

TABLE 2.2-1 (Continued)

REACTOR TRIP SYSTEM INSTRUMENTATION TRIP SETPOINTS

NOTATION

NOTE 1: OVERTEMPERATURE  $\Delta T$

$$\Delta T \frac{(1 + \cancel{\tau_1 S})}{(1 + \cancel{\tau_2 S})} \frac{1}{(1 + \cancel{\tau_3 S})} \leq \Delta T_0 \{ K_1 - K_2 \frac{(1 + \tau_4' S)}{(1 + \tau_5' S)} [T \frac{1}{(1 + \tau_6 S)} - T'] + K_3(P - P') - f_1(\Delta I) \}$$

Where:  $\Delta T$  = Measured  $\Delta T$  by RTD Manifold Instrumentation

$\frac{1 + \cancel{\tau_1 S}}{1 + \cancel{\tau_2 S}}$   $\neq$  ~~Lead-lag compensator on measured  $\Delta T$~~

$\cancel{\tau_1}, \cancel{\tau_2}$   $\neq$  ~~Time constants utilized in lead-lag controller for  $\Delta T$ ,  $\tau_1 = 8$  sec.,  $\tau_2 = 3$  sec.~~

$\frac{1}{1 + \cancel{\tau_3 S}}$   $\neq$  ~~Lag compensator on measured  $\Delta T$~~

$\cancel{\tau_3}$   $\neq$  ~~Time constants utilized in the lag compensator for  $\Delta T$ ,  $\tau_3 = 0$  secs.~~

$\Delta T_0$  = Indicated  $\Delta T$  at RATED THERMAL POWER

$K_1$  = 1.090

$K_2$  = 0.01450

$\frac{1 + \tau_4' S}{1 + \tau_5' S}$  = The function generated by the lead-lag controller for  $T_{avg}$  dynamic compensation

$\tau_4', \& \tau_5'$  = Time constants utilized in the lead-lag controller for  $T_{avg}$ ,  $\tau_4' = 33$  secs.,  $\tau_5' = 4$  secs.

$T$  = Average temperature °F

$\frac{1}{1 + \cancel{\tau_6 S}}$   $\neq$  ~~Lag compensator on measured  $T_{avg}$~~

$\cancel{\tau_6}$   $\neq$  ~~Time constant utilized in the measured  $T_{avg}$  lag compensator,  $\tau_6 = 0$  secs.~~

TABLE 2.2-1 (Continued)

## REACTOR TRIP SYSTEM INSTRUMENTATION TRIP SETPOINTS

## NOTATION (Continued)

NOTE 3: OVERPOWER  $\Delta T$ 

$$\Delta T \frac{(1 + \cancel{\tau_1 S})}{(1 + \cancel{\tau_2 S})} \frac{1}{(1 + \cancel{\tau_3 S})} \leq \Delta T_0 \{K_4 - K_5 \frac{\tau_7^3 S}{1 + \tau_7 S}\} \frac{1}{(1 + \cancel{\tau_6 S})} T - K_6 [T \frac{1}{(1 + \cancel{\tau_6 S})} - T"] - \cancel{f_2(\Delta T)}$$

Where:  $\Delta T$  = as defined in Note 1 $\frac{1 + \cancel{\tau_1 S}}{1 + \cancel{\tau_2 S}}$   $\neq$  as defined in Note 1 $\cancel{\tau_1}, \cancel{\tau_2}$   $\neq$  as defined in Note 1 $\frac{1}{1 + \cancel{\tau_3 S}}$   $\neq$  as defined in Note 1 $\cancel{\tau_3}$   $\neq$  as defined in Note 1 $\Delta T_0$  = as defined in Note 1 $K_4$  = 1.091 $K_5$  = 0.02/°F for increasing average temperature and 0 for decreasing average temperature $\frac{\tau_7^3 S}{1 + \tau_7 S}$  = The function generated by the rate-lag controller for  $T_{avg}$  dynamic compensation $\tau_7^3$  = Time constant utilized in the rate-lag controller for  $T_{avg}$ ,  $\tau_7^3 = 10$  secs. $\frac{1}{1 + \cancel{\tau_6 S}}$   $\neq$  as defined in Note 1 $\cancel{\tau_6}$   $\neq$  as defined in Note 1

TABLE 2.2-1 (Continued)REACTOR TRIP SYSTEM INSTRUMENTATION TRIP SETPOINTSNOTATION (Continued)

## NOTE 3 (continued)

$K_6 = 0.001190/^{\circ}\text{F}$  for  $T > T''$  and  $K_6 = 0$  for  $T \leq T''$

$T =$  as defined in Note 1

$T'' \leq 587.4^{\circ}\text{F}$  Reference  $T_{\text{avg}}$  at RATED THERMAL POWER

$S =$  as defined in Note 1

~~$f_2(\Delta T) = 0$  for all  $\Delta T$~~

NOTE 4: The channel's maximum trip setpoint shall not exceed its computed trip point by more than 2.7 percent  $\Delta T$  Span.