QUAD-CITIES NUCLEAR POWER STATION

UNITS 1 AND 2

MONTHLY PERFORMANCE REPORT

MARCH 1983

COMMONWEALTH EDISON COMPANY

AND

IOWA-ILLINOIS GAS & ELECTRIC COMPANY

NRC DOCKET NOS. 50-254 AND 50-265

LICENSE NOS. DPR-29 AND DPR-30

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I. INTRODUCTION

Quad-Cities Nuclear Power Station is composed of two Boiling Water Reactors, each with a Maximum Dependable Capacity of 769 MWe Net, located in Cordova, Illinois. The Station is jointly owned by Commonwealth Edison Company and Iowa-Illinois Gas & Electric Company. The Nuclear Steam Supply Systems are General Electric Company Boiling Water Reactors. The Architect/Engineer was Sargent & Lundy, Incorporated, and the primary construction contractor was United Engineers & Constructors. The condenser cooling method is a closed cycle spray canal, and the Mississippi River is the condenser cooling water source. The plant is subject to license numbers DPR-29 and DPR-30, issued October 1, 1971, and March 21, 1972, respectively, pursuant to Docket Numbers 50-254 and 50-265. The date of initial reactor criticalities for Units 1 and 2, respectively, were October 18, 1971, and April 26, 1972. Commercial generation of power began on February 18, 1973, for Unit 1 and March 10, 1973 for Unit 2.

This report was compiled by Becky Brown and Alex Misak, telephone number 309-654-2241, extensions 127 and 194.

II. SUMMARY OF OPERATING EXPERIENCE

A. UNIT ONE

March 1-6: Unit One began the month derated to 785 MWe due to fouling of the Main Condenser. At 0230 hours, on March 6, load was decreased at 200 MWe/hour to 620 MWe to perform weekly Turbine tests and reverse Main Condenser flow. Load was increased normally until 1435 hours when low Condenser vacuum caused the load increase to be terminated at 770 MWe.

March 7-10: The unit continued to be derated due to high Main Condenser backpressure until 2345 hours on March 10, when the unit was shutdown for a weekend Maintenance Outage.

March 11-18: From March 11-14, the unit was in Cold Shutdown for a weekend preventative Maintenance Outage to clean the Main Condenser Tubes. Unit startup commenced at 0410 hours on March 15, but the unit did not come on line until 0905 hours on March 18 due to gasket leaks on two valves and high Turbine vibration.

March 19-24: Load was increased normally until a load of 812 MWe was achieved at 0300 hours on March 21. This load was maintained until 2000 hours on March 22, when load was decreased to 300 MWe to perform maintenance on a thermocouple on the 1A MSIV. At 2345 hours, load was increased normally until 1010 hours on March 24, when a load of 831 MWe was achieved.

March 25-31: The unit load was maintained at an average of 825 MWe throughout the remainder of the month, except for a two hour period on March 27, when load was decreased to 700 MWe to perform weekly Turbine tests and reverse Main Condenser flow.

B. UNIT TWO

March 1-6: Unit Two began the month operating at 790 MWe. On three occasions during this period, load was reduced due to Condensate Demineralizer problems. In addition, at 0140 hours, on March 4, load was reduced to 700 MWe to perform weekly Turbine tests.

March 7-10: The unit load was increasing normally on March 7, following Condensate Demineralizer maintenance, until 1900 hours when the increase was terminated at 817 MWe. Also, during this period, the barrier fuel test was performed, and Unit Two began experiencing end of cycle fuel depletion deratings.

March 11-24: Unit load was maintained at an average of 780 MWe throughout this period. Load was reduced three times to 700 MWe, twice for weekly Turbine tests and once to reverse Condenser flow. At 0140 hours, on March 24, the 2A Recirculation Pump Motor-Generator Set ramped down to minimum speed. The 2B MG Set was reduced to 44 percent speed, dropping the unit load to 350 MWe. The 2A MG Set was repaired, and the unit load was increased to 650 MWe. This load was maintained for about three hours until normal shutdown procedures were initiated in preparation for a weekend preventative Maintenance Outage.

March 25-31: At 0030 hours on March 25, Unit Two was taken off line and placed in Cold Shutdown for a weekend preventative Maintenance Outage to repair a minor Feedwater piping leak and to perform preventative maintenance cleaning of the Main Condenser Tubes. This outage continued until 1150 hours on March 30, when the unit was placed on line with the load increasing normally.

III. PLANT OR PROCEDURE CHANGES, TESTS, EXPERIMENTS, AND SAFETY RELATED MAINTENANCE

A. Amendments to Facility Licens or Technical Specifications

On February 17, 1983, Amendment 78 was issued to License DPR-30. This Amendment allows adjustment of APRM gain instead of changing scram and rod block lines when operating with MFLPP/FRP greater than 1.0.

B. Facility or Procedure Changes Requiring NRC Approval

There were no Facility or Procedure changes requiring NRC approval for the reporting period.

C. Tests and Experiments Requiring NRC Approval

There were no Tests or Experiments requiring NRC approval for the reporting period.

D. Corrective Maintenance of Safety Related Equipment

The following represents a tabular summary of the safety related maintenance performed on Unit One and Unit Two during the reporting period. This summary includes the following headings: Work Request Numbers, LER Numbers, Components, Cause of Malfunctions, Results and Effects on Safe Operation, and Action Taken to Prevent Repetition.

UNIT ONE MAINTENANCE SUMMARY

W.R. NUMBER	LER NUMBER	COMPONENT	CAUSE OF MALFUNCTION	RESULTS & EFFECTS ON SAFE OPERATION	ACTION TAKEN TO PREVENT REPETITION
Q21535		'B' Outboard Feedwater Check Valve CV-1-220-62B	Normal wear of the O-ring.	The valve failed Local Leak Rate Test.	Replaced O-ring.
Q24751		Main Steam Drain 1-220-1	Valve does not seal well enough to pass LLRT. This is a result of wear and repeated lapping of the valve seat.	The inline 1-220-2 valve was closed during normal operation of the unit, and isolates on a Group II Isolation signal.	An oversize disc was installed in the valve and the seat was lapped to accommodate the disc. The valve then passed the Local Leak Rate Test.
Q24247		1B Recirc Pump Seal	Pressure between number 1 and number 2 seal was low due to seal deterioration.	The seal deterioration caused an increase in Drywell Equipment Drain leakage.	A rebuilt seal was installed.
Q21987		Condenser Off Gas Valve AO-1-5402A	The solenoid valve failed to operate properly due to normal wear of the valve internals.	The 1-5402A was operable, but the faulty solenoid valve prevented smooth operation of the valve.	The solenoid valve was repaired, successfully bench tested, and re-installed. The 1-5402A valve was then successfully tested.
Q21986		Condenser Off Gas Valve AO-1-5402B	Solenoid valve is bad.	The 1-5402B valve was operable, but the faulty solenoid valve prevented smooth valve operation.	The solenoid valve was rebuilt, bench tested, and re-installed.

UNIT ONE MAINTENANCE SUMMARY

W.R. NUMBER	LER NUMBER	COMPONENT	CAUSE OF MALFUNCTION	RESULTS & EFFECTS ON SAFE OPERATION	ACTION TAKEN TO PREVENT REPETITION
Q23610		TIP Machine #4 Ball Valve System 703	The ball valve internals were worn.	The ball valve was operable but did not operate smoothly.	A new ball valve was installed and leak tested.
Q23479		ACAD Air Supply Isolation Valve FCV-1-2599-113	Feed fuse failed.	Valve would not open; Containment integrity was intact.	The feed fuse in Control Room panel 901-56 was replaced.
Q24972		Inboard Feedwater Check Valve 1-220-58A	The valve bonnet pressure seal ring failed due to normal wear.	The worn pressure seal ring resulted in a small leak at pressure. All leakage was contained within the Drywell Floor Drain system.	The pressure seal ring was replaced, and the valve was visually checked for leaks at pressure. The seal ring still leaked (See Work Request Q25010).
Q25020		Drywell Floor Drain Sump Isolation Valve 1-2001-3	The valve had dual indication when being given open signal. This implied that the 1-2001-3 valve was not going full open.	The 1-2001-3 valve had been in the isolated position previous to this event and the inline 1-2001-4 valve was operable.	Disassembled valve, cleaned internals, and replaced air operator. The valve was then stroked, timed & successfully Local Leak Rate tested.
Q25068		Drywell Floor Drain Sump Pump Discharge 1-2001-3	Valve would not indicate closed.	The inline AO 1-2001-4 valve was operable & would have provided proper Containment isolation.	The valve stem was turned & the limits were re-adjusted. The valve was then successfully stroked and timed.

UNIT TWO MAINTENANCE SUMMARY

W.R. NUMBER	LER NUMBER	COMPONENT	CAUSE OF MALFUNCTION	RESULTS & EFFECTS ON SAFE OPERATION	ACTION TAKEN TO PREVENT REPETITION
Q24780		Torus to Drywell Vacuum Breaker AO-2-1601-20B	Pressure switch was out of calibration.	Redundant vacuum breaker was fully operable.	Installed new switch and calibrated.
Q23012		Drywell Electrical Penetration 100G	The penetration flange was loose.	The penetration would not hold N_2 pressure; Containment integrity was intact.	The flange was tightened and the penetration was successfully Local Leak Rate tested.
Q25221		2-1601-55 Valve	Failure of seals in the solenoid valve.	The solenoid valve was blowing air out the exhaust port, but was operable.	A new solenoid valve was installed.
Q25262		"A" Reactor Protection System MG Set Output Breaker	The undervoltage trip release coil failed.	The breaker tripped and would not close in.	A new undervoltage trip release coil was installed in the output breaker.

IV. LICENSEE EVENT REPORTS

The following is a tabular summary of all licensee event reports for Quad-Cities Units One and Two occurring during the reporting period, pursuant to the reportable occurrence reporting requirements as set forth in sections 6.6.B.1. and 6.6.B.2. of the Technical Specifications.

UNIT ONE

Licensee Event Report Number	Date	Title of Occurrence
83-10/03L	2-24-83	Reactor Building Ventilation System Trip
83-11/03L	2-25-83	Condenser Vacuum Scram Switch Out of Limits
83-12/01T	3-10-83	Unit One Shutdown Out of Sequence
83-13/03L	3-19-83	MSIV Pilot Temperature Detector Failed
83-14/03L	3-24-83	Unit One 250 Volt Battery Inoperable

UNIT TWO

83-5/03L	3-16-83	Low-Low Level Switch, 2-263-72C, did not respond

V. DATA TABULATIONS

The following data tabulations are presented in this report:

A. Operating Data Report

B. Average Daily Unit Power Level

C. Unit Shutdowns and Power Reductions

OPERATING DATA REPORT

DOCKET NO. 50-254

UNIT ONE

DATE April 05 1983

COMPLETED BY Alex Misak

TELEPHONE 309-654-2241x194

OPERATING STATUS

0000 030183

1. Reporting period: 2406 033183 Gross hours in reporting period: 744

2. Currently authorized power level (MWt): 2511 Max.Depend capacity (MWe-Net): 769* Design electrical rating (MWe-Net): 789

3. Power level to which restricted(if any)(MWe-Net): NA

4. Reasons for restriction (if any):

	This Month	Yr.to Date	Cumulative
5. Number of hours reactor was critical	591.3	2002.4	77173.6
6. Reactor reserve shutdown hours	0.0	0.0	3421.9
7. Hours generator on line	567.2	1973.9	74060.5
8. Unit reserve shutdown hours.	0.0	0.0	909.2
9. Gross thermal energy generated(MWH)	1318996	4739092	150952083
10. Gross electrical energy generated(MWH)	427232	1552900	48674781
11. Net electrical energy generated(MWH)	399701	1459803	45288711
12. Reactor service factor	79.5	92.7	80.9
13. Reactor availability factor	79.5	92.7	84.4
14. Unit service factor	76.2	91.4	77.6
15. Unit availability factor	76.2	91.4	78.5
16. Unit capacity factor (Using MDC)	69.9	87.9	61.7
17. Unit capacity factor (Using Des.MWe)	68.1	85.7	60.1
18. Unit forced outage rate	8.9	3.2	6.6

19. Shutdowns scheduled over next 6 months (Type,Date,and Duration of each):

20. If shutdown at end of report period,estimated date of startup NA

*The MDC may be lower than 769 MWe during periods of high ambient temperature due to the thermal performance of the spray canal.

#UNOFFICIAL COMPANY NUMBERS ARE USED IN THIS REPORT

OPERATING DATA REPORT

DOCKET NO. 50-265

UNIT TWO

DATE April 05 1983

COMPLETED BY Alex Misak

TELEPHONE 309-654-2241x194

OPERATING STATUS

0000 030183

1. Reporting period: 2400 033183 Gross hours in reporting period: 744

2. Currently authorized power level (MWt): 2511 Max.Depend capacity (MWe-Net): 769* Design electrical rating (MWe-Net): 789

3. Power level to which restricted(if any)(MWe-Net): NA

4. Reasons for restriction (if any):

	This Month	Yr.to Date	Cumulative
5. Number of hours reactor was critical	629.9	1896.0	74159.4
6. Reactor reserve shutdown hours	0.0	0.0	2985.8
7. Hours generator on line	612.7	1866.7	71454.8
8. Unit reserve shutdown hours.	0.0	0.0	702.9
9. Gross thermal energy generated(MWH)	1412692	4228411	148819905
10. Gross electrical energy generated(MWH)	461090	1348792	47386327
11. Net electrical energy generated(MWH)	430918	1264540	44448107
12. Reactor service factor	84.7	87.8	78.4
13. Reactor availability factor	84.7	87.8	81.6
14. Unit service factor	82.4	86.4	75.6
15. Unit availability factor	82.4	86.4	76.3
16. Unit capacity factor (Using MDC)	75.3	76.1	61.1
17. Unit capacity factor (Using Des.MWe)	73.4	74.2	59.6
18. Unit forced outage rate	2.8	5.4	9.0

19. Shutdowns scheduled over next 6 months (Type,Date,and Duration of each):

20. If shutdown at end of report period,estimated date of startup NA

*The MDC may be lower than 769 MWe during periods of high ambient temperature due to the thermal performance of the spray canal.

*UNOFFICIAL COMPANY NUMBERS ARE USED IN THIS REPORT

APPENDIX B
AVERAGE DAILY UNIT POWER LEVEL

DOCKET NO. 50-254
UNIT ONE
DATE April 05 1983
COMPLETED BY Alex Misak
TELEPHONE 309-654-2241x194

MONTH March 1983

DAY	AVERAGE DAILY POWER LEVEL (MWe-Net)	DAY	AVERAGE DAILY POWER LEVEL (MWe-Net)
1.	742.0	17.	-11.0
2.	746.1	18.	264.1
3.	764.1	19.	578.6
4.	733.0	20.	721.0
5.	772.2	21.	766.8
6.	701.5	22.	713.3
7.	676.3	23.	651.1
8.	636.7	24.	765.3
9.	588.8	25.	764.6
10.	537.2	26.	764.6
11.	-9.4	27.	749.1
12.	-6.2	28.	769.0
13.	-5.5	29.	775.3
14.	-6.3	30.	759.8
15.	-13.0	31.	778.2
16.	-12.5		

INSTRUCTIONS

On this form, list the average daily unit power level in MWe-Net for each day in the reporting month. Compute to the nearest whole megawatt.

These figures will be used to plot a graph for each reporting month. Note that when maximum dependable capacity is used for the net electrical rating of the unit, there may be occasions when the daily average power level exceeds the 100% line (or the restricted power level line). In such cases, the average daily unit power output sheet should be footnoted to explain the apparent anomaly

APPENDIX B
AVERAGE DAILY UNIT POWER LEVEL

DOCKET NO. 50-265

UNIT TWO

DATE April 05 1983

COMPLETED BY Alex Misak

TELEPHONE 309-654-2241x194

MONTH March 1983

DAY	AVERAGE DAILY POWER LEVEL (MWe-Net)	DAY	AVERAGE DAILY POWER LEVEL (MWe-Net)
1.	752.8	17.	719.6
2.	740.9	18.	734.4
3.	753.2	19.	721.2
4.	672.0	20.	729.0
5.	689.1	21.	721.8
6.	713.7	22.	718.3
7.	738.5	23.	718.8
8.	728.9	24.	459.4
9.	731.3	25.	-6.9
10.	767.8	26.	-6.8
11.	711.3	27.	-7.3
12.	743.3	28.	-9.7
13.	713.2	29.	-13.4
14.	726.0	30.	218.8
15.	735.6	31.	608.0
16.	731.9		

INSTRUCTIONS

On this form, list the average daily unit power level in MWe-Net for each day in the reporting month. Compute to the nearest whole megawatt.

These figures will be used to plot a graph for each reporting month. Note that when maximum dependable capacity is used for the net electrical rating of the unit, there may be occasions when the daily average power level exceeds the 100% line (or the restricted power level line). In such cases, the average daily unit power output sheet should be footnoted to explain the apparent anomaly

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APPENDIX D
UNIT SHUTDOWNS AND POWER REDUCTIONS

QTP 300-S13
Revision 6
August 1982

DOCKET NO. 50-254

UNIT NAME Quad-Cities Unit One

COMPLETED BY Alex Misak, ext 194

DATE April 4, 1983

REPORT MONTH MARCH 1983

TELEPHONE 309-654-2241

NO.	DATE	TYPE F OR S	DURATION (HOURS)	REASON	METHOD OF SHUTTING DOWN REACTOR	LICENSEE EVENT REPORT NO.	SYSTEM CODE	COMPONENT CODE	CORRECTIVE ACTIONS/COMMENTS
83-16	830306	S	0.0	B	5		HA	XXXXXX	Reduced load to perform weekly Turbine test
83-17	830308	F	0.0	H	5		HC	HTEXCH	Reduced load due to High Main Condenser Back Pressure
83-18	830310	S	101.2	B	1		HC	HTEXCH	Unit shutdown for Main Condenser Tube cleaning
83-19	830315	F	23.3	B	1		CH	VALVEX	Unit shutdown due to gasket leaks on continuous head vent and 58A Feedwater Check Valves
83-20	830316	F	34.4	B	1		CH	VALVEX	Unit shutdown due to gasket leak on 58A Feedwater Check Valve
83-21	830318	F	3.4	B	9		HA	TURBIN	Generator tripped due to high Turbine vibration
83-22	830322	F	0.0	B	5		CD	INSTRU	Reduced load to repair Thermocouple on 1A MSIV
83-23	830327	S	0.0	B	5		HA	XXXXXX	Reduced load to perform weekly Turbine test

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APPENDIX D
UNIT SHUTDOWNS AND POWER REDUCTIONS

QTP 300-S13
Revision 6
August 1982

DOCKET NO. 50-265

UNIT NAME Quad-Cities Unit Two

COMPLETED BY Alex Misak, ext 194

DATE April 4, 1983

REPORT MONTH MARCH 1983

TELEPHONE 309-654-2241

NO.	DATE	TYPE F OR S	DURATION (HOURS)	REASON	METHOD OF SHUTTING DOWN REACTOR	LICENSEE EVENT REPORT NO.	SYSTEM CODE	COMPONENT CODE	CORRECTIVE ACTIONS/COMMENTS
83-21	830303	F	0.0	B	5		HG	DEMINX	Reduced load due to plugged 2B Condensate Demineralizer
83-22	830304	S	0.0	B	5		HA	XXXXXX	Reduced load to perform weekly Turbine test
83-23	830304	F	0.0	B	5		HG	DEMINX	Reduced load due to Condensate Demineralizer problems
83-24	830306	F	0.0	B	5		HG	DEMINX	Reduced load due to Condensate Demineralizer problems
83-25	830313	S	0.0	B	5		HA	XXXXXX	Reduced load to perform weekly Turbine test
83-26	830319	S	0.0	B	5		HA	XXXXXX	Reduced load to perform weekly Turbine test
83-27	830320	S	0.0	H	5		HC	HTEXCH	Reduced load to reverse Condenser Flow direction
83-28	830324	F	0.0	A	5		CB	MECFUN	Reduced load due to 2A Recirculation pump Motor-Generator Set problems

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APPENDIX D
UNIT SHUTDOWNS AND POWER REDUCTIONS

QTP 300-S13
Revision 6
August 1982

DOCKET NO. 50-265

UNIT NAME Quad-Cities Unit Two

COMPLETED BY Alex Misak, ext 194

DATE April 4, 1983

REPORT MONTH MARCH 1983

TELEPHONE 309-654-2241

NO.	DATE	TYPE F OR S	DURATION (HOURS)	REASON	METHOD OF SHUTTING DOWN REACTOR	LICENSEE EVENT REPORT NO.	SYSTEM CODE	COMPONENT CODE	CORRECTIVE ACTIONS/COMMENTS
83-29	830325	S	113.8	B	1		ZZ	ZZZZZZ	Unit shutdown for minor Feedwater piping leak and preventative maintenance cleaning of Main Condenser
83-30	830329	F	17.5	B	1		SH	VALVEX	Unit shutd .n due to gasket leak on Electromatic Relief Valve 2-203-3C

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VI. UNIQUE REPORTING REQUIREMENTS

The following items are included in this report based on prior commitments to the commission:

A. MAIN STEAM RELIEF VALVE OPERATIONS

Relief valve operations during the reporting period are summarized in the following table. The table includes information as to which relief valve was actuated, how it was actuated, and the circumstances resulting in its actuation.

UNIT	DATE	VALVES ACTUATED	NO. & TYPE ACTUATIONS	PLANT CONDITIONS	DESCRIPTION OF EVENTS
1	3-11-83	1-203-3A	1 Manual	Rx Press 895	Surveillance T.S. 4.5.D.1.b
1	3-15-83	1-203-3B 1-203-3C 1-203-3D 1-203-3E	1 Manual 1 Manual 1 Manual 1 Manual	890	Post-Maintenance - replaced pilot valve
2	3-25-83	2-203-3A	1 Manual	910	Surveillance T.S. 4.5.D.1.b
2	3-29-83	2-203-3B 2-203-3C 2-203-3D 2-203-3E	1 Manual 1 Manual 1 Manual 1 Manual	918	Post-Maintenance - replaced pilot valve
2	3-30-83	2-203-3C	1 Manual	919	Post-Maintenance - replaced flange gasket

B. CONTROL ROD DRIVE SCRAM TIMING DATA FOR UNITS ONE AND TWO

There were no control rod drive scram timing data for the reporting period.

VII. REFUELING INFORMATION

The following information about future reloads at Quad-Cities Station was requested in a January 26, 1978, licensing memorandum (78-24) from D. E. O'Brien to C. Reed, et al., titled "Dresden, Quad-Cities, and Zion Station--NRC Request for Refueling Information", dated January 18, 1978.

QTP 300-S32
Revision 1
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QUAD-CITIES REFUELING INFORMATION REQUEST

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1. Unit: Q1 Reload: 6 Cycle: 7

2. Scheduled date for next refueling shutdown: 9-6-82

3. Scheduled date for restart following refueling: 12-18-82

4. Will refueling or resumption of operation thereafter require a technical specification change or other license amendment: Yes

5. Scheduled date(s) for submitting proposed licensing action and supporting information: 8-19-82: Tech. Spec. changes submitted to the NRC.

6. Important licensing considerations associated with refueling, e.g., new or different fuel design or supplier, unreviewed design or performance analysis methods, significant changes in fuel design, new operating procedures:
   a) All 7x7 fuel assemblies will be removed from the core.
   b) MAPLHGR curves for fuel types in the core are being extended to 40,000 MWD/ST.
   c) MCPR limits will be determined by GE's ODYN computer code.
   d) The vessel pressure safety limit is being modified to accommodate the potential for higher reactor pressures as calculated by ODYN.

7. The number of fuel assemblies.
   a. Number of assemblies in core: 724
   b. Number of assemblies in spent fuel pool: 800

8. The present licensed spent fuel pool storage capacity and the size of any increase in licensed storage capacity that has been requested or is planned in number of fuel assemblies:
   a. Licensed storage capacity for spent fuel: 3657
   b. Planned increase in licensed storage: 0

9. The projected date of the last refueling that can be discharged to the spent fuel pool assuming the present licensed capacity: 2003

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QTP 300-S32
Revision 1
March 1978

QUAD-CITIES REFUELING INFORMATION REQUEST

*

1. Unit: Q2 Reload: 6 Cycle: 7

2. Scheduled date for next refueling shutdown: 9-11-83

3. Scheduled date for restart following refueling: 11-20-83

4. Will refueling or resumption of operation thereafter require a technical specification change or other license amendment:
   Depending upon the Licensing analyses, a MCPR limit change may be needed.

5. Scheduled date(s) for submitting proposed licensing action and supporting information: 8-22-83 (if necessary)

6. Important licensing considerations associated with refueling, e.g., new or different fuel design or supplier, unreviewed design or performance analysis methods, significant changes in fuel design, new operating procedures:
   NFS intends to apply 10CFR50.59 to the Q2R6C7 reload unless MCPR Technical Specification change is required.

7. The number of fuel assemblies.

   a. Number of assemblies in core: 724

   b. Number of assemblies in spent fuel pool: 1140

8. The present licensed spent fuel pool storage capacity and the size of any increase in licensed storage capacity that has been requested or is planned in number of fuel assemblies:

   a. Licensed storage capacity for spent fuel: 3897

   b. Planned increase in licensed storage: 0

9. The projected date of the last refueling that can be discharged to the spent fuel pool assuming the present licensed capacity: 2003

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Q.C.O.S.R.

VIII. GLOSSARY

The following abbreviations which may have been used in the Monthly Report, are defined below:

ACAD/CAM	-	Atmospheric Containment Atmospheric Dilution/Containment Atmospheric Monitoring
ANSI	-	American National Standards Institute
APRM	-	Average Power Range Monitor
ATWS	-	Anticipated Transient Without Scram
BWR	-	Boiling Water Reactor
CRD	-	Control Rod Drive
EHC	-	Electro-Hydraulic Control System
EOF	-	Emergency Operations Facility
GSEP	-	Generating Stations Emergency Plan
HEPA	-	High-Efficiency Particulate Filter
HPCI	-	High Pressure Coolant Injection System
HRSS	-	High Radiation Sampling System
IPCLRT	-	Integrated Primary Containment Leak Rate Test
IRM	-	Intermediate Range Monitor
ISI	-	Inservice Inspection
LER	-	Licensee Event Report
LLRT	-	Local Leak Rate Test
LPCI	-	Low Pressure Coolant Injection Mode of RHRS
LPRM	-	Local Power Range Monitor
MAPLHGR	-	Maximum Average Planar Linear Heat Generation Rate
MCPR	-	Minimum Critical Power Ratio
MFLCPR	-	Maximum Fraction Limiting Critical Power Ratio
MPC	-	Maximum Permissible Concentration
MSIV	-	Main Steam Isolation Valve
NIOSH	-	National Institute for Occupational Safety and Health
PCI	-	Primary Containment Isolation
PCIOMR	-	Preconditioning Interim Operating Management Recommendations
RBCCW	-	Reactor Building Closed Cooling Water System
RBM	-	Rod Block Monitor
RCIC	-	Reactor Core Isolation Cooling System
RHRS	-	Residual Heat Removal System
RPS	-	Reactor Protection System
RWM	-	Rod Worth Minimizer
SBGTS	-	Standby Gas Treatment System
SBLC	-	Standby Liquid Control
SDC	-	Shutdown Cooling Mode of RHRS
SDV	-	Scram Discharge Volume
SRM	-	Source Range Monitor
TBCCW	-	Turbine Building Closed Cooling Water System
TIP	-	Traveling Incore Probe
TSC	-	Technical Support Center