

Nebraska Public Power District

Cooper Nuclear Station  
**PLANT UNIQUE ANALYSIS REPORT**  
Mark I Containment Program

Revision 0

April, 1982

## INTRODUCTION

- CNS MARK I CONTAINMENT REEVALUATION COMPLETE
- REEVALUATION BASED ON LOADS NOT CONSIDERED IN ORIGINAL DESIGN
- PUAR
  - DESCRIBES EVALUATIONS PERFORMED
  - LOAD DEFINITIONS
  - MODIFICATIONS INSTALLED
  - ACCEPTANCE CRITERIA
  - EVALUATION RESULTS
- PRESENTATION ATTENDEES
  - MR. L. KUNCL, (NPPD) DIVISION MANAGER,  
NUCLEAR ENGINEERING
  - MR. J. PILANT, (NPPD) DIVISION MANAGER,  
LICENSING AND QA
  - MR. R. D. BOYLE, (NPPD) MANAGER NUCLEAR ENGINEERING
  - MR. D. W. OGDEN, (KE) PROJECT MANAGER,  
CNS MARK I PROGRAM
  - MR. R. J. STUART, (EDS) VICE PRESIDENT
  - MR. M. N. SHULMAN, (EDS) DIVISION MANAGER,  
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  - MR. R. BROMAN, (EDS) DIVISION MANAGER,  
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ADVANCED ANALYSIS

# PRESENTATION CONTENTS

**SUMMARY  
OF CONTAINMENT  
MODIFICATIONS**

**SUMMARY  
OF LOAD DEFINITION  
AND TREATMENT**

**SUMMARY  
OF STRUCTURAL  
EVALUATIONS**

## OVERVIEW OF PROGRAM HISTORY

- ORIGINAL DESIGN CONSIDERED ONLY DESIGN TEMPERATURE AND PRESSURE FOR LOCA
- IDENTIFICATION OF ADDITIONAL LOADS
  - MARK III CONTAINMENT LARGE SCALE TESTING
  - MARK I OPERATING EXPERIENCE
- NRC REQUEST IN 1975
  - FEBRUARY, S/RV DISCHARGE
  - APRIL, NEW LOCA LOADS
- FORMATION OF OWNER'S GROUP
  - SHORT TERM PROGRAM
  - LONG TERM PROGRAM



## SHORT TERM PROGRAM

- OBJECTIVE

- VERIFY INTEGRITY AND FUNCTIONAL CAPABILITY
- JUSTIFY CONTINUED OPERATION

- RESULTS

- REPORT OUTLINING TASKS IN 1975
- EVALUATIONS COMPLETED IN 1976

REQUIRED ACTIONS TAKEN

REQUIREMENT FOR PUA ESTABLISHED

FUNCTIONAL PERFORMANCE OF  
CONTAINMENT DEMONSTRATED

FACTOR OF SAFETY OF 2 AGAINST  
FAILURE

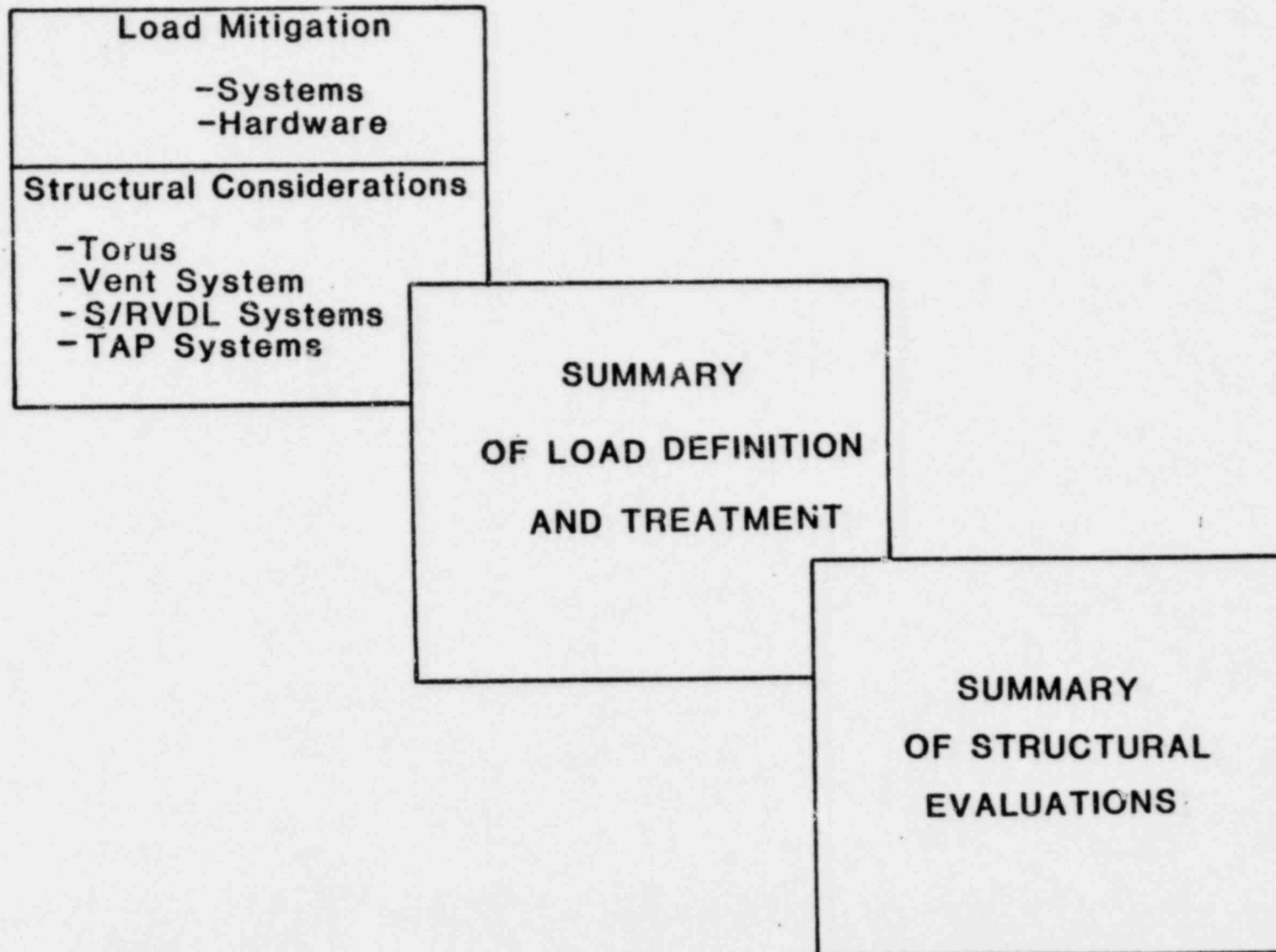
## LONG TERM PROGRAM

- INITIATED IN JUNE 1976
- OBJECTIVES
  - DESIGN BASIS LOADS
  - RESTORE ORIGINAL SAFETY MARGINS
- REQUIREMENTS
  - EXTENSIVE TESTING AND ANALYSIS PROGRAM
  - ESTABLISH CRITERIA
  - EVALUATE LOAD MITIGATION DEVICES AND SYSTEM MODIFICATIONS
  - PLANT UNIQUE ANALYSIS AND MODIFICATIONS
- STATUS
  - PUAR COMPLETED
  - MODIFICATION TO BE COMPLETED BY SEPTEMBER 1982

DESIGN CRITERIA

	Original Requirements	New Requirements	Exceptions
Structural	ASME B&PV Code, Section III June 1967	Mark I Structural Acceptance Criteria PUAAG - As modified by NRC Acceptance Criteria	Dynamic Response Combination
Piping	USAS B31.1 1967	Mark I Structural Acceptance Criteria PUAAG - As modified by NRC Acceptance Criteria	Dynamic Response Combination
Systems	FSAR	Mark I Structural Acceptance Criteria PUAAG - As modified by NRC Acceptance Criteria	None
Loads	Design Pressure and Temperature	G.E. Load Definition Report (Nov. 1981) as modified by NRC Acceptance Criteria	DBA CO Random Phasing MVA S/RV Pressure Combination 30% R.H. in S/RVDL

# PRESENTATION CONTENTS - SUMMARY OF MODIFICATIONS



## SUMMARY OF CONTAINMENT MODIFICATIONS

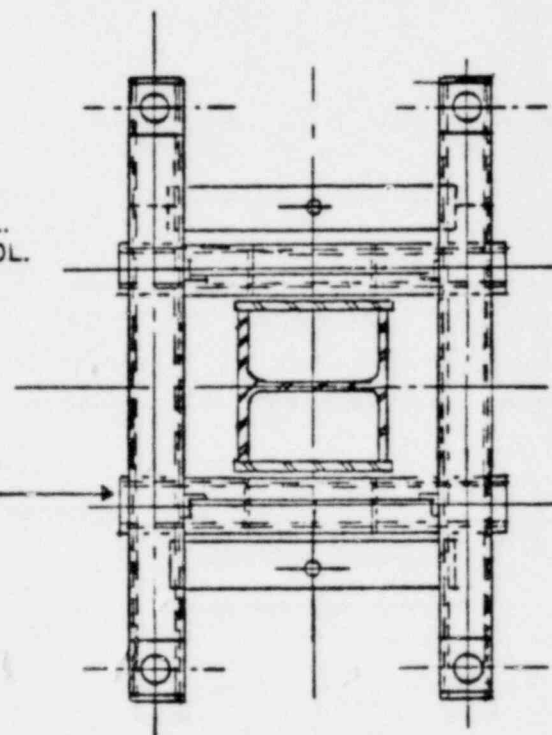
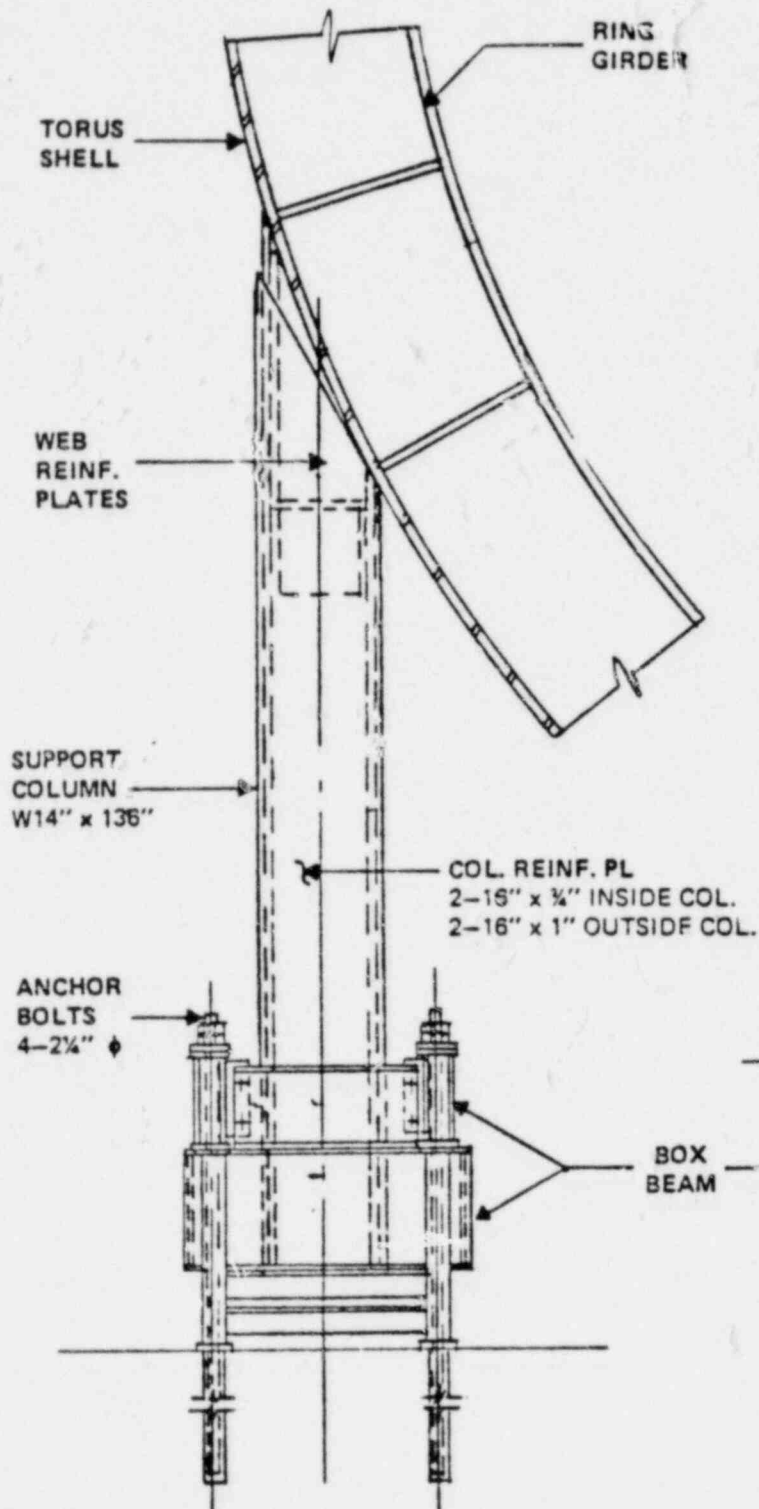
### ● LOAD MITIGATION

- PUMP AROUND SYSTEM - MAINTAIN  $\Delta P$
- S/RV LOW-LOW SET LOGIC
- MSIV WATER LEVEL TRIP
- TORUS TEMPERATURE MONITORING SYSTEM
- TRUNCATION OF DOWNCOMER
- VENT HEADER DEFLECTOR
- T-QUENCHER INSTALLATION

### ● STRUCTURAL REINFORCEMENT

- TORUS SUPPORTS STRENGTHENED
- ADDITION OF SADDLES
- TORUS RING GIRDER STIFFENERS
- DOWNCOMERS REINFORCED
- VENT SYSTEM SUPPORT ALTERED
- VACUUM BREAKERS REINFORCED
- PLATFORM AND MONORAIL SUPPORTS REINFORCED
- S/RVDL PIPING REROUTED
- S/RVDL PIPE SUPPORTS MODIFIED, ADDED
- TAP SUPPORTS MODIFIED, ADDED
- INTERNAL AND SMALL BORE PIPE REROUTED
- PUMP AND VALVE CONFIGURATIONS STRENGTHENED

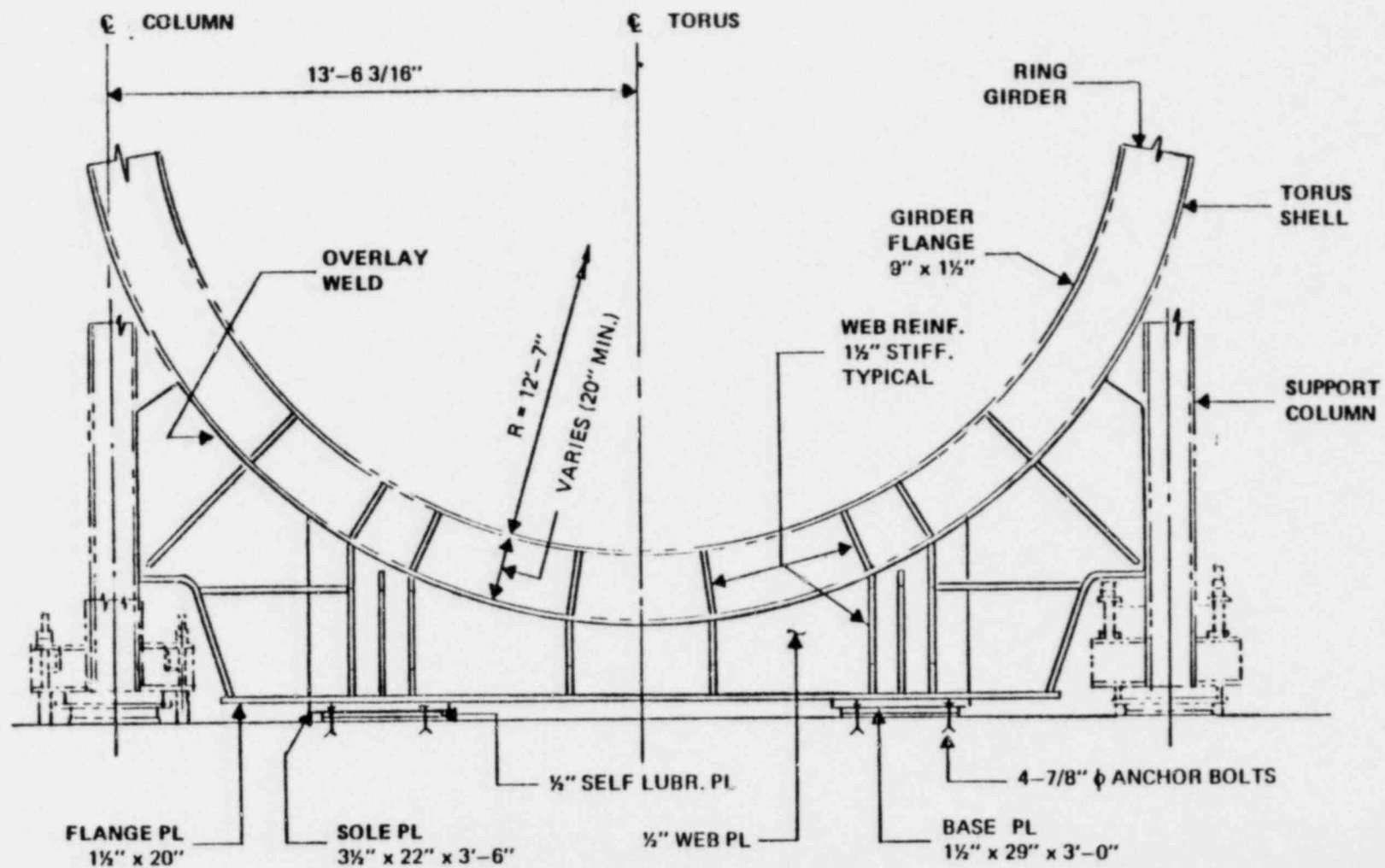
OBJECTIVE: INCREASED COLUMN CAPACITY



PLAN  
TYPICAL COL. ANCHOR ASSEMBLY

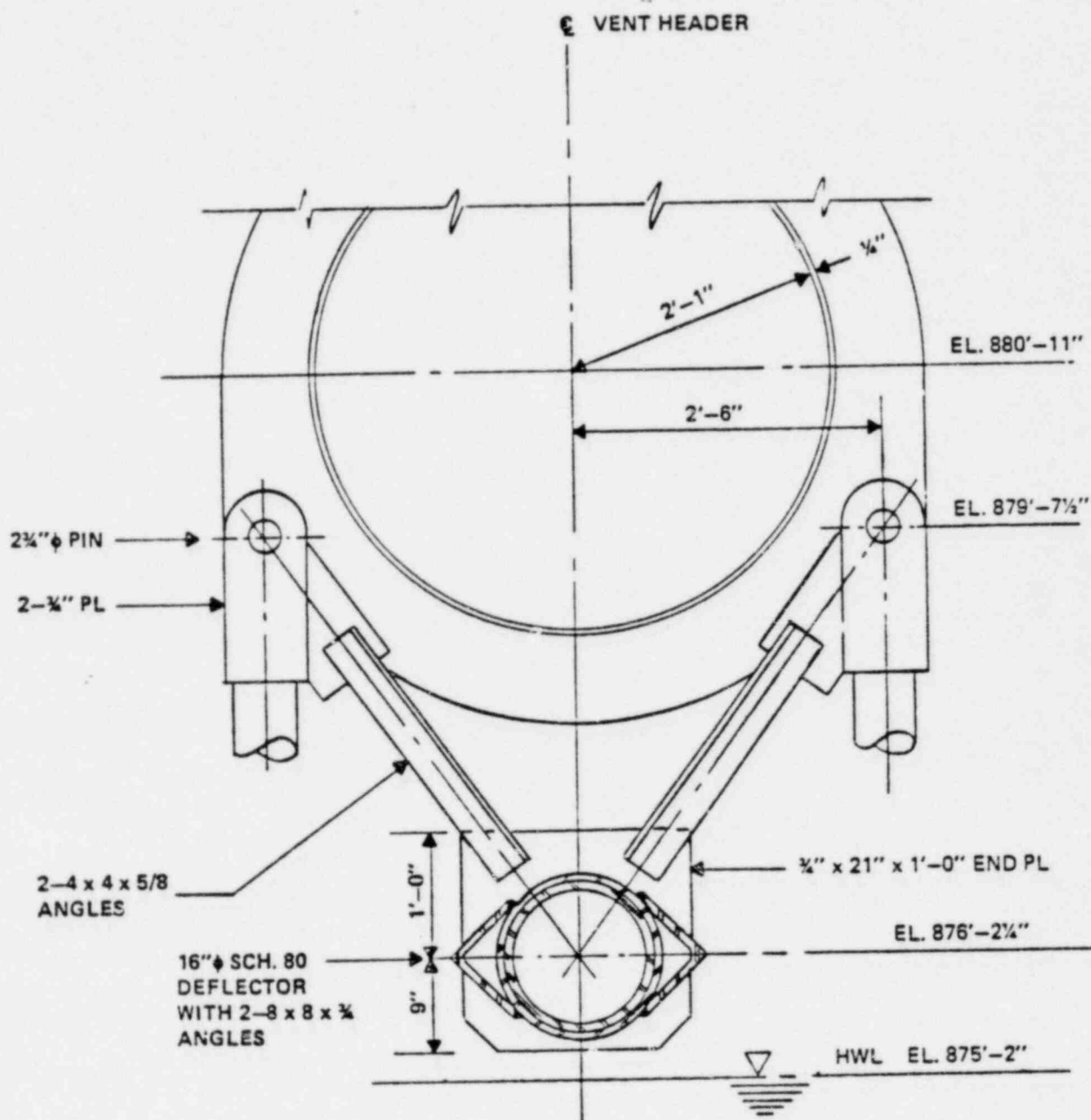
TORUS SUPPORT COLUMN

OBJECTIVE: INHIBIT SHELL OVALIZATION



TORUS SADDLE

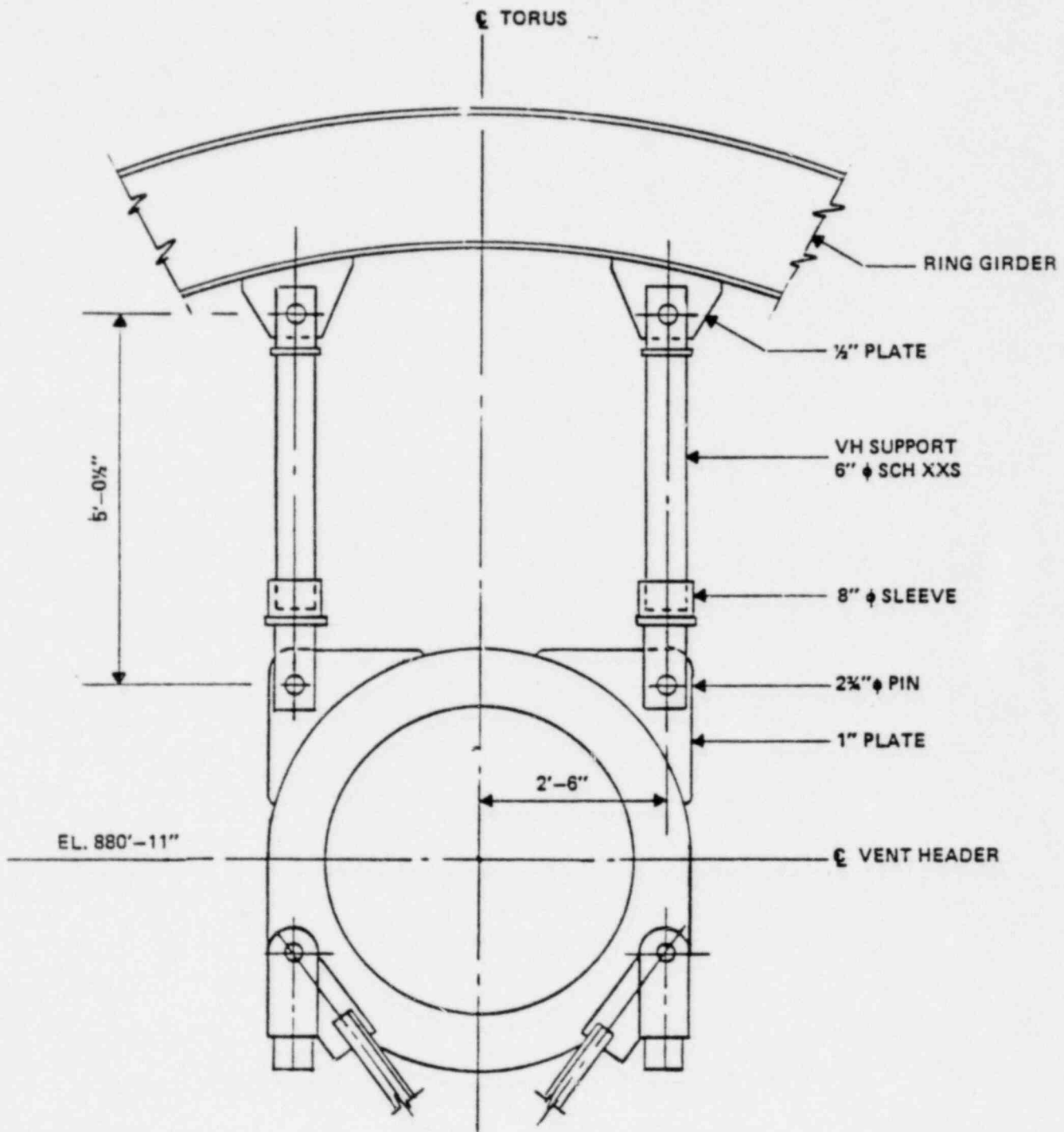
OBJECTIVE: MITIGATE POOL SWELL LOADS ON VENT HEADER



VENT HEADER DEFLECTOR

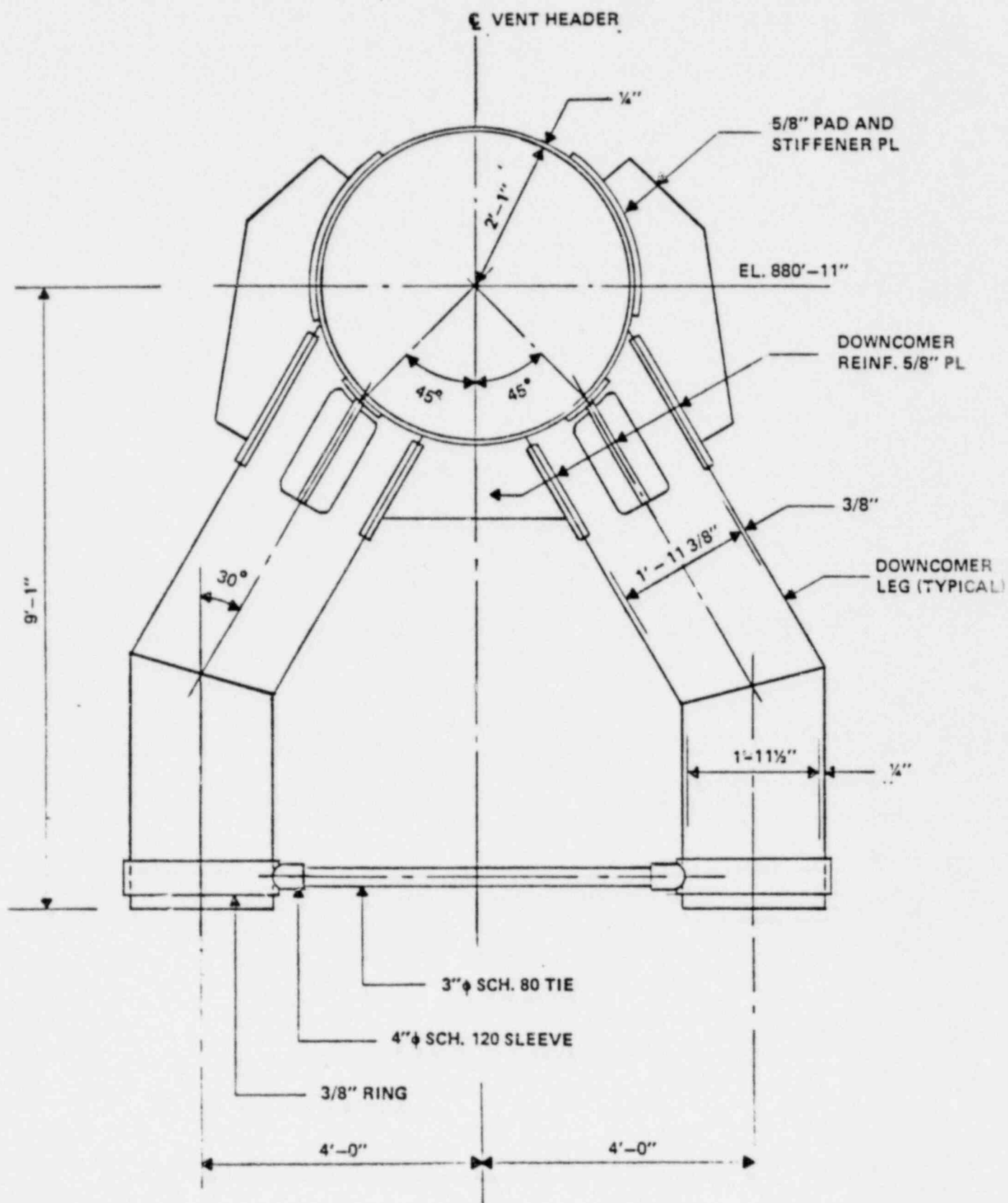


OBJECTIVE: REDUCE DRAG LOADS ON VENT HEADER SUPPORTS



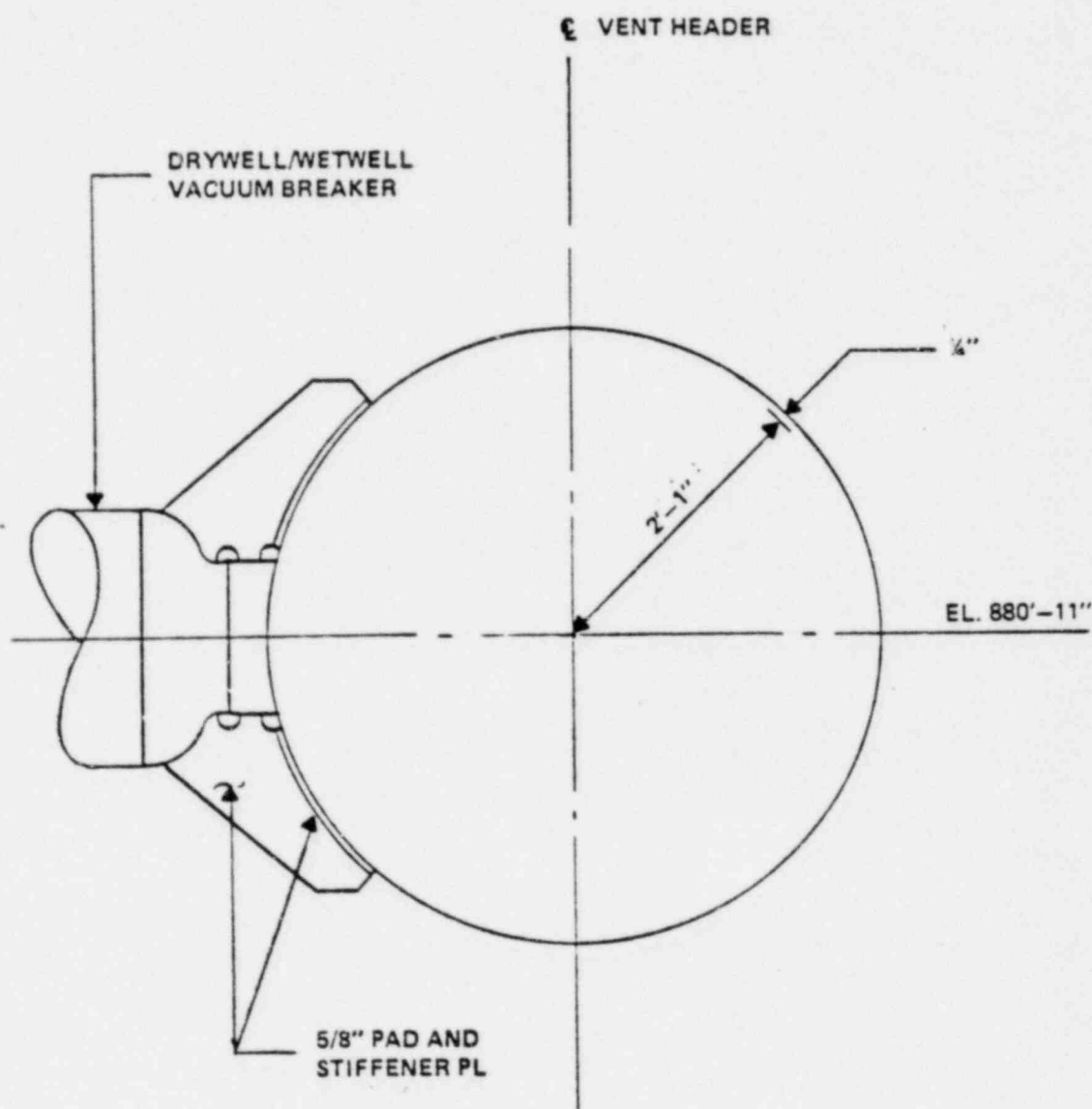
## VENT HEADER SUPPORT COLUMNS

OBJECTIVE: REDUCE STRESSES AT INTERSECTION



DOWNCOMER REINFORCEMENT

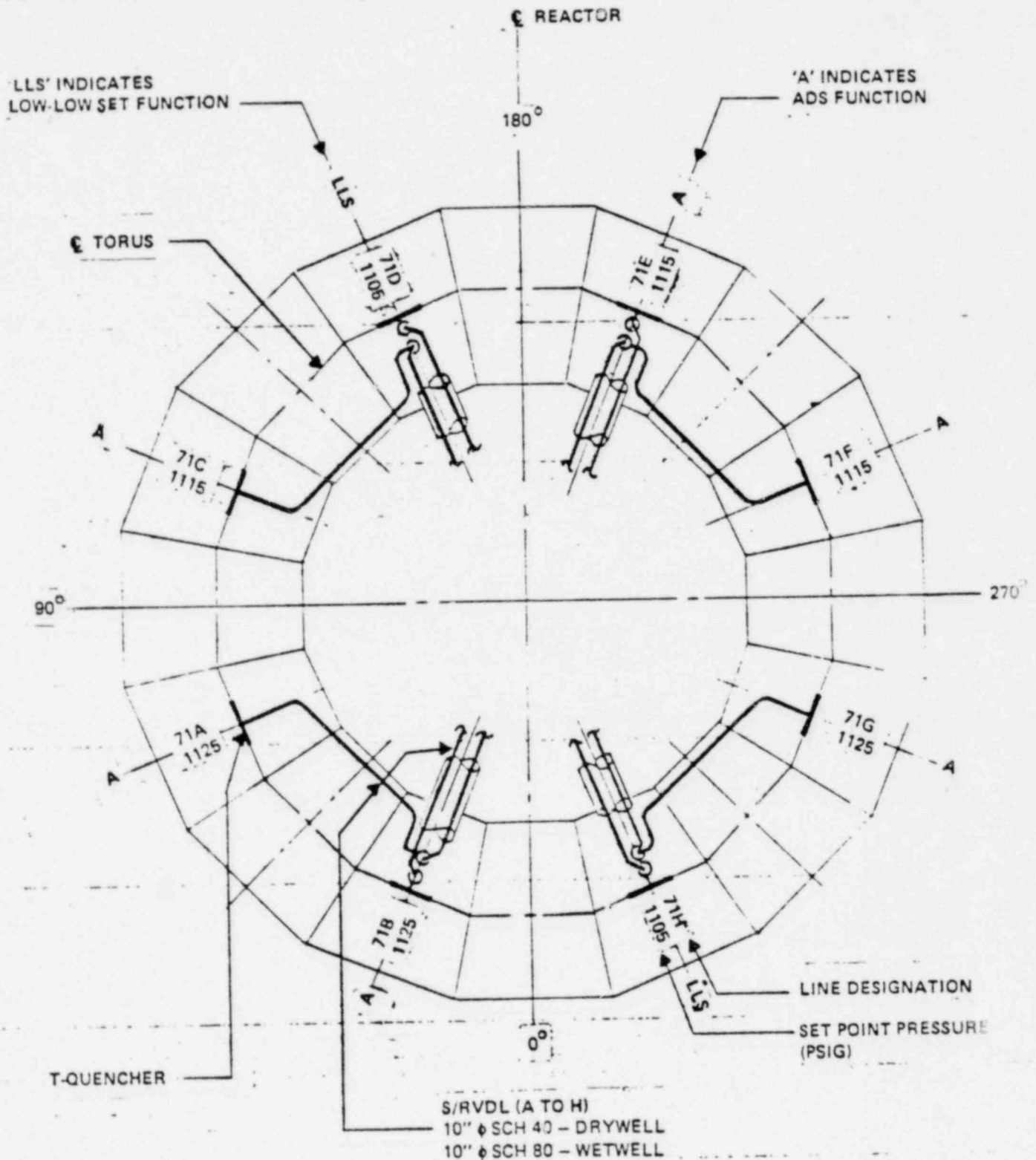
OBJECTIVE: REDUCE STRESSES AT PENETRATION DUE TO POOL  
SWELL IMPACT AND FROTH IMPINGEMENT



DRYWELL/WETWELL VACUUM BREAKER REINFORCEMENT

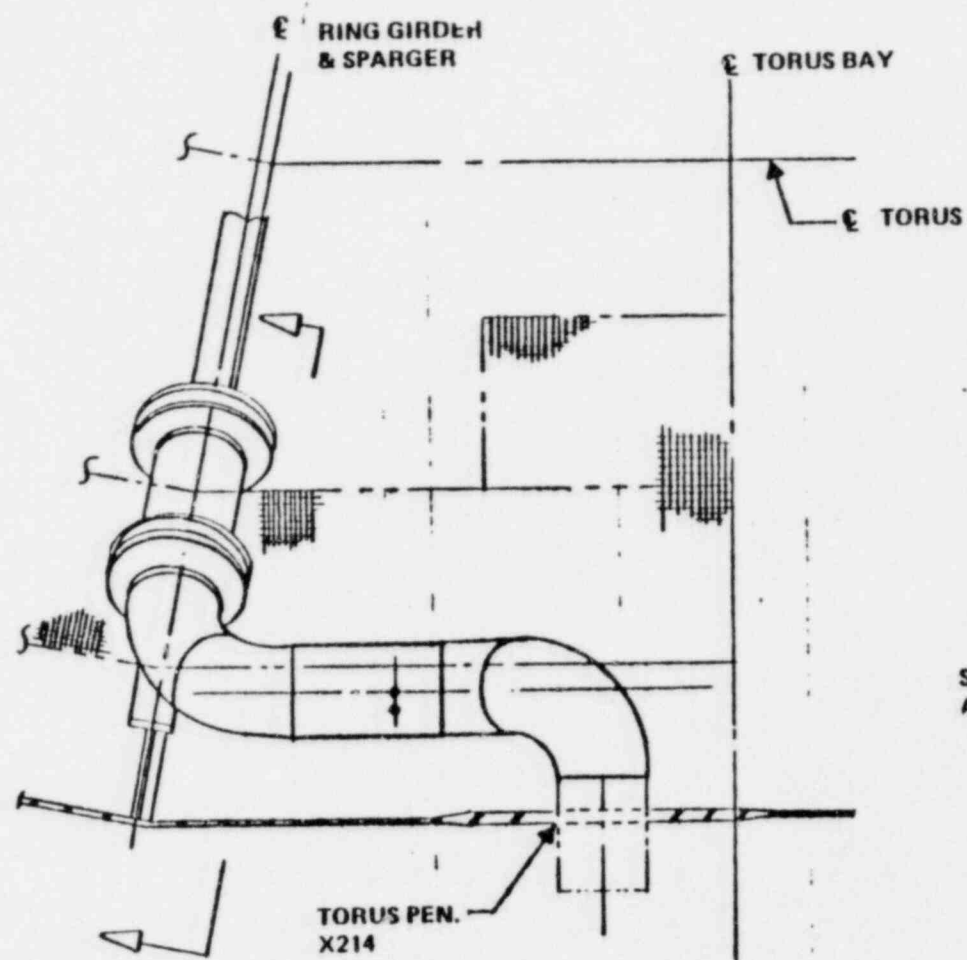
## OBJECTIVES:

- INSTALLATION OF T-QUENCHERS; BETTER DISCHARGE DEVICE DISTRIBUTION
- REROUTE PIPE; MINIMIZE LOADS
- RESUPPORT PIPING WETWELL AND DRYWELL; QUALIFY FOR LINE CLEARING LOADS

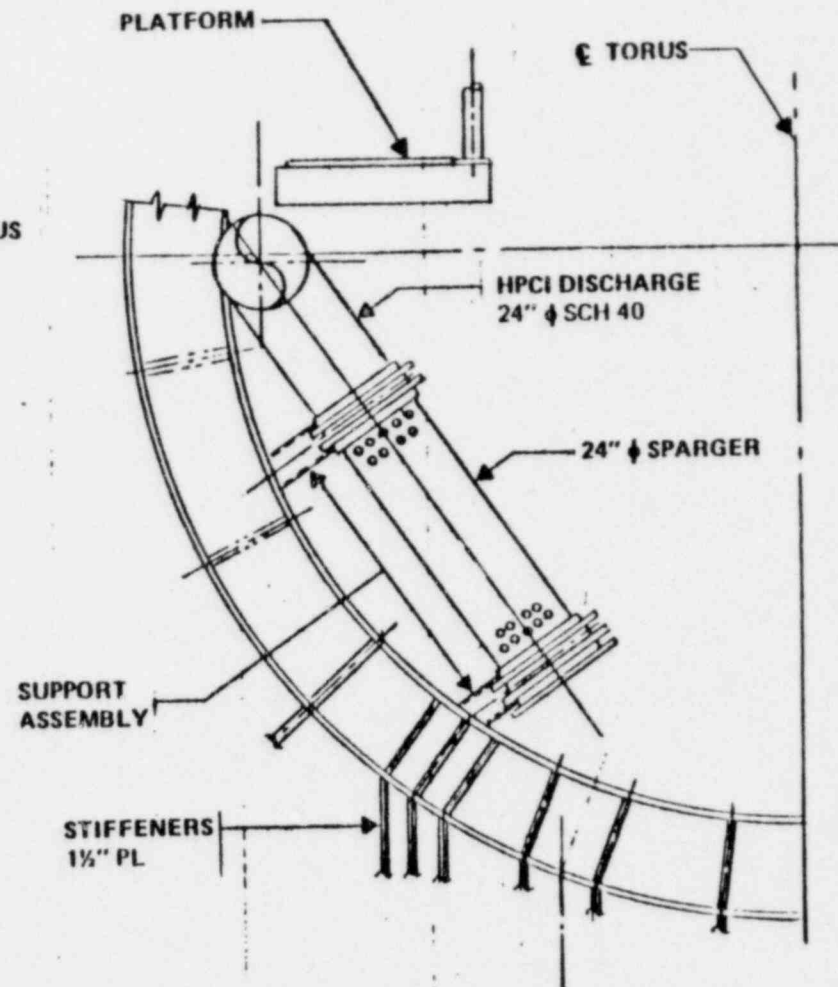


WETWELL ROUTING OF S/RVDLS

OBJECTIVE :  
TO REDUCE DRAG LOADS



PLAN

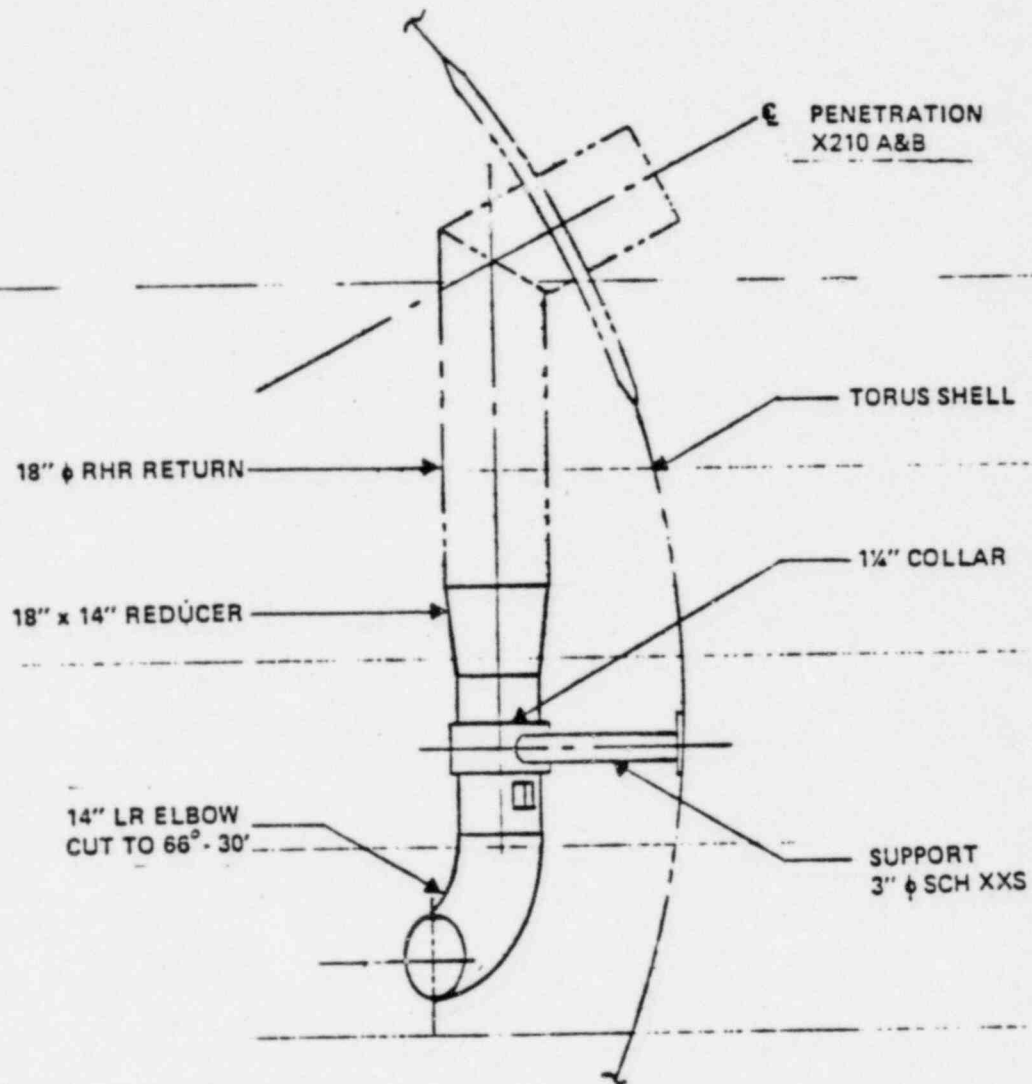


SECTION

HPCI TURBINE EXHAUST - REROUTE/RESUPPORT

OBJECTIVES:

- IMPROVE POOL CIRCULATION (THERMAL MIXING)
- BRACE: FOR HIGH DRAG LOADS



RHR PUMP TEST RETURN LINE MODIFICATION

## TORUS ATTACHED PIPING MODIFICATIONS

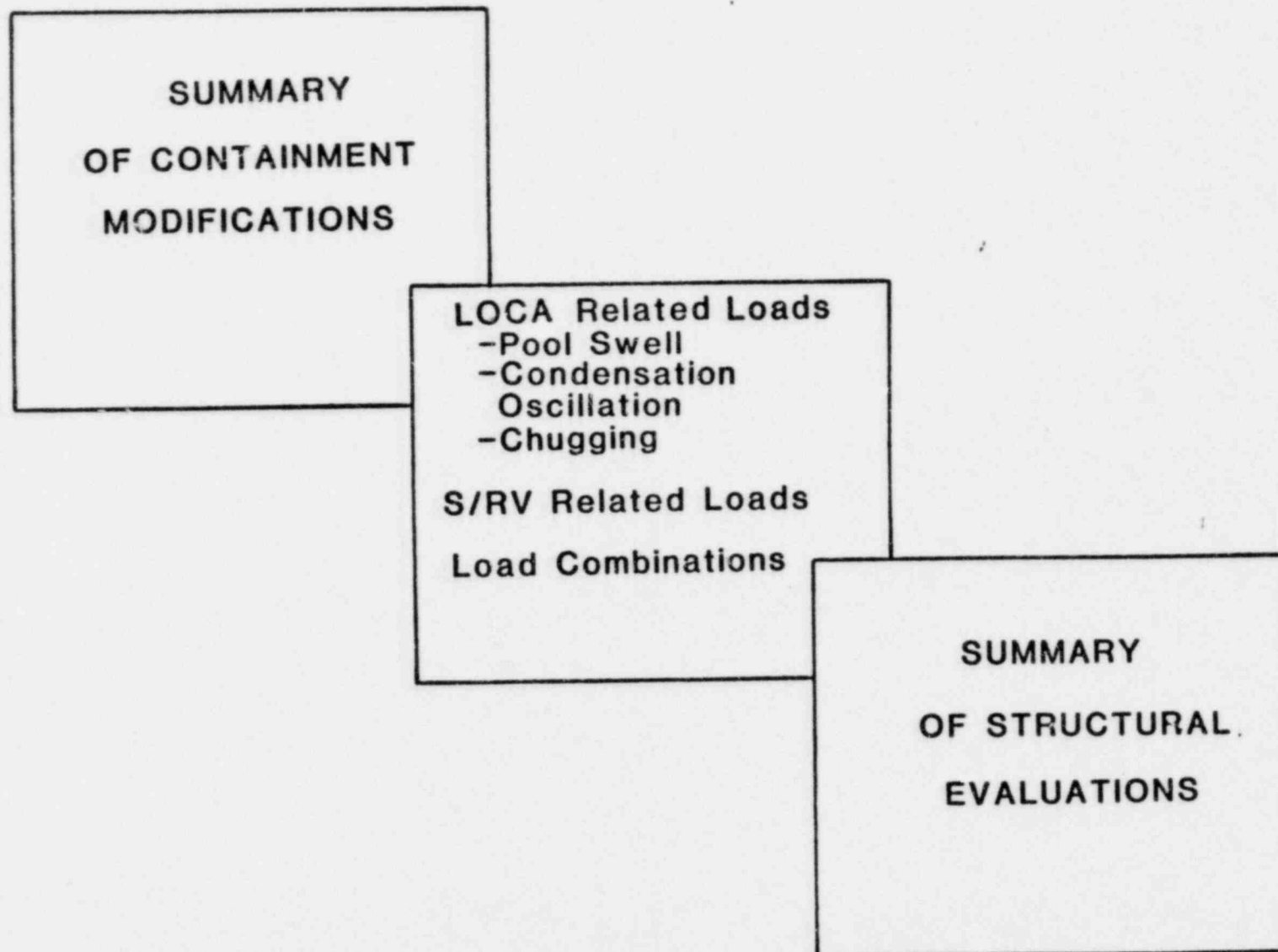
- PIPE SUPPORTS ON LARGE BORE TAP
  - 14 ADDED
  - 137 OF 239 MODIFIED
- SMALL BORE TAP
  - 60 NEW OR MODIFIED SUPPORTS
  - 4 LINES REROUTED
- BRANCH PIPING
  - 25 NEW OR MODIFIED SUPPORTS
- VALVES
  - 13 VALVES REINFORCED
- TORUS SHELL PENETRATIONS
  - 3 PENETRATIONS REINFORCED
- ECCS PUMPS
  - 4 PUMP ANCHORAGES REINFORCED

## SYSTEM MODIFICATIONS

- DRYWELL-TO-WETWELL  $\Delta P$ 
  - MAINTAIN PRESSURE DIFFERENTIAL BETWEEN DRYWELL AND TORUS
  - MITIGATE POOL SWELL LOADS ON TORUS AND VENT SYSTEM
  
- LOW-LOW SET RELIEF LOGIC
  - INCREASE REACTOR DEPRESSURIZATION FOLLOWING S/RV ACTUATION
  - INCREASE TIMING BETWEEN ACTUATIONS
  - REDUCE LOADS DUE TO CONSECUTIVE ACTUATIONS AND NUMBER OF S/RV ACTUATIONS
  
- MSIV WATER LEVEL TRIP
  - DELAY MSIV ISOLATION TO RELEASE MORE REACTOR ENERGY
  - ELIMINATE 2ND ACTUATIONS OF S/RV DURING IBA/SBA
  
- POOL TEMPERATURE MONITORING SYSTEM
  - MEASURE LOCAL POOL TEMPERATURES NEAR T-QUENCHERS
  - ENSURE POOL TEMPERATURES STAY WITHIN ALLOWABLE LIMITS



# PRESENTATION CONTENTS - LOAD DEFINITION AND TREATMENT



## SUMMARY OF LOAD DEFINITION AND APPLICATION

- LOAD DEFINITION IS BASED ON:
  - GE LOAD DEFINITION REPORT
  - MARK I PUAAG
  - NRC ACCEPTANCE CRITERIA
  - NRC SAFETY EVALUATION REPORT
  
- PLANT UNIQUE LOAD DEFINITIONS
  
- LOAD APPLICATION

## LOADS AND LOAD COMBINATIONS

- THERMAL-HYDRAULIC PARAMETERS
  - BASED ON CNS FSAR
  - ALTERED BY SYSTEM MODIFICATION
  - USED BOTH ZERO  $\Delta P$  AND CURRENT  $\Delta P$
- ORIGINAL DESIGN LOADS
  - DEAD LOADS
  - SEISMIC LOADS
  - PRESSURE AND TEMPERATURE
  - VENT THRUST LOAD
  - JET FORCES ON DOWNCOMER PIPES
- LOCA RELATED LOADS
- S/RV DISCHARGE RELATED LOADS
- DETERMINATION OF LOAD COMBINATIONS

## LOCA RELATED LOADS

- CATEGORIES OF A LOCA

- DESIGN BASIS ACCIDENT (DBA)
- INTERMEDIATE BREAK ACCIDENT (IBA)
- SMALL BREAK ACCIDENT (SBA)

- SPECIFIC LOADS AND TRANSIENTS

- PRESSURE AND TEMPERATURE
- VENT SYSTEM THRUST
- POOL SWELL
- CONDENSATION OSCILLATION
- CHUGGING

[illegible]

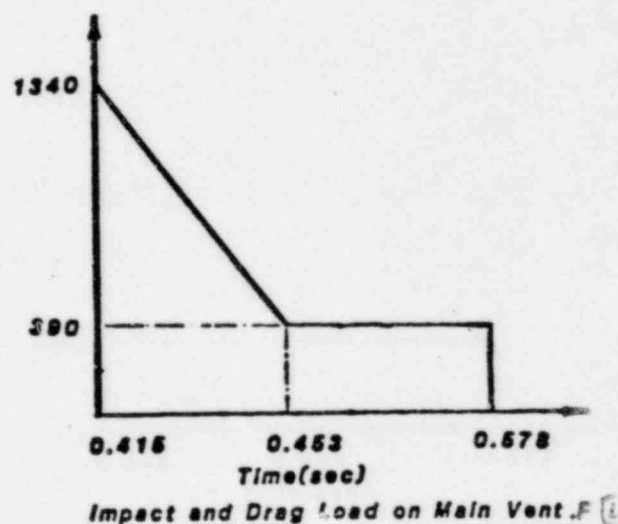
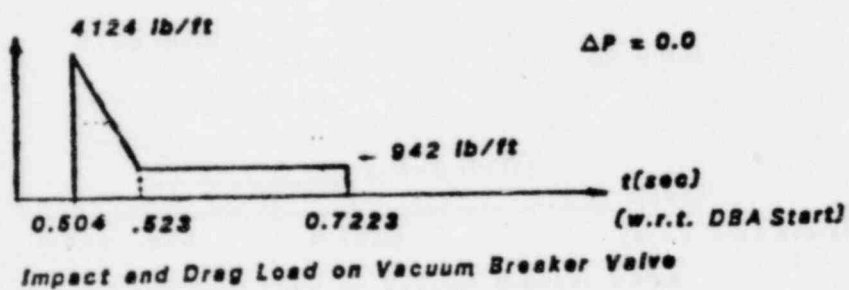
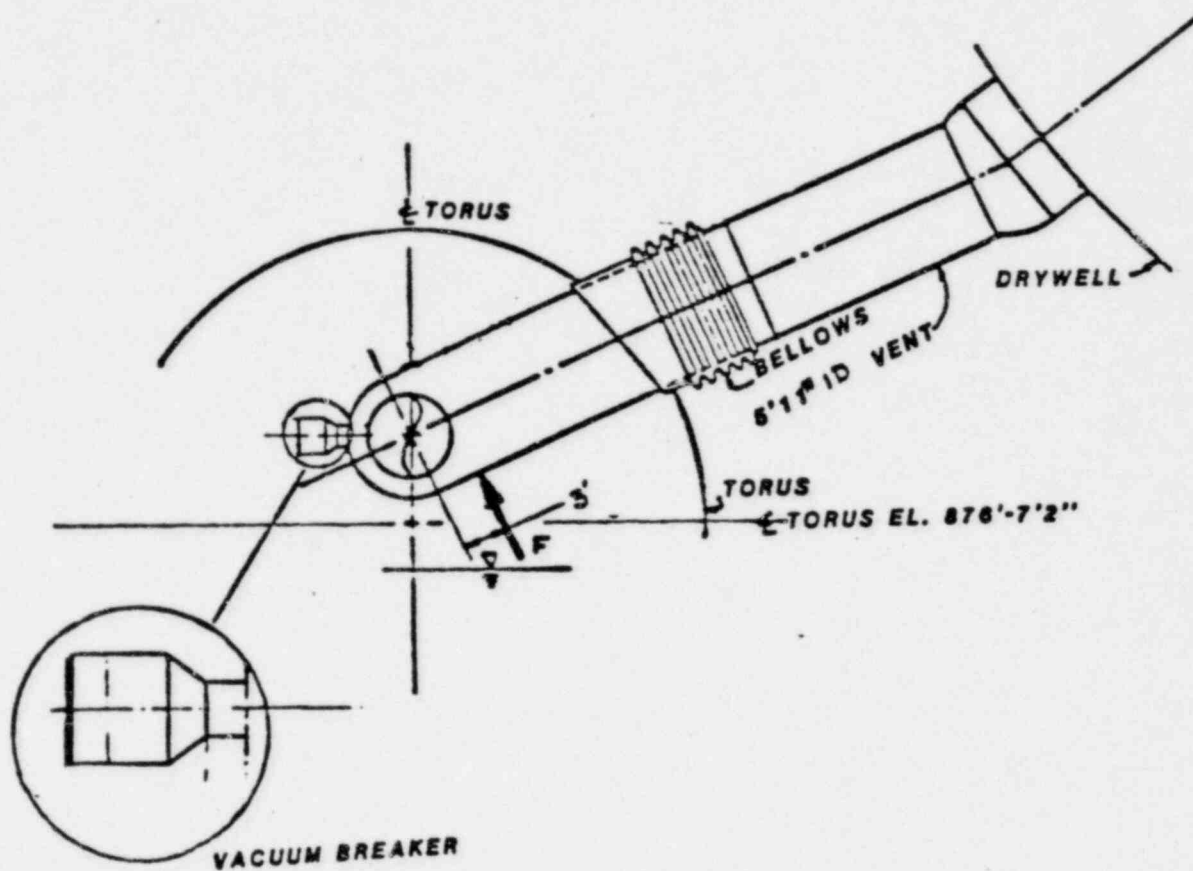


FIGURE 2.17

POOL SWELL IMPACT/DRAG LOAD TRANSIENTS  
ON MAIN VENT,  $\Delta P = 1.0$  psid

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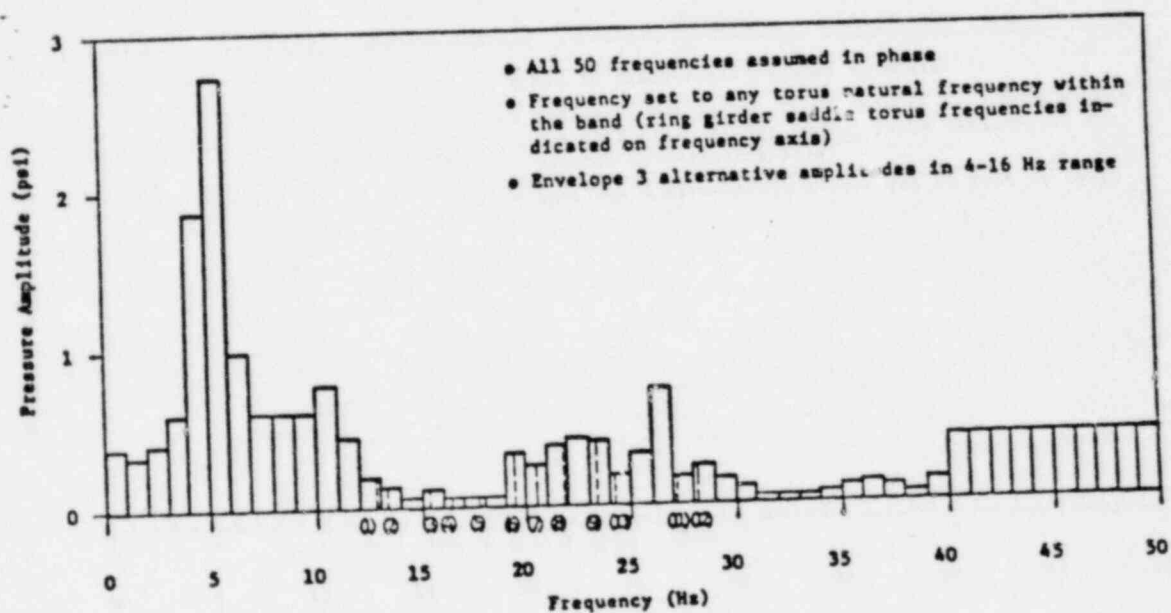
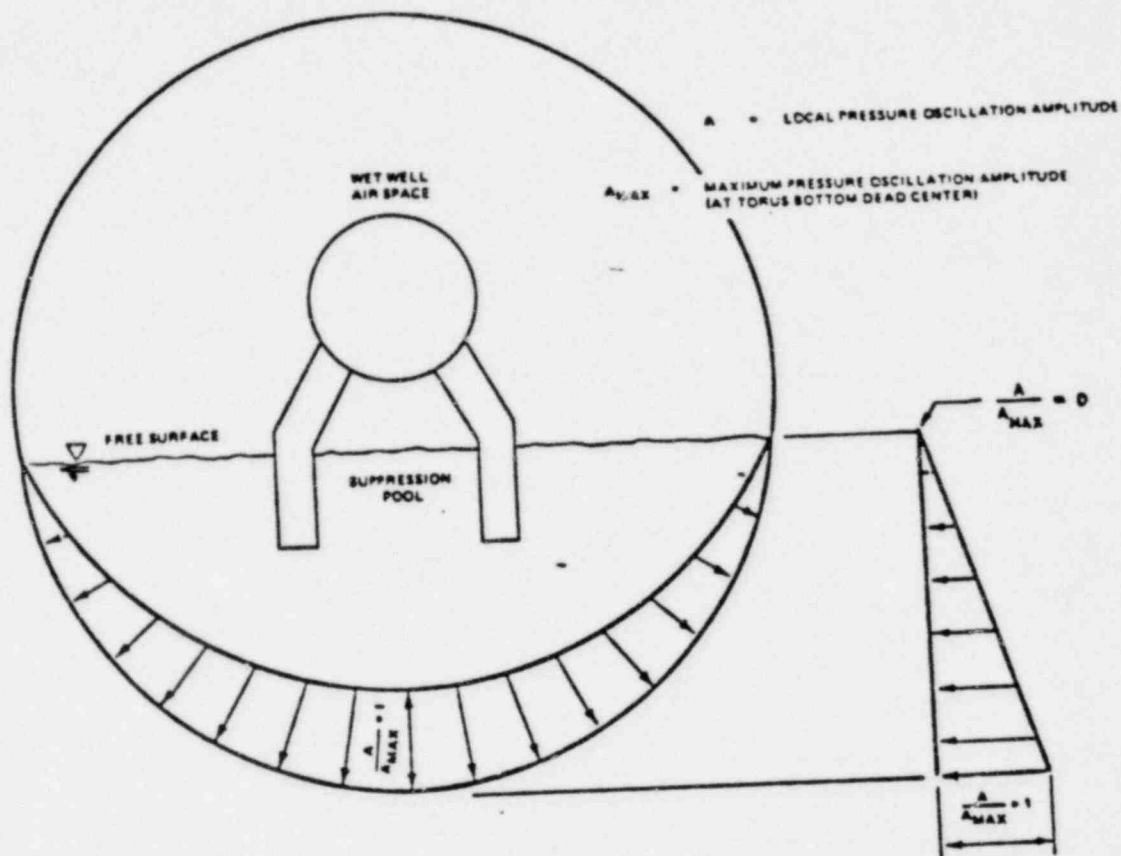


FIGURE 2.21

TORUS PRESSURE AMPLITUDE DISTRIBUTION FOR CONDENSATION OSCILLATION



## DBA CO RANDOM PHASING

### ● DESCRIPTION

- DESIGN RULE FOR COMBINING STRUCTURAL RESPONSES TO CO LOAD HARMONICS
- 4 ASUM + 46 SRSS
- 1.3 X TIME HISTORY WITH RANDOM PHASE ANGLES

### ● REASONS

- FSTF TEST DATA SHOWS RANDOMNESS
- ASUM RULE SIGNIFICANTLY OVERPREDICTS FSTF DATA
- OTHER AREAS OF CONSERVATISM IN CO LOAD DEFINITION

### ● JUSTIFICATION

- EMPIRICAL DATA
  - o EXAMINE FSTF DATA FOR RANDOMNESS
  - o DESIGN RULE PREDICTIONS BOUND FSTF MEASURED RESPONSE
- ANALYTICAL STUDIES
  - o STATISTICAL STUDIES WITH RANDOM PHASING
  - o DESIGN RULE EXCEEDS 84% NEP LEVEL
- GENERIC MARK I REPORT

[illegible]

[illegible]

## S/RV DISCHARGE TORUS SHELL PRESSURES MULTIPLE VALVE ACTUATIONS

### ● DESCRIPTION

- COMBINATION METHOD FOR SPATIAL DISTRIBUTION OF TORUS PRESSURES DUE TO MVA
- 1.2 X SRSS OF PRESSURE FROM EACH DISCHARGE DEVICE

### ● REASONS

- ABSOLUTE SUM OF PRESSURES ASSUMES IN-PHASE BEHAVIOR OF BUBBLES
- NO PHYSICAL BASIS FOR IN-PHASE BEHAVIOR
- MVA PRESSURES LIMIT DESIGN

### ● JUSTIFICATION

- PLANT UNIQUE STATISTICAL STUDY
- MODEL ACTUAL PHASING OF BUBBLES WITH RANDOM VARIATION OF PLANT PARAMETERS
- 1.2 SRSS PRESSURE BOUNDS RESULTS OVER 90% OF THE TIME

S/RV TORUS SHELL PRESSURES  
30% RELATIVE HUMIDITY

- DESCRIPTION

- INITIAL S/RV DL RELATIVE HUMIDITY OF 30%
- IBA/SBA CONDITIONS ONLY
- ADS ACTUATION ONLY

- REASONS

- PURE AIR MASS ASSUMPTION UNREALISTIC
- STEAM IN DRYWELL DURING IBA/SBA
- AT ADS, DRYWELL AIR PURGED TO WETWELL

- JUSTIFICATION

- EXAMINED

DRYWELL STEAM CONTENT TRANSIENTS  
CNS S/RV DL VACUUM BREAKER SET POINTS

- SHOW 90-100% RH IN DRYWELL
- SHOW 30% RH IN S/RV DL IS STILL CONSERVATIVE

## LOAD COMBINATIONS

- TORUS SHELL
- VENT SYSTEM
- INTERNAL STRUCTURES ABOVE POOL
- SUBMERGED STRUCTURES
- S/RVD PIPING
- TORUS ATTACHED PIPING
- FATIGUE
  - BASIS FOR 40 YEAR LIFE

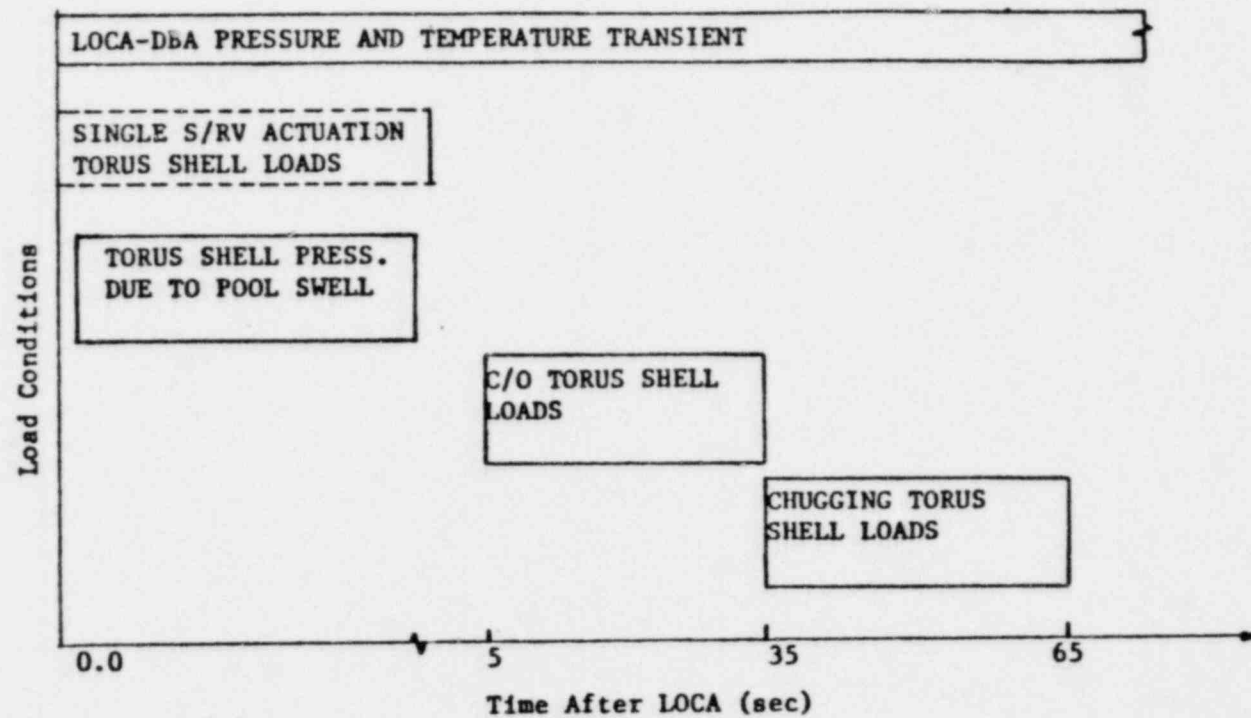
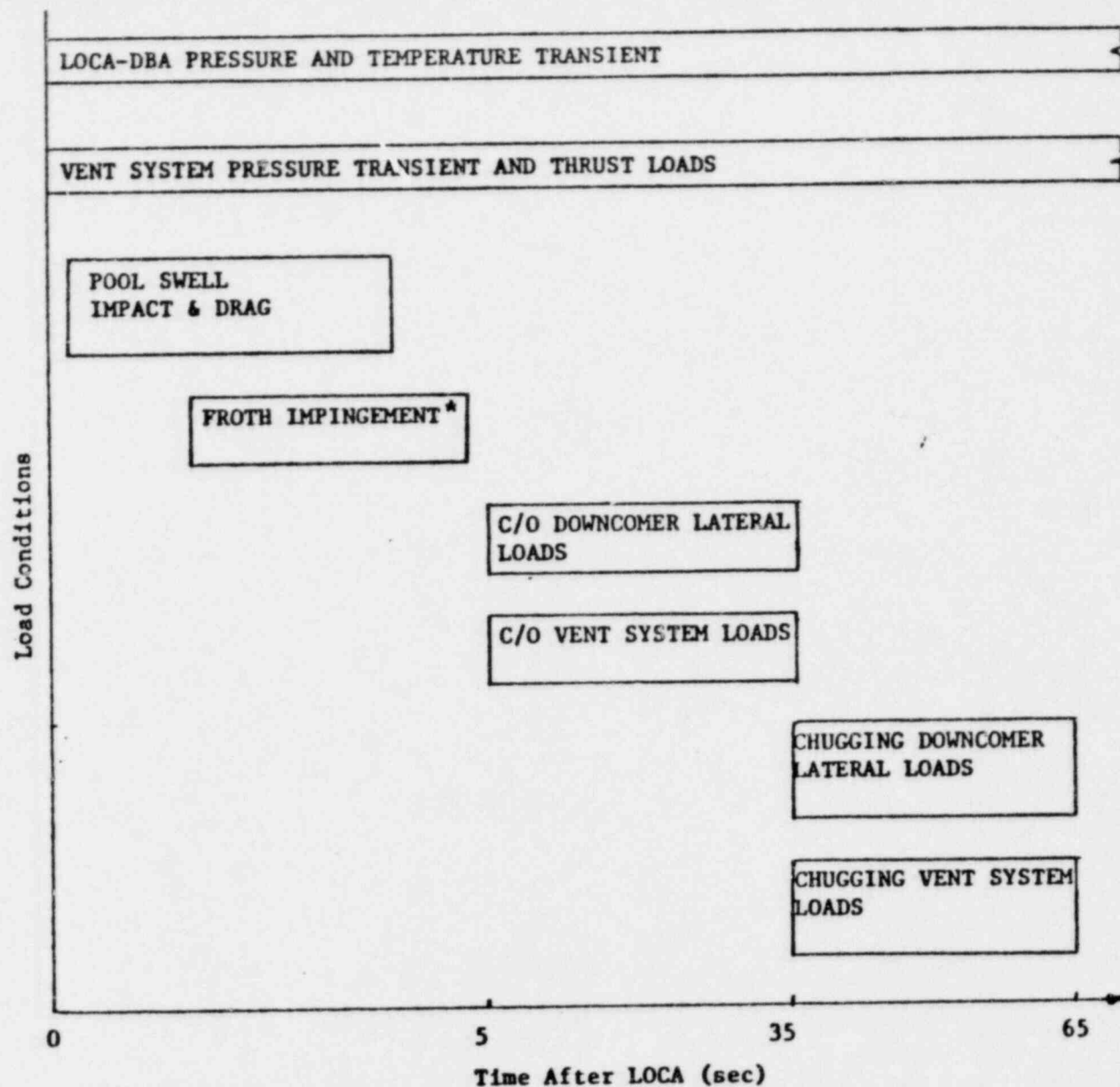


FIGURE 2.25

TORUS SHELL LOAD COMBINATIONS FOR LOCA-DBA



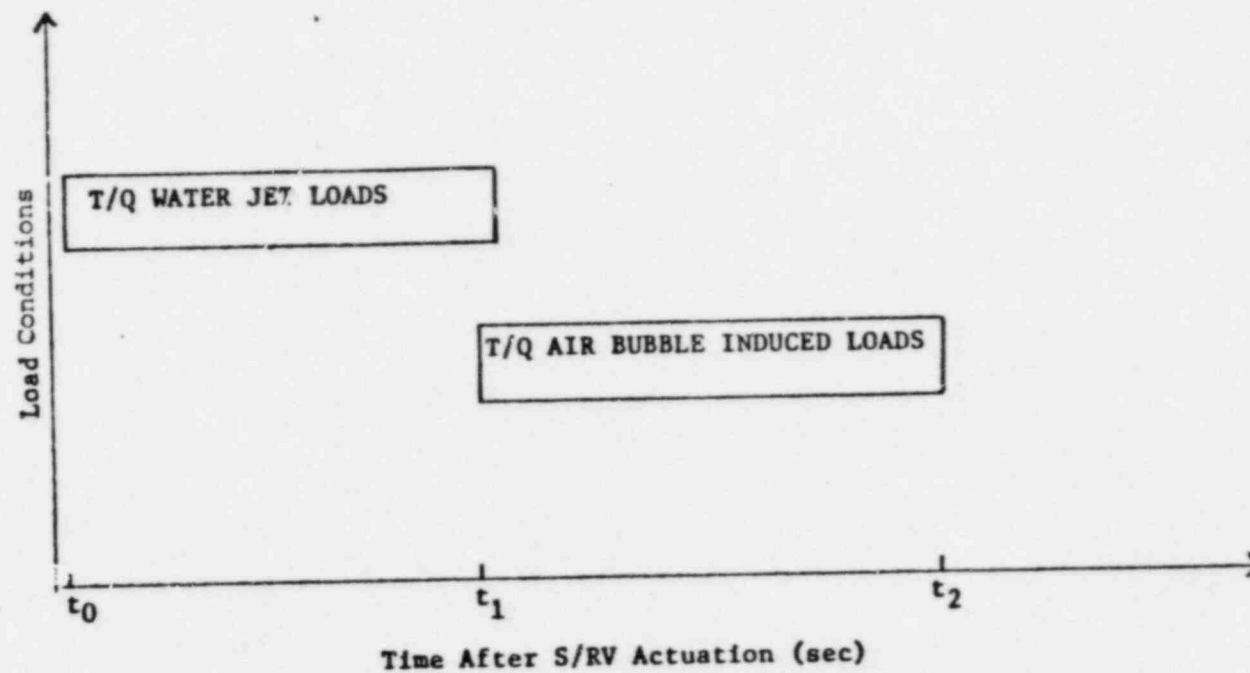
\*For main vent only.

\*\*For submerged portion of downcomers see also Figure 2.32

FIGURE 2.28

VENT SYSTEM LOAD COMBINATIONS FOR LOCA-DBA\*\*





$t_0$  = S/RV actuation time

$t_1$  = S/RVDL water clearing time

$t_2$  = time at which S/RV bubbles reach pool surface

FIGURE 2.35

S/RV DISCHARGE LOADS ON SUBMERGED STRUCTURES

# PRESENTATION CONTENTS - STRUCTURAL EVALUATION

**SUMMARY  
OF CONTAINMENT  
MODIFICATIONS**

**SUMMARY  
OF LOAD DEFINITION  
AND TREATMENT**

**Torus Shell & Support  
Vent System & Supports  
S/RV Discharge Piping  
Torus Attached Piping**

## TORUS SHELL

- LOADS

- 27 LOAD COMBINATIONS DEFINED
- POTENTIALLY BOUNDING ONES CONSIDERED

- DESIGN ALLOWABLES

- CLASS MC VESSEL - SUBSECTION NE
- BUCKLING ALLOWABLES

- ANALYSIS METHODS

- SHELL MODELS
  - 1/32 SEGMENT COUPLED SHELL-FLUID MODEL
  - 1/4 SEGMENT PLATE ELEMENT MODEL-SEISMIC
- STATIC ANALYSIS
  - PRESSURE AND TEMPERATURE
  - GRAVITY
  - SEISMIC
- DYNAMIC ANALYSIS
  - POOL SWELL
  - DBA CO
  - CHUGGING
  - S/RV DISCHARGE

- CODE EVALUATION

- MAXIMUM SHELL STRESS
- FATIGUE USAGE

## TORUS SHELL BUCKLING ALLOWABLES

- DESCRIPTION

- INVESTIGATION OF DYNAMIC TORUS BUCKLING
- BUCKLING NOT A CONCERN FOR MARK I LOADS

- REASONS

- CODE COMPRESSIVE STRESS ALLOWABLES  
BASED ON STATIC, UNIFORM LOADS
- MARK I LOADS ARE DYNAMIC, NON-UNIFORM
- COMPRESSIVE STRESSES OF SHORT DURATION

- JUSTIFICATION

- LOCA TRANSIENTS NOT CONTROLLING  
HIGH WETWELL PRESSURE
- S/RV DISCHARGE EVENTS CONTROL
- EMPIRICAL EVIDENCE  
IN-PLANT TESTS
- CONFIRMATORY NONLINEAR ANALYSIS  
GENERIC STUDY  
FACTOR OF SAFETY = 7  
SATISFY ASME CODE REQUIREMENTS
- APPLICATION TO CNS  
GEOMETRY  
LOADS

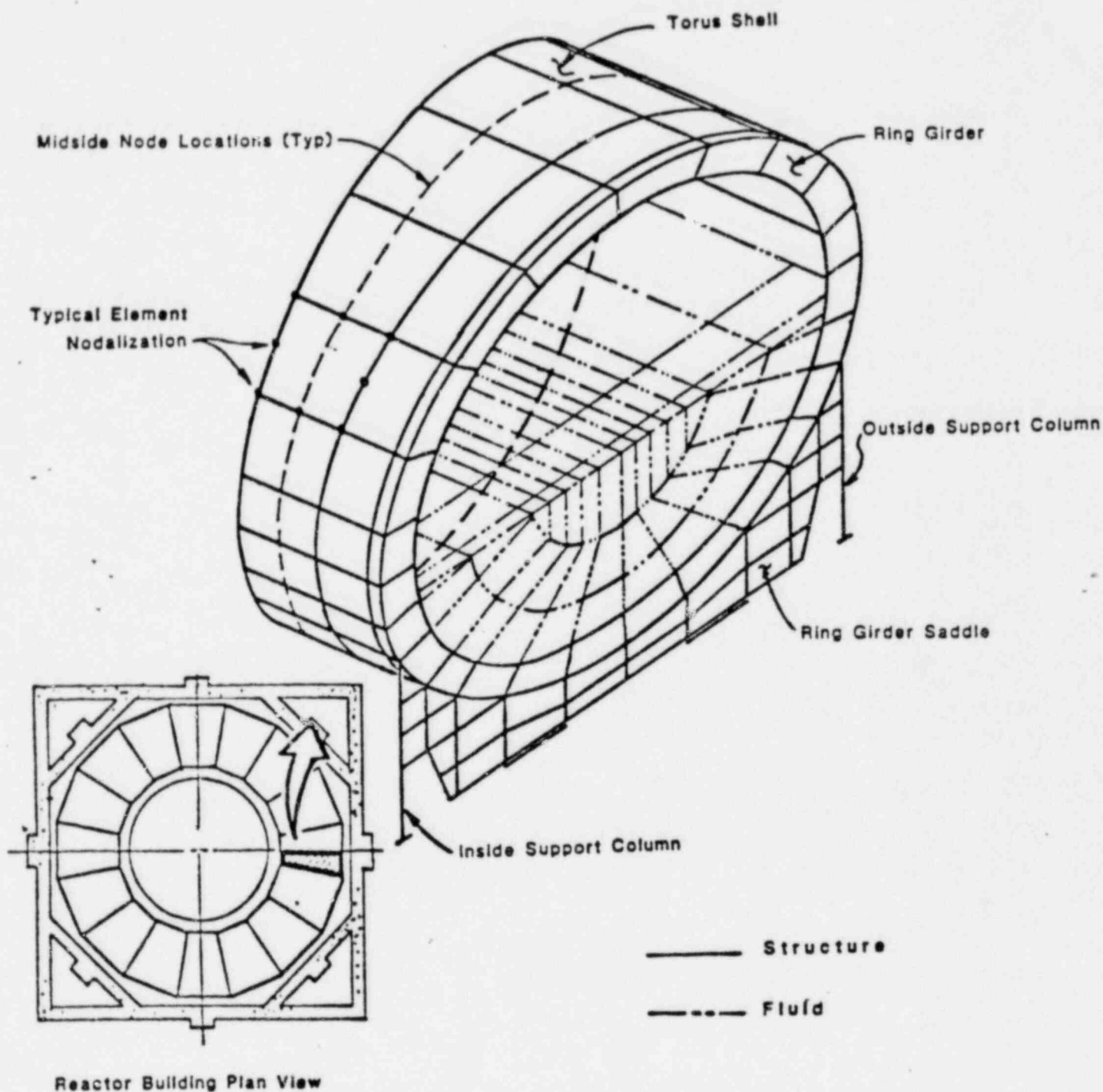


FIGURE 3.1  
1/32 SECTION TORUS MODEL

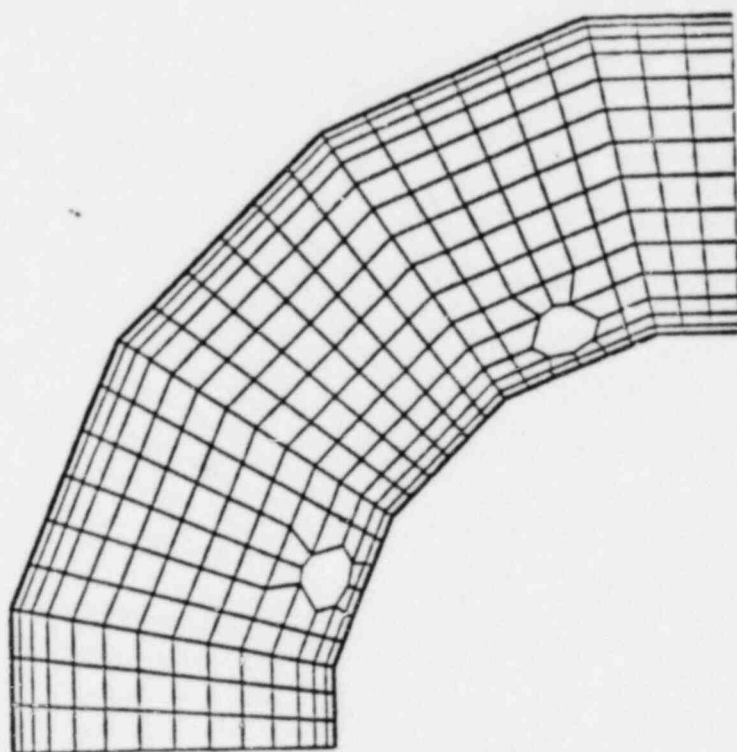


FIGURE 3.2  
90° SECTION TORUS MODEL

## TORUS SUPPORT SYSTEM

### ● DESIGN LOAD COMBINATIONS

- COLUMN AND ANCHORAGE  
TORUS SHELL LOADS
- SEISMIC TIES  
NET LATERAL LOAD  
SEISMIC  
S/RV DISCHARGE  
PRE-CHUG
- RING GIRDER SADDLE  
TORUS SHELL LOADS  
PRESSURE AND TEMPERATURE

### ● DESIGN ALLOWABLES

- LINEAR COMPONENTS - APPENDIX XVII
- PLATE AND SHELL SUPPORTS - SUBSECTION NF

### ● ANALYSIS METHODS

- SUPPORT COLUMNS
  - ANCHORAGE ASSEMBLY
  - SEISMIC TIES
  - RING GIRDER SADDLE
- }
- SUBSECTION NF  
AND  
APPENDIX XVII

USED 1/32 SEGMENT SHELL MODEL

NONLINEAR ANALYSIS USED FOR INTERMEDIATE SUPPORTS

### ● CODE EVALUATION

- MAXIMUM COLUMN/ANCHORAGE LOAD
- MAXIMUM FATIGUE USAGE

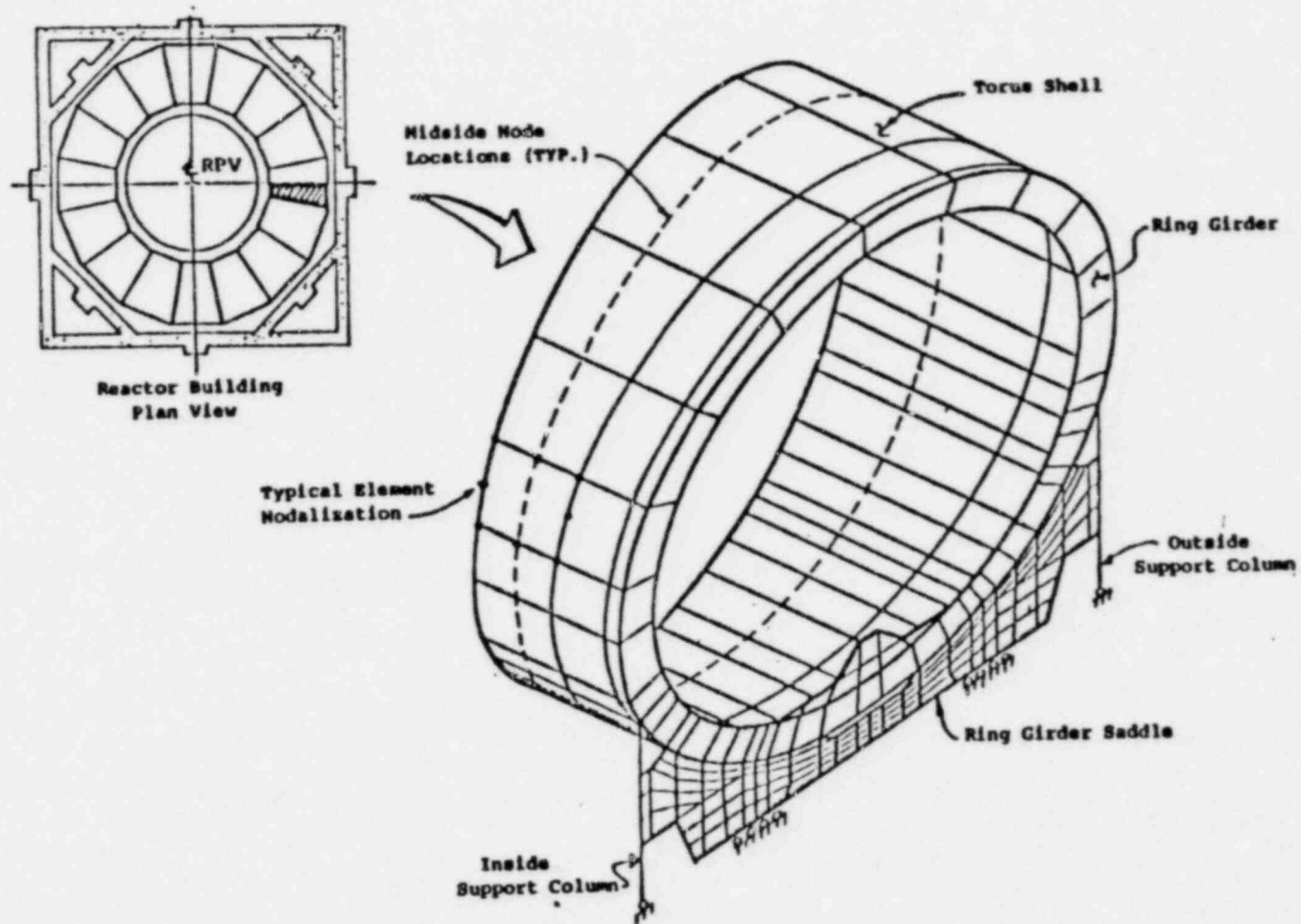


FIGURE 3.3

1/32 SECTION TORUS MODEL WITH DETAILED RING GIRDER SADDLE



## RING GIRDER

- LOADS

- SHELL LOAD COMBINATIONS
- SUBMERGED STRUCTURE
- CONCENTRATED REACTIONS

- DESIGN ALLOWABLES

- MC SUPPORT - SUBSECTION NF
- EXCEPT PORTION WITHIN LIMITS OF SHELL REINFORCEMENT WHERE SUBSECTION NE IS USED

- ANALYSIS METHODS

- RING GIRDER

ALL STRESSES FROM 1/32 SEGMENT MODEL EXCEPT FOR STRESSES DUE TO DRAG LOADS, WHICH ARE DETERMINED SEPARATELY

- RING GIRDER ATTACHMENTS

REACTIONS FROM VENT SYSTEM APPLIED AS EQUIVALENT STATIC LOAD

- CODE EVALUATION

- MAXIMUM STRESS IN RING GIRDER
- MAXIMUM STRESSES IN WELD TO SHELL
- MAXIMUM FATIGUE USAGE

## TORUS SHELL PENETRATION AND ATTACHMENTS

- PENETRATIONS AND ATTACHMENTS INCLUDE:

- TAP PENETRATIONS
- SEISMIC TIES
- MONORAIL SUPPORTS
- ECCS PIPING SUPPORTS

- ANALYSIS METHOD

- REACTIONS FROM APPROPRIATE ANALYSIS
- WRC BULLETIN 107 USED TO OBTAIN LOCAL STRESSES

- LOAD COMBINATIONS

- RESPONSE TO TWO DYNAMIC EVENTS  
COMBINED BY SRSS

## DYNAMIC RESPONSE COMBINATION

### ● DESCRIPTION

- COMBINATION METHOD FOR PEAK RESPONSES TO TWO (S/RV + LOCA) DYNAMIC LOADS
- 1.1 X SRSS OF PEAK DYNAMIC RESPONSES
- ASUM OF REMAINING DYNAMIC LOADS

### ● REASONS

- ASUM RECOGNIZED AS CONSERVATIVE (E.G. NUREG-0484)
- PUAAG ALLOWS CDF METHOD WITH 84% NEP

### ● JUSTIFICATION

- EXAMINE CDF'S USING MARK I DATA (GENERIC STUDY)
- SHOW 1.1 SRSS BOUNDS 84% NEP
- CONFIDENCE LEVEL >90%
- CONFIRM FINDINGS WITH CNS DATA

## VENT SYSTEM AND SUPPORTS

- VENT HEADER AND MAIN VENT
  - VENT SYSTEM ANALYSES
  - VENT HEADER AND MAIN VENT PENETRATIONS
  
- DOWNCOMER AND TIEBARS
  - DOWNCOMER/VENT HEADER INTERSECTION
  - DOWNCOMER ITSELF
  
- SIMPLIFIED ANALYSIS PERFORMED ON:
  - VENT DRAIN LINE
  - VENT HEADER DEFLECTOR
  - VENT HEADER SUPPORT SYSTEM

## VENT SYSTEM ANALYSES

- FINITE ELEMENT MODELS

- 1/16 SEGMENT SHELL MODEL
- BEAM MODEL - NON-SYMMETRIC LOADS
- DOWNCOMER/VENT HEADER INTERSECTION MODEL

- STATIC ANALYSES

- PRESSURE AND TEMPERATURE
- GRAVITY AND SEISMIC
- VENT SYSTEM THRUST

- DYNAMIC ANALYSES

- POOL SWELL, TIME HISTORY
- CO, FREQUENCY DOMAIN
- CHUGGING, EQUIVALENT STATIC
- S/RV DISCHARGE, EQUIVALENT STATIC

- CODE EVALUATION

- MAXIMUM STRESSES  
MAIN VENT  
HEADER  
PENETRATIONS

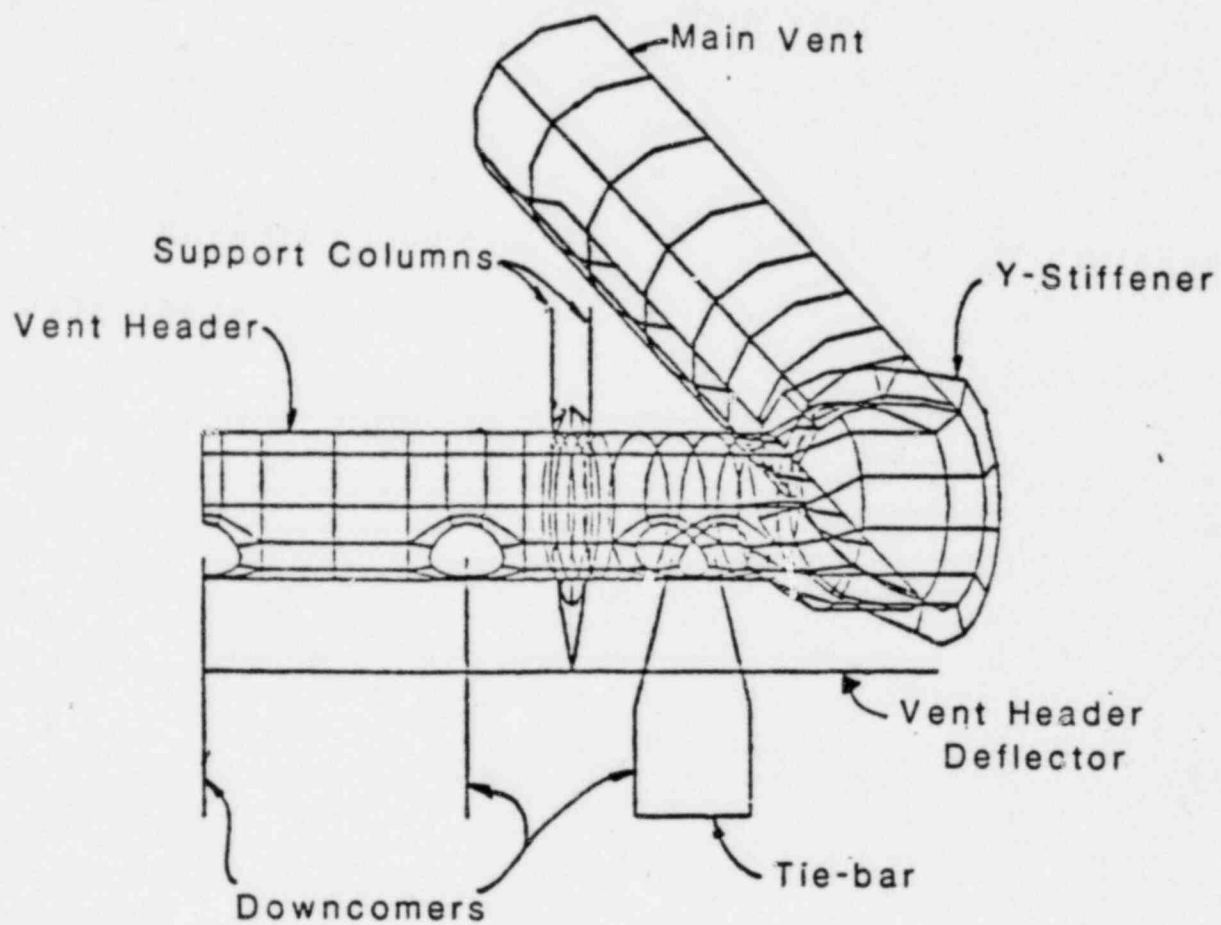


FIGURE 4.1

1/16TH FINITE ELEMENT SHELL MODEL OF VENT SYSTEM

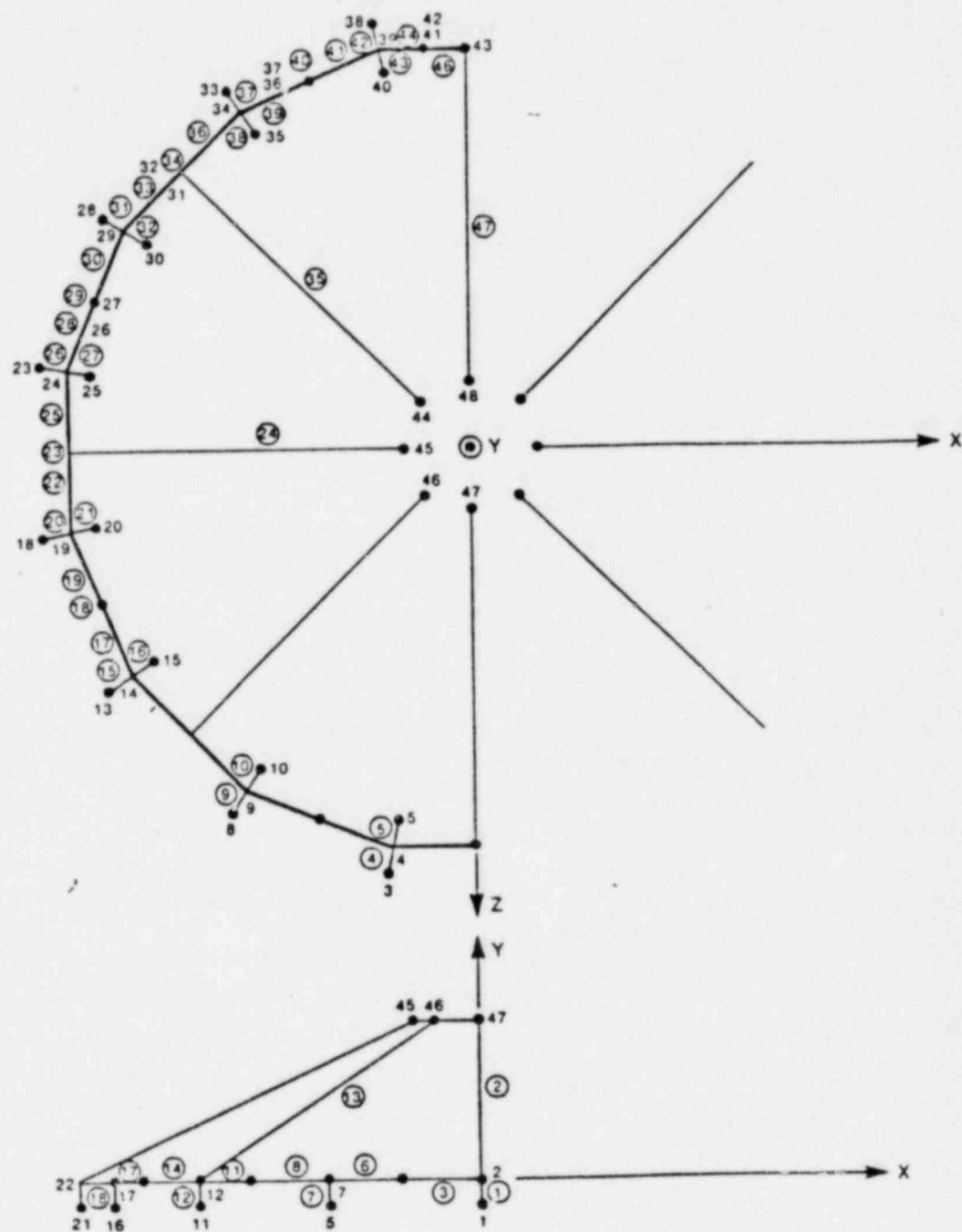


FIGURE 4.2  
180° VENT SYSTEM BEAM MODEL

## DOWNCOMER/VENT HEADER INTERSECTION ANALYSIS

- DESIGN ALLOWABLES

- MC COMPONENT  $\Rightarrow$  SUBSECTION NE
- $P_L$  AND  $P_L + P_B$  ALLOWABLE INCREASED BY 30% BASED ON LIMIT ANALYSIS

- FINITE ELEMENT MODEL

- DETAILED LOCAL MODEL
- UNIT LOAD CASES

- EQUIVALENT STATIC ANALYSIS

- POOL SWELL
- CO LATERAL LOAD
- CHUGGING LATERAL LOAD
- S/RV DISCHARGE DRAG LOADS

- DOWNCOMER ANALYZED USING DETAILED MODEL



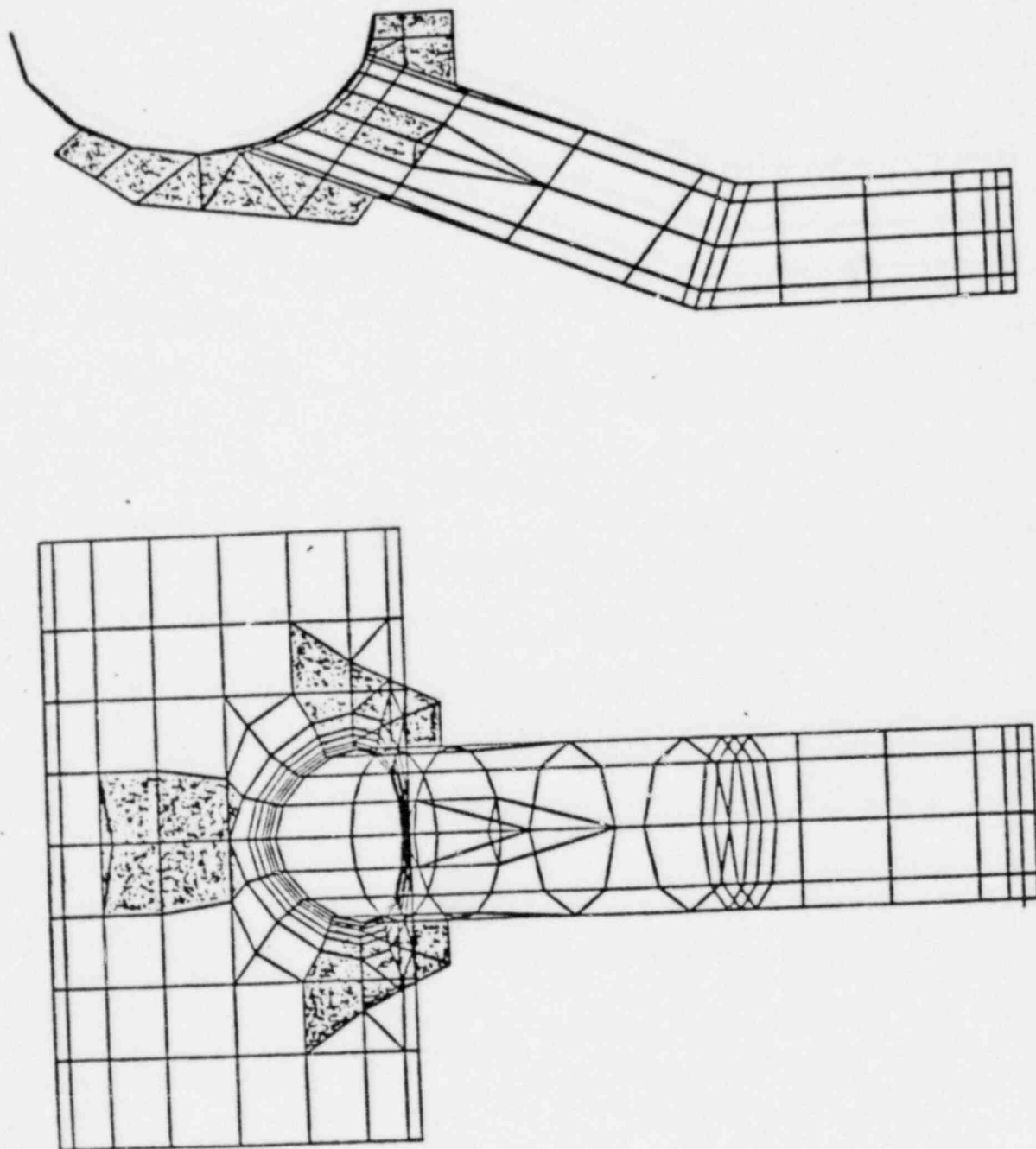


FIGURE 4.13  
DETAILED DOWNCOMER/VENT HEADER INTERSECTION MODEL  
INCLUDING GUSSET PLATE STIFFENERS

## S/RV DISCHARGE LINES

### ● DRYWELL PIPING

- DETERMINED BOUNDING LOADS FROM MAIN VENT PENETRATION COMBINATIONS
- SEPARATE MODEL FOR EACH LINE

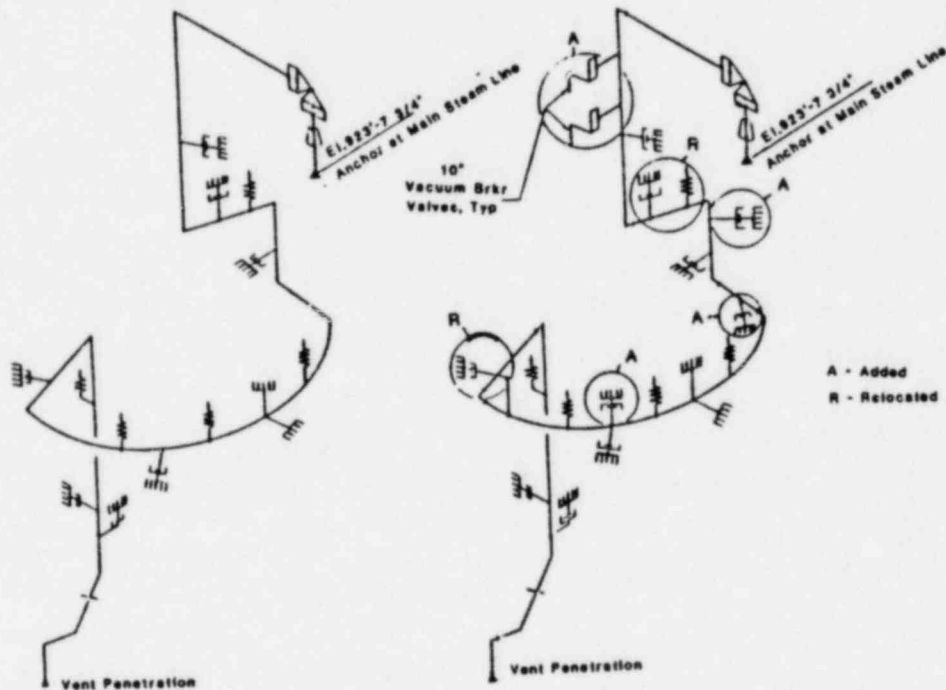


Figure 5.2  
Representative Drywell S/RVD Line Model (line 71G)  
Before and After Modifications

- STATIC ANALYSIS
- DYNAMIC ANALYSIS

TIME HISTORY FOR THRUST LOADS

RESPONSE SPECTRA FOR VENT SYSTEM MOTION

## S/RV DISCHARGE LINES

- WETWELL S/RVD PIPING

- LOADS

- S/RVD THRUST AND WATER CLEARING
    - POOL SWELL
    - CO AND CHUGGING DRAG
    - T-QUENCHER AIR BUBBLE DRAG

- T-QUENCHER EVALUATION

- VACUUM BREAKERS

- LOADS

- PRESSURE AND TEMPERATURE TRANSIENTS
    - GRAVITY AND SEISMIC

- COMPONENT EVALUATED

- ALL PRESSURE RETAINING PARTS
    - HINGE ARM SHAFT
    - FLANGE AND FLANGE BOLTS

## TORUS ATTACHED PIPING

- EXTERNAL PIPING

- ANALYSIS

- LARGE BORE - A TORUS COUPLING INCLUDED -  
MULTI-LEVEL RESPONSE SPECTRA

- SMALL BORE - UNCOUPLED RESPONSE SPECTRA

- BRANCH LINES

- PUMPS AND VALVES

- INTERNAL PIPING

- DYNAMIC LOADS

- POOL SWELL

- CO AND CHUGGING DRAG

- S/RV DISCHARGE DRAG

- TORUS SHELL MOTION

- LOADS ON PIPE SUPPORTS INCLUDE SUBMERGED  
STRUCTURE LOADS

## POOL TEMPERATURE EVALUATION

- DESIGN CRITERIA

- 200°F LOCAL TEMPERATURE LIMIT
- TRANSIENT CONDITIONS

- TRANSIENT ANALYSIS

- SUPPRESSION POOL MODEL
- LOCAL POOL TEMPERATURE MODEL
- SEVEN TRANSIENT EVENTS

- EVALUATION RESULTS

- MAXIMUM BULK POOL TEMPERATURE = 179°F
- MAXIMUM LOCAL POOL TEMPERATURE = 198°F

- POOL TEMPERATURE MONITORING SYSTEM

- REDUNDANT MONITORS
- CONTROL ROOM RECORDER
- SEISMIC CATEGORY I SENSORS
- ENVIRONMENTAL REQUIREMENTS

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