

CONTROL BLOCK:

(PLEASE PRINT OR TYPE ALL REQUIRED INFORMATION)

01 PASES1 200-000000-00 341111 4 5  
7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60

CONT

01 REPORT SOURCE L 605000387 7040783 8050683 9  
7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60

EVENT DESCRIPTION AND PROBABLE CONSEQUENCES 10

02 During the perform. of a startup test to determ. the capability of the shutdown  
03 cooling mode of RHR, the shutdown cooling loop in operation isolated. Concurrently,  
04 excessive vessel and primary coolant cooldown rates occurred. Engineering analysis  
05 has concluded that the effects of the cooldown did not impair the structural integ-  
06 rity of the reactor coolant system. The use of RWCU and subsequently, the "A" loop  
07 of RHR in shutdown cooling, prevented stratification in the vessel.

8

09 SYSTEM CODE C F 11 CAUSE CODE D 12 CAUSE SUBCODE Z 13 COMPONENT CODE Z Z Z Z Z Z Z 14 COMP. SUBCODE Z 15 VALVE SUBCODE Z 16  
7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60

17 LER/RO REPORT NUMBER 83 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60

18 ACTION TAKEN G 19 FUTURE ACTION F 20 EFFECT ON PLANT Z 21 SHUTDOWN METHOD Z 22 HOURS 0000 23 ATTACHMENT SUBMITTED Y 24 NPRD-4 FORM SUB. N 25 PRIME COMP. SUPPLIER Z 26 COMPONENT MANUFACTURER Z 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60

CAUSE DESCRIPTION AND CORRECTIVE ACTIONS 27

10 These events were caused by a complex series of interactions. Procedural changes  
11 have been made and engineering evaluations are underway to more closely control  
12 RHR system operation in the shutdown cooling mode. This LER will be updated.

13

14

15 FACILITY STATUS B 28 0000 29 NA 30 METHOD OF DISCOVERY C 31 Operator Observation 32  
7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60

16 ACTIVITY CONTENT RELEASED OF RELEASE Z 33 Z 34 NA 35 LOCATION OF RELEASE NA 36  
7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60

17 PERSONNEL EXPOSURES NUMBER 000 37 Z 38 NA 39  
7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60

18 PERSONNEL INJURIES NUMBER 000 40 NA 41  
7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60

19 LOSS OF OR DAMAGE TO FACILITY TYPE Z 42 NA 43  
7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60

20 PUBLICITY ISSUED N 44 NA 45  
7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60

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S PDR

Attachment  
LER 83-056/03L-0

A thorough review was performed of the events as described on the following time line. Operations and technical personnel identified main troublespots, and devised recommendations to correct them.

Present RHR system design requires 10,000 gpm through the heat exchanger to protect the physical integrity of the heat exchanger outlet valve. Lack of this throttling capability jeopardizes the allowed cooldown rate when transferring RHR shutdown cooling flow from bypassing the heat exchanger to establishing flow through the heat exchanger. The investigation to determine the feasibility of providing throttling capability with the existing RHR heat exchanger outlet valve and operator is underway.

Corrective actions also include splitting the present RHR operating procedure into six separate procedures to facilitate their proper use. The shutdown cooling mode procedure has also been revised for clarification.

EVENT TIME LINE

PRIOR TO  
START OF TEST  
ON 4/7/83

REACTOR TEMPERATURE/PRESSURE WAS MAINTAINED USING SHUT-DOWN COOLING BY VALVING IN THE RHR HEAT EXCHANGER FOR APPROXIMATELY 5 MINUTES EVERY HOUR. THE HEAT EXCHANGER WAS VALVED IN BY ALTERNATELY OPENING AND CLOSING EITHER THE HEAT EXCHANGER INLET OR DISCHARGE VALVE (F047 OR F003). THE HEAT EXCHANGER BYPASS VALVE F048 ALWAYS REMAINED FULL OPEN.

0256

WITH REACTOR VESSEL LEVEL AT 35", THE STARTUP TEST BEGAN. THE HEAT EXCHANGER HAD BEEN ISOLATED FOR APPROXIMATELY ONE HOUR BEFORE THE START OF THE TEST WITH RHR SW FLOW AT 5000 GPM AND SPRAY POND TEMPERATURE  $\sim 57^{\circ}\text{F}$ . THE RWCU SYSTEM WAS IN SERVICE WITH THE HEAT EXCHANGERS ISOLATED, THEN ALL FLOW IN RHR LOOP A WAS DIRECTED THROUGH THE HEAT EXCHANGER (10,000 GPM). THE HEAT EXCHANGER BYPASS VALVE WAS FULLY CLOSED APPROXIMATELY 3 MINUTES AFTER THE START OF THE TEST.

0304

WHEN A  $60^{\circ}\text{F}$  TEMPERATURE DROP IN THE SUCTION LINE OF THE 'A' RECIRC LOOP WAS APPROACHED, THE STARTUP TEST WAS ABORTED BY OPENING THE HEAT EXCHANGER BYPASS VALVE AND ISOLATING THE HEAT EXCHANGER AT THE SAME TIME. BY THE TIME THIS WAS ACCOMPLISHED, THE TEMPERATURE DROP REACHED APPROXIMATELY  $80^{\circ} - 90^{\circ}\text{F}$ . REACTOR LEVEL WAS DROPPING DUE TO SHRINKAGE. CRD FLOW WAS INCREASED FROM 42 TO 62 GPM. TEMPERATURES WERE BEING MONITORED ON THE CRT. THE RECIRC DISCHARGE VALVE WAS CLOSED WITH THE DISCHARGE BYPASS VALVE AND RECIRC SUCTION VALVE OPEN.

0306

REACTOR SCRAMMED ON LOW LEVEL ( $\sim 15"$ ). (NOTE: THIS WAS AN RPS ACTUATION ONLY. REACTOR WAS NOT CRITICAL.) SHUTDOWN COOLING ISOLATED, RHR PUMP A TRIPPED. LEVEL RESTORATION

0306 WAS ATTEMPTED BY OPENING CONDENSATE TRANSFER VALVE BUT A  
(CONTINUED) MANUAL NORMALLY CLOSED VALVE DOWNSTREAM PREVENTED THIS.  
LEVEL WAS RESTORED WITH CRD FLOW.

0327 NRC ENS NOTIFIED

0336 RHR LOOPS A&B FILLED & VENTED.

0435 OPENED INBOARD MSIV's TO STOP THE INCREASING  $\Delta T$  IN VESSEL.  
CRD FLOW WAS REDUCED TO 42 GPM AND RWCU WAS ESTABLISHED TO  
NORMAL LINEUP, STOPPING THE STRATIFICATION.

0444 RESTARTED 'A' RHR PUMP IN SHUTDOWN COOLING LINEUP WITH  
REACTOR LEVEL AT 35". THE F017 VALVE WAS NOT OPENED FAR  
ENOUGH AND THE MIN FLOW VALVE OPENED. OPERATOR TRIED TO  
CLOSE VALVE BUT DID NOT HOLD IN CLOSED POSITION. VALVE  
CYCLED OPEN AND CLOSED IN  $\sim 1$  MINUTE WITH FLOW AT 4000 GPM.  
REACTOR SCRAMMED ON LOW LEVEL ( $\sim 15$ ").

0450 THE F008, F009, F015 VALVES WERE OPENED AND THE F017 VALVE  
CRACKED TO ALLOW LEVEL TO BE INCREASED TO 54" USING  
CONDENSATE TRANSFER (THE MANUAL NORMALLY CLOSED VALVE  
DOWNSTREAM OF THE CONDENSATE TRANSFER VALVE WAS OPENED  
AFTER PRIOR SCRAM). OPERATOR OBSERVED A TEMPERATURE  
DECREASE FROM 290°F TO 170°F IN 5 MINUTES. THE F008 AND  
017 VALVES WERE SHUT IMMEDIATELY. LEVEL HAD INITIALLY BEEN  
RECOVERED THROUGH CRD.

0502 WHILE STARTING 'B' RHR PUMP IN SHUTDOWN COOLING, AN ISOLATION  
SIGNAL WAS RECEIVED ON F008 CAUSING THE 'B' PUMP TO TRIP.

0516 NRC NOTIFIED OF SECOND SCRAM.

0518 PLACED RHR PUMP 'A' IN SHUTDOWN COOLING.

4/8/83

0130 'B' RHR HEAT EXCHANGER DISCHARGE VALVE WOULD NOT OPEN.

0500 'B' RHR HEAT EXCHANGER DISCHARGE VALVE OPENED MANUALLY.

THE MOTOR FROM THE CORRESPONDING VALVE ON UNIT 2 WAS USED TO REPLACE THE FAILED  
MOTOR ON THE UNIT 1 VALVE. THE UNIT 1 VALVE DID NOT OPEN DUE TO AN OPEN MOTOR  
WINDING.