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June 4, 1982

BECO. Ltr. #82-160

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Operating Reactors Branch #2
Division of Licensing
Office of Nuclear Reactor Regulation
U.S. Nuclear Regulatory Commission
Washington, D. C. 20555

License No. DPR-35
Docket No. 50-293

NUREG 0803, Generic SER Regarding Integrity of
BWR Scram System Piping

Dear Sir:

In response to NRC's Generic Letter 81-34 and in accordance with our letter of January 14, 1982 (BECO. Ltr. #82-9), Boston Edison Company's response to the subject NUREG is submitted herewith.

Very truly yours,

A. V. Morisi

Attachments:

- 1 - BECo Response to NUREG 0803
- 2 - BECo As-Built Drawings:
 - 1. M-4894
 - 2. M-4895
 - 3. M-4896
 - 4. M-4897
 - 5. M-4898
 - 6. M-4899

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BOSTON EDISON COMPANY

Response to NUREG 0803,
Generic Safety Evaluation Report
Regarding Integrity of BWR
Scram System Piping

May 25, 1982

The information below is presented in the same order as discussed in Section 5 of NUREG 0803.

I. Piping Integrity

A. Seismic & As-Built Requirements

Requirement:

"The quality assurance of SDV piping should be verified at each plant by providing the results of any as-built inspections and seismic reanalysis of the SDV piping and its supports conducted in accordance with IE Bulletins or otherwise. If such an inspection has not been previously conducted, the responses should provide a schedule for conducting an as-built inspection and seismic reanalysis of the SDV piping and its supports and a program for correcting any deficiencies identified."

Response:

Both the FSAR (Section A.3.1 and 12.2.1.2) and the GE CRD Piping Specification specify that the scram discharge volume (SDV) piping is seismically designed. The SDV piping was designed using the rigid range (or span) method as described in Bechtel Topical Report BP-TOP-1. Using this method in lieu of a detailed dynamic analysis, pipe supports are located such that the first fundamental frequency of each piping span (assuming a simply supported beam) is in the rigid range. Pipe stress and pipe support loads are then obtained by applying static equivalent loads corresponding to the acceleration in the rigid range of the response spectrum curves for the applicable floor elevations. The use of this method for the CRD system design was confirmed by Bechtel as part of the IE Bulletin 79-14 work scope.

Attached are six as-built drawings of the SDV system which were developed as part of the IE Bulletin 80-17 work scope. Support locations and type are indicated on these drawings; however, no detailed as-built support drawings are included.

Stone & Webster is currently under contract to perform the modifications to make the SDV system comply with IE Bulletin 80-17. Part of this work scope is to develop as-built drawings (including supports) and to perform a reanalysis of the system. This will meet the requirements of NUREG 0803 and is scheduled for completion by December, 1983. At that time a final report will be made to the NRC.

B. Maintenance Procedure Review

Requirement:

Provide "...A schedule and program for reviewing and revising, as appropriate, the HCU-SDV maintenance, surveillance, and modification procedures..."

Response:

Boston Edison Co. is reviewing all maintenance, surveillance, and modification procedures for the SDV system against the following criteria:

1. Is this procedure applicable to the concerns of NUREG 0803 (i.e., is there any potential for breaching SDV integrity while rods are withdrawn)?
2. Is there sufficient guidance to the operator to ensure system integrity?
3. Can the procedure be improved to reduce risks to system integrity?

The following procedures will be reviewed:

PNPS 2.1.1 Startup from Cold Shutdown
 2.2.87 Control Rod Drive System
 3.M.1-1.3 Preventive Maintenance (Mechanical)
 3.M.4-1 Control Rod Drive Removal and Installation
 3.M.4-10 Valve Packing
 3.M.4-20 Valve Disassembly and Assembly
 8.E.3 Control Rod Accumulators Operability
 8.E.3.1 Control Rod Drive Flow Inst. Calibration
 8.I.11 Cold Shutdown Valve Testing
 8.7.1.3 Local Leak Rate Test
 3.M.2-8 Control Rod Drive Performance
 3.M.2-16 Scram Pilot Valve Maintenance
 3.M.2-18 CRD Collet Finger Flushing

The review and revision of these procedures (where applicable) will be completed by September 30, 1982.

C. Inservice Inspection Requirements

Requirement:

"...licensees and applicants for BWR plants should propose in their responses a program of periodic inservice inspection for the SDV system meeting the requirements for Class 2 piping in the Section XI ASME Code. This revised inservice inspection program should be implemented on a schedule consistent with the requirements of the licensee's inservice inspection program for ASME Section XI Class 2 piping."

Response:

PNPS 1 has incorporated the SDV system piping into its inservice inspection program in conformance with the requirements for Class 2 piping of Section XI of the ASME Code. Inspections were started during our 1980 outage, and all requirements for the first inspection interval were completed during our recent refueling outage.

II. Mitigation Capability

A. Revision of Emergency Procedures

Requirement:

"Provide a commitment to implement the required revised emergency procedures in their plant-specific responses by the first refueling outage occurring after January 1, 1982." It is recommended that these changes be implemented through the BWR Owners' Group on Emergency Procedures Guidelines.

Response:

Per its charter, the BWR Owners' Group cannot respond directly to NRC requests for utility action, except at the discretion of its members. Neither can BECo commit the Owners' Group to a specific course of action except by its participation in Owners' Group decisions by vote. Thus, BECo can only provide a response to the staff's guidance to the BWR Owners' Group in NUREG 0803 as if it were addressed to BECo directly.

However, the BWR Owners' Group has discussed the guidance of NUREG 0803 regarding modification of the Emergency Procedure Guidelines and acknowledges the benefits of treating the subject generically. The BWR Owners' Group is in the process of completing an extension of the Guidelines to include steps for reactivity control, and certain other modifications to the Guidelines which have been discussed with your staff. It is BECo's judgment that completion of these modifications outweighs, in immediate importance, the NUREG 0803 guidance for other Guideline modifications. After current activities on the Guidelines are substantially complete, BECo will support a preliminary study by the BWR Owners' Group to determine the best approach to fulfilling the intent of the guidance provided in NUREG 0803. It is not clear that the best approach will involve modification of the Guidelines. When that study is complete the Owners' Group will determine whether to authorize specific actions to modify the Emergency Procedure Guidelines. We will then determine what course of action is necessary for PNPS and advise you of our plan.

B. Iodine Concentration Limits

Requirement:

The Standard Technical Specification (STS) limit of 0.2 microcuries per ml of water iodine concentration should be implemented for all operating BWR's unless 1) "it is demonstrated that the probability of requiring operator access to the reactor building is consistent with the staff's quantitative risk assessment (pipe break plus failure to reset scram)" and 2) based on analysis of operating history and current and projected fuel performance, the probability of operating at coolant activity levels in excess of those allowed by STS is less than 10^{-5} per reactor year.

Response:

Boston Edison Company does not plan to implement the STS limit for coolant activity at Pilgrim as recommended by NUREG 0803. This decision is not based on meeting the conditions (1 and 2) specified above but rather on an evaluation of the NRC's basis for the required change. Specifically, the NRC calculations show that activity levels above the STS level could cause violation of 10 CFR 100 limits and could preclude reactor building access after an SDV rupture. This is not the case for PNPS 1.

A plant specific analysis conducted for BECo by Entech Engineering, Inc., shows that 1) the current technical specification activity limit (20.0 microcuries of total iodine per ml of water, or 100 times STS) does not result in violation of 10 CFR 100 limits after a rupture of the SDV system, and 2) a concentration of 2.0 microcuries per ml of water (10 times STS) is low enough to allow reactor building access for the worst case SDV rupture. Therefore, based on this analysis, a technical specification limit reduction to 2.0 microcuries is being proposed. This level will provide the necessary margin of safety for reactor building access while placing no undue restrictions on reactor power operations. This proposed change will be submitted in July, 1982.

It should be noted that the Entech analysis assumes a plant configuration that will exist after modifications required by IE Bulletin 80-17 are completed (i.e., two separate isolation scram discharge instrument volumes. These modifications will be completed by December, 1983. Continued operation with the present configuration is based on the following logic which is similar to the NRC reasoning in NUREG 0803 Section 5:

1. Violation of 10 CFR 100 will not occur even with the present configuration.
2. Reactor building access will only be hampered under the worst case SDV rupture.
3. Probability of SDV leak actually occurring during the time period prior to the modifications is low.
4. No SDV piping leaks or breaks have been reported in any operating BWR.

III. Environmental Qualification

A. Detection Equipment

Requirement:

"Identify the equipment that would be used to detect a break and/or leak in the SDV system and include the qualification of this equipment in the NRC's ongoing EQ program to show that it would perform the identification function."

Response:

Table 1 provides the qualification information for equipment available for detection of a leak or break in the SDV system. Not all this equipment is qualified to the expected environment; however, it is BECo's contention that sufficient equipment is qualified to these parameters, as shown on Table 1, to perform the intended function and provide reliable indication. This detection equipment includes 1) ECCS and RCIC rooms temperature indications and alarms (TS 2370 & 2372 C&D, TS2371 & 2373 A & B, TS 1360-14 & 1360-16 C & D, and TS 1360 15 & 1360-17A & B) and 2) reactor building exhaust ventilation radiation alarms (Process Radiation Monitors 032A & B). In addition, there are numerous temperature alarms (TE 8125-56, 58, 62, 65, 66, 70, 72, 73, 74, 78, 79, 80 and 83) which, while not qualified in the strict sense, are expected to alarm when their set-point is reached. Since BECo's evaluation of the consequences of this accident adopts the position that recognition and proper corrective action do not occur for 4 hours, it is felt that these indications working together are sufficient to warn the operators of a problem and allow for investigation of the conditions in the reactor building.

BECo also contends that it is highly unlikely that the environment created by the rupture will cause failure of all the unqualified equipment and that operators can expect supplementary alarms from the drain sump level alarms, CRD high temperature alarms and area radiation alarms. This coupled with expected routine inspections of the area and the fact that a rupture of this size will be audible from anywhere in the reactor building ensures detection of this condition within four hours of the scram.

B. Mitigation Equipment

Requirement:

Identify the equipment needed to mitigate an unisolable break in the SDV system and include the qualification of this equipment in the NRC's ongoing EQ program to show that it would perform the mitigation function, paying particular attention to the following guidelines:

1. Qualification of ADS
2. Qualification for water impingement and wetdown by 212°F water.
3. Verification of feedwater and condensate system operation independent of the reactor building environment.
4. Availability of HPCI and RCIC turbines due to high ambient temperature trips.

Response:

BECO has evaluated this accident and concludes that the following systems and support systems should be available to ensure adequate mitigation:

1. Automatic Depressurization System (ADS)
2. Feedwater & Condensate System
3. Core Spray System
4. Residual Heat-Removal System (for LPCI)
5. Reactor Building Closed Cooling Water (RBCCW) System and Salt Water Systems
6. Standby Gas Treatment System

This system list is based on the Pilgrim 1 FSAR and NEDO-24342, "GE Evaluation in Response to NRC Request Regarding BWR Scram System Pipe Breaks", April, 1981, and is consistent with the NRC probability analysis of NUREG 0803. Only equipment required during the first six hours is considered, based on four hours for break detection and two hours for SDV isolation. After that time, the environment is not expected to impact equipment operation.

The bases for the systems selected are as follows:

1. ADS is required for plant depressurization, which will reduce the leak rate and allow reactor building access for isolation.
2. The feedwater and condensate system is provided as a backup for plant cooldown and depressurization using the main condenser (assuming MSIV's remain open).
3. Core Spray and the LPCI mode of RHR are required for redundant low pressure core cooling.
4. RBCCW is needed to supply cooling water to the RHR heat exchangers as the ultimate heat sink if the main condenser is not available.
5. Standby Gas Treatment is required to provide cleanup of the reactor building environment created by the rupture.

High pressure cooling (HPCI & RCIC) is not considered necessary because 1) the plant must be depressurized to preclude undesirable consequences, and 2) HPCI and RCIC are expected to isolate on high temperature within one hour of the rupture.

Table 2 provides the present qualification of equipment required for operation of the mitigation systems. Only components located in the reactor building are listed, since equipment outside the reactor building will not be affected. Water impingement and wetdown are considered only for equipment located in the CRD modules area where the SRV's are located. Results of FSAR Amendment 34 flooding calculations based on Pilgrim I conditions show that flooding will not affect any significant equipment.

Additionally, major load centers and distribution equipment were evaluated within the post-accident environment. This evaluation shows this equipment should be available for operation in an environment in excess of 212°F and at 100% humidity and to be protected from failure by direct impingement.

C. Plant Specific Qualification

Requirement:

"For any equipment required for identification and/or mitigation that is not qualified for service at 212°F and 100% humidity, provide a schedule for defining the plant-specific SDV break environment and a commitment to qualify the equipment in accordance with the NRC's ongoing EQ program."

Response:

BECO has contracted for Bechtel Power Corporation to model the reactor building and generate pressure and temperature profiles during a SDV rupture. Preliminary results from this analysis show the maximum temperatures to be significantly less than the NRC requirement of 212°F. Additionally, we are participating in work by the BWR Owners' Group to evaluate further the SDV rupture scenario and potentially reduce the need for environment qualifications to meet this transient. Since the above work will not be completed before late September 1982, BECO does not feel any decision on a commitment to environmental qualification under NUREG 0803 can be made before October 15, 1982. At that time we will provide an update of our intentions.

| EQUIPMENT NO | DESCRIPTION | LOCATION | QUALIFICATION Temp / Humidity 2120 F 100% RH | | QUAL OK | COMMENTS |
|--------------------------|-----------------------------|-----------------------|--|-------|---------|--|
| LS 8016 | RHR Pump Room A Water Level | RHR&CS Pump Room A | NQ(1) | NQ(1) | NO | No flooding of this area is expected |
| LS 8017 | RHR Pump Room B Water Level | RHR&CS Pump Room B | NQ(1) | NQ(1) | NO | No flooding of this area is expected |
| TE1001-92A | RHR Steam Leak Detection | RHR&CS Pump Room A | NQ(1) | NQ(1) | NO | No flooding of this area is expected |
| TE1001-92B | RHR Steam Leak Detection | RHR&CS Pump Room A | NQ(1) | NQ(1) | NO | No flooding of this area is expected |
| TE1001-92F | RHR STEAM LEAK Detection | RHR&CS Pump Room B | NQ(1) | NQ(1) | NO | No flooding of this area is expected |
| TE1001-92G | RHR Steam Leak Detection | RHR&CS Pump Room A | NQ(1) | NQ(1) | NO | No flooding of this area is expected |
| TE1001-92H | RHR Steam Leak Detection | RHR&CS Pump Room B | NQ(1) | NQ(1) | NO | No flooding of this area is expected |
| LS 8018 | HPCI Pump Room Level Switch | HPCI Pump Room | NQ(1) | NQ(1) | NO | |
| TS 2370&2372 C&D | Hi Space Temp Switch | CRD Modules Area West | 305 | 100% | YES | Note: Switch monitors temp. In duct from HPCI valve room. |
| TS 2371 & 2373 A & B | Hi Space Temp Switch | RHR&CS Pump Room B | 305 | 100% | YES | Note: Switch monitors temperature in duct from HPCI Pump room. |
| LS 8019 | RCIC Pump Room Level Switch | RCIC Pump Room | NQ(1) | NQ(1) | NO | |
| TS 1360-14C&D 1360-16C&D | RCIC Steam Leak Detection | RCIC Piping Room | 305 | 100% | YES | |
| TS 1360-15A&B 1360-17A&B | RCIC Steam Leak Detection | RCIC Pump Room | 305 | 100% | YES | |
| TE 8125-56 | HPCI Room Temp | HPCI Room (1') | NQ(1) | NQ(1) | NO | Reads & Alarms in control room BECO contends environment will not contribute to failure prior to alarm. |

NOTE: (1) Qualification is not yet proven

| Equipment No. | Description | Location | Qualification Temp / Humidity 2120 F 100% RH | Qual Ok. | Comments |
|------------------------------|--|------------------------|--|-------------|--|
| TE 8125 - 58 | RHR Room A Temperature | RHR Room A (12') | NQ (1) | NQ(1) No | Reads & Alarms in Control Room BECo contends environment will not contribute to failure prior to alarm |
| TE 8125 - 62 | RCIC Room Temp. | RCIC Room (2') | NQ (1) | NQ(1) No | Reads & Alarms in Control Room BECo contends environment will not contribute to failure prior to alarm |
| TE 8125 - 65 | CRD Pump Room Temp. | CRD Pump Room (7') | NQ (1) | NQ(1) No | Reads & Alarms in Control Room BECo contends environment will not contribute to failure prior to alarm |
| TE 8125 - 66 | RHR Room B Temp. | RHR Room B (7') | NQ (1) | NQ(1) No | Reads & Alarms in Control Room BECo contends environment will not contribute to failure prior to alarm |
| TE 8125 - 70 | RCIC PIPING Area Temp | RCIC Piping Room (23') | NQ (1) | NQ(1) No | Reads & Alarms in Control Room BECo contends environment will not contribute to failure prior to alarm |
| TE 8125 - 72 | RHR Piping Area Temp | RHR Piping Area 23'el | NQ (1) | NQ(1) No | Reads & Alarms in Control Room BECo contends environment will not contribute to failure prior to alarm |
| TE 8125 - 74 | CRD Area Temp. | CRD Area West (23) | NQ (1) | NQ(1) No | Reads & Alarms in Control Room BECo contends environment will not contribute to failure prior to alarm |
| TE 8125 - 73 | CRD Area Temp. | CRD Area East (23') | NQ (1) | NQ(1) No | Reads & Alarms in Control room BECo contends environment will not contribute to failure prior to alarm |
| TE 8125 - 78 | 51' Level Temp Ind | Drywell Wall North | NQ (1) | NQ(1) No | Reads & Alarms in Control Room BECo contends environment will not contribute to failure prior to alarm |
| TE 8125 - 79 | 74' Level Temp Ind | Drywell Wall North | NQ (1) | NQ(1) No | Reads & Alarms in Control Room BECo contends environment will not contribute to failure prior to alarm |
| TE 8125 - 80 | Fuel Pool Area Temp | Fuel Pool Area 74' el | NQ(1) | NQ(1) No | Reads & Alarms in Control Room BECo contends environment will not contribute to failure prior to alarm |
| TE 8125 - 83 | 91' Level Ind | West Wall 91' Level | NQ (1) | NQ(1) No | Reads & Alarms in Control Room BECo contends environment will not contribute to failure prior to alarm |
| Process RAD Monitors 032 A&B | Exhaust Ventilation Radiation Monitors | See Comments | Not Required | Yes | These monitors are located external to the Reactor Building |
| 41 ARM Ch #8 | AREA RADIATION MONITOR | Rx Bldg 23' Level | NQ (1) | NQ(1) No | |

Table 1 (Cont.)

[illegible]

TABLE 2 REQUIRED FOR MITIGATION

| EQUIPMENT NO. | DESCRIPTION | LOCATION | QUALIFICATION | | QUAL. | COMMENTS |
|--------------------------|-------------------------------------|-------------------------------|------------------|---------------------|-------|---|
| | | | Temp / 212° F | Humidity 100% RH | | |
| <u>ADS SYSTEM</u> | | | | | | |
| SV 203-3A | ADS Actuation Valve | DRYWELL | 347 F | 100% | YES | Will not be affected by Rupture Environment |
| SV 203-3B | ADS Actuation Valve | DRYWELL | 347 F | 100% | YES | Will not be affected by Rupture Environment |
| SV 203-3C | ADS Actuation Valve | DRYWELL | 347 F | 100% | YES | Will not be affected by Rupture Environment |
| SV 203-3D | ADS Actuation Valve | DRYWELL | 347 | 100% | YES | Will not be affected by Rupture Environment |
| <u>CORE SPRAY SYSTEM</u> | | | | | | |
| DPIS 1459A&B | Rx Vessel CS Line Rupture Detection | CRD PUMP ROOM MEZZANINE | 212 F | 100% | YES | |
| MO1400-3A | CS Pump A suction Valve | RHR & CS Pump Room A | 250 F | 100% | YES | |
| MO1400-3B | CS Pump B Suction Valve | RHR & CS Pump Room B | 250 F | 100% | YES | |
| MO1400-4A | CS Pump A Test Line Block Valve | RHR & CS Pump Room A | 250 F | 100% | YES | |
| MO1400-4B | CS Pump B Test Line Block Valve | RHR & CS Pump Room B | 250 F | 100% | YES | |
| MO1400-24A MO1400-25A | Injection Block Valves Loop A | RWCU Hx. Ex. & Pump Room | 212 F | 100% | YES | |
| MO1400-24B MO1400-25A | Injection Block Valves Loop B | Open Area 51' Level West Half | 212 F | 100% | YES | |
| P 215 A | Core Spray Pump A. | RHR & CS Pump Room A | 212 F | 100% | YES | |

| EQUIPMENT NO. | DESCRIPTION | LOCATION | QUALIFICATION | | QUAL OK | COMMENTS |
|---------------|--------------------------------------|---------------------------------|---------------|----------|---------|----------|
| | | | Temp | Humidity | | |
| P 215 B | Core Spray Pump B | RHR & CS Pump Room B | 212 F | 100% | YES | |
| PS253-52A | CS & RHR Valve Open Permissive | Open Area 51' Level East Half | 212 F | 100% | YES | |
| | | | | | | |
| PS 1451 A | ADS Permissive | RHR & CS Pump Room A | 212 F | 100% | YES | |
| PS 1451B | ADS Permissive | RHR & CS Pump Room B | 212 F | 100% | YES | |
| PS 1464A | ADS Permissive | RHR & CS Pump Room A | 212 F | 100% | YES | |
| PS 1464B | Ads Permissive | RHR & CS Pump Room B | 212 F | 100% | YES | |
| SV1400-51A&B | Testable Check Valve Bypass Vav. | Drywell | 346 F | 100% | YES | |
| RHR SYSTEM | | | | | | |
| DPIS1001-79A | Low Flow Trip Signal to MO1001 - 18A | RHR & CS Pump Room A | 212 F | 100% | YES | |
| SPIS1001-79B | Low Flow Trip Signal to MO1001 - 18A | RHR & CS Pump Room B | 212 F | 100% | YES | |
| LIS263-72 A&C | RHR Pump Start (LPCI) | OPEN AREA, 51' Level, East Half | 250 F | 98% | NO | |
| LIS263-72 B&D | RHR Pump Start (LPCI) | OPEN AREA, 51' Level, West Half | 250 F | 98% | NO | |
| LITS263-73A | Containment Spray Perm (Monitoring) | CRD Modules Area East | 250 F | 100% | YES | |

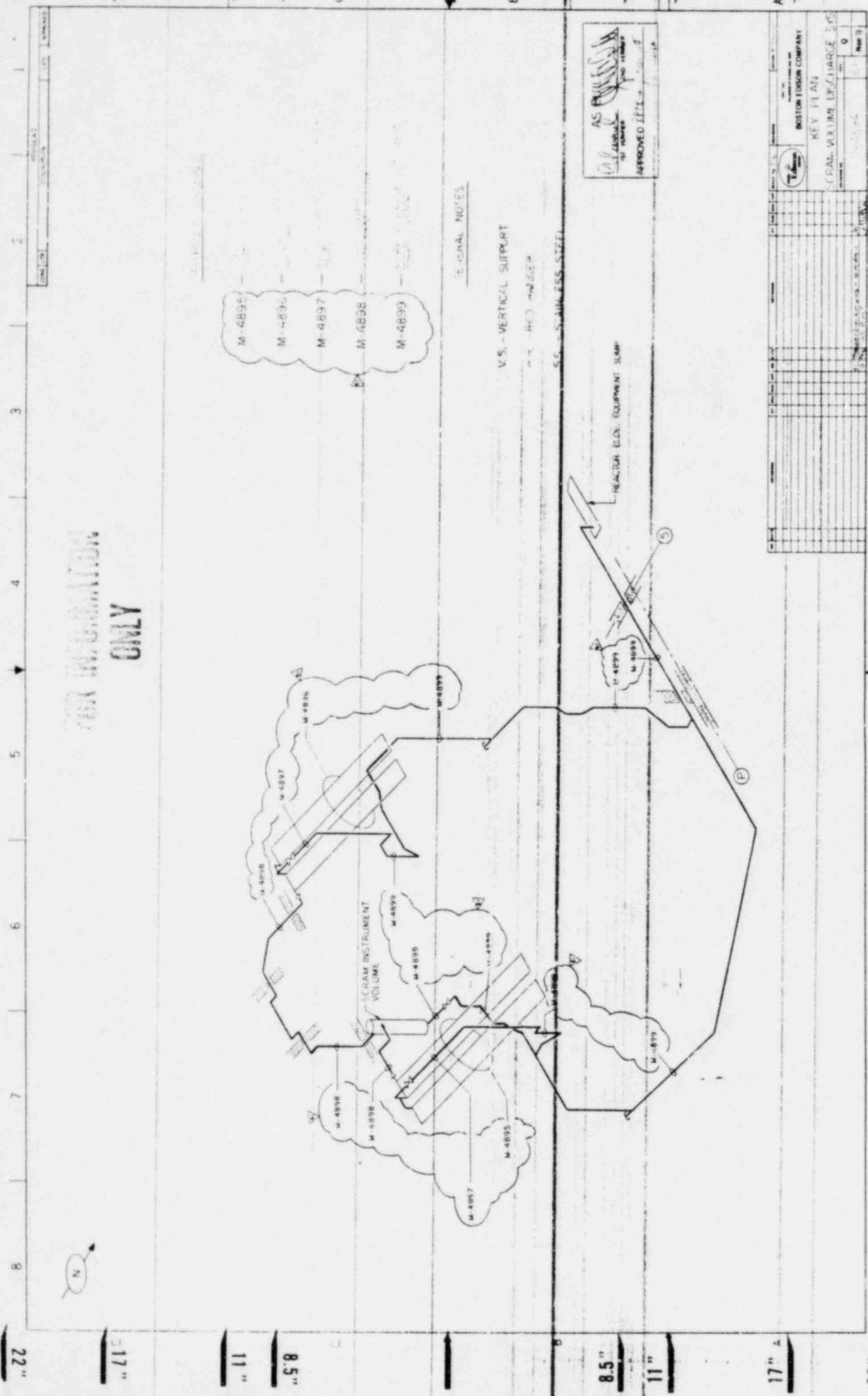
Table 2 (Cont.)

| EQUIPMENT NO. | DESCRIPTION | LOCATION | QUALIFICATION | | QUAL. OK | COMMENTS |
|------------------|---------------------------------------|-----------------------|---------------|----------|----------|---|
| | | | Temp | Humidity | | |
| | | | 212 F | 100% RH | | |
| LITS263-73B | Containment Spray Perm (Monitoring) | CRD Modules Area West | 250 F | 100% | YES | |
| M01001-7A&C | RHR Pump A&C Suct. Block Valve | RHR & CS Pump Room A | 250 F | 100% | YES | |
| M01001-7B&D | RHR Pump B&D Suct. Block Valve | RHR & CS Pump Room B | 250 F | 100% | YES | |
| M01001-16A | A RHR Ht. Ex. Bypass Block Valve | RHR & CS PUMP Room A | 250 | 100% | YES | |
| M01001-16B | B RHR Ht. Ex. Bypass Block Valve | RHR & CS Pump Room B | 250 F | 100% | YES | |
| M01001-18A | RHR Pumps A&C Min. Recirc Block Valve | RHR & CS Pump Room A | 250 F | 100% | YES | |
| M01001-18B | RHR Pumps B&D Min Recirc Block Valve | RHR & CS Pump Room B | 250 F | 100% | YES | |
| M01001-21 | RHR to CHEM WASTE Block Valve | CRD Pump Room Mezz. | 250 F | 100% | YES | Valve is normaly shut & will fail as is |
| M01001-23A & 26A | Containment Spray Block Valve | RWCU Ht.Ex Pump Room | 212 F | 100% | YES | |
| M01001-23B & 26B | Containment Spray Block Valve | RCIC Piping Room | 212 F | 100% | YES | |
| M01001-28A | LPCI Flow Control Valve | RHR Piping Room | 250 F | 100% | YES | |
| M01001-28B | LPCI Flow Control Valve | RHR/HPCI Piping Room | 250 F | 100% | YES | |
| M01001-29A | LPCI Loop A Block Valve | RHR Piping Room | 250 F | 100% | YES | |
| M01001-29B | LPCI Loop B Block Valve | RHR/HPCI Piping Room | 250 F | 100% | YES | |

| EQUIPMENT NO. | DESCRIPTION | LOCATION | QUALIFICATION | | QUAL OK | COMMENTS |
|---------------|--|-------------------------------|---------------|----------|---------|----------|
| | | | Temp | Humidity | | |
| | | | 212°F | 100% RH | | |
| M01001-32 | Block Valve to Chemical Waste | CRD PUMP Room Mezz. | 250 F | 100% | Yes | |
| M01001-34A | Loop A Torus Cooling & Spray Block Valve | RHR & CS pump Room A | 250 F | 100% | Yes | |
| M01001-34B | Loop B Torus Cooling & Spray Block Valve | RHR & CS Pump Room B | 250 F | 100% | Yes | |
| M01001-36A | Loop A Torus Cooling Block Vlv | RHR & CS Pump Room A | 250 F | 100% | Yes | |
| M01001-36B | Loop B Torus Spray Block Valve | RHR & CS Pump Room B | 250 F | 100% | Yes | |
| M01001-37A | Loop A Torus Spray Throttle Valve | RHR & CS Pump Room A | 250 F | 100% | Yes | |
| M01001-37B | Loop B Torus Spray Throttle Valve | RHR & CS Pump Room B | 250 F | 100% | Yes | |
| M01001-43A&C | RHR & Shutdown Cooling Block valves for Pumps A & C | RHR & CS Pump Room A | 250 F | 100% | Yes | |
| M01001-43B&D | RHR & Shutdown Cooling Block Valves for Pumps B & D | RHR&CS Pump Room B | 250 F | 100% | Yes | |
| M01001-47 | Common RHR & Shutdown cooling downstream block Valve | RHR Piping Room | 250 F | 100% | Yes | |
| M01001-50 | Common RHR & Shutdown cooling downstream block valve | Drywell | 329 F | 100% | Yes | |
| M01001-60 | Rx Vessel Head Spray Upstream Block Valve | Fuel pool Ht. Ex Area 51' Lv. | 250 F | 100% | Yes | |
| M01001-63 | Rx Vessel Head Spray downstream Block Valve | Drywell | 329 F | 100% | Yes | |
| P 203 A&C | RHR PUMPS A & C | RHR & Cs Pump Room A | 212 F | 100% | Yes | |

| EQUIPMENT NO. | DESCRIPTION | LOCATION | QUALIFICATION | | QUAL. OK | COMMENTS |
|-------------------------------|--|--------------------------|---------------|----------|----------|----------|
| | | | Temp | Humidity | | |
| P203 B&D | RHR Pumps B&D | RHR & CS PUMP Room B | 212 F | 100% | YES | |
| PS261-23 A&B | Close Shutdown System & Headspray Isolation Valves | CRD Pump Room Mezzanine | 200 F | 100% | NO | |
| PS263-52 A | CS & RHR Valve Open Permissive | 51' Level Open Area East | NO DATA | | NO | |
| PS263-52 B | CS & RHR Valve Open Permissive | 51' Level Open Area West | NO DATA | | NO | |
| PS263-52 A | CS & RHR Pump Permissive | 51' Level Open Area East | No Data | | NO | |
| PS263-52 B | CS & RHR Pump Permissive | 51' Level Open Area West | No Data | | NO | |
| PS1001-89A&C | ADS Permissive | 74' 3" Level North | 212 F | 100% | YES | |
| PS1001-89B&D | ADS Permissive | 51' Level Open Area West | 212 F | 100% | YES | |
| PS1001-90A&C | CS & RHR Initiation (Drywell Pressure) | 74' 3" Level North | 212 F | 100% | YES | |
| PS1001-90B&C | CS & RHR Initiation (Drywell Pressure) | 51' Level Open Area West | 212 F | 100% | YES | |
| PS1001-93A&C PS1001-104A&C | ADS Auto Actuation Permissive | RHR & CS Pump Room A | 212 F | 100% | YES | |
| PS1001-93B&D PS1001-104B&D | ADS Auto Actuation Permissive | RHR & CS Pump Room B | 212 F | 100% | YES | |
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| EQUIPMENT NO. | DESCRIPTION | LOCATION | QUALIFICATION | | QUAL OK | COMMENTS |
|-------------------------------------|--|--------------------------|---------------|----------|---------|--|
| | | | Temp / | Humidity | | |
| | | | 212° F | 100% RH | | |
| <u>RBCCW</u> | | | | | | |
| MO 4060 A&B | A RHR Ht. Ex. Isolation Valves | RHR & CS Pump Room A | 250 F | 100% | YES | |
| MO 4010 A&B | B RHR Ht. Ex Isolation Valves | RHR & CS Pump Room B | 250 F | 100% | YES | |
| MO-4065 | Fuel Pool Ht. Ex Isolation Vlv. | 74' 3" Level | NQ (1) | NQ (1) | NO | Need to insure isolation to provide flow to RHR Ht Ex. |
| <u>STANDBY GAS TREATMENT SYSTEM</u> | | | | | | |
| SVL 55 & 56 | CRD Maintenance Room Vent Isolation | 51' Level Open Area West | 346 F | 100% | YES | |
| SVL 57 | Reactor Building Containment Exhaust To SGTS | RCIC Piping Room | 346 F | 100% | YES | |
| SVL 58 | SGTS Filter A Inlet | RCIC Piping Room | 346 F | 100% | YES | |
| SVL 60 | REFUELING Area to SGTS ISOLATION | RCIC Piping Room | 346 F | 100% | YES | |
| SVL 62 | SGTS Filter B Inlet | RCIC Piping Room | 346 F | 100% | YES | |
| SVL 79 | Reactor Building Cl. Up Exhaust to SGTS | RCIC Piping Room | 346 F | 100% | YES | |
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ONLY

GENERAL NOTES

V.S. - VERTICAL SUPPORT

SCRAM INSTRUMENT VOLUME

REACTOR ELEC. EQUIPMENT SHED

AS
APPROVED 11/1/54

| | |
|------------------------|-----|
| BOSTON ENGINE COMPANY | |
| KEY PLAN | |
| CEAS. VOLUME 18/1/1954 | |
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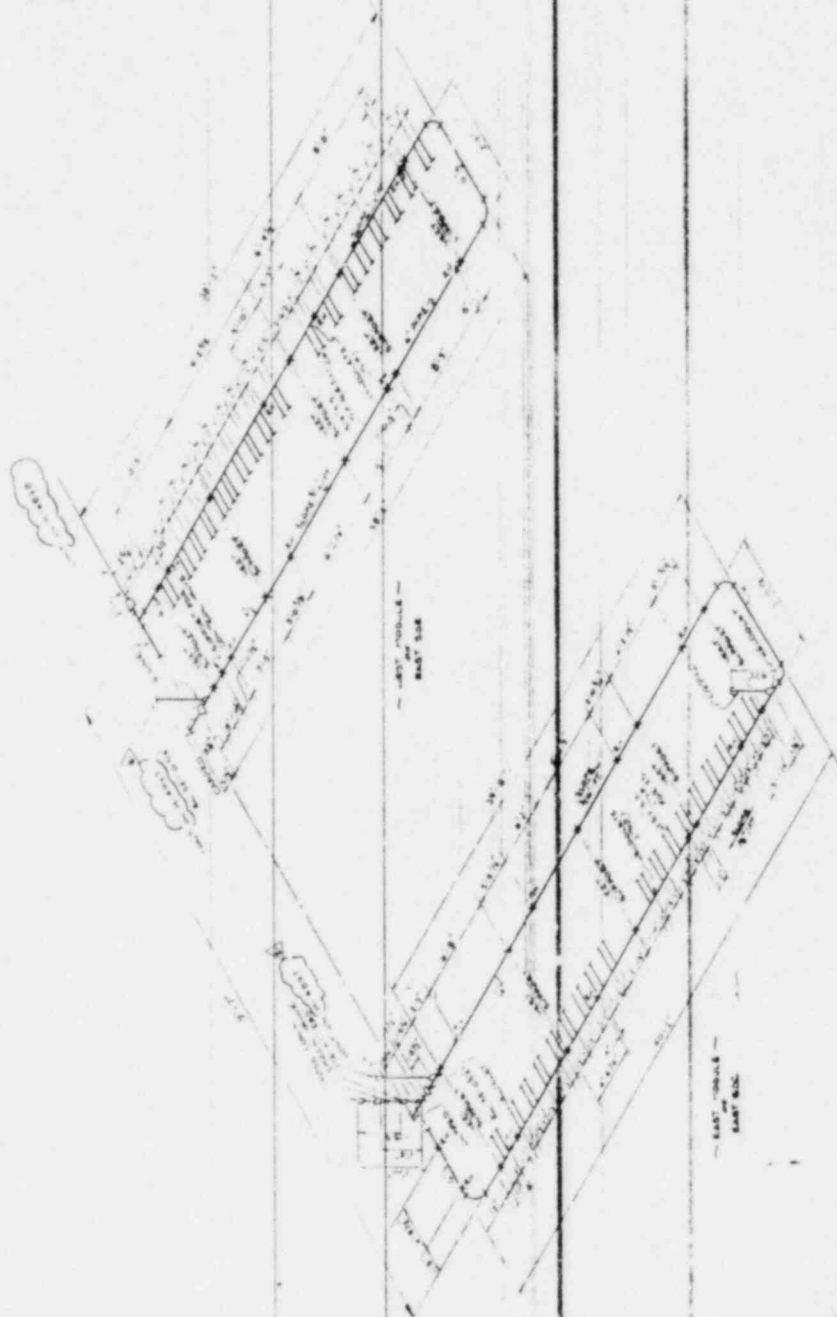
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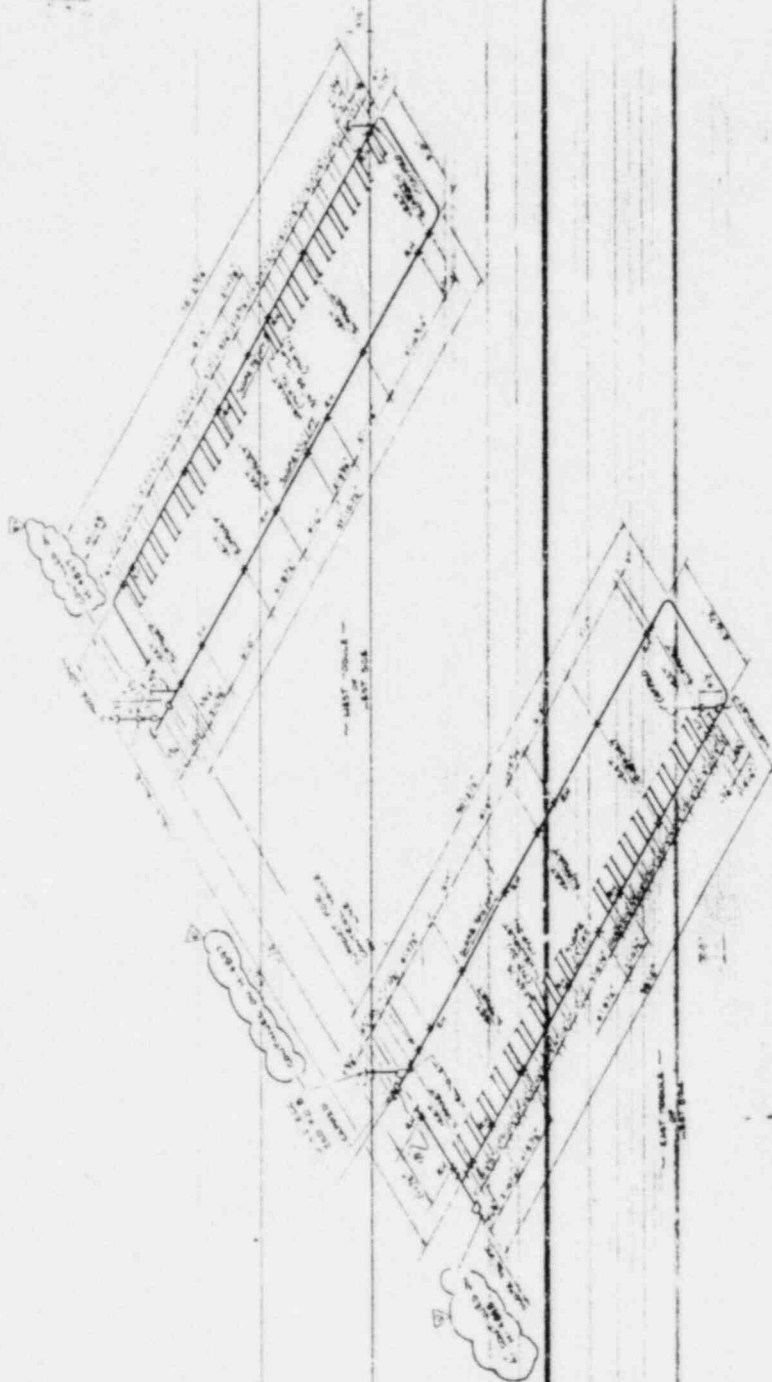
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AS BUILT
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DATE: 10/10/10

| NOTION LOGS COMPANY | | DATE | TIME | LOCATION | DEPTH | REMARKS |
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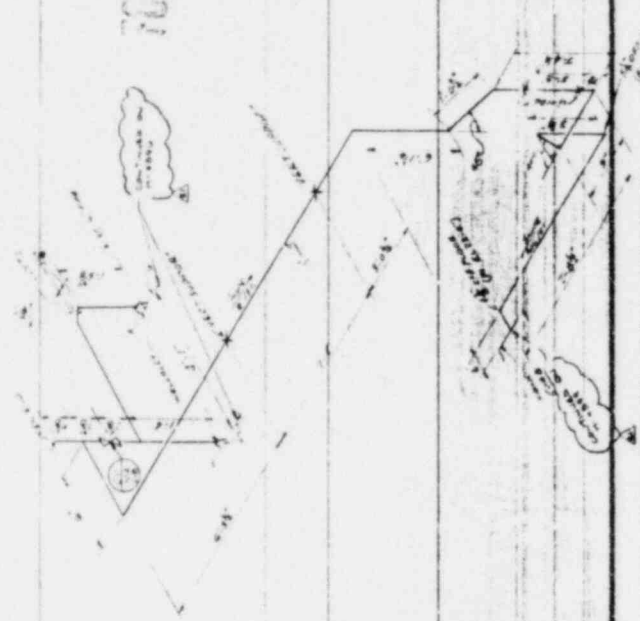


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FOR INFORMATION ONLY



EAST SIDE

WEST SIDE

APPROVED
 [Signature]
 [Stamp]

17"

22"

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|------------------|---------|--|---|
| | | BOSTON LUMBER COMPANY 1000 LUMBER STREET BOSTON, MASS. 02110 | |
| DATE | 10/1/77 | BY | 0 |
| PROJECT NO. 1000 | | SHEET NO. 0 | |

