

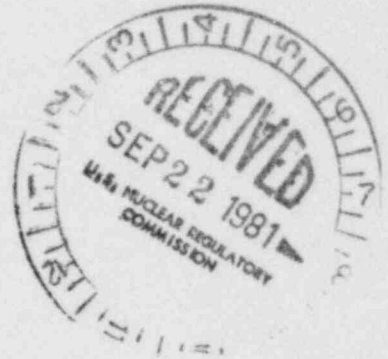
TEXAS UTILITIES SERVICES INC.

2001 BRYAN TOWER · DALLAS, TEXAS 75201

Log # TXX-3400  
File # 906

September 15, 1981

Mr. Spottswood Burwell  
Licensing Project Manager  
U. S. Nuclear Regulatory Commission  
Office of Nuclear Reactor Regulation  
Washington, D.C. 20555



SUBJECT: COMANCHE PEAK STEAM ELECTRIC STATION  
CPSES TO INFORMAL NRC QUESTION ON ECCS  
SWITCHOVER

Dear Mr. Burwell:

Please find attached a response to the subject concern raised by RSB.

If you have any questions, please call.

Sincerely,

A handwritten signature in dark ink, appearing to read "H. C. Schmidt".

H. C. Schmidt

AND:tls

Attachment

cc: R. D. Calder  
J. T. Merritt  
J. C. Kuykendall  
R. A. Jones  
F. W. Madden  
A. T. Parker  
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NRC REACTOR SYSTEMS BRANCH QUESTION  
ON REACTOR OPERATOR FAILURE TO COMPLETE  
ECCS SWITCHOVER FOLLOWING A LOCA

Question: Will the Reactor Operators' failure to complete manual operations (following LOCA) to switchover the ECCS from the injection to the recirculation mode jeopardize the recirculation mode?

Answer: We have completed a calculation which shows that a Reactor Operators' failure to manually switchover the ECCS does not jeopardize the recirculation mode. During the injection phase of ECCS the RHR pumps are taking suction from the RWST. At the low-low level (829'2") in the RWST the sump valve in the line from the sump to the RHR pump suction, open automatically so that the RHR pump is taking suction from both the RWST and the sump. The operator close a valve in the line from the RWST to the RHR pump suction. Our calculation shows that failure to close this valve has no effect on the RHR pump operation, hence the recirculation mode of ECCS, because an adequate water leg exists in the piping line from the RWST to the RHR pump suction. The calculation is presented here.

Calculation: A schematic diagram of one RHR train is provided in Figure 1.

Assumptions

1. The motor operated valve in the piping line from the RWST to the RHR pump suction is open.
2. Piping losses are based on RHR system runout flowrate (4500 gpm).
3. The water level in the sump is at the bottom elevation of the sump.
4. Containment pressure is atmospheric (0.0 psig).
5. Sump water temperature is 212°F; RWST water temperature is 32°F.

The pressure at point A (see Figure 1) is given by (1) and (2).

$$P_A = P_{\text{sump}} + \frac{\rho_{\text{sump}}}{144} (Z_{\text{sump}} - Z_A) - h_{\text{pipe}}$$

where:  $P_A$  - pressure at point A  
 $P_{\text{sump}}$  - sump pressure  
 $\rho_{\text{sump}}$  - water density in the sump  
 $Z_{\text{sump}}$  - sump water elevation  
 $Z_A$  - elevation at point A  
 $h_{\text{pipe}}$  - head loss due to friction

$$P_A = P_{\text{RWST}} + \frac{\rho_{\text{RWST}}}{144} Z_1 \quad (2)$$

where:  $P_{\text{RWST}}$  - RWST pressure  
 $\rho_{\text{RWST}}$  - water density in the RWST  
 $Z_1$  - water leg above point A

therefore

$$P_{\text{sump}} + \frac{\rho_{\text{sump}}}{144} \left[ (Z_{\text{sump}} - Z_A) - h_{\text{pipe}} \right] = P_{\text{RWST}} + \frac{\rho_{\text{RWST}}}{144} Z_1 \quad (3)$$

Equilibrium is reached when

$$P_{\text{sump}} = P_{\text{RWST}} \quad (4)$$

Substituting (4) into (3) and solving for  $Z_1$  yields

$$Z_1 = \frac{\rho_{\text{sump}}}{\rho_{\text{RWST}}} \left[ (Z_{\text{sump}} - Z_A) - h_{\text{pipe}} \right] \quad (5)$$

values used are

$$\rho_{\text{sump}} = \rho_{212^{\circ}\text{F}} = 59.9 \text{ lb/ft}^3$$

$$\rho_{\text{RWST}} = \rho_{32^{\circ}\text{F}} = 62.4 \text{ lb/ft}^3$$

$$Z_{\text{sump}} = 806 \text{ ft}$$

$$Z_A = 781.5 \text{ ft}$$

$$h_{\text{pipe}} = 3.8 \text{ ft}$$

Substituting these values into (5) yields

$$Z_1 = 19.9 \text{ ft}$$

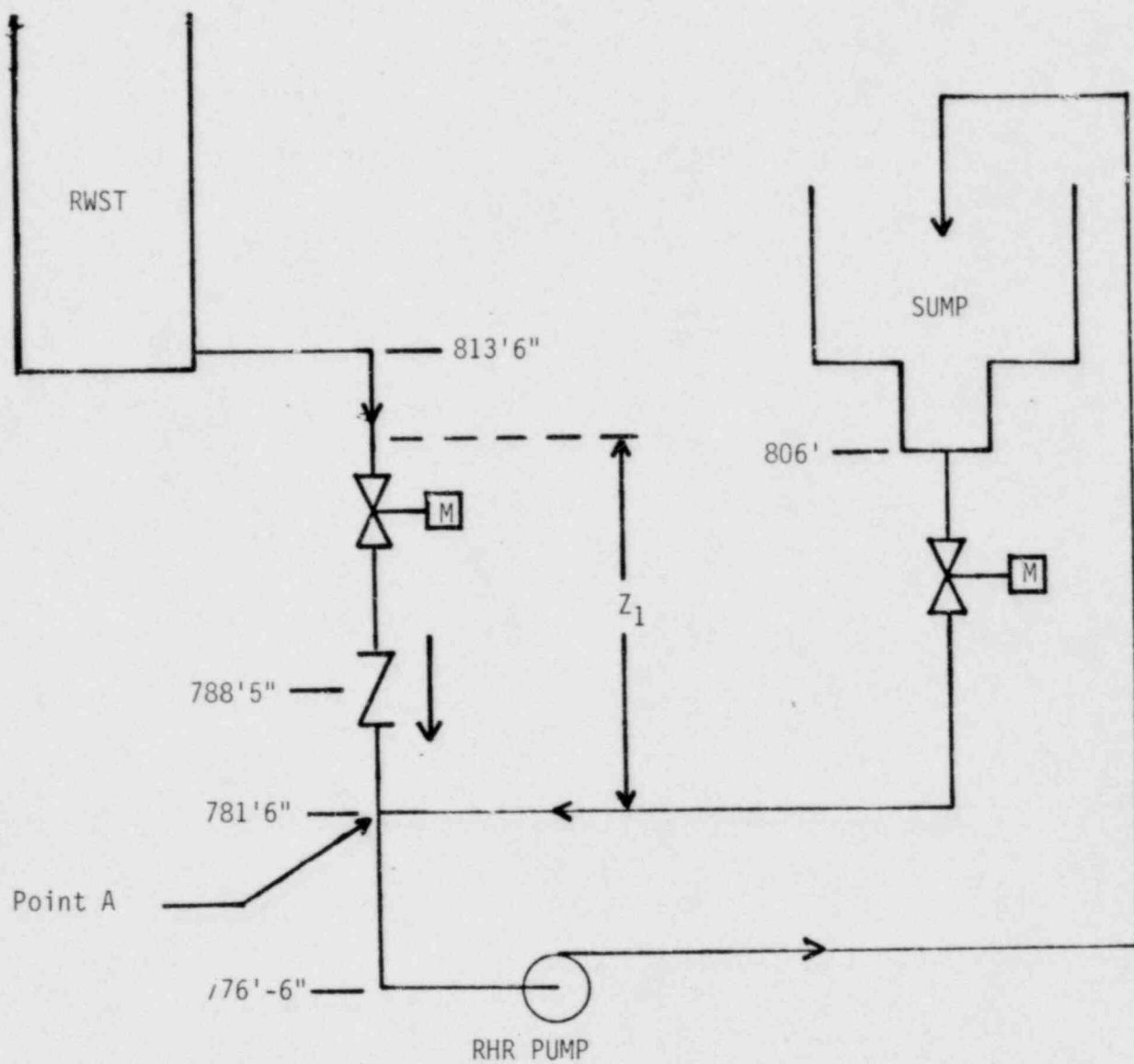


FIGURE 1  
CPSES ECCS SWITCHOVER SCHEMATIC