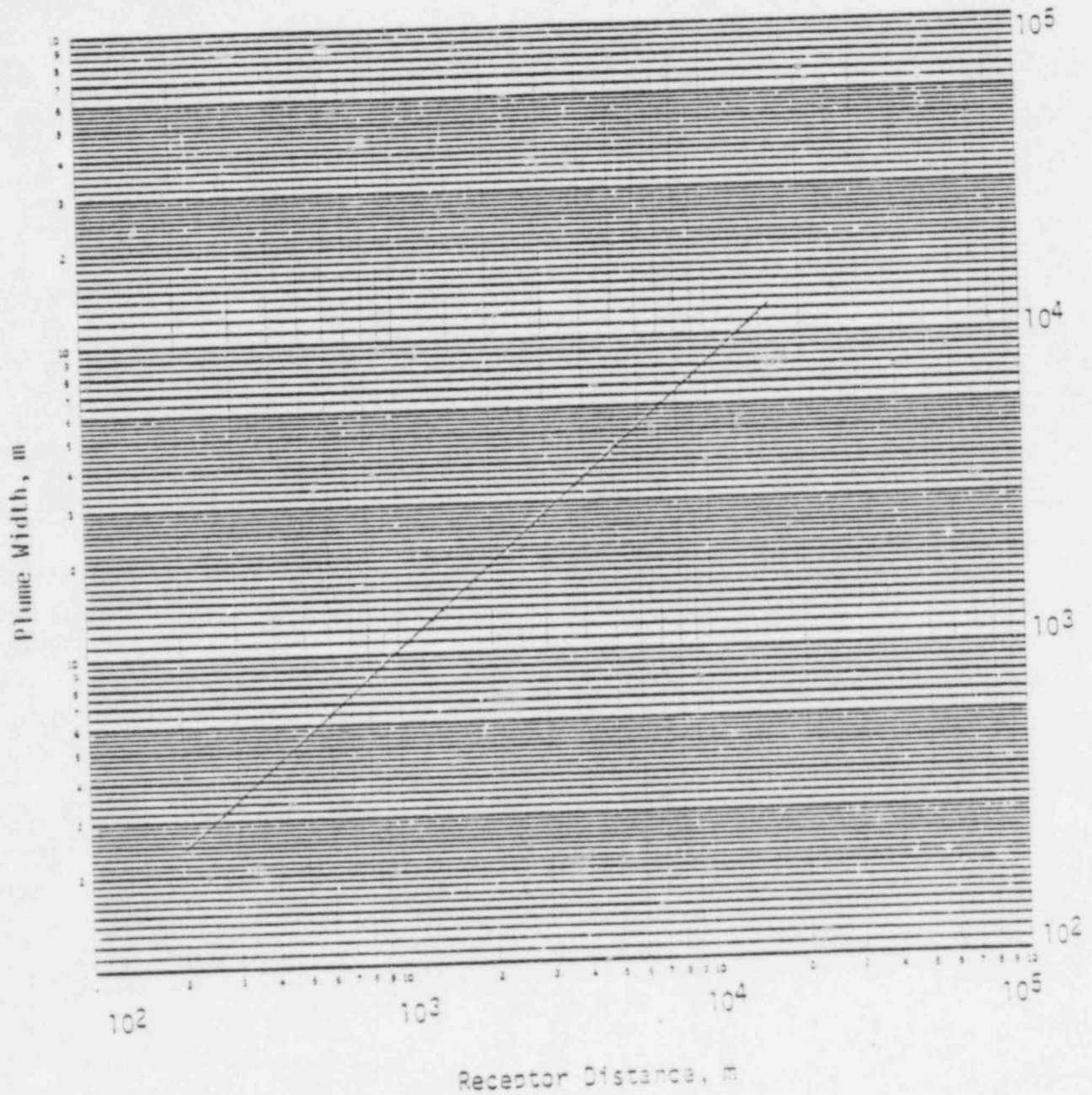


FIGURE 11

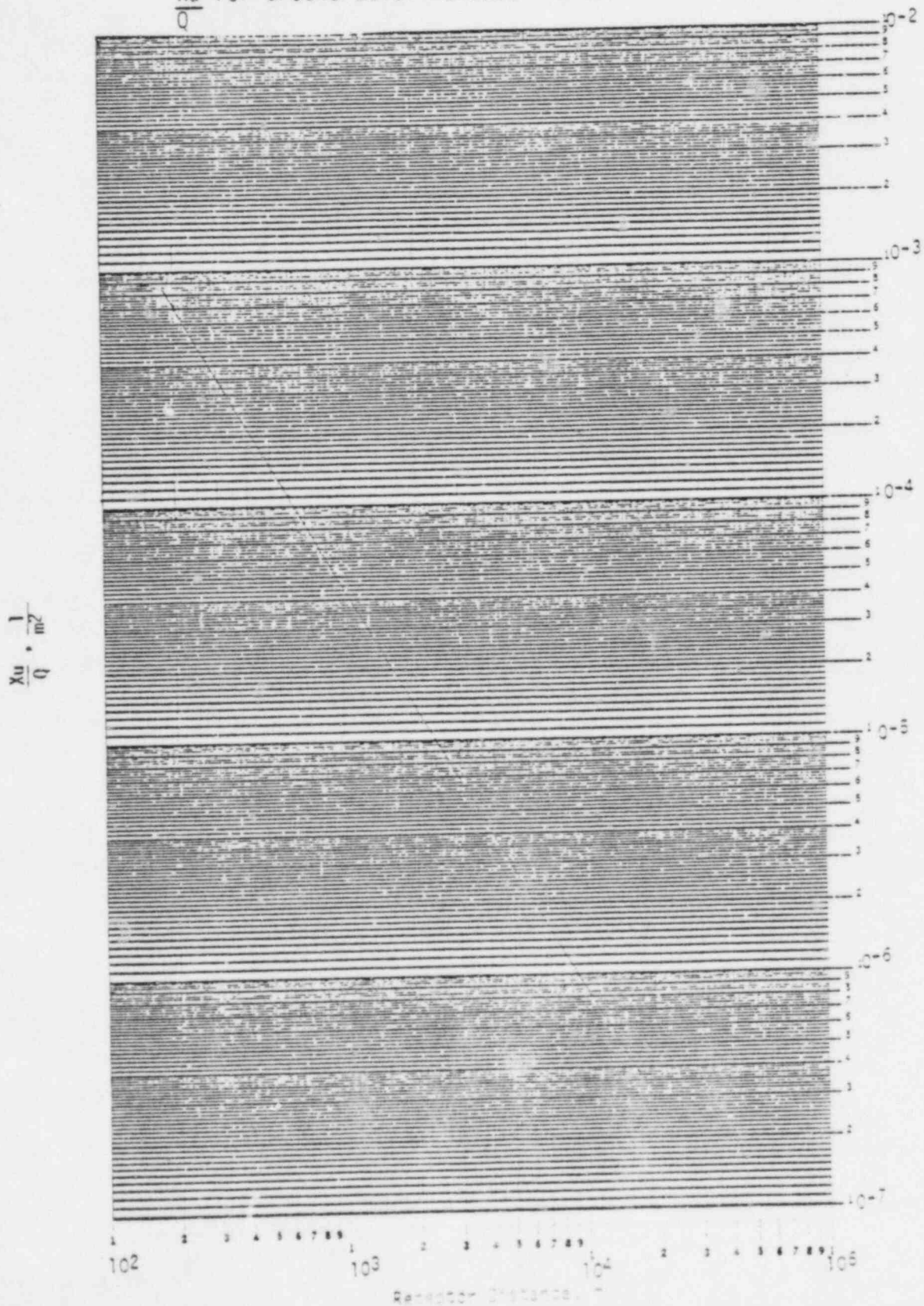
 $\frac{X_u}{Q}$  for Ground Level Release - Class C

FIGURE 12

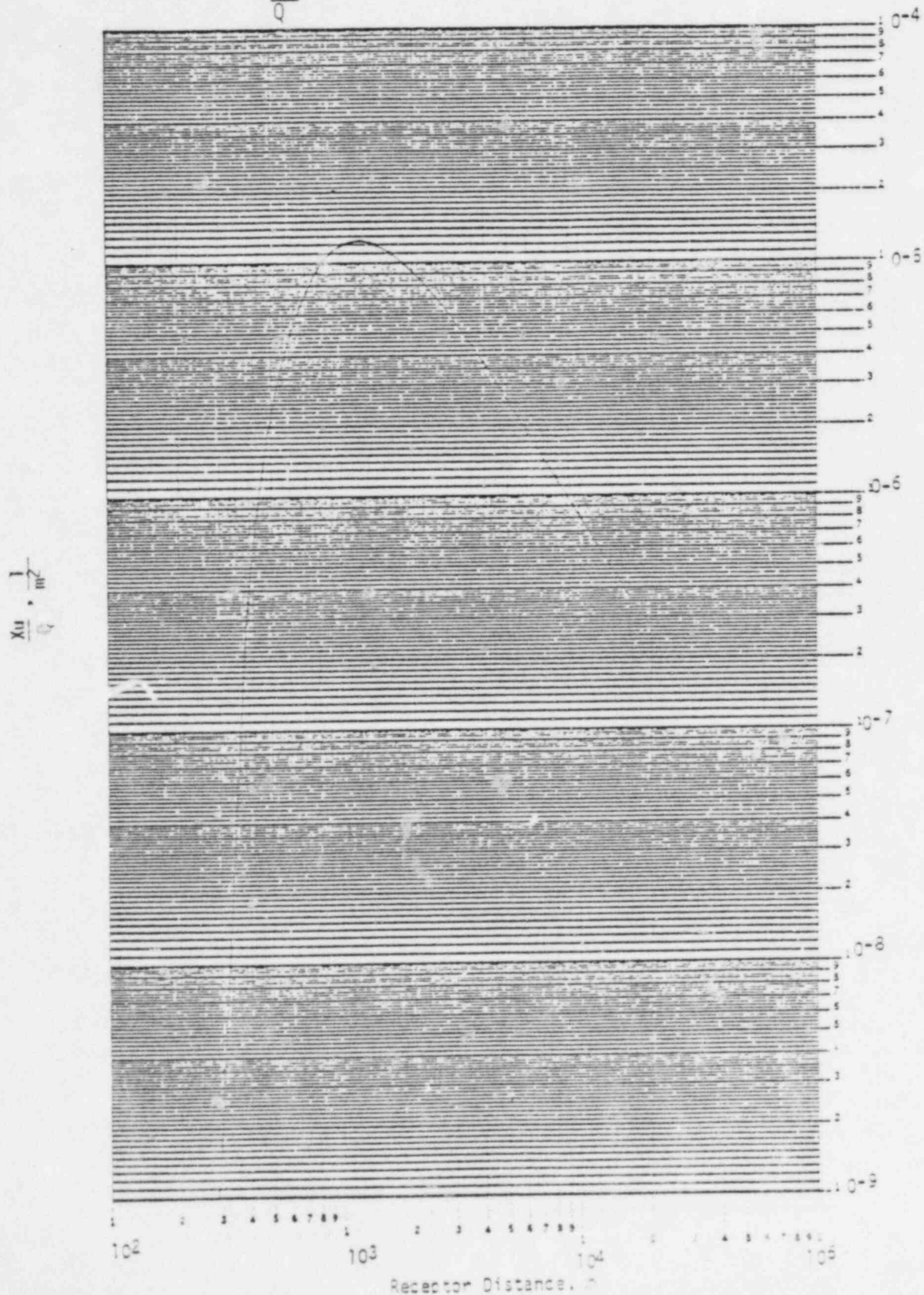
 $\frac{X_u}{Q}$  for Elevated Release - Class C

FIGURE 13

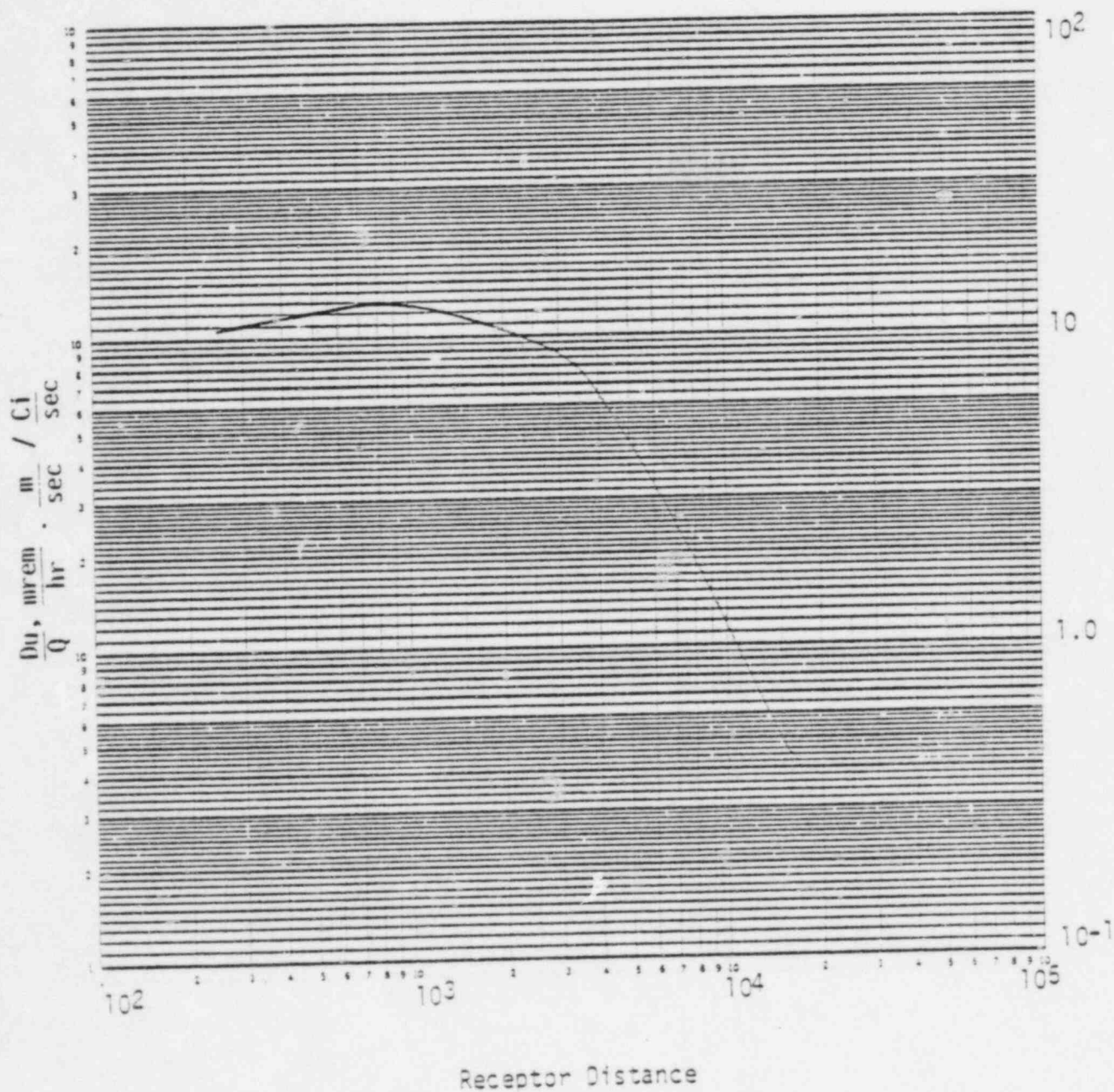
 $\frac{D_u}{Q}$  for Iodine - Class C

FIGURE 14

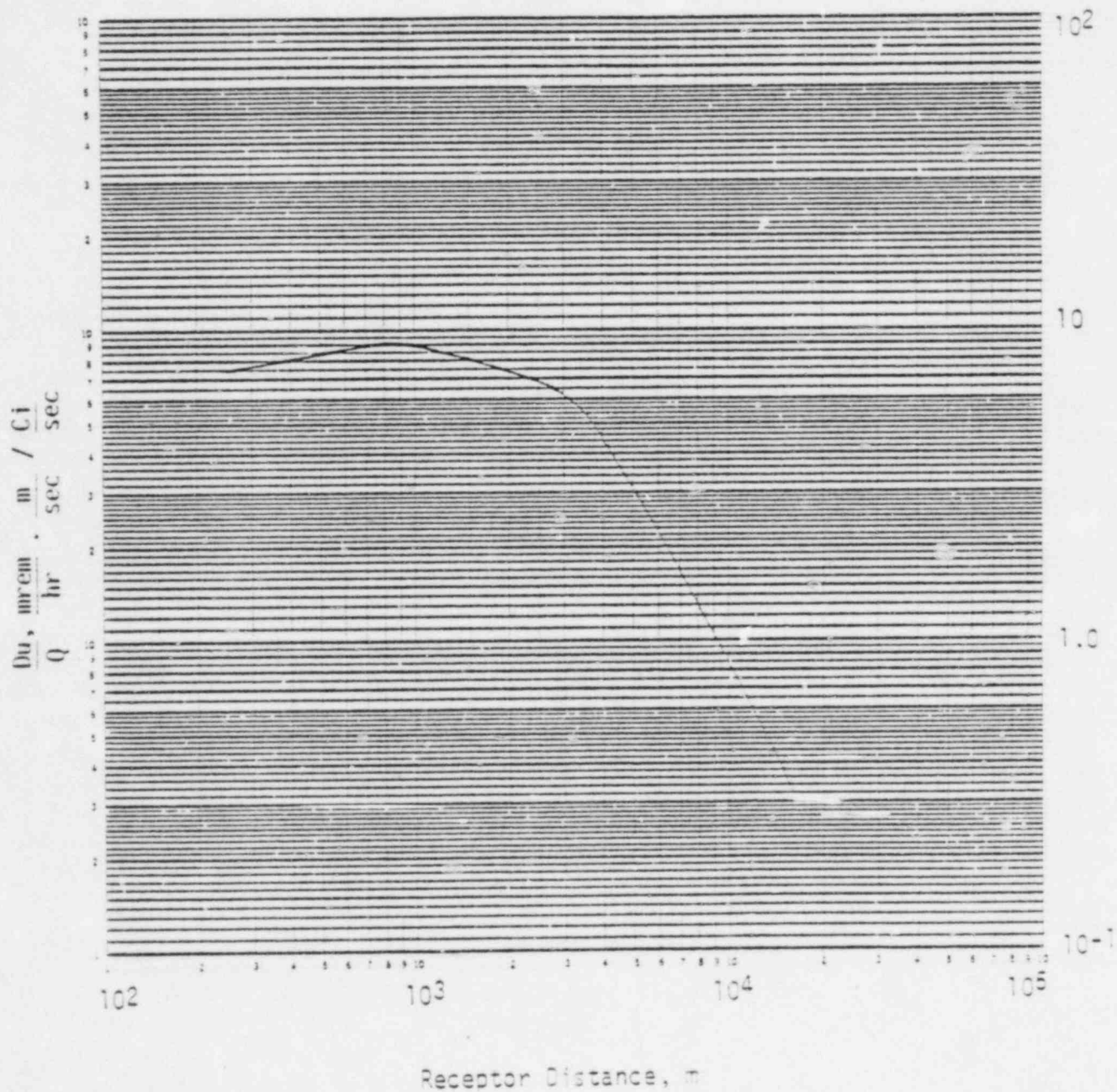
 $\frac{D_u}{Q}$  for Noble Gas - Class C

FIGURE 15

Plume Width - Class C

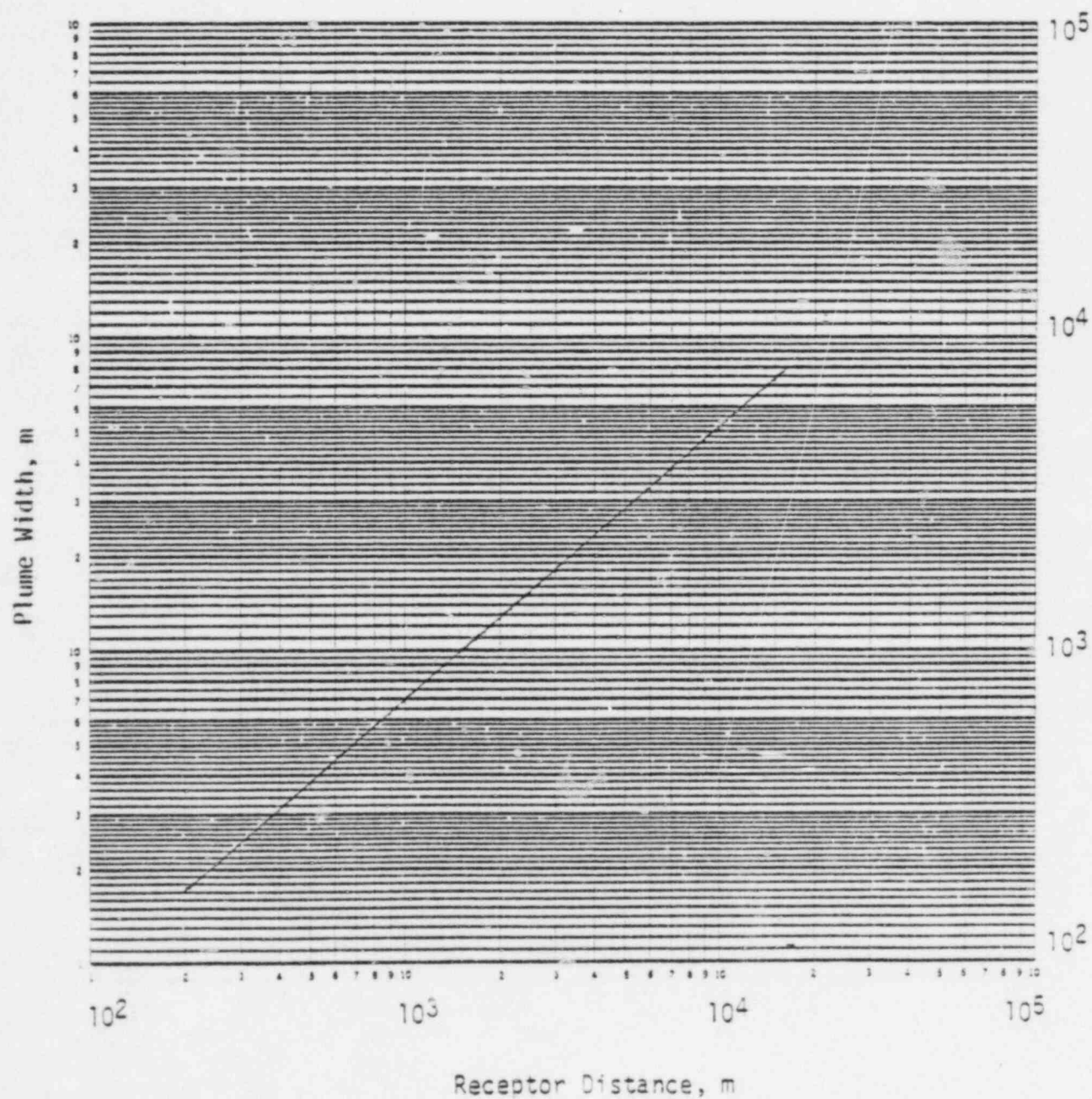


FIGURE 16  
 $\frac{X_u}{Q}$  for Ground Level Release - Class DE

$$\frac{X_u}{Q} \cdot \frac{1}{m^2}$$

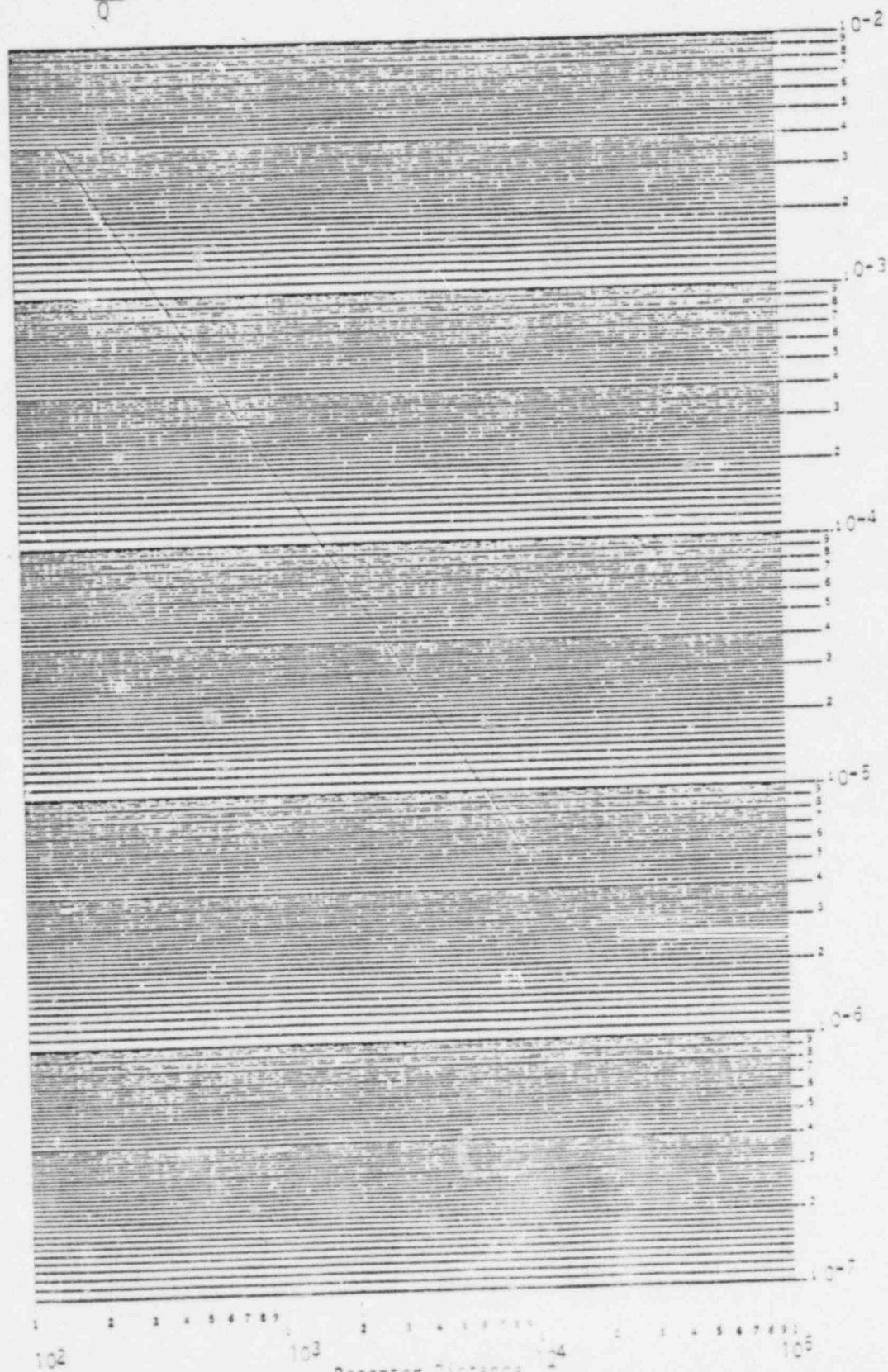


FIGURE 17

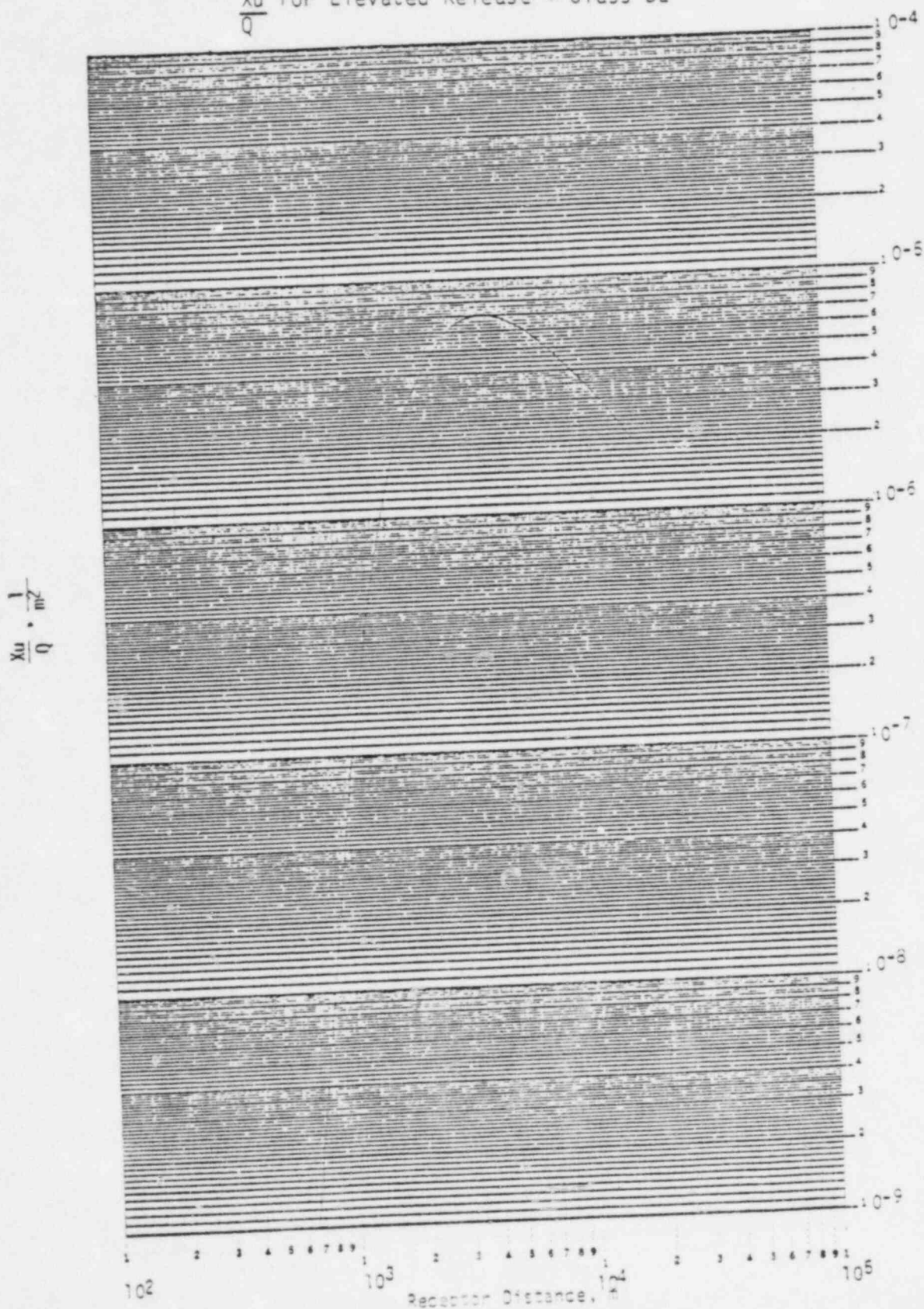
 $\frac{X_u}{Q}$  for Elevated Release - Class DE

FIGURE 18

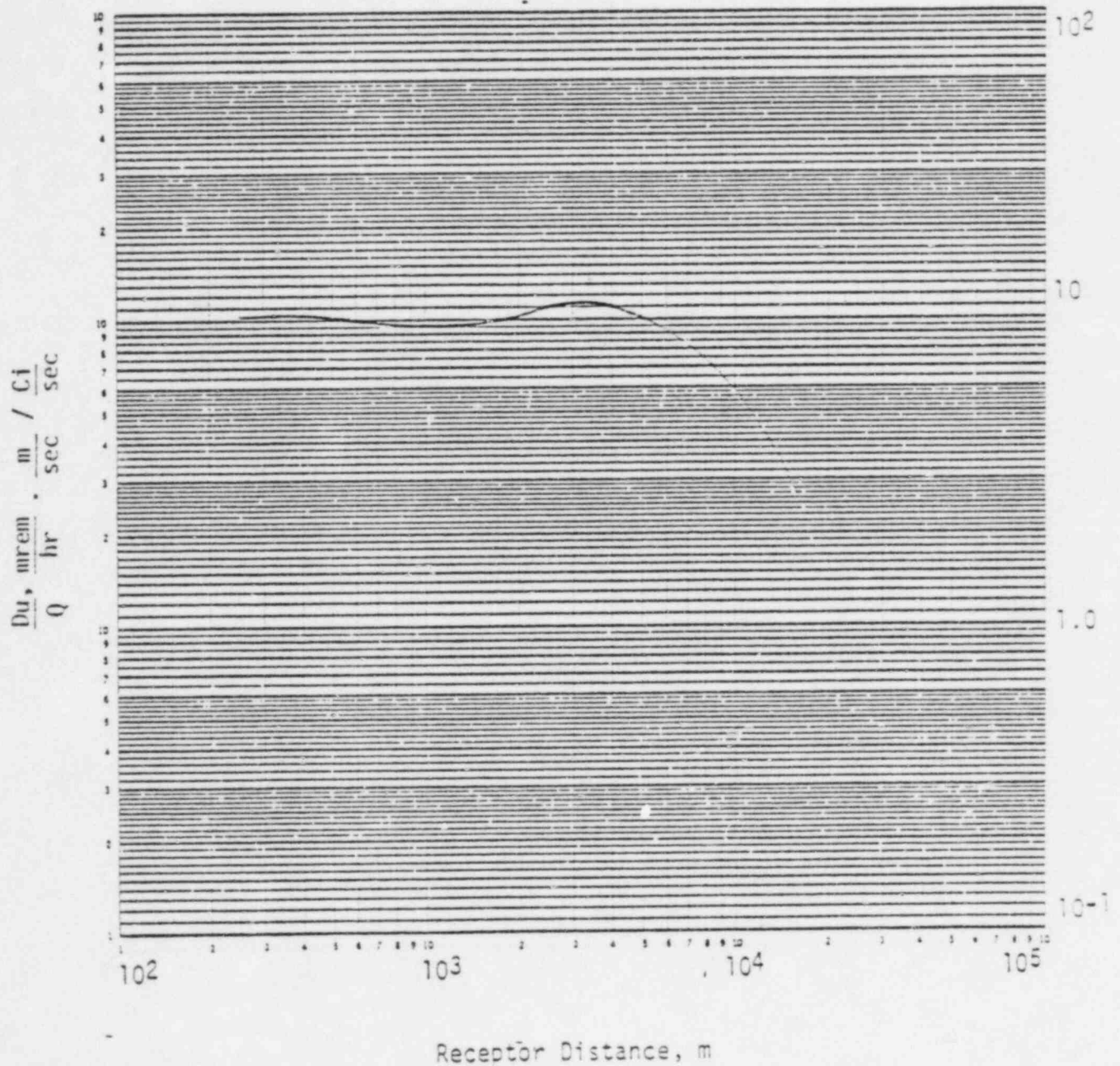
 $\frac{D_u}{Q}$  for Iodine - Class DE

FIGURE 19

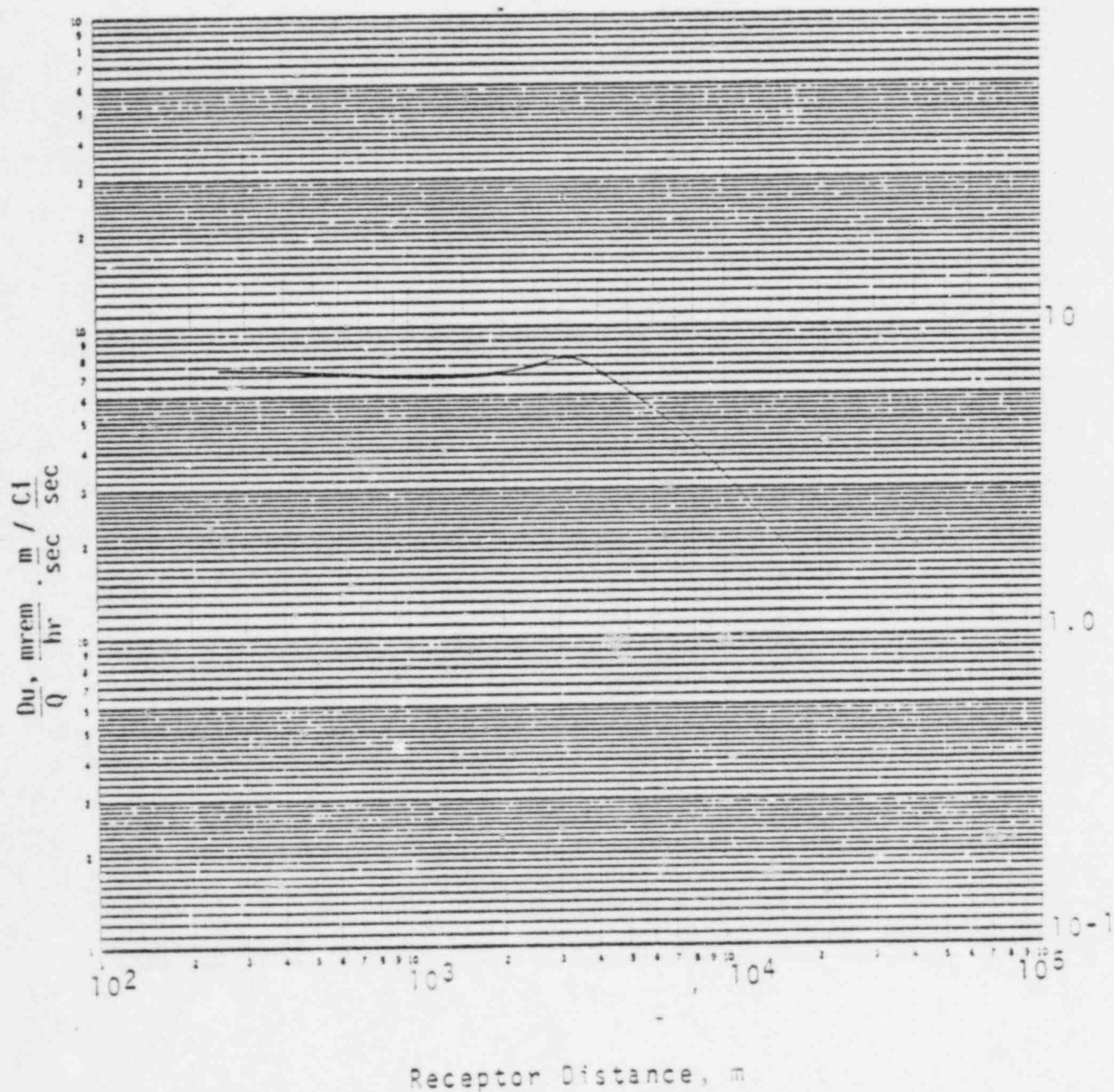
 $\frac{D_u}{Q}$  for Noble Gas - Class DE

FIGURE 20

Plume Width - Class DE

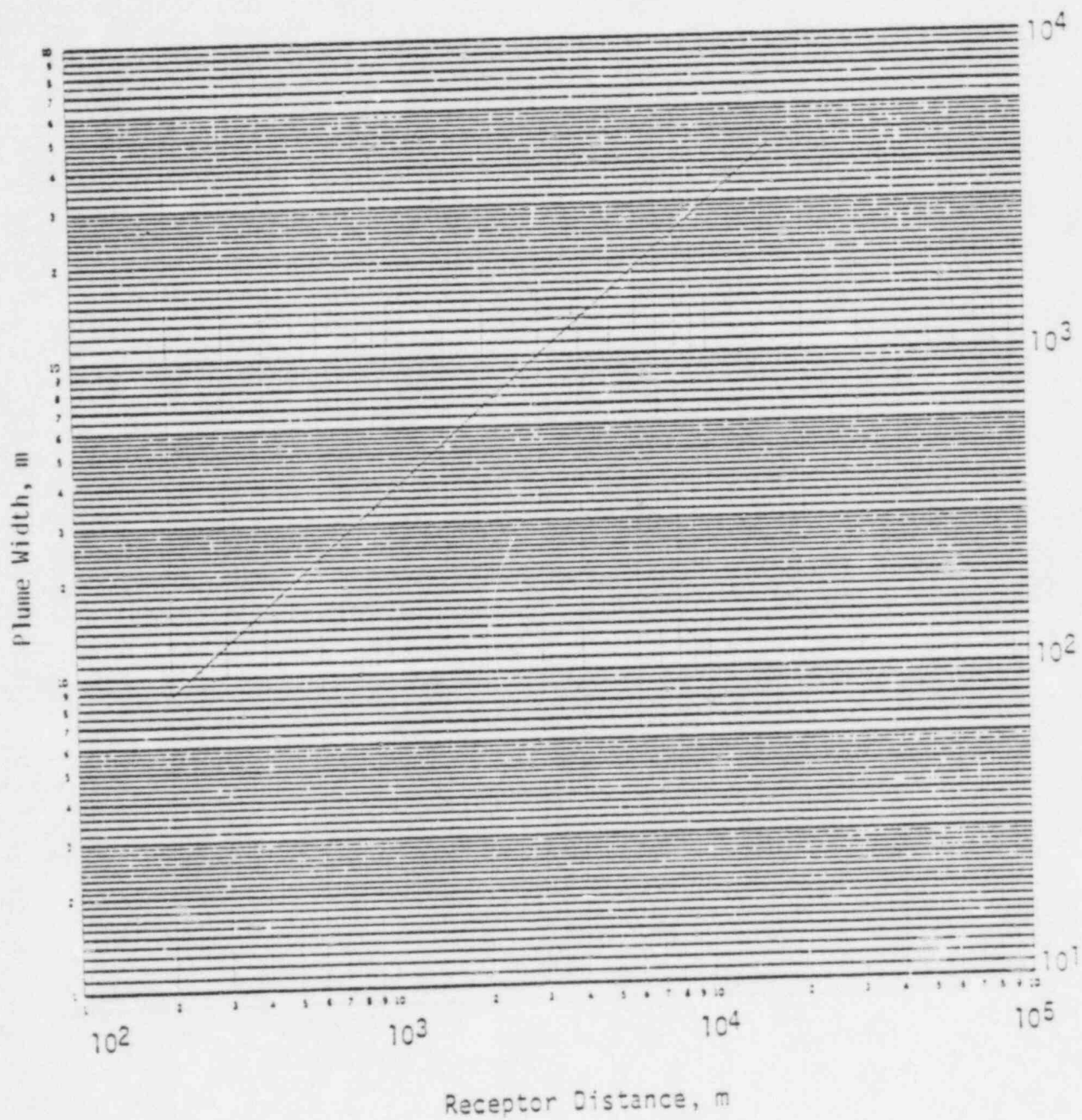


FIGURE 21

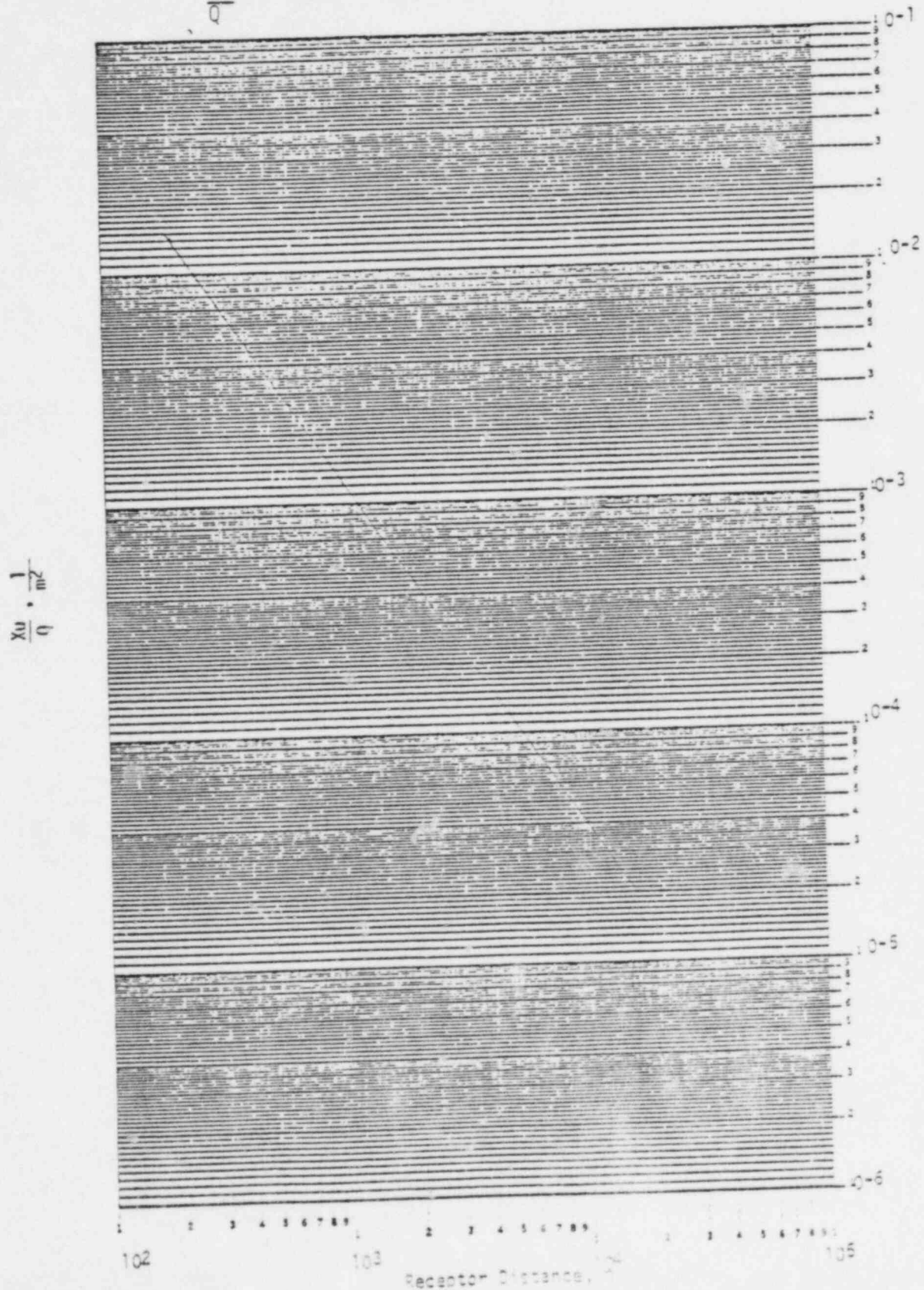
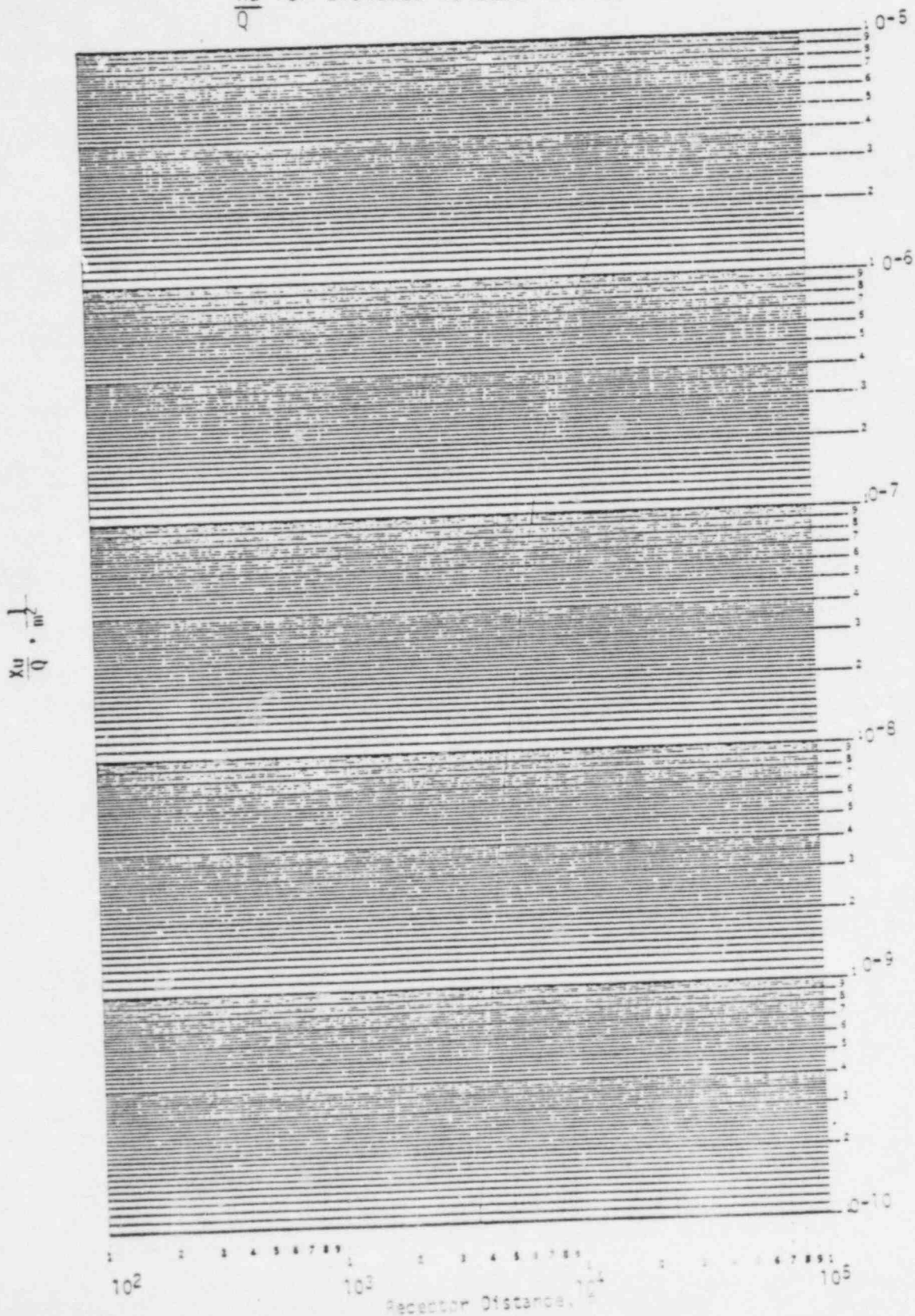
 $\frac{X_u}{Q}$  for Ground Level Release - Class FG

FIGURE 22

 $\frac{X_u}{Q}$  for Elevated Release - Class FG

## FOLLOW-UP DOSE PROJECTIONS

FIGURE 23

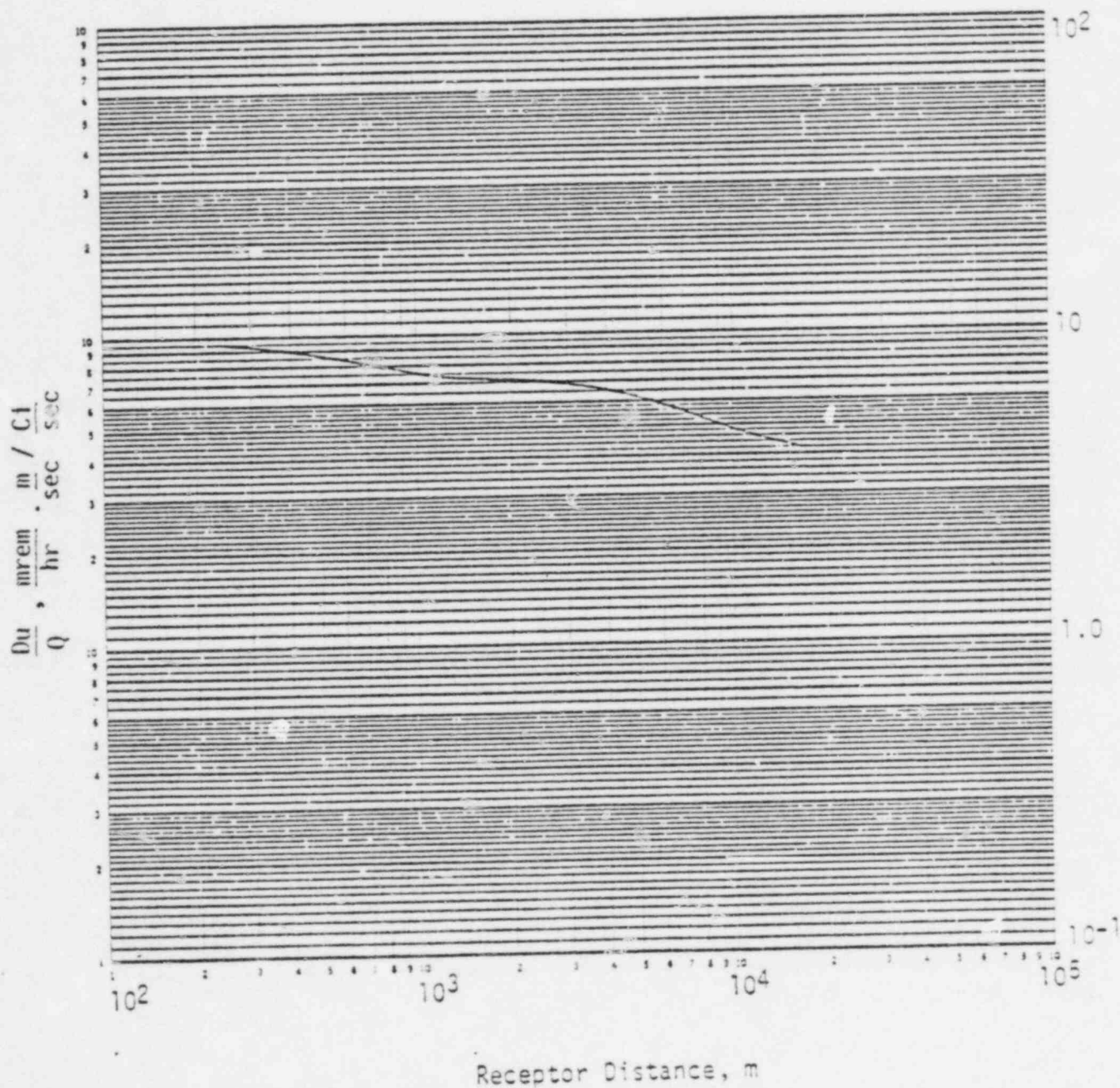
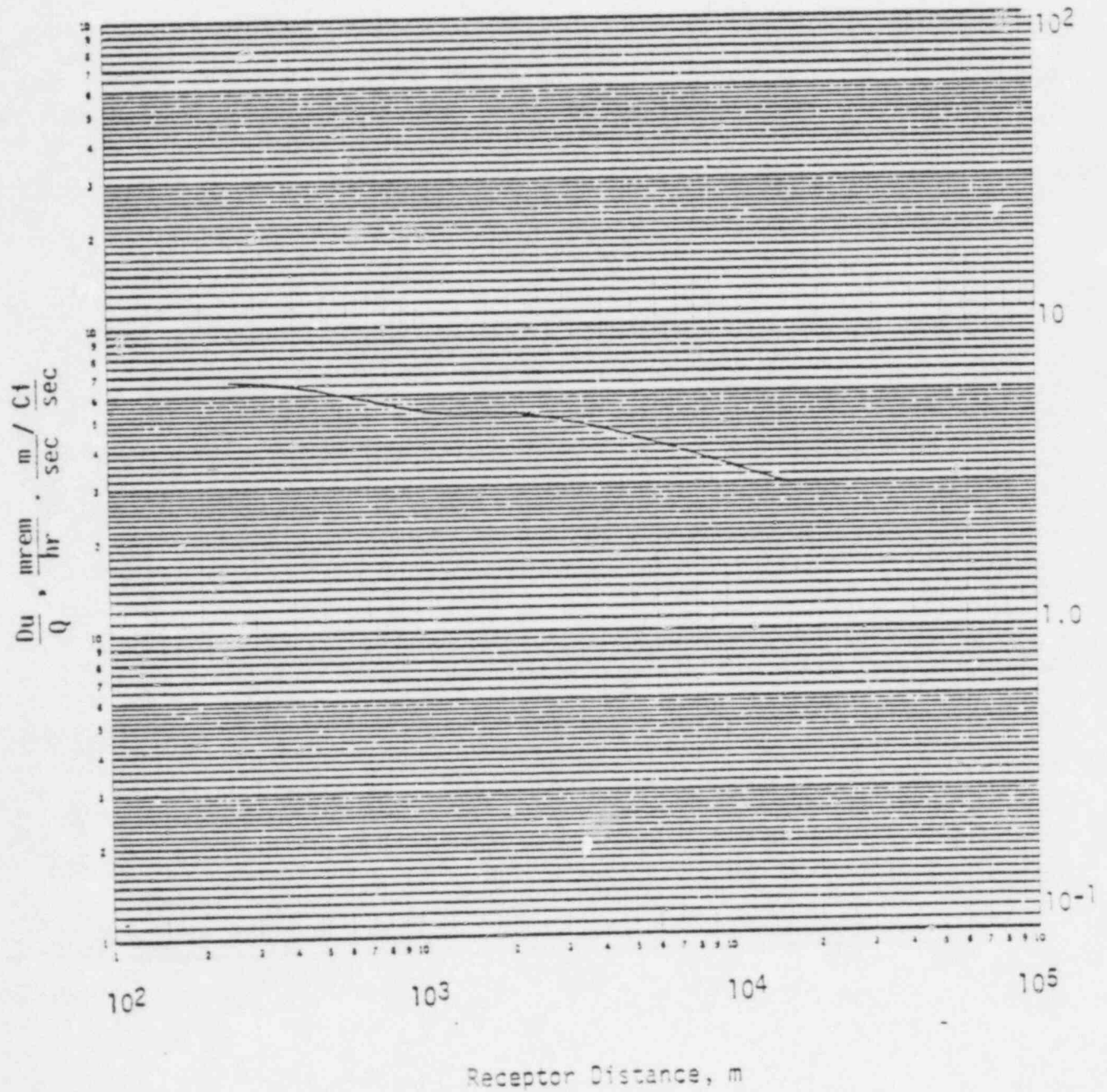
 $\frac{Du}{Q}$  for Iodine - Class FG

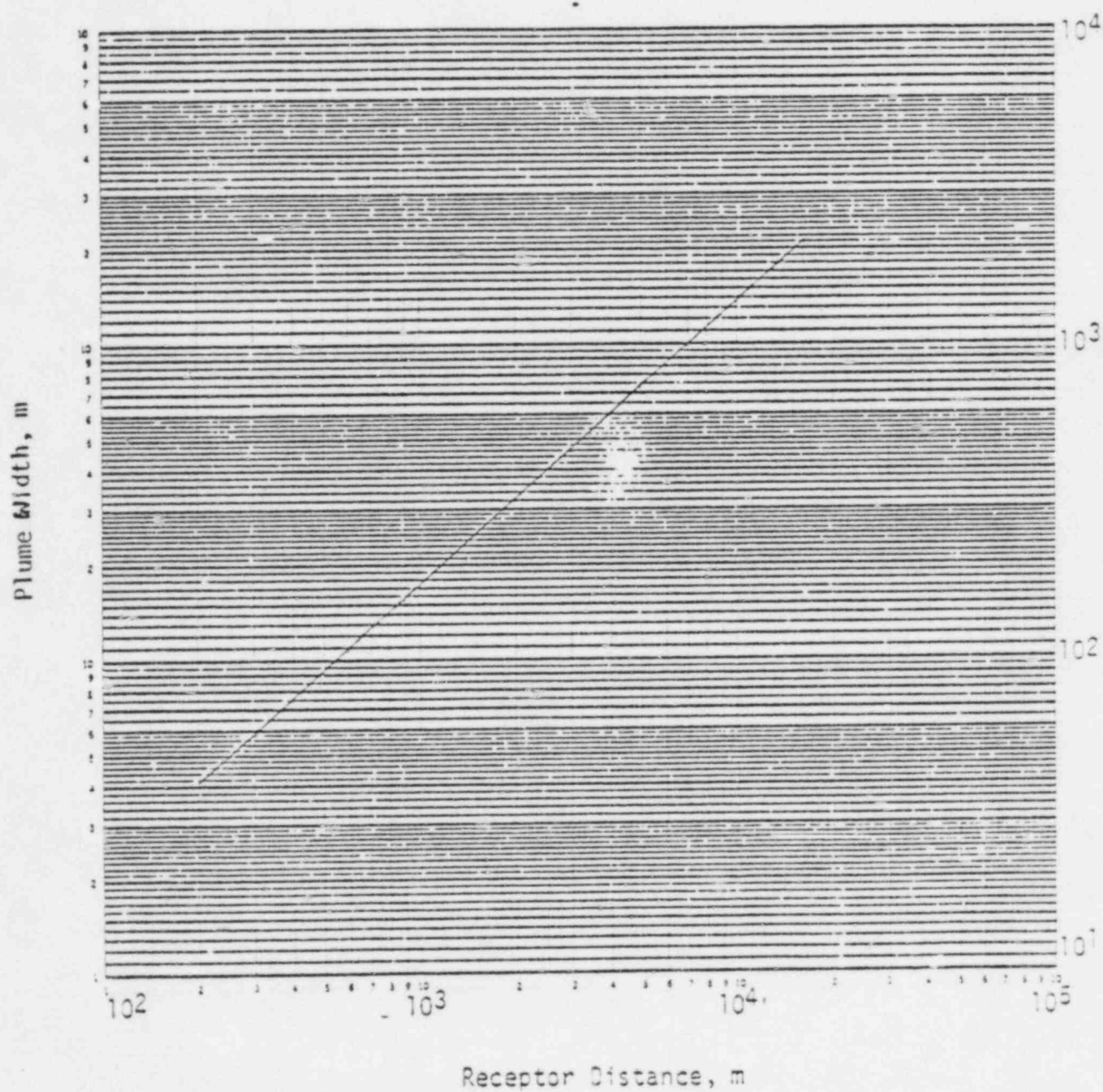
FIGURE 24

 $\frac{D_u}{Q}$  for Noble Gas - Class FG

## FOLLOW-UP DOSE PROJECTIONS

FIGURE 25

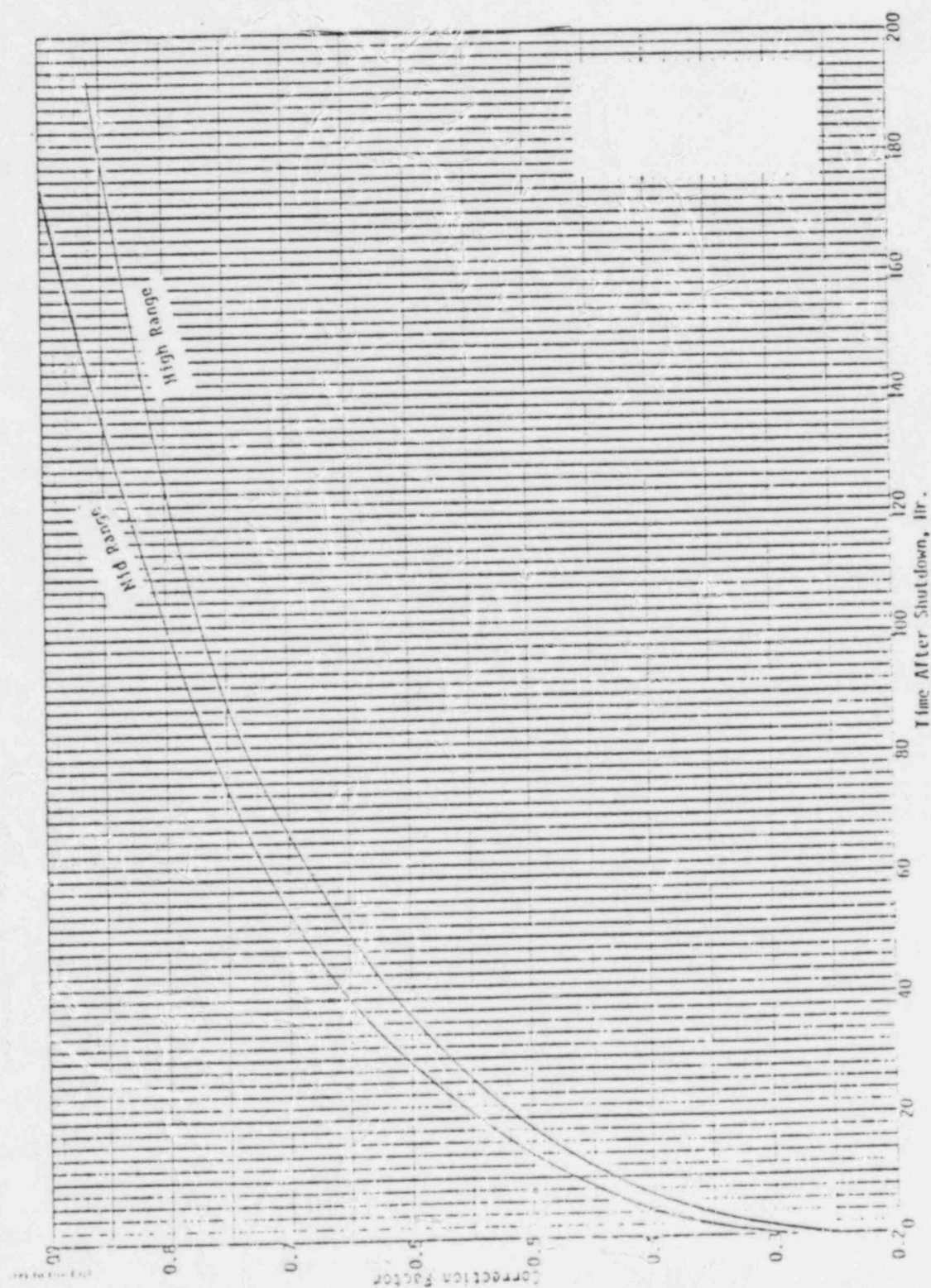
Plume Width - Class FG



## FOLLOW-UP DOSE PROJECTIONS

FIGURE 26

Monitor Response Correction Factor



EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 6.4
EMERGENCY PREPAREDNESS COMMUNICATIONS	Page 1 of 11
TESTING	Revision 3
	Date 3/19/83

## 1.0 PURPOSE

This procedure defines the requirements for emergency preparedness communications systems checks to be conducted on a periodic basis as defined in 10CFR50 Appendix E.

## 2.0 APPLICABILITY

This procedure applies to the emergency communications systems that are installed at both the DAEC and at the IE Tower which are associated with emergency preparedness response efforts.

## 3.0 RESPONSIBILITIES

### 3.1 Emergency Planning Coordinator

- 3.1.1 Ensure communications checks are performed as assigned in Section 4.0
- 3.1.2 Verify satisfactory completion of the communications checks conducted on a periodic basis, as defined in Attachments 1 through 4.

### 3.2 STA Coordinator

- 3.2.1 Verify that emergency preparedness communications systems checks are completed as assigned.
- 3.2.2 Coordinate with the Emergency Planning Coordinator, as required, to insure satisfactory completion of the communications systems checks.

### 3.3 Security Supervisor

- 3.3.1 Verify that emergency preparedness communications systems checks are completed as assigned.

## 4.0 INSTRUCTIONS

- 4.1 The following communications systems shall be checked and verified operable at the specified frequency.

- 4.1.1 Completion of monthly communications checks shall be documented on Attachments 1 and 2.

The following systems or circuits are included:

- a) NRC ENS
- b) NRC HPN

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 6.4
EMERGENCY PREPAREDNESS COMMUNICATIONS	Page 2 of 11
TESTING	Revision 3
	Date 3/19/83

- c) PBX and Centrix connections to:
- (1) Office of Disaster Services
  - (2) Linn County Sheriff
  - (3) Benton County Sheriff

4.1.2 Completion of the quarterly communications checks shall be documented on Attachment 3, "Quarterly DAEC Emergency Communications Checks".

The following systems or circuits are included:

4.1.2.1 Dedicated telephone circuits between:

- (a) Control Room and  
Technical Support Center  
Access Control  
Security Control Point  
Emergency Operations Facility
- (b) Technical Support Center and  
Control Room  
Access Control  
Security Control Point  
Emergency Operations Facility
- (c) Access Control and  
Control Room  
Technical Support Center  
Security Control Point
- (d) Security Control Point and  
Control Room  
Technical Support Center  
Access Control

4.1.2.2 Operations Radio between:

- (a) Control Room (base station)
- (b) Technical Support Center (console)
- (c) Access Control (console)
- (d) Site Boundary (portable radio)

4.1.2.3 Security/Radiological Survey Radio between:

- (a) Ten (10) mile radius (portable radio)
- (b) Technical Support Center (console)
- (c) Emergency Operation Facility (console)
- (d) Security Control Point (base station)

4.1.2.4 Check operability and inventory the following equipment:

- (a) Six Button Phones in the Control Room (2)
- (b) Headset in the Control Room (1)
- (c) Two Button Phones in the TSC (8)

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 6.4
EMERGENCY PREPAREDNESS COMMUNICATIONS TESTING	Page 3 of 11 Revision 3 Date 3/19/83

- (d) Headsets in the TSC (5)
- (e) Operations Radios in the SCP (4)
- (f) Security/Radiological Porta-Mobiles in the SCP (2)
- (g) Magnetic Mount Antennas in the SCP (2)
- (h) Antenna Adapters in the SCP (2)

NOTE

The head sets in the TSC are located in the cabinet in the Communications Room.

- 4.1.3 Completion of the annual communications checks shall be documented on Attachment 4, "Annual IE Tower Emergency Communications Checks".

4.1.3.1 Centrix connections to:

- (a) FEMA
- (b) DOE
- (c) Linn County Civil Defense
- (d) Benton County Civil Defense

- 4.2 Communications checks should be conducted as follows:

4.2.1 Monthly - first full calendar week

4.2.2 Quarterly - first full calendar week during January, April, July and October

4.2.3 Annual - first full calendar week during October.

- 4.3 A message similar to that shown on Attachment 5, "Example Communications Check Message Format", should be used when conducting communications systems checks external to IELP.

- 4.4 The Emergency Planning Coordinator shall ensure that all of the communications checks are performed.

4.4.1 The communications checks identified on Attachment 1, "Monthly DAEC Emergency Communications Checks", should be completed as follows:

- a) Items 1 through 3a - STA
- b) Items 3b through 7 - Security

NOTE

The IWAS Phone check should be initiated by the Office of Disaster Services on the first working Monday of every month.

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 6.4
EMERGENCY PREPAREDNESS COMMUNICATIONS TESTING	Page 4 of 11 Revision 3 Date 3/19/83

4.4.2 The communications checks identified on Attachments 2 through 4 shall be completed as directed by the Emergency Planning Coordinator.

4.5 The Emergency Planning Coordinator shall review all documentation associated with the communications checks.

4.6 Acceptance Criteria

4.6.1 All required communications checks shall be made and satisfactorily completed.

4.6.2 In the event that a call cannot be completed

- a. Contact the party by another means and inform them of the problem. Make sure the party understands no problem exists at the DAEC and their response is not required.
- b. Determine the cause of the problem, if possible, and rectify it as soon as possible.
- c. If the problem cannot be readily resolved, attach a note clearly stating which phone was being used, who and what number (if any) was being called, who was placing the call and any other pertinent information to the EPIP checklist in use.

4.6.3 After completing the communications checks, forward the checklist and comments to the Emergency Planning Coordinator.

## 5.0 REFERENCE


5.1 10 CFR 50, Appendix E

5.2 NUREG 0654, Rev. 1

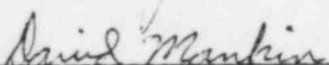
## 6.0 ATTACHMENTS


- 6.1 Monthly DAEC Emergency Communications Checks
- 6.2 Monthly IE Tower Emergency Communications Checks
- 6.3 Quarterly DAEC Emergency Communications Checks
- 6.4 Annual IE Tower Emergency Communications Checks
- 6.5 Example Communications Check Message Format

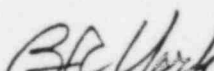
EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 6.4
EMERGENCY PREPAREDNESS COMMUNICATIONS	Page 5 of 11
TESTING	Revision 3
	Date 3/19/83


Approved by:  Date 5/6/83  
Emergency Planning Coordinator

Approved by: \_\_\_\_\_ Date \_\_\_\_\_  
Security Supervisor

Approved by:  Date 5/11/83  
STA Coordinator

Reviewed by:  Date 5/13/83  
ALARA Coordinator

Reviewed by:  Date 5/16/83  
Operations Committee Chairman

Approved by:  Date 5/16/83  
Plant Superintendent - Nuclear

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 6.4
EMERGENCY PREPAREDNESS COMMUNICATIONS	Page 6 of 11
TESTING	Revision 3
	Date 3/19/83

ATTACHMENT 1  
Monthly DAEC Emergency Communications Checks

Communication Circuit	Initiated By (Name)	Received By (Name)	Time	Date
1. NRC ENS				
a) Control Room				
b) Technical Support Center (TSC)				
2. NRC HPN				
a) Access Control Dial 22 (Bethesda)				
b) TSC Dial 22 (Bethesda)				
c) TSC Dial 23 (Region III - During Regular Business Hours Only)				
d) Security Control Point Dial 22 (Bethesda)				
3. COMMERCIAL TELEPHONES				
a) NRC-Bethesda (202) 951-0550 or (301) 427-4056 or (301) 492-7000				
b) Office of Disaster Services (515) 281-3231 or (515) 281-3561				
c) Linn Co. Sheriff 398-3911				
d) Benton Co. Sheriff 1-472-4777 or 1-472-2337				
4. POINT TO POINT RADIOS				
a) Linn County Sheriff				
b) Benton County Sheriff				
c) Iowa Highway Patrol				
5. IWAS PHONE - Initiated by the Office of Disaster Services				
6. NWS FIRST ORDER STATION, Cedar Rapids Flight Service (During Regular Business Hours only) 364-7127				
7. NWS FORECASTING STATION Des Moines (515) 284-4496				

COMMENTS:

REVIEWED BY \_\_\_\_\_ DATE \_\_\_\_\_  
Security Supervisor

REVIEWED BY \_\_\_\_\_ DATE \_\_\_\_\_  
STA Coordinator

REVIEWED BY \_\_\_\_\_ DATE \_\_\_\_\_  
Emergency Planning Coordinator

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 6.4
EMERGENCY PREPAREDNESS COMMUNICATIONS	Page 7 of 11
TESTING	Revision 3
	Date 3/19/83

ATTACHMENT 2

Monthly IE TOWER Emergency Communications Checks

Communication Circuit	Initiated By (initials)	Received By (Name)	Time	Date
Centrex				
NRC Region III (312)932-2500				
NRC Bethesda (202)951-0550				
or (301)427-4056				
or (301)492-7000				
Office of Disaster				
Services (515)281-3231				
or (515)281-3561				
Linn County Sheriff 398-3911				
iton County Sheriff 1-472-4777				
or 1-472-2337				
NRC ENS				
Emergency Operations Facility				
NRC HPN - Bethesda Dial 22				
NRC HPN - Region III Dial 23				
NWS First Order Station				
Cedar Rapids Flight Service				
(During Regular Business Hours only)				
364-7127				
NWS Forecasting Station(515)284-4496				

COMMENTS:

CONDUCTED BY \_\_\_\_\_ DATE \_\_\_\_\_

REVIEWED BY \_\_\_\_\_ DATE \_\_\_\_\_  
Emergency Planning Coordinator

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 6.4
EMERGENCY PREPAREDNESS COMMUNICATIONS	Page 8 of 11
TESTING	Revision 3
	Date 3/19/83

ATTACHMENT 3

Quarterly DAEC Emergency Communications Checks

Communication Circuit	Initiated By (initials)	Received By (Name)	Time	Date	Remarks
Control Room Dedicated Circuits					
TSC					
Access Control					
Security Control Point					
EOF					
Back Panel Circuit to TSC					
Intercom					
Operability Check and Inventory					
(1) Headset					
(2) Six Button Phones					
TSC Dedicated Circuits					
Control Room					
Control Room (back panel)					
Access Control					
Security Control Pt.					
TSC to EOF					
EOF to TSC					
Intercom					
Operability Check and Inventory					
(5) Headsets					
(8) Twenty Button Phones					
Access Control Dedicated Circuits					
Control Room					
TSC					
Security Control Pt.					
Intercom					
Security Control Pt. Dedicated Circuits					
Control Room					
TSC					
Access Control					
Intercom					

Continued on next page

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 6.4
EMERGENCY PREPAREDNESS COMMUNICATIONS	Page 9 of 11
TESTING	Revision 3
	Date 3/19/83

ATTACHMENT 3 (continued)

Quarterly DAEC Emergency Communications Checks

Communication Circuit	Initiated By (initials)	Received By (Name)	Time	Date	Remarks
Operations Radio (TSC)					
Secondary Alarm Station					
Security Control Point					
Site Boundary					
Operability Check and Inventory					
(4) Hand Held Radios					
Security/Health Physics Radio (TSC)					
EOF					
Security Control Point					
10 mile radius					
Operability Check and Inventory					
(2) Porta Mobile Radios					
(2) Magnetic Mount Antennas					
(2) Antenna Adapters					

COMMENTS:

CONDUCTED BY \_\_\_\_\_ DATE \_\_\_\_\_

REVIEWED BY \_\_\_\_\_ DATE \_\_\_\_\_  
                    Emergency Planning Coordinator

EMERGENCY PLAN IMPLEMENTING PROCEDURE	EPIP 6.4
EMERGENCY PREPAREDNESS COMMUNICATIONS	Page 10 of 11
TESTING	Revision 3
	Date 3/19/83

ATTACHMENT 4

Annual IE Tower Emergency Communications Checks

Communication Circuit	Initiated By (initials)	Received By (Name)	Time	Date
Centrex				
FEMA (816)374-5912				
DOE (312)972-4800 or (312)972-5731				
Linn County CD 363-2671				
Benton County CD 1-472-4519				

COMMENTS:

CONDUCTED BY \_\_\_\_\_ DATE \_\_\_\_\_

REVIEWED BY \_\_\_\_\_ DATE \_\_\_\_\_  
Emergency Planning Coordinator

