

ATTACHMENT 1

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b. With the pre-heaters tested in 4.6.1.8.a and 4.6.1.8.d.5 inoperable, restore the inoperable pre-heaters to operable status within 7 days, or file a Special Report in accordance with Specification 6.9.2 within 30 days specifying the reason for inoperability and the planned actions to return the pre-heaters to operable status.

CONTAINMENT SYSTEMS

ANNULUS VENTILATION SYSTEM

LIMITING CONDITION FOR OPERATION

3.6.1.8 Two independent Annulus Ventilation Systems shall be OPERABLE.

APPLICABILITY: MODES 1, 2, 3, and 4.

ACTION:

for reasons other than the pre-heaters tested in 4.6.1.8.a and 4.6.1.8.d.5

With one Annulus Ventilation System inoperable, restore the inoperable system to OPERABLE status within 7 days or be in at least HOT STANDBY within the next 6 hours and in COLD SHUTDOWN within the following 30 hours.

SURVEILLANCE REQUIREMENTS

4.6.1.8 Each Annulus Ventilation System shall be demonstrated OPERABLE:

- a. At least once per 31 days on a STAGGERED TEST BASIS, by initiating, from the control room, flow through the HEPA filters and charcoal adsorbers and verifying that the system operates for at least 10 hours with the pre-heaters operating;
- b. At least once per 18 months, or (1) after any structural maintenance on the HEPA filter or charcoal adsorber housings, or (2) following painting, fire, or chemical release in any ventilation zone communicating with the system, by:
 - 1) Verifying that the ventilation system satisfies the in-place penetration and bypass leakage testing acceptance criteria of less than 1% and uses the test procedure guidance of Regulatory Positions C.5.a, C.5.c and C.5.d of Regulatory Guide 1.52, Revision 2, March 1978, and the system flow rate is 8000 cfm \pm 10%;
 - 2) Verifying within 31 days after removal that a laboratory analysis of a representative carbon sample obtained in accordance with Regulatory Position C.6.b of Regulatory Guide 1.52, Revision 2, March 1978, ~~meets the laboratory testing criteria of Regulatory Position C.6.a of Regulatory Guide 1.52, Revision 2, March 1978, for a methyl iodide penetration of less than 1% (Unit 2), and meets the laboratory testing criteria of Regulatory Position C.6.a of Regulatory Guide 1.52, Revision 2, March 1978, as supplemented by ASTM D3803-86, Test Method A, for a methyl iodide penetration of less than 0.71% (Unit 1)*; and~~
and tested per ASTM D3803-86 has 4%
3) Verifying a system flow rate of 8000 cfm \pm 10% during system operation when tested in accordance with ANSI N510-1975.

~~This specification for Unit 1 shall apply until July 16, 1991. Thereafter, this specification for Unit 1 shall read the same as for Unit 2.~~

CONTAINMENT SYSTEMS

SURVEILLANCE REQUIREMENTS (Continued)

- c. After every 720 hours of charcoal adsorber operation, by verifying within 31 days after removal that a laboratory analysis of a representative carbon sample obtained in accordance with Regulatory Position C.6.b of Regulatory Guide 1.52, Revision 2, March 1978, ~~meets the laboratory testing criteria of Regulatory Position C.6.a of Regulatory Guide 1.52, Revision 2, March 1978, for a methyl iodide penetration of less than 1% (Unit 2), and meets the laboratory testing criteria of Regulatory Position C.6.a of Regulatory Guide 1.52, Revision 2, March 1978, as supplemented by ASTM D3803-86, Test Method A, for a methyl iodide penetration of less than 0.71% (Unit 1)*;~~
- and tested per ASTM D3803-86 has
- d. At least once per 18 months, by: 4%
- 1) Verifying that the pressure drop across the combined HEPA filters and charcoal adsorber banks is less than 6 inches Water Gauge while operating the system at a flow rate of 8000 cfm \pm 10%;
 - 2) Verifying that the system starts automatically on any Phase B Isolation test signal;
 - 3) Verifying that the filter cooling electric motor-operated bypass valves can be opened;
 - 4) Verifying that each system produces a negative pressure of greater than or equal to 0.5 inch W.G. in the annulus within 22 seconds after a start signal and that this negative pressure goes to -3.5 inches W.G. within 48 seconds after the start signal. Verifying that upon reaching a negative pressure of -3.5 inches W.G. in the annulus, the system switches into its recirculation mode of operation and that the time required for the annulus pressure to increase to 0.5 inch W.G. is greater than or equal to 278 seconds; A + a nominal voltage of 600 VAC.
 - 5) Verifying that the pre-heaters dissipate 43.0 ± 6.4 kW (Unit 2) and $43.0 \pm 6.4 / -17.5$ kW (Unit 1)* when tested in accordance with ANSI N510-1975.
- e. After each complete or partial replacement of a HEPA filter bank, by verifying that the HEPA filter bank satisfies the in-place penetration and bypass leakage testing acceptance criteria of less than 1% in accordance with ANSI N510-1975 for DOP test aerosol while operating the system at a flow rate of 8000 cfm \pm 10%; and
- f. After each complete or partial replacement of a charcoal adsorber bank, by verifying that the charcoal adsorber satisfies the in-place penetration and bypass leakage testing acceptance criteria of less than 1% in accordance with ANSI N510-1975 for a halogenated hydrocarbon refrigerant test gas while operating the system at a flow rate of 8000 cfm \pm 10%.

~~*This specification for Unit 1 shall apply until July 16, 1991. Thereafter, this specification for Unit 1 shall read the same as for Unit 2.~~

PLANT SYSTEMS

3/4.7.6 CONTROL AREA VENTILATION SYSTEM

LIMITING CONDITION FOR OPERATION

3.7.6 Two independent Control Area Ventilation Systems shall be OPERABLE.

APPLICABILITY: ALL MODES

ACTION: (Units 1 and 2)

MODES 1, 2, 3 and 4:

a. With one Control Area Ventilation System inoperable, restore the inoperable system to OPERABLE status within 7 days or be in at least HOT STANDBY within the next 6 hours and in COLD SHUTDOWN within the following 30 hours.

MODES 5 and 6:

- a. With one Control Area Ventilation System inoperable, restore the inoperable system to OPERABLE status within 7 days or initiate and maintain operation of the remaining OPERABLE Control Area Ventilation System in the recirculation mode; and
- b. With both Control Area Ventilation Systems inoperable, or with the OPERABLE Control Area Ventilation System, required to be in the recirculation mode by ACTION a., not capable of being powered by an OPERABLE emergency power source, suspend all operations involving CORE ALTERATIONS or positive reactivity changes.

The provisions of Specification 3.0.4 are not applicable.

SURVEILLANCE REQUIREMENTS

4.7.6 Each Control Area Ventilation System shall be demonstrated OPERABLE:

- a. At least once per 12 hours, by verifying that the control room air temperature is less than or equal to 90°F;
- b. At least once per 31 days on a STAGGERED TEST BASIS, by initiating, from the control room, flow through the HEPA filters and charcoal adsorbers and verifying that the system operates for at least 10 hours with the heaters operating;

With the heaters tested in 4.7.6.b and 4.7.6.e.4 inoperable, restore the inoperable heaters to operable status within 7 days, or file a Special Report in accordance with specification 6.9.2, within 30 days specifying the reason for inoperability and the planned actions to return the heaters to operable status.

for reasons other than the heaters specified in 4.7.6.a and 4.7.6.e.4

PLANT SYSTEMS

SURVEILLANCE REQUIREMENTS (Continued)

- c. At least once per 18 months, or (1) after any structural maintenance on the HEPA filter or charcoal adsorber housings, or (2) following painting, fire or chemical release in any ventilation zone communicating with the system, by:

- 1) Verifying that the system satisfies the in-place penetration and bypass leakage testing acceptance criteria of less than 1% and uses the test procedure guidance of Regulatory Positions C.5.a, C.5.c, and C.5.d of Regulatory Guide 1.52, Revision 2, March 1978, and the system flow rate is $2000 \text{ cfm} \pm 10\%$;

- 2) Verifying, within 31 days after removal, that a laboratory analysis of a representative carbon sample obtained in accordance with Regulatory Position C.6.b of Regulatory Guide 1.52, Revision 2, March 1978, ~~meets the laboratory testing criteria of Regulatory Position C.6.a of Regulatory Guide 1.52, Revision 2, March 1978, for a methyl iodide penetration of less than 0.175%, and~~

- 3) Verifying a system flow rate of $2000 \text{ cfm} \pm 10\%$ during system operation when tested in accordance with ANSI N510-1975.

- d. After every 720 hours of charcoal adsorber operation, by verifying within 31 days after removal, that a laboratory analysis of a representative carbon sample obtained in accordance with Regulatory Position C.6.b of Regulatory Guide 1.52, Revision 2, March 1978, ~~meets the laboratory testing criteria of Regulatory Position C.6.a of Regulatory Guide 1.52, Revision 2, March 1978, for a methyl iodide penetration of less than 0.175%,~~

- e. At least once per 18 months, by:

- 1) Verifying that the pressure drop across the combined pre-filters, HEPA filters and charcoal adsorber banks is less than 5 inches Water Gauge while operating the system at a flow rate of $2000 \text{ cfm} \pm 10\%$;
- 2) Verifying that upon actuation of a diesel generator sequencer the system automatically switches into a mode of operation with flow through the HEPA filters and charcoal adsorber banks;
- 3) Verifying that the system maintains the control room at a positive pressure of greater than or equal to 1/8 inch W.G. relative to the outside atmosphere during system operation; and
At a nominal voltage of 600 VAC
- 4) Verifying that the heaters dissipate $10 \pm 1.0 \text{ kW}$ when tested in accordance with ANSI N510-1975.

PLANT SYSTEMS

SURVEILLANCE REQUIREMENTS (Continued)

- f. After each complete or partial replacement of a HEPA filter bank, by verifying that the HEPA filter bank satisfies the in-place penetration and bypass leakage testing acceptance criteria of less than 1% in accordance with ANSI N510-1975 for a DOP test aerosol while operating the system at a flow rate of 2000 cfm \pm 10%; and
- g. After each complete or partial replacement of a charcoal adsorber bank, by verifying that the charcoal adsorber satisfies the in-place penetration and bypass leakage testing acceptance criteria of less than 1% in accordance with ANSI N510-1975 for a halogenated hydrocarbon refrigerant test gas while operating the system at a flow rate of 2000 cfm \pm 10%.

PLANT SYSTEMS

BASES

STANDBY NUCLEAR SERVICE WATER POND (Continued)

The limitations on minimum water level and maximum temperature are based on providing a 30-day cooling water supply to safety-related equipment without exceeding their design basis temperature and is consistent with the recommendations of Regulatory Guide 1.27, "Ultimate Heat Sink for Nuclear Plants," March 1974. The Surveillance Requirements specified for the dam inspection will conform to the recommendations of Regulatory Guide 1.127, Revision 1, March 1978.

3/4.7.6 CONTROL AREA VENTILATION SYSTEM

The OPERABILITY of the Control Area Ventilation System ensures that: (1) the ambient air temperature does not exceed the allowable temperature for continuous duty rating for the equipment and instrumentation cooled by this system, and (2) the control room will remain habitable for operations personnel during and following all credible accident conditions. Cumulative operation of the system with the heaters on for 10 hours over a 31-day period is sufficient to reduce the buildup of moisture on the adsorbers and HEPA filters. *Add 1* The OPERABILITY of this system in conjunction with control room design provisions *from* is based on limiting the radiation exposure to personnel occupying the control room to 5 rem or less whole body, or its equivalent. This limitation is *Attached* consistent with the requirements of General Design Criterion 19 of Appendix A, 10 CFR 50. ANSI N510-1975 will be used as a procedural guide for surveillance testing.

3/4.7.7 AUXILIARY BUILDING FILTERED VENTILATION EXHAUST SYSTEM

The OPERABILITY of the Auxiliary Building Filtered Ventilation Exhaust System ensures that radioactive materials leaking from the ECCS equipment within the auxiliary building following a LOCA are filtered prior to reaching the environment. The operation of this system and the resultant effect on offsite dosage calculations were assumed in the accident analyses. ANSI N510-1980 will be used as a procedural guide for surveillance testing. The methyl iodide penetration test criterion for the carbon samples has been established at 10% (i.e., 90% removal) which is greater than the iodine removal in the accident analysis.

CONTAINMENT SYSTEMS

BASES

3/4.6.1.7 REACTOR BUILDING STRUCTURAL INTEGRITY

This limitation ensures that the structural integrity of the containment reactor building will be maintained comparable to the original design standards for the life of the facility. Structural integrity is required to provide: (1) protection for the steel vessel from external missiles, (2) radiation shielding in the event of a LOCA, and (3) an annulus surrounding the steel vessel that can be maintained at a negative pressure during accident conditions. A visual inspection is sufficient to demonstrate this capability.

3/4.6.1.8 ANNULUS VENTILATION SYSTEM

The OPERABILITY of the Annulus Ventilation System ensures that during LOCA conditions, containment vessel leakage into the annulus will be filtered through the HEPA filters and charcoal adsorber trains prior to discharge to the atmosphere. Cumulative operation of the system with the heaters on for 10 hours over a 31-day period is sufficient to reduce the buildup of moisture on the adsorbers and HEPA filters. ~~This requirement is necessary to meet the assumptions used in the accident analyses and limit the SITE BOUNDARY radiation doses to within the dose guideline values of 10 CFR Part 100 during LOCA conditions. ANSI N510-1975 will be used as a procedural guide for surveillance testing. ASTM D3803-86, Test Method A, will be used for Unit 1 surveillance testing (laboratory test) for methyl iodide penetration in lieu of the laboratory test specified in Regulatory Guide 1.52, Rev. 2, March 1978, Regulatory Position G.6.a. The ASTM D3803-86 test method is used for a relative humidity of 95% at 30°C. The use of this test and the acceptance criterion of a methyl iodide penetration of less than 0.71% are consistent with assumed decontamination efficiencies of 95%. This change resulted from lower VE system heater capacity on Unit 1.~~

3/4.6.1.9 CONTAINMENT VENTILATION SYSTEM

The containment purge supply and exhaust isolation valves for the lower compartment (24-inch) and instrument room (12-inch and 24-inch) are required to be sealed closed during plant operations since these valves have not been demonstrated capable of closing during a LOCA. Maintaining these valves sealed closed during plant operation ensures that excessive quantities of radioactive material will not be released via the Containment Purge System. To provide assurance that these containment valves cannot be inadvertently opened, the valves are sealed closed in accordance with Standard Review Plan 6.2.4 which includes mechanical devices to seal or lock the valve closed, or prevents power from being supplied to the valve operator.

The use of the containment purge lines is restricted to the purge supply and exhaust isolation valves in the upper compartment (24-inch) since, unlike the valves in the lower compartment and instrument room, the upper compartment valves will close during a LOCA. Therefore, the SITE BOUNDARY dose guideline values of 10 CFR Part 100 would not be exceeded in the event of an accident during containment purging operation. Operation with these valves open will be limited to 250 hours during a calendar year.

Leakage integrity tests with a maximum allowable leakage rate for containment purge supply and exhaust supply valves will provide early indication of resilient material seal degradation and will allow opportunity for repair before gross leakage failures could develop. The 0.60 L leakage limit of Specification 3.6.1.2b, shall not be exceeded when the leakage rates determined by the leakage integrity tests of these valves are added to the previously determined total for all valves and penetrations subject to Type B and C tests.

Noted from
Heater Operation
Attached.
IS not

1. Because the carbon adsorber filter decontamination efficiency is verified by the ASTM D3803-89 test method without the use of the moisture reducing heaters, the decontamination efficiency used in the dose calculation is not dependent on heater operation. The heaters serve to reduce the moisture buildup in the carbon filters and extend the useful filter life.

ATTACHMENT 2

McGUIRE NUCLEAR STATION
TECHNICAL SPECIFICATION CHANGE REQUEST

BACKGROUND

During a review of the HVAC systems at Catawba Nuclear Station it was discovered that the pre-heaters in some ESF filter units were not conservatively sized for all postulated operating modes. A station specific review revealed that this problem also applied to McGuire. The pre-heaters are used to control the relative humidity of the influent air entering the carbon adsorber. These filters were designed in a manner that assumes the heaters maintain the relative humidity of the air at 70% or less. Duke Power's review revealed that during postulated low voltage conditions with loss of one of the two offsite power sources and all plant auxiliaries of the unit aligned to the other power source through the remaining step-up transformer with a concurrent LOCA, sufficient power may not be supplied to these heaters to enable them to maintain the less than or equal to 70% relative humidity. The affected systems are the Annulus Ventilation System and the Control Area Ventilation System.

Five (5) different options were considered for permanently addressing this relative humidity problem. The options were:

- 1) Increase the minimum voltage available
- 2) Provide supplemental heaters
- 3) Restrict upper flow limit
- 4) Reduce upper and lower flow limits
- 5) Change carbon test to factor in high humidity (95%)

Option (1) was rejected since this solution would create problems during normal operation. The low voltage concern is the result of a rare series of events outlined earlier. Increasing the minimum voltage to provide enough heater capacity during a low voltage event would cause over voltage concerns during normal operation.

Option (2) was rejected because the additional heaters and associated controls are costly and would make the system needlessly more complex. This option would also require additional emergency power during loss of preferred power conditions, reducing the spare power margin available on the diesels.

Option (3) would require that the flow be restricted through the filter units. This would allow the heaters to properly control humidity in a degraded bus situation. This option was rejected because of the increased operator burden caused by the flow restrictions. With the flow margin reduced, operators would have a very restrictive flow range which could lead to system unavailability.

Option (4) would relieve the flow margin restriction of Option (3) by decreasing the lower flow parameter. Even though there is no increased operator burden with Option (4), it was rejected because of possible increases in dose consequences. This is most apparent in the Annulus Ventilation System. Reducing the flow range would increase the time required to draw the annulus to a negative pressure which significantly increases the Exclusion Area Boundary (EAB) (2 hour) thyroid dose. For the Control Area Ventilation System, pressurization of the control room to the TS required pressure would be difficult to obtain at the lower flow parameter.

Option (5) involved changing the carbon penetration test method to factor in high humidity. This option was chosen even though it will require a change to the TS and will require more frequent carbon change-out. The benefits of this option are: (1) no increased burden on operator due to flow restrictions, (2) was the subject of early discussions between the NRC and Duke Power and appeared to be the option the NRC wanted Duke Power to pursue (reference temporary Technical Specification change submitted 5/9/90), and (3) no increase or change in the dose consequences. This option does increase operator burden by requiring more frequent carbon change out, however, this is acceptable to the station.

PURPOSE

The purpose of this Technical Specification amendment is to address humidity control associated with the Annulus Ventilation (VE) and the Control Area Ventilation (VC) Systems.

TERMS

The following terms are defined as they apply to this document and to provide clarity to the discussion.

- 1) bypass leakage (BL) - the percentage of flow that passes around a filter without being filtered.
- 2) penetration (PE) - the amount of methyl iodide which will pass through a sample of carbon without being adsorbed. This value can be established by testing per ASTM D3803-89.

- 3) decontamination efficiency (DE) - the percent of radioactive iodine that will be removed by a filter system. This value is a function of bypass leakage and penetration.

$$DE : 100\% - (BL + PE)$$

- 4) carbon filter efficiency - same as decontamination efficiency.

CHANGES TO TECHNICAL SPECIFICATIONS AND TECHNICAL DISCUSSION

1. CHANGES TO TS

The Surveillance Requirement (SR) 4.6.1.8.b.2, 4.6.1.8.c, 4.7.6.c.2, and 4.7.6.d are changed to indicate that the laboratory testing criteria of ASTM D3803-89 will be used.

TECHNICAL JUSTIFICATION

The proposed carbon testing standard, ASTM D3803-89, is a stringent procedure for establishing the capability of new and used activated carbon. The following table compares this standard with the original TS required test method and ASTM D3803-86 (temporary TS test method for Annulus Ventilation) for used carbons.

Test Period	Original Test Method	ASTM D3803-86 Test Method A	ASTM D3803-89
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Pre-	not required	not required	30°C 95%RH
Equilibration			16 hours
Equilibration 95%RH	not required	not required	30°C 2 hours
Challenge 95%RH (Feed)	80°C 70%RH 2 hours	30°C 95%RH 2 hours	30°C 1 hour

The major difference between the ASTM D3803-89 and the other test methods is that the ASTM D3803-89 method requires the carbon beds to be pre-conditioned with 30°C and 95% relative humidity air for eighteen (18) hours before the methyl iodide challenge (feed) period. This

approach is intended to make the carbon test repeatable so that results from similar tests can be compared. The pre-conditioning is conservative because it saturates the carbon beyond the conditions expected during Design Basis Events for the Annulus Ventilation and Control Area Ventilation Systems. The water vapor competes with the methyl iodide for adsorption sites on the carbon, therefore, the higher the relative humidity the harder it is for methyl iodide to be adsorbed. ASTM D3803-89 is a more repeatable test for carbon adsorber, and the pre-equilibration period at 95% relative humidity makes it more stringent than previous standards.

2. CHANGES TO TS

SRs 4.6.1.8.b.2 and 4.6.1.8.c are changed to indicate that a methyl iodide penetration of 4% will be used for the Annulus Ventilation System and 4.7.6.c.2 and 4.7.6.d are changed to indicate that a methyl iodide penetration of 0.95% will be used for the Control Area Ventilation System as the acceptance criteria for carbon adsorber testing.

TECHNICAL JUSTIFICATION

Reference to the test criteria of Regulatory Guide 1.52 will be removed from TS 4.6.1.8.b.2, 4.6.1.8.c, 4.7.6.c.2 and 4.7.6.d, because the Regulatory Guide, Revision 2, March 1978, does not address the testing of a system without humidity control which operate outside the primary containment.

Because of the pre-equilibration period, which does not exist in previous carbon adsorber test standards, the carbon is tested at a more conservative point. Using the ASTM D3803-89 testing standard would always be expected to give a more conservative methyl iodide penetration value than current test methods. The ASTM D3803-89 test method is also conservative with respect to the plant conditions expected during an accident. Postulated accident conditions do not subject the carbon to saturated conditions, therefore, the radioactive iodine penetration during an actual accident would be lower than that predicted by the lab. A 4% methyl iodide penetration is acceptable for the Annulus Ventilation System and a 0.95% methyl iodide penetration is acceptable for the Control Area Ventilation System since added conservatism is built into the new carbon adsorber test, and current Design Bases decontamination efficiencies are met using this value.

Duke Power believes that this method for defining penetration is conservative for the following reasons:

- a) The scope of ASTM D3803-89 describes this standard as "a very stringent procedure" and says that it "is recommended for the quantification of the degradation of used carbons."
- b) Limited testing done by Duke Power shows that testing done per the 1989 revision of ASTM D3803 will result in more frequent carbon change out than testing per the 1986 revision is used. Per this TS change, Duke Power will generally have newer, fresher carbon in its filter systems.
- c) The 1989 revision also requires that the carbon be pre-saturated before being tested. Saturating the carbon limits its ability to adsorb iodine. Postulated accident scenarios do not subject the carbon adsorber to saturated air, therefore, testing per the 1989 revision will yield conservative results relative to actual adsorption ability.
- d) Design basis dose analysis for McGuire show that the combination of all ESF systems (ie., containment sprays, ice condenser, HEPA and carbon filters) and most importantly the containment itself, serve to keep offsite and onsite doses well below regulatory limits. The relative importance of the carbon adsorbers to mitigate iodine releases is questionable in light of source term studies over the last decade which predict only a small elemental iodine constituent in the release.

3. CHANGES TO TS

The ACTION for TS 3.6.1.8, Annulus Ventilation System, and 3.7.6, Control Area Ventilation System, are changed to indicate that they apply for reasons other than pre-heaters. New ACTIONS have been added to indicate that if the heaters are inoperable, they will be fixed within 7 days, or a report filed with the NRC.

TECHNICAL JUSTIFICATION

Since the Design Basis decontamination efficiencies can be met for the Annulus and the Control Area Ventilation Systems using a test that assumes no heaters, operability of the systems will no longer be dependent on heater operability. The heater testing requirements will remain the same as they are currently, and the heaters will be required to be fixed in a timely manner in the event of failure. Even though the heaters will remain in service, no credit will be taken for them, resulting in additional margin.

4. CHANGES TO TS

"At a nominal voltage of 600 VAC" has been added to SRs 4.6.1.8.d.5 and 4.7.6.e.4.

TECHNICAL JUSTIFICATION

The statement "at a nominal voltage of 600 VAC" has been added to the heater testing requirements. This clarifies how the heater testing should be done. With the heaters tested at a nominal voltage of 600 VAC, a failure of the heater surveillance would be indicative of a heater problem, not a system problem.

5. CHANGES TO TS

The sections of TS 3.6.1.8, Annulus Ventilation System, which apply only until July 16, 1991, have been deleted. This change is administrative in nature.

6. The TS Bases have been marked up to reflect these changes.
NO SIGNIFICANT HAZARDS ANALYSIS

10 CFR 50.92 states that a proposed amendment involves no significant hazards consideration if operation in accordance with the proposed amendment would not:

- 1) Involve a significant increase in the probability or consequences of an accident previously evaluated; or
- 2) Create the possibility of a new or different kind of accident from any accident previously evaluated; or
- 3) Involve a significant reduction in the margin of safety.

This proposed TS amendment will not increase the probability or consequences of an accident which has been previously evaluated. No physical changes will be made to the plant, therefore, there is no increased probability of an accident. As discussed in the Technical Justification, the decontamination efficiencies of the filters remain unchanged. Because of this, the offsite dose and Control Room dose calculation results are unaffected. The dose calculations remain conservative due to the conservative assumptions in the source term dose conversion factors and release times. In addition to requiring the carbon adsorber to meet Design Basis decontamination efficiencies at 95% relative humidity, additional margin, for which no credit is taken, will be provided by the heaters. For the reasons stated above, there will be no increase in the consequences of an accident previously evaluated.

This proposed amendment to the TS does not create the possibility of a new or different kind of accident from any accident previously evaluated. This proposed TS change will

not cause any physical changes to the plant or changes to operating procedures. Because the plant will continue to operate the same way it does now, this proposed amendment does not create the possibility of any new or different accident from any previously evaluated.

This proposed TS change will not cause a significant reduction in the margin of safety. The new test method is more restrictive than the previous test methods, and based on limited testing, Duke Power expects to have to change out carbon more frequently. The change in the allowed methyl iodide penetration was made to support the change in test method, does not represent a significant decrease in the margin of safety. It represents the requirement of the test standard to pre-saturate the carbon adsorber. This pre-saturation causes a higher penetration during testing, and is conservative with respect to Design Basis Events. The test method D3803-89 is expected to provide a penetration value during testing which is higher than what would be expected during a Design Basis Event. These conservative results reflect the fact that the new test conditions are more harsh than expected plant conditions. An added conservatism is that even though no credit is taken for the heaters, they will be tested and maintained, so the expected relative humidity of air entering the carbon adsorber would never be expected to reach 95%.

The addition of "at a nominal voltage of 600 VAC" to the heater SR is administrative, and clarifies that the purpose of the requirement is to detect heater degradation. This change involves no significant hazards consideration.

Footnotes and statements related to the footnotes which expire on July 16, 1991 have been removed. This change is administrative, and involves no significant hazards consideration.

The proposed Technical Specification change has been reviewed against the criteria of 10 CFR 51.22 for environmental considerations. As shown above, the proposed change does not involve significant hazards consideration or increase individual or cumulative occupational radiation exposure. Based on this, the proposed amendment meets the criteria given in 10 CFR 51.22(c)(9) for categorical exclusion from the requirements for an Environmental Impact Statement.