

Y1003J01A25
CLASS I
AUGUST 1981

**SUPPLEMENTAL RELOAD LICENSING
SUBMITTAL FOR JAMES A.
FITZPATRICK NUCLEAR POWER PLANT
RELOAD 4**

8111230633 811118
PDR ADOCK 05000333
P PDR

GENERAL  ELECTRIC

Y1003J01A25
Revision 0
Class I
August 1981

SUPPLEMENTAL RELOAD LICENSING SUBMITTAL
FOR
JAMES A. FITZPATRICK NUCLEAR POWER PLANT
RELOAD 4

Prepared: J. D. Leaser
J. D. Leaser

Verified: J. S. Charnley
J. S. Charnley

Approved: R. E. Engel
R. E. Engel, Manager
Reload Fuel Licensing

NUCLEAR POWER SYSTEMS DIVISION • GENERAL ELECTRIC COMPANY
SAN JOSE, CALIFORNIA 95125

GENERAL  ELECTRIC

IMPORTANT NOTICE REGARDING
CONTENTS OF THIS REPORT
PLEASE READ CAREFULLY

This report was prepared by General Electric solely for The Power Authority of the State of New York (The Authority) for The Authority's use with the U.S. Nuclear Regulatory Commission (USNRC) for amending The Authority's operating license of the James A. FitzPatrick Nuclear Power Plant. The information contained in this report is believed by General Electric to be an accurate and true representation of the facts known, obtained or provided to General Electric at the time this report was prepared.

The only undertakings of the General Electric Company respecting information in this document are contained in the contract between The Authority and General Electric Company for nuclear fuel and related services for the nuclear system for The James A. FitzPatrick Nuclear Power Plant, dated June 12, 1970, and nothing contained in this document shall be construed as changing said contract. The use of this information except as defined by said contract, or for any purpose other than that for which it is intended, is not authorized; and with respect to any such unauthorized use, neither General Electric Company nor any of the contributors to this document makes any representation or warranty (express or implied) as to the completeness, accuracy or usefulness of the information contained in this document or that such use of such information may not infringe privately owned rights; nor do they assume any responsibility for liability or damage of any kind which may result from such use of such information.

1. PLANT UNIQUE ITEMS (1.0)*

Transient Analysis Initial Conditions: Appendix A

2. RELOAD FUEL BUNDLES (1.0, 2.7, 3.3.1 and 4.0)

	<u>Fuel Designation</u>	<u>Cycle Loaded</u>	<u>Number</u>	<u>Number Drilled</u>
Irradiated	8DB274L	2	20	20
	8DB274H	2	56	56
	8DRB265L	3	36	36
	8DRB283	3	100	100
	P8DRB265L	4	24	24
	P8DRB283	4	136	136
New	P8DRB284H	5	128	128
	P8DRB299	5	<u>60</u>	<u>60</u>
Total			560	560

3. REFERENCE CORE LOADING PATTERN (3.3.1)

Nominal previous cycle core average exposure at end of cycle: 16.7 GWd/T

Minimum previous cycle core average exposure at end of cycle
from cold shutdown considerations: 16.4 GWd/T

Assumed reload cycle core average exposure at end of cycle: 17.2 GWd/T

Core loading pattern: Figure 1

*() refers to areas of discussion in "General Electric Boiling Water Reactor Generic Reload Fuel Application," NEDE-24011-P-A-1 and NEDO-24011-A-1, July 1979, as revised by amendments 2-10.

4. CALCULATED CORE EFFECTIVE MULTIPLICATION AND CONTROL SYSTEM WORTH - NO VOIDS, 20°C (3.3.2.1.1 and 3.3.2.1.2)

BOC k_{eff}	
Uncontrolled	1.116
Fully Controlled	0.957
Strongest Control Rod Out	0.987
R, Maximum Increase in Cold Core Reactivity with Exposure Into Cycle, Δk	0.000

5. STANDBY LIQUID CONTROL SYSTEM SHUTDOWN CAPABILITY (3.3.2.1.3)

<u>ppm</u>	<u>Shutdown Margin (Δk)</u> <u>(20°C, Xenon Free)</u>
600	0.03

6. RELOAD UNIQUE TRANSIENT ANALYSIS INPUTS (3.3.2.1.5 and 5.2) ⁽¹⁾

	<u>EOC</u>	<u>EOC-1</u> <u>GWd/T</u>
Void Coefficient N/A* (c/% Rg)	-8.8/-11.0	-9.6/-12.0
Void Fraction (%)	41.7	41.7
Doppler Coefficient N/A (c/°F)	-0.23/-0.22	-0.23/-0.22
Average Fuel Temperature (°F)	1343	1343
Scram Worth N/A (%) ⁽²⁾		
Scram Reactivity vs Time ⁽²⁾		

*N = Nuclear Input Data

A = Used in Transient Analysis

(1) Applies to Inadvertent Startup of HPCI Pump Event Only

(2) Generic, exposure independent values are used as given in "General Electric Boiling Water Reactor Generic Reload Fuel Application," NEDE-24011-P-A-1, Amendment 10, April 1981.

7. RELOAD UNIQUE GETAB TRANSIENT ANALYSIS INITIAL CONDITION PARAMETERS (5.2)

Fuel Design	Exposure (GWd/T)	Peaking Factors (Local, Radial, Axial)	R-Factor	Bundle Power (MWt)	Bundle Flow (10 ³ lb/hr)	Initial MCPR
8x8	EOC	1.22, 1.35, 1.40	1.10	5.75	115	1.29
	EOC-1	1.22, 1.39, 1.40	1.10	5.92	114	1.25
8x8R	EOC	1.20, 1.50, 1.40	1.05	6.40	115	1.29
	EOC-1	1.20, 1.54, 1.40	1.05	6.58	114	1.25
P8x8R	EOC	1.20, 1.48, 1.40	1.05	6.29	116	1.31
	EOC-1	1.20, 1.52, 1.40	1.05	6.46	115	1.28

8. SELECTED MARGIN IMPROVEMENT OPTIONS (5.2.2)

Transient Recategorization:	No
Recirculation Pump Trip:	No
Rod Withdrawal Limiter:	No
Thermal Power Monitor:	Yes
Measured Scram Time:	No
Exposure Dependent Limits:	Yes
Exposures Analyzed (GWd/T):	EOC
	EOC-1

9. CORE-WIDE TRANSIENT ANALYSIS RESULTS (5.2.1)

<u>Transient</u>	<u>Exposure Range</u> (Gwd/T)	ϕ (% NBR)	Q/A (%)	Δ CPR 8x8/8x8R	P8x8R	<u>Figure</u>
Load Rejection	EOC	653	125	0.22	0.24	3a
without Bypass	EOC-1	609	122	0.18	0.21	3b
Inadvertent Start of HPCI Pump	BOC to EOC	128	120	0.14	0.15	4
Feedwater	EOC	362	122	0.17	0.19	5a
Controller Failure	EOC-1	311	120	0.15	0.16	5b

10. LOCAL ROD WITHDRAWAL ERROR (WITH LIMITING INSTRUMENT FAILURE)
TRANSIENT SUMMARY (5.2.1)

Limiting Rod Pattern:

Figure 6

Includes 2.2% Power Spiking Penalty: Yes

Rod Block Reading*	Rod Position (Feet Withdrawn)	Δ CPR	MLHGR (kW/ft)
		8x8**8x8R/P8x8R	8x8**8x8R/P8x8R
104	3.0	0.12	16.1
105	3.5	0.15	16.5
106	4.0	0.17	16.8
107	5.0	0.20	16.9
108*	6.5	0.24	16.9
109	7.0	0.24	16.9
110	8.0	0.25	16.9

11. CYCLE MCPR VALUES (5.2)

Exposure Range (GWd/t)	Pressurization Events	Option A	Option B
BOC to EOC-1		8x8/8x8R/P8x8R	8x8/8x8R/P8x8R
	Load Rejection w/o Bypass	0.23/0.23/0.27	0.04/0.04/0.06
	Feedwater Controller Failure	0.19/0.20/0.21	0.13/0.14/0.15
EOC-1 to EOC			
	Load Rejection w/o Bypass	0.28/0.28/0.30	0.16/0.16/0.18
	Feedwater Controller Failure	0.22/0.22/0.25	0.16/0.16/0.18
BOC to EOC	Non-Pressurization Events	8x8/8x8R/P3x8R	
	Inadvertent PCI Pump Start	0.14/0.14/0.15	
	Rotated Bundle Error	--/--/0.13	
	Rod Withdrawal Error	-- 0.24/0.24	

*Indicates set point selected.

**Not Limiting

12. OVERPRESSURIZATION ANALYSIS SUMMARY (5.3)

<u>Transient</u>	<u>P_{sl}</u> <u>(psig)</u>	<u>P_v</u> <u>(psig)</u>	<u>Plant</u> <u>Response</u>
MSIV Closure (Flux Scram)	1236	1275	Figure 7

13. STABILITY ANALYSIS RESULTS (5.4)

Rod Line Analyzed:	Extrapolated Rod Block
Decay Ratio:	Figure 8
Reactor Core Stability Decay Ratio, x_2/x_0 :	0.87
Channel Hydrodynamic Performance Decay Ratio, x_2/x_0	
8x8 Channel:	0.37
8x8R/P8x8R Channel:	0.30

14. ROTATED BUNDLE ERROR RESULTS (5.4)

Variable Water Gap Misoriented Bundle Analysis:	Yes
Includes 2.2% Power Spiking Penalty:	Yes

<u>Initial</u> <u>MCPR</u>	<u>Resulting</u> <u>MCPR</u>	<u>Resulting</u> <u>LHGR (kW/ft)</u>
1.18	1.07	15.32

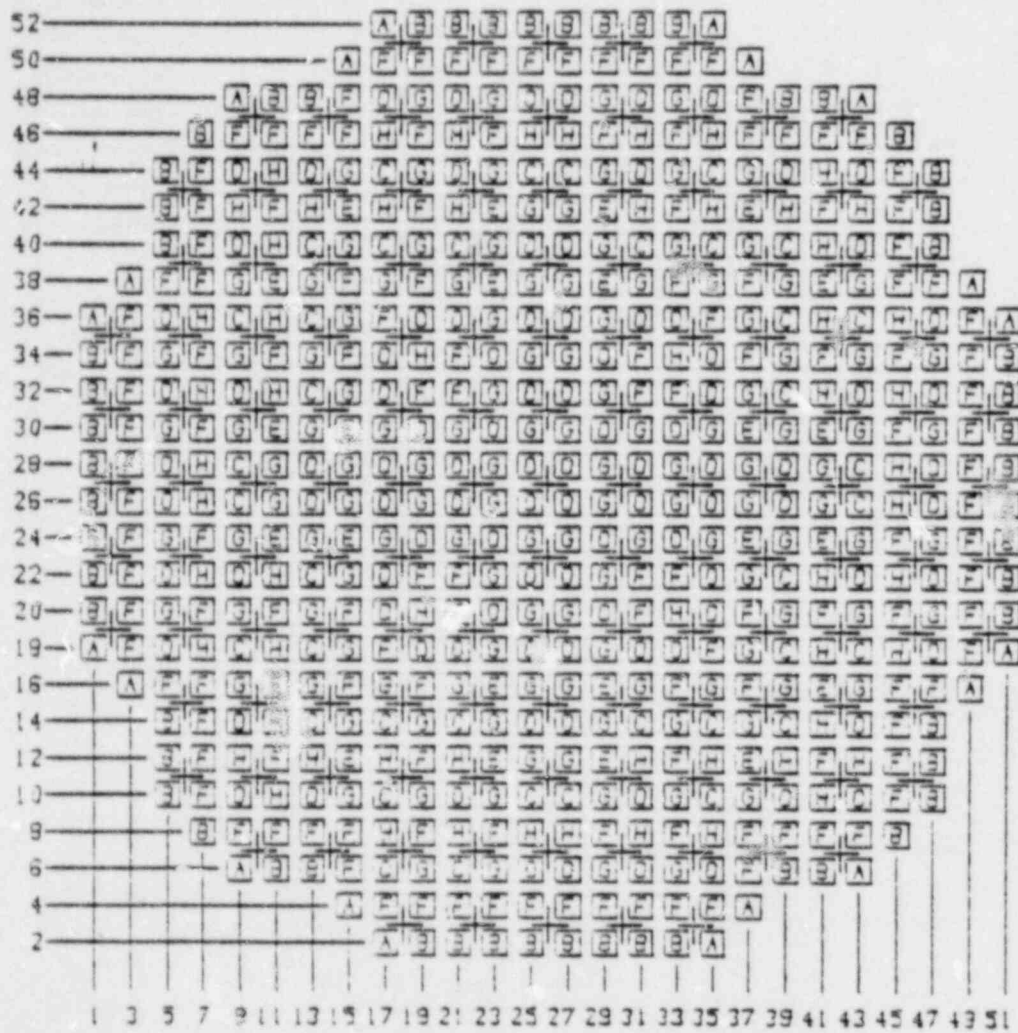
15. CONTROL ROD DROP ANALYSIS RESULTS (5.5.1)

Bounding Analysis Results:

Doppler Reactivity Coefficient:	Figure 9
Accident Reactivity Shape Functions:	Figures 10 and 11
Scram Reactivity Functions:	Figures 12 and 13

16. LOSS-OF-COOLANT ACCIDENT RESULTS, NEW FUEL (5.5.2)

See "Loss-of-Coolant Accident Analysis Report for James A. FitzPatrick Nuclear Power Plant (Lead Plant)," July 1977, NEDO-21662, as amended.

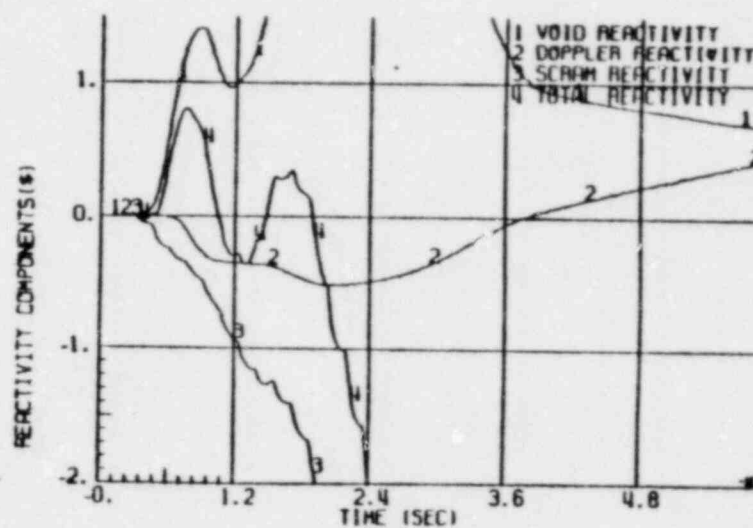
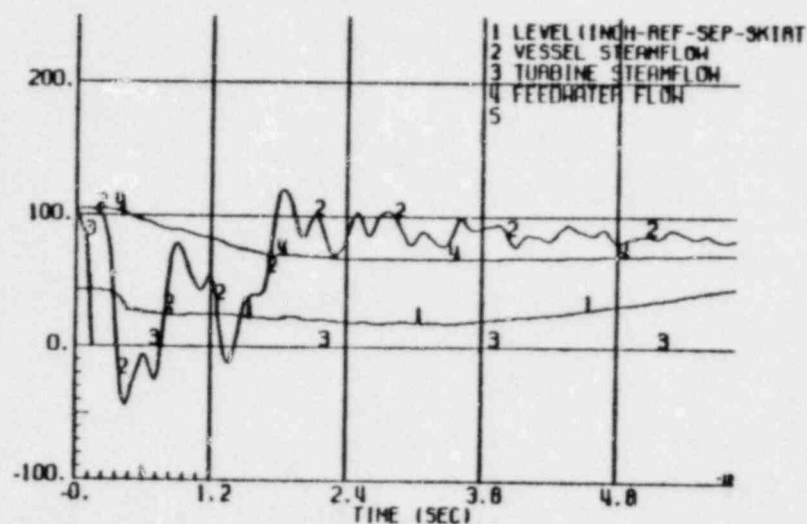
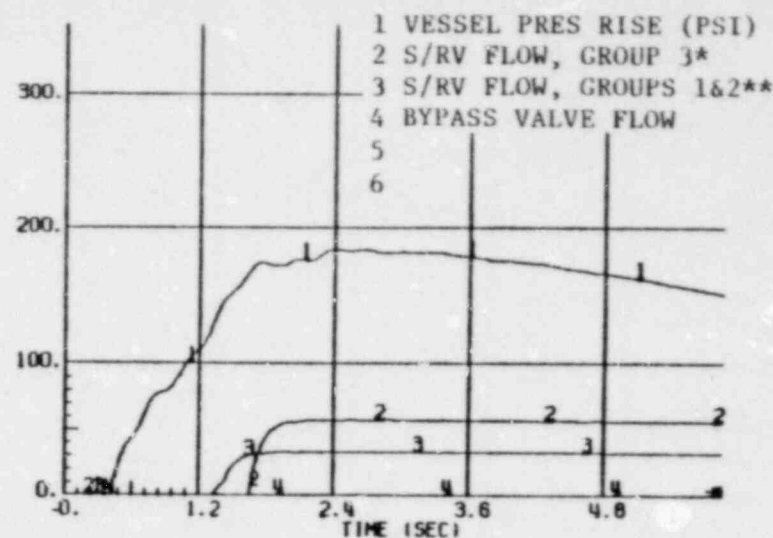
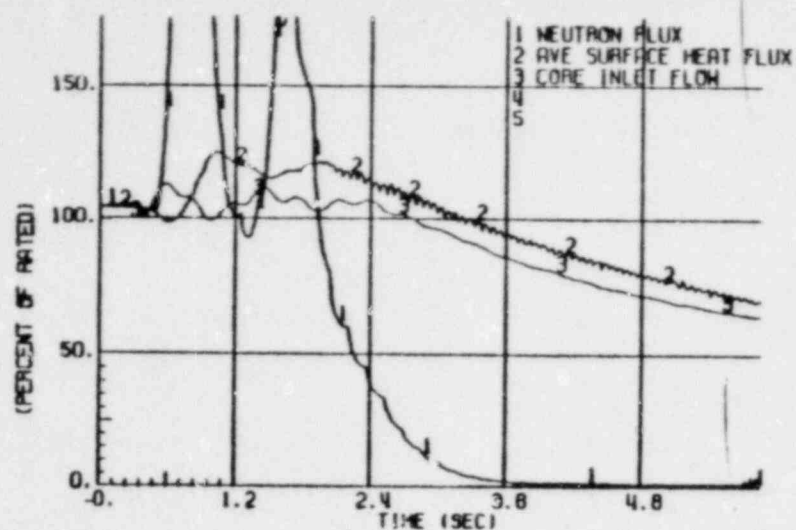


FUEL TYPE	
A = 8DB274L	E = P8DRB265L
B = 8DB274H	F = P8DRB283
C = 8DRB265L	G = P8DRB284H
D = 8DRB283	H = P8DRB299

Figure 1. Reference Core Loading Pattern

DELETED
See Section 6

Figure 2. Scram Reactivity and Control Rod
Drive Specifications



*Group 3 S/RV Set Point = 1140 psig +1%
 **Group 1 S/RV Set Point = 1090 psig +1%
 Group 2 S/RV Set Point = 1105 psig +1%

Figure 3a. Plant Response to Generator Load Rejection Without Bypass, EOC 5

11093J01A25

Rev. 0

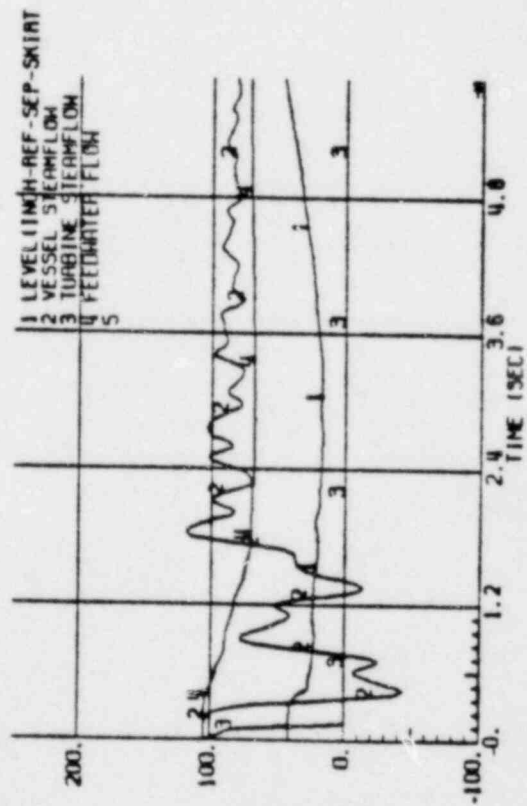
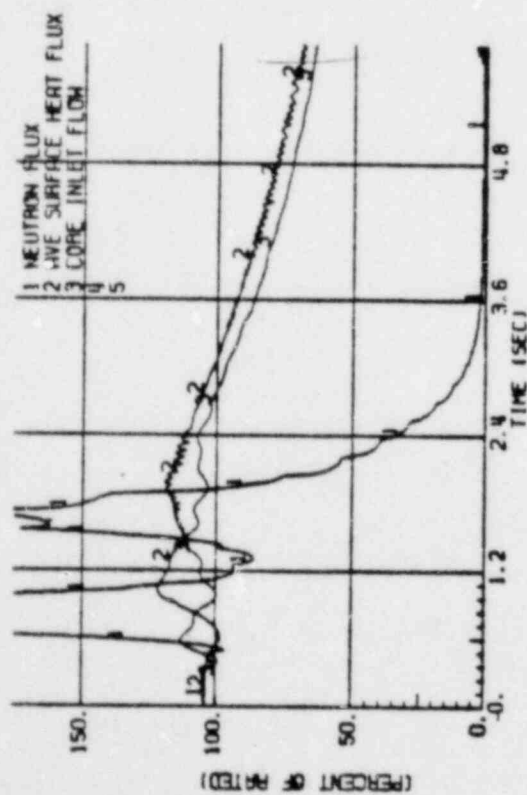
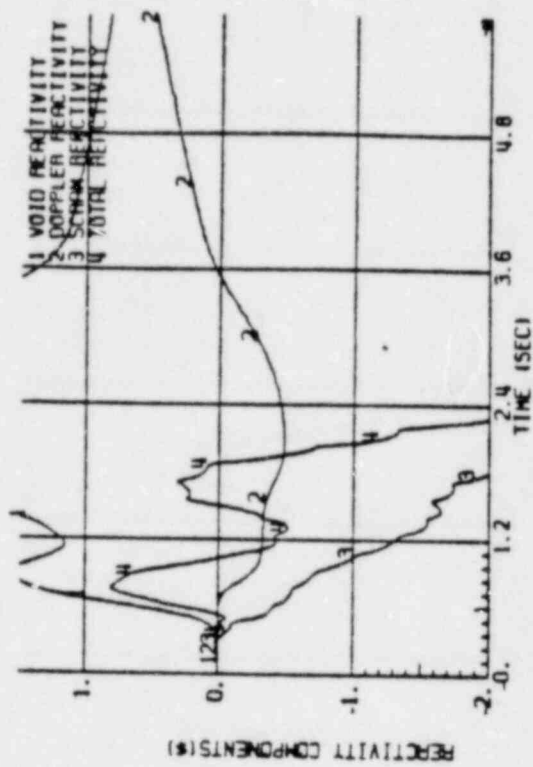
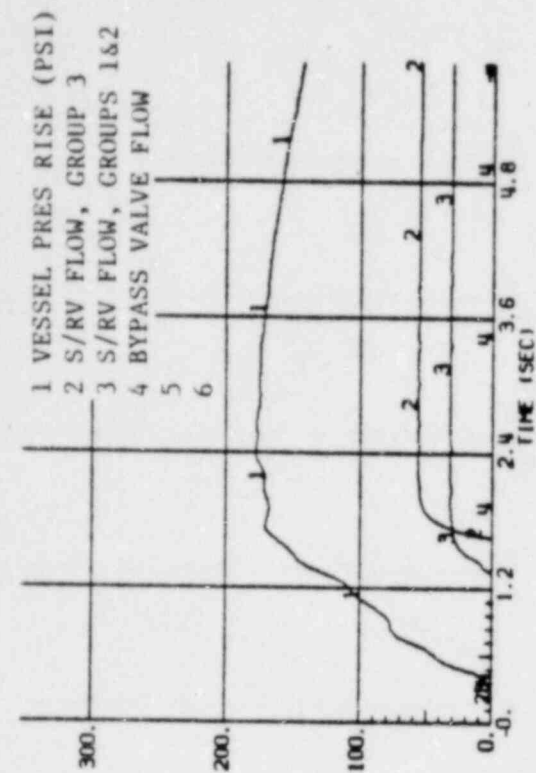


Figure 3b. Plant Response to Generator Load Rejection Without Bypass, EOC 5-1000 MWd/t

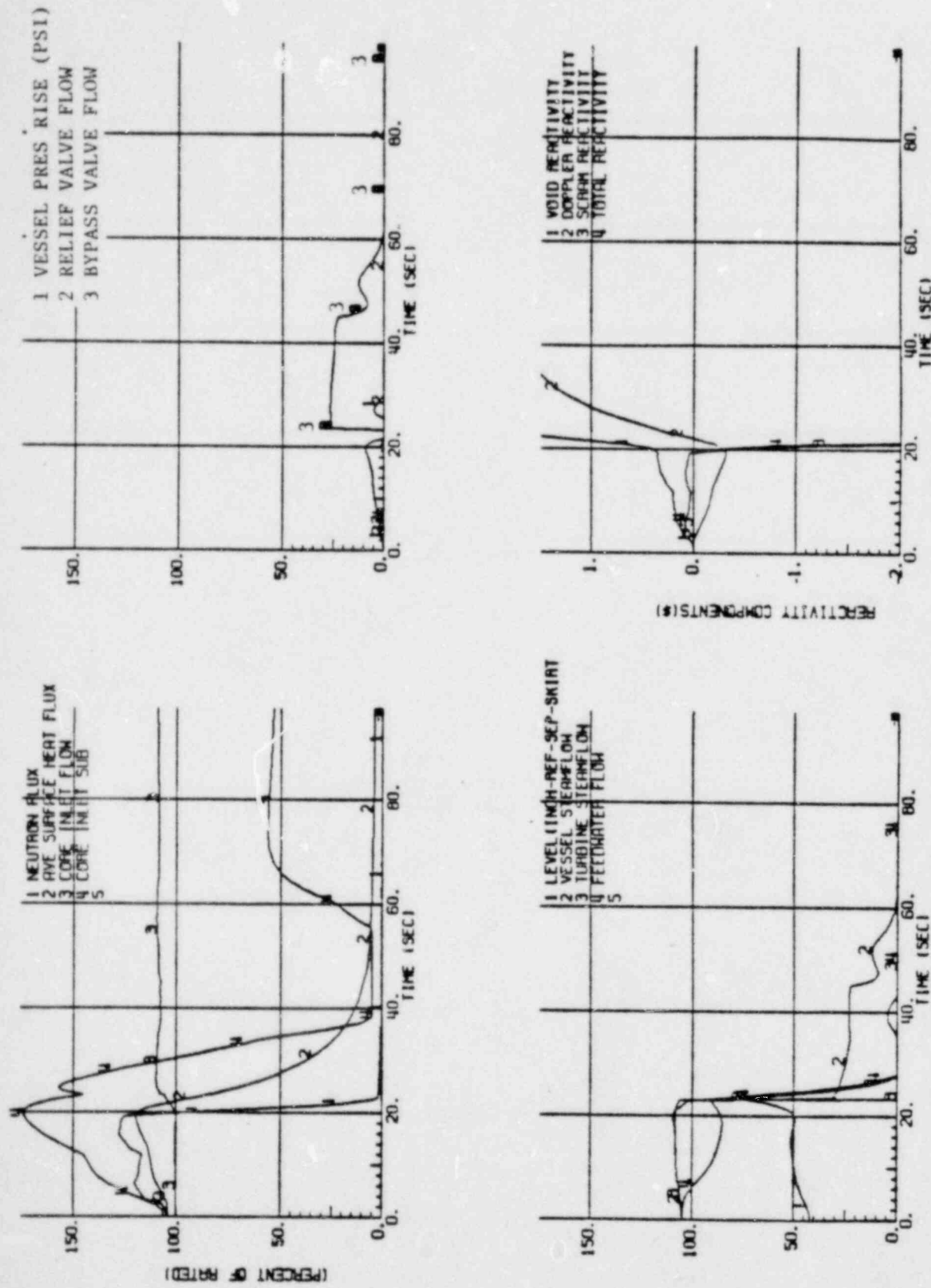


Figure 4. Plant Response to Inadvertent Start of HPCI Pump

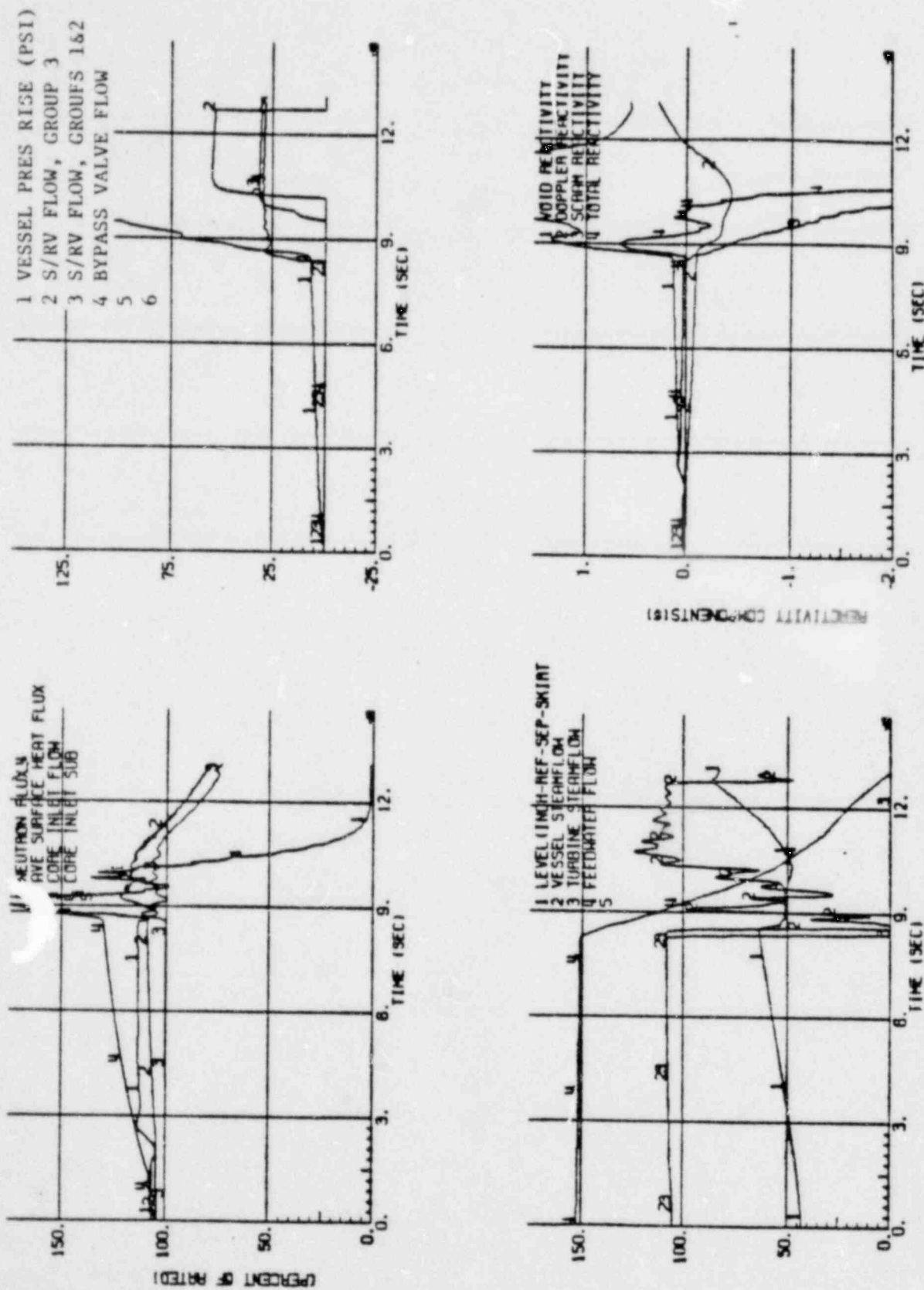


Figure 5a. Plant Response to Feedwater Controller Failure, EOC 5

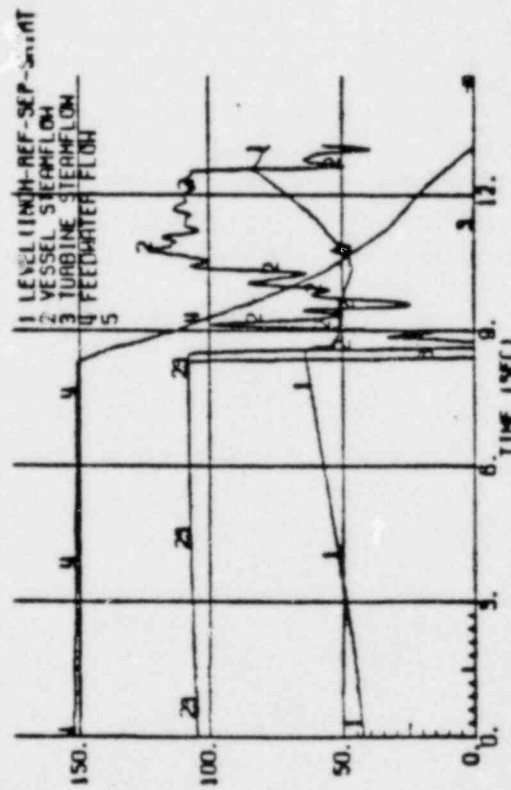
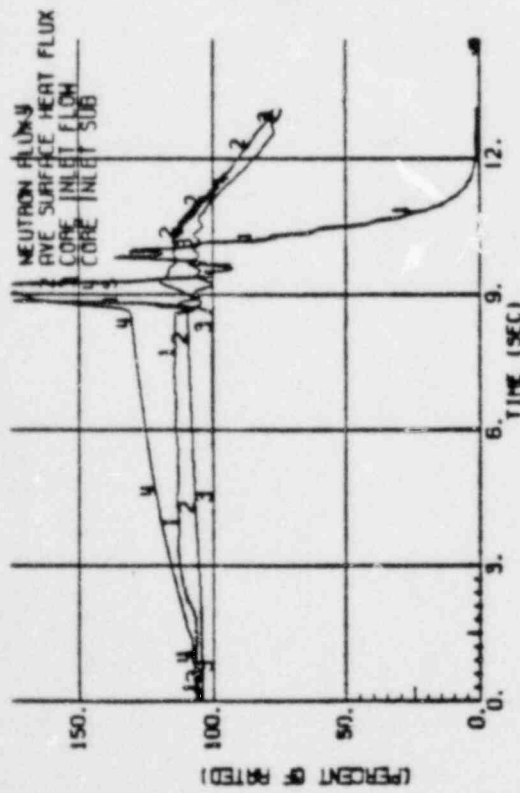
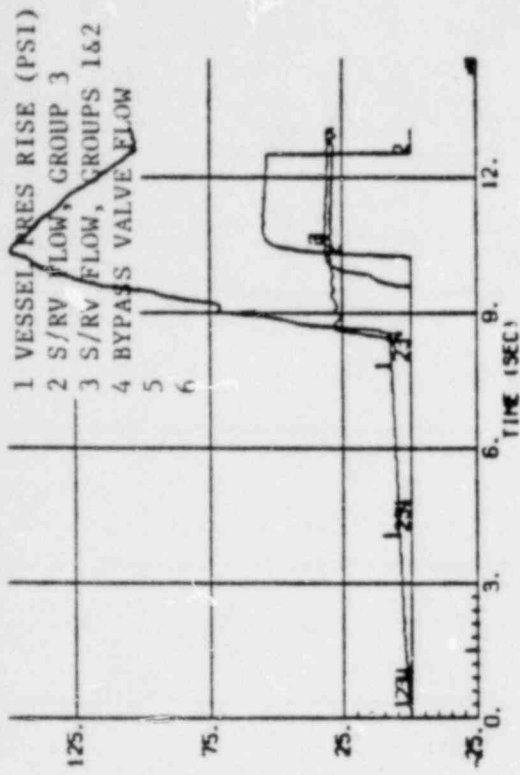


Figure 5b. Plant Response to Feedwater Controller Failure, EOC 5-1000 MWd/t

	02	06	10	14	18	22	26
51							
47				30		12	
43					12		24
39		30		10		10	
35			12		32		32
31		12		10		0	
27			24		32		32

- Notes: 1. Rod Pattern Is 1/4 Core Mirror Symmetric, Upper Left Quadrant Shown on Map.
2. Numbers Indicate Number of Notches Withdrawn out of 48. Blank Is a Withdrawn Rod.
3. Error Rod Is Rod (22,31).

Figure 6. Limiting RWE Rod Pattern

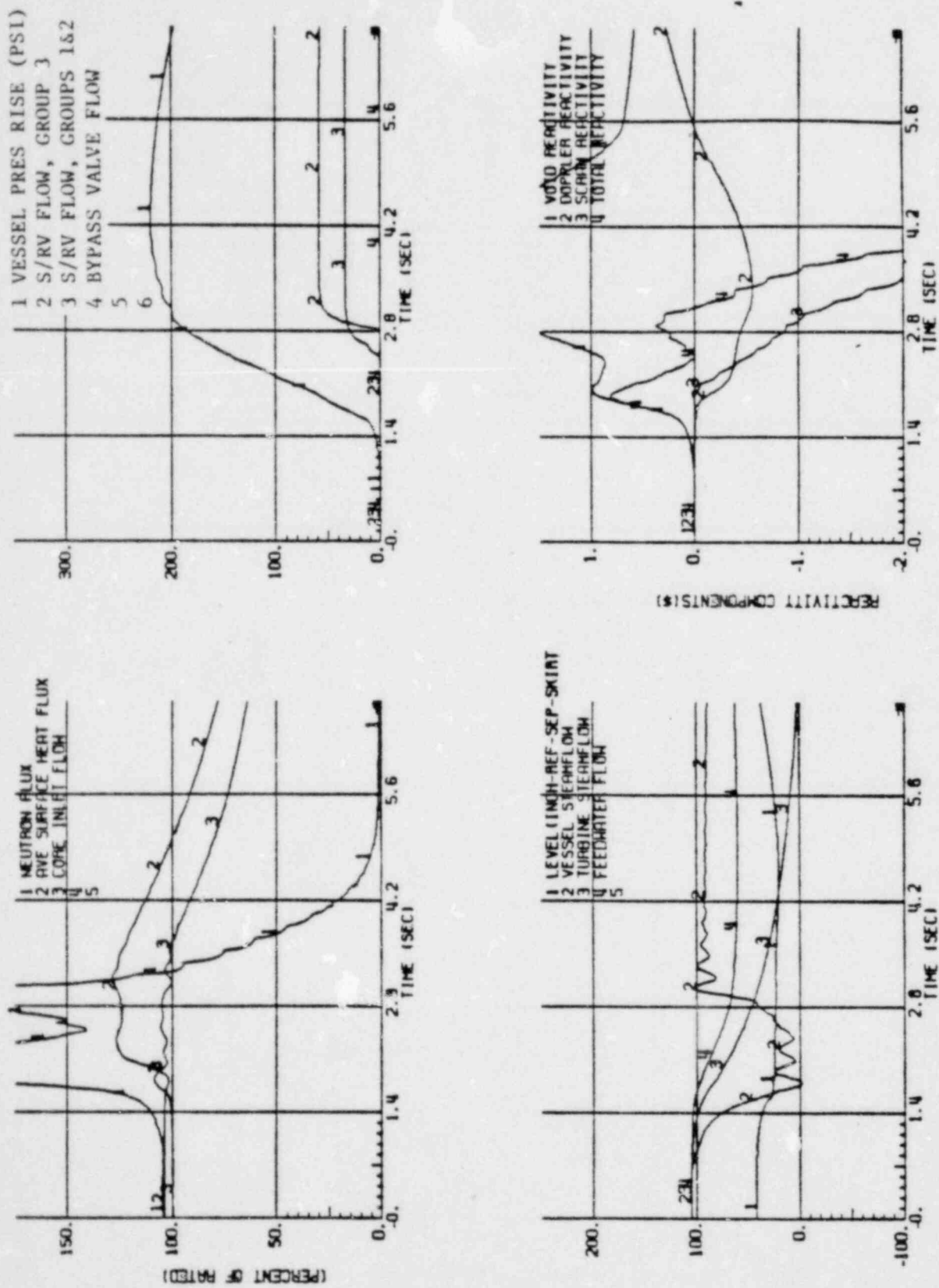


Figure 7. Plant Response to MSIV Closure (Flux Scram)

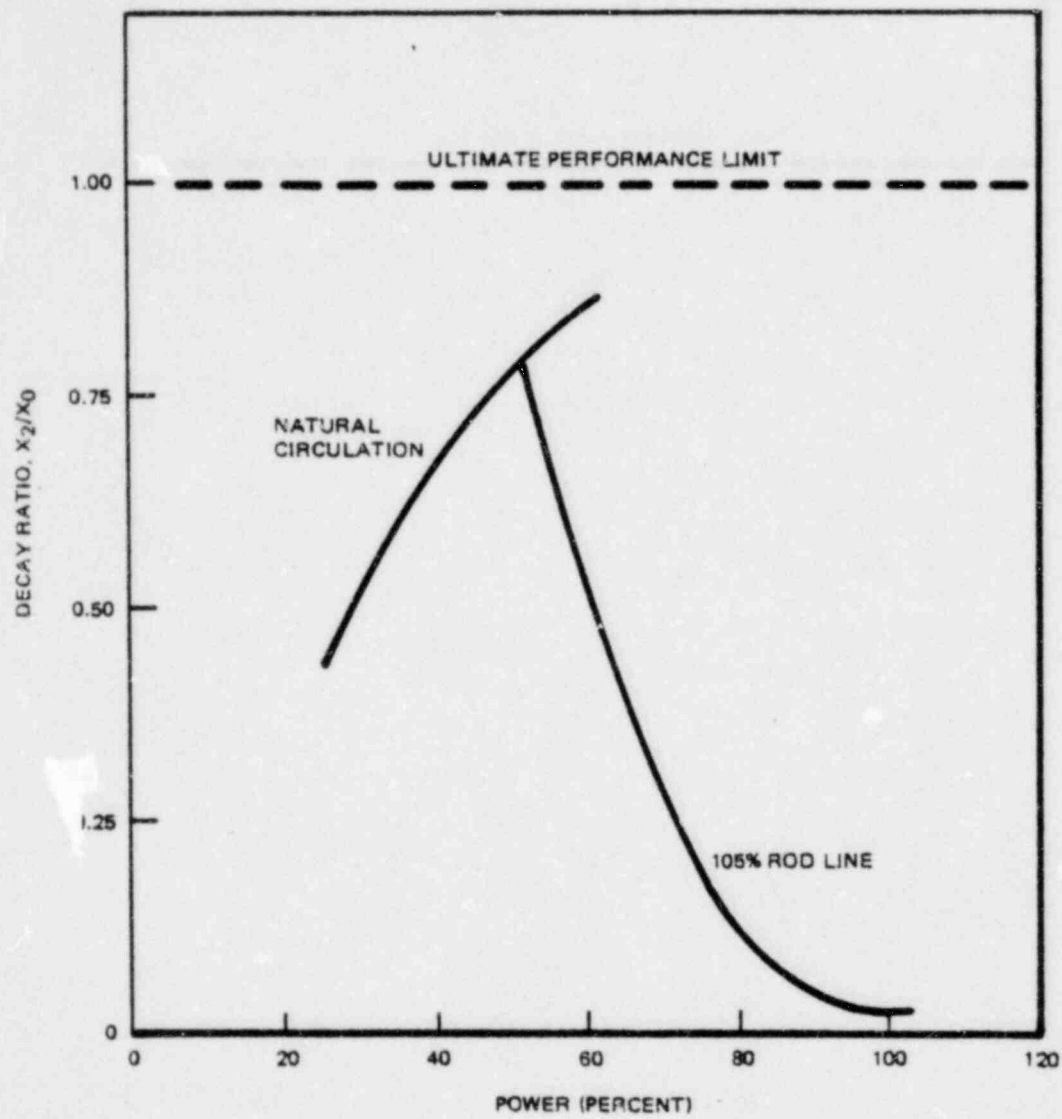


Figure 8. Reactor Core Decay Ratio versus Power

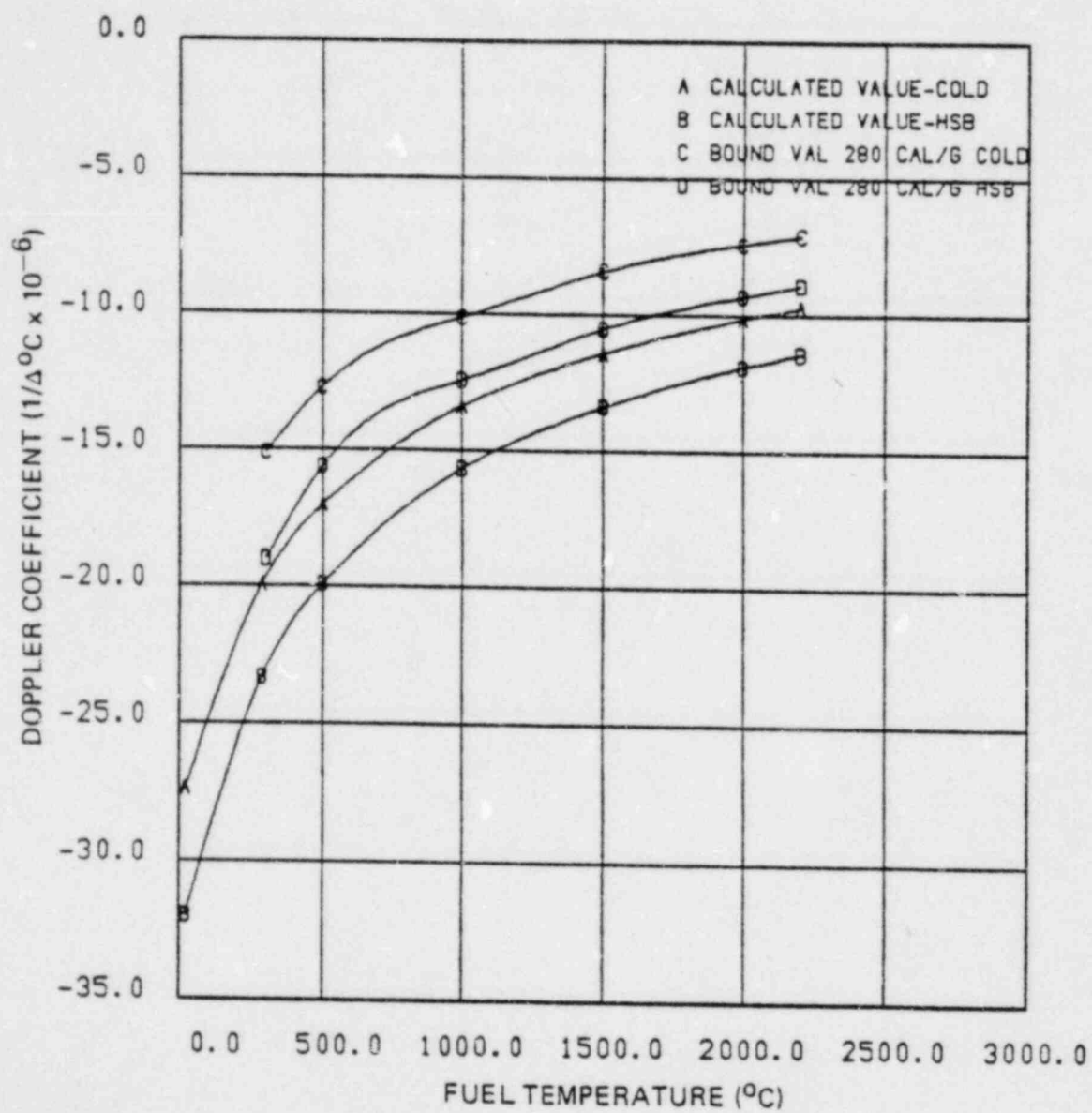


Figure 9. Doppler Reactivity Coefficient Comparison for RDA

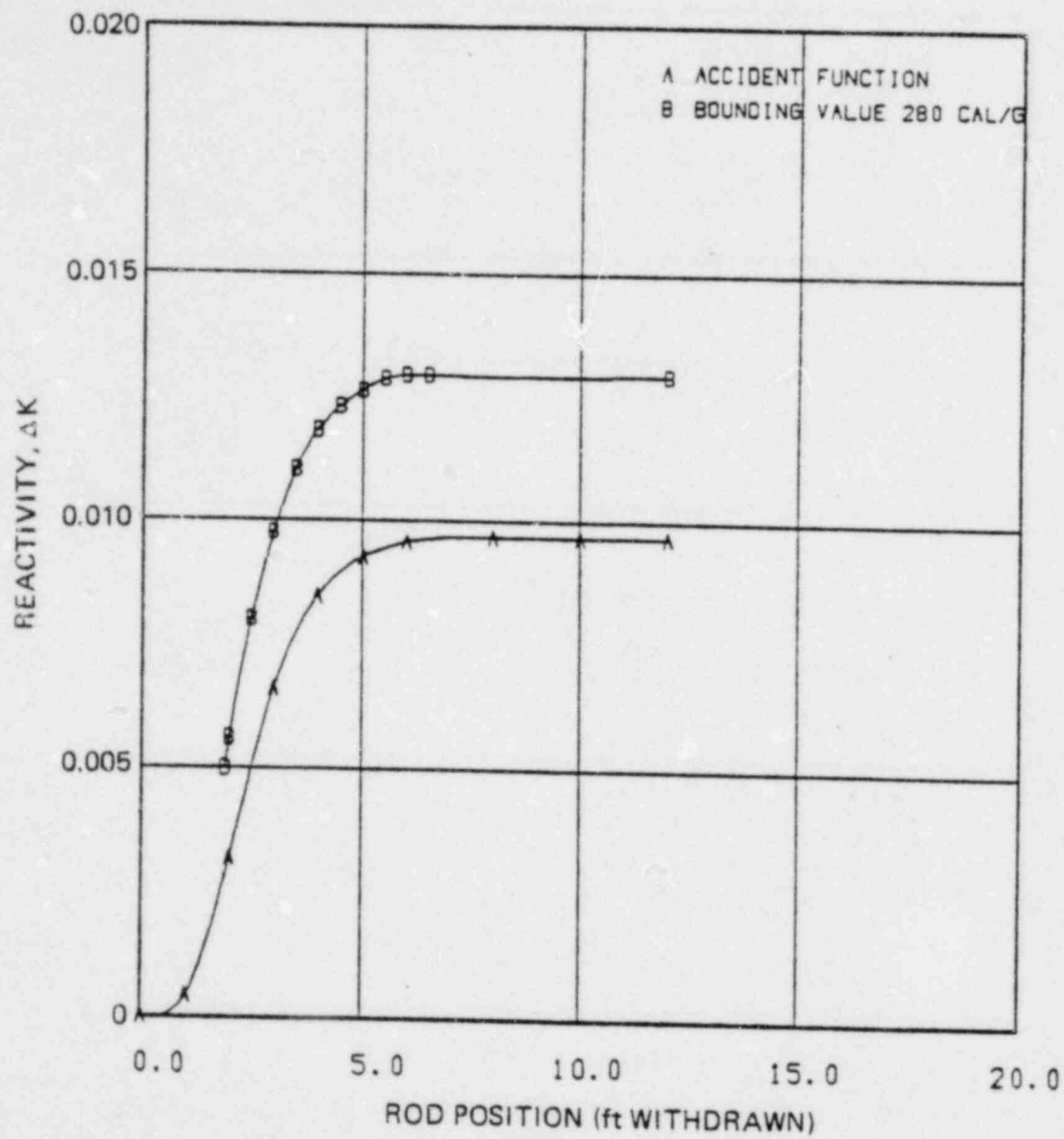


Figure 10. RDA Reactivity Shape Function, Cold

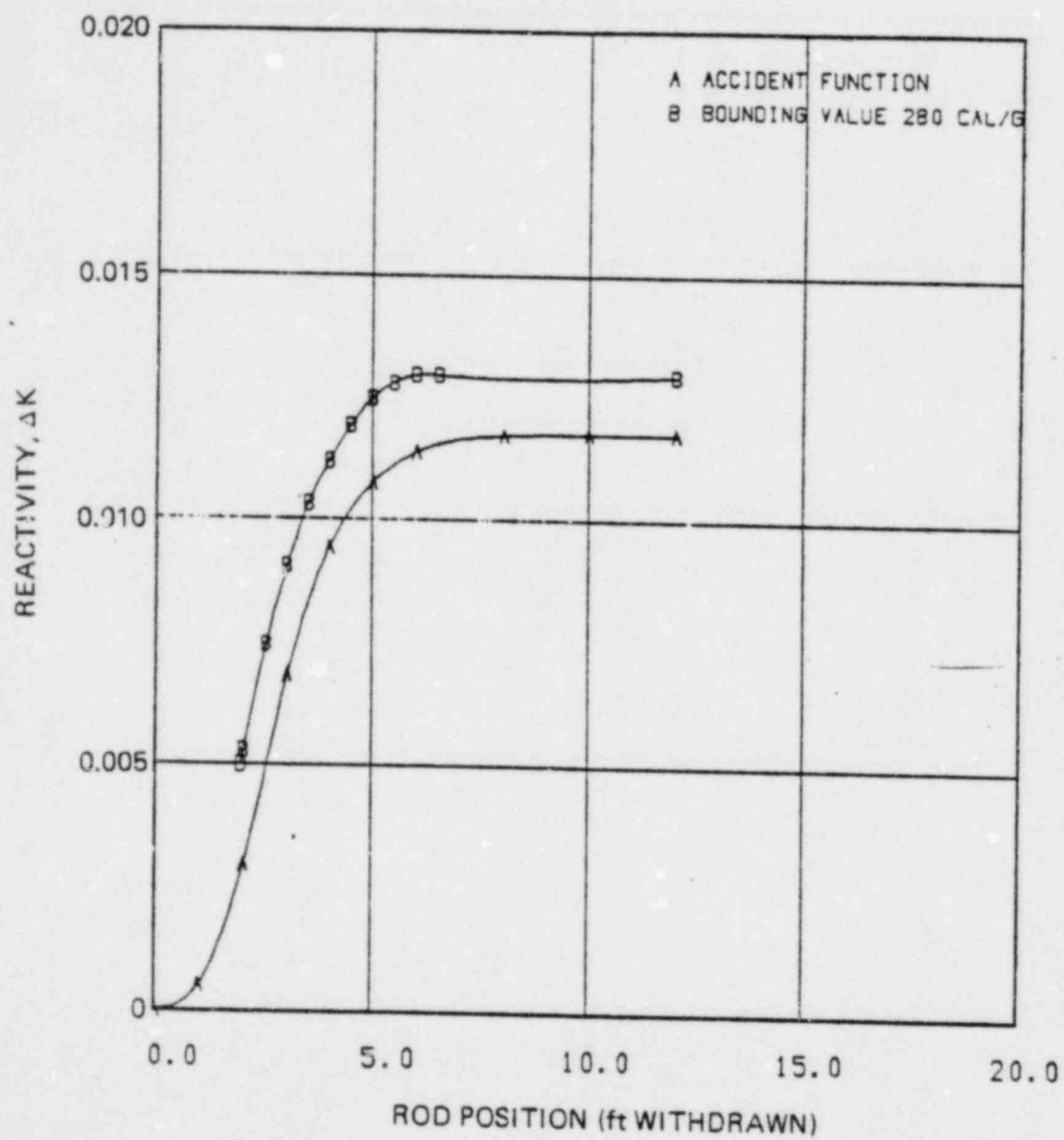


Figure 11. RDA Reactivity Shape Function, Hot Standby

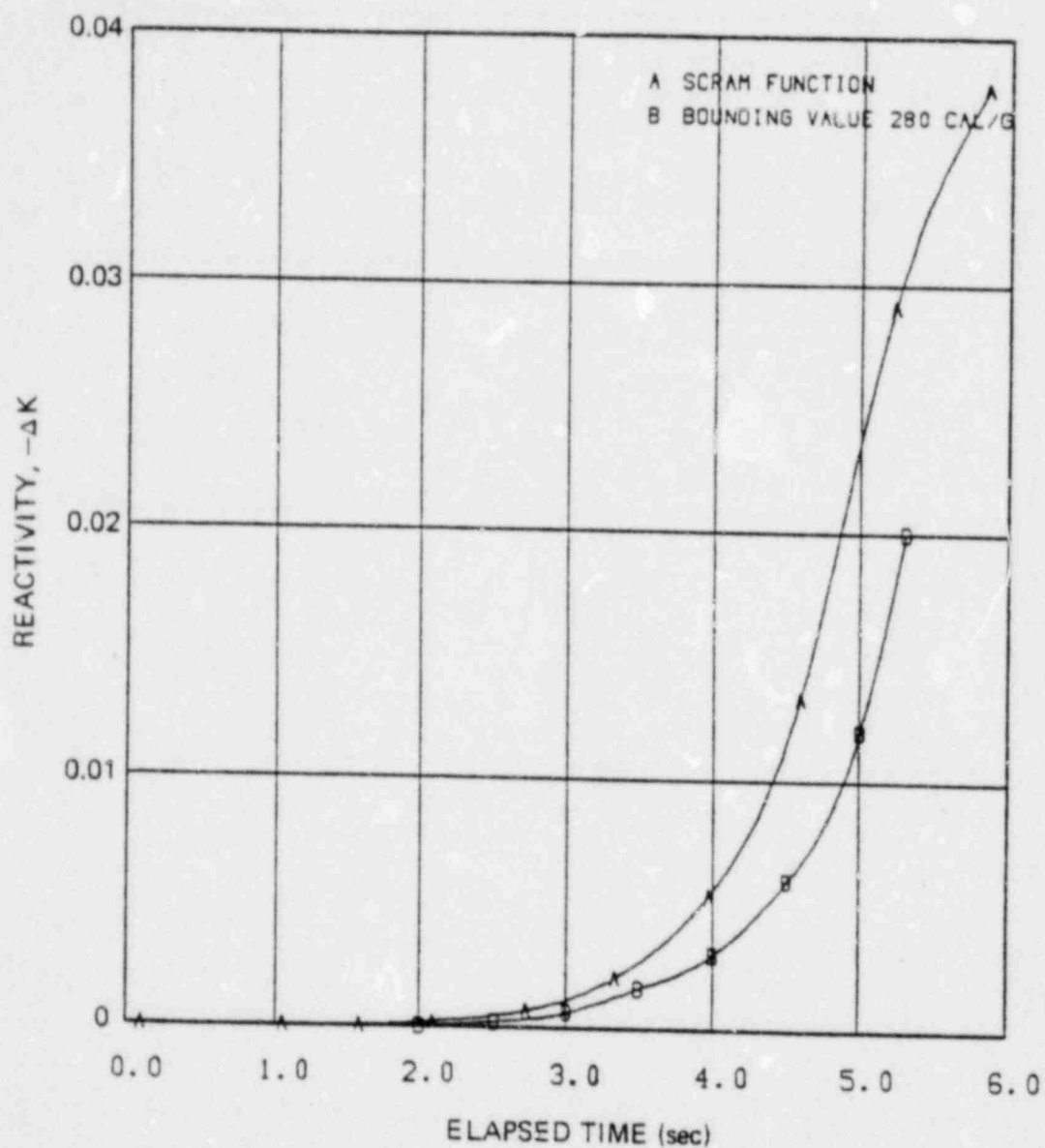


Figure 12. RDA Scram Reactivity Function, Cold

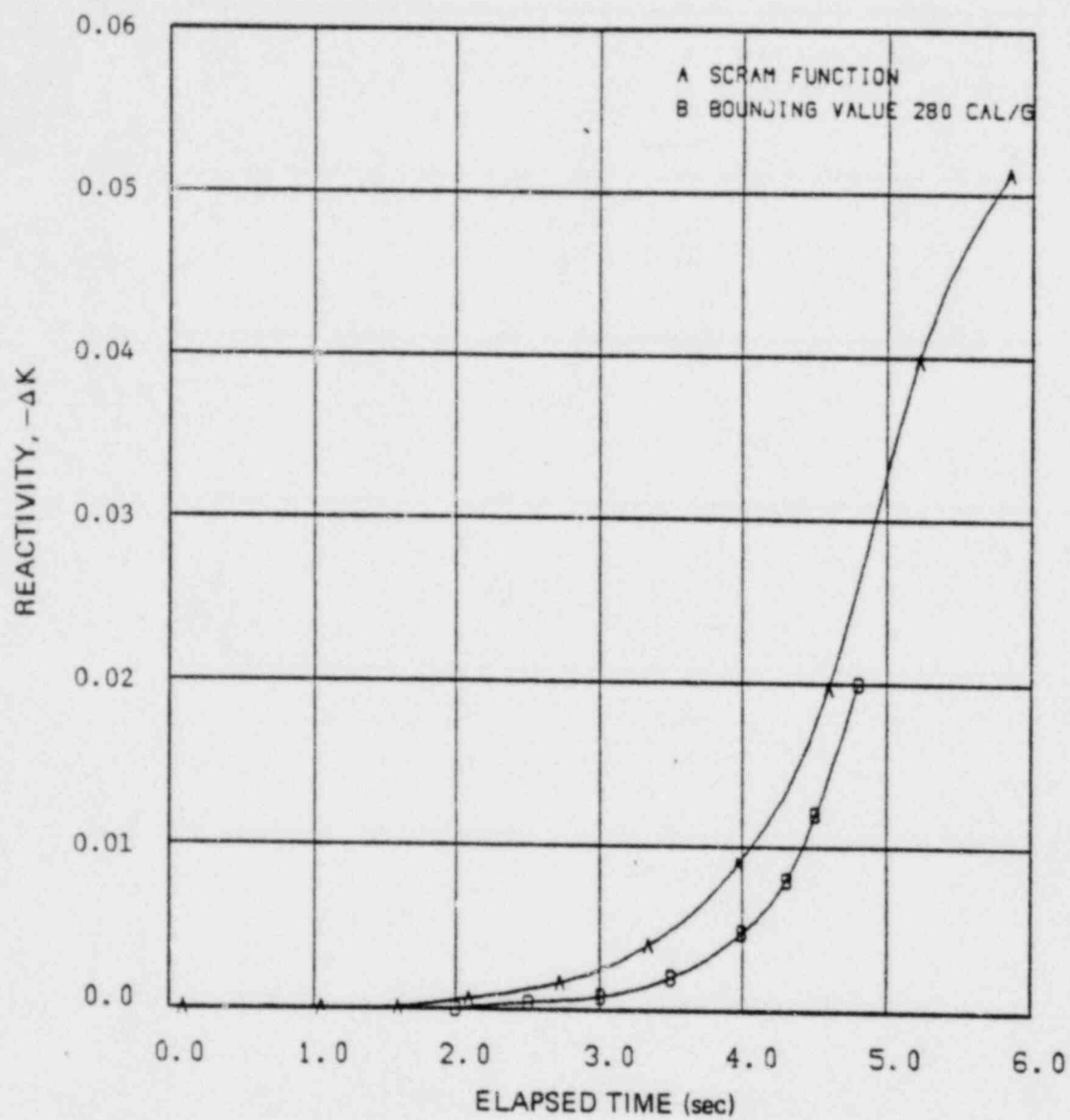


Figure 13. RDA Scram Reactivity Function, Hot Standby

APPENDIX A
TRANSIENT ANALYSIS INITIAL CONDITIONS

S/RV Capacity 84.2%

This valve more accurately represents the capacity of the S/RVs in the "as-installed" conditions.

GENERAL  ELECTRIC