

# LICENSEE EVENT REPORT

CONTROL BLOCK: 1

(PLEASE PRINT OR TYPE ALL REQUIRED INFORMATION)

01 | M | N | P | I | N | 1 | 2 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | 0 | 0 | 3 | 4 | 1 | 1 | 1 | 1 | 4 | 5  
7 8 9 14 15 25 26 30 57 CAT 58  
 LICENSEE CODE      LICENSE NUMBER      LICENSE TYPE

CON'T  
01 | REPORT SOURCE | L | 6 | 0 | 5 | 0 | 0 | 0 | 2 | 8 | 2 | 7 | 0 | 4 | 2 | 3 | 8 | 2 | 8 | 0 | 5 | 0 | 7 | 8 | 2 | 9  
60 61 68 69 74 75 80  
 DOCKET NUMBER      EVENT DATE      REPORT DATE

## EVENT DESCRIPTION AND PROBABLE CONSEQUENCES 10

02 | Measured reactor coolant boron concentration is higher than the originally  
03 | predicted value by about 120 ppm at a cycle burnup of about 6200 MWD/MTU.  
04 | Not repetitive. Tech Spec 4.9 applies. No effect on public health and safety.  
05 | See attached details.  
06 |  
07 |  
08 |

09 | R | C | 11 | X | 12 | Z | 13 | Z | Z | Z | Z | Z | 14 | Z | 15 | Z | 16  
9 10 11 12 13 18 19 20  
 SYSTEM CODE      CAUSE CODE      CAUSE SUBCODE      COMPONENT CODE      COMP. SUBCODE      VALVE SUBCODE  
17 | 8 | 2 | 0 | 0 | 6 | 0 | 1 | T | 0  
21 22 23 24 26 27 28 29 30 31 32  
 LE/RO REPORT NUMBER      EVENT YEAR      SEQUENTIAL REPORT NO.      OCCURRENCE CODE      REPORT TYPE      REVISION NO.  
X | 18 | X | 19 | Z | 20 | Z | 21 | 0 | 0 | 0 | 0 | Y | 23 | N | 24 | Z | 25 | Z | 9 | 9 | 9 | 9 | 26  
33 34 35 36 37 40 41 42 43 44 45 46 47  
 ACTION TAKEN      FUTURE ACTION      EFFECT ON PLANT      SHUTDOWN METHOD      HOURS      ATTACHMENT SUBMITTED      NPR-4 FORM SUB.      PRIME COMP. SUPPLIER      COMPONENT MANUFACTURER

## CAUSE DESCRIPTION AND CORRECTIVE ACTIONS 27

10 | Apparent miscalculation of the predicted worth and/or depletion rate of  
11 | gadolinium in the fresh fuel assemblies. See attached details.  
12 |  
13 |  
14 |

15 | E | 1 | 0 | 0 | 29 | NA | 30 | B | 31 | Surveillance Test | 32  
7 8 9 10 12 13 44 45 46 80  
 FACILITY STATUS      % POWER      OTHER STATUS      METHOD OF DISCOVERY      DISCOVERY DESCRIPTION  
16 | Z | 33 | Z | 34 | NA | NA | 35 | NA | 36  
7 8 9 10 11 44 45 80  
 ACTIVITY CONTENT      RELEASED OF RELEASE      AMOUNT OF ACTIVITY      LOCATION OF RELEASE  
17 | 0 | 0 | 0 | 37 | Z | 38 | NA | 39  
7 8 9 11 12 13 80  
 PERSONNEL EXPOSURES      NUMBER      TYPE      DESCRIPTION  
18 | 0 | 0 | 0 | 40 | NA | 41  
7 8 9 11 12 80  
 PERSONNEL INJURIES      NUMBER      DESCRIPTION  
19 | Z | 42 | NA | 43  
7 8 9 11 12 80  
 LOSS OF OR DAMAGE TO FACILITY      TYPE      DESCRIPTION

20 | N | S | 8205140500 820507 PDR AD0CK 05000282 PDR  
7 8 9 10 68 69 80  
 ISSU      NRC USE ONLY

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NORTHERN STATES POWER COMPANY  
PRAIRIE ISLAND NUCLEAR GENERATING PLANT

Docket No. 50-282  
50-306

LER 82-006/OIT-0

#### Event Description

On April 23, 1982 surveillance test SP 1104, Reactivity Anomalies, was performed. This surveillance compares the measured RCS full power equilibrium boron concentration as a function of burnup to the normalized predicted boron concentration. The comparison resulted in a deviation between predicted and measured RCS boron concentration which, within the limits of measurement error, reached the equivalent of 1%  $\Delta k/k$ . The disagreement on April 23 was 114ppm at a burnup of 6221 MWD/MTU or the equivalence of 0.98%  $\Delta k/k$  or 3ppm from the limit. The disagreement has been determined to be a modelling concern and not a deviation in core performance.

#### Cause Description and Corrective Actions

Three apparent causes were considered. These are: 1. a miscalculation of burnup; 2. a miscalculation of the predicted gadolinium worth and/or depletion rate, and; 3. RCS soluble boron with a reduced B-10 abundance. Further investigation has eliminated possibilities 1 and 3 as major contributors to the disagreement. Additional independent analysis by both NSP\* and the fuel vendor definitely indicate that the disagreement is related to the analytical description of the 4 w/o gadolinia assemblies.

The predicted RCS boron concentration as a function of burnup was supplied by Exxon in their Unit 1-Cycle 7 Startup and Operations Report. NSP also calculates the predicted boron concentration vs burnup; however, the Exxon curve is used for the comparisons in SP 1104. (Note: By comparison to NSP's original normalized predictions the deviation is less than half.) The predicted Exxon curve was normalized to measured data at about 10% of cycle burnup as per T.S. 4.9. This normalization point was at 1339 MWD/MTU and a measured RCS boron concentration of 896ppm. The predicted boron concentration at this time is 914ppm for a correction of -18ppm. Subsequent comparison of normalized predicted vs measured boron concentration (Figure 1) has shown a gradual increase in the deviation between measured and predicted up to a burnup of approximately 6000 MWD/MTU where the disagreement stopped diverging and leveled off at about 1%  $\Delta k/k$ . The most recent measurements (up to May 5, 1982) indicate the disagreement has started to converge and is presently at 0.9%  $\Delta k/k$  corresponding to a burnup of approximately 6630 MWD/MTU.

Burnup is calculated using the FOLLOW code where the hourly power history, as recorded by the Nuclear Instrumentation System (NIS), and core MTU are used as input. The FOLLOW output burnup calculation is checked by comparing the unit capacity factor based on monthly burnup to the monthly electrical capacity factor. The NIS is calibrated daily using a secondary system calorimetric. All primary, secondary and electrical plant parameters show the NIS is indicating the correct power level. Based on this evidence a miscalculation of burnup has been dismissed as a cause of the boron disagreement.

\* See NSP Topicals (NSPNAD-8101P and NSPNAD-8102P) submitted 2/12/82 for review.

May 7, 1982  
Attachment (Page 2 of 5)

The RCS boron concentration is measured approximately daily by titration of a sample of the RCS coolant. The measurement uncertainty is  $< 1\%$  of the measured value. Only full power equilibrium xenon data points are used in the comparisons. Soluble boron with a reduced B-10 abundance was considered as a contributor to the disagreement but was dismissed because: 1. Chemistry data on lithium (a by-product of B-10, neutron reactions) removal from the RCS could account for less than 30% of the disagreement (using very conservative calculations) and 2. The Unit 2 comparison of measured and predicted RCS boron concentration agree very well (Unit 1 and 2 share boron reprocessing equipment and much intermixing of boric acid supplies exists). Concentrated samples of the Unit 1 coolant have been prepared and sent offsite for an isotopic analysis of boron. Results of this analysis are not yet available.

Analytical analysis of the disagreement by Exxon and NSP has shown that the deviation can be partially in Exxon's case or more closely in NSP's analysis, accounted for by adjustments in the modeling of the 4 w/o gadolinia assemblies.

Both analyses indicate the disagreement should start to converge at about 6200 MWD/MTU and disappear by the end of the cycle.

Power distribution measurement using the incore instrumentation system results in good agreement with predictions with margin to Tech Spec limits. No axial shifts in the power distribution have been noted. The RCS equilibrium coolant activity has remained stable since the first month of the cycle.

Surveillance frequency of the predicted and measured boron concentration measurements and power distribution measurements has been increased until the disagreement starts to converge. Analyses by Exxon and NSP have resulted in improvements in gadolinia modeling. Continuing analysis is being performed to monitor the disagreement. Reviews of the disagreement indicate no safety related problems and demonstrate adequate shutdown margin.

FIGURE 1

## PRAIRIE ISLAND UNIT 1 CYCLE 7

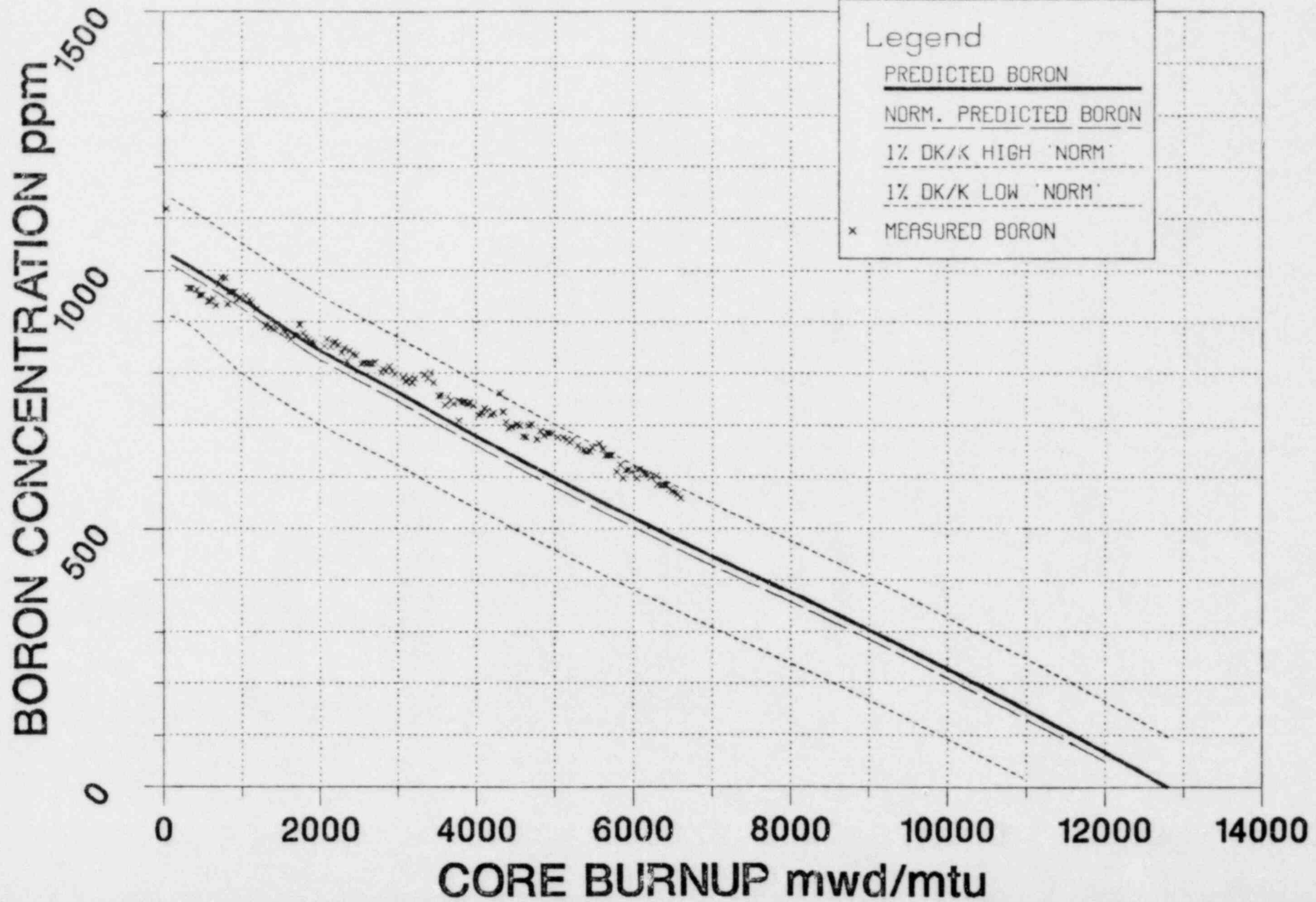


Figure 2

M	L	K	J	I	H	G	F	E	D	C	B	A	
				9 I08	G4 G10	9 I01							1
		9 I14	H4 G29	9** I32	C3 H09	9** I25	F4 G14	9 I15					2
	9 I12	9* I36	J2 H14	H2 H40	G13 H23	F2 H33	D2 H15	9* I33	9 I09				3
9 I13	9* I37	D10 G20	J3 G37	I2 H31	G11 G33	E2 H32	D3 G19	J10 G24	9* I38	9 I16			4
J6 G13	L4 H13	K4 G25	M6 H07	H5 G05	9** I21	F5 G18	A6 H02	C4 G38	B4 H16	D6 G30			5
9 I07	9** I31	L6 H39	L5 H30	I6 G17	F13 H04	G6 G09	H13 H05	E6 G26	B5 H25	B6 H34	9** I26	9 I02	6
J7 G01	K3 H12	A7 H22	C7 G02	9** I24	H7 G36	E10 F34	F7 G34	9** I22	K7 G03	M7 H24	C11 H10	D7 G11	7
9 I06	9** I30	L8 H38	L9 H29	I8 G28	F1 H01	G8 G04	H1 H08	E8 G06	B9 H26	B8 H35	9** I27	9 I03	8
	J8 G32	L10 H20	K10 G40	M8 H06	H9 G23	9** I23	F9 G27	A8 H03	C10 G07	B10 H17	D8 G15		9
	9 I20	9* I40	D4 G22	J11 G35	I12 H28	G3 G12	E12 H27	D11 G39	J4 G21	9* I39	9 I17		10
		9 I11	9* I35	J12 H19	H12 H37	G1 H21	F12 H36	D12 H18	9* I34	9 I10			11
			9 I19	H10 G16	9** I29	K11 H11	9** I28	F10 G31	9 I18				12
				9 I05	G10 G08	9 I04							13

- \* 8 pins of 4 w/o gadolinia per assembly  
\*\* 12 pins of 4 w/o gadolinia per assembly

	Batch Id (new fuel) or core location in Cycle 6
	Assembly Serial number

Figure 4.1 Prairie Island Unit 1, Cycle 7  
Loading Pattern Startup and Operations



TABLE 1 Prairie Island Unit 1 Cycle 7 Fuel Assembly Design Parameters

	Batch					
	5	7	8	9	9*	9**
Enrichment, wt % U-235	3.30	3.40	3.47	3.56	3.52	3.50
TOPROD Fuel Assemblies						
Central 11 Feet, wt % U-235	----	----	----	3.82	3.82	3.82
UO <sub>2</sub> -Gd <sub>2</sub> O <sub>3</sub> , wt % U-235	----	----	----	----	2.90	2.90
Upper and Lower 6 inches, wt % U-235	----	----	----	.71	.71	.71
Number of Assemblies	1	40	40	20	8	12
Pellet Density, % TD	94.5	94.0	94.0	94.0	94.0	94.0
Pellet to Clad Diametrical Gap, mil	7.5	7.5	7.5	7.5	7.5	7.5
Fuel Stack Height, inches	144.0	144.0	144.0	144.0	144.0	144.0
Batch Average Burnup at BOC7, MWD/MT	27,434	24,680	7,604	0	0	0

\* Fuel with 8 pins of 4 w/o gadolinia per assembly

\*\* Fuel with 12 pins of 4 w/o gadolinia per assembly