QUAD-CITIES NUCLEAR POWER STATION

UNITS 1 AND 2

MONTHLY PERFORMANCE REPORT

MARCH 1982

COMMONWEALTH EDISON COMPANY

AND

IOWA-ILLINOIS GAS & ELECTRIC COMPANY

NRC DOCKET NOS. 50-254 AND 50-265

LICENSE NOS. DPR-29 AND DPR-30

TABLE OF CONTENTS

I. INTRODUCTION

Quad-Cities Nuclear Power Station is composed of two Boiling Water Reactors, each with a Maximum Dependable Capacity of 769 MWe net, located in Cordova, Illinois. The Station is jointly owned by Commonwealth Edison Company and Iowa-Illinois Gas & Electric Company. The Nuclear Steam Supply Systems are General Electric Company Boiling Water Reactors. The Architect/Engineer was Sargent & Lundy, Incorporated, and the primary construction contractor was United Engineers & Constructors. The condenser cooling method is a closed cycle spray canal, and the Mississippi River is the condenser cooling water source. The plant is subject to license numbers DPR-29 and DPR-30, issued October 1, 1971, and March 21, 1972, respectively, pursuant to Docket Numbers 50-254 and 50-265. The date of initial reactor criticalities for Units 1 and 2 respectively were October 18, 1971, and April 26, 1972. Commercial generation of power began on February 18, 1973 for Unit 1 and March 10, 1973 for Unit 2.

This report was compiled by Becky Brown and Erich Weinfurter, telephone number 309-654-2241, extensions 127 and 192.

II. SUMMARY OF OPERATING EXPERIENCE

A. UNIT ONE

March 1-6: The unit started the month holding at maximum attainable load as coastdown began for the September, 1982, end of cycle six refueling outage. On March 6, at 0030 hours, a load drop was initiated at 100 MWe/hour to 700 MWe for weekly Turbine tests. At 0215 hours, load was increased 50 MWe/hour to 760 MWe then 5 MWe/hour to 785 MWe which was obtained Marcn 6 at 0800 hours.

March 7-13: The unit continued to coastdown at maximum attainable load until March 12 at 2345 hours when a load drop to 700 MWe at 100 MWe/hour was initiated for weekly Turbine tests. On March 13, at 0055 hours, load was increased 50 MWe/hour for one hour, then 5 MWe/hour until 760 MWe was achieved at 0400 hours.

March 14-21: On March 19, at 2310 hours, a load drop was initiated to reduce load to 600 MWe by 0010 hours on March 20. Weekly Turbine tests were completed along with control rod pattern movements by 0130 hours. Load was increased 40 MWe/hour for one hour, then 5 MWe/hour to maximum attainable load at this point in coastdown.

March 22-31: The unit was holding at a load of 700 MWe, on March 29, when condenser vacuum started to decrease due to an empty loop seal in the steam seal piping. A load drop to 300 MWe was initiated in an attempt to increase the condenser vacuum. At 0733 hours, March 29, the Reactor scrammed on low condenser vacuum. The Reactor became critical at 1245 hours, and the Generator was put on line at 1645 hours. At 1830 hours all control rods were fully withdrawn and load was increased to 777 MWe by 0530 hours, March 31.

B. UNIT TWO

March 1-5: Unit Two began the month continuing to increase load at 5 MWe/hour until March 3 when the unit was holding load for Xenon build-up. The load increase began at 2000 hours, March 3, at 5 MWe/hour until 0845 hours March 4, when a maximum attainable load of 810 MWe was achieved.

March 6-12: On March 6, at 0704 hours, the unit scrammed when the "B" Feedwater Regulating valve failed in the open position causing a Reactor high level. This caused a Turbine trip and subsequently a Reactor scram. The Reactor became critical at 1415 hours and the Generator was on line by 1813 hours. Load was increased 100 MWe/hour to 500 MWe then 50 MWe/hour to 550 MWe where it was held for a Xenon build-up. Load increases were continued at 0915 hours on March 7 until a maximum achievable load of 815 MWe was obtained.

March 13-15: On March 13, from 2302 hours to 0010 hours March 14, a core flow drop test was conducted in order to complete the Cycle 6 Start-up Program. The unit dropped load at 50 MWe/minute to 460 MWe. Load was then increased at 350 MWe/hour to 700 MWe. The weekly Turbine test was completed and a fuel preconditioning ramp continued to 800 MWe. On March 15, at 0100 hours, condensate demineralizer problems necessitated a load drop to 700 MWe; by 0345 hours, load was initiated to 805 MWe.

March 16-28: Maximum attainable load was held except for two load drops for Turbine tests on March 20 and March 27. Load was increased in accordance with normal preconditioning ramp.

March 29-31: Due to the "A" Feedwater Regulating valve locking up, the "A" Feedwater valve was isolated and load was dropped to 520 MWe, at 1215 hours on March 30. By 1230 hours, load was increased 200 MWe/hour to 700 MWe, 20 MWe/hour for one and one-half hours, then 5 MWe/hour to a maximum attainable load of 810 MWe.

III. PLANT OR PROCEDURE CHANGES, TESTS, EXPERIMENTS, AND SAFETY RELATED MAINTENANCE

A. Amendments to Facility License or Technical Specifications

On December 18, 1981, the NRC issued Amendments 75 and 68 to licenses DPR-29 and DPR 30, respectively. This amendment provides the Technical Specification changes needed to allow Units One and Two to be operated with the "A" loops of the RHR Service Water System cross-tied. These changes will be in effect until June 1, 1982.

B. Facility or Procedure Changes Requiring NRC Approval

There were no Facility or Procedure Changes requiring NRC approval for the reporting period.

C. Tests and Experiments Requiring NRC Approval

There were no Tests and Experiments requiring NRC approval for the reporting period.

D. Corrective Maintenance of Safety Related Equipment

The following represents a tabular summary of the safety related maintenance performed on Unit One and Unit Two during the reporting period. The headings indicated in this summary include: Work Request Numbers, LER Numbers, Components, Cause of Malfunctions, Results and Effects on Safe Operation, and Action Taken to Prevent Repetition.

UNIT ONE MAINTENANCE SUMMARY

W.R. NUMBER	LER NUMBER	COMPONENT	CAUSE OF MALFUNCTION	RESULTS & EFFECTS ON SAFE OPERATION	ACTION TAKEN TO PREVENT REPETITION
Q13537		LPRM 16-33B Channel 1	Connector dirty & loose.	Intermittent readings.	Cleaned & tightened connector.
Q13538		LPRM 37-40D Channel 3	Cable connector under the Reactor vessel was dirty.	LPRM reading downscale.	Cleaned the connector and returned to service.
Q14122		LPRM 16-25A Channel 6	The cable connector was corroded.	LPRM is spiking downscale.	Replaced LPRM cable connector under vessel.
Q15930		LPRM 48-49A	The cable connector was corroded.	LPRM reading 11% at zero power.	Replaced LPRM cable connector under vessel.
Q15931		LPRM 16-25C	The cable connector was corroded.	LPRM reading at zero power.	Replaced LPRM cable connector under vessel.
Q14576	81-16/03L	"A" SBGT Train 1/2-7506A	The damper lever counterweight was out of adjustment.	Lever damper on the discharge of blower does not work. The SBGT Train was still operable.	The counterweight was adjusted and the damper operates freely.
Q14577	81-16/03L	"B" SBGT Train 1/2-7506B	The damper level counterweight was out of adjustment.	Lever damper on the discharge of blower does not work. The SBGT Train was still operable.	The counterweight was adjusted and the damper operates freely.

UNIT ONE MAINTENANCE SUMMARY

W.R. NUMBER	LER NUMBER	COMPONENT	CAUSE OF MALFUNCTION	RESULTS & EFFECTS ON SAFE OPERATION	ACTION TAKEN TO PREVENT REPETITION
Q15004		Battery 125 VDC	Grounded wire siren #57.	When Control Room operator sounded the fire warning horn in the Control Room, the 125 V ground alarm came up. The battery was still operable.	The ground was traced and repaired.
Q16146		1B MSL Rad Monitor 1-1705-2B	A faulty circuit board was found.	The monitor spikes downscale.	Repaired chassis; calibrated and re-installed.
Q18055		Core Spray Low Flow Switch FSI-1-1464A & B	The flow switches were out of calibration.	The low flow valves do not auto-open on decreasing Core Spray flow.	The switches were recalibrated and the valves were stroked.
Q18201		1B MSL Rad Monitor 1-1705-2B	The monitor indication was out of calibration.	It was reading less than the other three monitors.	Calibrated and functionally tested.

UNIT TWO MAINTENANCE SUMMARY

W.R. NUMBER	LER NUMBER	COMPONENT	CAUSE OF MALFUNCTION	RESULTS & EFFECTS ON SAFE OPERATION	ACTION TAKEN TO PREVENT REPETITION
Q16643		HPCI 2-2302	Bad outboard seal and shaft nut.	Outboard seal on HP stage. Leaks badly when HPCI is running.	Replaced outboard seal and replaced the shaft nut.
Q17296		RHR Pump Suction Valve 2-1001-7B	The valve operator was faulty.	The valve will not open or close from Control Room. The Reactor was shutdown at the time.	The valve operator was replaced with the operator from the 2-1001-43B. The 43B valve was taken out of service and the interlock was jumpered out.
Q17882		Shutdown Cooling Suction Valve 2-1001-43A	Dirty Bellville washers in motor operator.	Breaker trips when the valve closes.	Installed a grease bypass line and cleaned Bellville washers.
Q17898		Limit Switch MSIV 2-203-2A	The slide contacts & stationary block on the limit switch was worn.	Limit switch which indicates valve less than 90% full open is sticking.	Replaced slide contacts & stationary contact block on limit switch and tested.
Q17735	82-3/01T	CRD 42-07 Insert/Withdrawal Line	Pitting was found on the I.D. of the withdraw line where it fits into the CRD housing flange.	The line is spraying water where the line meets the flange. The Reactor was already shutdown when the leak was discovered.	Ground out the existing seal weld between the pipe and flange. The withdraw line was fillet welded to the back side of the flange.
Q17911		Main Steam Line Rad Monitor RE-1734 A - D	The monitor calibration drifted slightly.	Reading veries as much as 20 difference between the monitors.	Recalibrated A - D monitor.

UNIT TWO MAINTENANCE SUMMARY

W.R. NUMBER	LER NUMBER	COMPONENT	CAUSE OF MALFUNCTION	RESULTS & EFFECTS ON SAFE OPERATION	ACTION TAKEN TO PREVENT REPETITION
Q17609		MO-2-2301-8 HPCI Supply Valve	Worn torque switch in the valve operator.	The valve was still operable.	Replaced torque switch, limit switch, and motor.
Q17244 Q17140	82-1/01T	Clean-up Suction Piping 2-1202-6A	A crack was found in the heat affected zone of one of the welds. A subsequent ultrasonic inspection revealed several linear indications.	The Reactor was shut-down immediately following discovery of the leak. Primary Containment integrity was maintained at all times.	The isolatable portion of the pipe was replaced with low-carbon stain less steel. The non-isolatable portion was repaired using sleeves and weld overlays.
Q09171		250 VDC Battery Charger Feed from MCC 29-2	The breaker and cable was under-sized for the new larger-capacity charger.	The breaker trips when a large load is required from the battery charger.	A larger breaker and cable were installed to carry the required current.

IV. LICENSEE EVENT REPORTS

The following is a tabular summary of all licensee event reports for Quad-Cities Units One and Two occurring during the reporting period, pursuant to the reportable occurrence reporting requirements as set forth in sections 6.6.B.1. and 6.6.B.2. of the Technical Specifications.

UNIT ONE

Licensee Event Report Number	Date	Title of Occurrence
82-4/03L	03-07-82	RCIC Isolation - High Flow/DP
82-5/03L	03-25-82	RCIC Trip on Overspeed

UNIT TWO

There were no Licensee Event Reports for Unit Two for the reporting period.

V. DATA TABULATIONS

The following data tabulations are presented in this report:

A. Operating Data Report

B. Average Daily Unit Power Level

C. Unit Shutdowns and Power Reductions

OPERATING DATA REPORT

DOCKET NO. 50-254

UNIT ONE

DATE April 06 1982

COMPLETED BY Erich Weinfurter

TELEPHONE 309-654-2241x192

OPERATING STATUS

1. Reporting period: 0000 030182 2400 033182 Gross hours in reporting period: 744

2. Currently authorized power level (MWt): 2511 Max.Depend capacity (MWe-Net): 769* Design electrical rating (MWe-Net): 789

3. Power level to which restricted(if any)(MWe-Net): NA

4. Reasons for restriction (if any):

	This Month	Yr.to Date	Cumulative
5. Number of hours reactor was critical	738.8	2144.4	71243.5
6. Reactor reserve shutdown hours	0.0	0.0	3421.9
7. Hours generator on line	734.8	2134.7	63266.2
8. Unit reserve shutdown hours.	0.0	0.0	909.2
9. Gross thermal energy generated(MWH)	1686197	5006518	140064877
10. Gross electrical energy generated(MWH)	547656	1639540	45168473
11. Net electrical energy generated(MWH)	505623	1521233	42105317
12. Reactor service factor	99.3	99.3	82.2
13. Reactor availability factor	99.3	99.3	86.1
14. Unit service factor	98.8	98.8	78.7
15. Unit availability factor	98.8	98.8	79.8
16. Unit capacity factor (Using MDC)	88.4	91.6	63.2
17. Unit capacity factor (Using Des.MWe)	86.1	89.3	61.6
18. Unit forced outage rate	1.2	1.2	7.0

19. Shutdowns scheduled over next 6 months (Type,Date,and Duration of each):

20. If shutdown at end of report period,estimated date of startup NA

*The MDC may be lower than 769 MWe during periods of high ambient temperature due to the thermal performance of the spray canal.

OPERATING DATA REPORT

DOCKET NO. 50-265

UNIT TWO

DATE April 06 1982

COMPLETED BY Erich Weinfurter

TELEPHONE 309-654-2241x192

OPERATING STATUS

1. Reporting period: 0000 030182 / 2400 033182 Gross hours in reporting period: 744

2. Currently authorized power level (MWt): 2511 Max.Depend capacity (MWe-Net): 769* Design electrical rating (MWe-Net): 789

3. Power level to which restricted(if any)(MWe-Net): NA

4. Reasons for restriction (if any):

	This Month	Yr.to Date	Cumulative
5. Number of hours reactor was critical	736.8	1099.7	65951.5
6. Reactor reserve shutdown hours	0.0	0.0	2985.8
7. Hours generator on line	732.9	1079.8	63321.0
8. Unit reserve shutdown hours.	0.0	0.0	702.9
9. Gross thermal energy generated(MWH)	1750579	2378293	130265376
10. Gross electrical energy generated(MWH)	567002	766177	41472417
11. Net electrical energy generated(MWH)	542600	722760	38847344
12. Reactor service factor	99.0	50.9	76.9
13. Reactor availability factor	99.0	50.9	80.4
14. Unit service factor	98.5	50.0	73.8
15. Unit availability factor	98.5	50.0	74.6
16. Unit capacity factor (Using MDC)	94.8	43.5	58.9
17. Unit capacity factor (Using Des.MWe)	92.4	42.4	57.4
18. Unit forced outage rate	1.5	50.0	9.7

19. Shutdowns scheduled over next 6 months (Type,Date,and Duration of each):

20. If shutdown at end of report period,estimated date of startup NA

*The MDC may be lower than 769 MWe during periods of high ambient temperature due to the thermal performance of the spray canal.

APPENDIX B
AVERAGE DAILY UNIT POWER LEVEL

DOCKET NO. 50-254
UNIT ONE
DATE April 06 1982
COMPLETED BY Erich Weinfurter
TELEPHONE 309-654-2241x192

MONTH March 1982

DAY	AVERAGE DAILY POWER LEVEL (MWe-Net)	DAY	AVERAGE DAILY POWER LEVEL (MWe-Net)
1.	738.6	17.	684.5
2.	739.1	18.	681.4
3.	732.4	19.	672.7
4.	731.4	20.	634.5
5.	747.5	21.	701.9
6.	700.2	22.	665.5
7.	728.0	23.	672.5
8.	722.9	24.	673.8
9.	714.7	25.	669.2
10.	707.3	26.	657.5
11.	710.0	27.	685.3
12.	706.1	28.	658.7
13.	703.9	29.	301.8
14.	684.0	30.	578.7
15.	686.8	31.	692.1
16.	684.5		

INSTRUCTIONS

On this form, list the average daily unit power level in MWe-Net for each day in the reporting month. Compute to the nearest whole megawatt.

These figures will be used to plot a graph for each reporting month. Note that when maximum dependable capacity is used for the net electrical rating of the unit, there may be occasions when the daily average power level exceeds the 100% line (or the restricted power level line). In such cases, the average daily unit power output sheet should be footnoted to explain the apparent anomaly

APPENDIX B
AVERAGE DAILY UNIT POWER LEVEL

DOCKET NO. 50-265
UNIT TWO
DATE April 06 1982
COMPLETED BY Erich Weinfurter
TELEPHONE 309-654-2241x192

MONTH March 1982

DAY	AVERAGE DAILY POWER LEVEL (MWe-Net)	DAY	AVERAGE DAILY POWER LEVEL (MWe-Net)
1.	513.3	17.	779.3
2.	723.5	18.	777.3
3.	731.4	19.	775.8
4.	771.8	20.	764.9
5.	794.0	21.	782.4
6.	289.7	22.	759.8
7.	583.7	23.	774.1
8.	723.0	24.	777.5
9.	775.5	25.	765.2
10.	771.0	26.	769.8
11.	775.9	27.	624.8
12.	779.8	28.	731.8
13.	777.4	29.	759.0
14.	714.8	30.	759.5
15.	741.6	31.	769.7
16.	771.3		

INSTRUCTIONS

On this form, list the average daily unit power level in MWe-Net for each day in the reporting month. Compute to the nearest whole megawatt.

These figures will be used to plot a graph for each reporting month. Note that when maximum dependable capacity is used for the net electrical rating of the unit, there may be occasions when the daily average power level exceeds the 100% line (or the restricted power level line). In such cases, the average daily unit power output sheet should be footnoted to explain the apparent anomaly

APPENDIX D
UNIT SHUTDOWNS AND POWER REDUCTIONS

QTP 300-S13
Revision 5
March 1978

DOCKET NO. 050-254
UNIT NAME Quad-Cities Unit One
DATE April 1, 1982
REPORT MONTH March 1982
COMPLETED BY E Weinfurter
TELEPHONE 309-654-2241, ext. 192

*

NO.	DATE	TYPE F OR S	DURATION (HOURS)	REASON	METHOD OF SHUTTING DOWN REACTOR	LICENSEE EVENT REPORT NO.	SYSTEM CODE	COMPONENT CODE	CORRECTIVE ACTIONS/COMMENTS
82-8	820306	S	0.0	B	5	N/A	HA	TURBIN	Load reduction to perform Turbine tests.
82-9	820312	S	0.0	B	5	N/A	HA	TURBIN	Load reduction to perform Turbine tests.
82-10	820319	S	0.0	B	5	N/A	RB	CONROD	Load reduction to perform Turbine tests and perform control rod maneuvers.
82-11	820329	F	9.2	A	3	N/A	HJ	XXXXXX	Reactor scram on Condenser Low Vacuum due to loop seal blowing through.

APPENDIX D
UNIT SHUTDOWNS AND POWER REDUCTIONS

QTP 300-S13
Revision 5
March 1978

DOCKET NO. 050-265

UNIT NAME Quad-Cities Unit Two

DATE April 1, 1982

REPORT MONTH March 1982

COMPLETED BY E Weinfurter

TELEPHONE 309-654-2241, ext. 192

*

NO.	DATE	TYPE F OR S	DURATION (HOURS)	REASON	METHOD OF SHUTTING DOWN REACTOR	LICENSEE EVENT REPORT NO.	SYSTEM CODE	COMPONENT CODE	CORRECTIVE ACTIONS/COMMENTS
82-4	820306	F	9.1	A	3	N/A	CH	VALVOP	Reactor scram on Vessel High Water Level due to "B" Feedwater Regulating valve failing in the open position.
82-5	820313	S	0.0	B	5	N/A	CB	XXXXXX	Load reduction to perform flow drop test and perform Turbine tests.
82-6	820315	F	0.0	A	5	N/A	WC	DEMINX	Load reduction due to Demineralizer problems.
82-7	820320	S	0.0	B	5	N/A	HA	TURBIN	Load reduction to perform Turbine tests.
82-8	820327	S	0.0	B	5	N/A	RB	CONROD	Load reduction to perform control rod maneuvers.
82-9	820330	F	0.0	A	5	N/A	CH	VALVOP	Load reduction to isolate "A" Feedwater regulating valve when the valve started to drift open.

VI. UNIQUE REPORTING REQUIREMENTS

The following items are included in this report based on prior commitments to the commission:

A. MAIN STEAM RELIEF VALVE OPERATIONS

There were no Main Steam Relief Valve Operations for the reporting period.

B. CONTROL ROD DRIVE SCRAM TIMING DATA FOR UNITS ONE AND TWO

There was no Control Rod Drive Scram Timing Data for Units One and Two for the reporting period.

VII. REFUELING INFORMATION

The following information about future reloads at Quad-Cities Station was requested in a January 26, 1978, licensing memorandum (78-24) from D. E. O'Brien to C. Reed, et al., titled "Dresden, Quad-Cities, and Zion Station--NRC Request for Refueling Information", dated January 18, 1978.

QTP 300-S32
Revision 1
March 1978

QUAD-CITIES REFUELING INFORMATION REQUEST

*

1. Unit: 1 Reload: 6 Cycle: 7

2. Scheduled date for next refueling shutdown: Sept 12, 1982

3. Scheduled date for restart following refueling: Dec 4, 1982

4. Will refueling or resumption of operation thereafter require a technical specification change or other license amendment:

   YES

5. Scheduled date(s) for submitting proposed licensing action and supporting information:

   JULY 26, 1982

6. Important licensing considerations associated with refueling, e.g., new or different fuel design or supplier, unreviewed design or performance analysis methods, significant changes in fuel design, new operating procedures:

   IMPLEMENTATION OF THE ODYN TRANSIENT ANALYSIS CODE AND RESULTS
   (MCPR SCRAM TIME DEPENDENCE)

7. The number of fuel assemblies.

   a. Number of assemblies in core: 224 new/724 total

   b. Number of assemblies in spent fuel pool: after the outage 1940

8. The present licensed spent fuel pool storage capacity and the size of any increase in licensed storage capacity that has been requested or is planned in number of fuel assemblies:

   a. Licensed storage capacity for spent fuel: 2920

   b. Planned increase in licensed storage: 4636 new/7556 total

9. The projected date of the last refueling that can be discharged to the spent fuel pool assuming the present licensed capacity:

   LOSS OF FULL CORE DISCHARGE CAPABILITY - 3/84
   LOSS OF RELOAD CORE DISCHARGE CAPABILITY - 2/86

APPROVED
APR 20 1978
Q.C.O.S.R.

QTP 300-S32
Revision 1
March 1978

QUAD-CITIES REFUELING INFORMATION REQUEST

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1. Unit: 2 Reload: 6 Cycle: 7

2. Scheduled date for next refueling shutdown: Feb 27, 1983

3. Scheduled date for restart following refueling: April 23, 1983

4. Will refueling or resumption of operation thereafter require a technical specification change or other license amendment:

   NO

5. Scheduled date(s) for submitting proposed licensing action and supporting information:

   NONE

6. Important licensing considerations associated with refueling, e.g., new or different fuel design or supplier, unreviewed design or performance analysis methods, significant changes in fuel design, new operating procedures:

   NONE

7. The number of fuel assemblies.

   a. Number of assemblies in core: 192 new/724 total

   b. Number of assemblies in spent fuel pool: after the outage 2132

8. The present licensed spent fuel pool storage capacity and the size of any increase in licensed storage capacity that has been requested or is planned in number of fuel assemblies:

   a. Licensed storage capacity for spent fuel: 2920

   b. Planned increase in licensed storage: 4636 new/7556 total

9. The projected date of the last refueling that can be discharged to the spent fuel pool assuming the present licensed capacity:

   LOSS OF FULL CORE DISCHARGE CAPABILITY - 3/84
   LOSS OF RELOAD CORE DISCHARGE CAPABILITY - 2/86

APPROVED
APR 20 1978
Q.C.O.S.R.

VIII. GLOSSARY

The following abbreviations which may have been used in the Monthly Report, are defined below:

ACAD/CAM	-	Atmospheric Containment Atmospheric Dilution/Containment Atmospheric Monitoring
ANSI	-	American National Standards Institute
APRM	-	Average Power Range Monitor
ATWS	-	Anticipated Transient Without Scram
BWR	-	Boiling Water Reactor
CRD	-	Control Rod Drive
EHC	-	Electro-Hydraulic Control System
EOF	-	Emergency Operations Facility
GSEP	-	Generating Stations Emergency Plan
HEPA	-	High-Efficiency Particulate Filter
HPCI	-	High Pressure Coolant Injection System
HRSS	-	High Radiation Sampling System
IPCLRT	-	Integrated Primary Containment Leak Rate Test
IRM	-	Intermediate Range Monitor
ISI	-	Inservice Inspection
LER	-	Licensee Event Report
LLRT	-	Local Leak Rate Test
LPCI	-	Low Pressure Coolant Injection Mode of RHRS
LPRM	-	Local Power Range Monitor
MAPLHGR	-	Maximum Average Planar Linear Heat Generation Rate
MCPR	-	Minimum Critical Power Ratio
MFLCPR	-	Maximum Fraction Limiting Critical Power Ratio
MPC	-	Maximum Permissible Concentration
MSIV	-	Main Steam Isolation Valve
NIOSH	-	National Institute for Occupational Safety and Health
PCI	-	Primary Containment Isolation
PCIOMR	-	Preconditioning Interim Operating Management Recommendations
RBCCW	-	Reactor Building Closed Cooling Water System
RBM	-	Rod Block Monitor
RCIC	-	Reactor Core Isolation Cooling System
RHRS	-	Residual Heat Removal System
RPS	-	Reactor Protection System
RWM	-	Rod Worth Minimizer
SBGTS	-	Standby Gas Treatment System
SBLC	-	Standby Liquid Control
SDC	-	Shutdown Cooling Mode of RHRS
SDV	-	Scram Discharge Volume
SRM	-	Source Range Monitor
TBCCW	-	Turbine Building Closed Cooling Water System
TIP	-	Traveling Incore Probe
TSC	-	Technical Support Center