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CLASS I

JUNE 1979

# **MARK I CONTAINMENT PROGRAM QUARTER SCALE PLANT UNIQUE TESTS**

**TASK NUMBER 5.5.3, SERIES 2**

**VOLUME 2**

1348 129

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Class I  
June 1979

MARK I CONTAINMENT PROGRAM  
1/4 SCALE PRESSURE  
SUPPRESSION POOL SWELL TEST PROGRAM: PLANT UNIQUE TESTS  
TASK NUMBER 5.5.3, SERIES 2

Volume 2, Appendix A

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INTRODUCTION - APPENDICES

The large quantity of data and descriptive material produced by each test series has necessitated the inclusion of a set of appendices with this report. The main report highlights data from a typical plant's tests and summarizes information of general interest. Eight Appendices have been included to present data for the remaining plants, to discuss in detail certain phenomena of particular interest, and to document areas that have received additional investigative effort. The contents of these appendices are summarized below.

Appendix A, which is a continuation of Section 3, presents the test data for the other sixteen plant configurations tested. The data in Section 3 and Appendix A are not necessarily design basis data. The Task 5.5.3-2 Plant Unique Tests were performed at conditions being evaluated for plant operation. Supplementary tests are being performed for several Mark I Utilities to evaluate alternate conditions including variations in water level, submergence, drywell/wetwell pressure differential and vent header deflector design. After a review of these data, a set of test conditions will be selected for each plant to serve as a design basis for pool swell loads.

Appendix B defines the methodology used for vent header pressure integration. The values used for the six point fits to the impact pressure transducer transients and the resulting pressure integrals are also provided.

Appendix C presents plant unique data comparisons and the results of a linear regression correlation of the plant unique test data.

Appendix D estimates the amount of pool mass that is suspended during the upload.

Appendix E presents a series of still pool swell pictures for each plant configuration.

Appendix F presents the results of a measurement uncertainty analysis.

Appendix G presents the specification for vent system resistance and the methods used to meet the specification.

Appendix H presents the results of evaluations of torus window related download oscillations in the plant unique data and a description of the methods employed to remove these effects for several plants.

APPENDIX A

The data for one typical test configuration was presented and discussed in Section 3. The data for the other sixteen configurations tested during the Task 5.5.3-2 Plant Unique Tests is presented and discussed in this appendix in the same format as Section 3.

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APPENDIX AA.1 Hatch 2 TestsA.1.1 Typical Data

Time-history plots of the driving conditions and pool response are presented in this section for Hatch 2, Tests 2 and 6. Test 2 was a load definition test, which was conducted without an initial drywell/wetwell differential pressure (0"  $\Delta P$ ) and with no deflector.

Test 6 was conducted with an initial drywell/wetwell differential pressure of 14.35"  $H_2O$   $\Delta P$  (full  $\Delta P$ ) and with no deflector.

A.1.1.1 Driving Conditions

Driving conditions for Hatch 2 Test 2 are presented in Figures A-1 through A-5. Similar plots for Test 6 are shown in Figures A-6 through A-10. Comparison of the driving conditions indicates that enthalpy flow into the pool starts at an earlier time and peaks out at a lower value in Test 6 with full  $\Delta P$  (Figure A-5 versus A-10).

A.1.1.2 Pool Response

Downcomer internal pressure and wetwell pressures for Hatch 2 Test 2 are presented in Figures A-11 and A-12, respectively. The same pressures for Test 6 are shown in Figures A-13 and A-14. An oscillation can be observed in the downcomer internal pressure in Figure A-11, which is a characteristic of 0"  $\Delta P$  runs. Net torus force from the pressure integral (Figures A-15 and A-16) shows no oscillation in downforce. Some oscillations in upforce, however, can be observed in Test 2 with 0"  $\Delta P$ . Net torus force that is determined from the torus load cell (Figures A-17 and A-19) by applying inertial correction with the torus accelerometer (Figures A-18 and A-20) is shown in Figures A-21 and A-22 and compared

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with net torus force determined from the pressure integral. Figures A-23 and A-24 present the net torus force based on the torus pressure integral, corrected for inertia.

Upforce oscillations which occur in some of the plant tests (type II downcomer with 30° bend) are well illustrated in the Hatch 2 zero  $\Delta P$  tests. These oscillations are caused by delayed breakthrough which allows the water slug to bounce between the torus freespace and the LOCA air bubbles. The upforce oscillations (Figure A-15), which correspond to oscillations in the acceleration of the water slug, are clearly visible in the downcomer (bubble) pressure (Figure A-11) as well as in the torus pool pressures (Figure A-12). The bubble and water pressures are together oscillating out of phase with the torus air pressure as the rising air slug alternately over compresses the freespace and then the bubble.

The high speed movies of previous reference plant tests show that the pool separates at the 45° downcomer bend. When the top of the bubble reaches this separated region, breakthrough is observed to begin in the films and in the data (as signified by an increase in the noise in the pressure integral). Movie of type II downcomer tests with 30° bends transitioning to vertical downcomers near the waterline do not exhibit separated flow behind the downcomers. The pool flows around the downcomers and does not appear to break through until well after peak upforce.

The "average" pool pressures for Hatch 2, Tests 2 and 6 are shown in Figures A-26 and 27. Figures A-25 and A-28 are the same as Figures A-23 and A-24 with force replaced by average pressure (force/ torus projected area).

The vent header impact pressures for Hatch 2 Test 2 are presented in Figures A-29 through A-31. Vent header impact pressures for Test 6 are presented in Figures A-32 through A-34.

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The vent header impact forces from the pressure integral and the corrected load cell agree reasonably well (Figure A-35). Vent header vertical acceleration measurements from Tests 2 and 6 are shown in Figures A-36 and A-37, respectively.

#### A.1.2 Pool Dynamics

The pool contours at various times of pool swell are shown in Figures A-38 through A-41 for Hatch 2, Tests 1, 2, 3, and 5.

Pool surface displacement curves are shown in Figures A-42 and A-44. The pool surface velocity profiles are shown in Figures A-43 and A-45.

The pool surface displacement versus time and velocity profile viewed from the side window during Test 4 are shown in Figure A-46. The downcomer water slug displacement, velocity, and acceleration versus time for Test 2 are shown in Figure A-47.

#### A.1.3 Data Summaries

Tables A-1 and A-2 present the Hatch 2 test data for wetwell vertical forces.

Table A-3 presents the Hatch 2 test data for vent header impact forces.

#### A.1.4 Discussion and Analysis

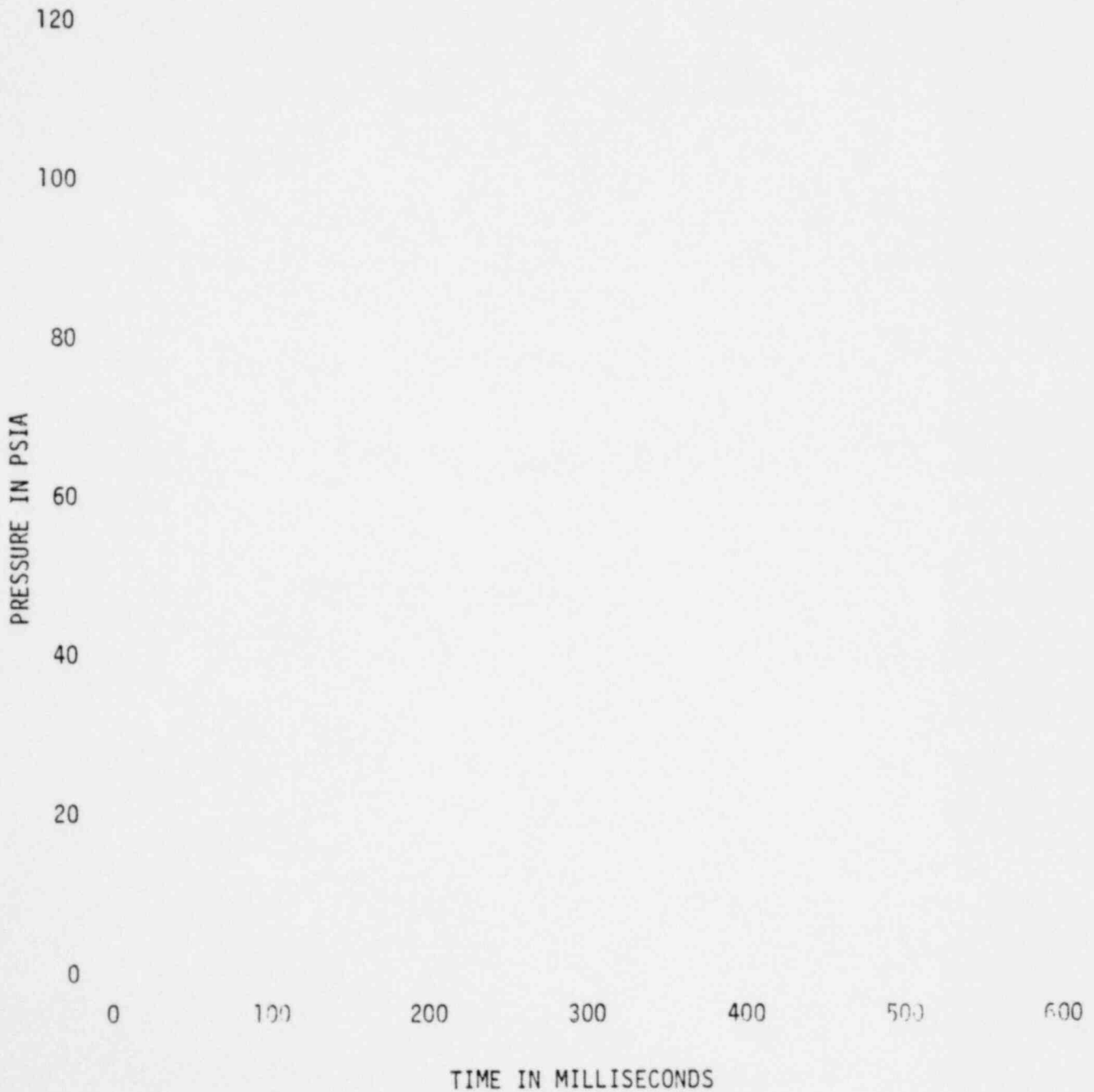
Figure A-48 presents the effect of drywell/wetwell  $\Delta P$  on enthalpy flow into the bubbles. The enthalpy flow starts at an earlier time (vents clear at an earlier time) and reaches a lower steady state value in the full  $\Delta P$  run (Test 6). The effect of drywell/wetwell  $\Delta P$  on downcomer internal pressure is shown in Figure A-49. Figure A-50 presents the effect of drywell/wetwell  $\Delta P$  on pool and freespace pressures. The Hatch 2, Test 2 data parallels that for

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Test 8 of the "typical" plant in Section 3.0. The Hatch 2, Test 6 data parallels the "typical" Test 2 data.

The Hatch 2 load definition tests were conducted at 0" H<sub>2</sub>O  $\Delta$ P with no deflector.  $\Delta$ P sensitivity tests at 14.35" H<sub>2</sub>O  $\Delta$ P (full  $\Delta$ P) was also conducted. Downforce showed no oscillation, but upforce showed some oscillations in the 0" H<sub>2</sub>O  $\Delta$ P runs. The vent header impact force was significantly higher than for plants using deflectors.

FIGURE A-1  
DRYWELL ORIFICE UPSTREAM PRESSURE  
Task 5.5.3-2 Hatch 2 Test 2



\*Proprietary information deleted.

1348 140

FIGURE A-2  
DRYWELL PRESSURE  
Task 5.5.3-2 Hatch 2 Test 2



\*Proprietary information deleted.

1343 141

FIGURE A-3  
DOWNCOMER ORIFICE DIFFERENTIAL PRESSURE  
Task 5.5.3-2 Hatch 2 Test 2

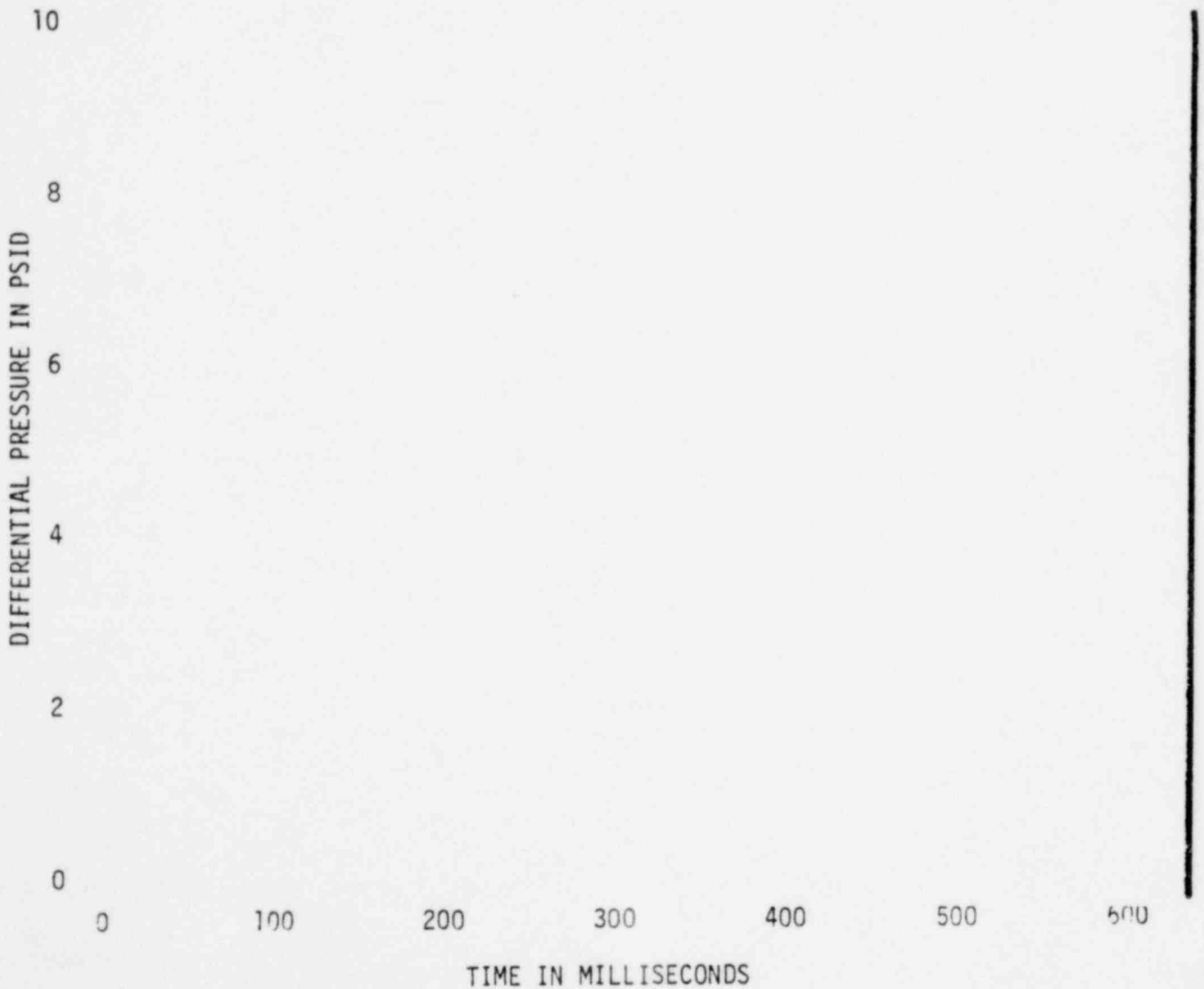


FIGURE A-4  
DOWNCOMER ORIFICE UPSTREAM TEMPERATURE  
Task 5.5.3-2 Hatch 2 Test 2

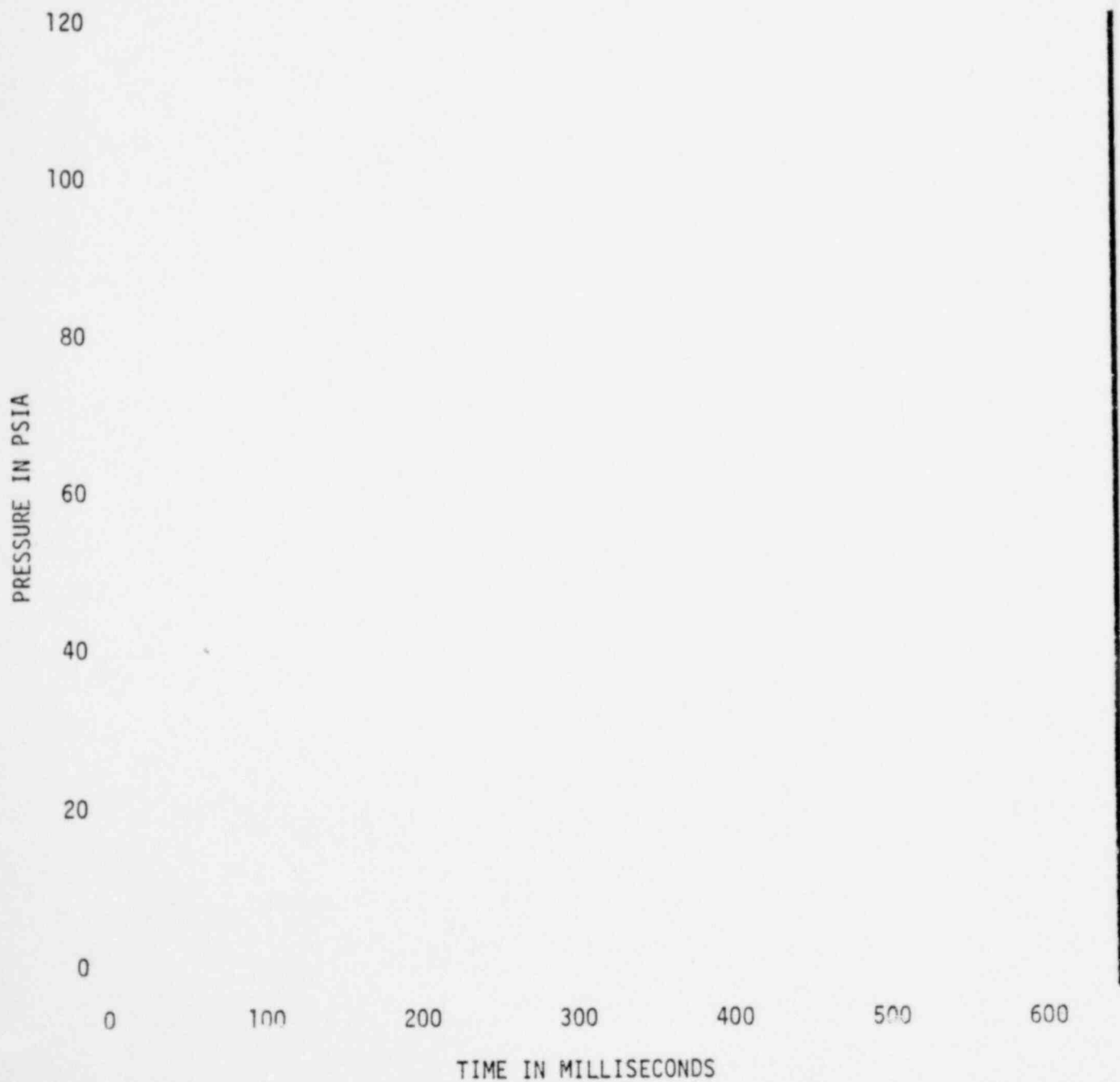


FIGURE A-5  
ENTHALPY FLOW INTO POOL  
Task 5.5.3-2 Hatch 2 Test 2



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FIGURE A-6  
DRYWELL ORIFICE UPSTREAM PRESSURE  
Task 5.5.3-2 Hatch 2 Test 6



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FIGURE A-7  
DRYWELL PRESSURE  
Task 5.5.3-2 Hatch 2 Test 6



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FIGURE A-8

DOWNCOMER ORIFICE DIFFERENTIAL PRESSURE

Task 5.5.3-2 Hatch 2 Test 6



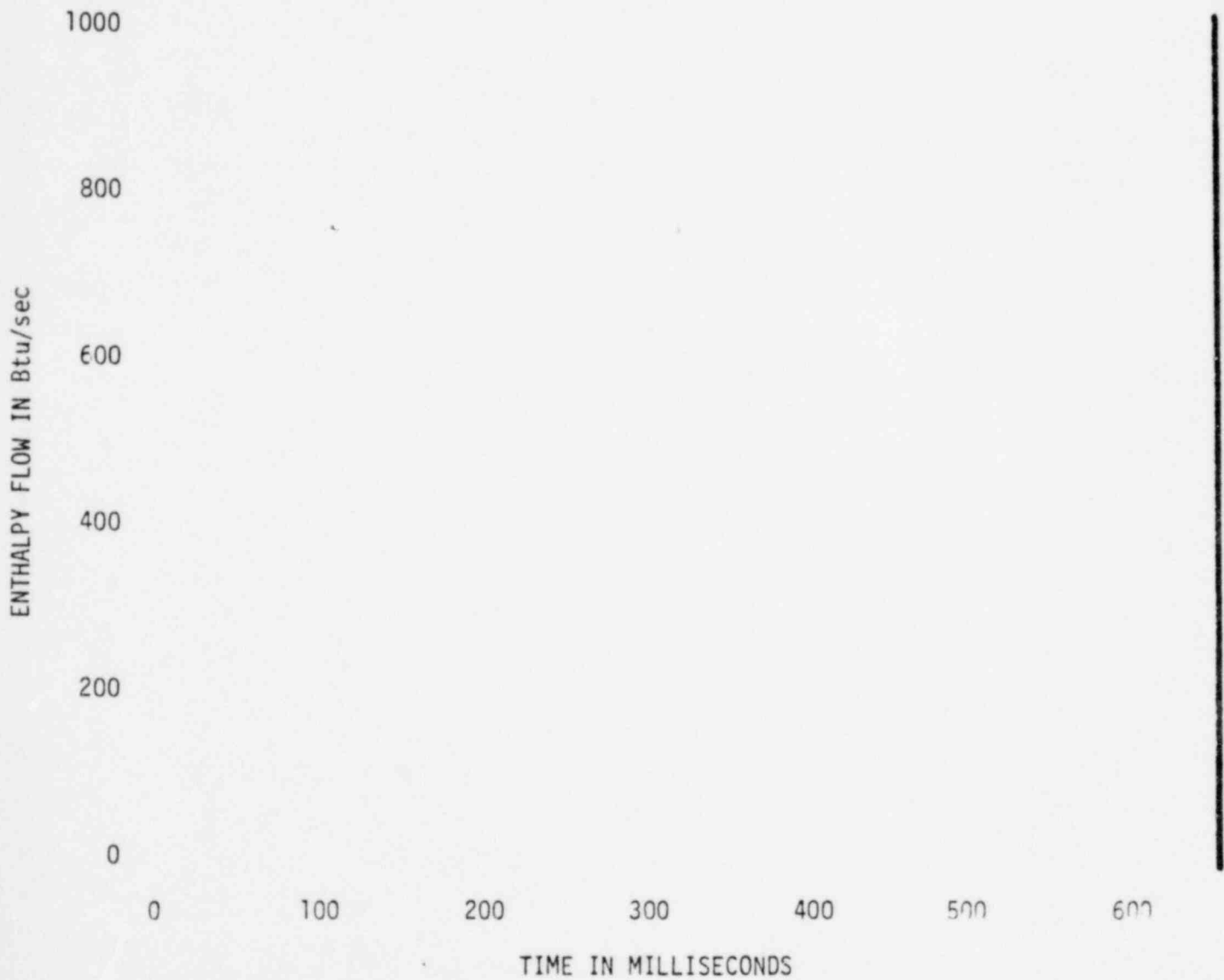
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FIGURE A-9  
DOWNCOMER ORIFICE UPSTREAM TEMPERATURE  
Task 5.5.3-2 Hatch 2 Test 6



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FIGURE A-10  
ENTHALPY FLOW INTO POOL  
Task 5.5.3-2 Hatch 2 Test 6



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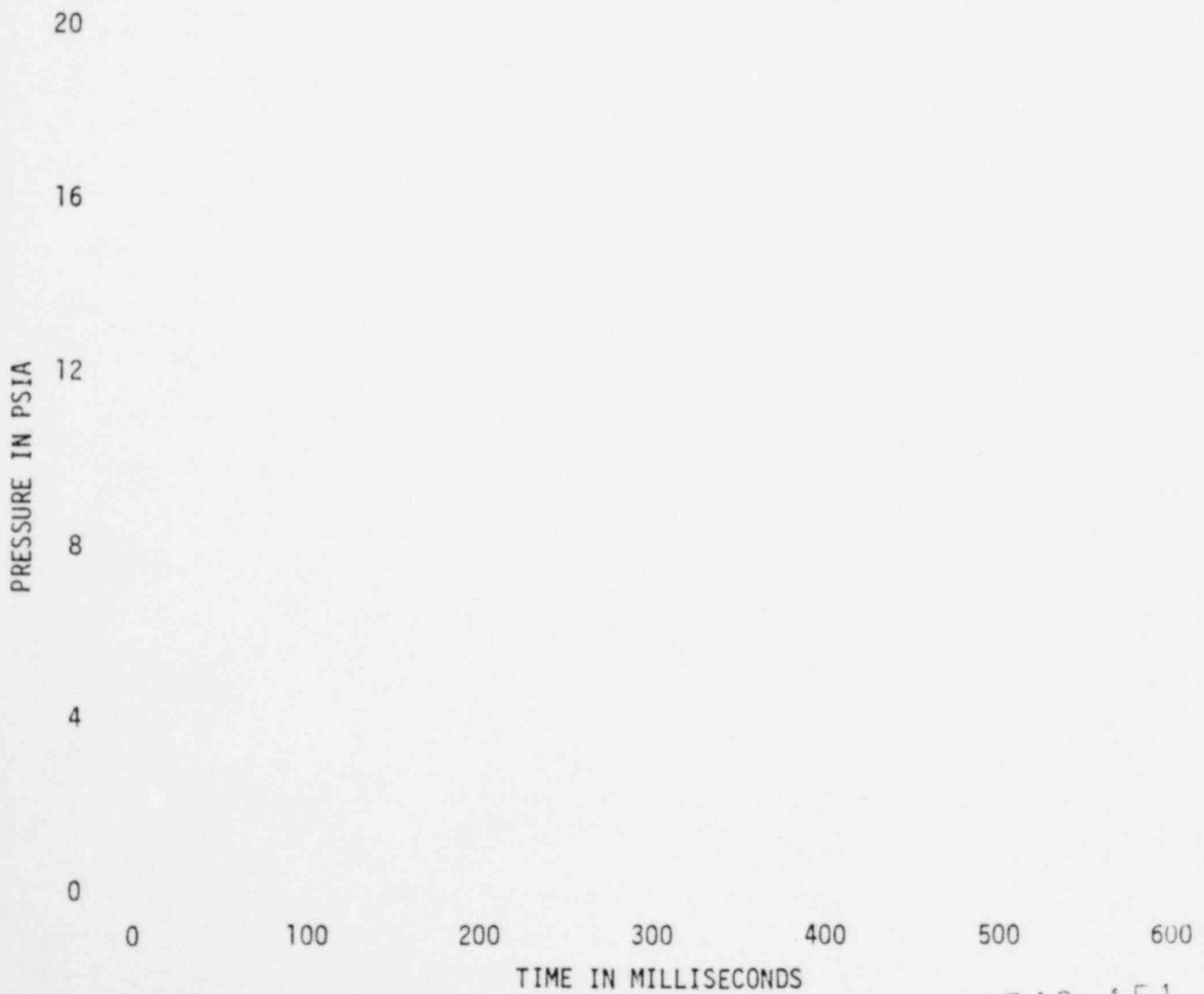
FIGURE A-11  
DOWNCOMER INTERNAL PRESSURE  
Task 5.5.3-2 Hatch 2 Test 2



FIGURE A-12

WETWELL PRESSURES

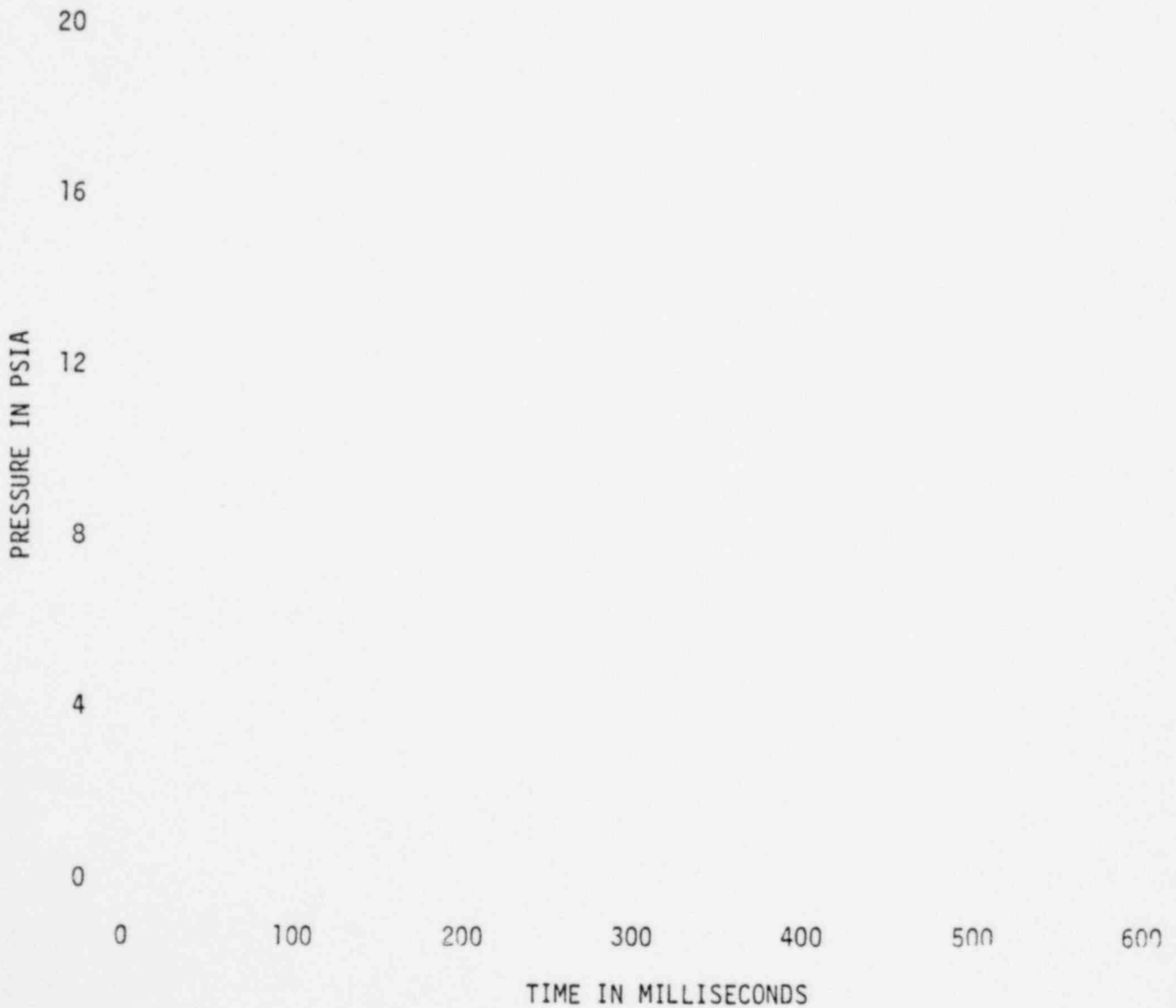
Task 5.5.3-2 Hatch 2 Test 2



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FIGURE A-13

DOWNCOMER INTERNAL PRESSURE  
Task 5.5.3-2 Hatch 2 Test 6



1348 152

FIGURE A-14

WETWELL PRESSURES

Task 5.5.3-2 Hatch 2 Test 6



TIME IN MILLISECONDS

1318 153

FIGURE A-15

NET TORUS FORCE FROM PRESSURE INTEGRAL

Task 5.5.3-2 Hatch 2 Test 2

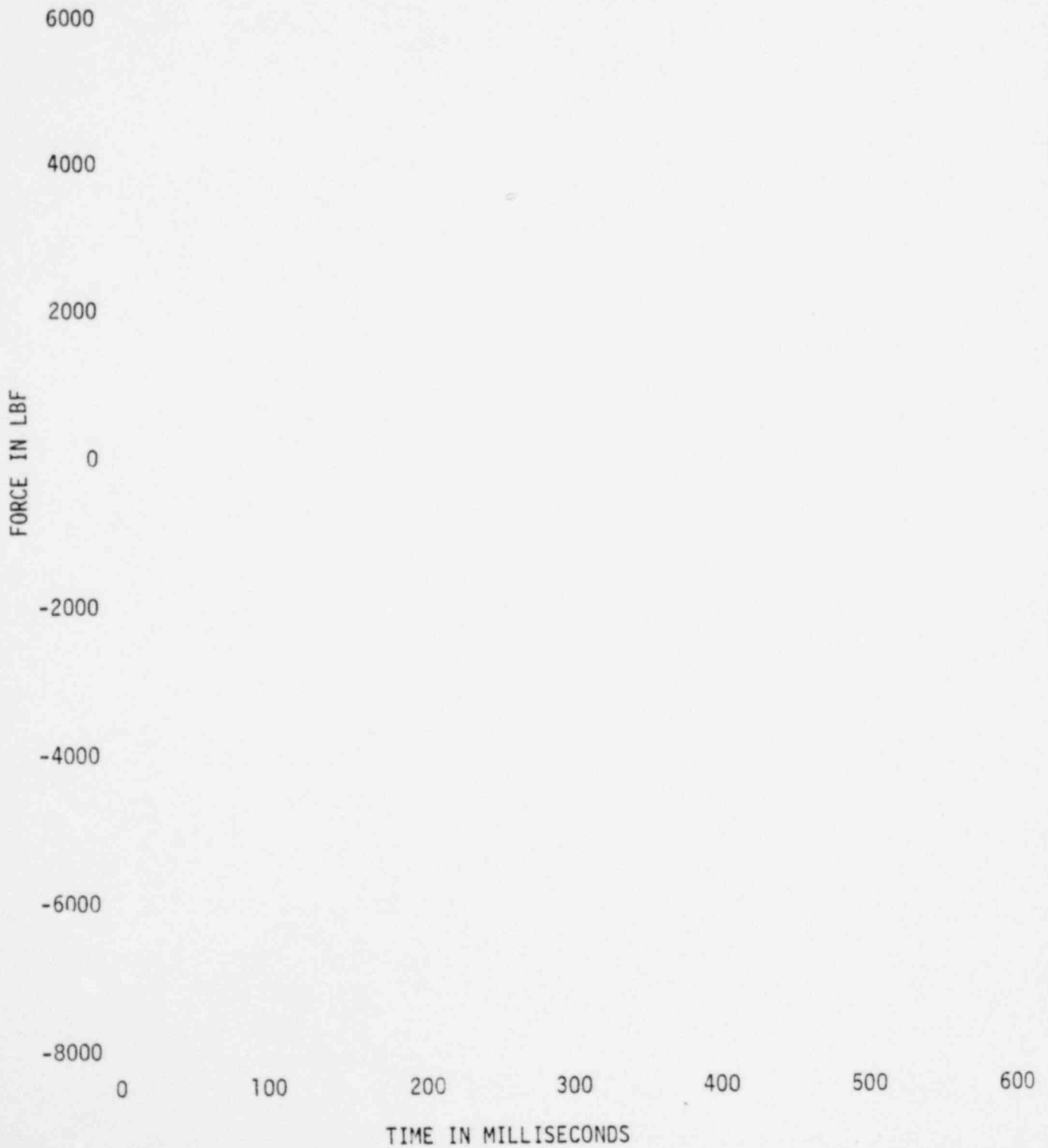


FIGURE A-16

NET TORUS FORCE FROM PRESSURE INTEGRAL

Task 5.5.3-2 Hatch 2 Test 6

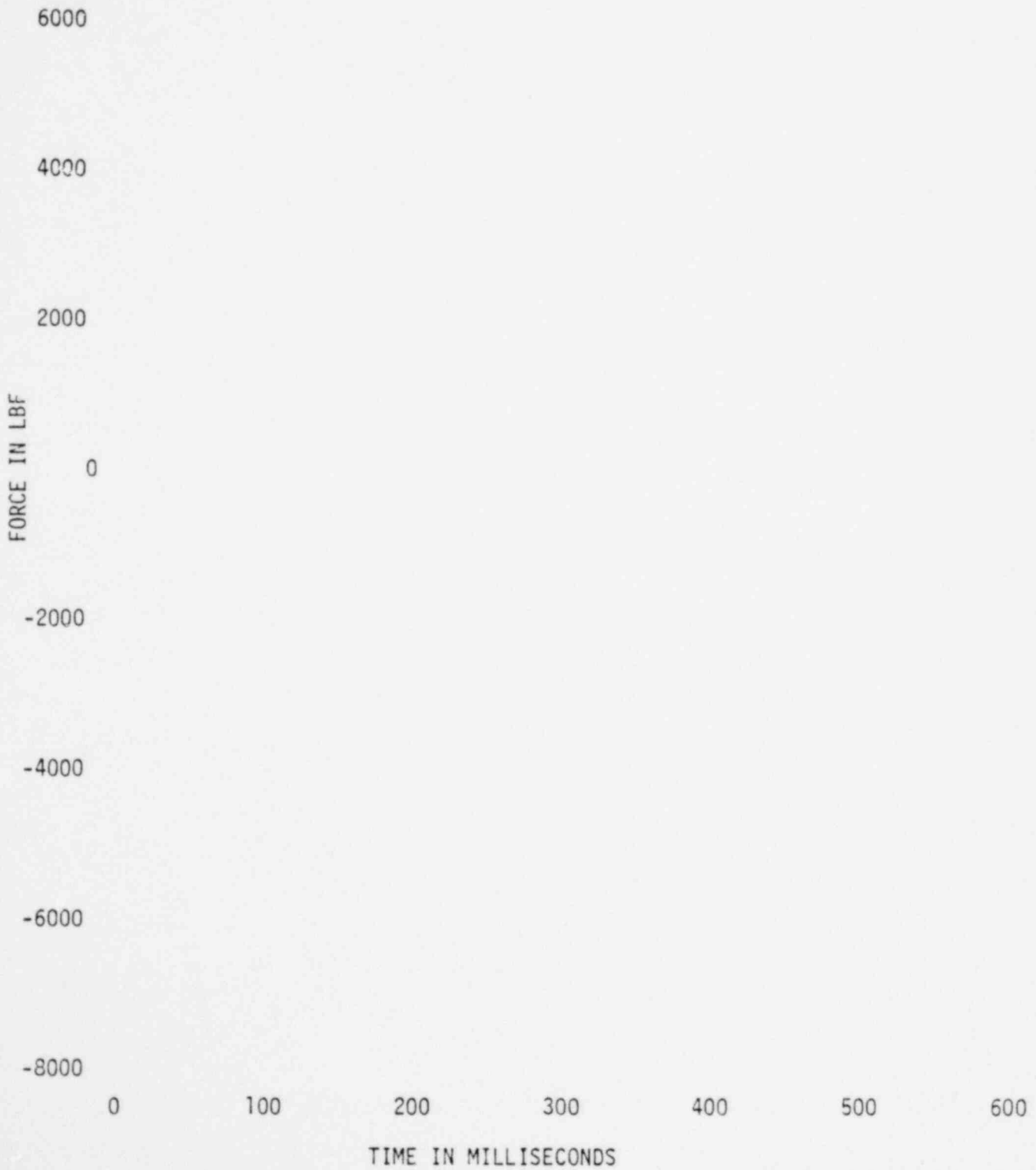


FIGURE A-17

TORUS LOAD CELL

Task 5.5.3-2 Hatch 2 Test 2

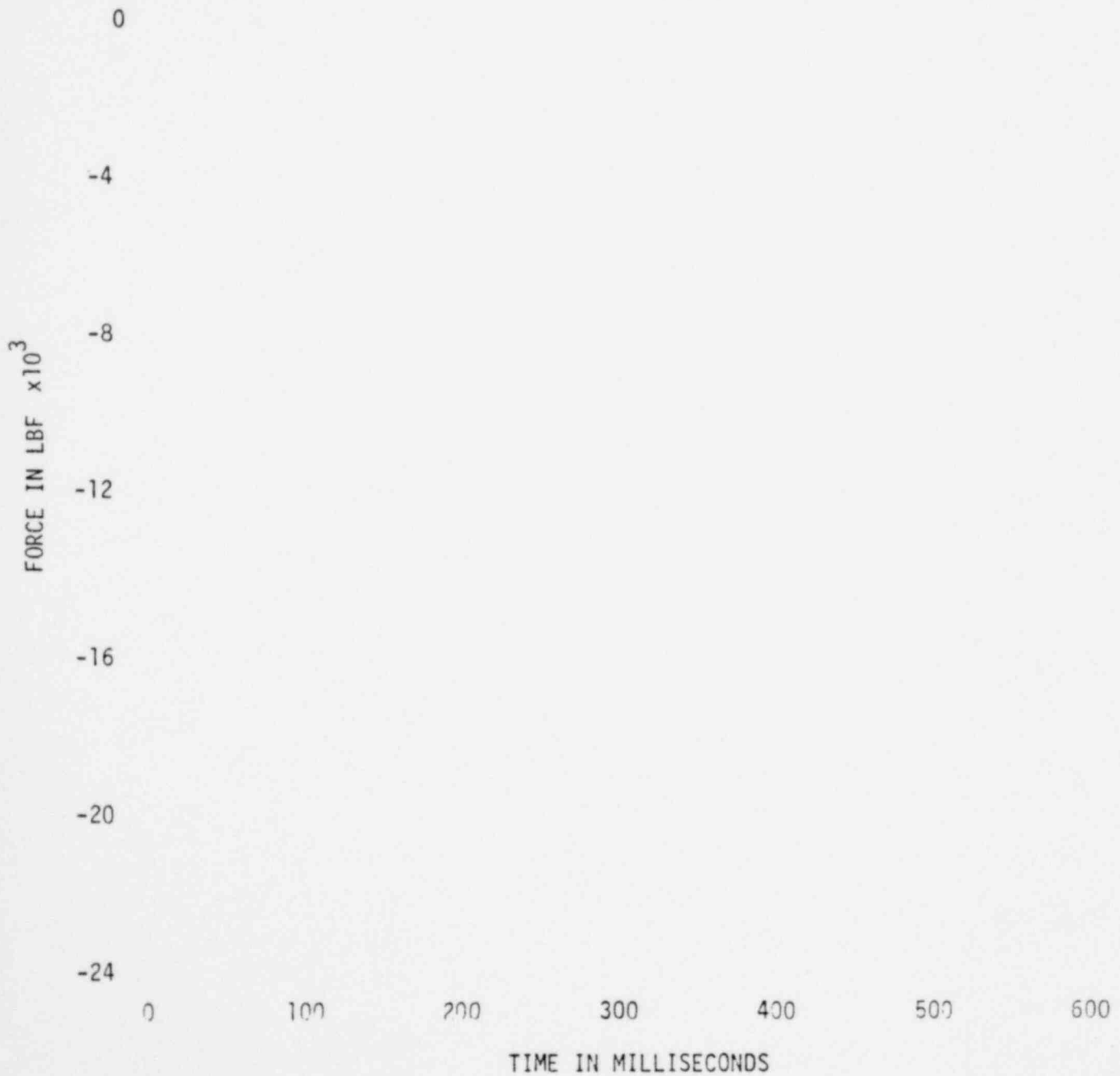
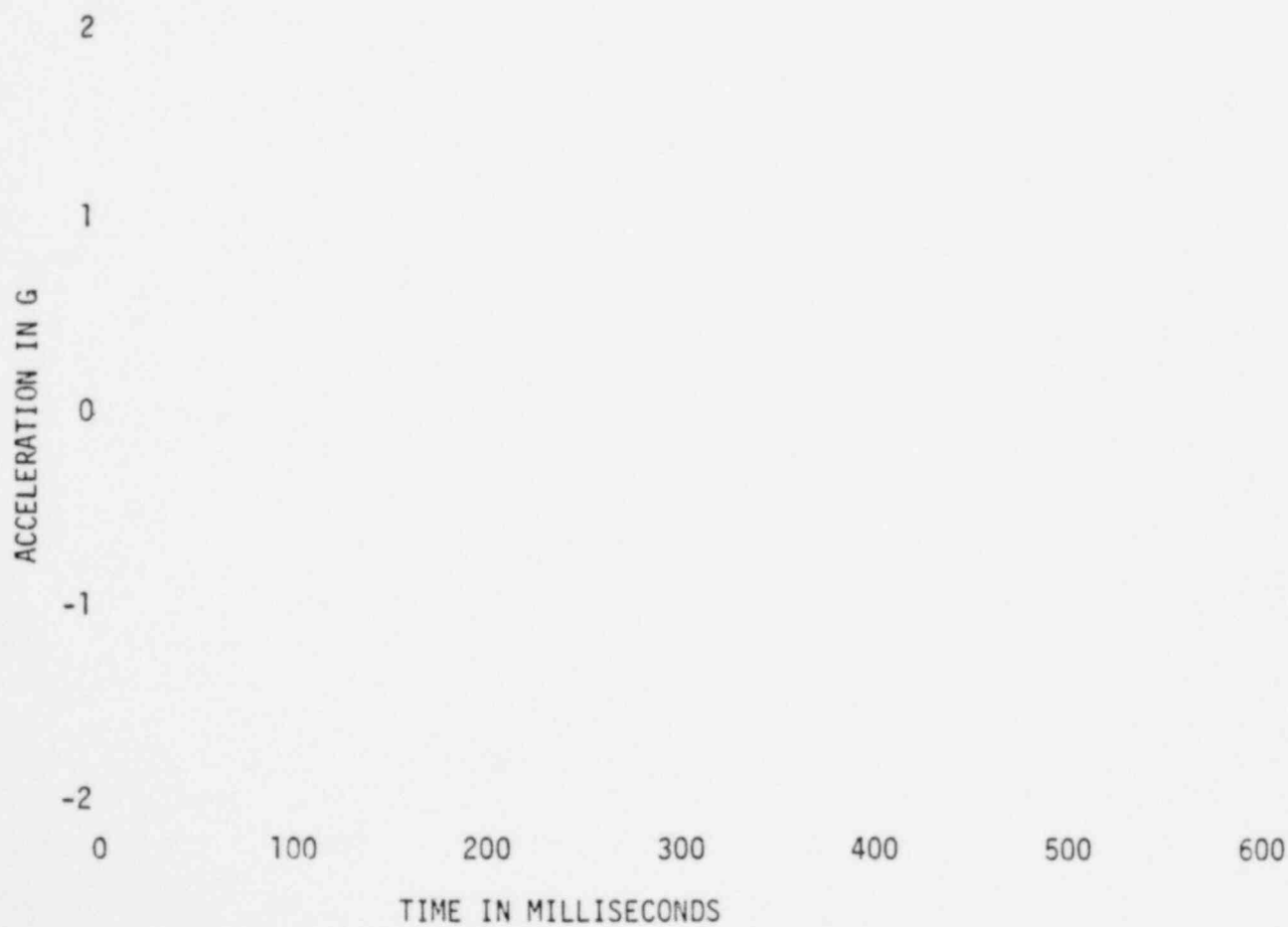


FIGURE A-18

TORUS VERTICAL ACCELERATION

Task 5.5.3-2 Hatch 2 Test 2

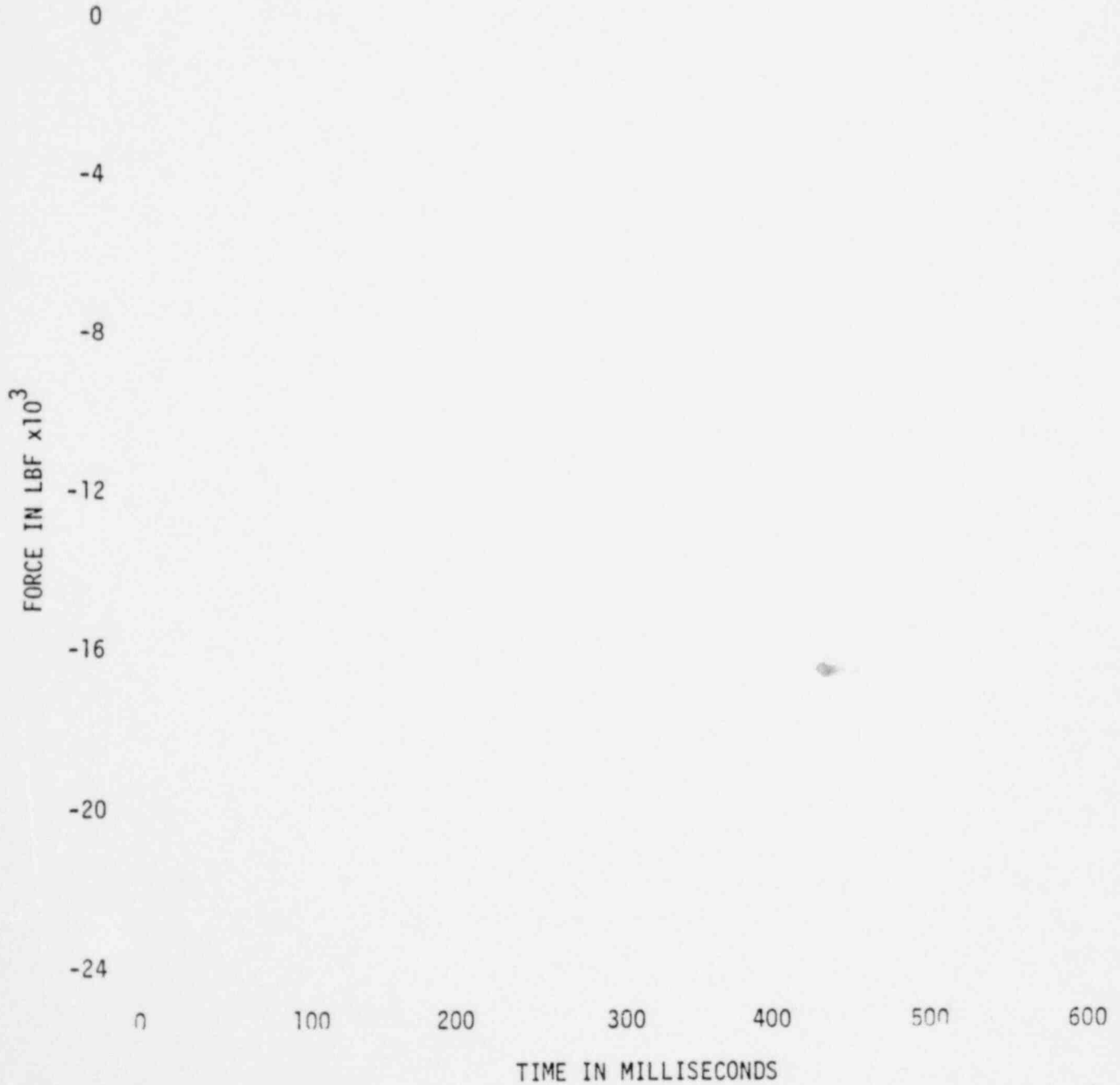


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FIGURE A-19

TORUS LOAD CELL

Task 5.5.3-2 Hatch 2 Test 6

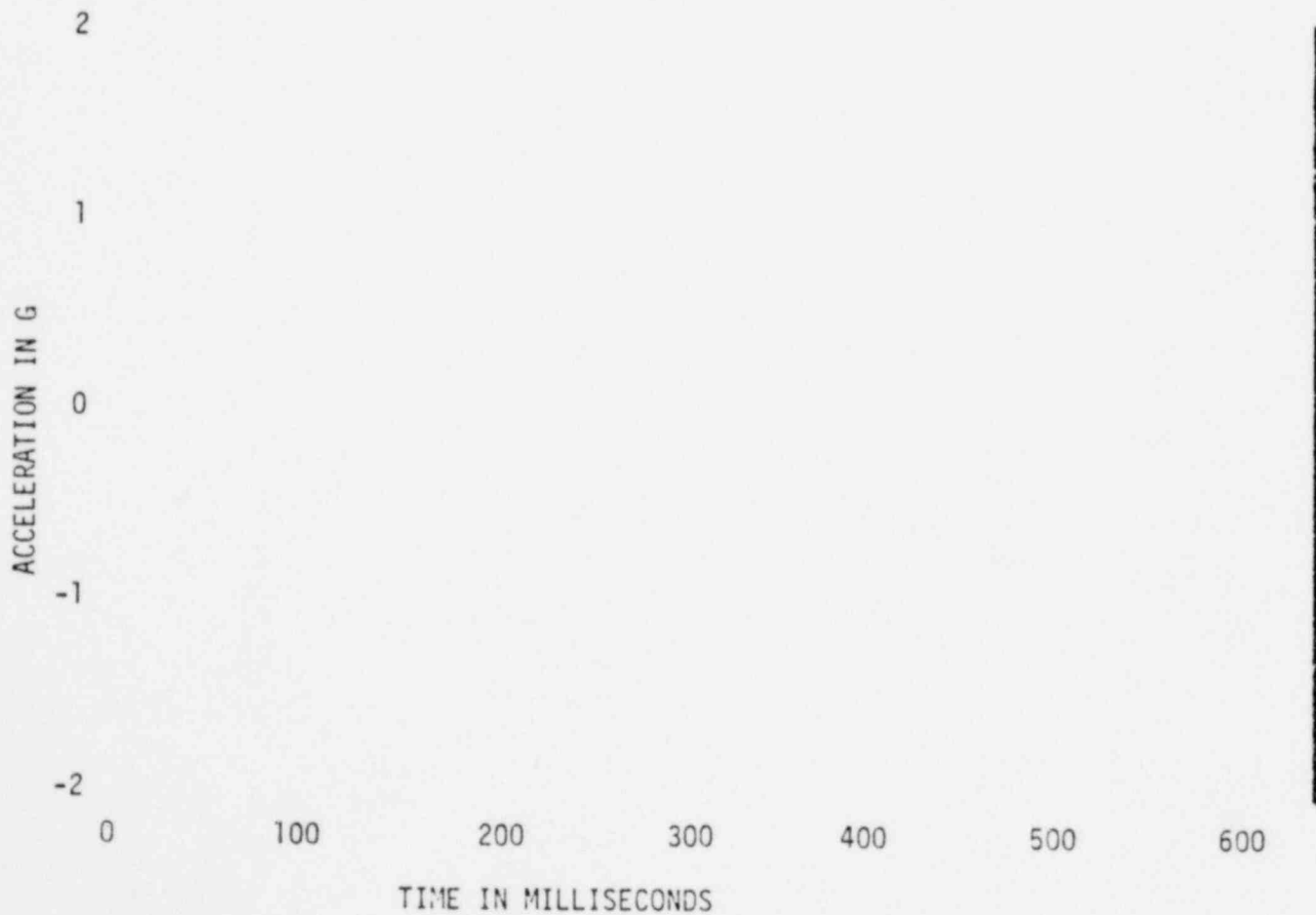


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FIGURE A-20

TORUS VERTICAL ACCELERATION

Task 5.5.3-2 Hatch 2 Test 6



1348 159

FIGURE A-21 COMPARISON OF NET TORUS FORCE FROM PRESSURE INTEGRAL  
WITH NET TORUS FORCE FROM LOAD CELL CORRECTED FOR TORUS INERTIA

Task 5.5.3-2 Hatch 2 Test A2



COMPARISON OF NET TORUS FORCE FROM PRESSURE INTEGRAL  
WITH NET TORUS FORCE FROM LOAD CELL CORRECTED FOR TORUS INERTIA  
Task 5.5.3-2 Hatch 2 Test 6



FIGURE A-23

NET TORUS FORCE FROM PRESSURE INTEGRAL, CORRECTED FOR WATER INERTIA

Task 5.5.3-2 Hatch 2 Test 2

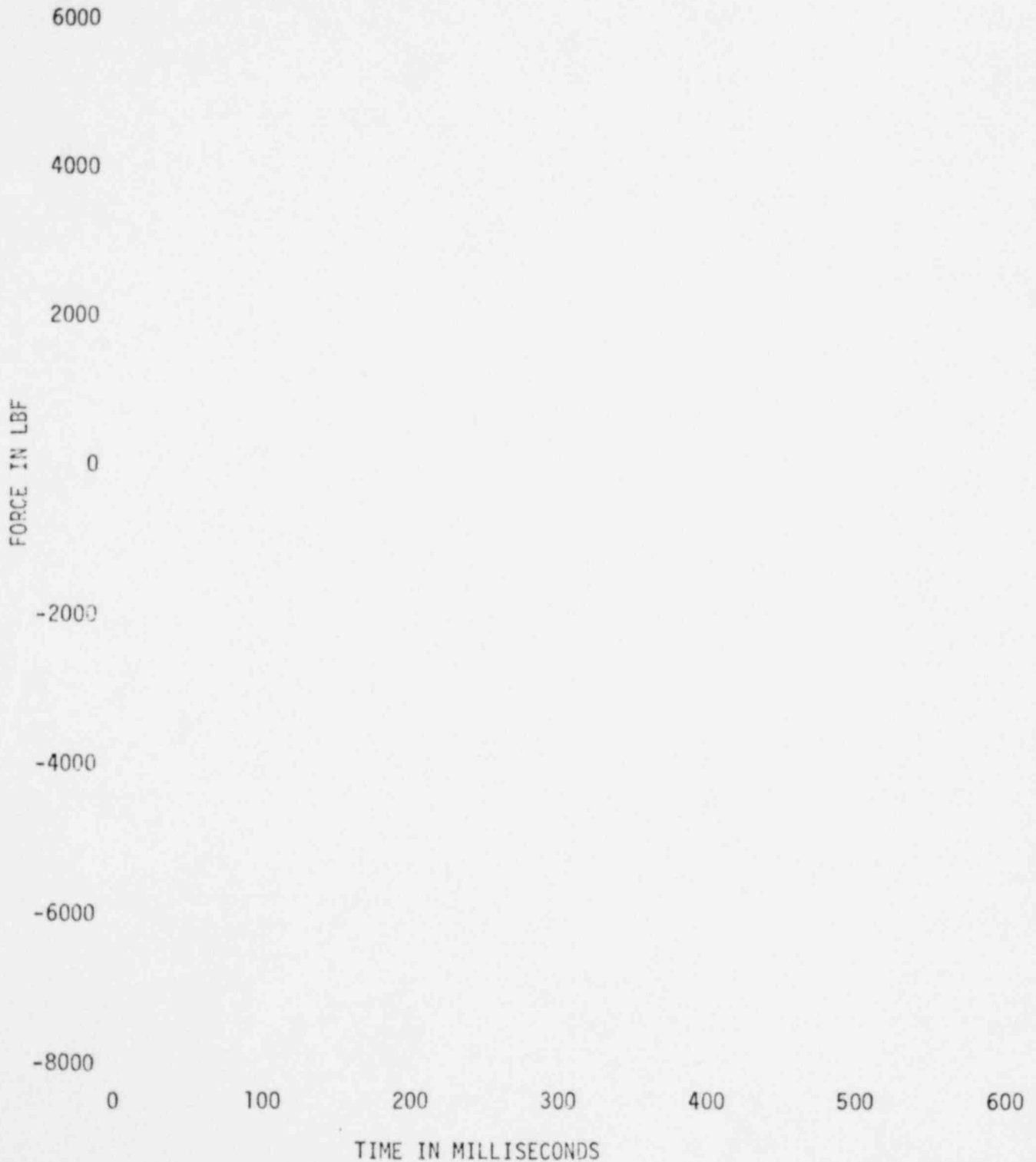


FIGURE A-24

NET TORUS FORCE FROM PRESSURE INTEGRAL, CORRECTED FOR WATER INERTIA

Task 5.5.3-2 Hatch 2 Test 6

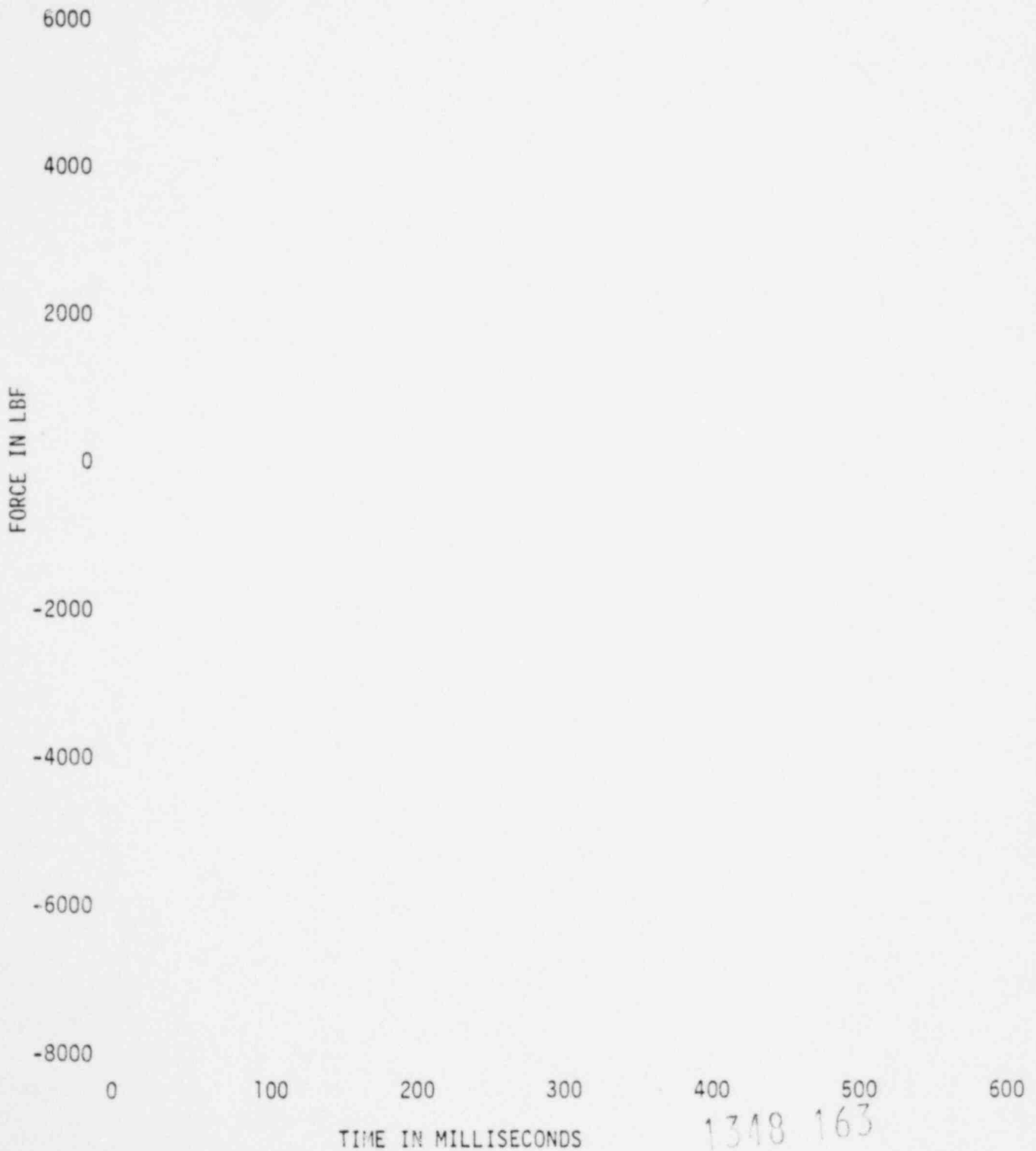
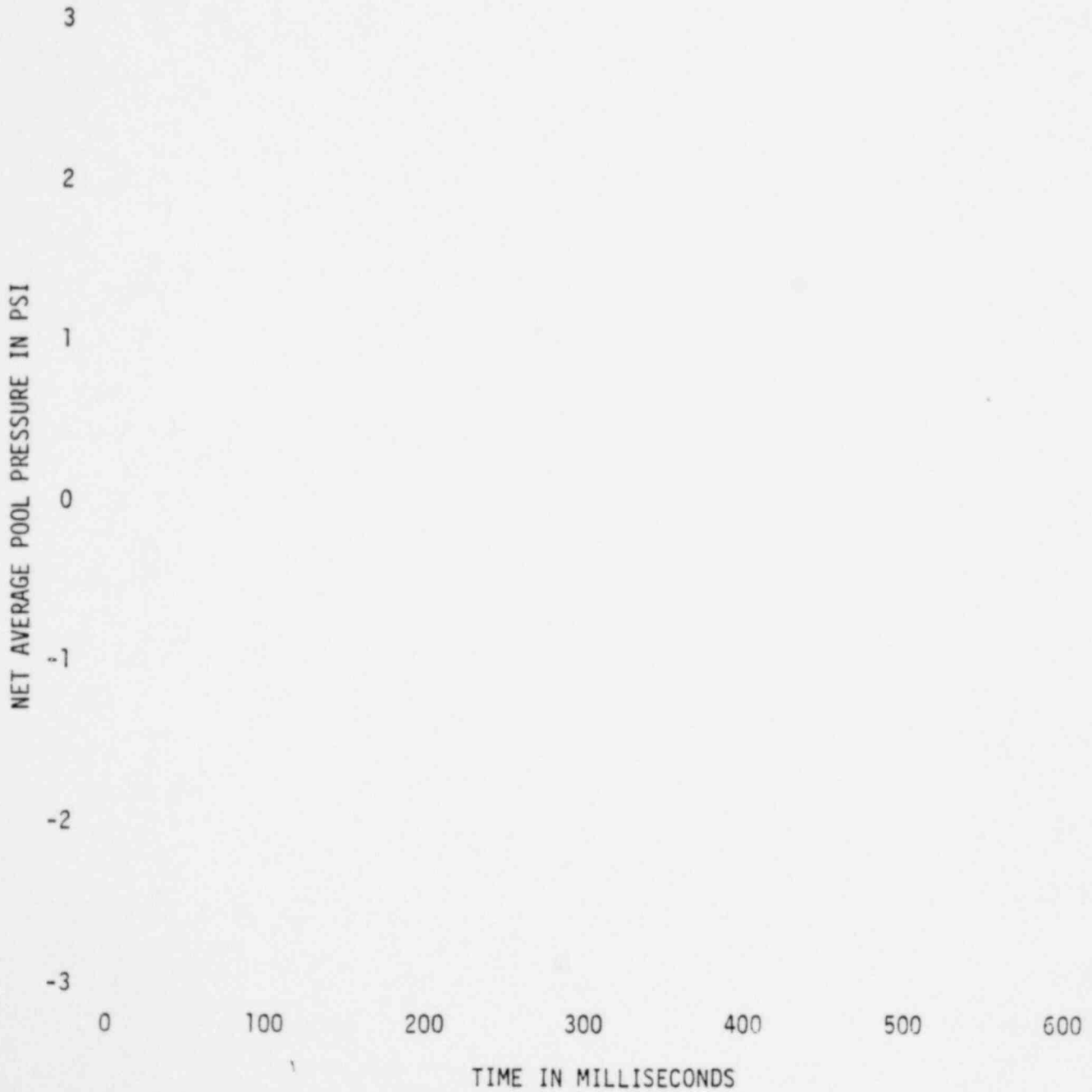


FIGURE A-25

NET AVERAGE POOL PRESSURE, CORRECTED FOR WATER INERTIA

Task 5.5.3-2 Hatch 2 Test 2

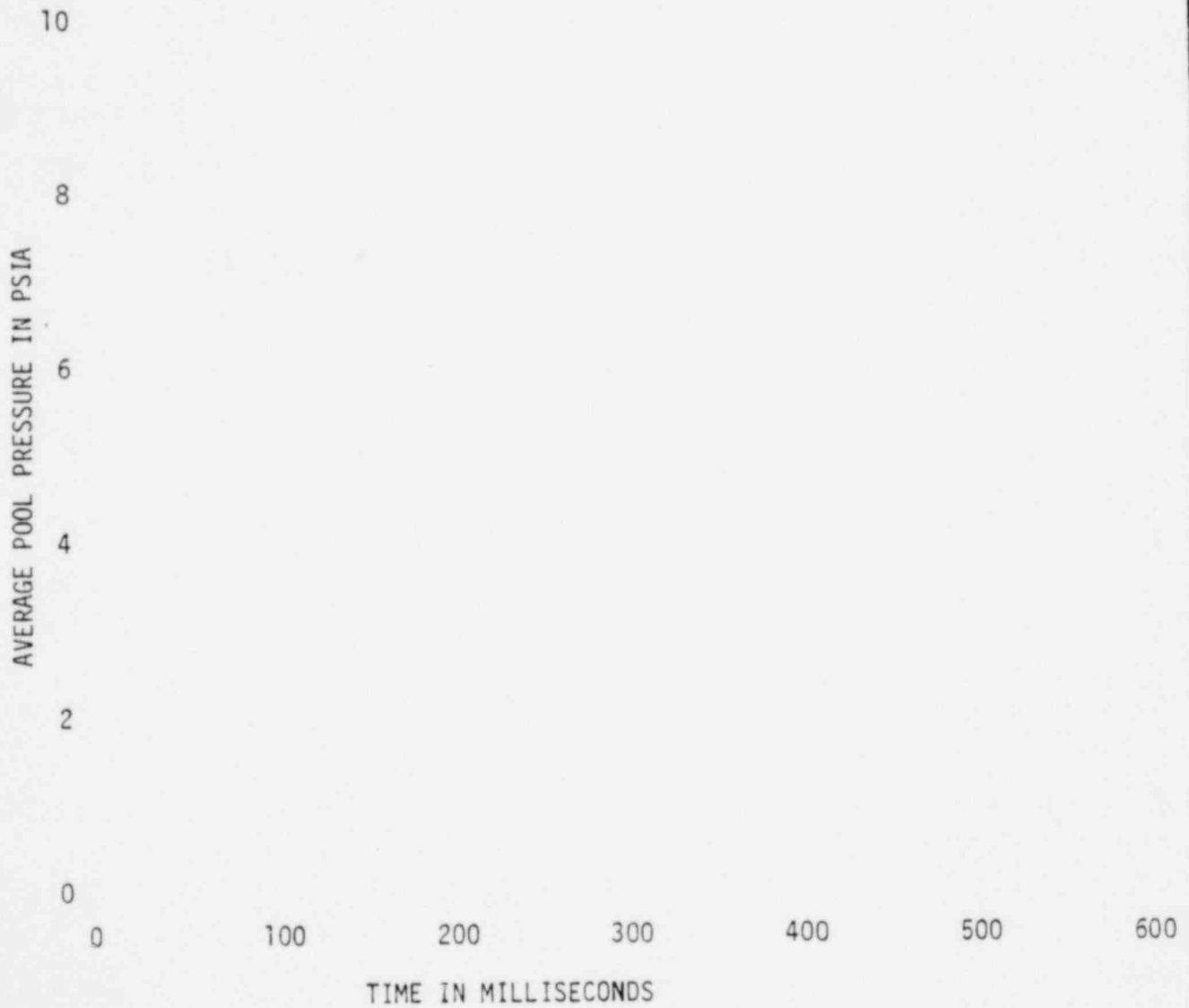


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FIGURE A-26

AVERAGE POOL PRESSURE, CORRECTED FOR WATER INERTIA

Task 5.5.3-2 Hatch 2 Test 2



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FIGURE A-27

AVERAGE POOL PRESSURE, CORRECTED FOR WATER INERTIA

Task 5.5.3-2 Hatch 2 Test 6

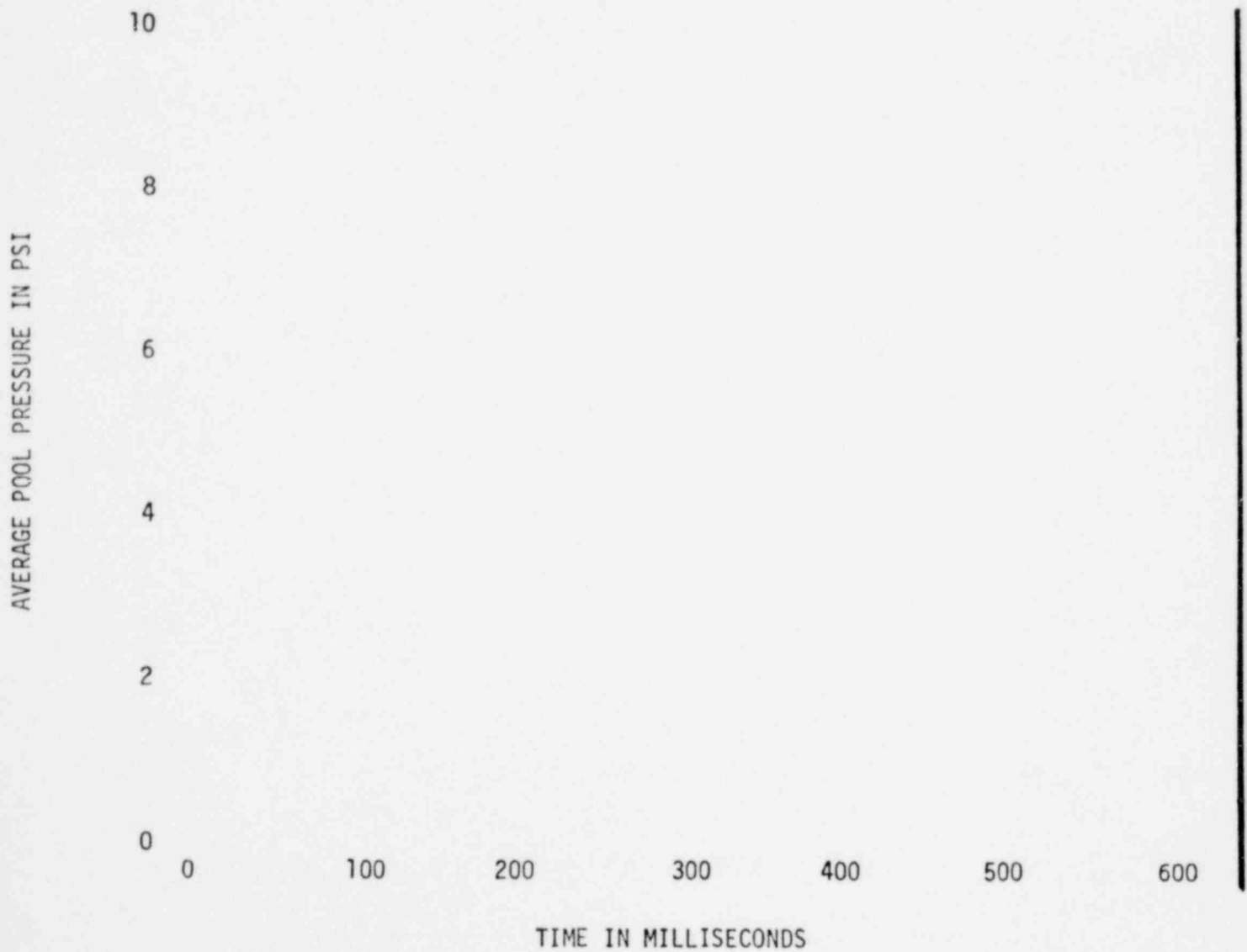


FIGURE A-28

NET AVERAGE POOL PRESSURE, CORRECTED FOR WATER INERTIA

Task 5.5.3-2 Hatch 2 Test 6

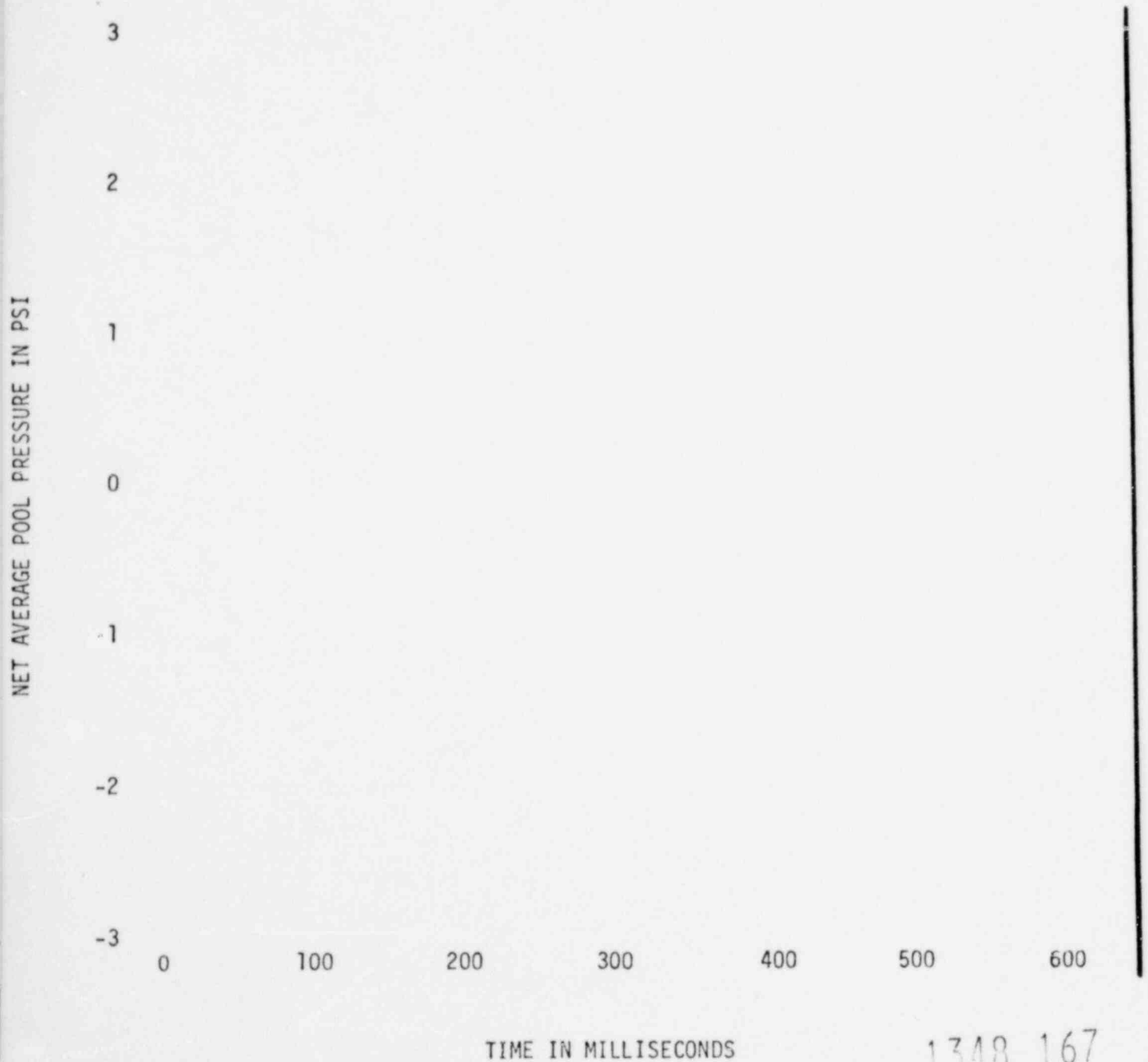


FIGURE A-29

VENT HEADER IMPACT PRESSURES

Task 5.5.3-2 Hatch 2 Test 2

PRESSURE IN PSIA

A-34

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FIGURE A-30

VENT HEADER IMPACT PRESSURES  
Task 5.5.3-2 Hatch 2 Test 2

PRESSURE IN PSIA

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A-35

FIGURE A-31

VENT HEADER IMPACT PRESSURES

Task 5.5.3-2 Hatch 2 Test 2

A-36

PRESSURE IN PSIA

1348 170

FIGURE A-32

VENT HEADER IMPACT PRESSURES

Task 5.5.3-2 Hatch 2 Test 6

PSIA IN PRESSURE

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FIGURE A-33

VENT HEADER IMPACT PRESSURES

Task 5.5.3-2 Hatch 2 Test 6

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PSIA IN VISA

172 177 182

A-38

FIGURE A-34

VENT HEADER IMPACT PRESSURES

Task 5.5.3-2 Hatch 2 Test 6

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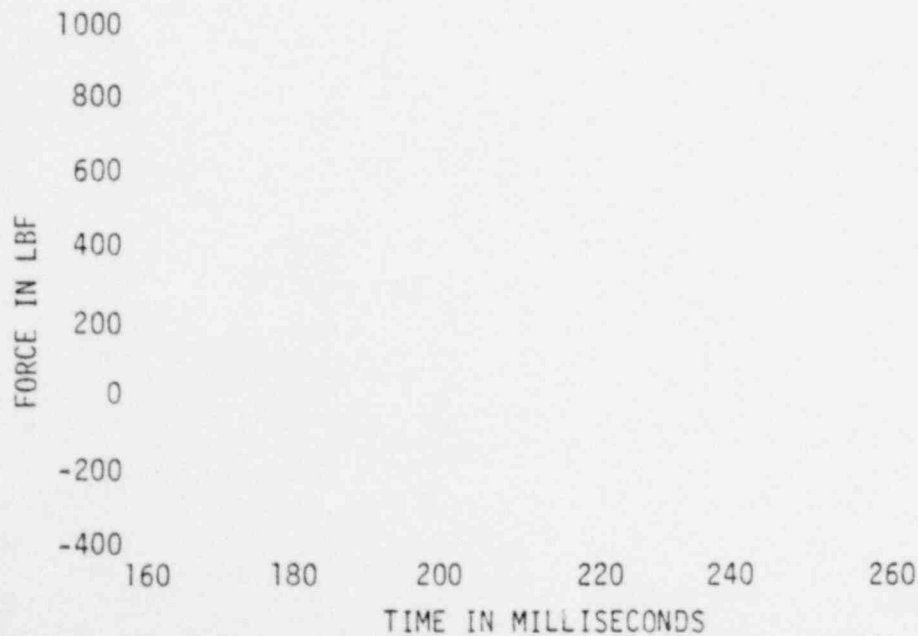
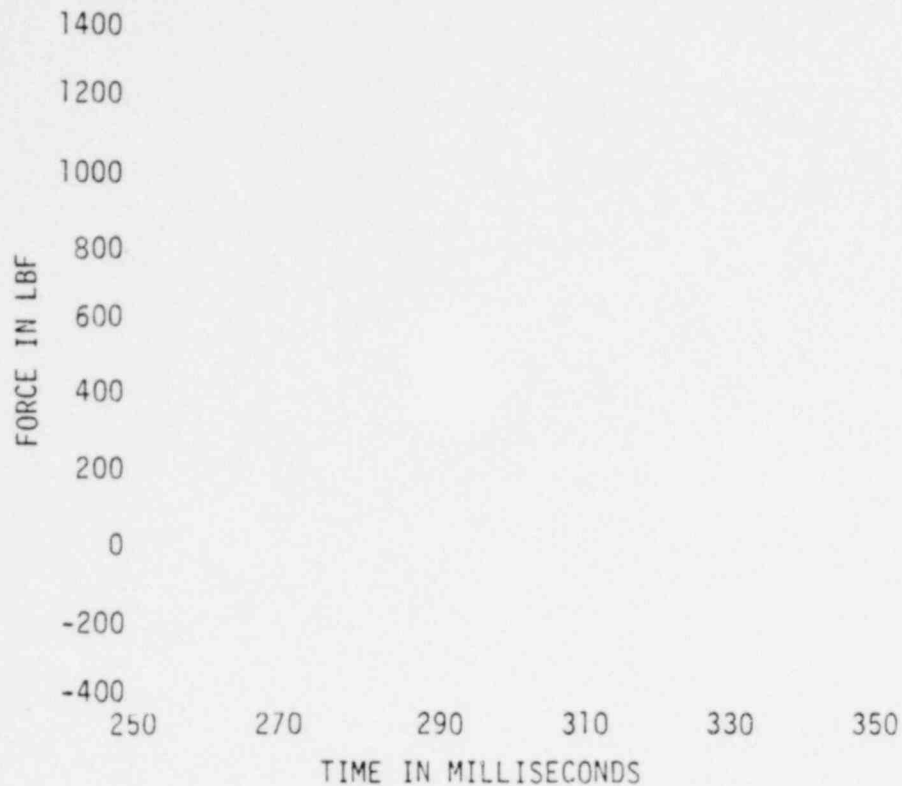
PRESSURE IN PSIA

A-39

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FIGURE A-35

COMPARISON OF VENT HEADER IMPACT RESULTS  
(Corrected Load Cell and Pressure Integration)  
Task 5.5.3 Hatch 2 Tests 2, 6

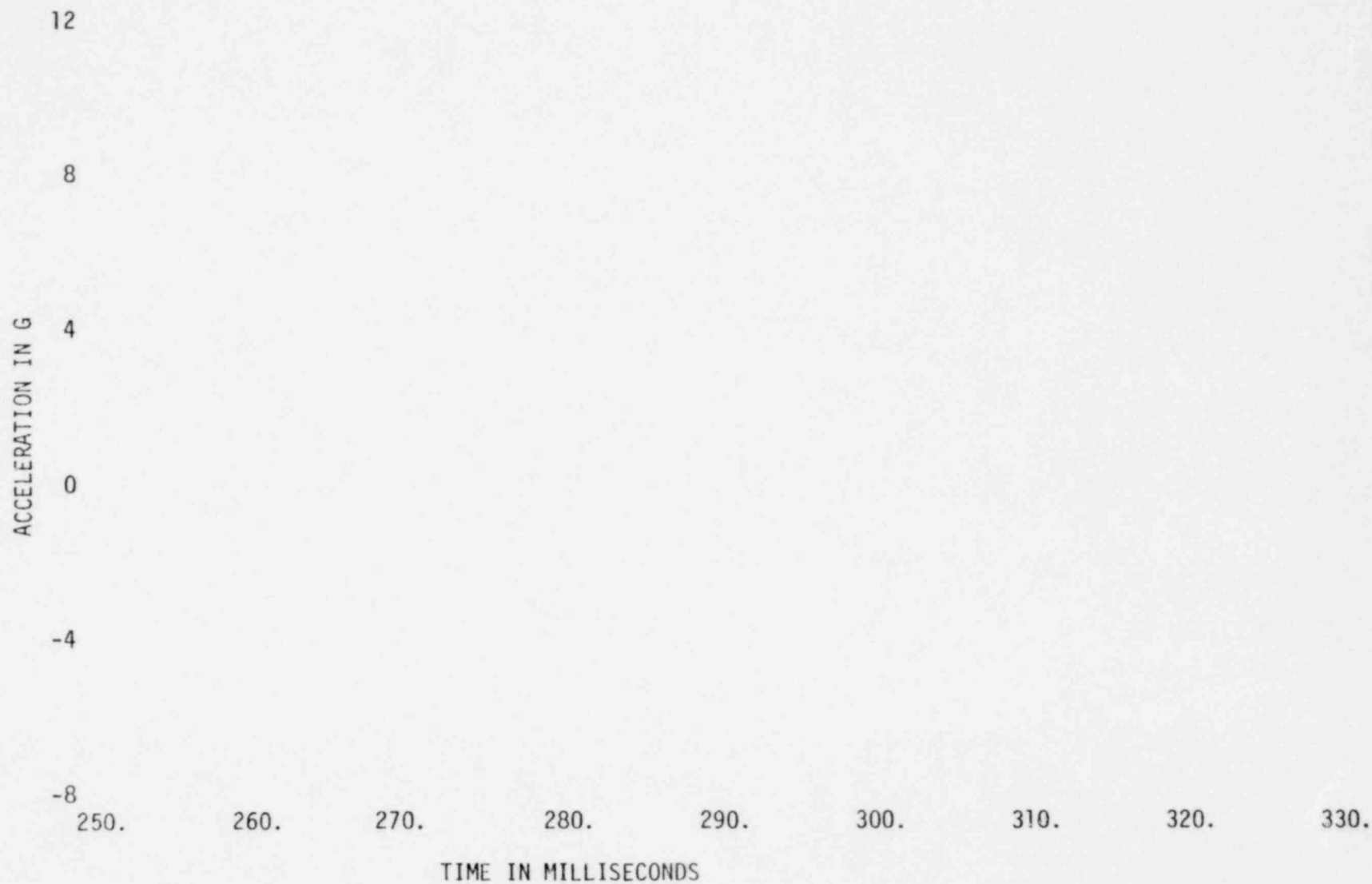


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FIGURE A-36

VENT HEADER VERTICAL ACCELERATION

Task 5.5.3-2 Hatch 2 Test 2



A-41

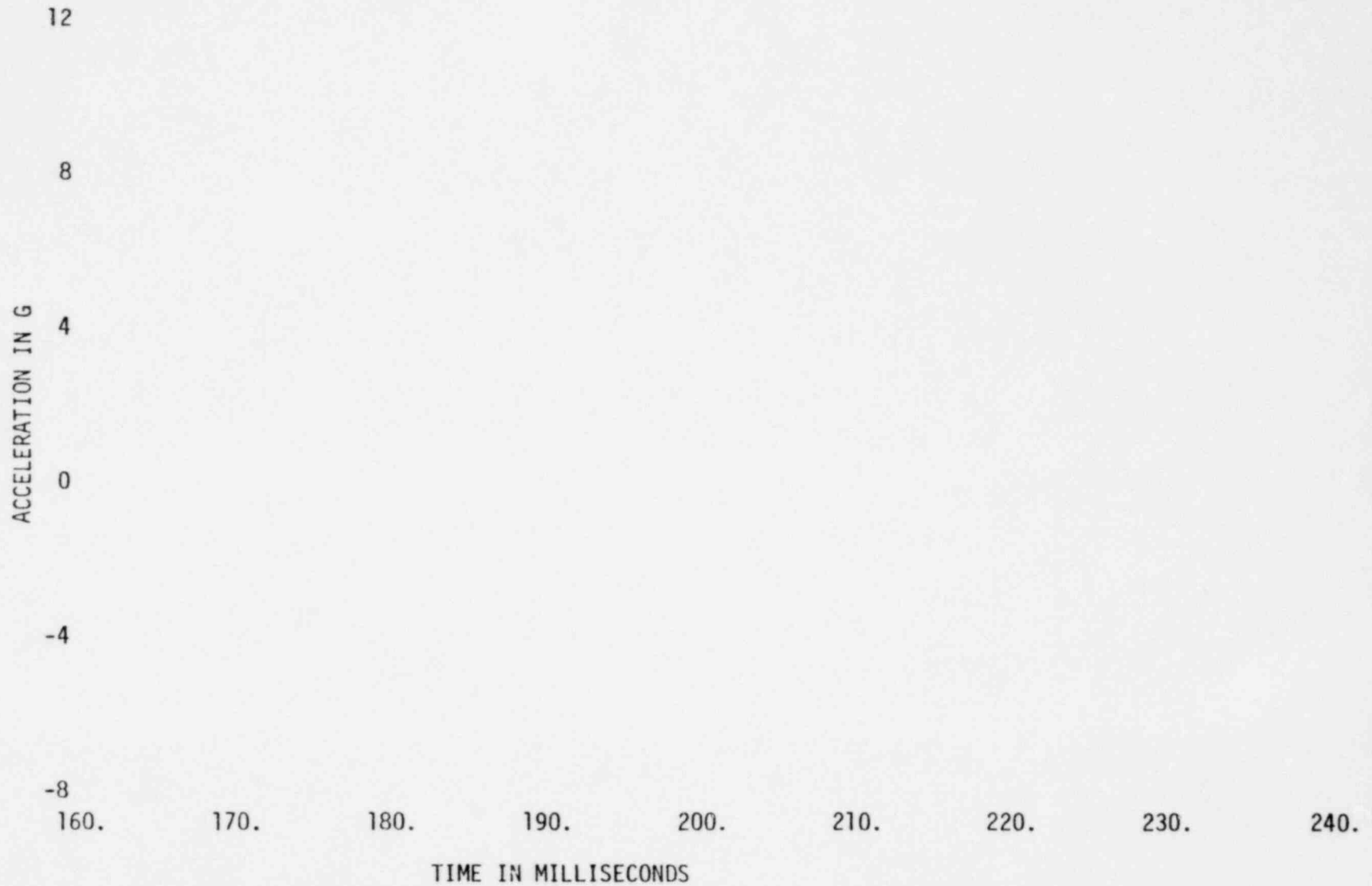
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FIGURE A-37

VENT HEADER VERTICAL ACCELERATION

Task 5.5.3-2 Hatch 2 Test 6



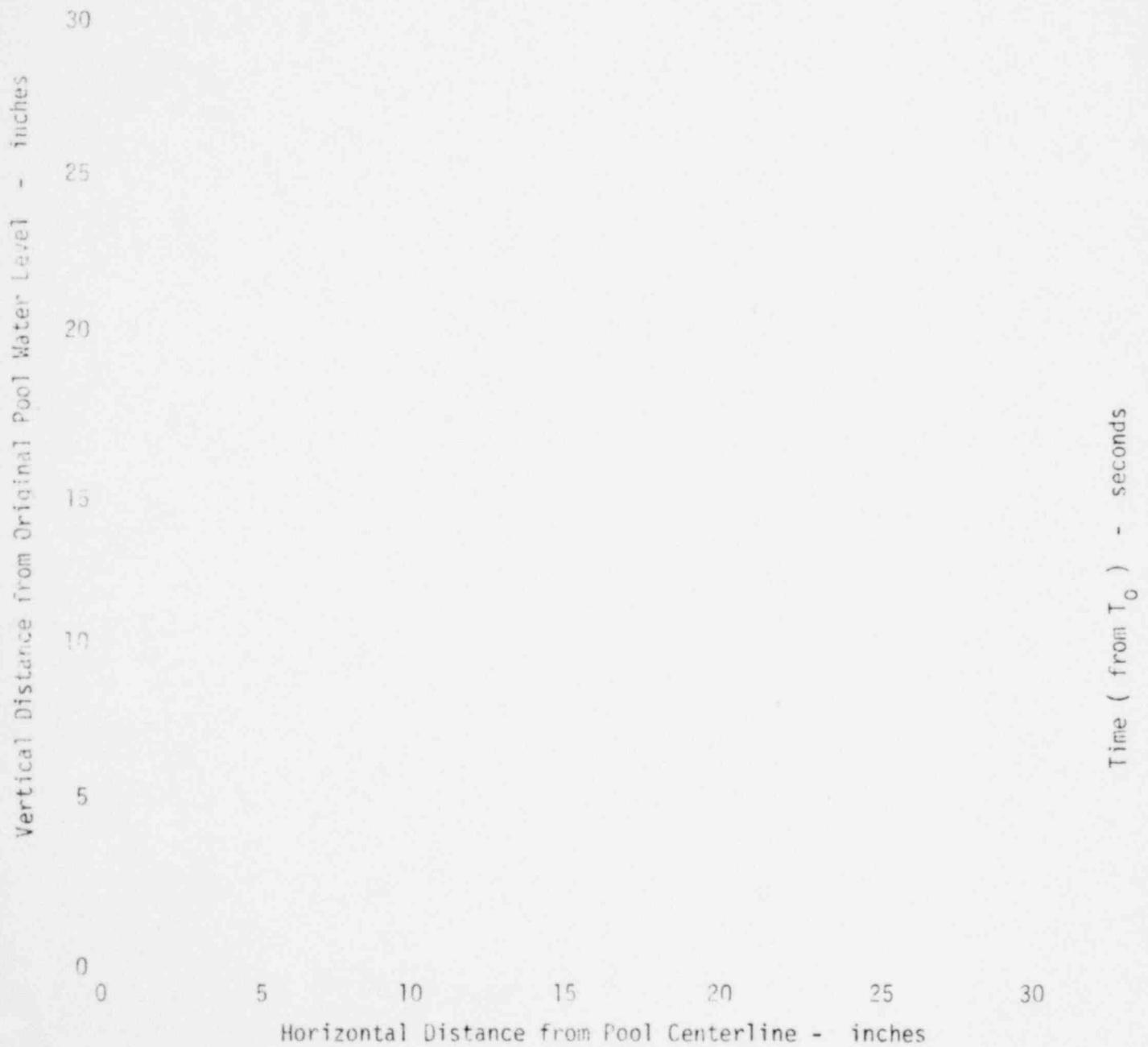
A-42

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Time History Of  
Pool Displacement

HATCH 2, TEST 1

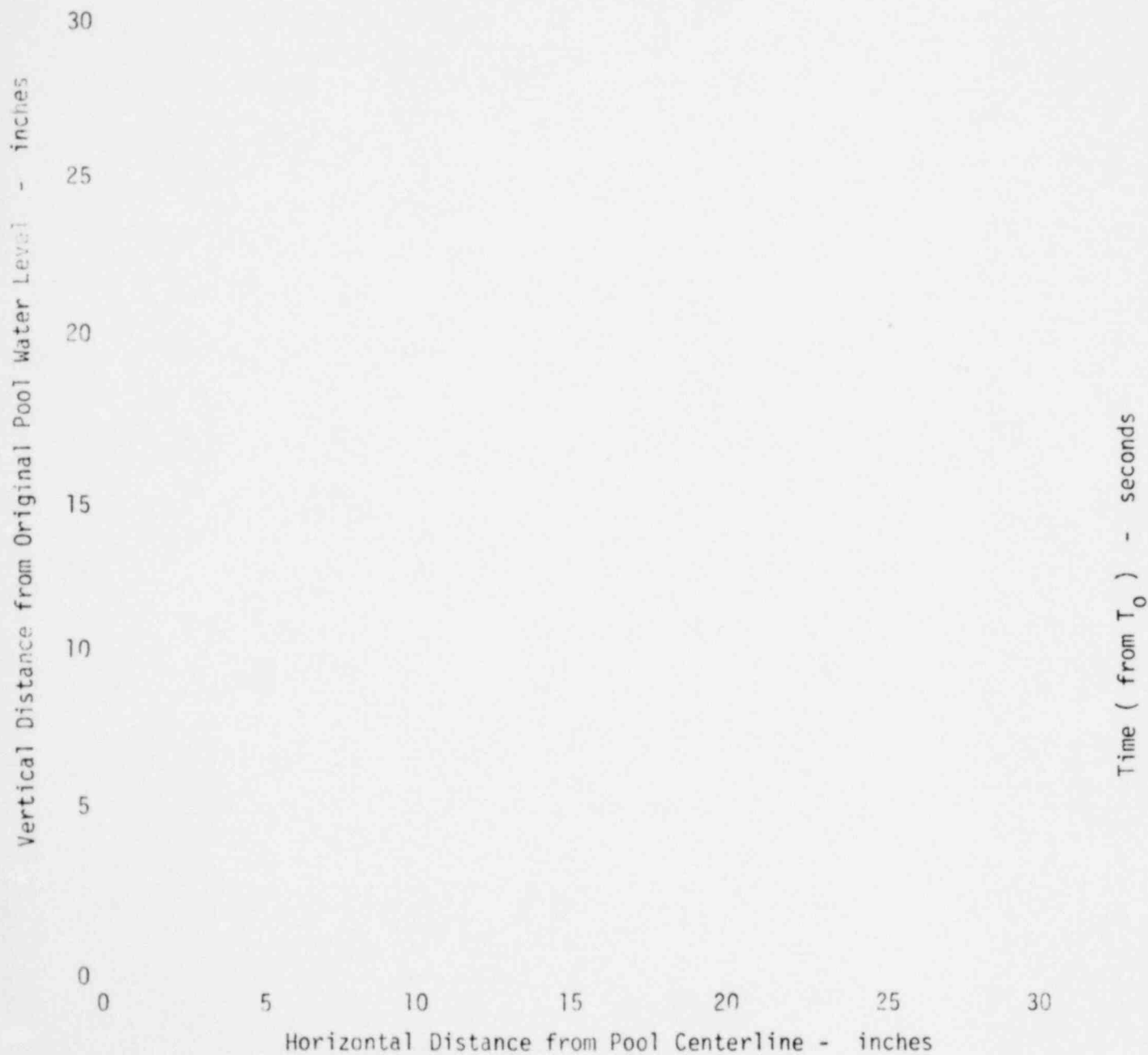


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FIGURE A-39

Time History Of  
Pool Displacement

HATCH 2, TEST 2



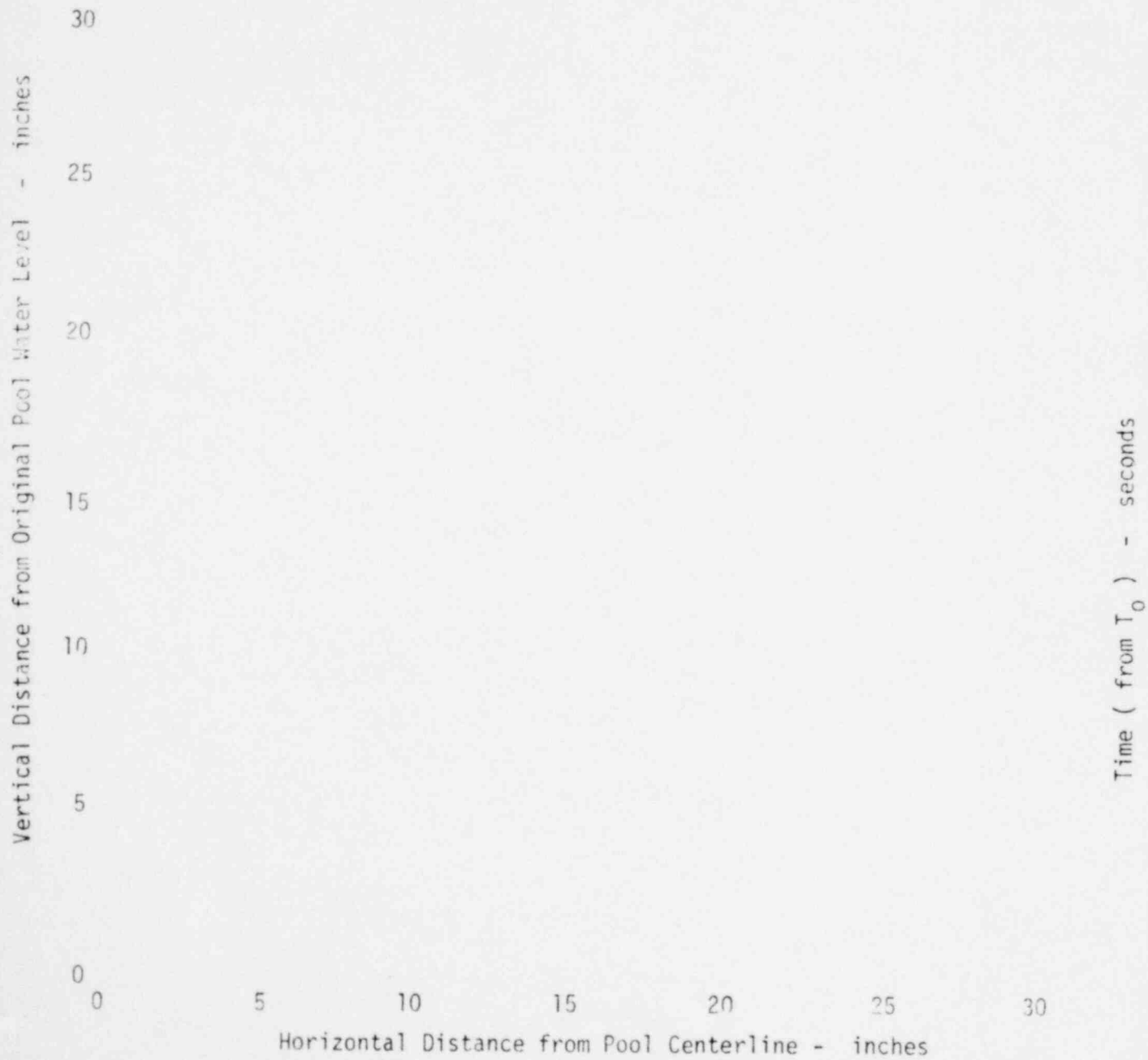
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FIGURE A-40

Time History Of  
Pool Displacement

HATCH 2, TEST 3



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FIGURE A-41

Time History Of  
Pool Displacement

HATCH 2, TEST 5



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FIGURE A-42

POOL SURFACE DISPLACEMENT

HATCH 2, TESTS 1, 2, 3

Height above original pool surface - inches

A-47

500

400

300

200

Time - milliseconds

1348 181  
0 100

NUCLEAR SERVICES CORPORATION

FIGURE A-43 40% SURFACE VELOCITY PROFILES

HATCH 2, TESTS 1, 2, 3

40

35

30

25

20

15

10

5

DISTANCE FROM POOL CENTERLINE - INCHES

0 0

1348 18

FIGURE A-44  
POOL SURFACE DISPLACEMENT

HATCH 2, TEST 5

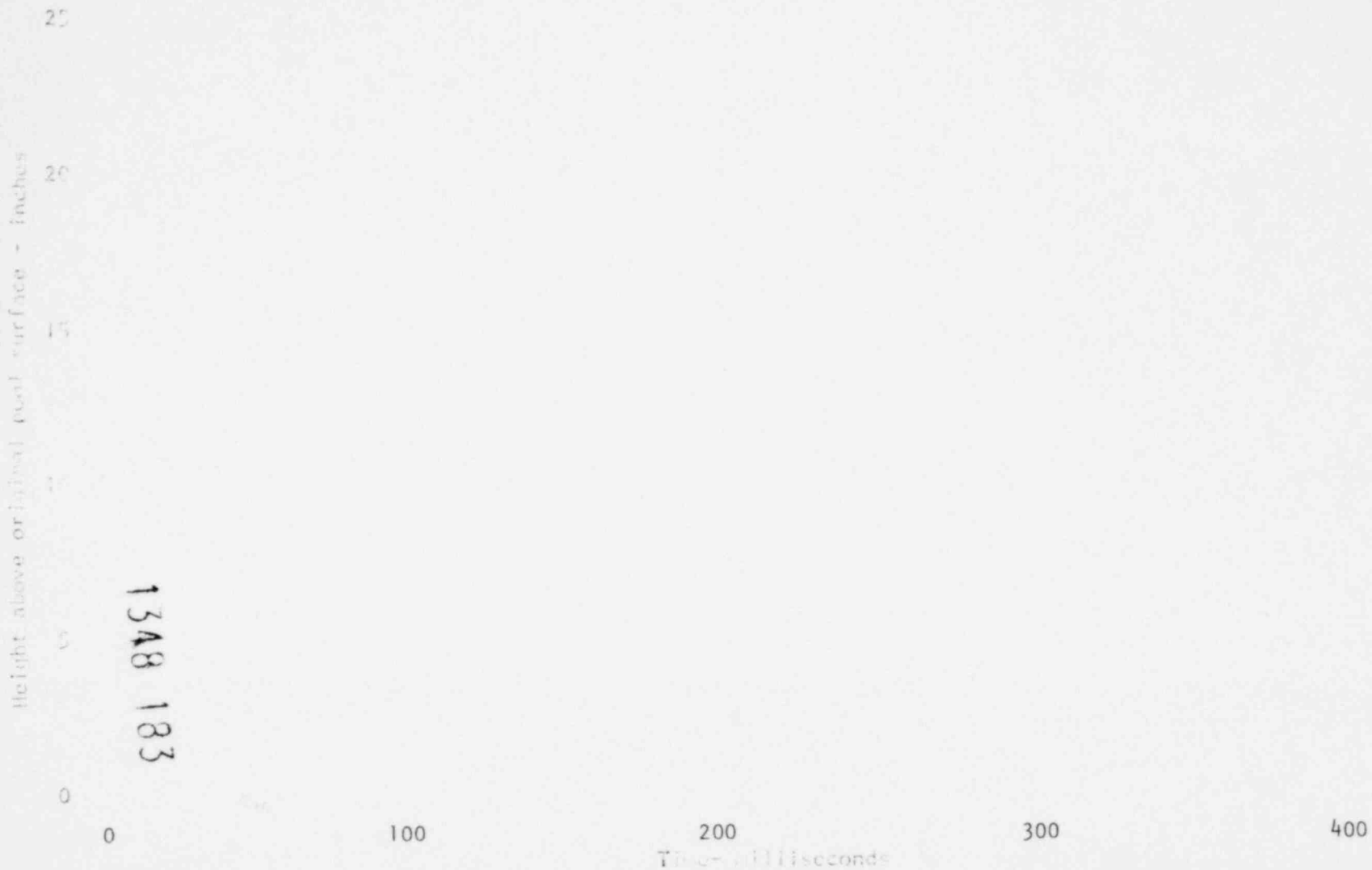


FIGURE A-45

POOL SURFACE VELOCITY PROFILES

HATCH 2, TEST 5

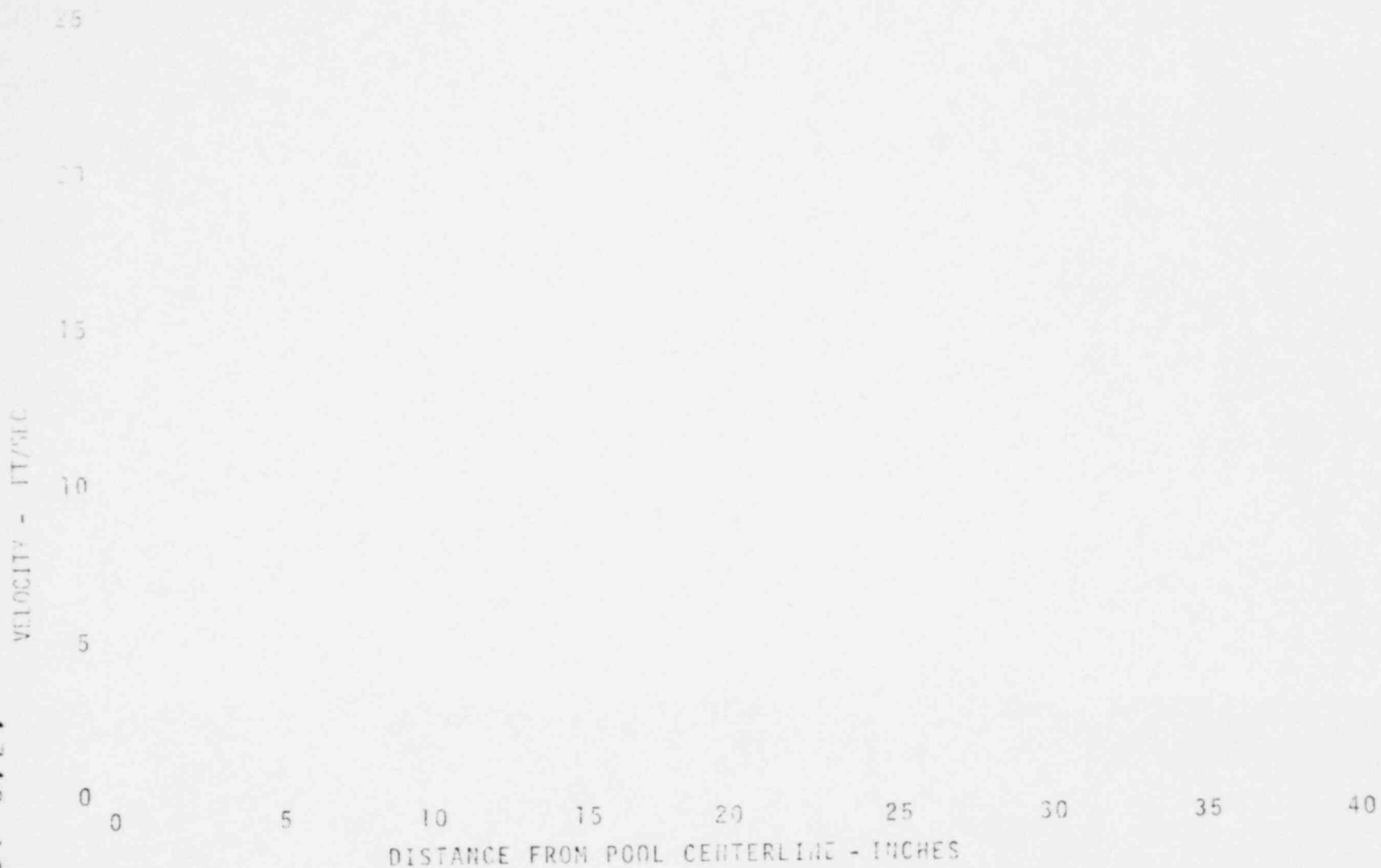


FIGURE A-46

SIDE WINDOW DISPLACEMENT AND VELOCITY PROFILES

HATCH 2, TEST 4

VERTICAL DISPLACEMENT - INCHES

12

8

4

0

-4

100

200

300

400

VERTICAL VELOCITY - FT/SEC

15.

10.

5.

0.

100

200

300

400

TIME - Seconds

A-51

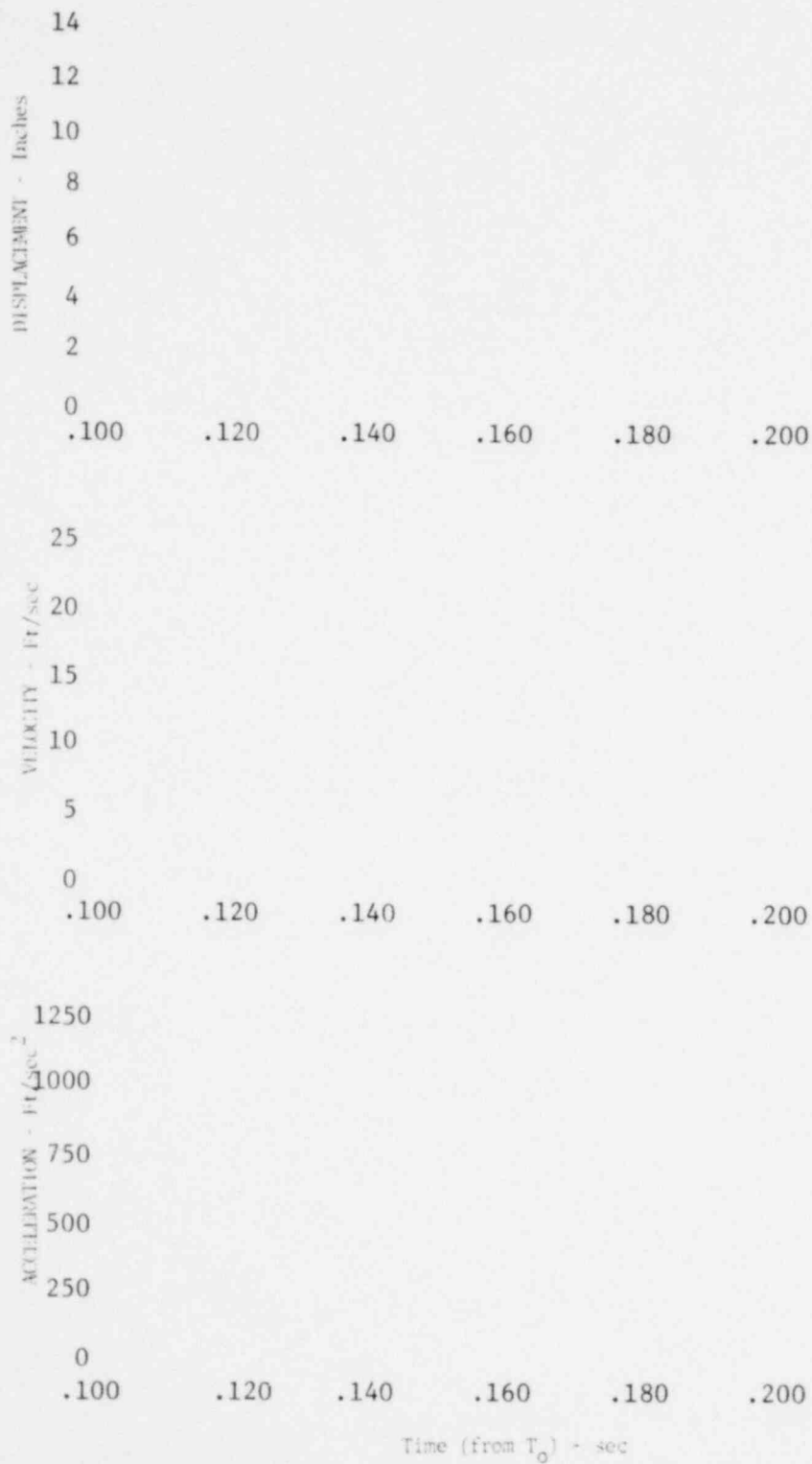
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FIGURE A-47

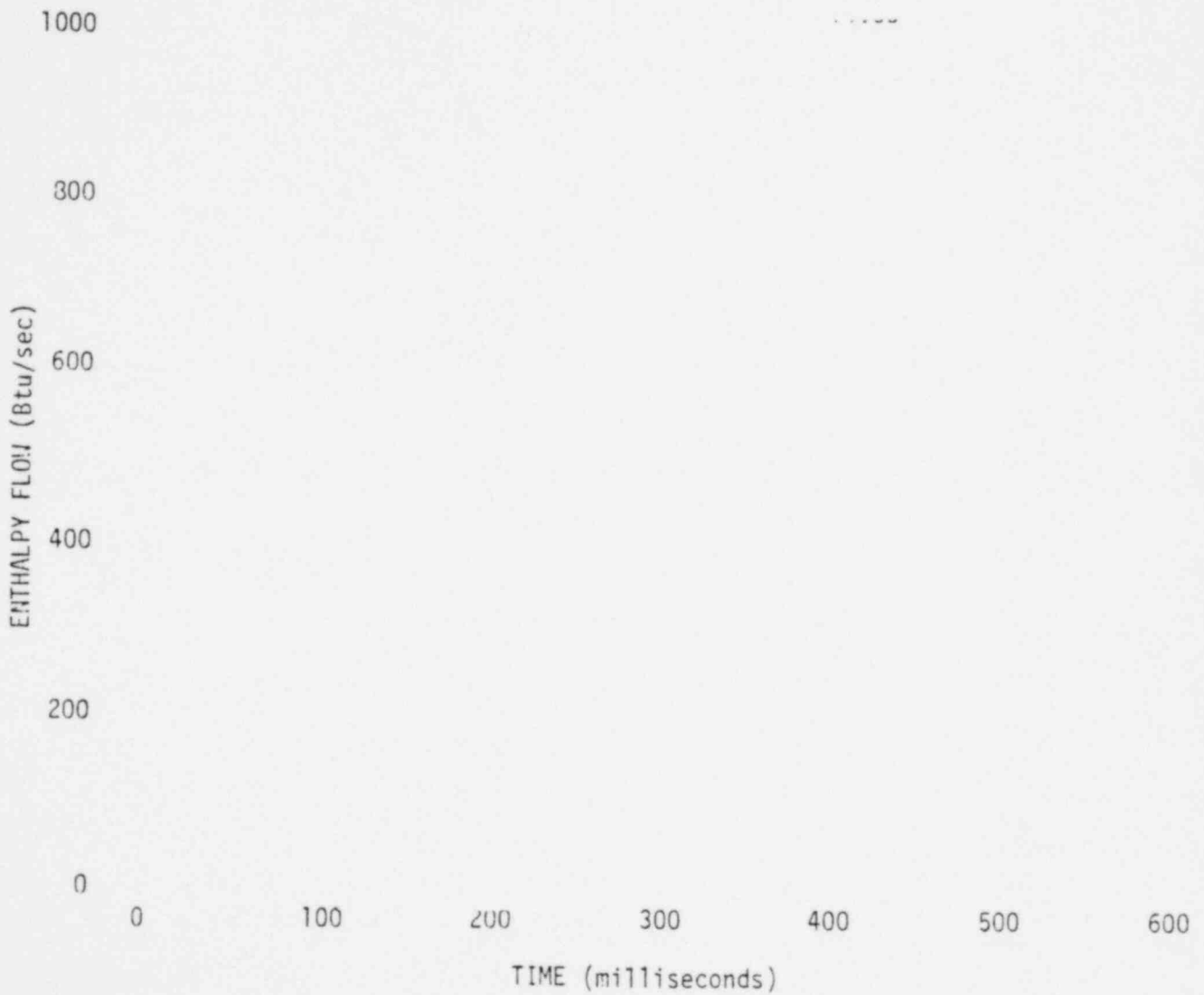
DOWNCOMER WATER SLUG EJECTION

HATCH 2, TEST 2



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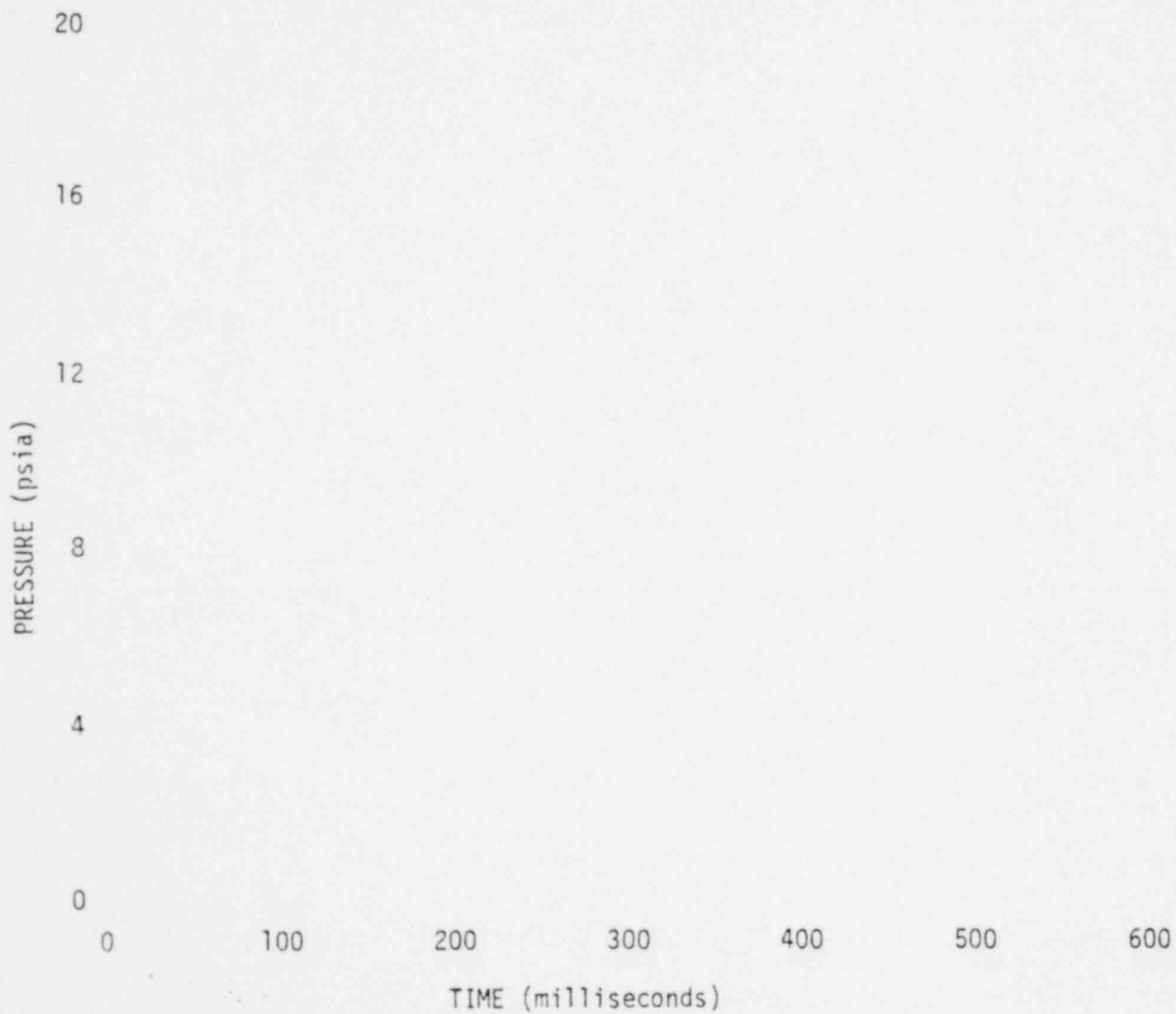
FIGURE A-48  
EFFECT OF DRYWELL/WETWELL  $\Delta P$  ON  
ENTHALPY FLOW INTO POOL  
Hatch 2 Tests



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FIGURE A-49

EFFECT OF DRYWELL/WETWELL  $\Delta P$  ON  
DOWNCOMER INTERNAL PRESSURE  
Hatch 2 Tests



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FIGURE A-50

EFFECT OF DRYWELL/WETWELL  $\Delta P$  ON POOL PRESSURE

AT 180 DEGREE AND FREESPACE PRESSURE

Hatch 2 Tests

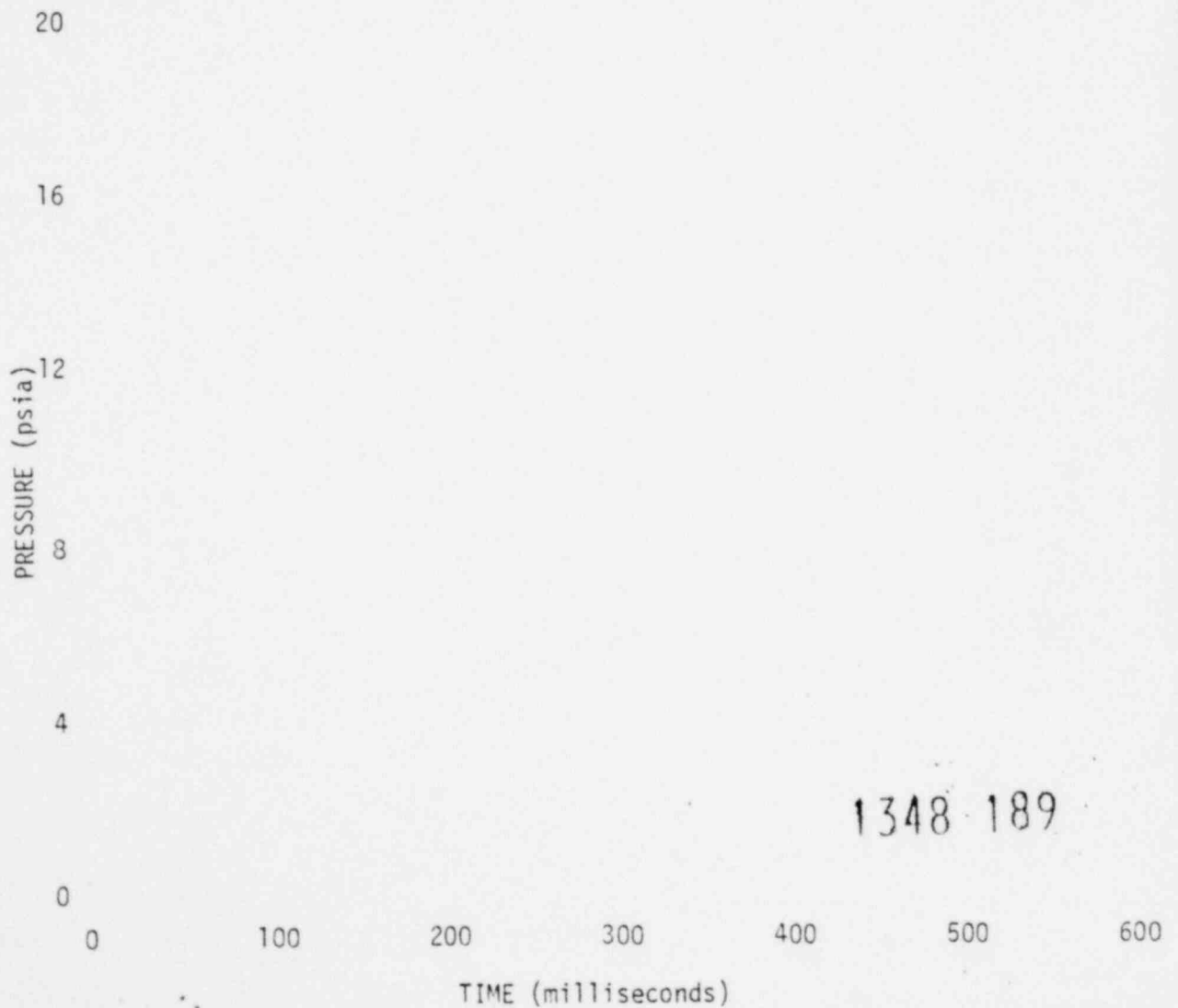


TABLE A-1  
DATA FOR WETWELL VERTICAL LOADS  
 Task 5.5.3-2 Hatch 2 Tests

\*Vent clearing time (from  $T_0$ ) determined from the movie films.

\*\*Time difference from  $T_0$  to time of zero downforce.

—No significant downforce valley or 2nd peak downforce.

\*(1) Start-of-test reference time

Parameter	Test No.	$\frac{Q''}{A} \Delta P$				Mean	Std. Dev.
		(1)	(2)	(3)	(4)		
*(1)							
$T_0$	(sec)						
Vent Clearing Time*	(sec)						
<u>Peak Downforce</u>							
Pressure Integral:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
Corrected Pressure Integral:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
Corrected Load Cell:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
<u>Downforce Valley</u>							
Pressure Integral:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
Corrected Pressure Integral:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
Corrected Load Cell:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
<u>2nd Peak Downforce</u>							
Pressure Integral:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
Corrected Pressure Integral:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
Corrected Load Cell:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
<u>[At] Downforce Time**</u>							
Pressure Integral	(sec)						
Corrected Pressure Integral	(sec)						
Corrected Load Cell	(sec)						
<u>Downforce Impulse</u>							
Pressure Integral:							
Impulse	(lb-sec)						

TABLE A-1 (Continued)  
 DATA FOR WETWELL VERTICAL LOADS (continued)

Task 5.5.3-2 Hatch 2 Tests

Parameter	Test No.	0" $\Delta P$				Mean	Std. Dev.
		(1)	(2)	(3)	(4)		
<u>Peak Upforce</u>							
Pressure Integral:							
Force (lb)	(1b)						
Time (from $T_0$ ) (sec)	(sec)						
Corrected Pressure Integral:							
Force (lb)	(1b)						
Time (from $T_0$ ) (sec)	(sec)						
Corrected Load Cell:							
Force (lb)	(1b)						
Time (from $T_0$ ) (sec)	(sec)						
<u>Upforce Valley</u>							
Pressure Integral:							
Force (lb)	(1b)						
Time (from $T_0$ ) (sec)	(sec)						
Corrected Pressure Integral:							
Force (lb)	(1b)						
Time (from $T_0$ ) (sec)	(sec)						
Corrected Load Cell:							
Force (lb)	(1b)						
Time (from $T_0$ ) (sec)	(sec)						
<u>2nd Peak Upforce</u>							
Pressure Integral:							
Force (lb)	(1b)						
Time (from $T_0$ ) (sec)	(sec)						
Corrected Pressure Integral:							
Force (lb)	(1b)						
Time (from $T_0$ ) (sec)	(sec)						
Corrected Load Cell:							
Force (lb)	(1b)						
Time (from $T_0$ ) (sec)	(sec)						
<u>Zero Force Time*</u>							
Pressure Integral (sec)	(sec)						
Corrected Pressure Integral (sec)	(sec)						
Corrected Load Cell (sec)	(sec)						

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TABLE A-2  
DATA FOR WETWELL VERTICAL LOADS  
 Task 5.5.3 -2 Hatch 2 Tests

\*Vent clearing time (from  $T_0$ ) determined from the movie films.  
 \*\*Time difference from  $T_0$  to time of zero downforce.  
 —No significant downforce valley or 2nd peak downforce.  
 \*(1) Start-of-test reference time

Parameter	Test No.	14.35" $\Delta P$				Mean	Std. Dev.
		(5)	(6)	(7)	(8)		
$T_0$ *(1)	(sec)						
Vent Clearing Time*	(sec)						
<u>Peak Downforce</u>							
Pressure Integral:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
Corrected Pressure Integral:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
Corrected Load Cell:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
<u>Downforce Valley</u>							
Pressure Integral:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
Corrected Pressure Integral:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
Corrected Load Cell:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
<u>2nd Peak Downforce</u>							
Pressure Integral:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
Corrected Pressure Integral:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
Corrected Load Cell:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
<u>[<math>\Delta t</math>] Downforce Time**</u>							
Pressure Integral	(sec)						
Corrected Pressure Integral	(sec)						
Corrected Load Cell	(sec)						
<u>Downforce Impulse</u>							
Pressure Integral:							
Impulse	(lb-sec)						

TABLE A-2 (Continued)  
DATA FOR WETWELL VERTICAL LOADS (continued)

Task 5.5.3-2 Hatch 2 Tests

Parameter \ Test No.	14.35" $\Delta P$				Mean	Std. Dev.
	(5)	(6)	(7)	(8)		
<u>Peak Upforce</u>						
Pressure Integral:						
Force (lb)						
Time (from $T_0$ ) (sec)						
Corrected Pressure Integral:						
Force (lb)						
Time (from $T_0$ ) (sec)						
Corrected Load Cell:						
Force (lb)						
Time (from $T_0$ ) (sec)						
<u>Upforce Valley</u>						
Pressure Integral:						
Force (lb)						
Time (from $T_0$ ) (sec)						
Corrected Pressure Integral:						
Force (lb)						
Time (from $T_0$ ) (sec)						
Corrected Load Cell:						
Force (lb)						
Time (from $T_0$ ) (sec)						
<u>2nd Peak Upforce</u>						
Pressure Integral:						
Force (lb)						
Time (from $T_0$ ) (sec)						
Corrected Pressure Integral:						
Force (lb)						
Time (from $T_0$ ) (sec)						
Corrected Load Cell:						
Force (lb)						
Time (from $T_0$ ) (sec)						
<u>Zero Force Time*</u>						
Pressure Integral (sec)						
Corrected Pressure Integral (sec)						
Corrected Load Cell (sec)						

1348 193

TABLE A-3

## DATA FOR VENT HEADER IMPACT LOADS

## Task 5.5.2-2 Hatch 2 Tests

Parameter \ Test No.	0" $\Delta P$				Mean	Std. Dev.
	( 1 )	( 2 )	( 3 )	( 4 )		
$T_0$ + (sec)						
Vent Header Impact						
Pressure Integral:						
Maximum Force (lb)						
Impulse (lb-sec)						
Duration* (sec)						
Load Cell Corrected: ++						
Maximum Force (lb)						
Impulse (lb-sec)						
Duration (sec)						
Pool Surface Velocity (ft/sec)						
Time (from $T_0$ )** (sec)						

\*(2) Offset 6" from pool centerline

\* Based on impact pressure measurements

\*\* At start of the first impact pressure recorded

+ Start of reference time

++ represents peak of very noisy data (acceleration corrected); mean value would be lower

1348 194

TABLE A-3a

DATA FOR VENT HEADER IMPACT LOADS

Task 5.5.3-2 Hatch 2 Tests

Parameter	Test No.	14.35" $\Delta P$					Std. Dev.
		( 5 )	( 6 )	( 7 )	( 8 )	Mean	
$T_{ot}$	(sec)						
<u>Vent Header Impact</u>							
Pressure Integral:							
Maximum Force	(lb)						
Impulse	(lb-sec)						
Duration*	(sec)						
Load Cell Corrected: $\dagger\dagger$							
Maximum Force	(lb)						
Impulse	(lb-sec)						
Duration	(sec)						
Pool Surface Velocity	(ft/sec)						
Time (from $T_o$ )**	(sec)						

\*(2) Offset 6" from pool centerline

\* Based on impact pressure measurements

\*\* At start of the first impact pressure recorded

+ Start of reference time

 $\dagger\dagger$  represents peak of very noisy data (acceleration corrected);  
mean value would be lower

1348 195

## A.2 Pilgrim Tests

### A.2.1 Typical Data

Time-history plots of the driving conditions and pool response are presented in this section for Pilgrim Tests 3 and 5. Test 3 was a load definition test which was conducted at a partial drywell/wetwell differential pressure of 10.9"  $\Delta P$  and with a 4.20 inch pipe deflector (16 inch full scale). Test 5 was conducted without an initial drywell/wetwell differential pressure (0"  $\Delta P$ ) and with the same 4.20 inch pipe deflector.

#### A.2.1.1 Driving Conditions

Driving conditions for Pilgrim Test 3 are presented in Figures A-51 through A-55. Similar plots for Pilgrim Test 5 are shown in Figures A-56 through A-60. Pilgrim's driving conditions had the same characteristics as the "typical" plant discussed in Section 3.0 of this report.

#### A.2.1.2 Pool Response

Downcomer internal pressure and wetwell pressure for Pilgrim Tests 3 and 5 are presented in Figures A-61 through A-62 and A-63 through A-64, respectively. These pressure plots have the same characteristics as the "typical" plant in Section 3.0. However, the characteristic one cycle oscillation of the downcomer internal pressure is negligibly small at 0"  $H_2O$   $\Delta P$ .

Figures A-65 and A-66 present net torus force based on the torus pressure integral for Pilgrim Tests 3 and 5, respectively. The net torus forces show no or very little oscillations in downforce but show some oscillations in upforce.

1348 196

The net torus force which was determined by applying the inertial correction from the torus accelerometer (Figures A-68 and A-70) to the torus load cell (Figures A-67 and A-69) is compared with the torus force obtained from the torus pressure integral in Figures A-71 and A-72. Residual oscillations are present in the corrected load cell. Figures A-73 and A-74 present the net torus force based on the torus pressure integral corrected for inertia.

The "average" pool pressures for Pilgrim Tests 3 and 5 are shown in Figures A-75 and A-77. Figures A-76 and A-78 are the same as Figures A-73 and A-74 with force replaced by average pressure (force/torus projected area).

The vent header impact pressures for Pilgrim Test 3 are presented in Figures A-79 through A-81. Vent header pressures for Pilgrim Test 5 are presented in Figures A-82 through A-84. These figures indicate that the deflector was effective in reducing the peak local vent header impact pressure.

Figure A-85 presents a comparison of the vent header impact force derived from the pressure integral with that derived from the corrected load cell. Vent header vertical accelerations from Tests 3 and 5 are shown in Figures A-86 and A-87, respectively.

#### A.2.2 Pool Dynamics

The pool contours at various times of pool swell are shown in Figures A-88 through A-91 for Pilgrim Tests 1, 2, 3, and 5.

The pool surface displacement curves for Tests 1, 2, and 3 are shown on Figure A-92. The pool surface velocities for Tests 1, 2, and 3 are shown on Figure A-93. The pool surface displacement graph and pool surface velocity profiles for Test 5 are shown in Figures A-94 and A-95, respectively.

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The pool surface displacements and velocity profile viewed from the side window during Test 4 are shown in Figure A-96. The downcomer water slug displacement, velocity, and acceleration versus time for Tests 3 and 5 are presented in Figures A-97 and A-98.

Pilgrim pool dynamics are similar to those of the "typical" plant discussed in Section 3.0.

#### A.2.3 Data Summaries

Table A-4 presents the Pilgrim test data for wetwell vertical forces.

Table A-5 presents the Pilgrim test data for vent header impact forces.

#### A.2.4 Discussion and Analysis

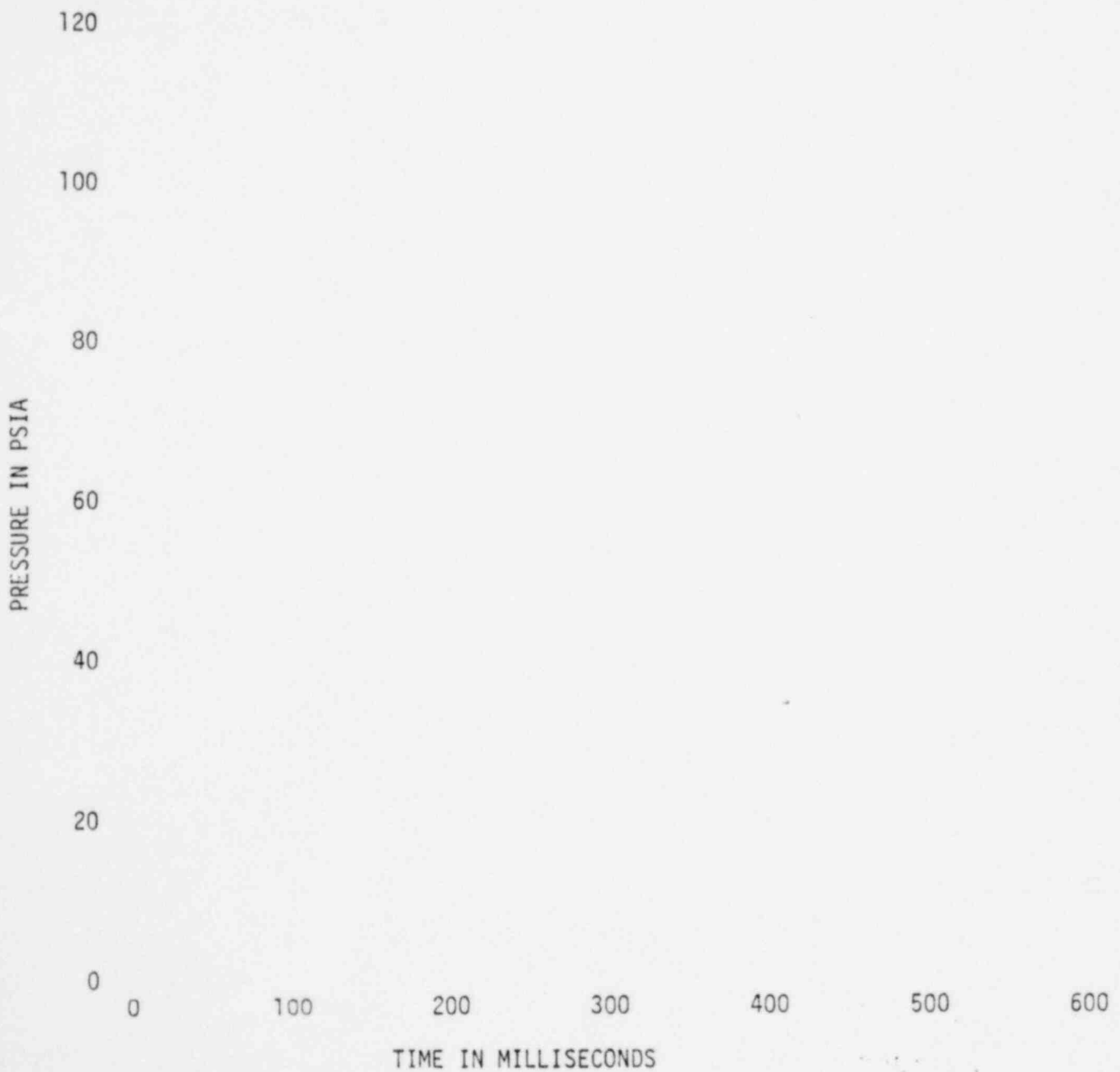
Figure A-99 presents the effect of drywell/wetwell  $\Delta P$  on enthalpy flow into the bubbles. Effect of drywell/wetwell  $\Delta P$  on downcomer internal pressure is shown in Figure A-100. Figure A-101 presents the effect of drywell/wetwell  $\Delta P$  on pool and freespace pressures. The data for Pilgrim parallels that for the "typical" plant in Section 3.0.

The Pilgrim load definition tests were conducted at 10.9"  $H_2O$   $\Delta P$  and with a pipe deflector installed below the vent header. A  $\Delta P$  sensitivity test at 0"  $H_2O$   $\Delta P$  was also conducted. Downforce showed no or very little oscillations, but upforce showed some oscillations. The pipe deflector (16 inch full scale) effectively reduced vent header impact force.

FIGURE A-51

DRYWELL ORIFICE UPSTREAM PRESSURE

Task 5.5.3-2 Pilgrim Test 3



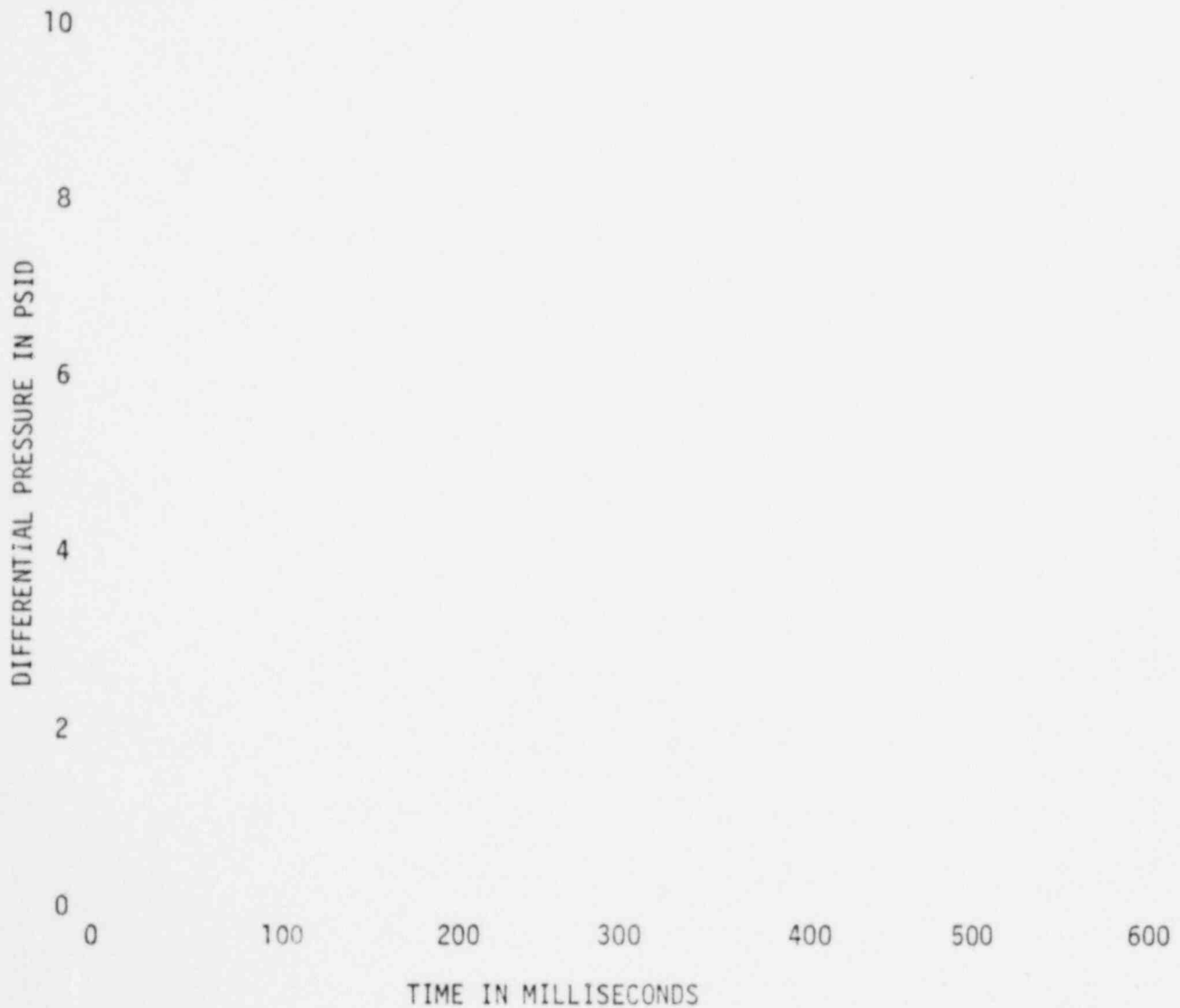
1348 199

FIGURE A-52  
DRYWELL PRESSURE  
Task 5.5.3-2 Pilgrim Test 3



1348 200

FIGURE A-53  
DOWNCOMER ORIFICE DIFFERENTIAL PRESSURE  
Task 5.5.3-2 Pilgrim Test 3



1348 201

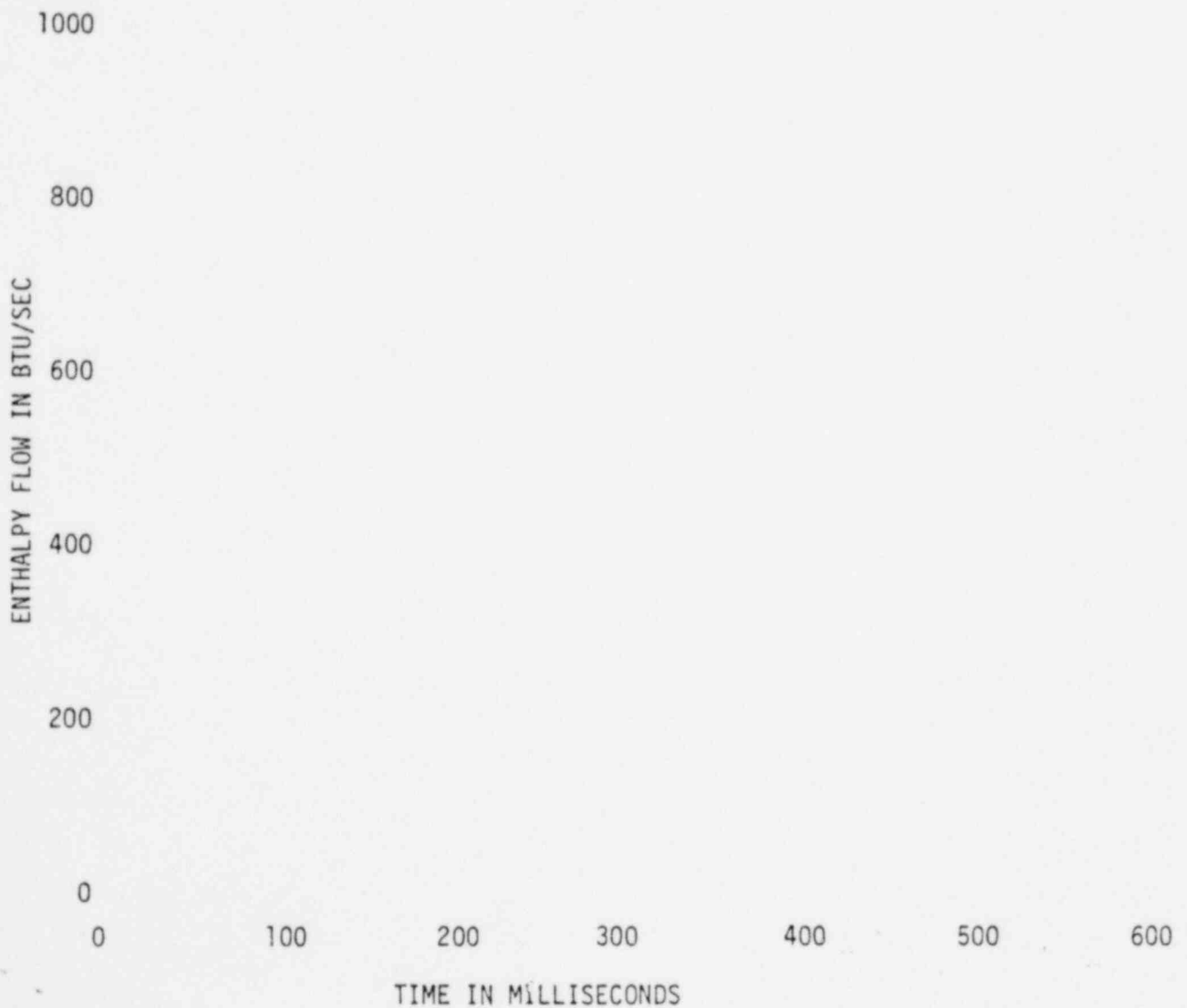
FIGURE A- 54  
DOWNCOMER ORIFICE UPSTREAM TEMPERATURE  
Task 5.5.3-2 Pilgrim Test 3



FIGURE A- 55

ENTHALPY FLOW INTO POOL

Task 5.5.3-2 Pilgrim Test 3

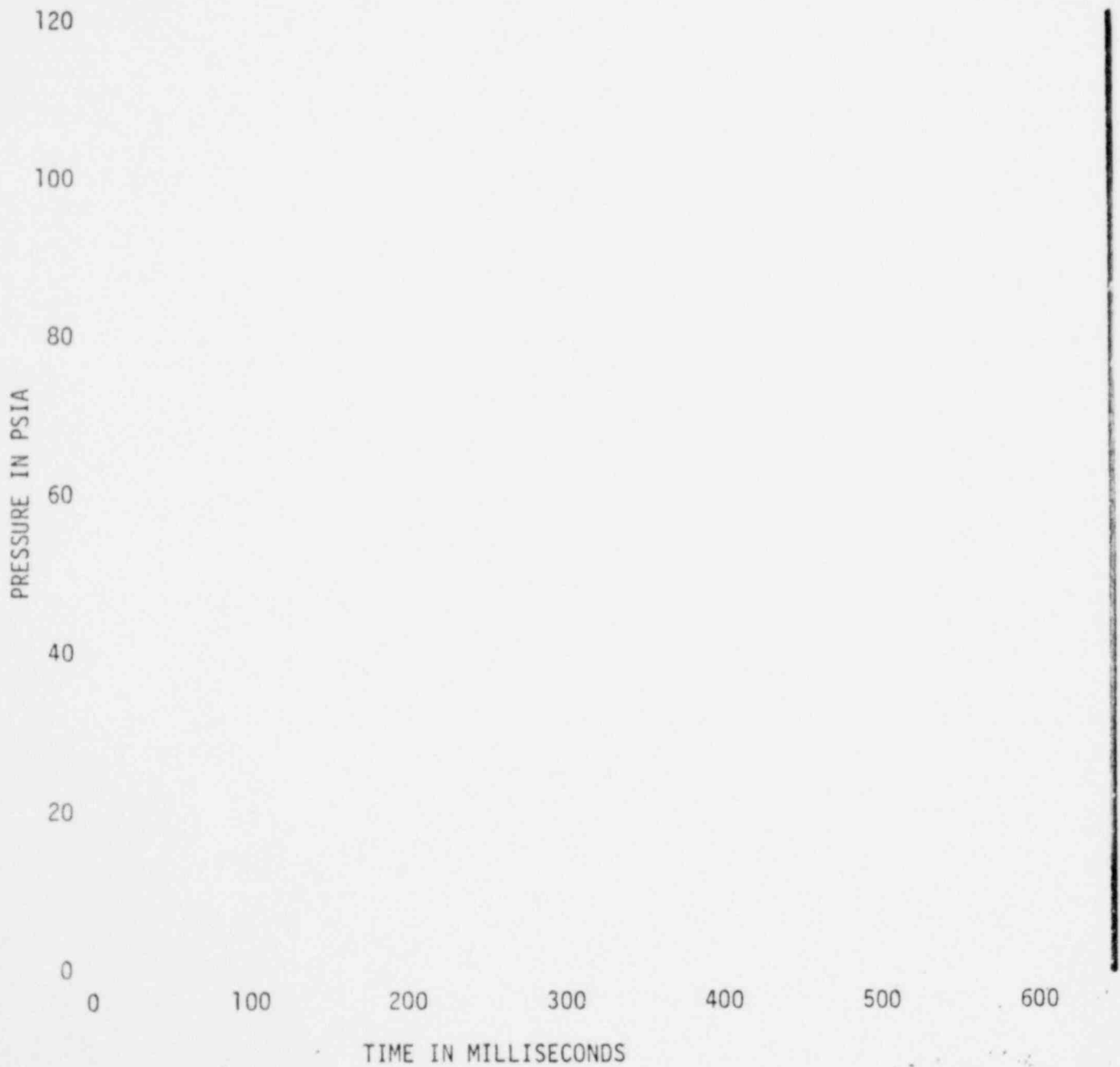


1348 203

FIGURE A- 56

DRYWELL ORIFICE UPSTREAM PRESSURE

Task 5.5.3-2 Pilgrim Test 5



1348 204

FIGURE A-57

DRYWELL PRESSURE

Task 5.5.3-2 Pilgrim Test 5



1348 205

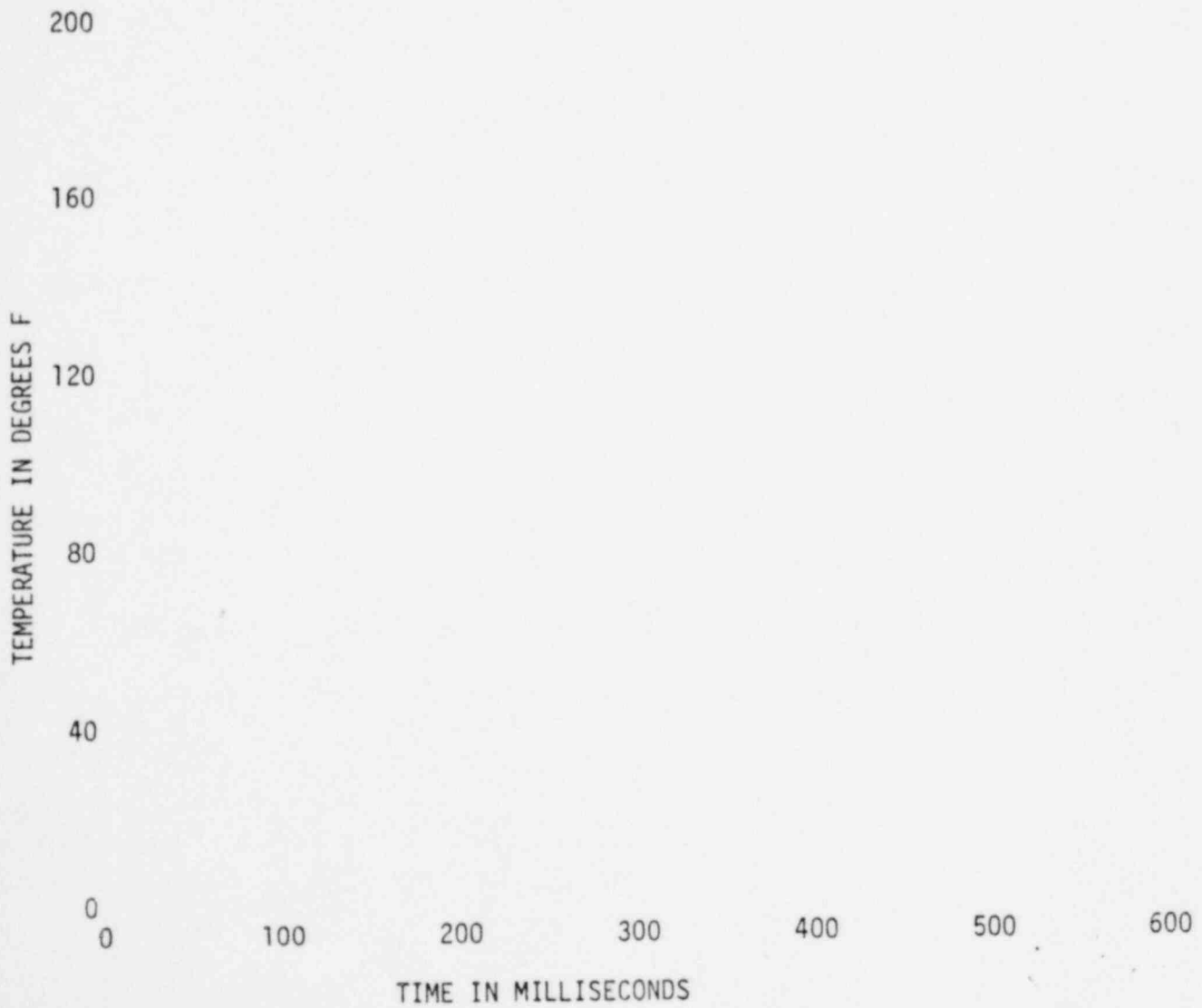
FIGURE A-58  
DOWNCOMER ORIFICE DIFFERENTIAL PRESSURE  
Task 5.5.3-2 Pilgrim Test 5



FIGURE A- 59

DOWNCOMER ORIFICE UPSTREAM TEMPERATURE

Task 5.5.3-2 Pilgrim Test 5

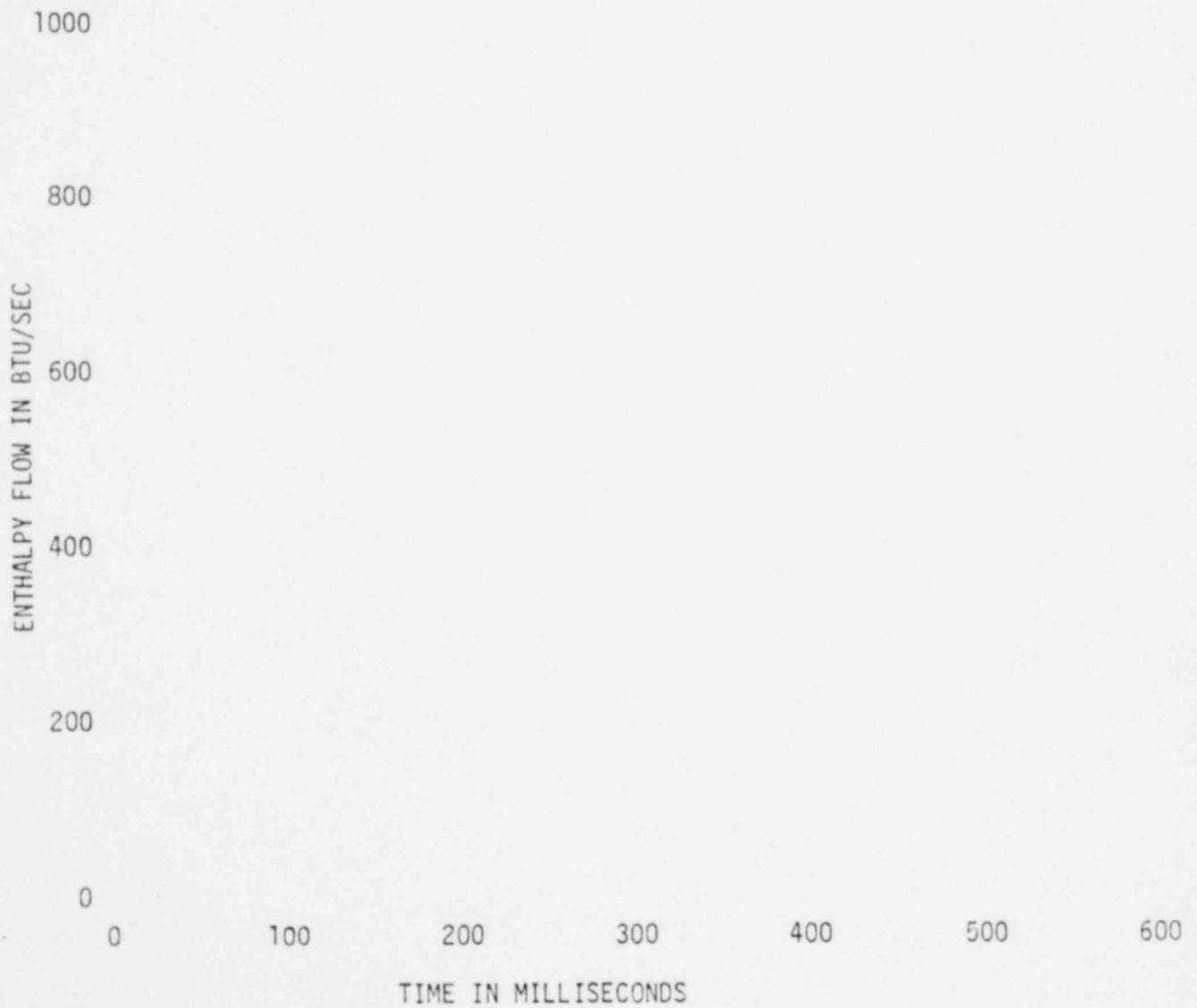


1348 207

FIGURE A-60

ENTHALPY FLOW INTO POOL

Task 5.5.3-2 Pilgrim Test 5



1348 208

FIGURE A-61

DOWNCOMER INTERNAL PRESSURE

Task 5.5.3-2 Pilgrim Test 3



1348 209

NEDO-21944

FIGURE A-62

WETWELL PRESSURES

Task 5.5.3-2 Pilgrim Test 3



1348 210

FIGURE A-63

DOWNCOMER INTERNAL PRESSURE

Task 5.5.3-2 Pilgrim Test 5

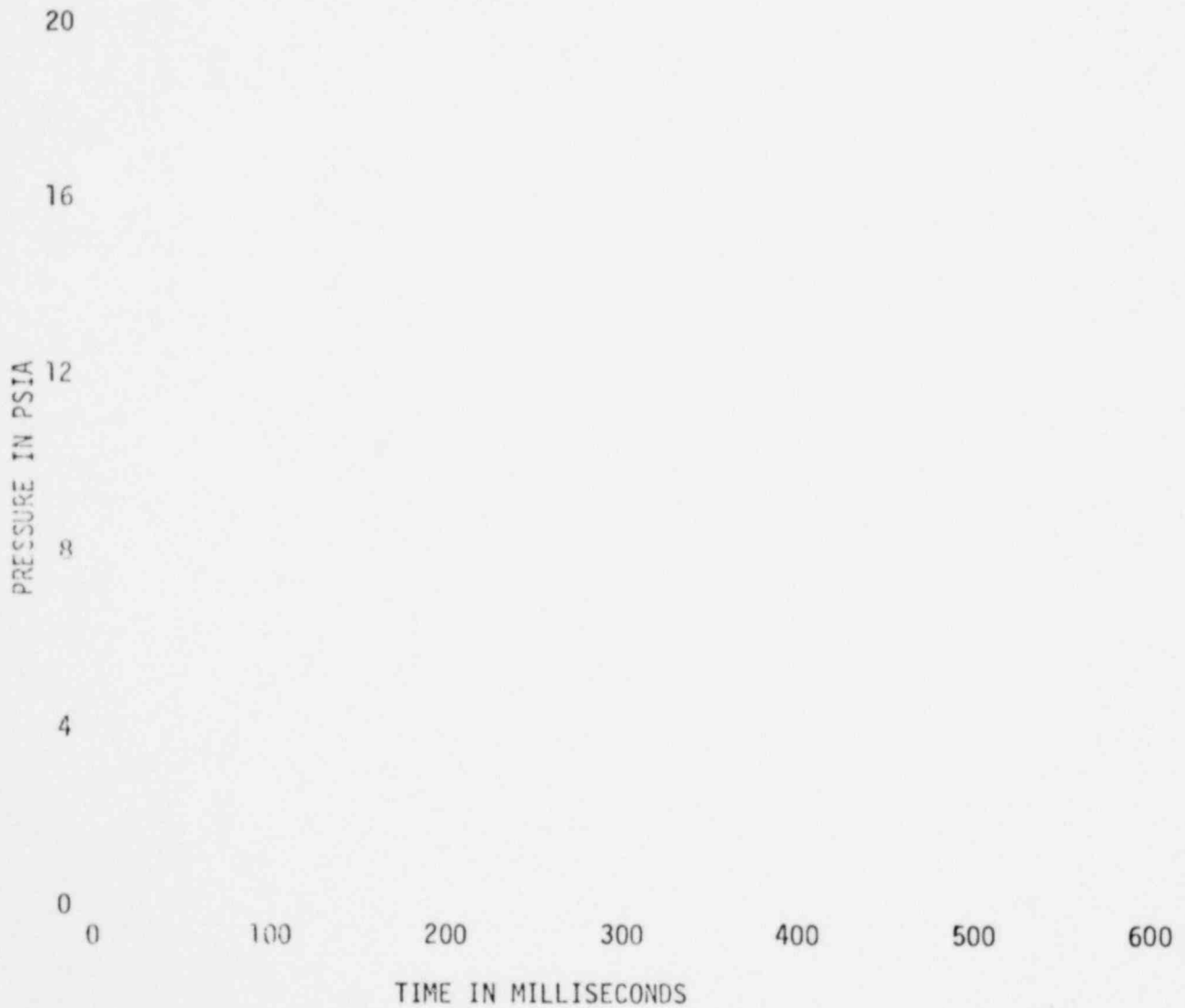


1348 211

NEDO-21944  
FIGURE A-64

WETWELL PRESSURES

Task 5.5.3-2 Pilgrim Test 5



1348-212

FIGURE A-65

NET TORUS FORCE FROM PRESSURE INTEGRAL

Task 5.5.3-2 Pilgrim Test 3

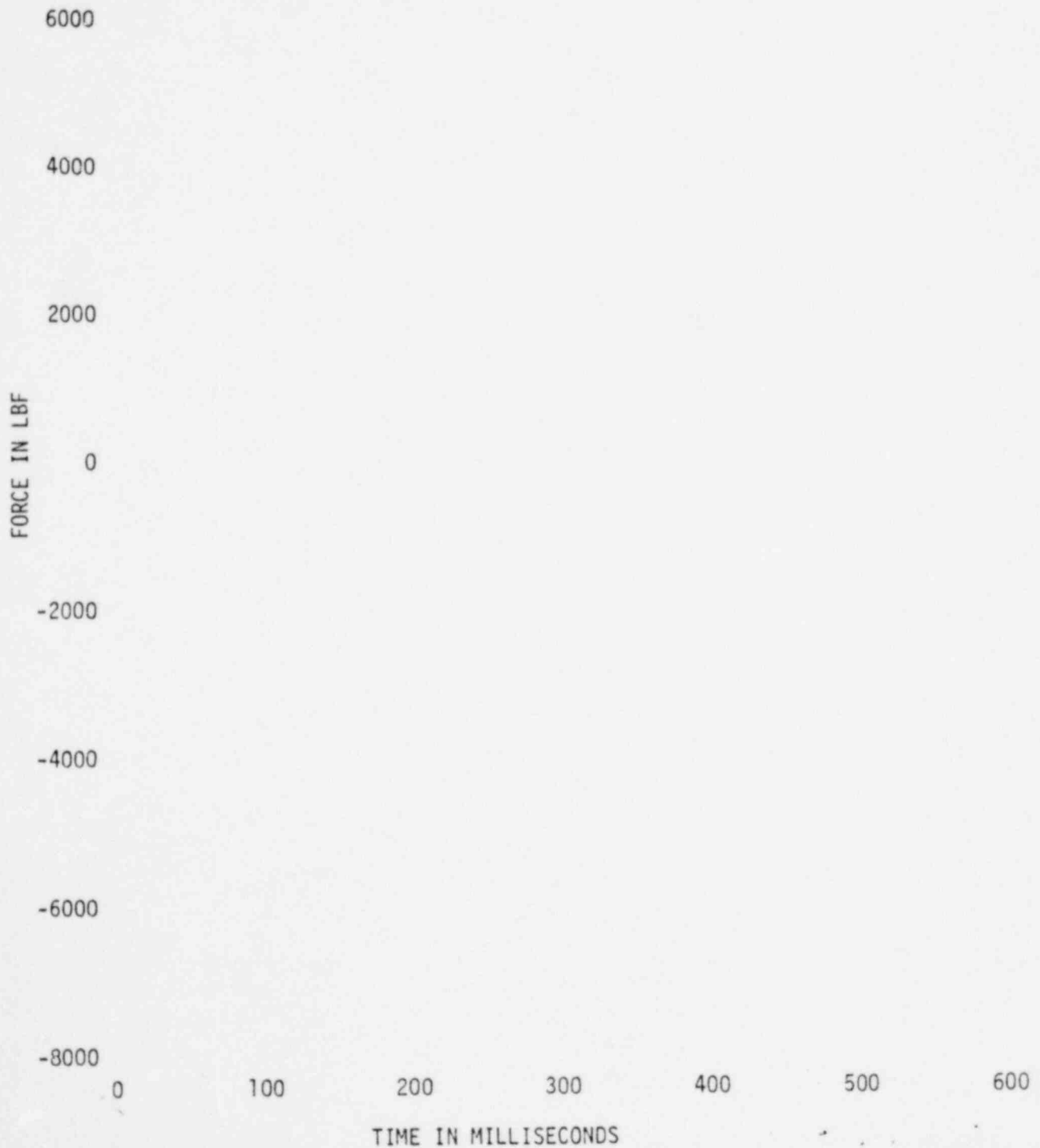
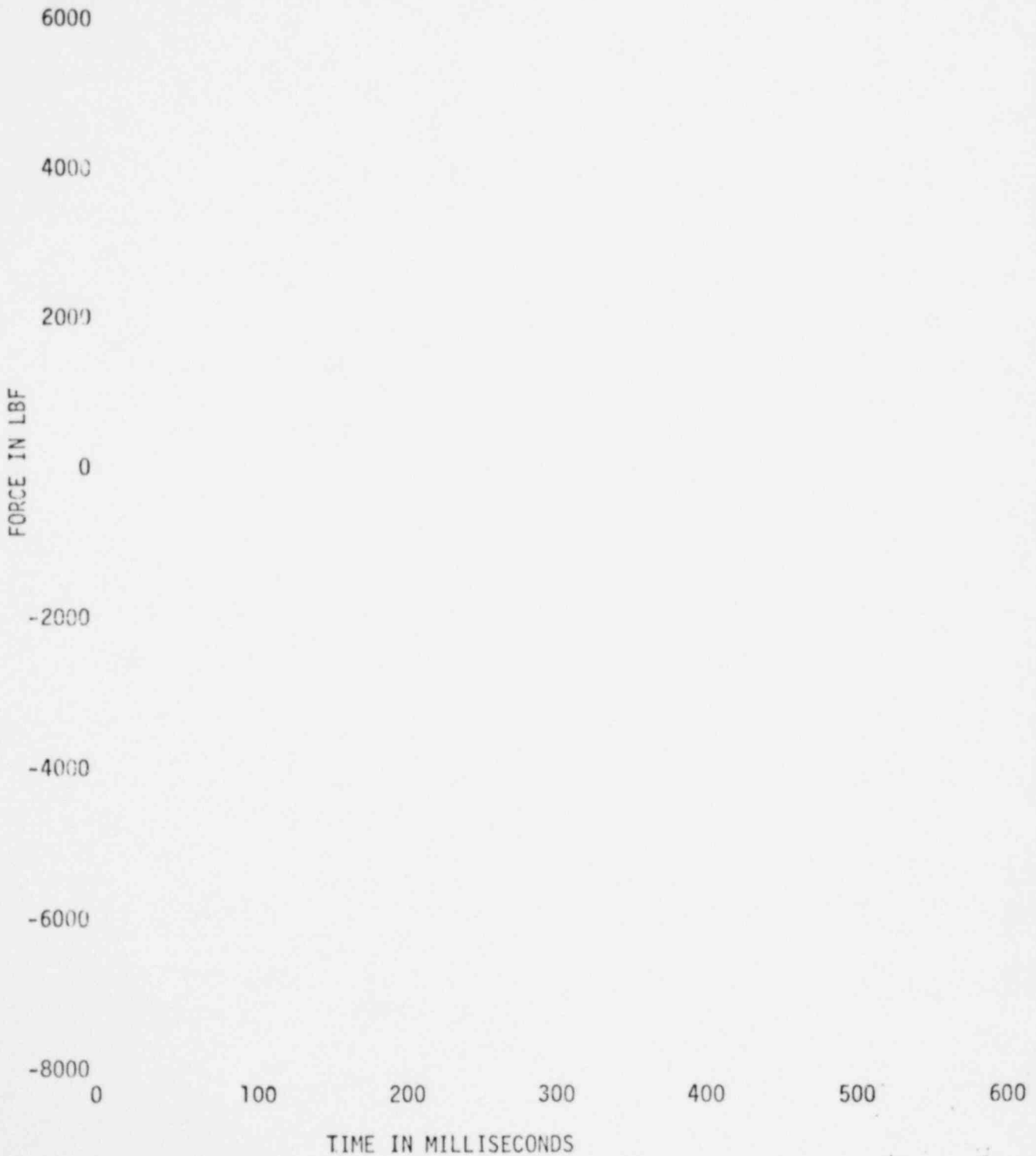


FIGURE A- 66

NET TORUS FORCE FROM PRESSURE INTEGRAL

Task 5.5.3-2 Pilgrim Test 5

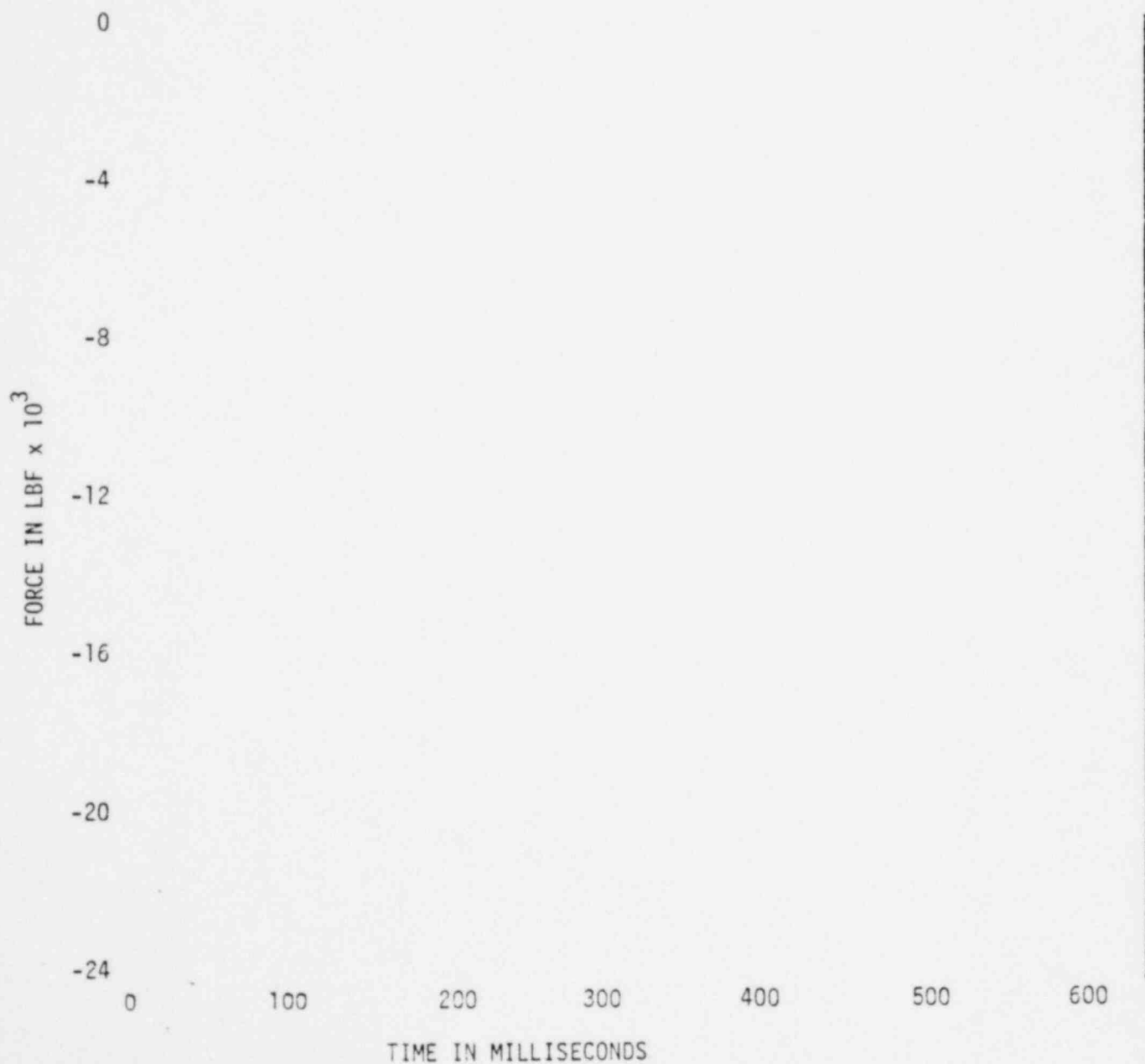


1348 214

FIGURE A-67

TORUS LOAD CELL

Task 5.5.3-2 Pilgrim Test 3



1348 215

FIGURE A-68

TORUS VERTICAL ACCELERATION

Task 5.5.3-2 Pilgrim Test 3

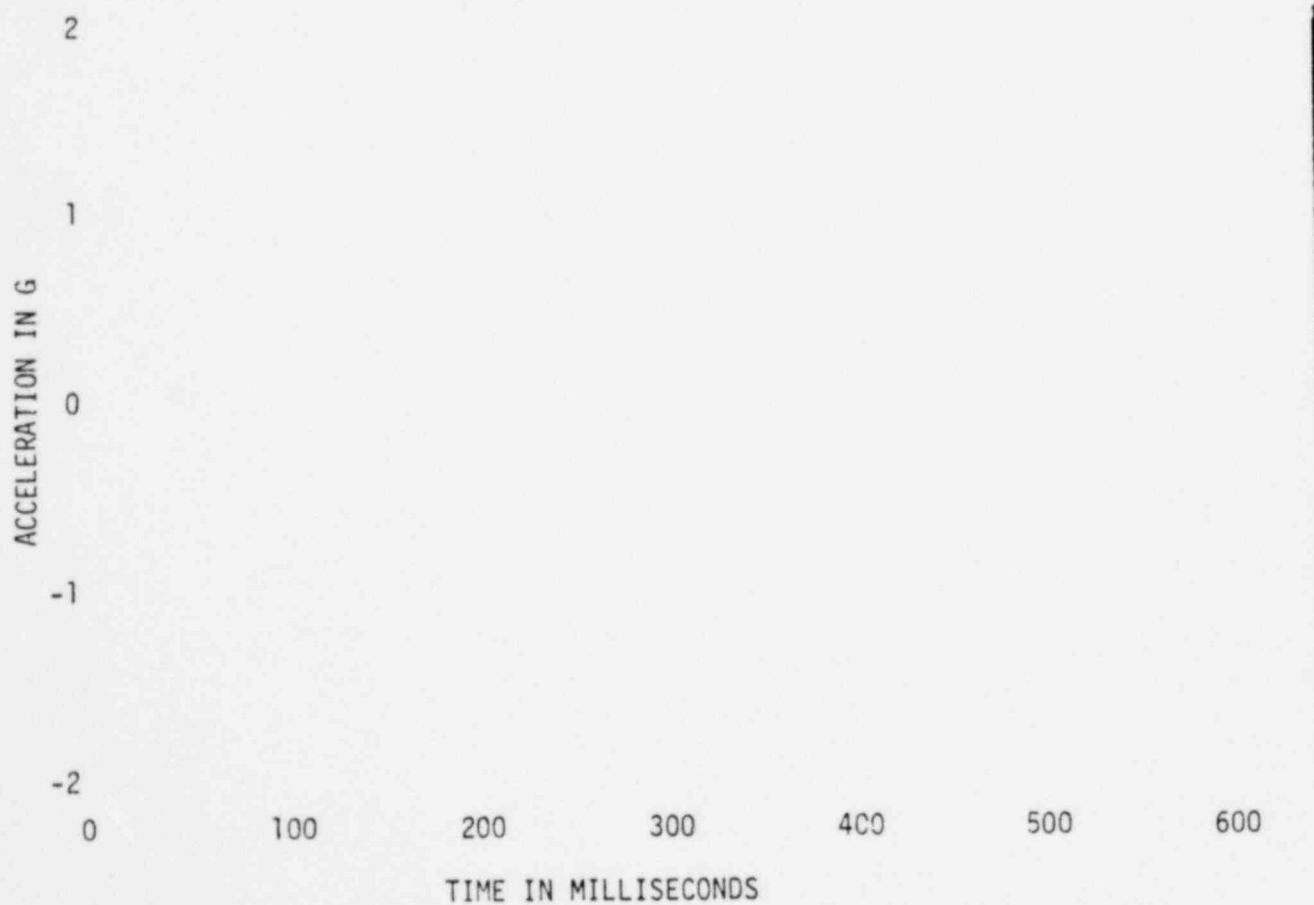
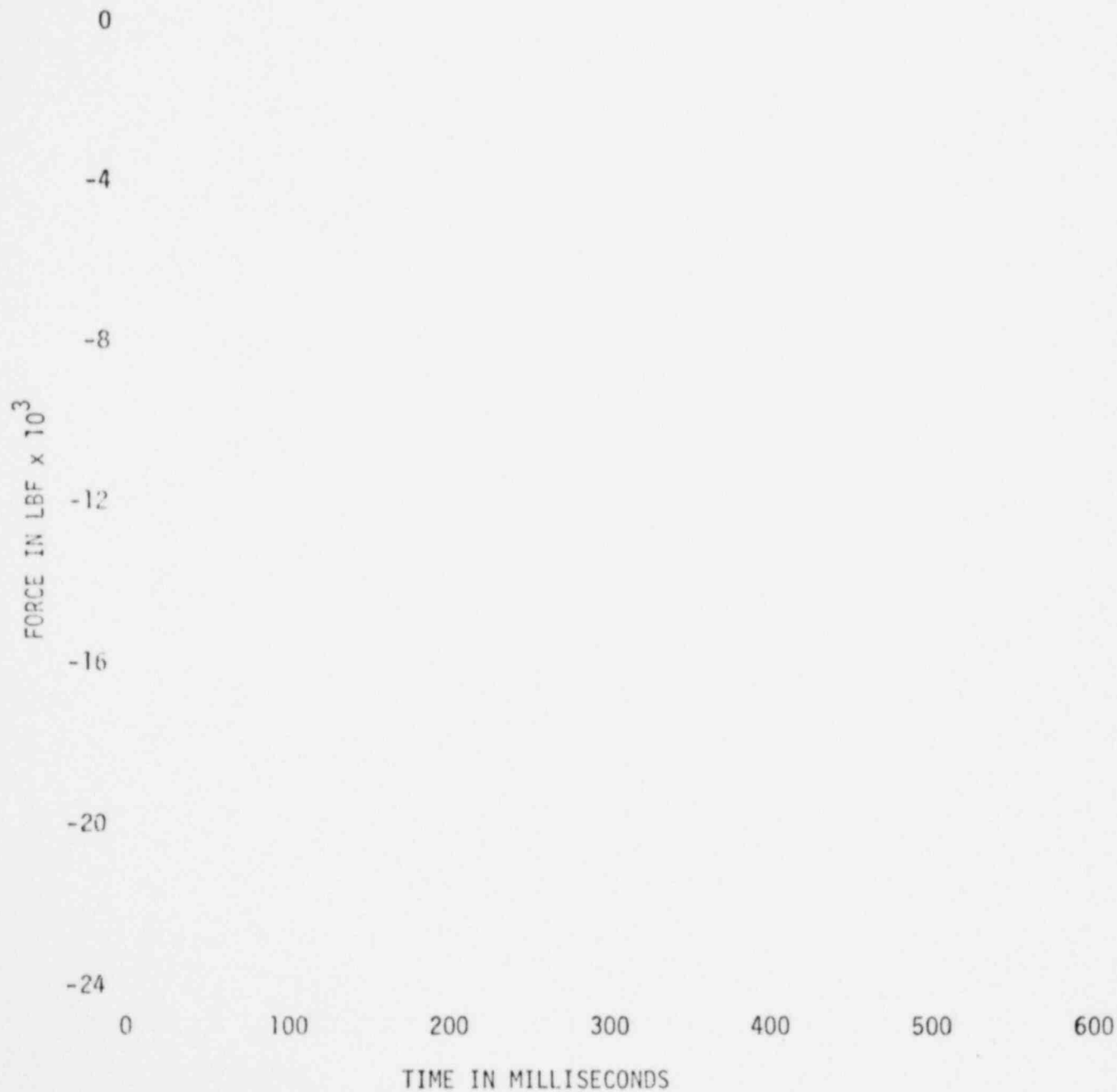


FIGURE A-69

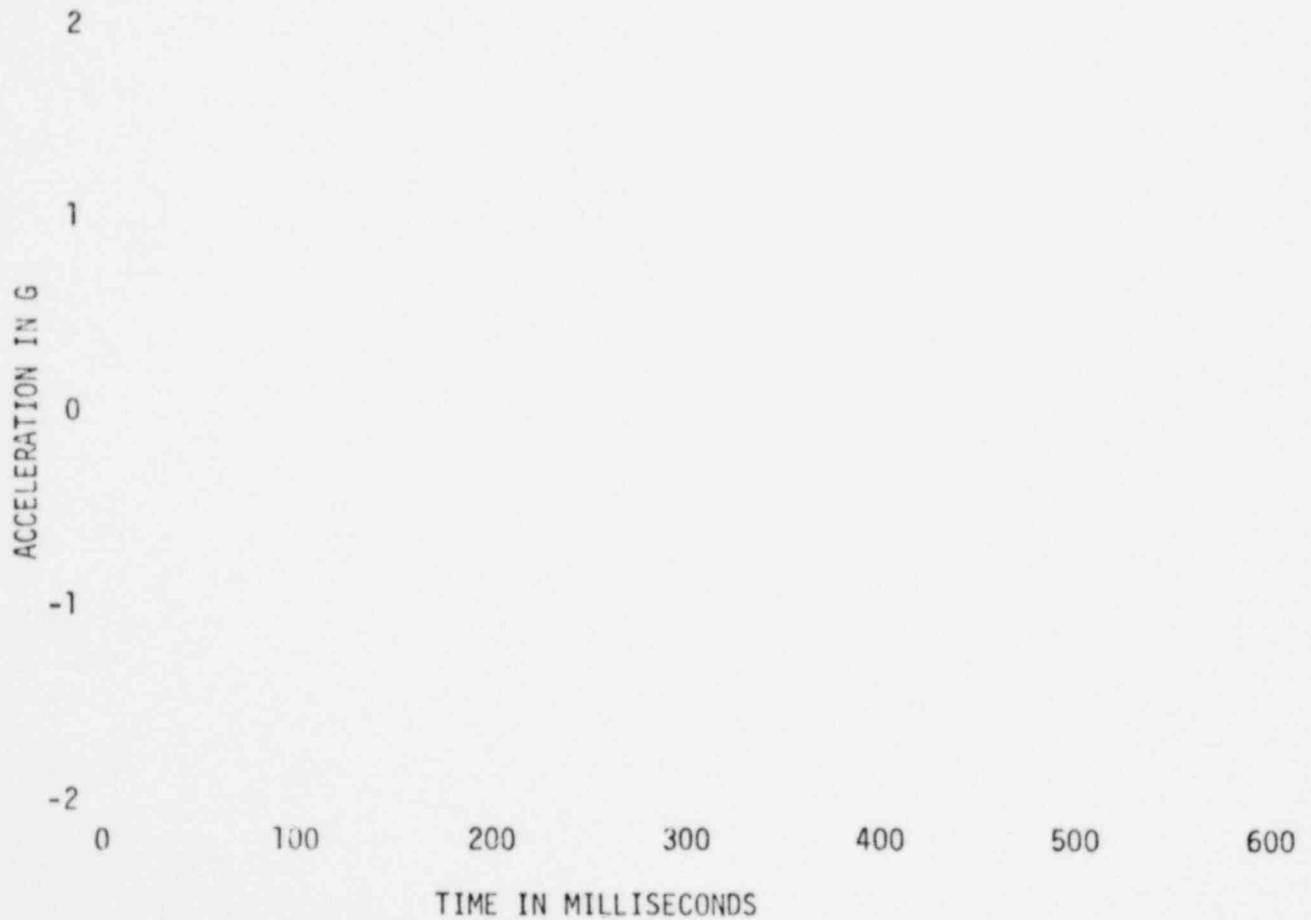
TORUS LOAD CELL

Task 5.5.3-2 Pilgrim Test 5



1348 217

FIGURE A-70  
TORUS VERTICAL ACCELERATION  
Task 5.5.3-2 Pilgrim Test 5



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FIGURE A-71 COMPARISON OF NET TORUS FORCE FROM PRESSURE INTEGRAL  
WITH NET TORUS FORCE FROM LOAD CELL CORRECTED FOR TORUS INERTIA  
Task 5.5.3-2 Pilgrim Test 3

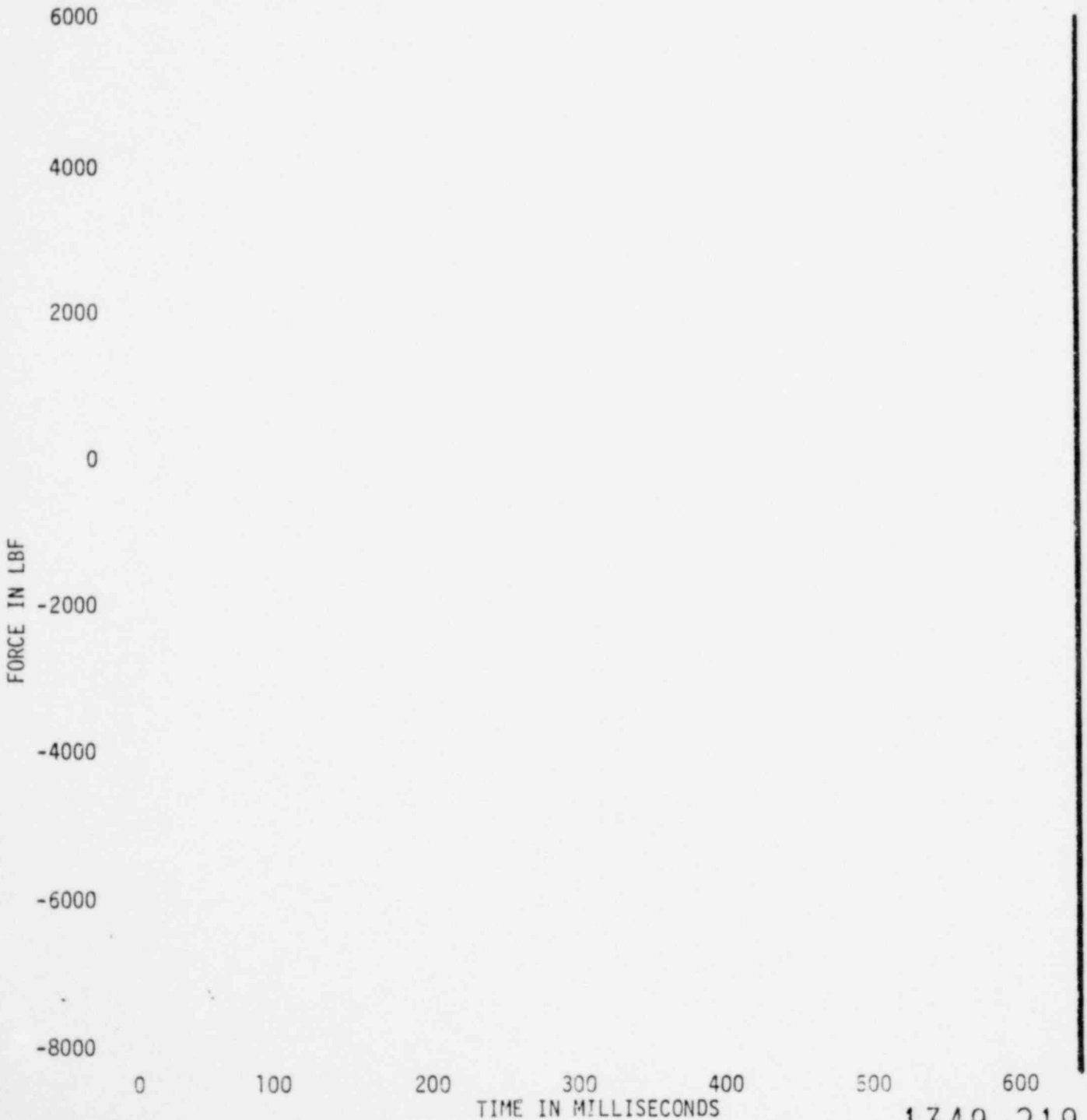
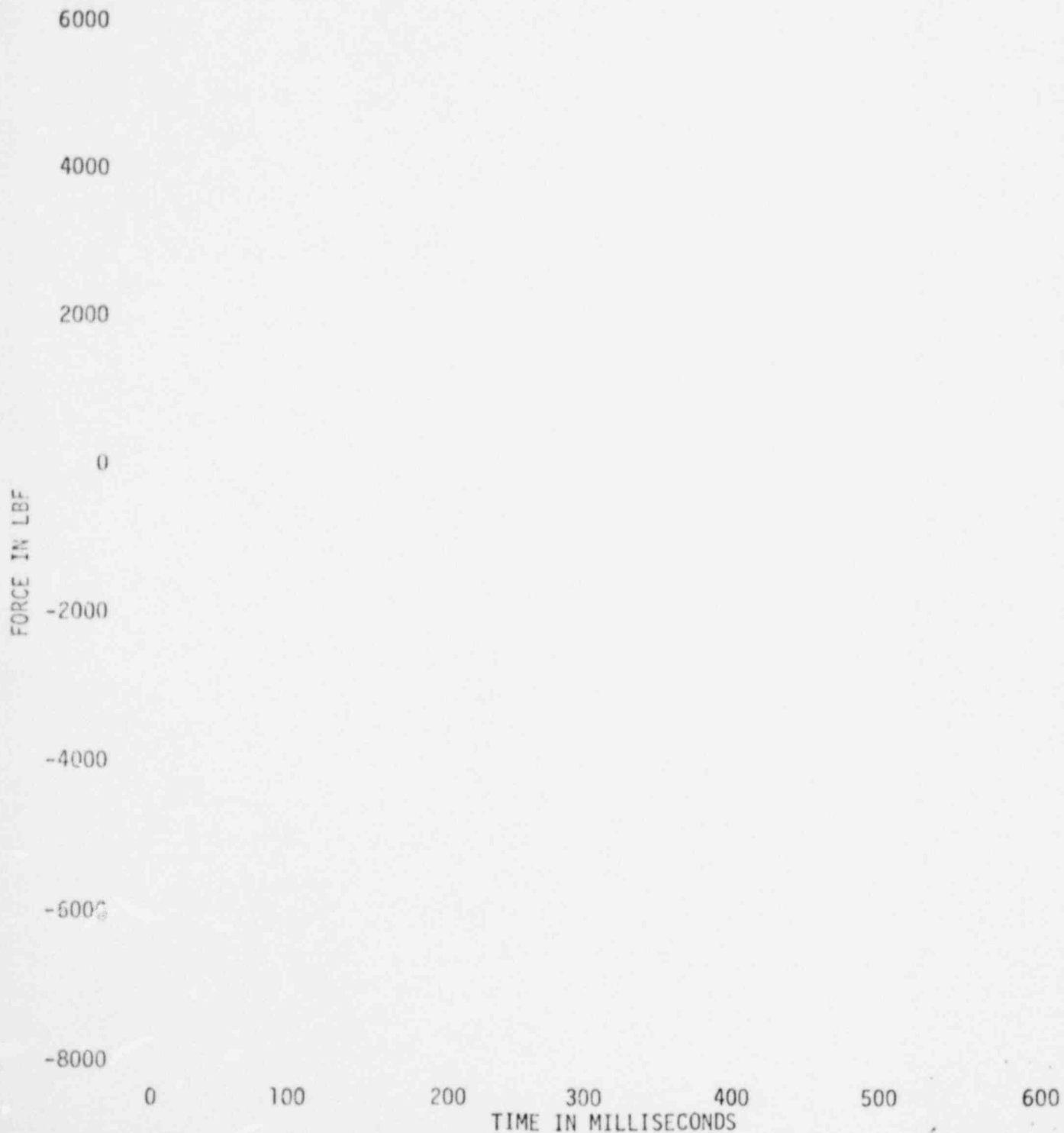


FIGURE A-72 COMPARISON OF NET TORUS FORCE FROM PRESSURE INTEGRAL  
WITH NET TORUS FORCE FROM LOAD CELL CORRECTED FOR TORUS INERTIA  
Task 5.5.3-2 Pilgrim Test 5



NEDO-21944  
FIGURE A-73

NET TORUS FORCE FROM PRESSURE INTEGRAL, CORRECTED FOR WATER INERTIA

Task 5.5.3-2 Pilgrim Test 3

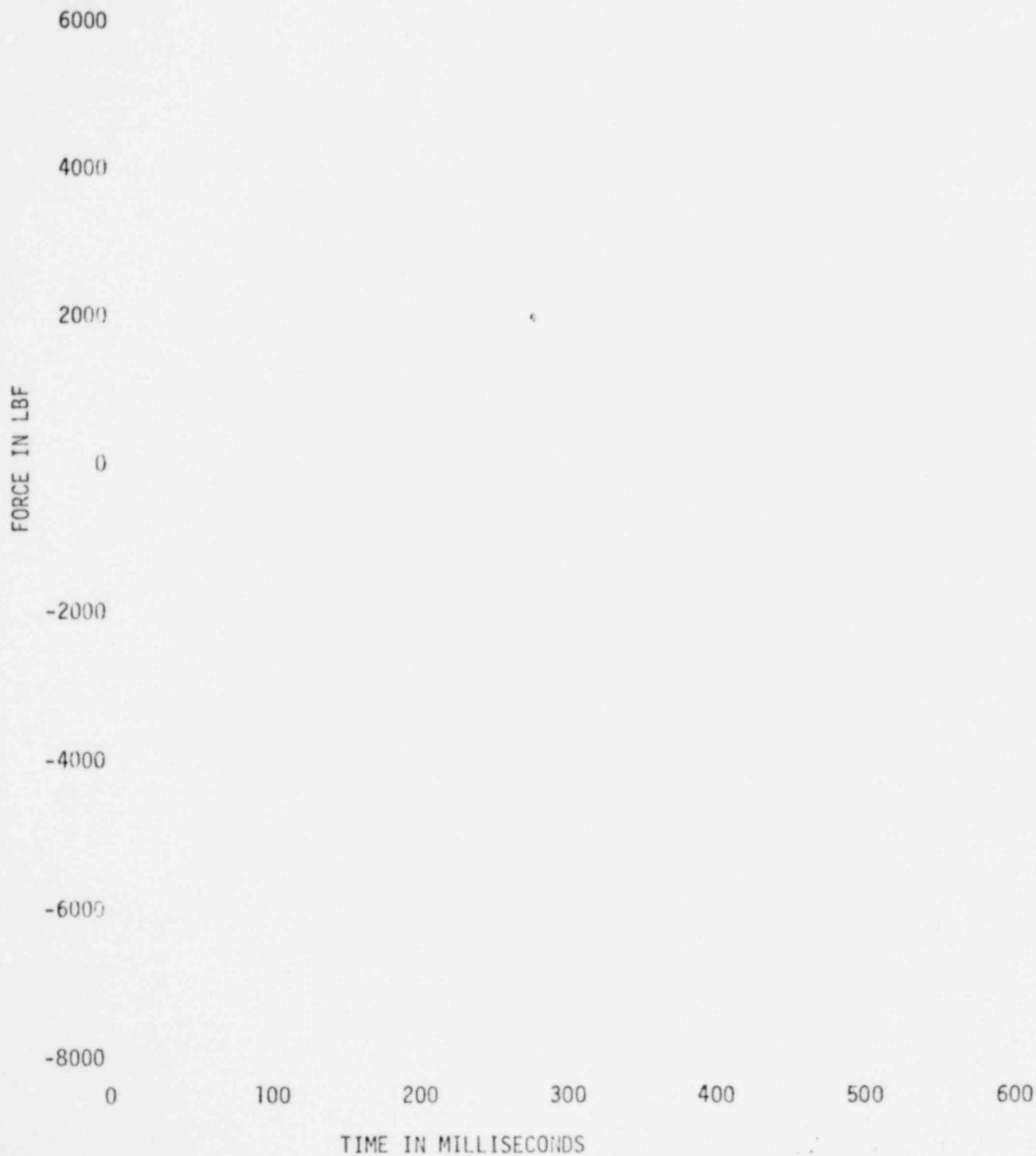


FIGURE A-74

NET TORUS FORCE FROM PRESSURE INTEGRAL, CORRECTED FOR WATER INERTIA

Task 5.5.3-2 Pilgrim Test 5

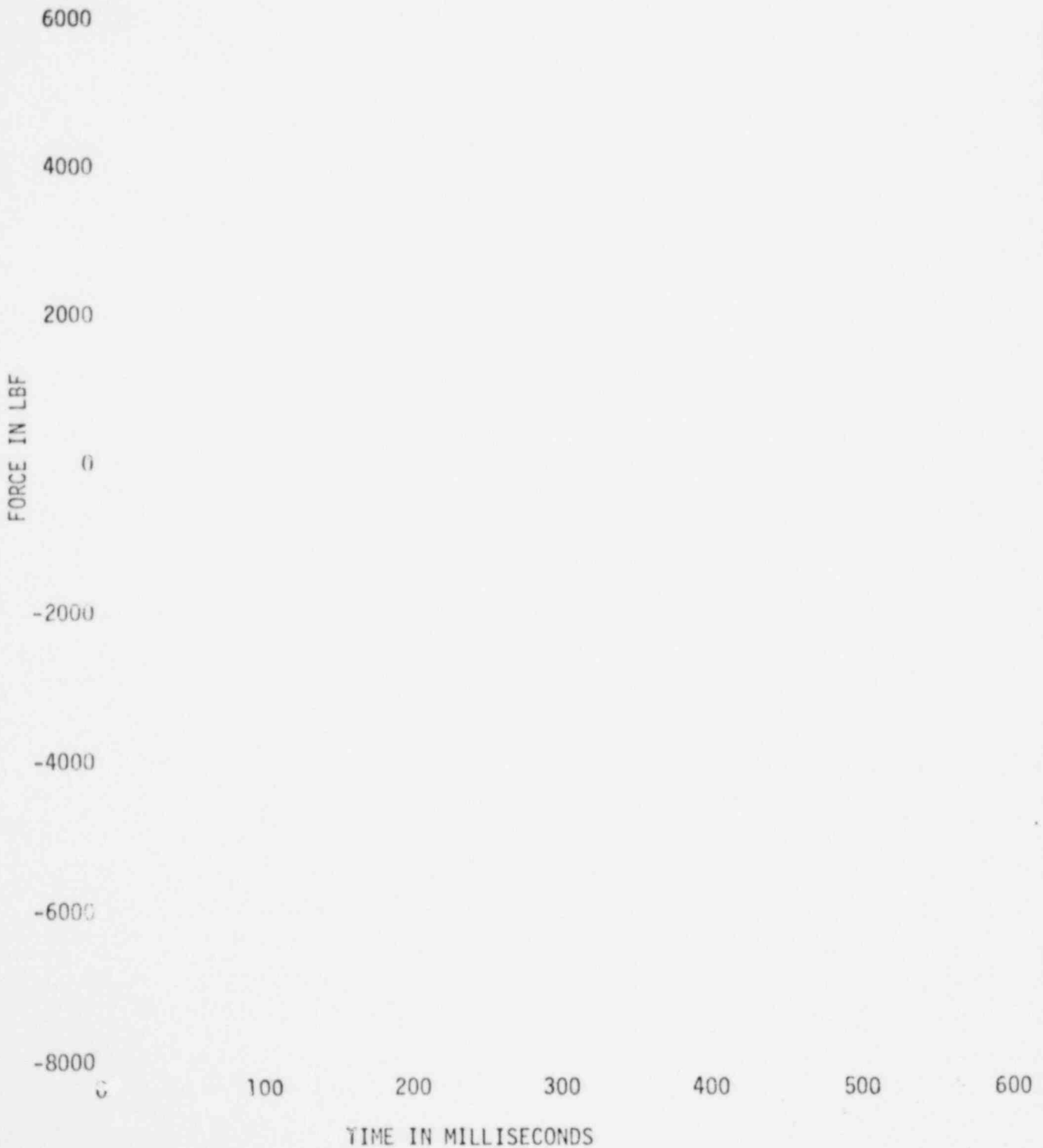


FIGURE A-75

AVERAGE POOL PRESSURE, CORRECTED FOR WATER INERTIA

Task 5.5.3-2 Pilgrim Test 3

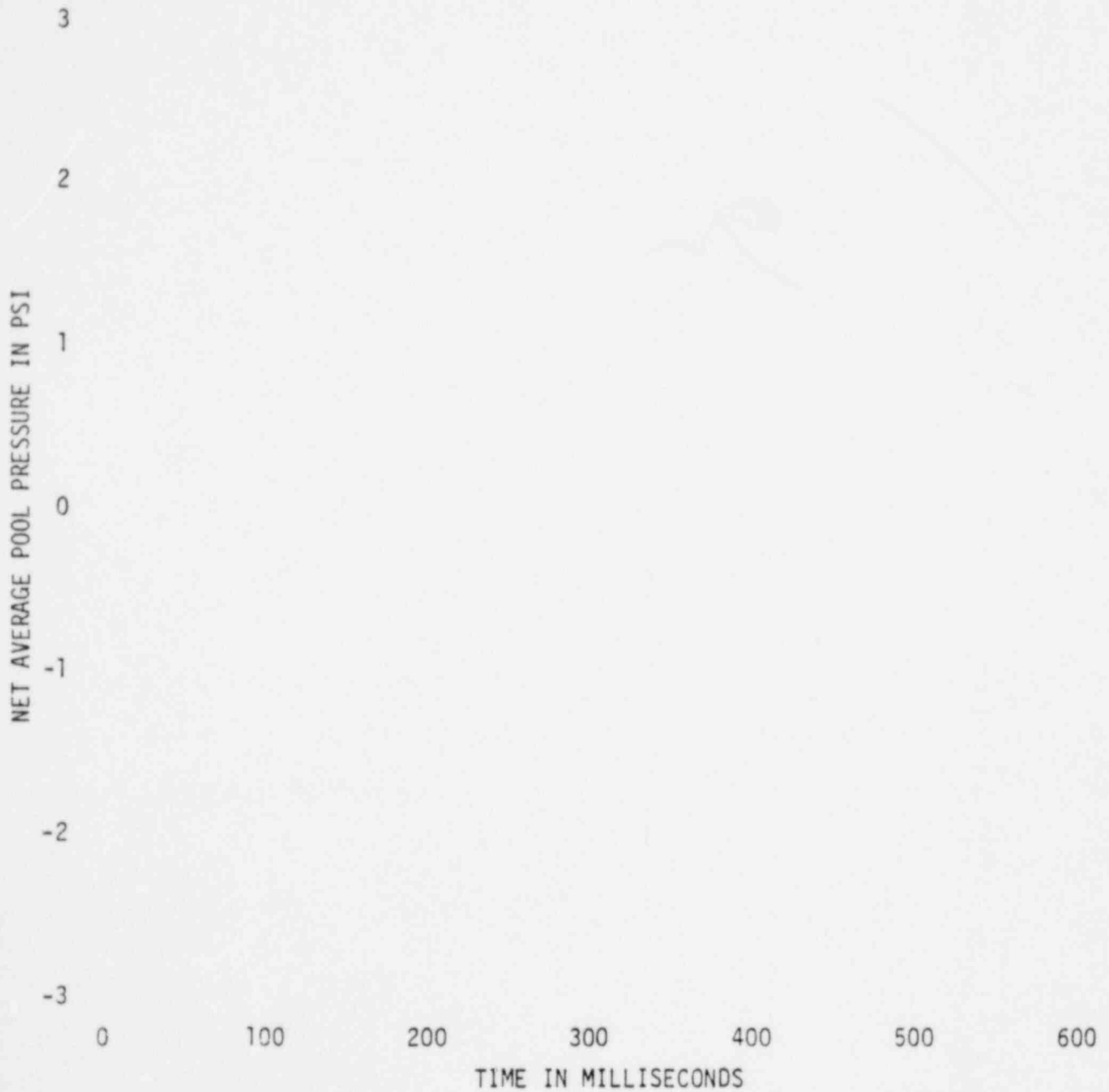


1348 223

FIGURE A-76

NET AVERAGE POOL PRESSURE, CORRECTED FOR WATER INERTIA

Task 5.5.3-2 Pilgrim Test 3

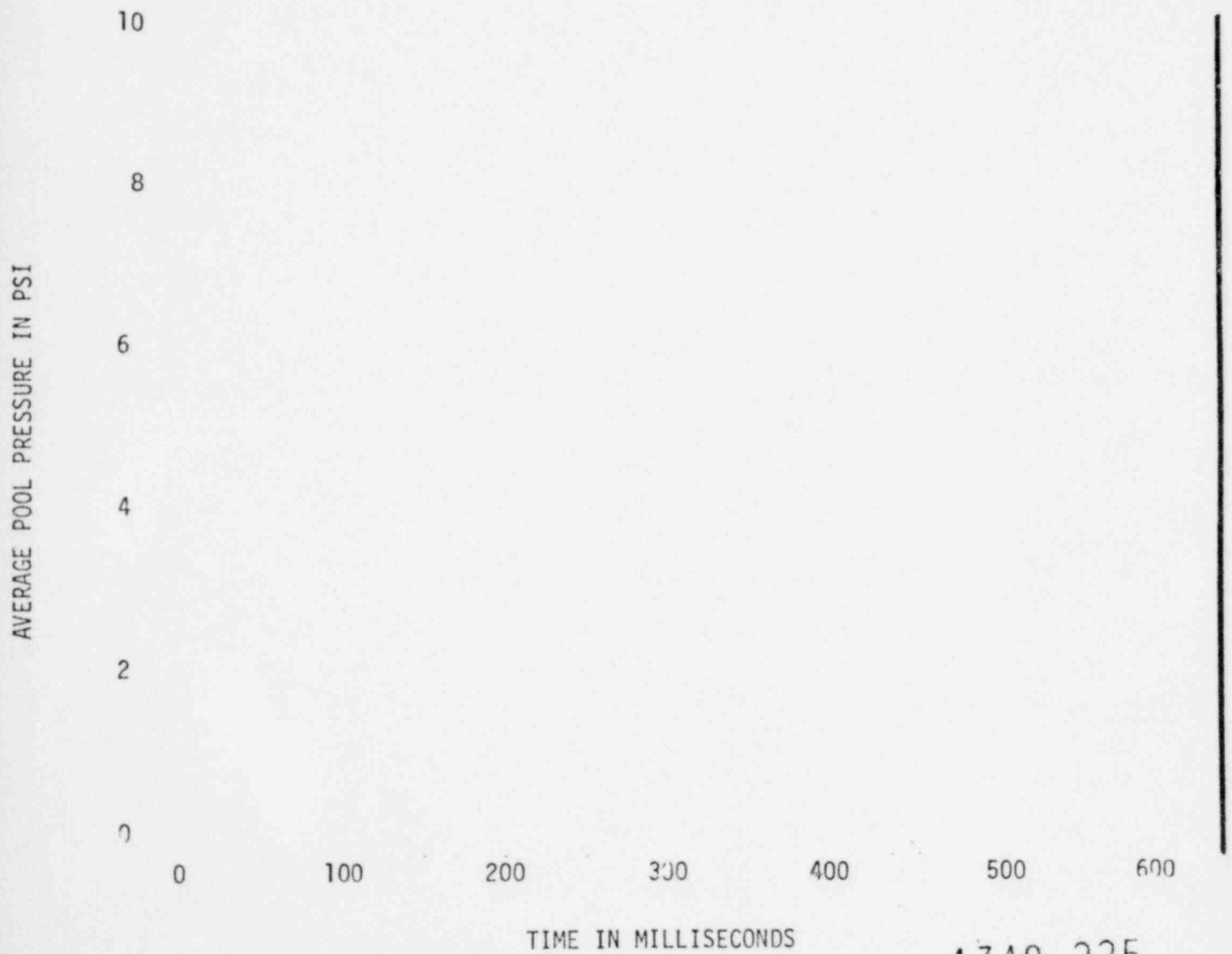


1348 224

FIGURE A-77

AVERAGE POOL PRESSURE, CORRECTED FOR WATER INERTIA

Task 5.5.3-2 Pilgrim Test 5

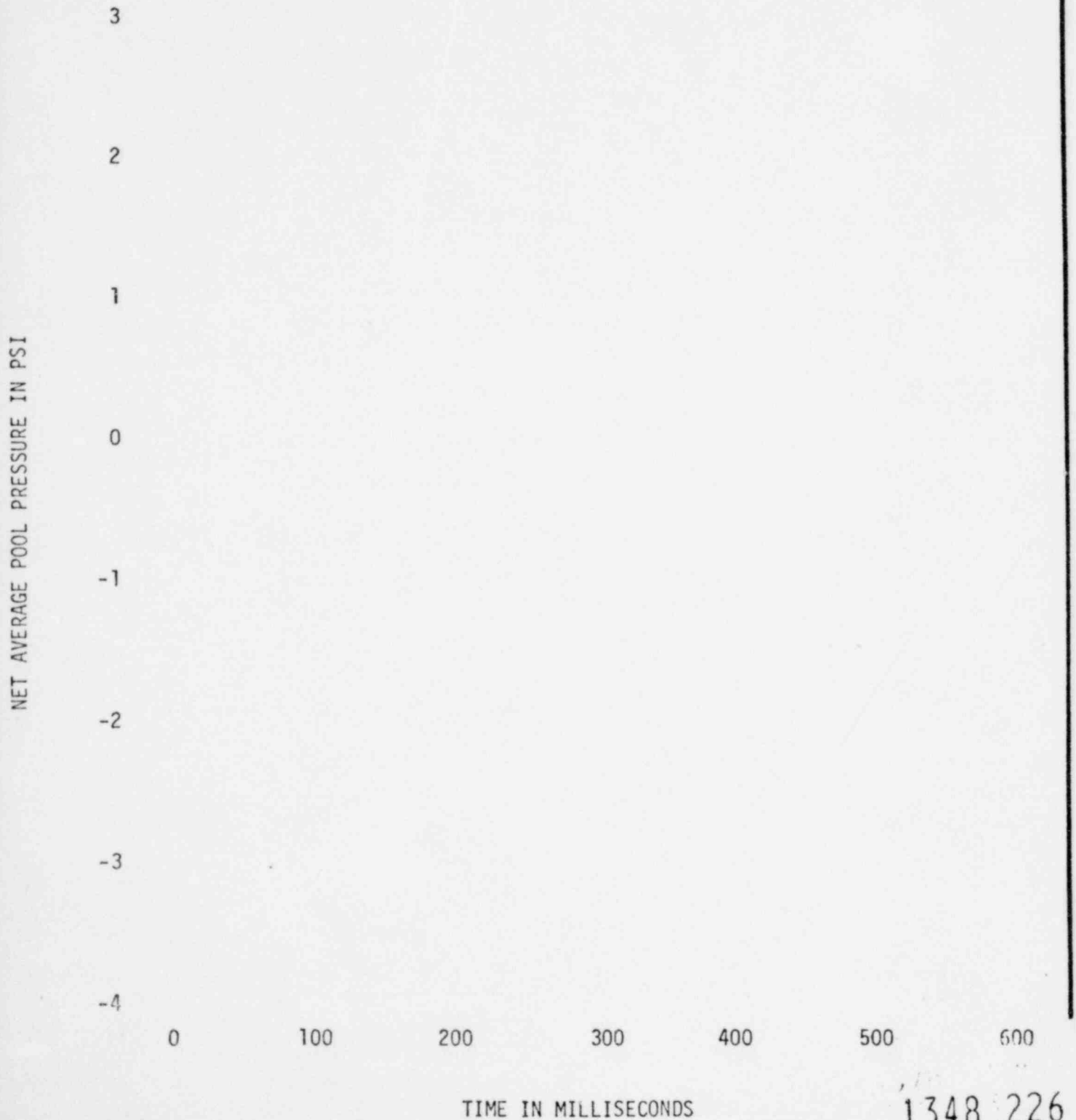


NEDO-21944

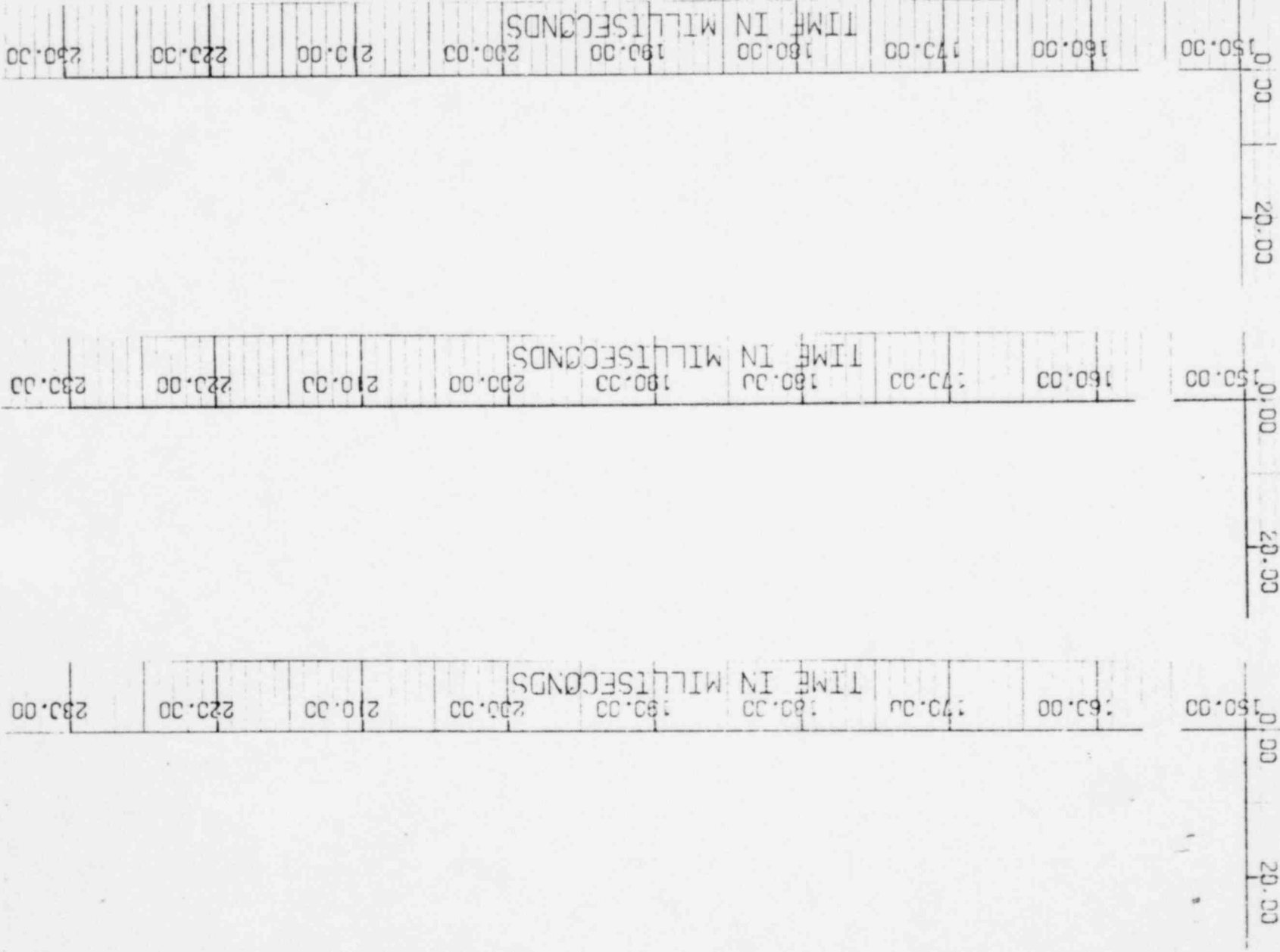
FIGURE A-78

NET AVERAGE POOL PRESSURE, CORRECTED FOR WATER INERTIA

Task 5.5.3-2 Pilgrim Test 5



IMPACT PRESSURE IN PSIA



VENT HEADER IMPACT PRESSURES  
FIGURE A-79  
Task 5.5.3-2 Pilgrim Test 3

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IMPACT PRESSURE IN PSIA

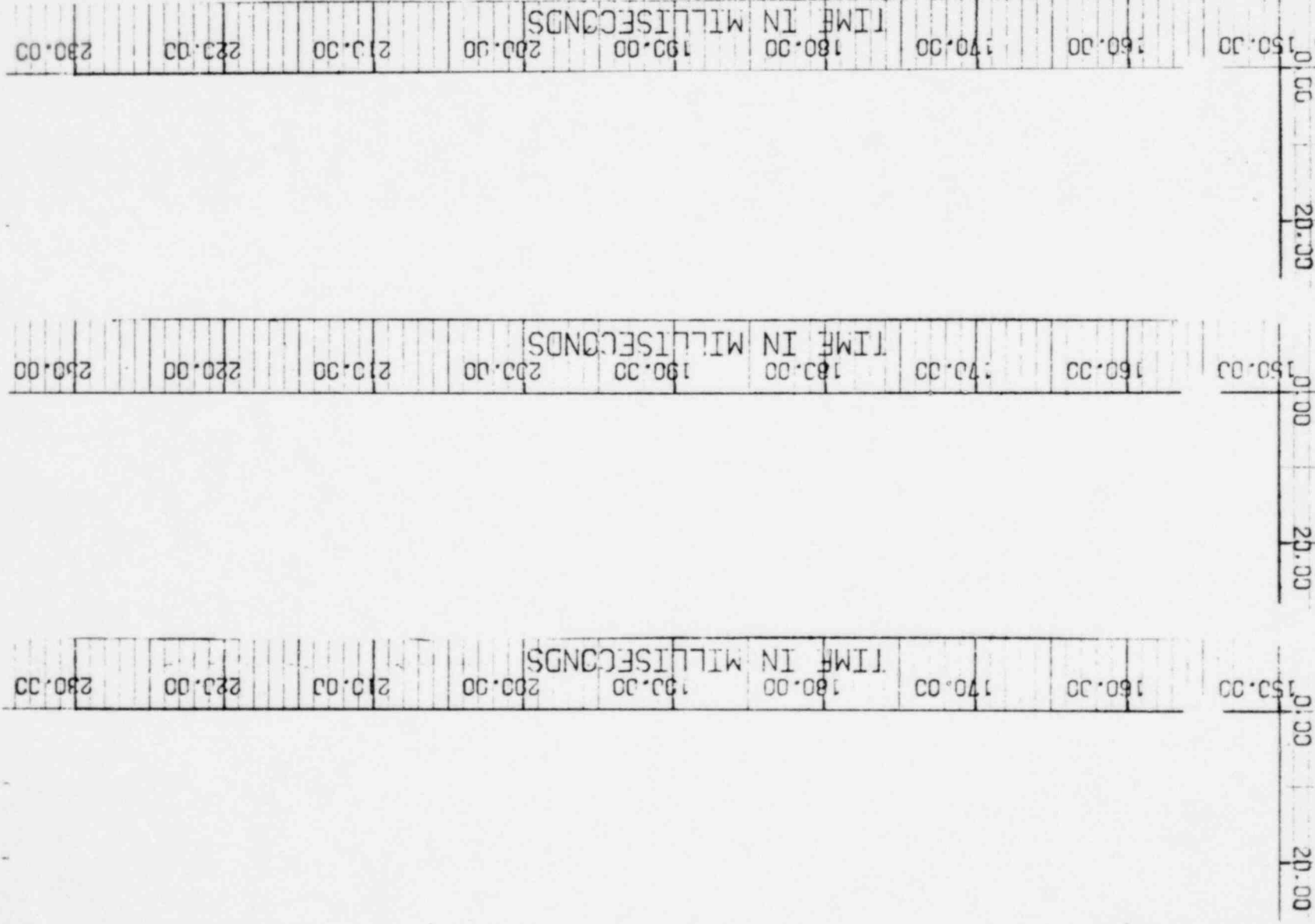


FIGURE A-80

VENT HEADER IMPACT PRESSURES  
Task 5.5.3-2 Pilgrim Test 3

IMPACT PRESSURE IN PSIA

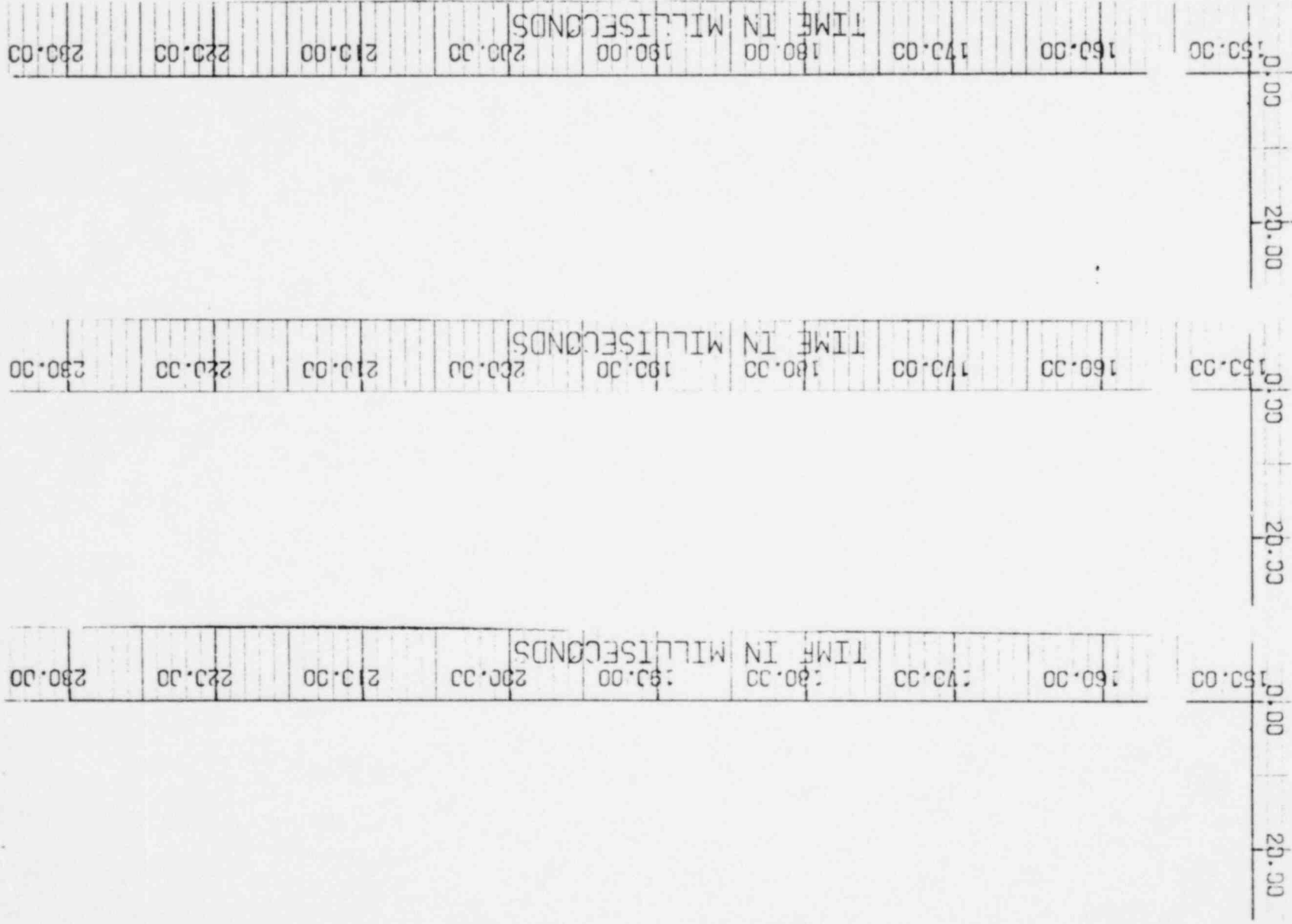


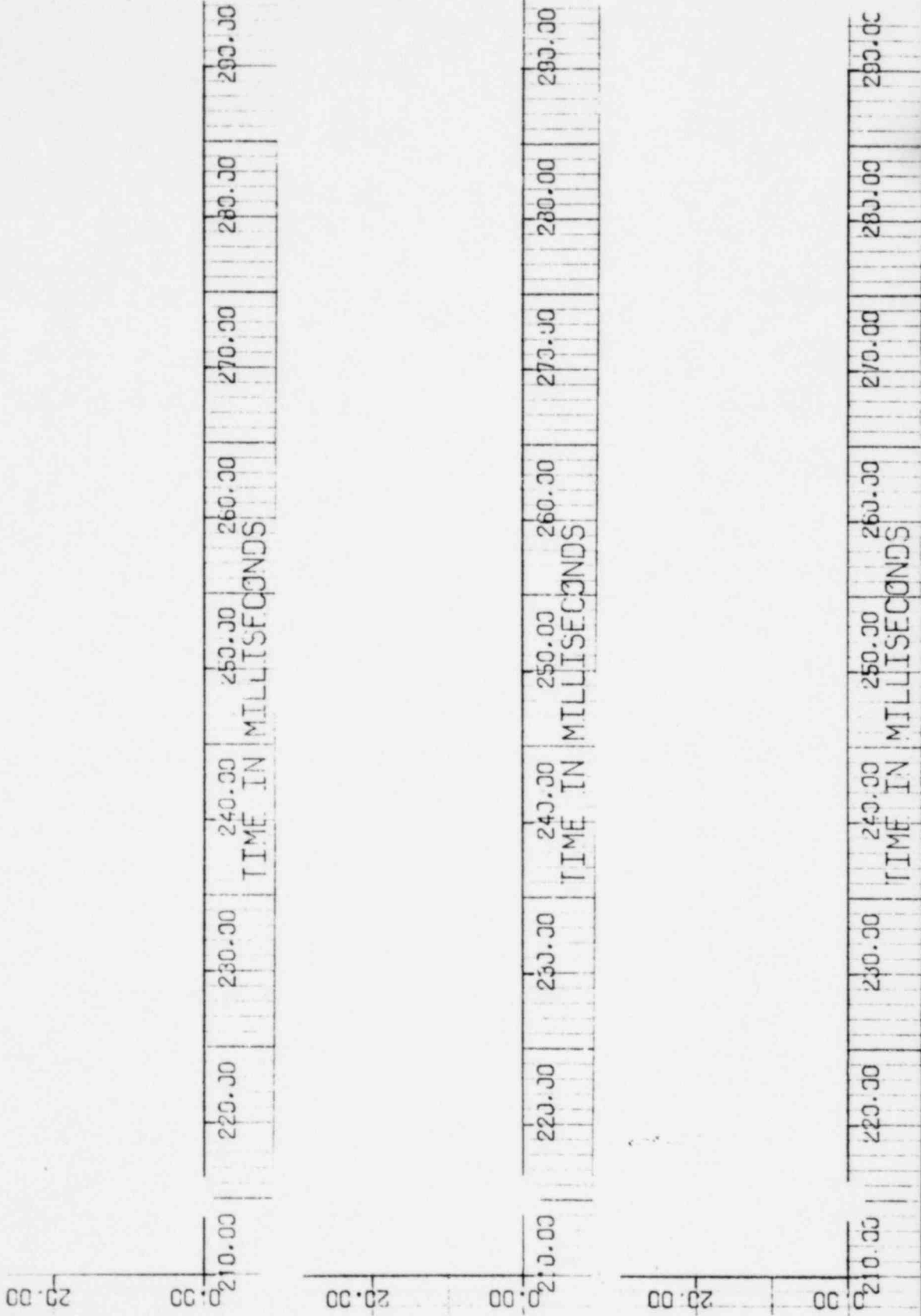
FIGURE A-81

VENT HEADER IMPACT PRESSURES  
Task 5.5.3-2 Pilgrim Test 3

FIGURE A-82

VENT HEADER IMPACT PRESSURES

Task 5.5.3-2 Pilgrim Test 5



IMPACT PRESSURE IN PSIA

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VENT HEADER IMPACT PRESSURES  
Task 5.5.3-2 Pilgrim Test 5

0.00		20.00		40.00	
210.00	220.00	210.00	220.00	210.00	220.00
230.00	240.00	230.00	240.00	230.00	240.00
TIME IN MILLISECONDS					
250.00	260.00	250.00	260.00	250.00	260.00
270.00	280.00	270.00	280.00	270.00	280.00
290.00		290.00		290.00	

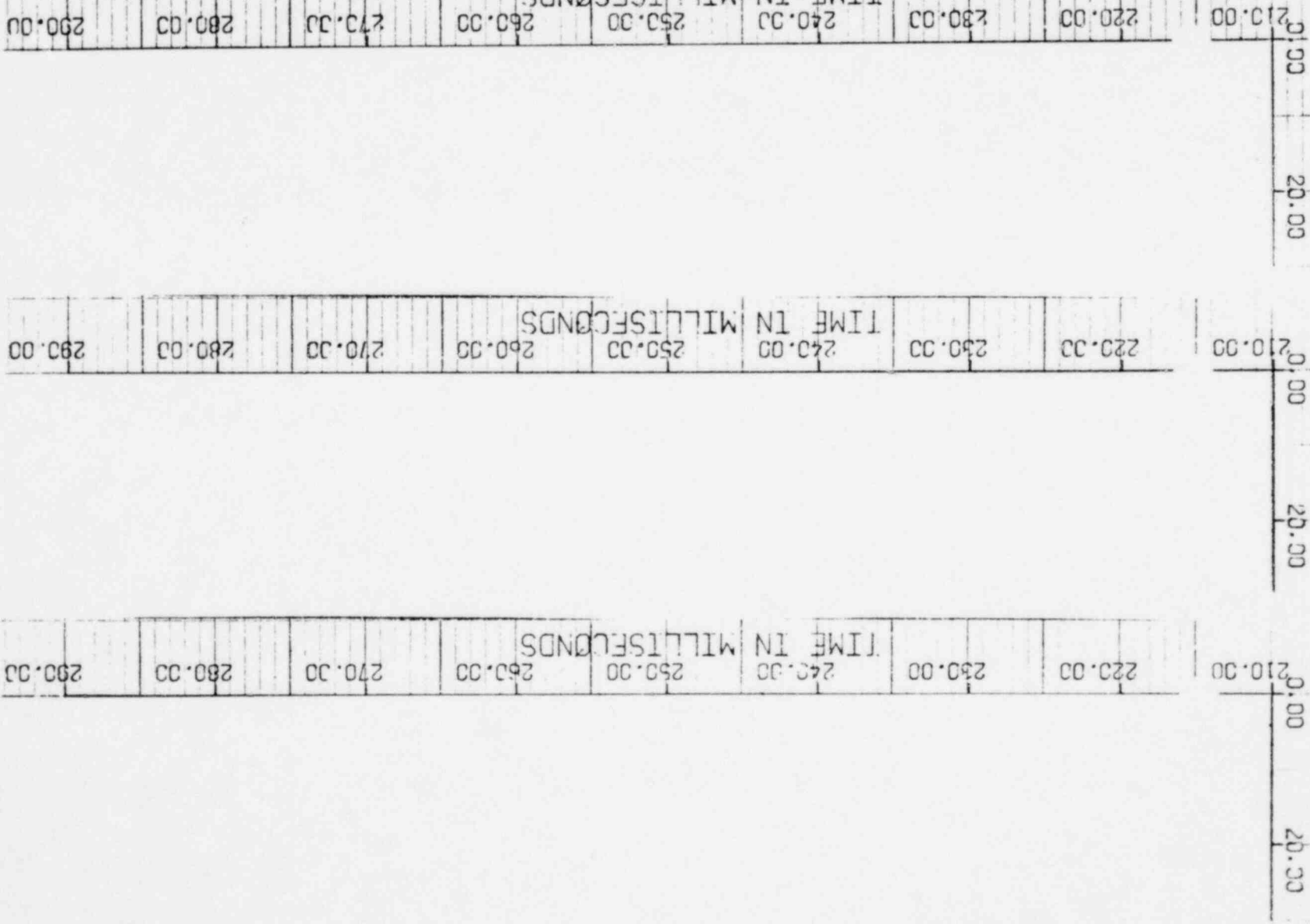
IMPACT PRESSURE IN PSIA

A-97

1348 231

7-7 0451

IMPACT PRESSURE IN PSIA

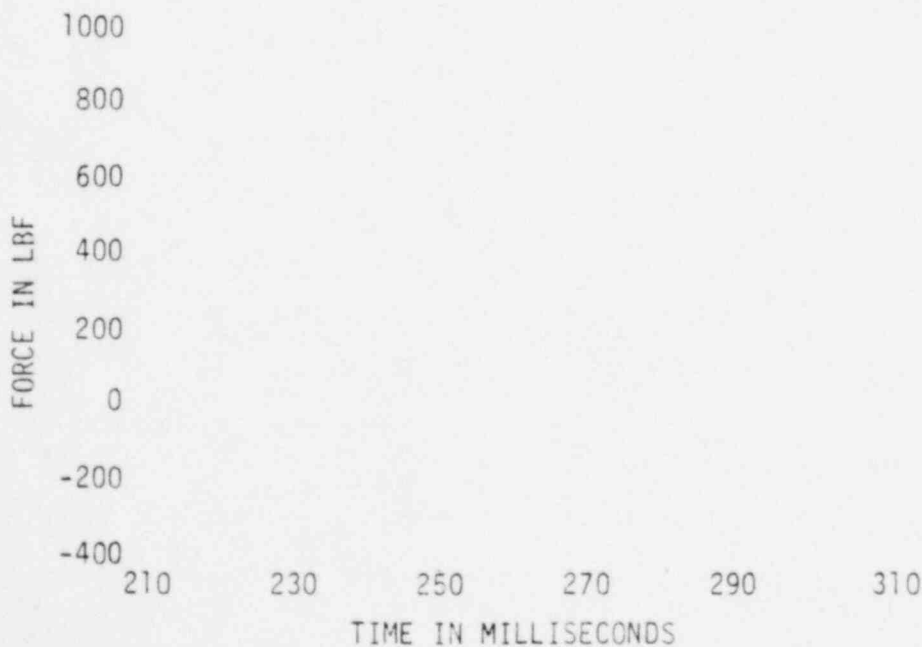
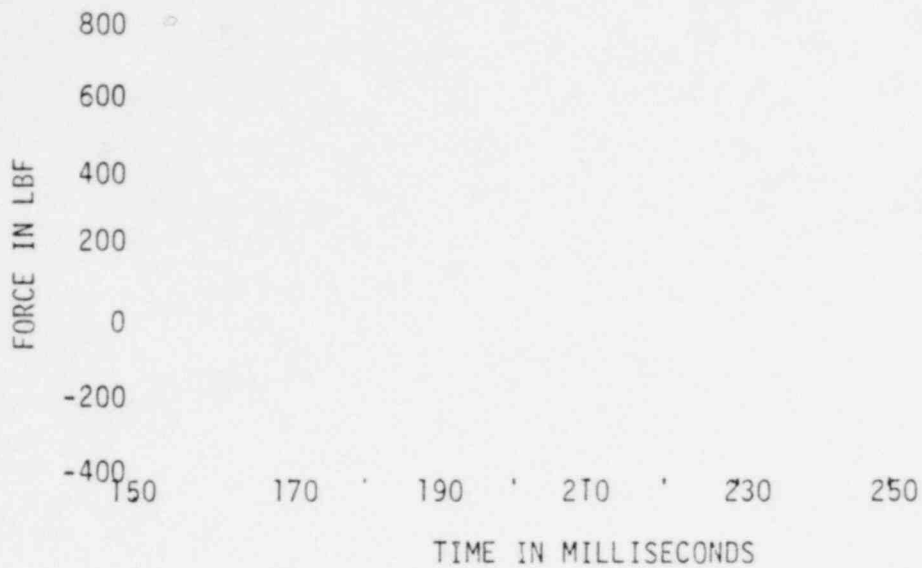


Task 5.5.3-2 Pilgrim Test 5  
VENT HEADER IMPACT PRESSURES

FIGURE A-84

NEDO-21944  
FIGURE A-85

COMPARISON OF VENT HEADER IMPACT RESULTS  
(Corrected Load Cell and Pressure Integration)  
Task 5.5.3 Pilgrim Tests 3, 5

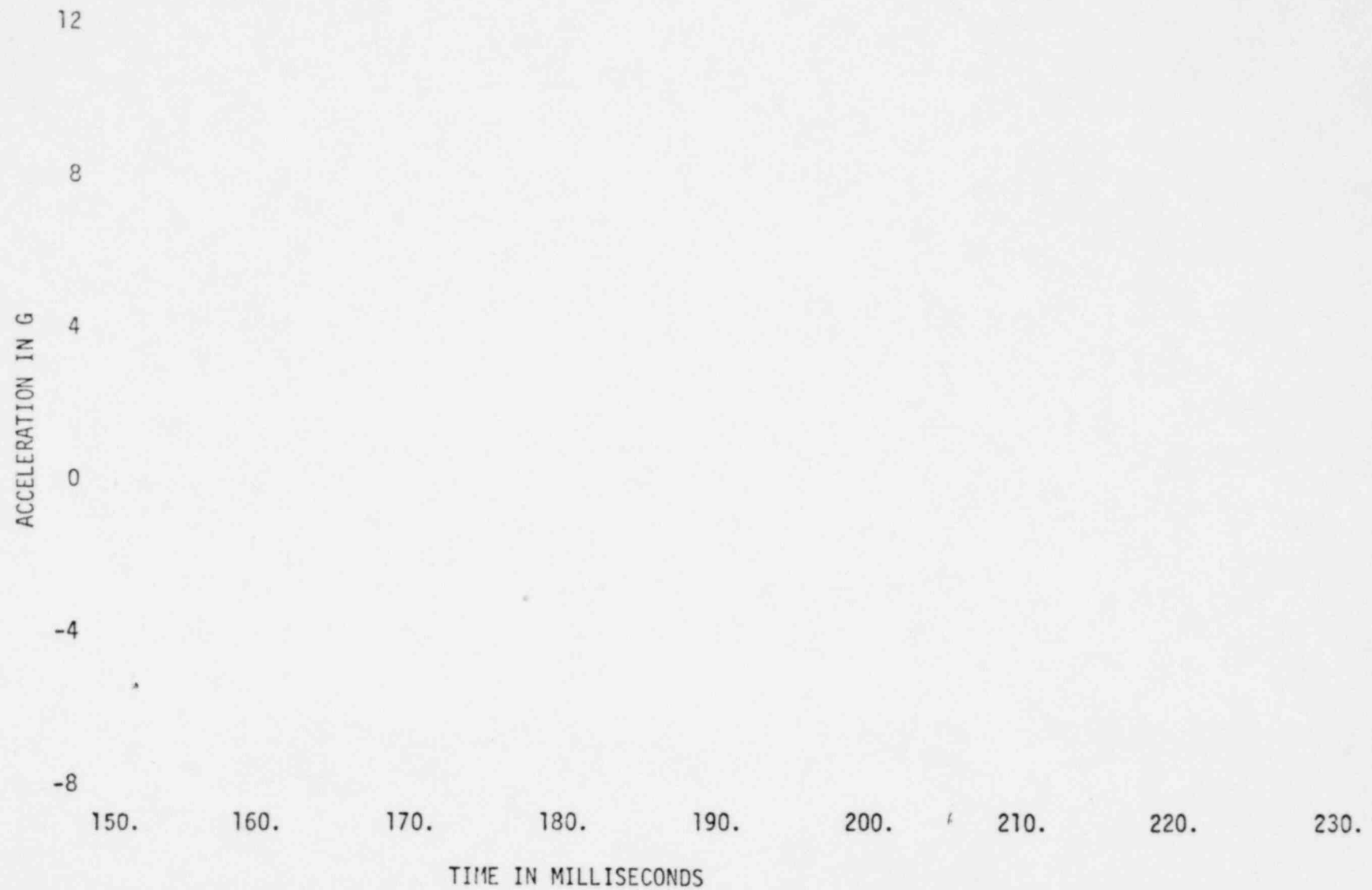


1348 233

FIGURE A-86

VENT HEADER VERTICAL ACCELERATION

Task 5.5.3-2 Pilgrim Test 3



A-100

1348 234

NEDO-21944

FIGURE A-87

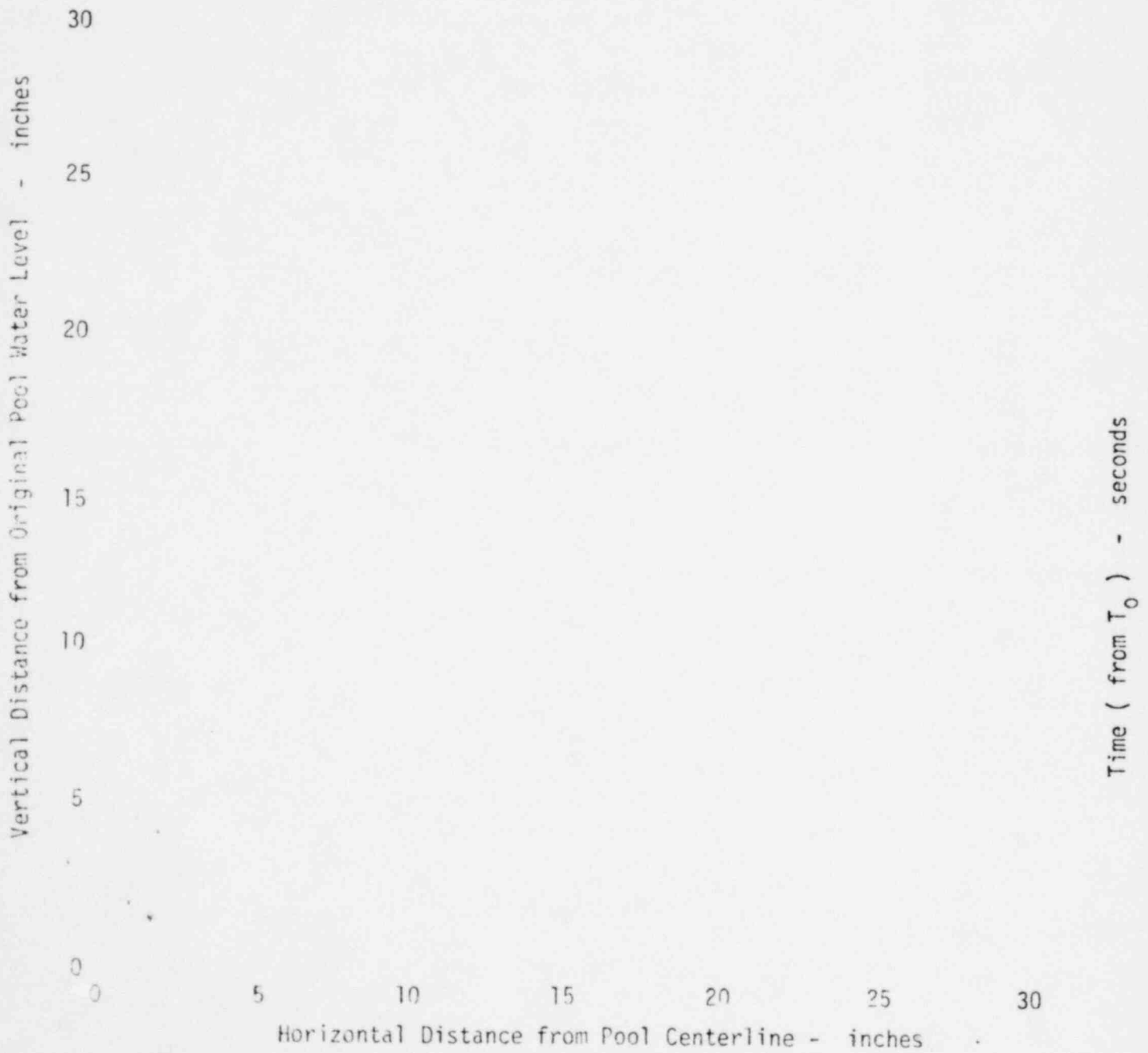
VENT HEADER VERTICAL ACCELERATION

Task 5.5.3-2 Pilgrim Test 5



Time History Of  
Pool Displacement

PILGRIM, TEST 1



NEDO-21944

FIGURE A-89

Time History Of  
Pool Displacement

PILGRIM, TEST 2

30

25

20

15

10

5

0

5

10

15

20

25

30

Horizontal Distance from Pool Centerline - inches

Time ( from  $T_0$  ) - seconds

1348 237

NEDO-21944

FIGURE A-90

Time History Of  
Pool Displacement

PILGRIM, TEST 3

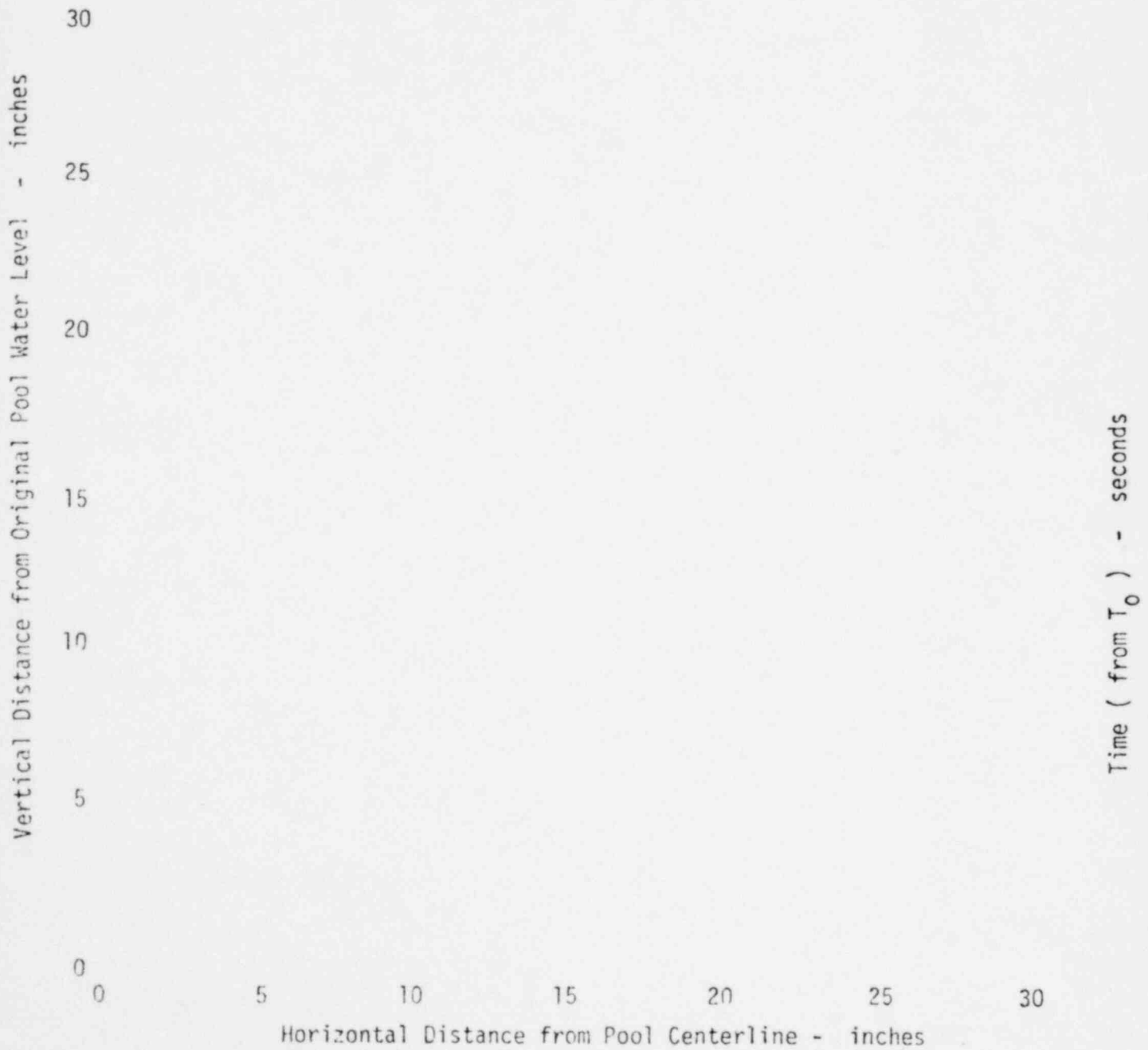


FIGURE A-91

Time History Of  
Pool Displacement

PILGRIM, TEST 5

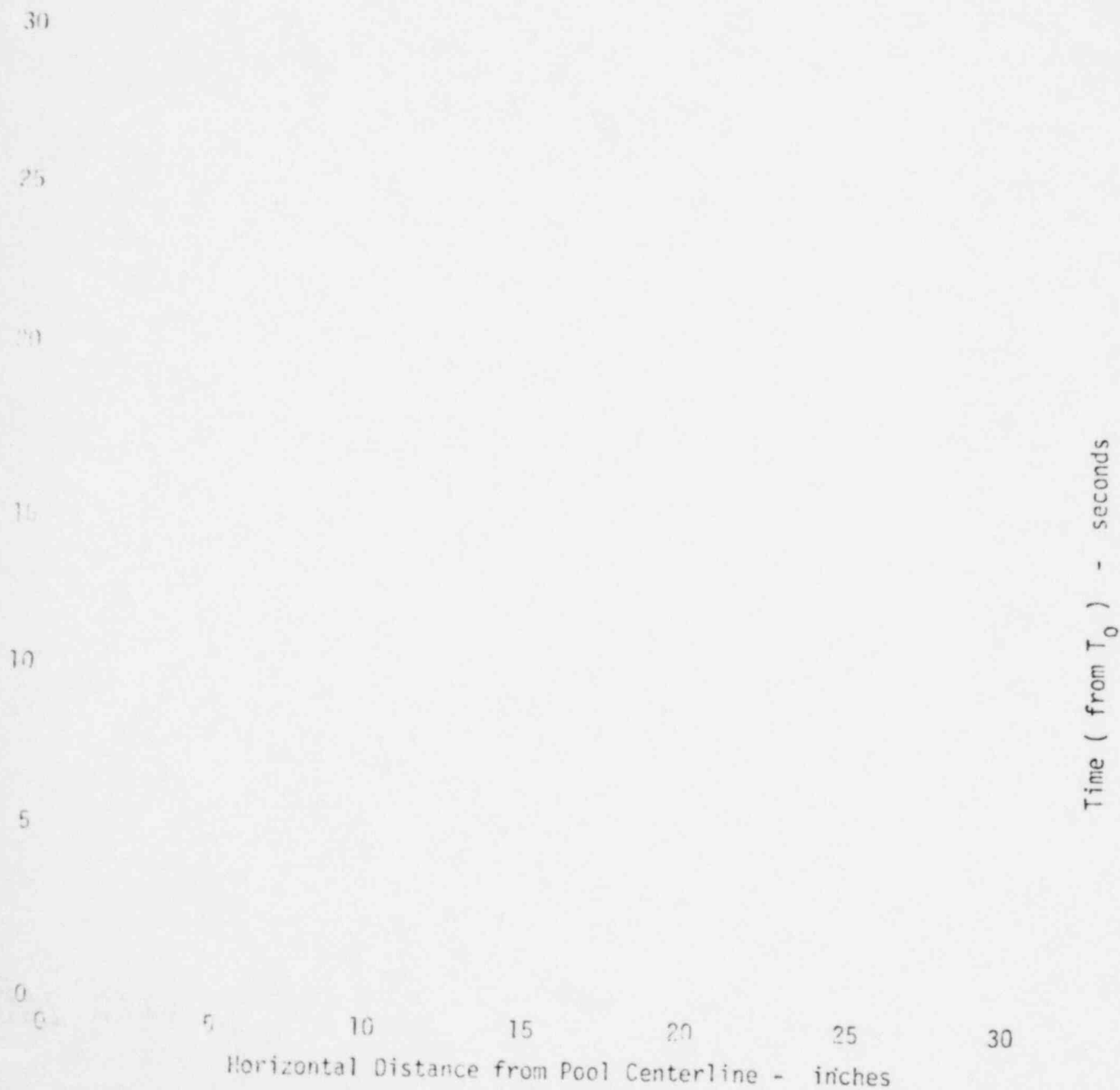
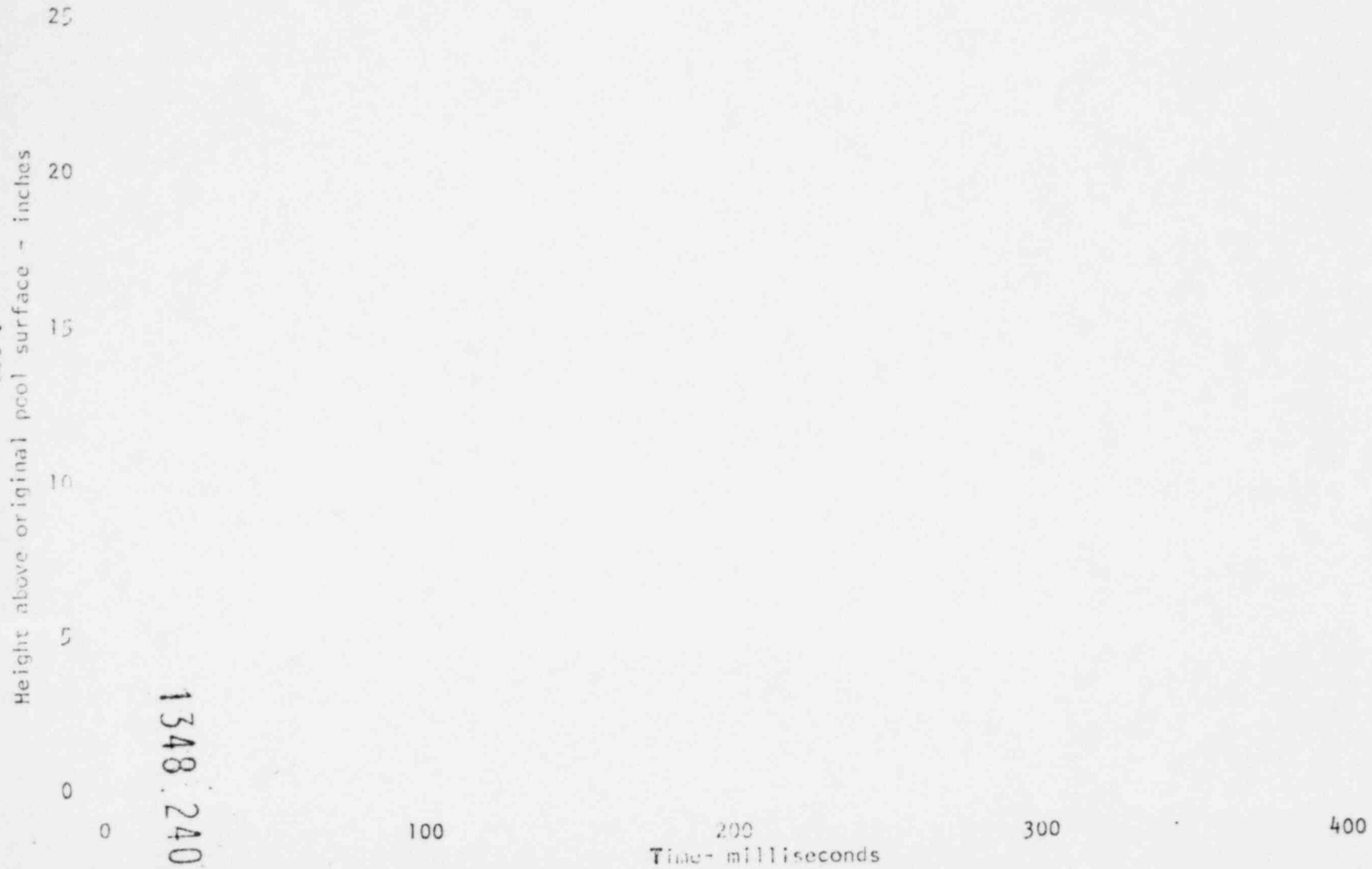


FIGURE A-92

POOL SURFACE DISPLACEMENT

PILGRIM, TESTS 1, 2, 3



PILGRIM, TESTS 1, 2, 3

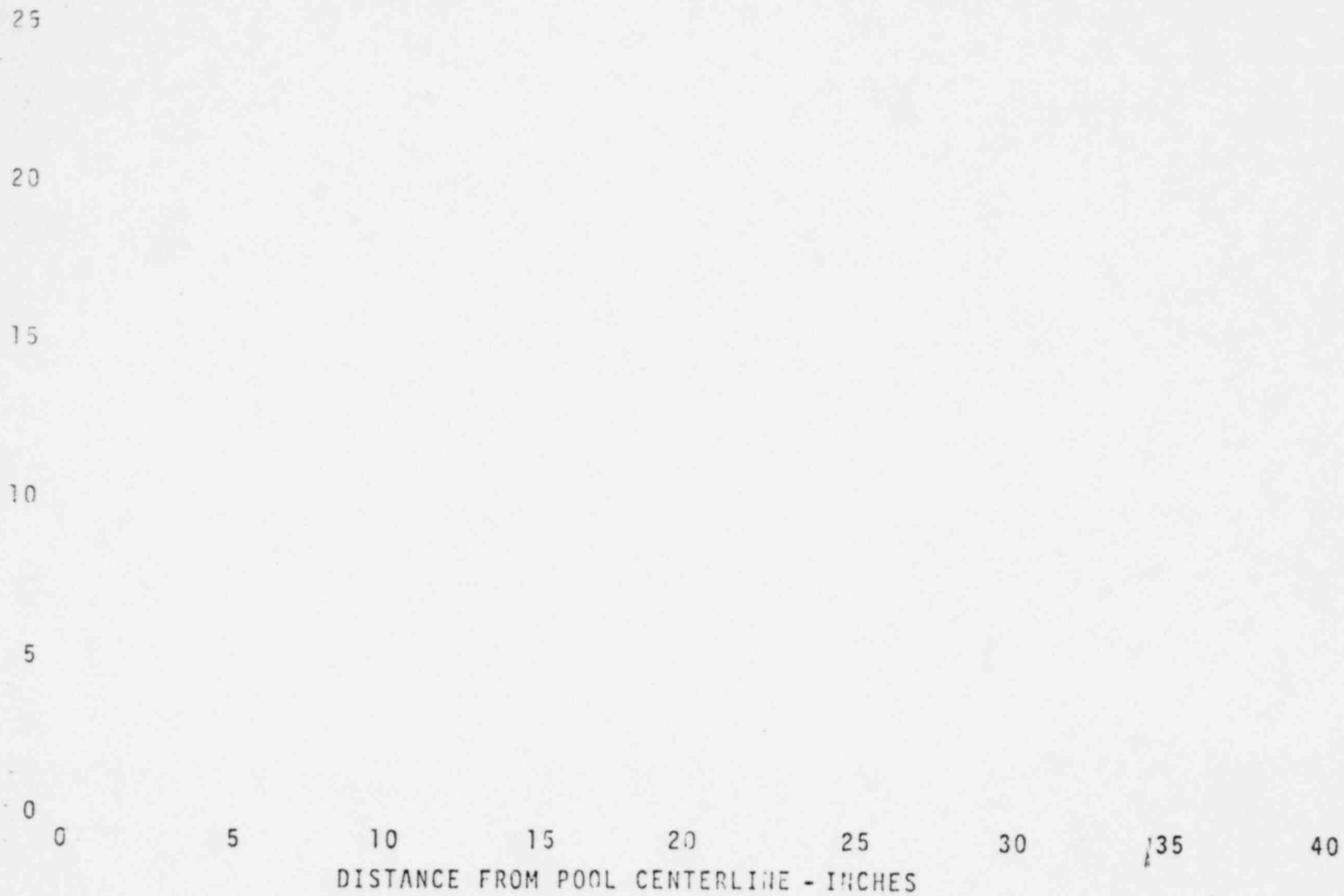


FIGURE A-94

POOL SURFACE DISPLACEMENT

PILGRIM, TEST 5

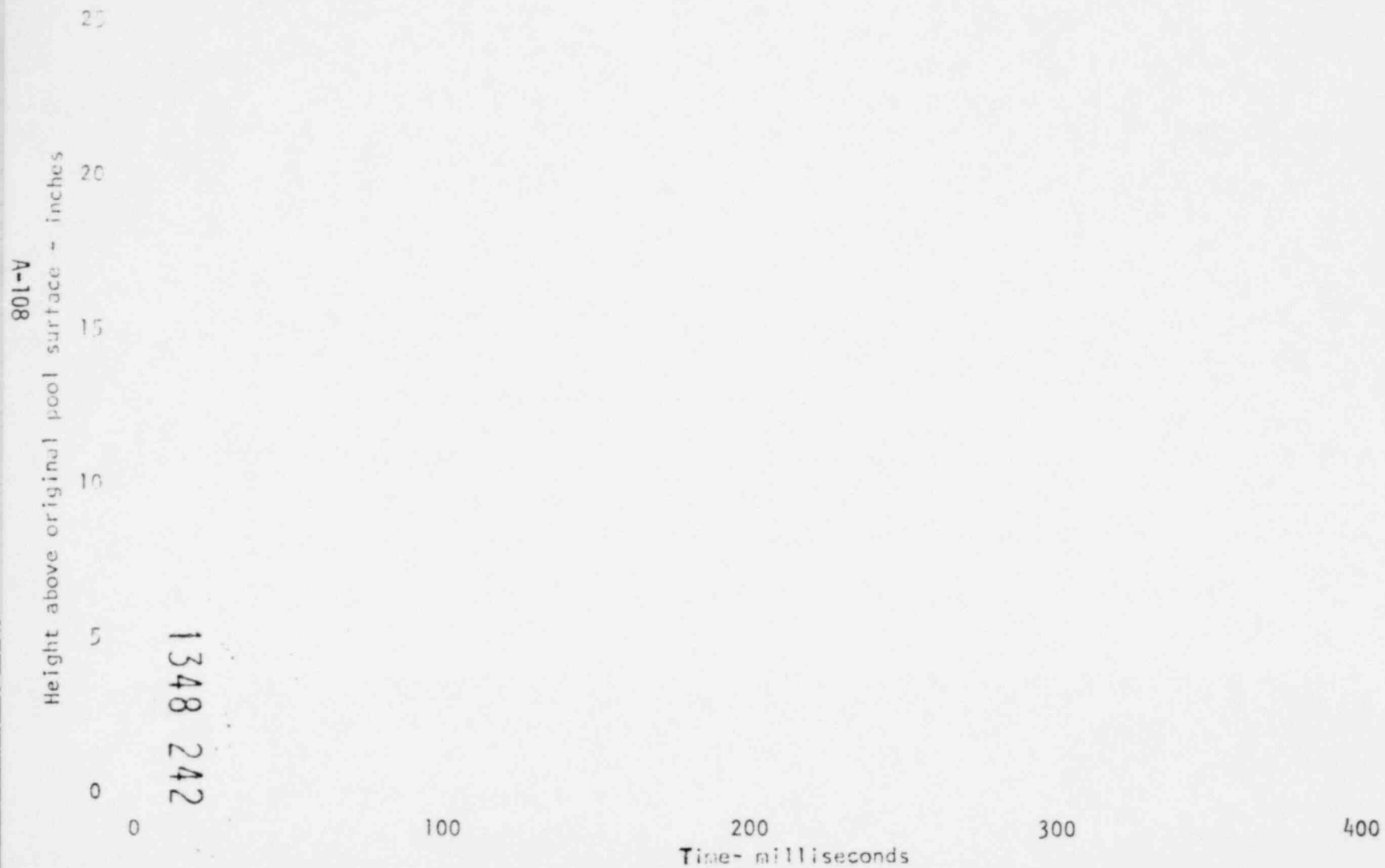


FIGURE A-95 POOL SURFACE VELOCITY PROFILES

PILGRIM, TEST 5

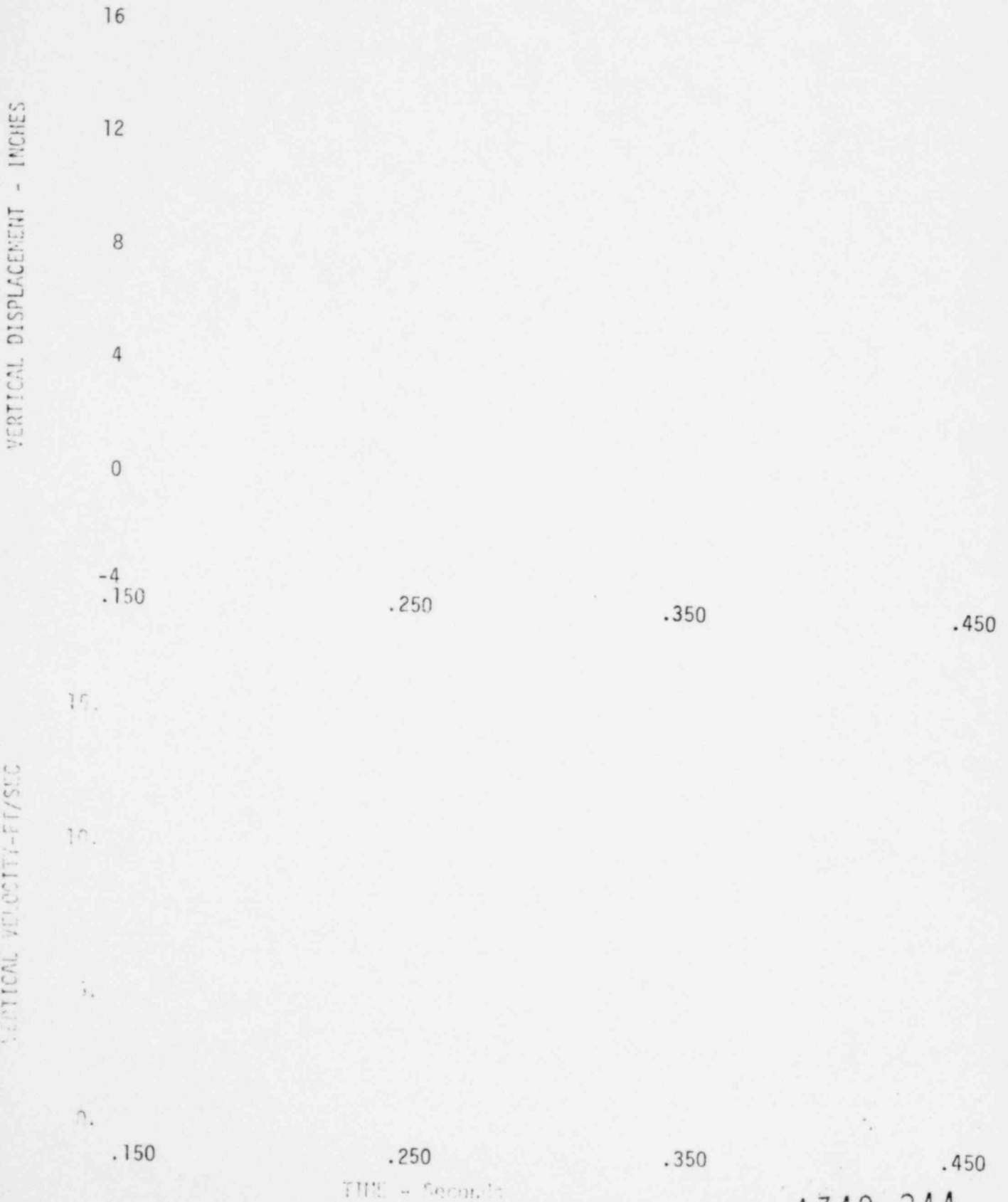


NEDO-21944  
SERIALS CONTINUATION

FIGURE A-96

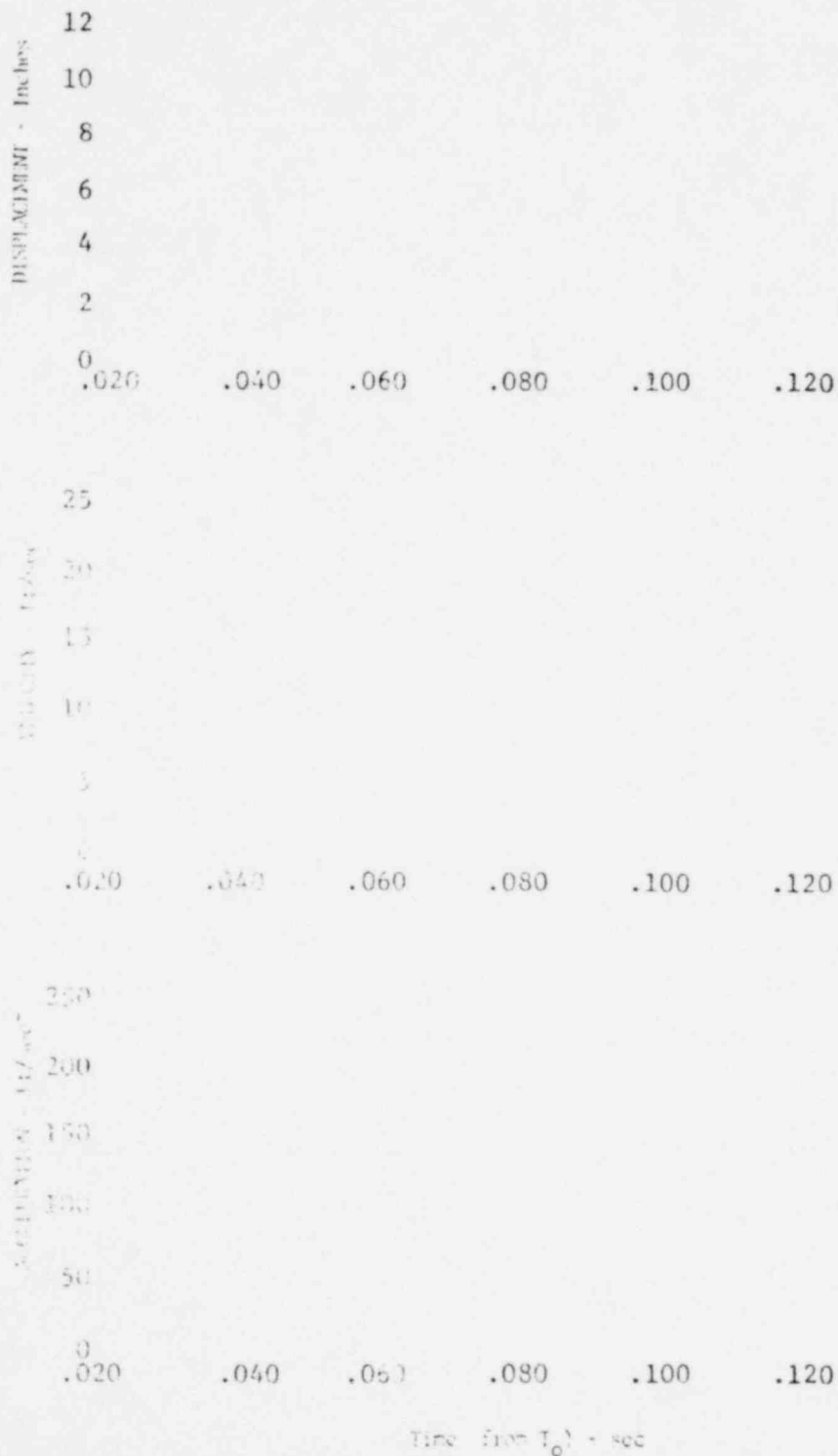
SIDE WINDOW DISPLACEMENT AND VELOCITY PROFILES

PILGRIM, TEST 4



DOWNHOLE WATER SLUG EJECTION

PILGRIM, TEST 3

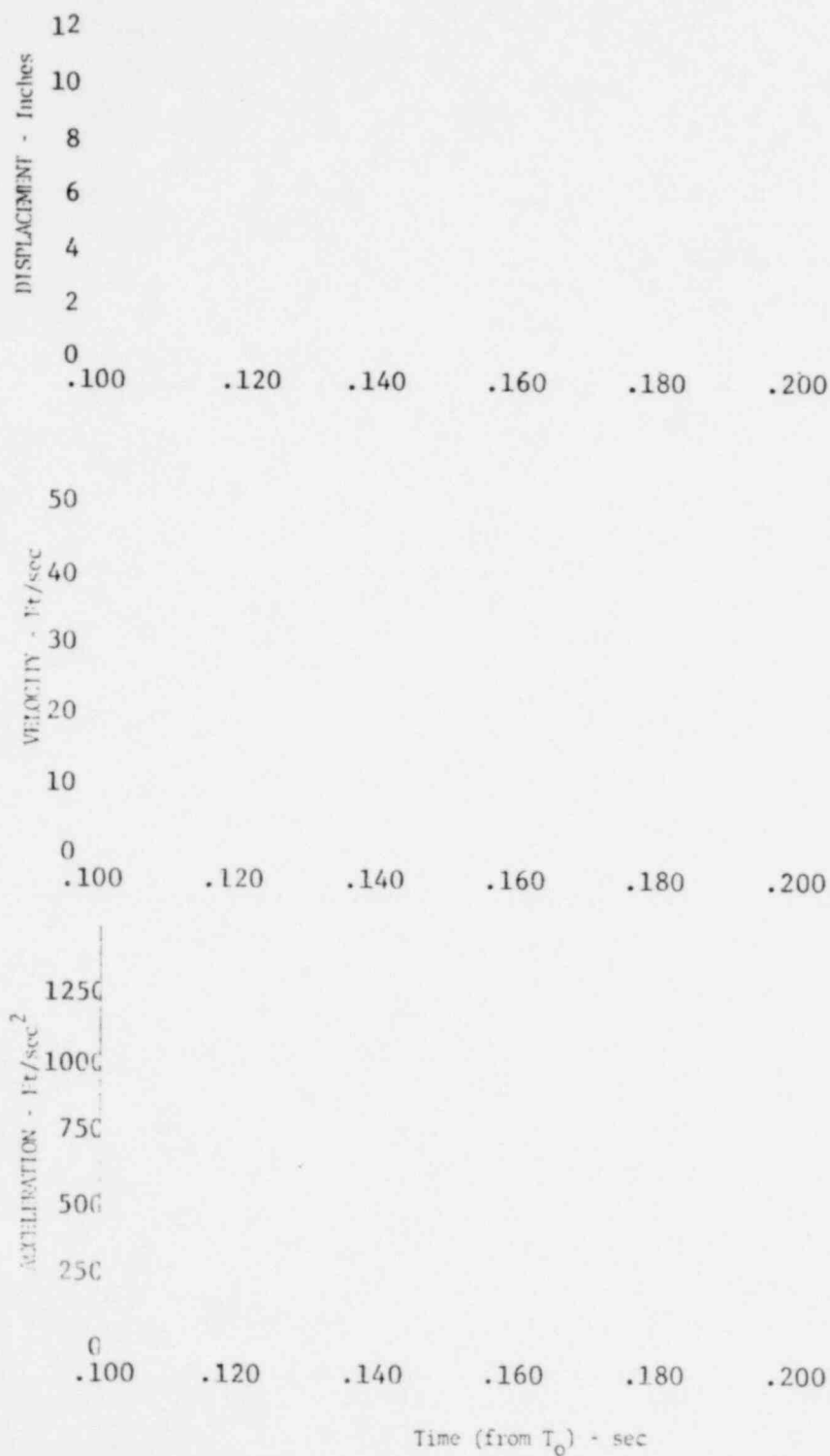


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DOWNCOMER WATER SLUG EJECTION

PILGRIM, TEST 5



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FIGURE A-99

EFFECT OF DRYWELL/WETWELL  $\Delta P$  ON

ENTHALPY FLOW INTO POOL

Pilgrim Tests

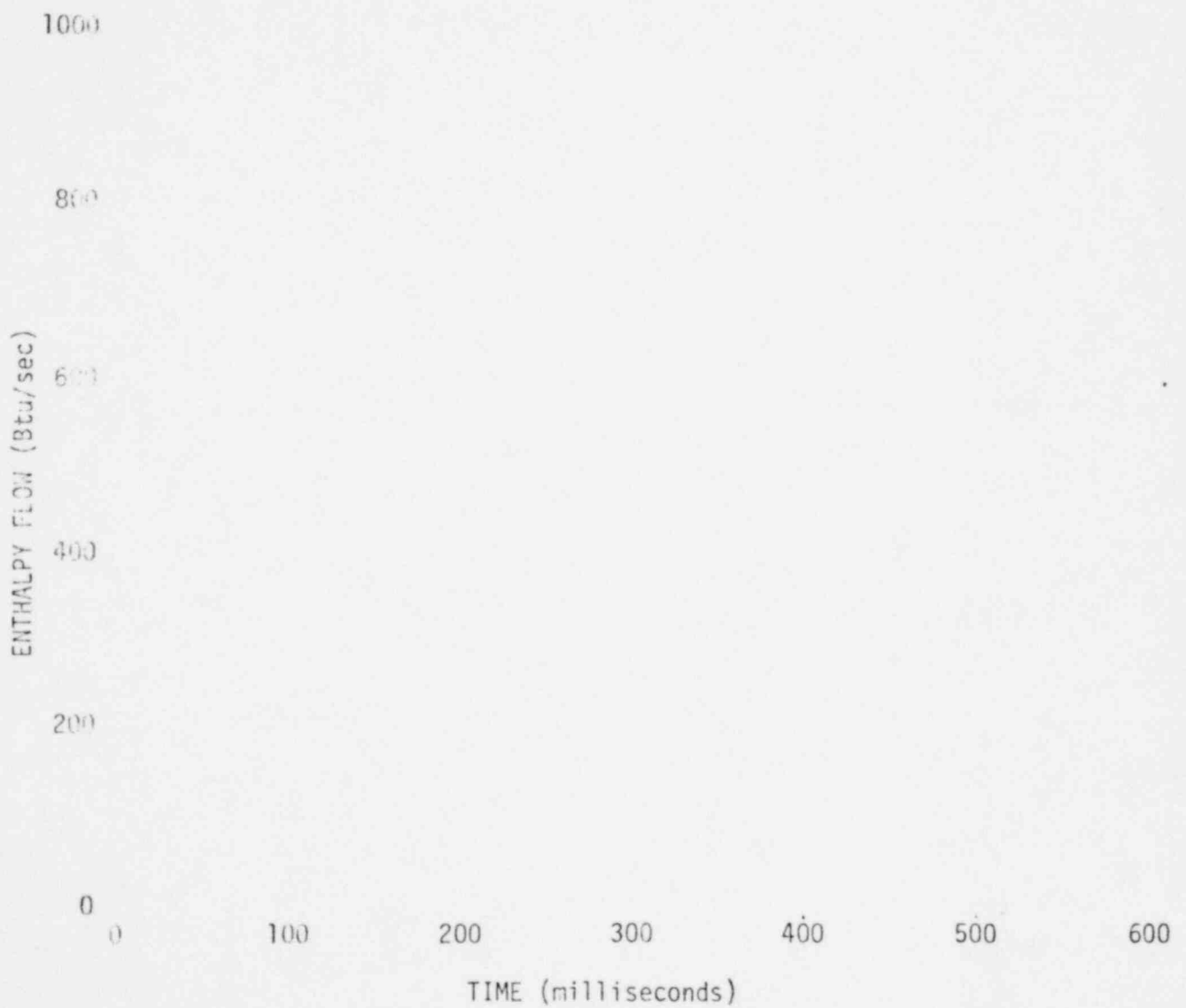
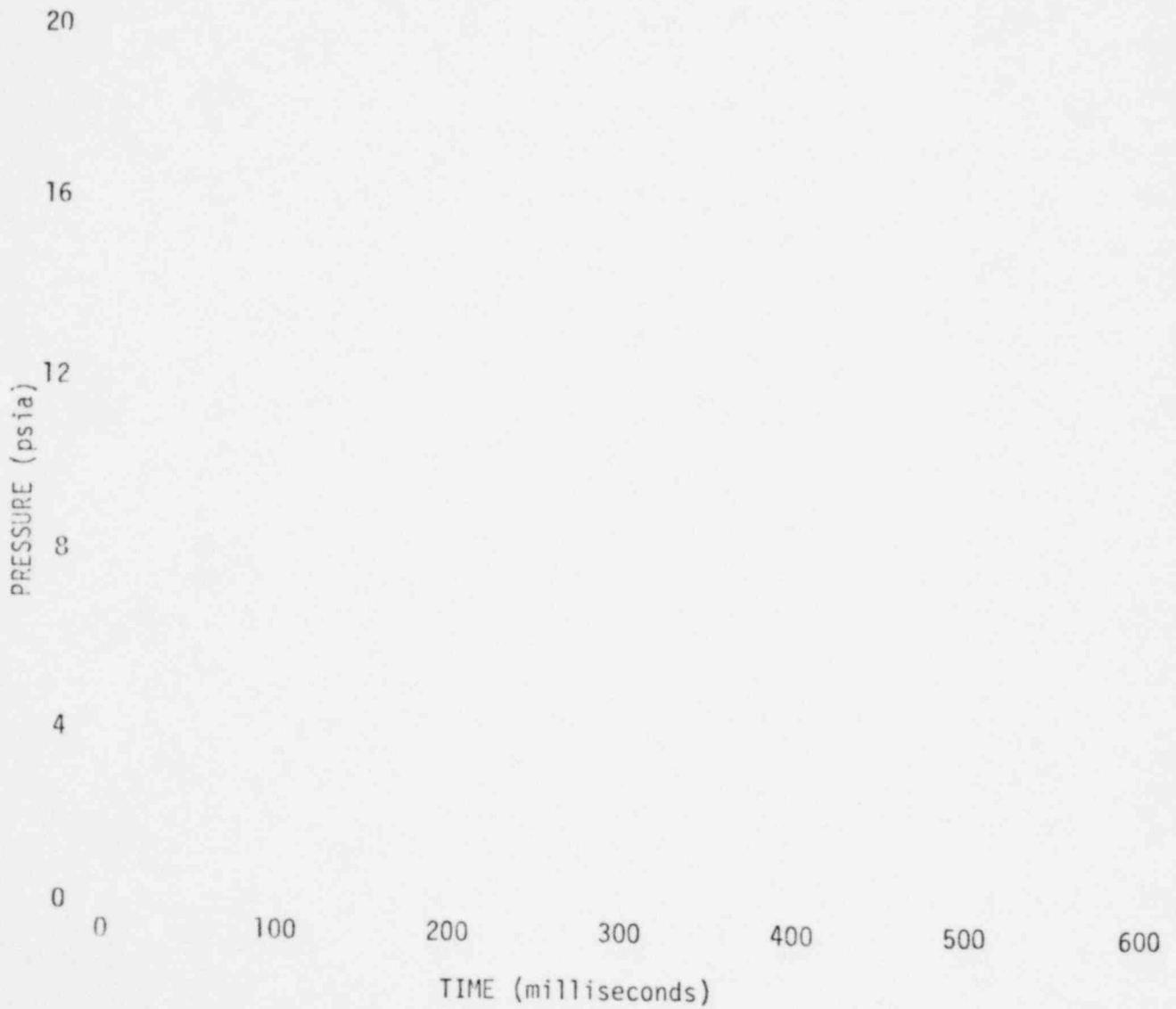


FIGURE A-100  
EFFECT OF DRYWELL/WETWELL  $\Delta P$  ON  
DOWNCOMER INTERNAL PRESSURE  
Pilgrim Tests



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FIGURE A-101

EFFECT OF DRYWELL/WETWELL  $\Delta P$  ON POOL PRESSURE

AT 180 DEGREE AND FREESPACE PRESSURE

Pilgrim Tests

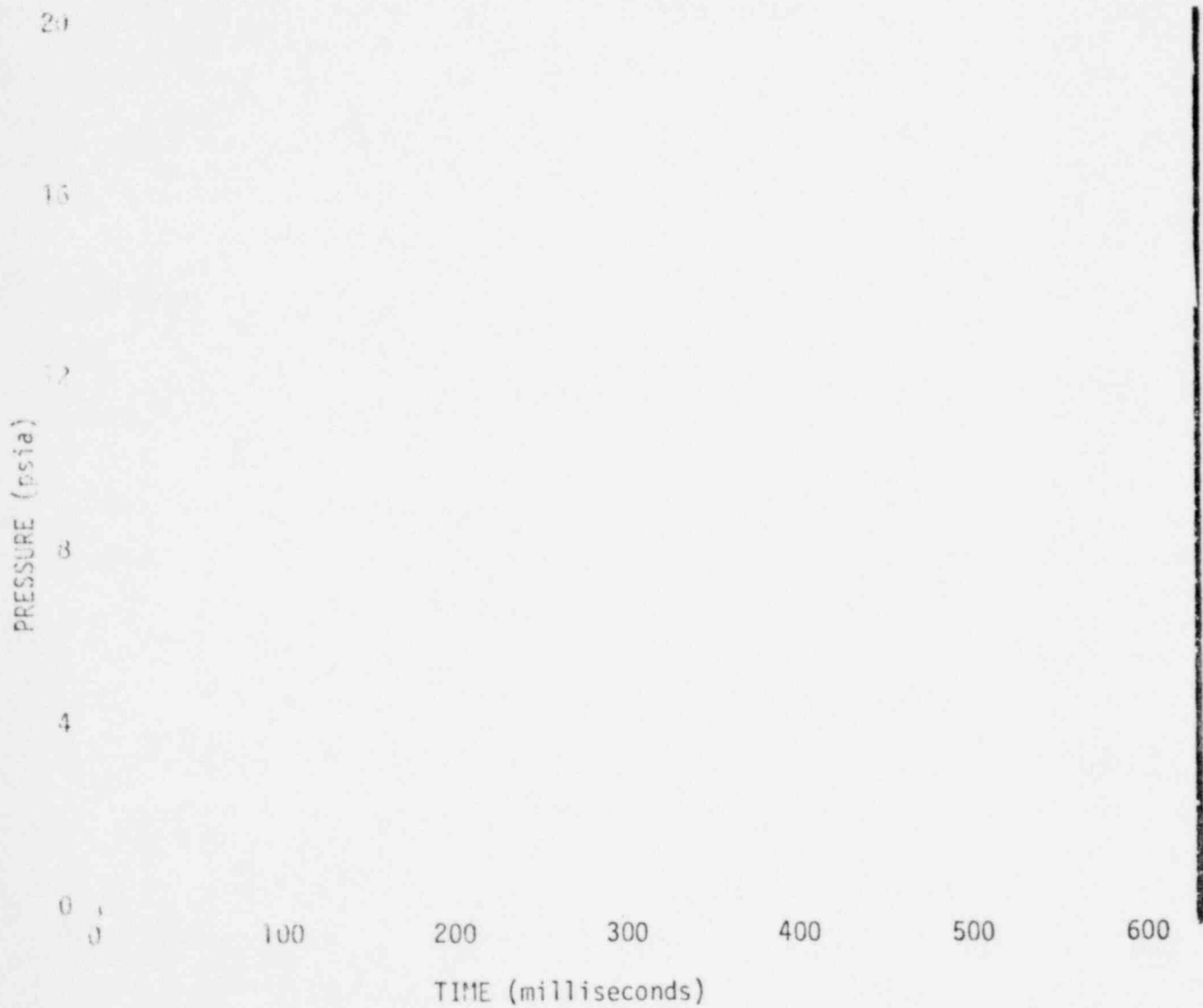


TABLE A-4  
DATA FOR WETWELL VERTICAL LOADS  
Task 5.5.3-2 Pilgrim Tests

\*Vent clearing time (from  $T_0$ ) determined from the movie films.  
\*\*Time difference from  $T_0$  to time of zero downforce.  
—No significant downforce valley or 2nd peak downforce.  
\*(1) Start-of-test reference time

Parameter	Test No.	10.9" $\Delta P$ , 4.20" Deflector				Mean	Std. Dev.	0" $\Delta P$
		(1)	(2)	(3)	(4)			(5)
*(1)								
$T_0$	(sec)							
Vent Clearing Time*	(sec)							
Peak Downforce								
Pressure Integral:								
Force	(lb)							
Time (from $T_0$ )	(sec)							
Corrected Pressure Integral:								
Force	(lb)							
Time (from $T_0$ )	(sec)							
Corrected Load Cell:								
Force	(lb)							
Time (from $T_0$ )	(sec)							
Downforce Valley								
Pressure Integral:								
Force	(lb)							
Time (from $T_0$ )	(sec)							
Corrected Pressure Integral:								
Force	(lb)							
Time (from $T_0$ )	(sec)							
Corrected Load Cell:								
Force	(lb)							
Time (from $T_0$ )	(sec)							
2nd Peak Downforce								
Pressure Integral:								
Force	(lb)							
Time (from $T_0$ )	(sec)							
Corrected Pressure Integral:								
Force	(lb)							
Time (from $T_0$ )	(sec)							
Corrected Load Cell:								
Force	(lb)							
Time (from $T_0$ )	(sec)							
[ $\Delta t$ ] Downforce Time**								
Pressure Integral	(sec)							
Corrected Pressure Integral	(sec)							
Corrected Load Cell	(sec)							
Downforce Impulse								
Pressure Integral:								
Impulse	(lb-sec)							

\*Time at force is zero (from  $T_0$ )  
 \*(1) Data not available

TABLE A-4 (Continued)  
DATA FOR WETWELL VERTICAL LOADS (continued)

Task 5.5.3-2 Pilgrim Tests

Parameter	Test No.	10.9" ΔP, 4.20" Deflector				Std. Dev.	0" ΔP
	(1)	(2)	(3)	(4)	Mean		(5)
<u>Peak Upforce</u>							
Pressure Integral:							
Force	(1b)						
Time (from T <sub>0</sub> )	(sec)						
Corrected Pressure Integral:							
Force	(1b)						
Time (from T <sub>0</sub> )	(sec)						
Corrected Load Cell:							
Force	(1b)						
Time (from T <sub>0</sub> )	(sec)						
<u>Upforce Valley</u>							
Pressure Integral:							
Force	(1b)						
Time (from T <sub>0</sub> )	(sec)						
Corrected Pressure Integral:							
Force	(1b)						
Time (from T <sub>0</sub> )	(sec)						
Corrected Load Cell:							
Force	(1b)						
Time (from T <sub>0</sub> )	(sec)						
<u>2nd Peak Upforce</u>							
Pressure Integral:							
Force	(1b)						
Time (from T <sub>0</sub> )	(sec)						
Corrected Pressure Integral:							
Force	(1b)						
Time (from T <sub>0</sub> )	(sec)						
Corrected Load Cell:							
Force	(1b)						
Time (from T <sub>0</sub> )	(sec)						
<u>Zero Force Time*</u>							
Pressure Integral	(sec)						
Corrected Pressure Integral	(sec)						
Corrected Load Cell	(sec)						

TABLE A-5

DATA FOR VENT HEADER IMPACT LOADS

## Task 5.5.3-2 Pilgrim Tests

Parameter \ Test No.	10.9" $\Delta P$ , 4.20" Deflector				0" $\Delta P$ , 4.20" Deflector	
	( 1 )	( 2 )	( 3 )	( 4 )	Mean Std. Dev.	( 5 )
$T_0 +$ (sec)						
Vent Header Impact						
Pressure Integral:						
Maximum Force (lb)						
Impulse (lb-sec)						
Duration* (sec)						
Load Cell Corrected:††						
Maximum Force (lb)						
Impulse (lb-sec)						
Duration (sec)						
Pool Surface Velocity (ft/sec)						
Time (from $T_0$ )** (sec)						

\*(2) Offset 6" from pool centerline

\* Based on impact pressure measurements

\*\* At start of the first impact pressure recorded

† Start of reference time

†† Represents peak of very noisy data (acceleration corrected);  
mean value would be lower

### A.3 Fermi 2 Tests

#### A.3.1 Typical Data

Time-history plots of the driving conditions and pool response are presented in this section for Fermi 2 Tests 3 and 7. Test 3 was a load definition test conducted with a partial drywell/wetwell differential pressure of 7.03" H<sub>2</sub>O and with a 6.566 inch "T" deflector (25.8" full-scale).<sup>\*</sup> Test 7 was conducted with 0" H<sub>2</sub>O ΔP and with the same "T" deflector.

##### A.3.1.1 Driving Conditions

Driving conditions for Fermi 2 Test 3 are presented in Figures A-102 through A-106. Similar plots for Test 7 are shown in Figures A-107 through A-111. Fermi 2 driving conditions had the same characteristics as the "typical" plant discussed in Section 3.0 of this report.

##### A.3.1.2 Pool Response

Downcomer internal pressure and wetwell pressures for Fermi 2 Tests 3 and 7 are presented in Figures A-112 through A-113 and A-114 through A-115, respectively. Net torus force from the pressure integral (Figures A-116 and A-117) shows relatively smooth upforce but some minor downforce oscillation. Net torus force that is determined from the torus load cell (Figures A-118 and A-120) by applying inertial correction with the torus accelerometer (Figures A-119 and A-121) is shown in Figures A-122 and A-123 and compared to net torus force determined from the pressure integral. Figures A-124 and A-125 present the net torus force based on the torus pressure integral, corrected for inertia.

---

<sup>\*</sup> "T" deflector is a pipe with structural "Ts".

The "average" pool pressures for Fermi 2 Tests 3 and 7 are shown in Figures A-126 and A-128. Figures A-127 and A-129 are the same as Figures A-124 and A-125 with force replaced by average pressure (force/torus projected area).

The vent header impact pressures for Fermi 2 Test 3 are presented in Figures A-130 through A-133. These figures indicate that the "T" deflector was effective in mitigating vent header impact. Vent header vertical acceleration measurements from Tests 3 and 7 are shown in Figures A-134 and A-135, respectively.

#### A.3.2 Pool Dynamics

The pool contours at various times of pool swell are shown in Figures A-136 through A-139 for Fermi 2 Tests 1, 2, 3, and 5.

Pool surface displacement curves for Tests 1, 2, and 3 are shown in Figure A-140. The pool surface velocity profiles for Tests 1, 2, and 3 are shown in Figure A-141. The pool surface displacement graph and pool surface velocity profiles for Test 5 are shown in Figures A-142 and A-143, respectively.

The pool surface displacement and velocity profile viewed from the side window during Test 4 are shown in Figure A-144. The downcomer water slug displacement, velocity, and acceleration versus time for Tests 3 and 7 are presented in Figures A-145 and A-146.

#### A.3.3 Data Summaries

Tables A-6 and A-7 present the Fermi 2 test data for wetwell vertical forces.

Table A-8 presents the Fermi 2 test data for vent header impact forces.

#### A.3.4 Discussion and Analysis

Figure A-147 presents the effect of drywell/wetwell  $\Delta P$  on enthalpy flow into the bubbles. Effect of  $\Delta P$  on downcomer internal pressure is shown in Figure A-148. Figure A-149 presents the effect of  $\Delta P$  on pool and freespace pressures. This data for Fermi 2 parallels that for the "typical" plant in Section 3.0, except that the air space and pool pressures did not oscillate out of phase, as in the typical plant, after peak upforce.

The Fermi 2 load definition tests were conducted at 7.03"  $H_2O$   $\Delta P$  and with a "T" deflector installed below the vent header.  $\Delta P$  sensitivity tests at 0"  $\Delta P$  were also conducted. Both the downforce and upforce were relatively smooth. The "T" deflector (25.8" full-scale) effectively mitigated vent header impact.

FIGURE A-102

DRYWELL ORIFICE UPSTREAM PRESSURE

Task 5.5.3-2 Fermi 2 Test 3

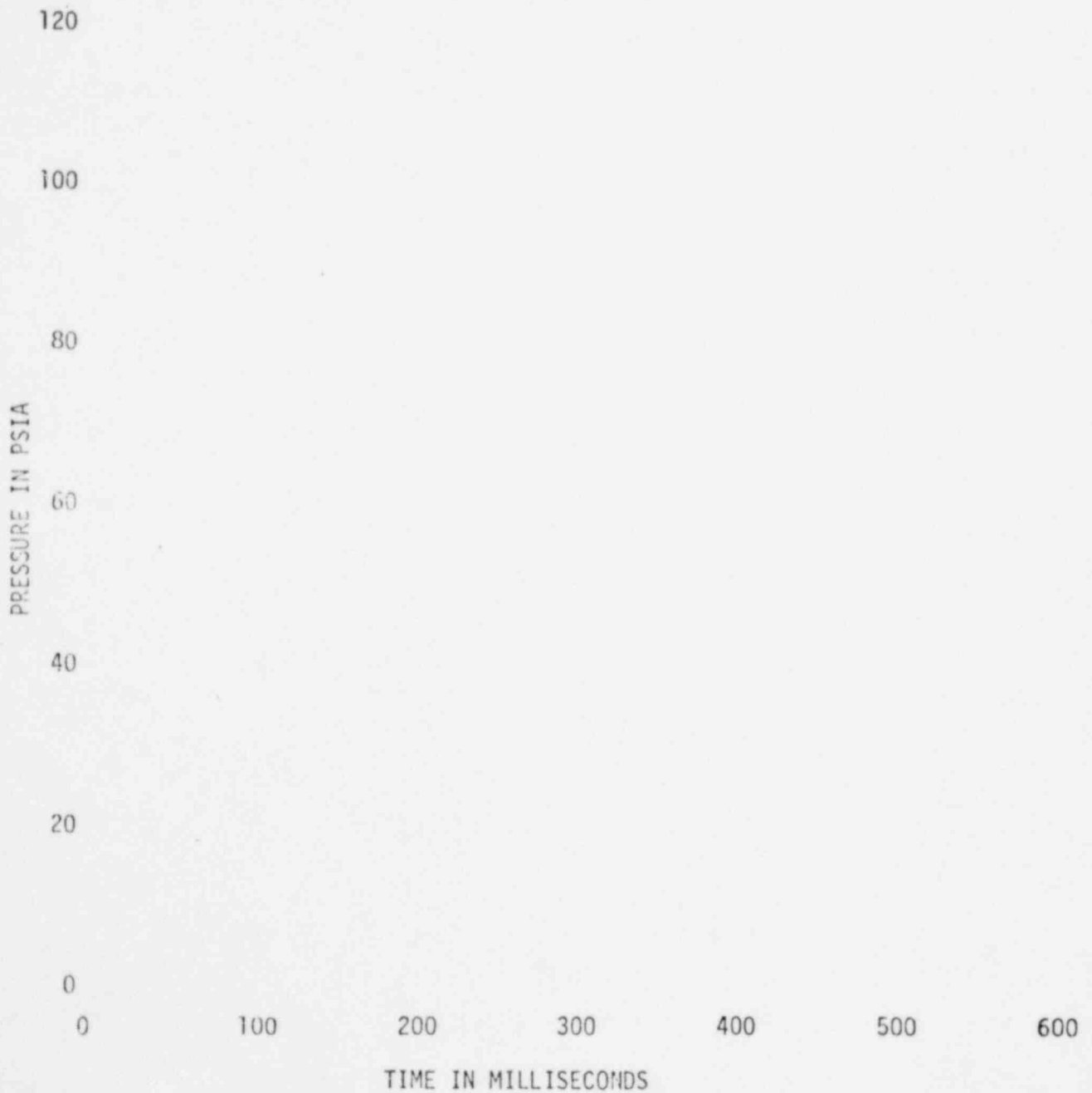
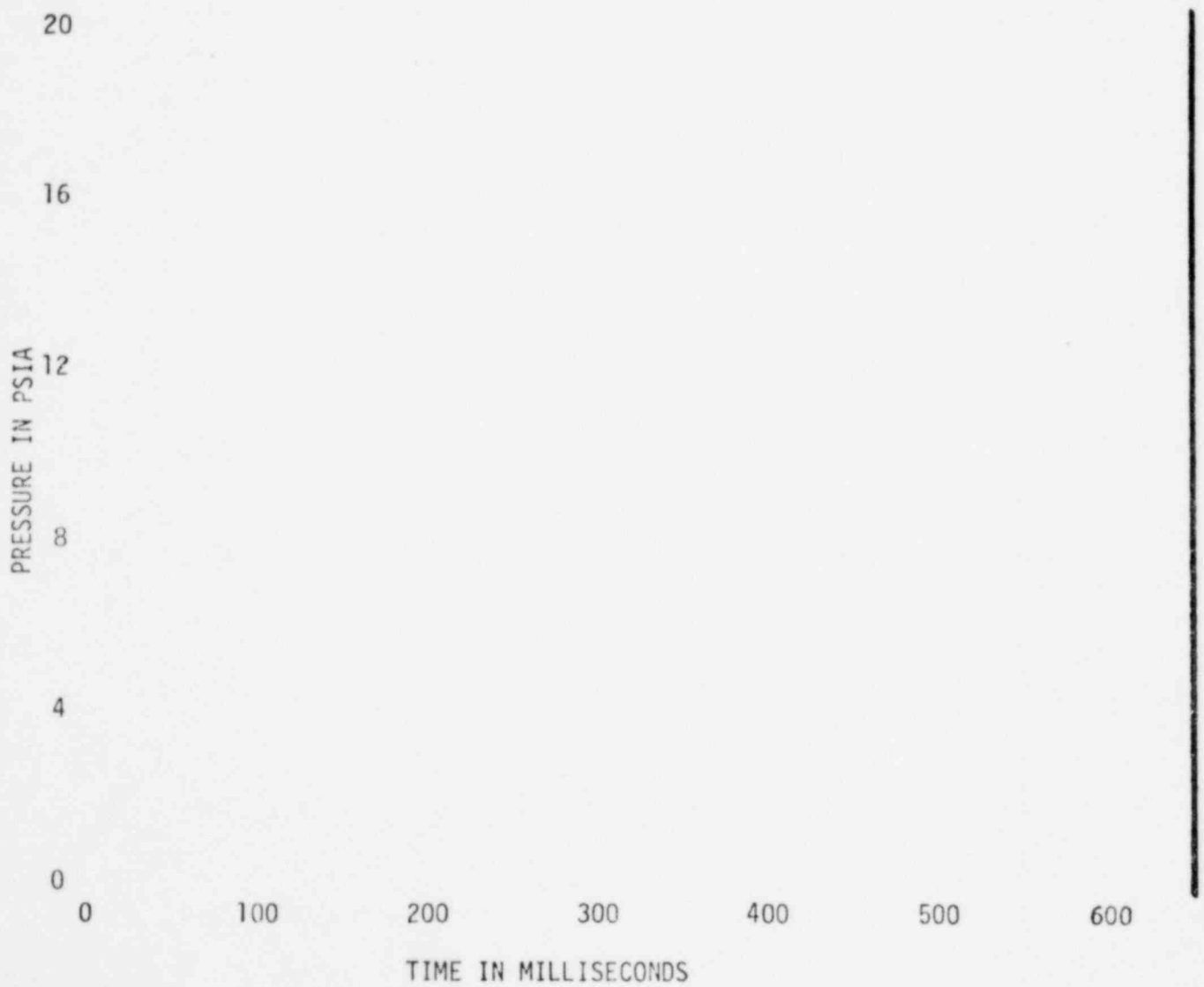


FIGURE A-103

DRYWELL PRESSURE

Task 5.5.3-2 Fermi 2 Test 3



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FIGURE A-104

DOWNCOMER ORIFICE DIFFERENTIAL PRESSURE

Task 5.5.3-2 Fermi 2 Test 3



FIGURE A-105

DOWNCOMER ORIFICE UPSTREAM TEMPERATURE

Task 5.5.3-2 Fermi 2 Test 3



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FIGURE A-106

ENTHALPY FLOW INTO POOL

Task 5.5.3-2 Fermi 2 Test 3

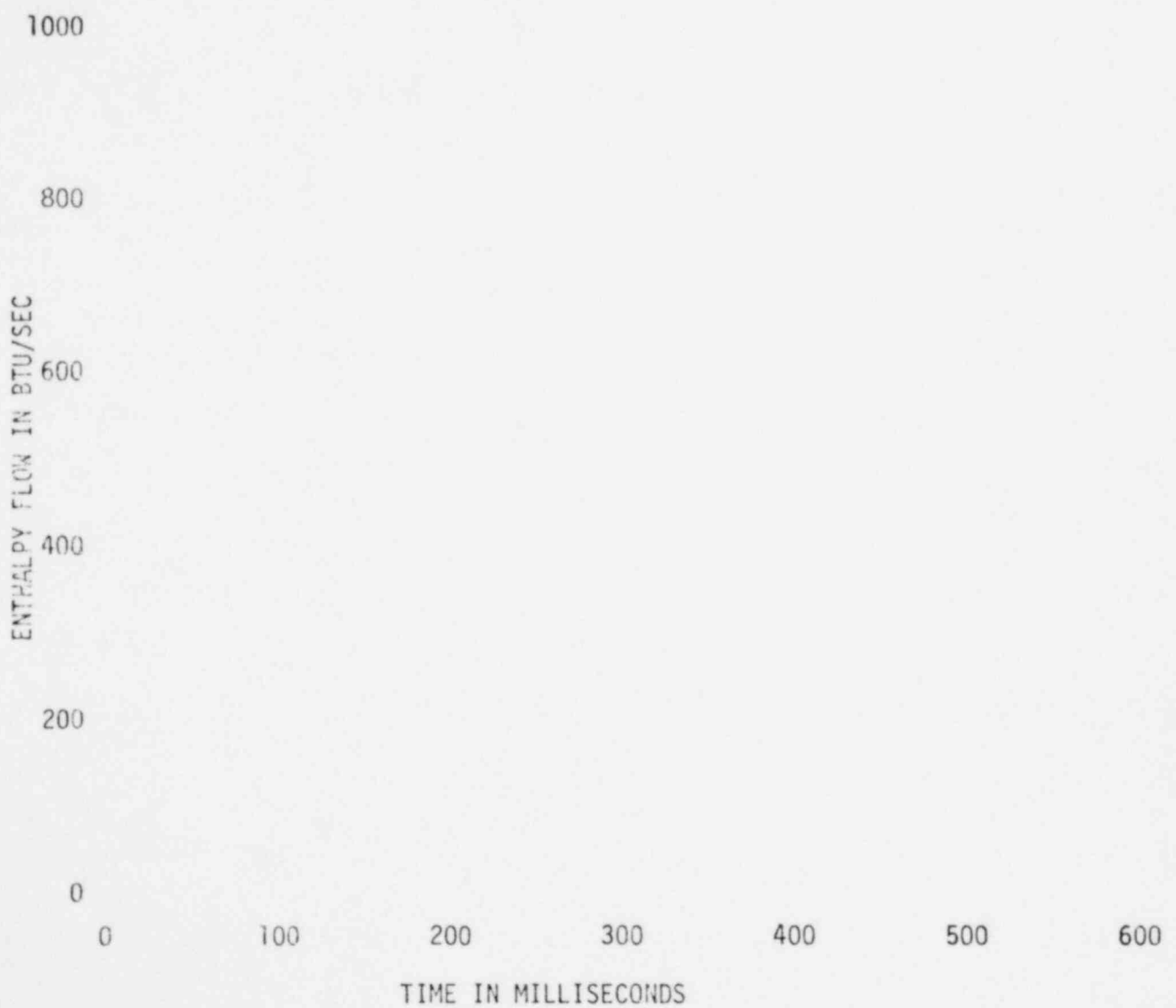
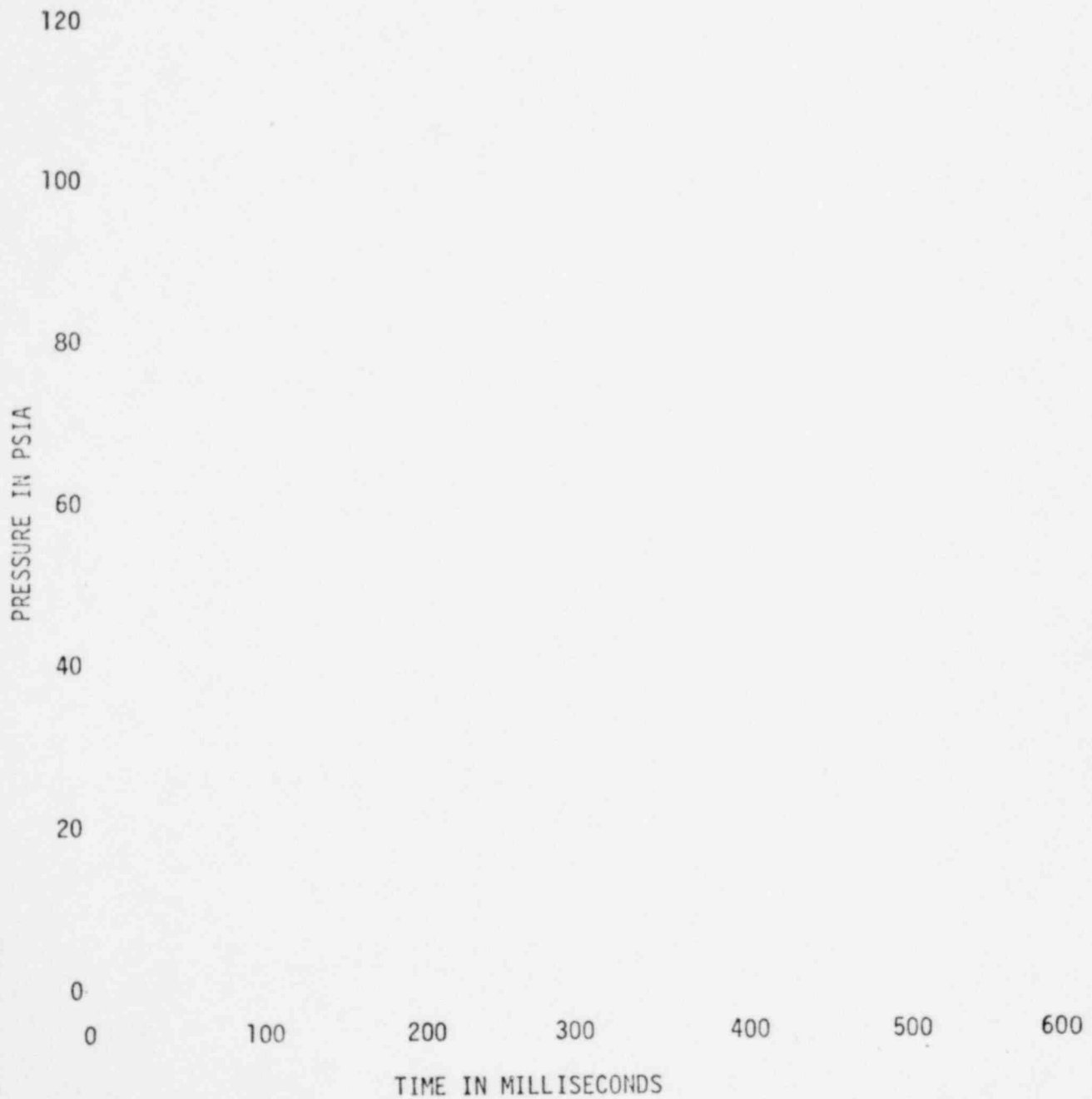


FIGURE A-107

DRYWELL ORIFICE UPSTREAM PRESSURE

Task 5.5.3-2 Fermi 2 Test 7



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FIGURE A-108

DRYWELL PRESSURE

Task 5.5.3-2 Fermi 2 Test 7



FIGURE A-109

DOWNCOMER ORIFICE DIFFERENTIAL PRESSURE

Task 5.5.3-2 Fermi 2 Test 7

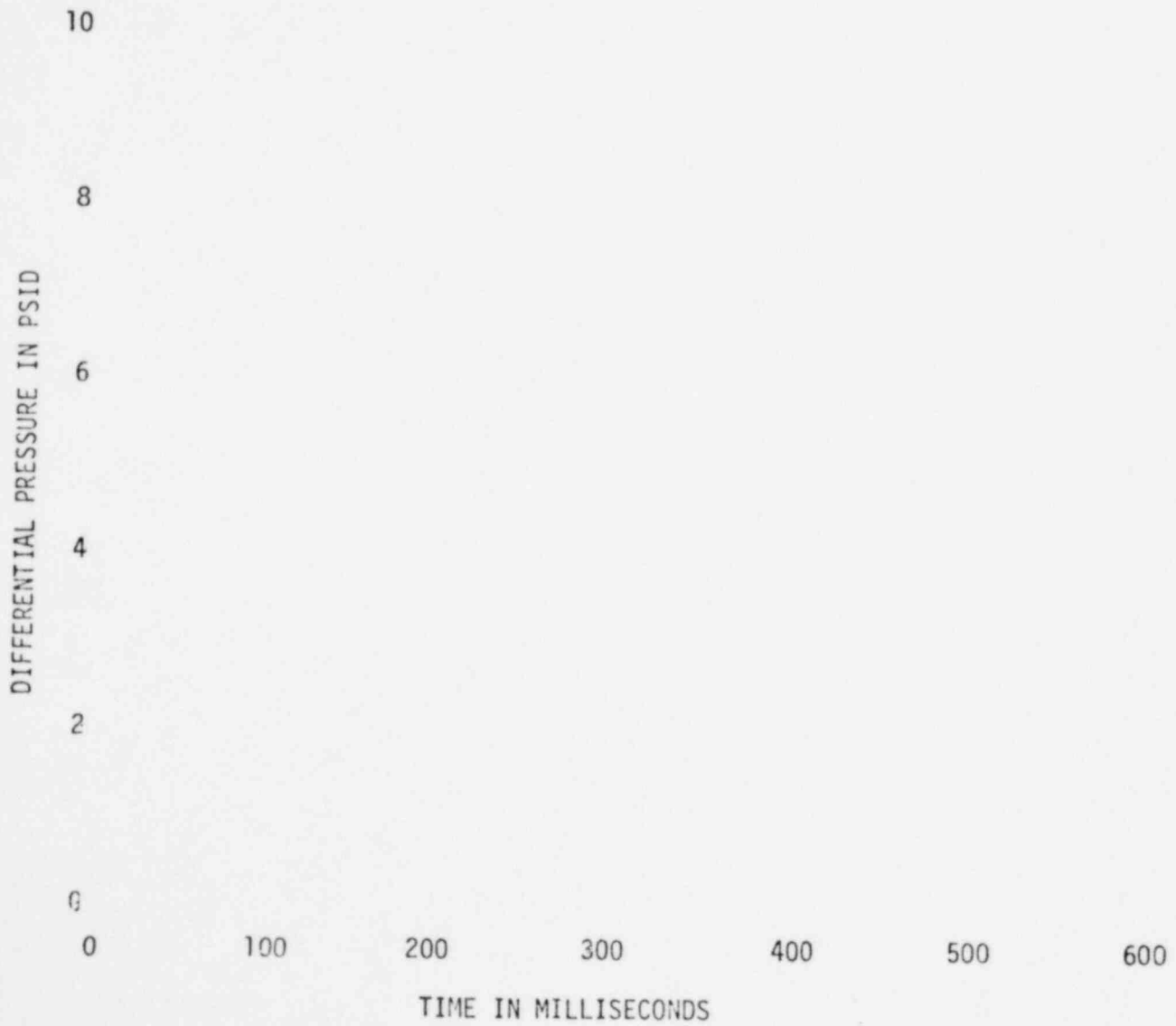


FIGURE A-110

DOWNCOMER ORIFICE UPSTREAM TEMPERATURE

Task 5.5.3-2 Fermi 2 Test 7

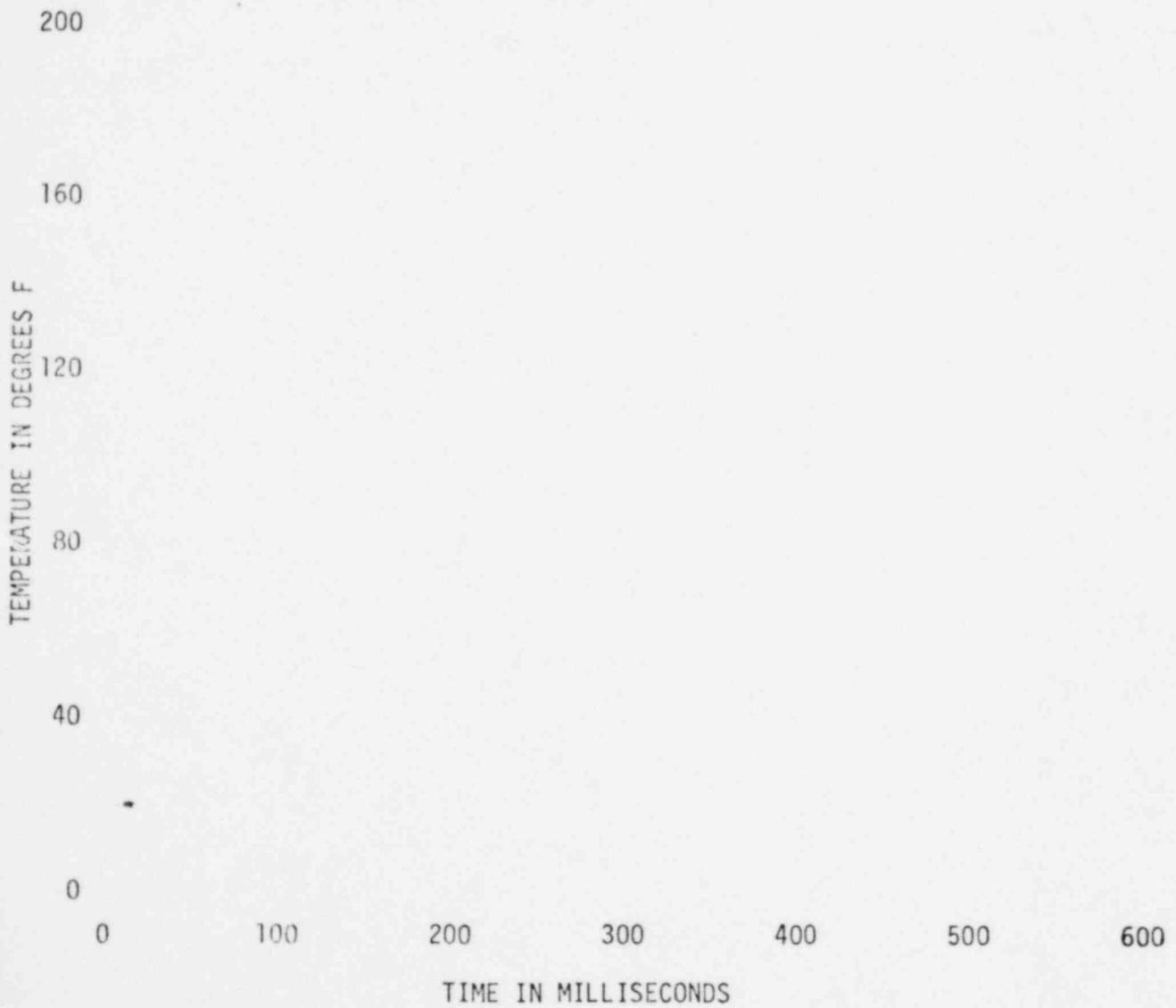


FIGURE A-111

ENTHALPY FLOW INTO POOL

Task 5.5.3-2 Fermi 2 Test 7

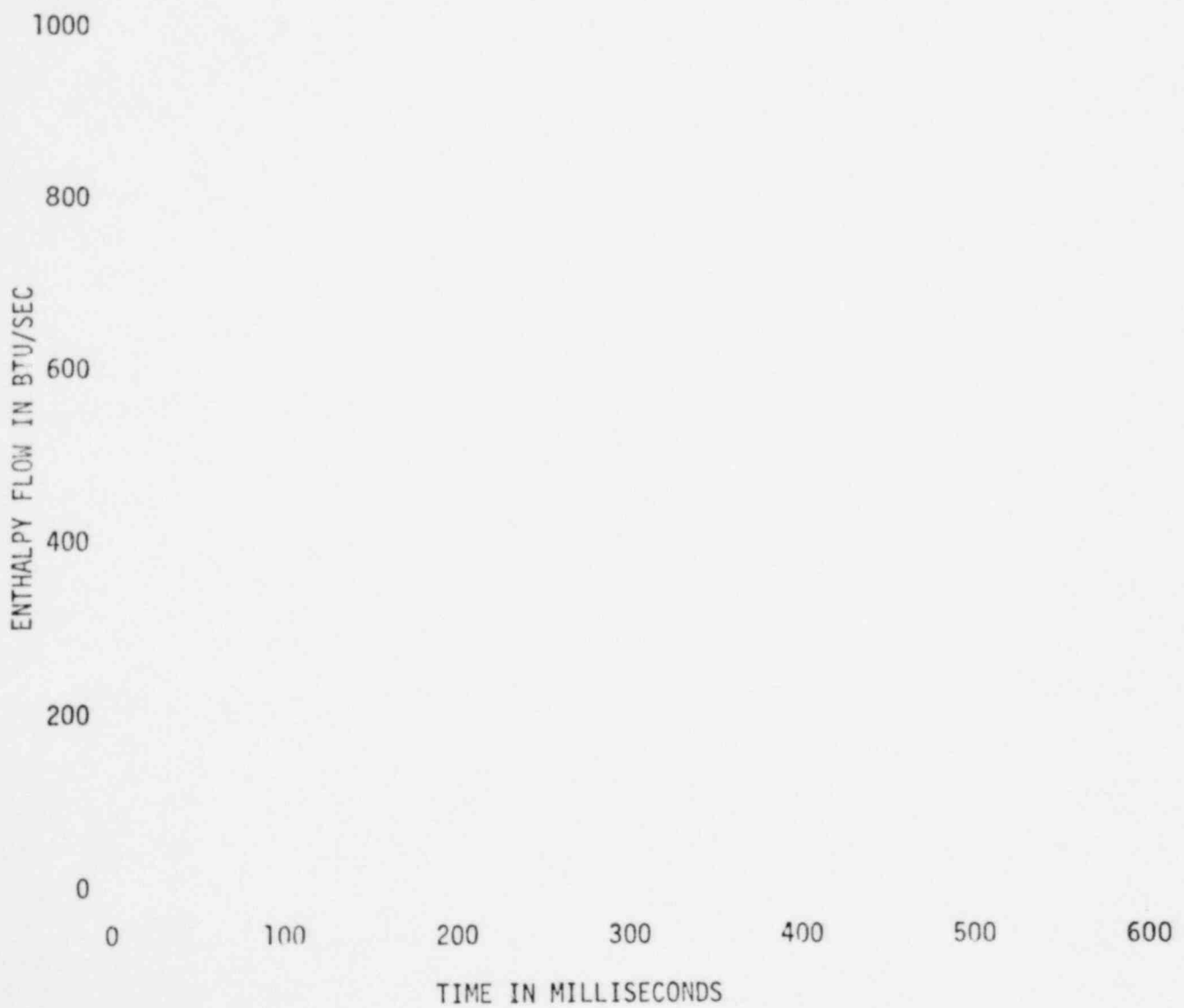


FIGURE A-112

DOWNCOMER INTERNAL PRESSURE

Task 5.5.3-2 Fermi 2 Test 3

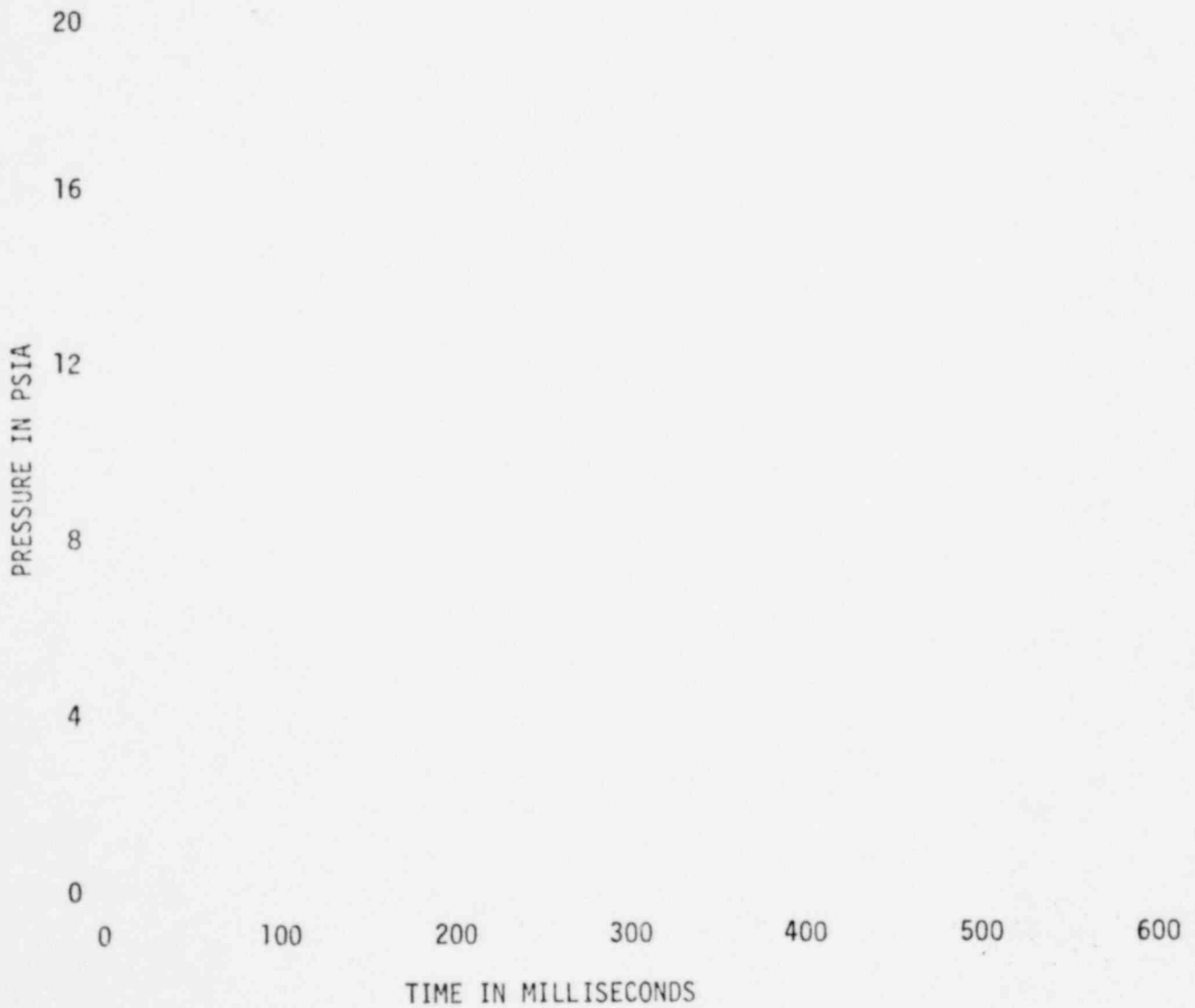


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FIGURE A-113

WETWELL PRESSURES

Task 5.5.3-2 Fermi 2 Test 3



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FIGURE A-114

DOWNCOMER INTERNAL PRESSURE

Task 5.5.3-2 Fermi 2 Test 7

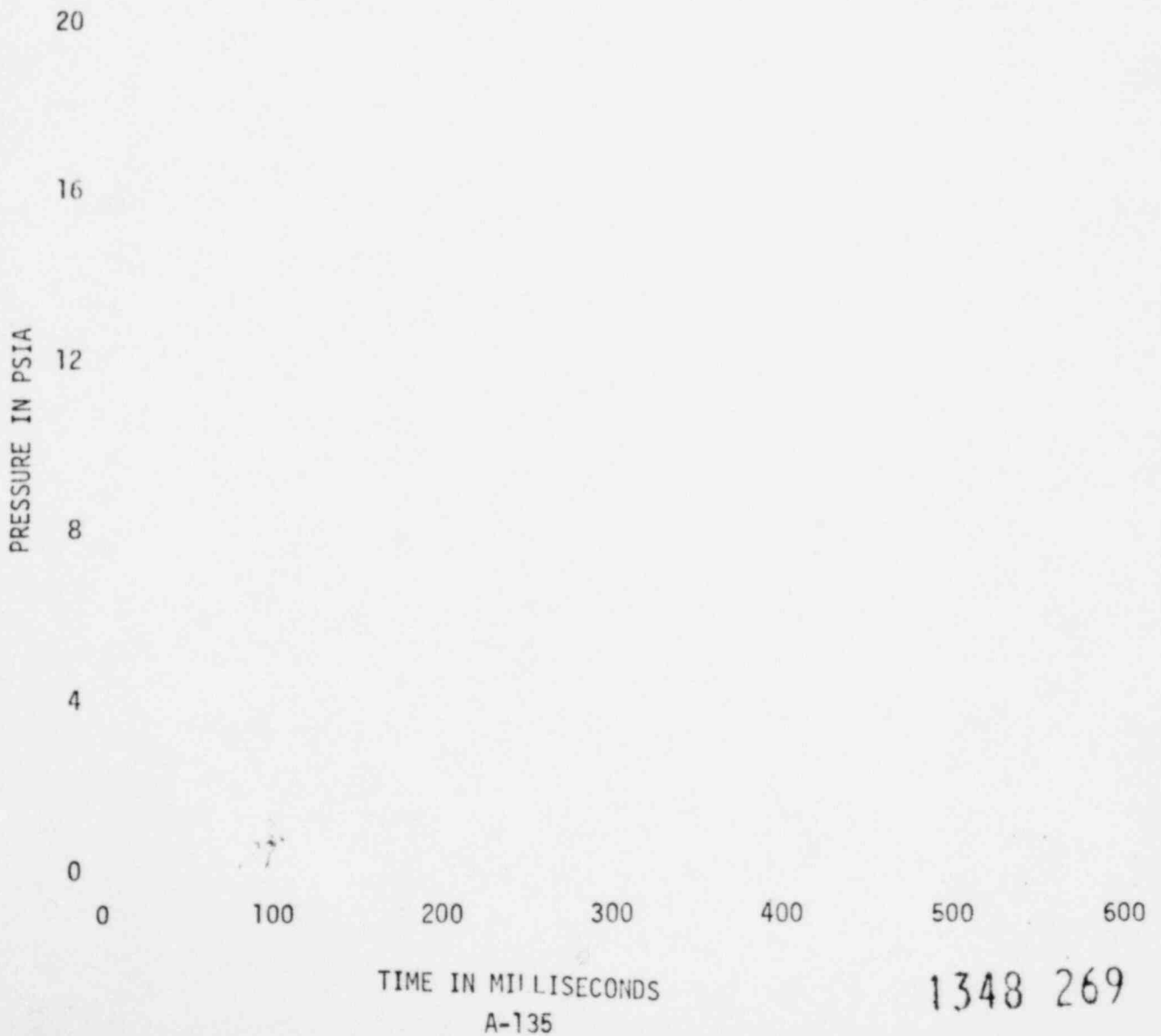


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FIGURE A-115

WETWELL PRESSURES

Task 5.5.3-2 Fermi 2 Test 7



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FIGURE A-116

NET TORUS FORCE FROM PRESSURE INTEGRAL

Task 5.5.3-2 Fermi 2 Test 3

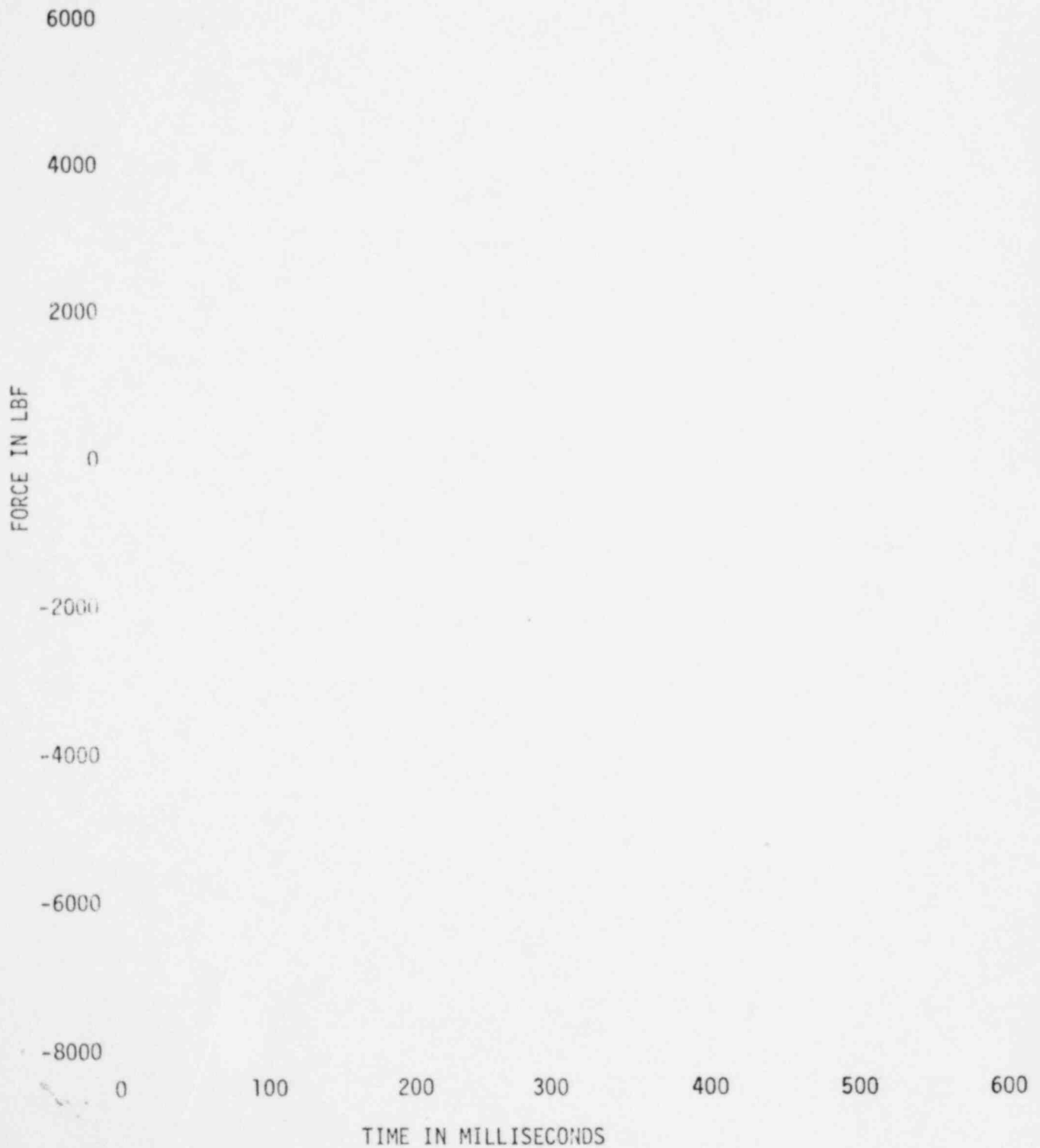


FIGURE A-117

NET TORUS FORCE FROM PRESSURE INTEGRAL

Task 5.5.3-2 Fermi 2 Test 7

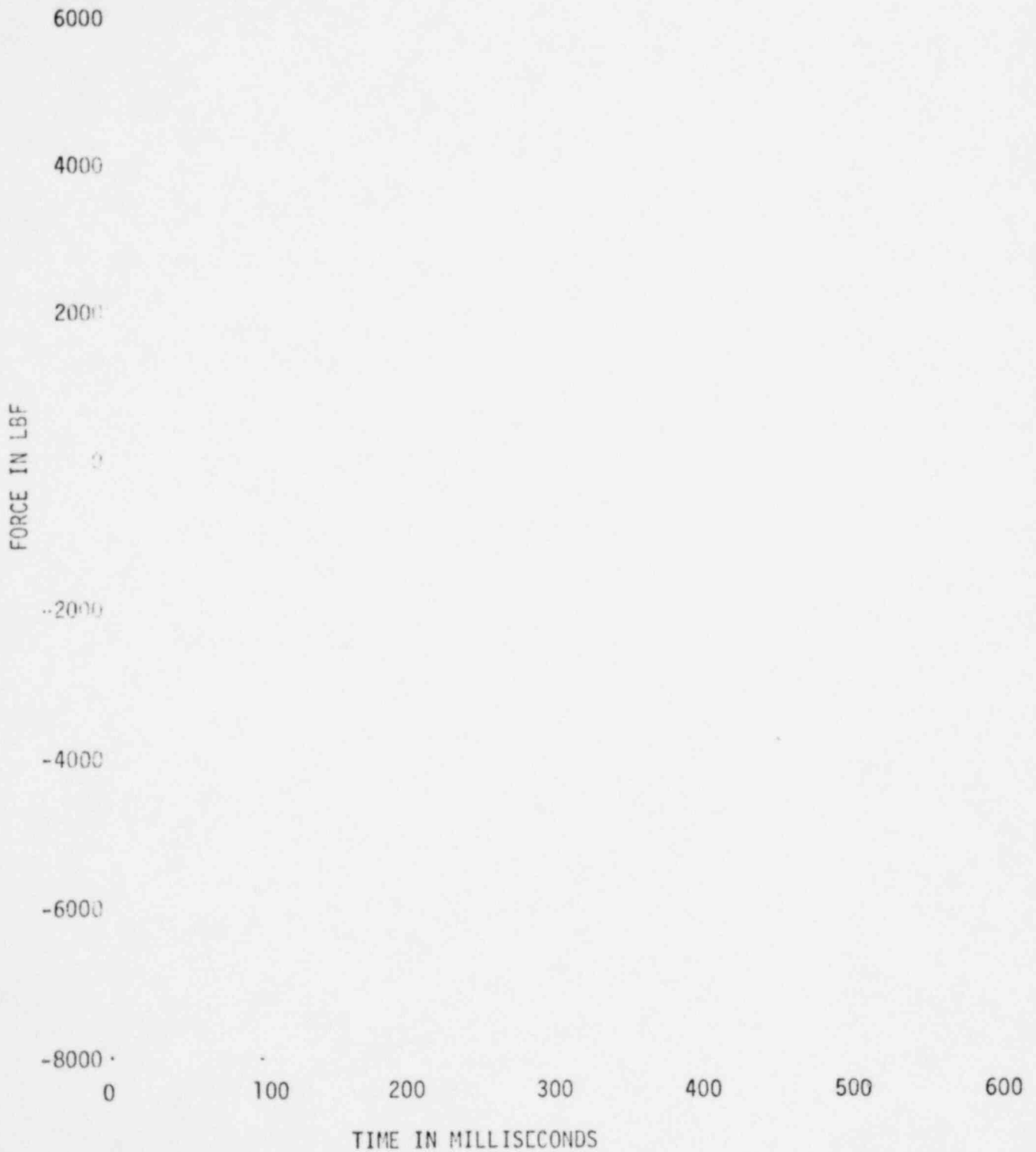


FIGURE A-118

TORUS LOAD CELL

Task 5.5.3-2 Fermi 2 Test 3

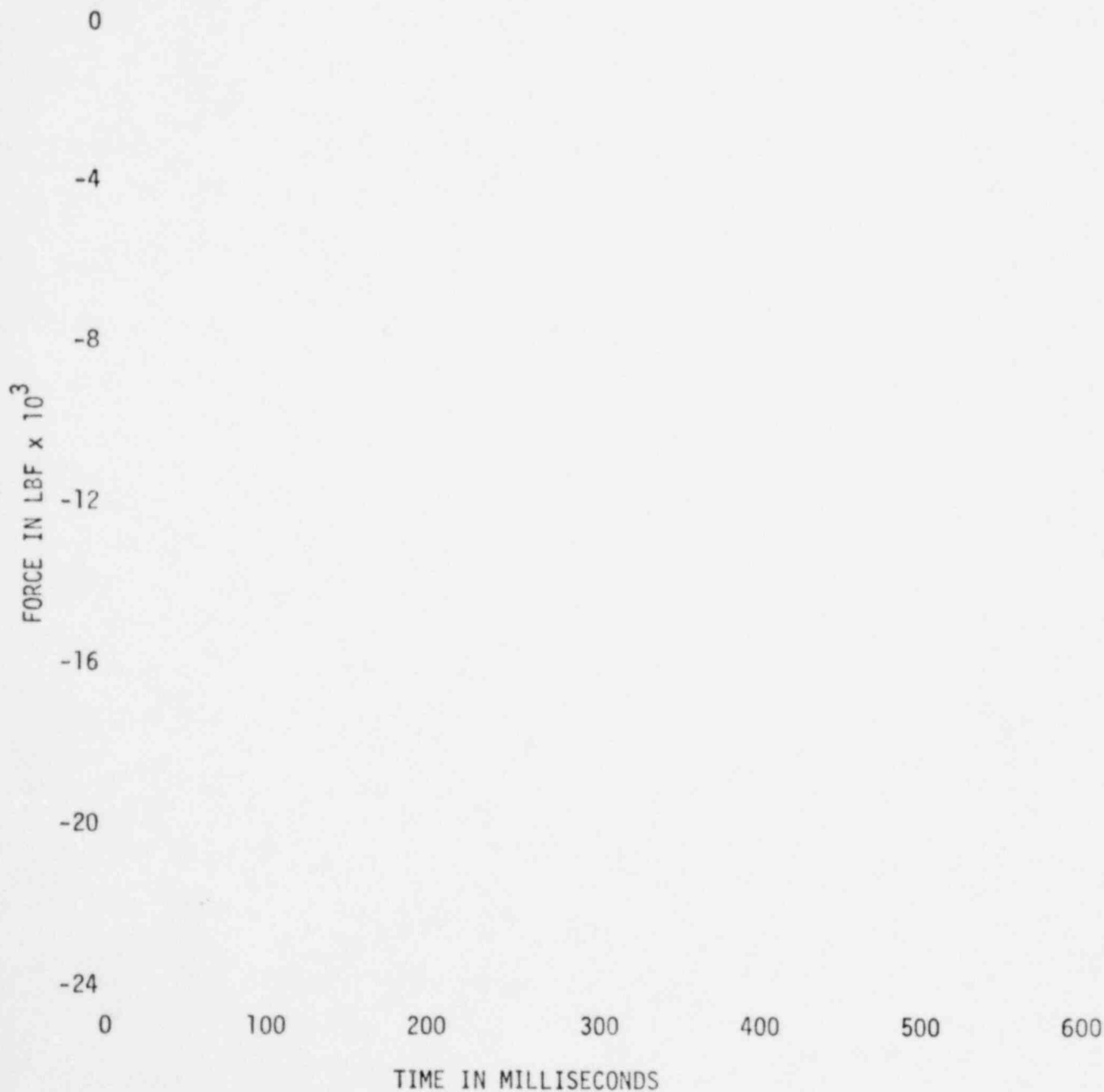


FIGURE A-119

TORUS VERTICAL ACCELERATION

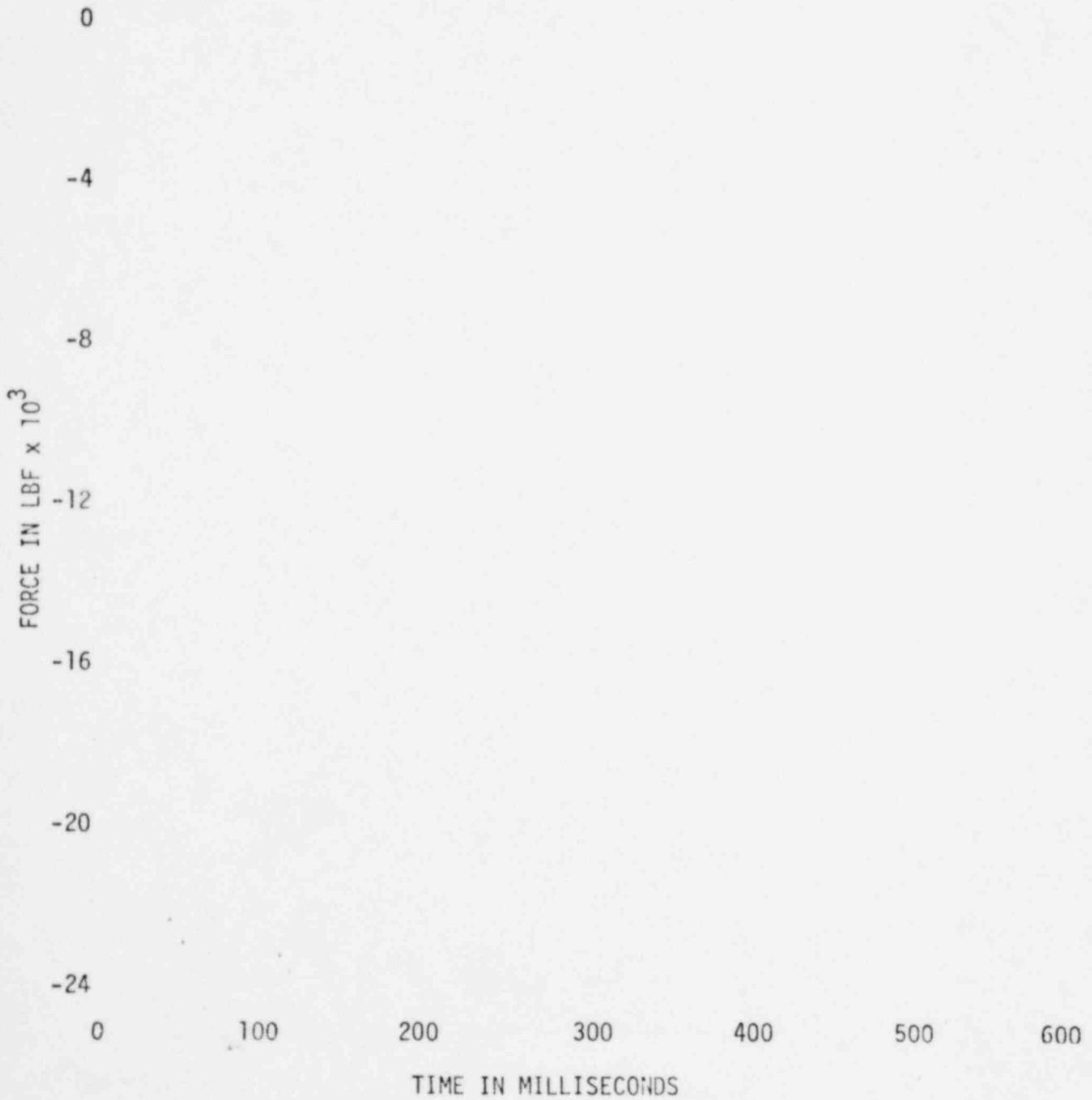
Task 5.5.3-2 Fermi 2 Test 3



FIGURE A-120

TORUS LOAD CELL

Task 5.5.3-2 Fermi 2 Test 7



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FIGURE A-121  
TORUS VERTICAL ACCELERATION  
Task 5.5.3-2 Fermi 2 Test 7



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FIGURE A-122 COMPARISON OF NET TORUS FORCE FROM PRESSURE INTEGRAL  
WITH NET TORUS FORCE FROM LOAD CELL CORRECTED FOR TORUS INERTIA  
Task 5.5.3-2 Fermi Test 3

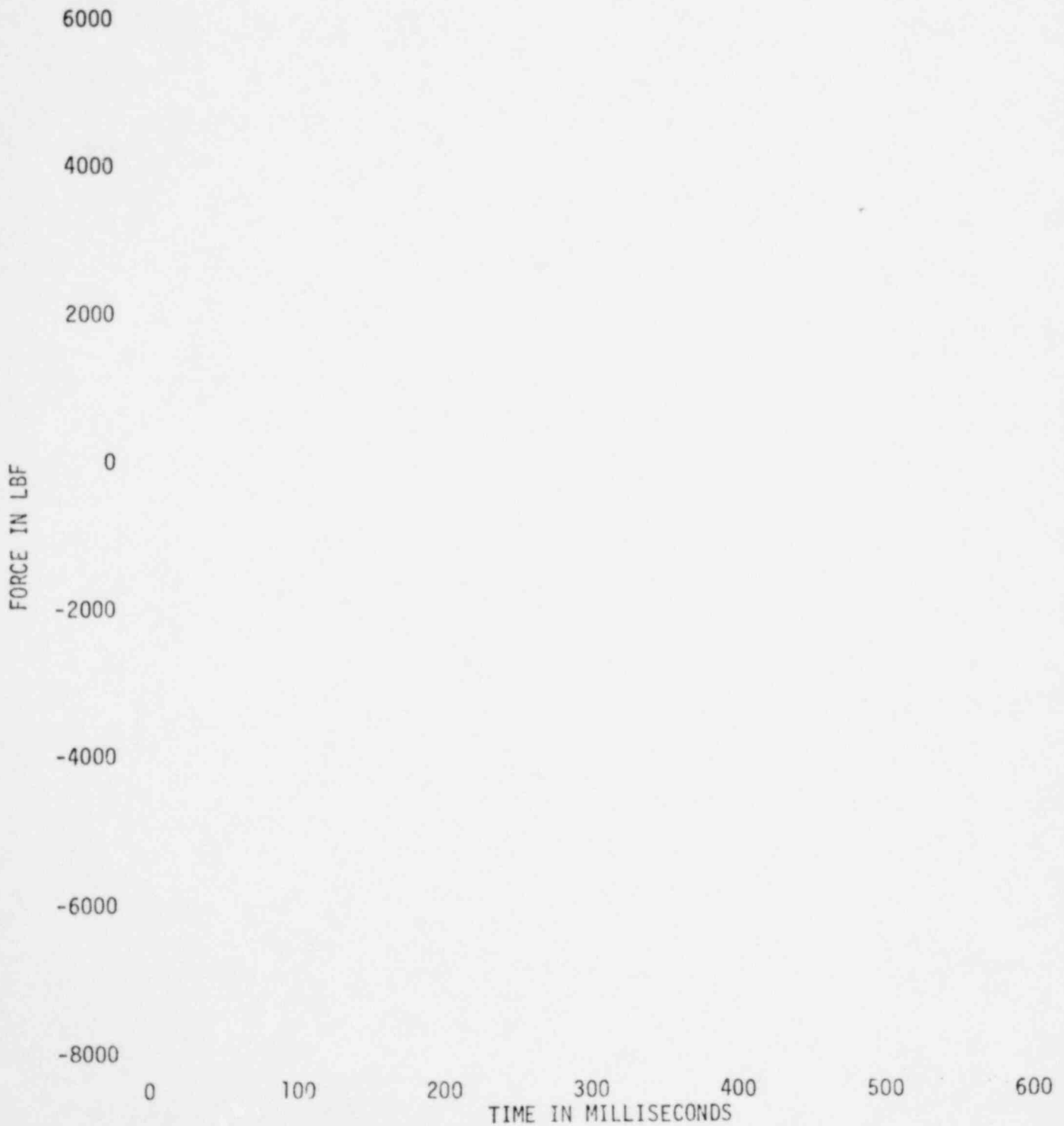
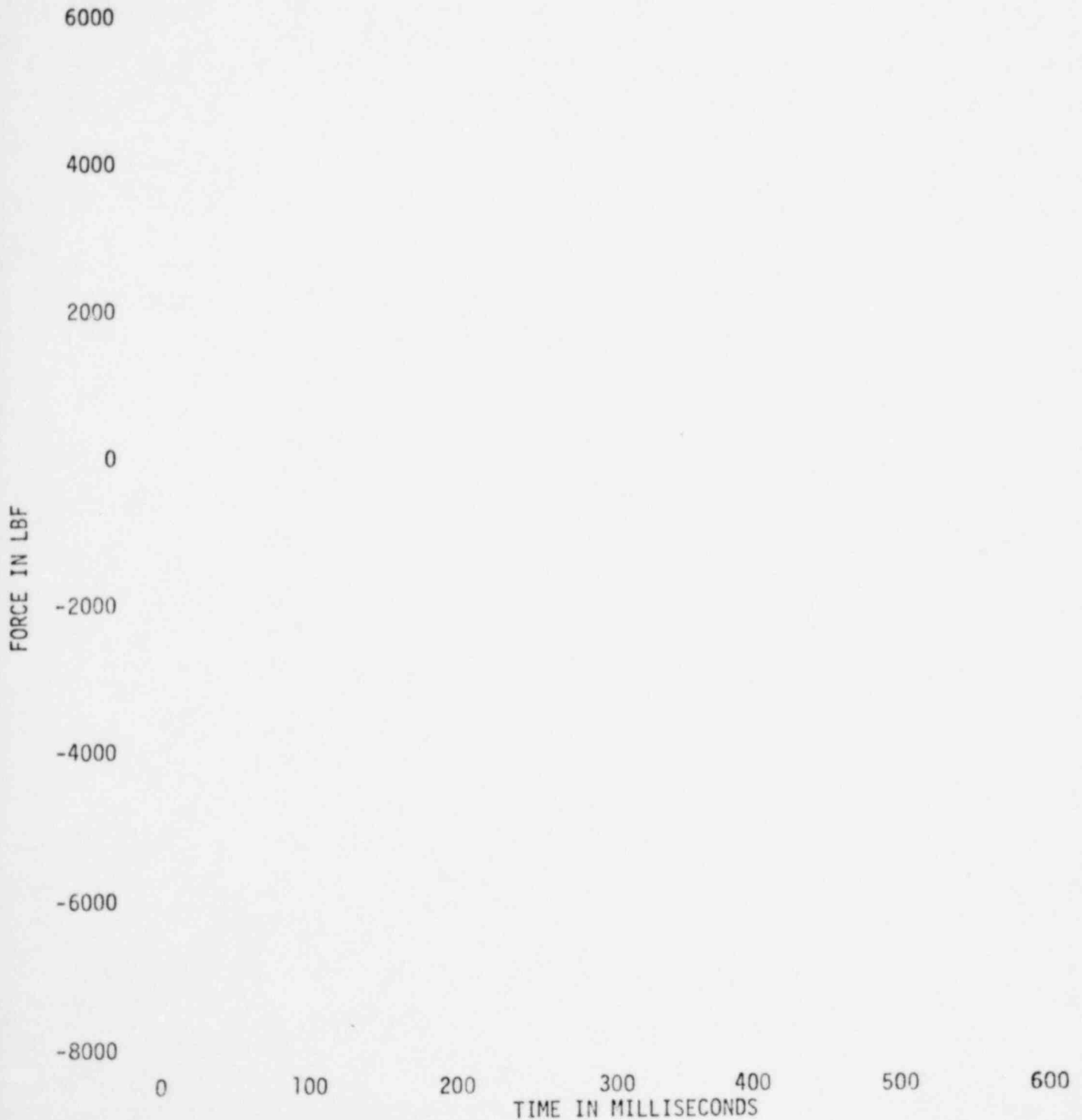


FIGURE A-123 COMPARISON OF NET TORUS FORCE FROM PRESSURE INTEGRAL  
WITH NET TORUS FORCE FROM LOAD CELL CORRECTED FOR TORUS INERTIA  
Task 5.5.3-2 Fermi Test 7



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FIGURE A-124

NET TORUS FORCE FROM PRESSURE INTEGRAL, CORRECTION FOR WATER INERTIA

Task 5.5.3-2 Fermi 2 Test 3

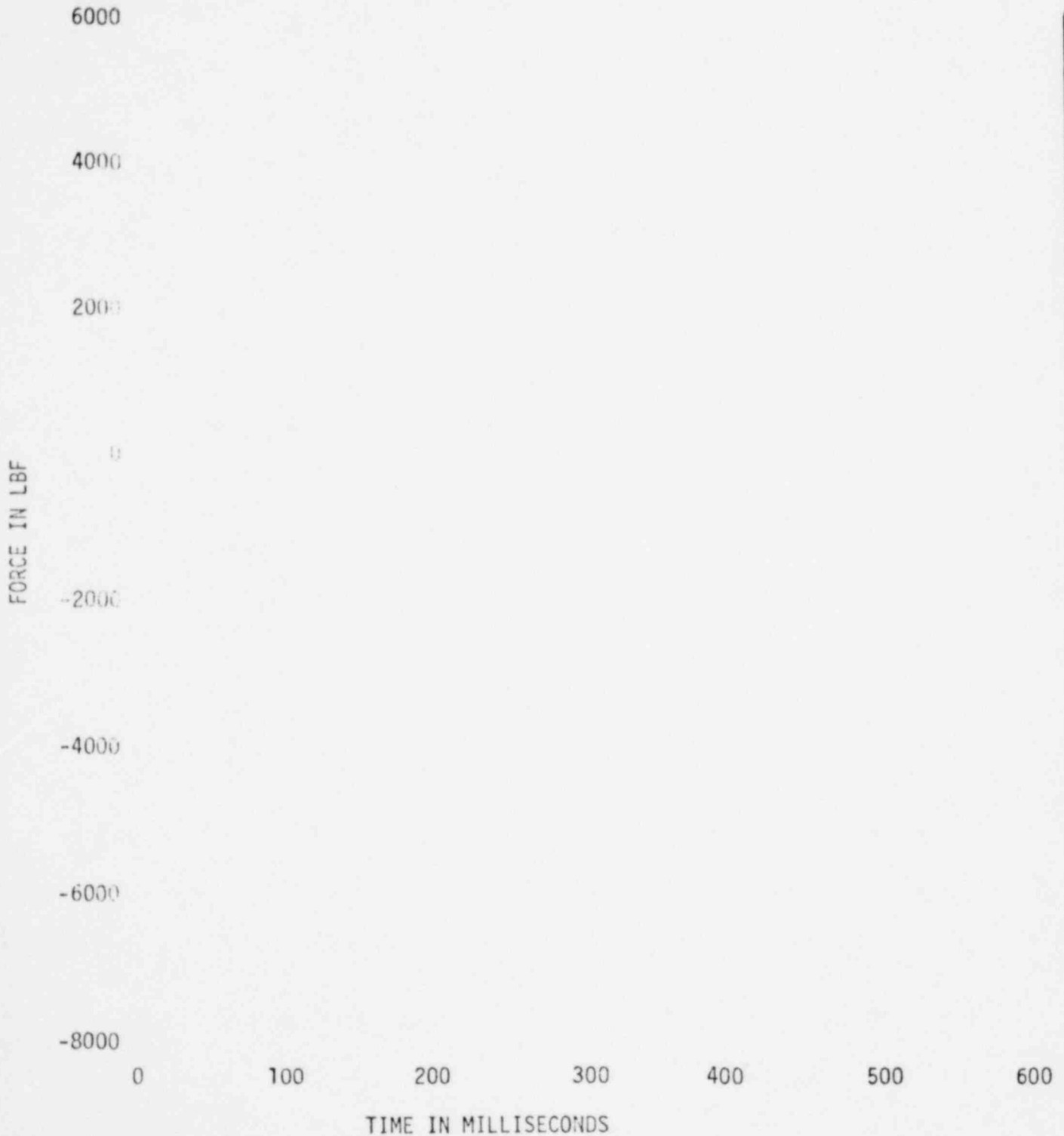
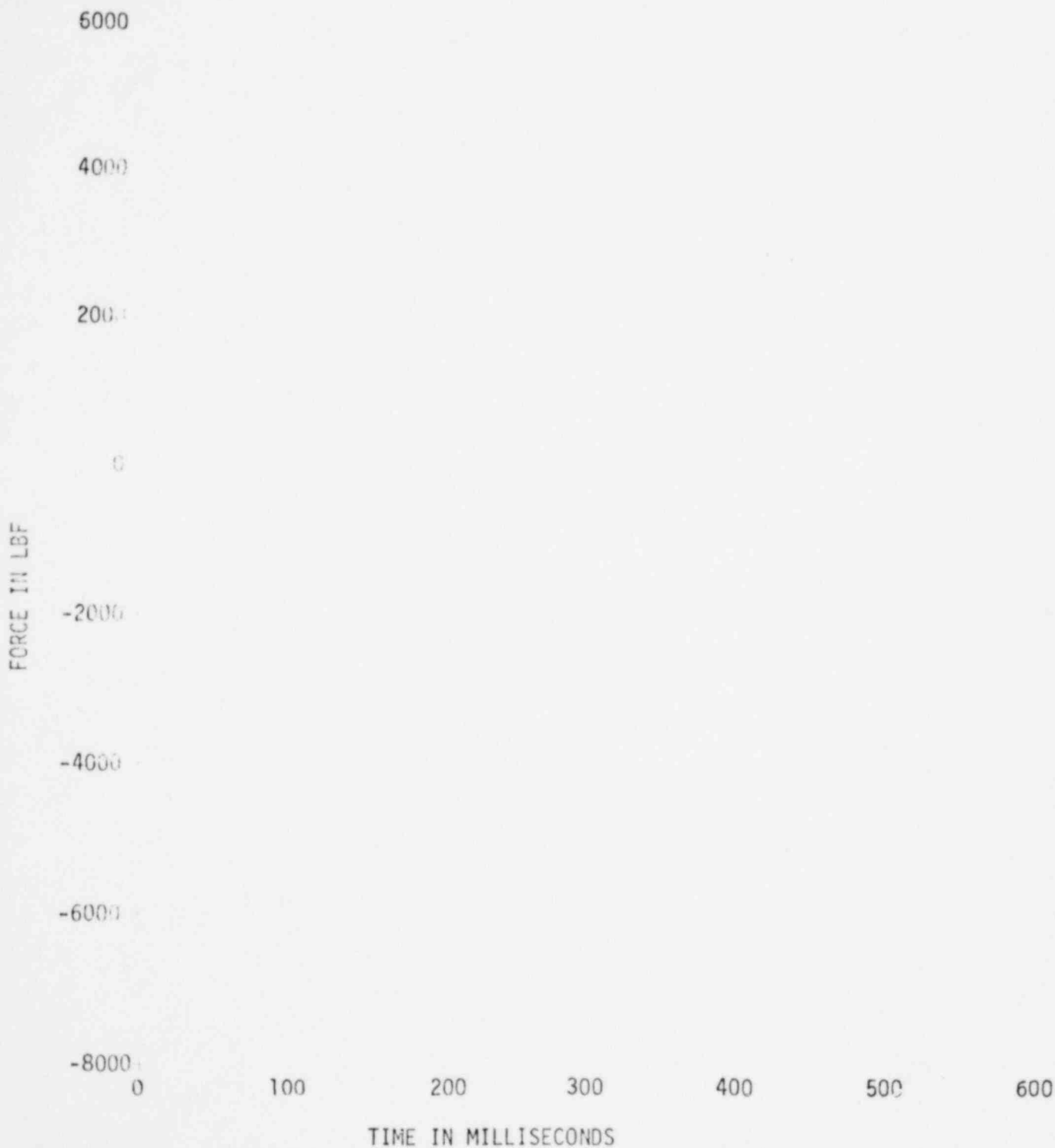


FIGURE A-125

NET TORUS FORCE FROM PRESSURE INTEGRAL, CORRECTED FOR WATER INERTIA

Task 5.5.3-2 Fermi 2 Test 7



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FIGURE A-126

AVERAGE POOL PRESSURE, CORRECTED FOR WATER INERTIA

Task 5.5.3-2 Fermi 2 Test 3



FIGURE A-127

NET AVERAGE POOL PRESSURE, CORRECTED FOR WATER INERTIA

Task 5.5.3-2 Fermi 2 Test 3

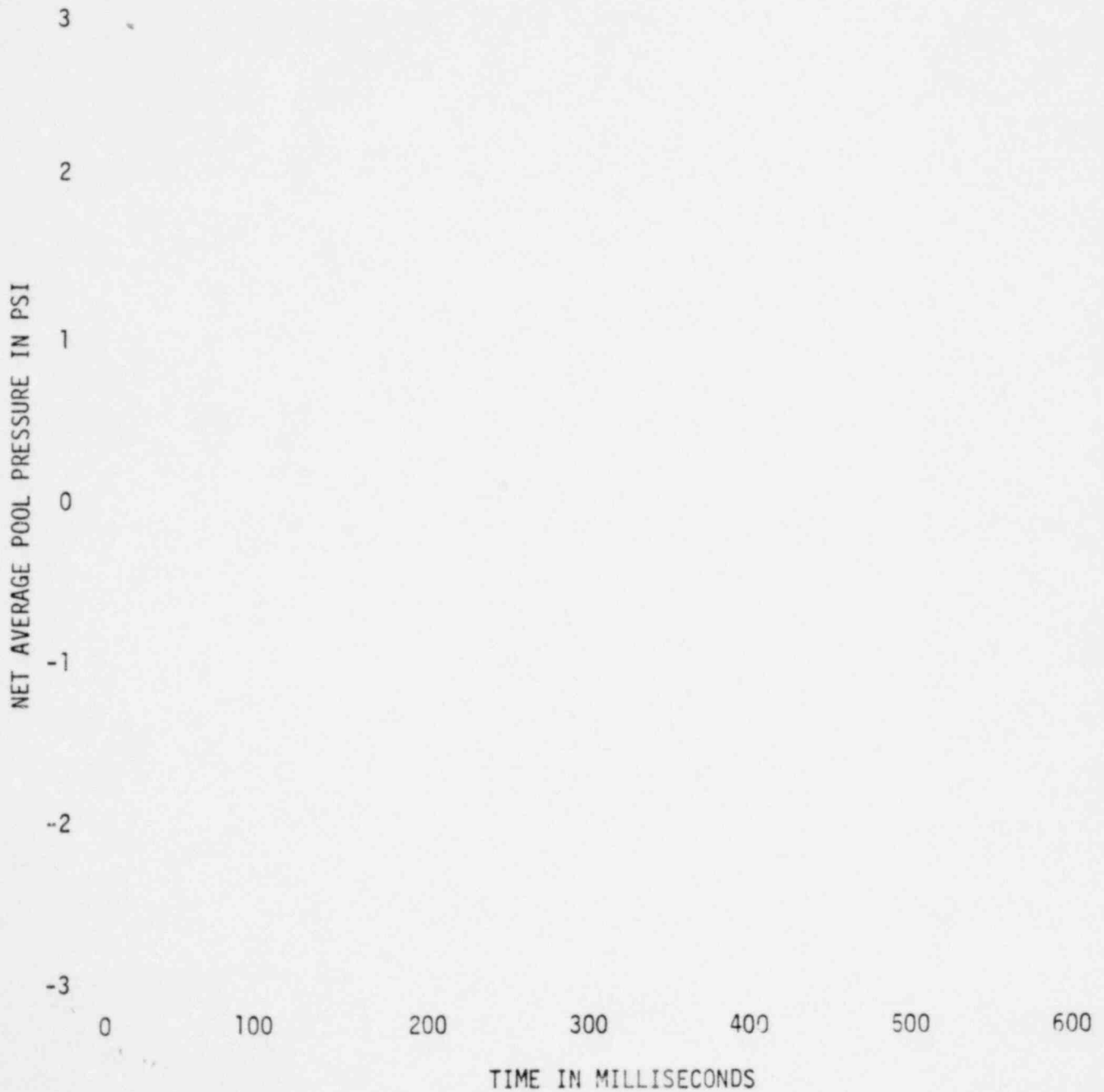


FIGURE A-128

AVERAGE POOL PRESSURE, CORRECTED FOR WATER INERTIA

Task 5.5.3-2 Fermi 2 Test 7

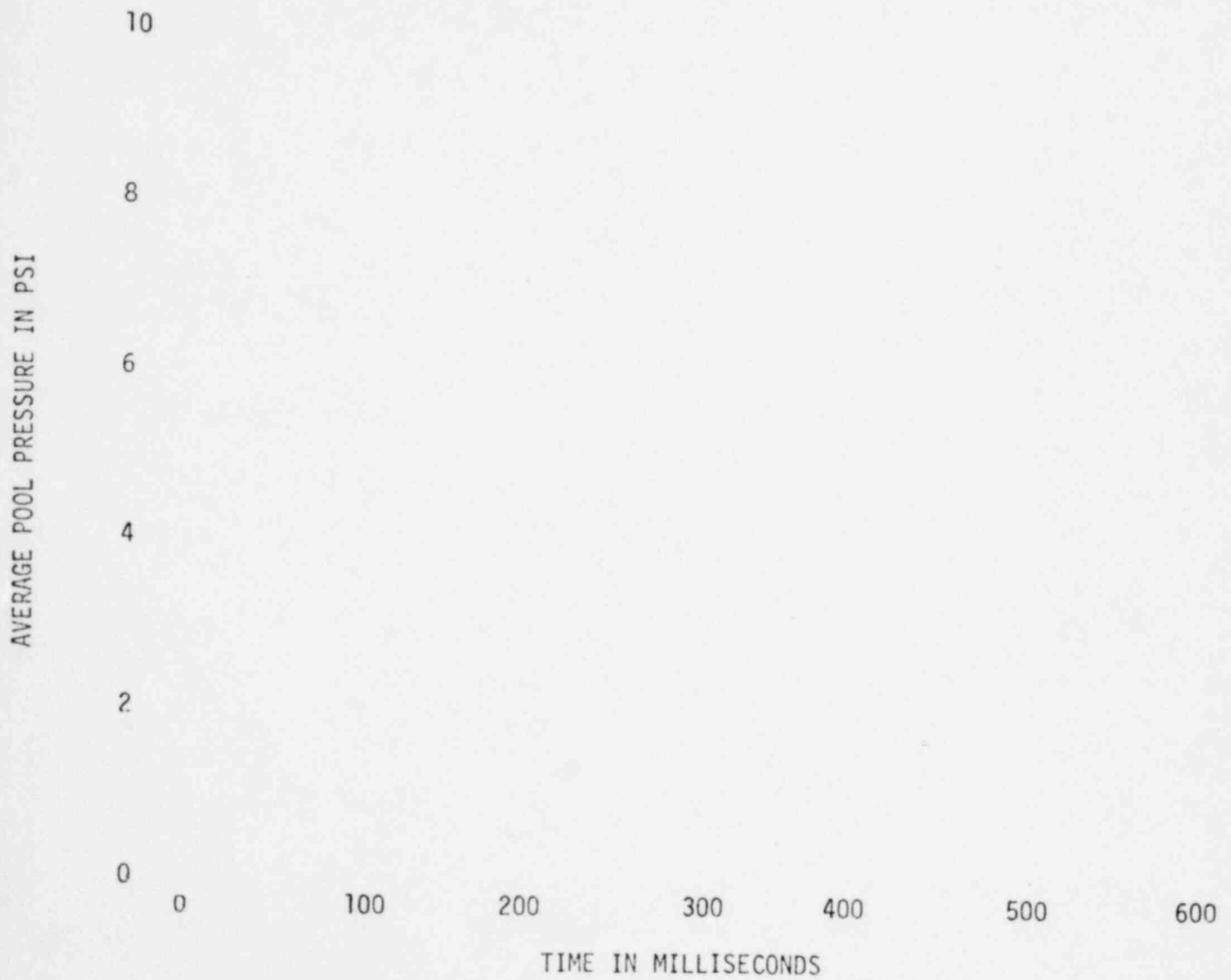
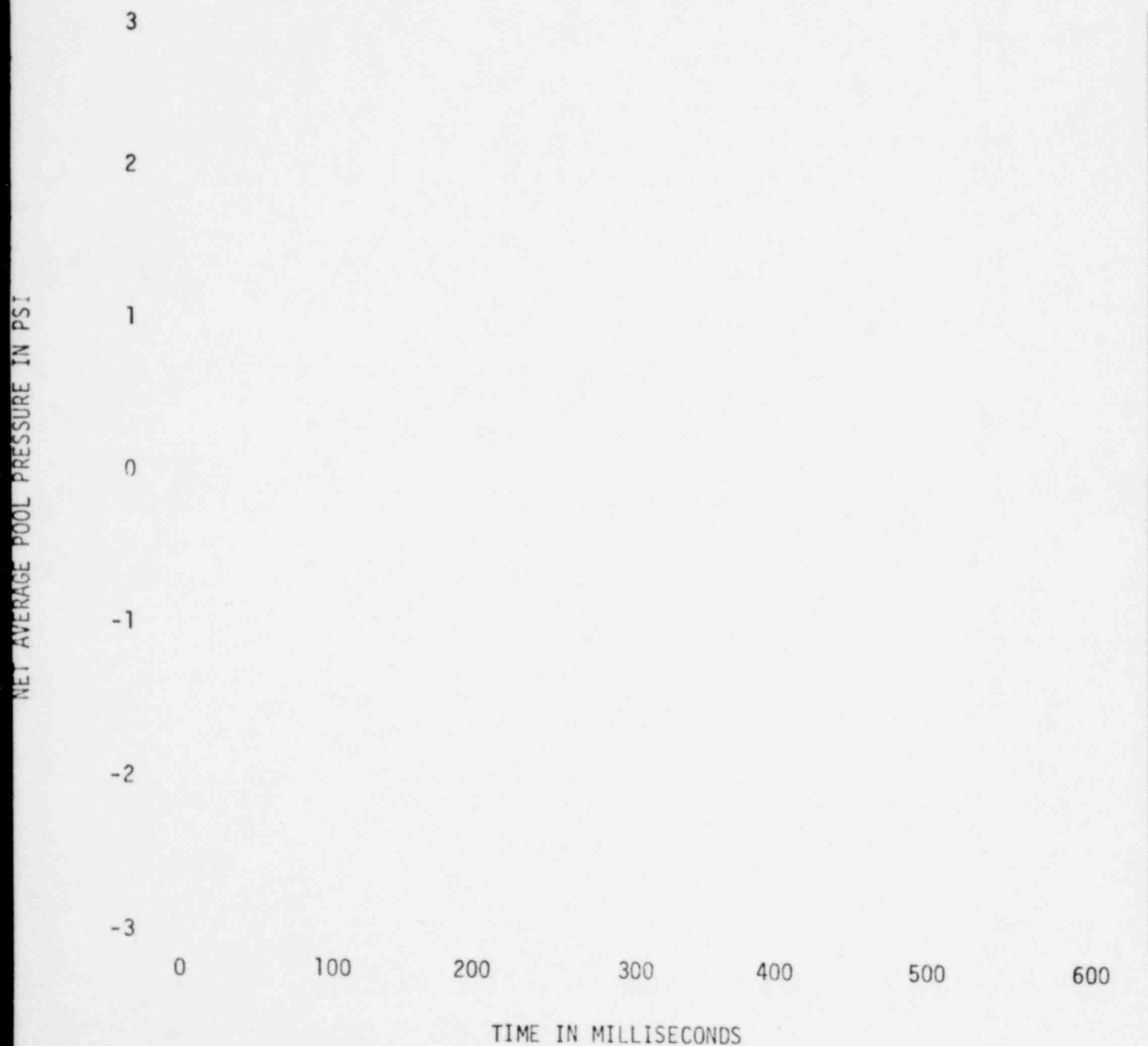


FIGURE A-129

NET AVERAGE POOL PRESSURE, CORRECTED FOR WATER INERTIA

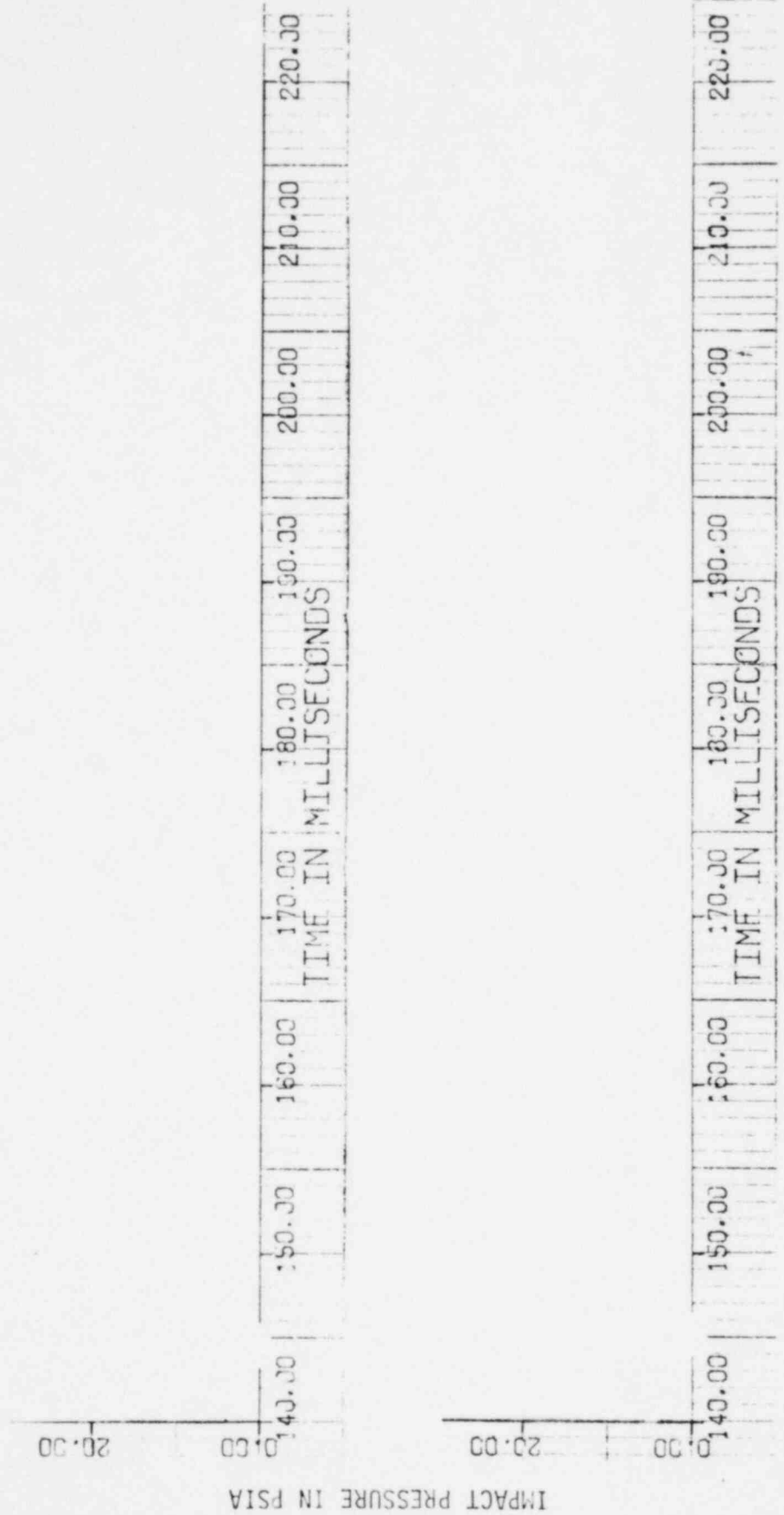
Task 5.5.3-2 Fermi 2 Test 7



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VENT HEADER IMPACT PRESSURES  
Task 5.5.3-2 Fermi 2 Test 3

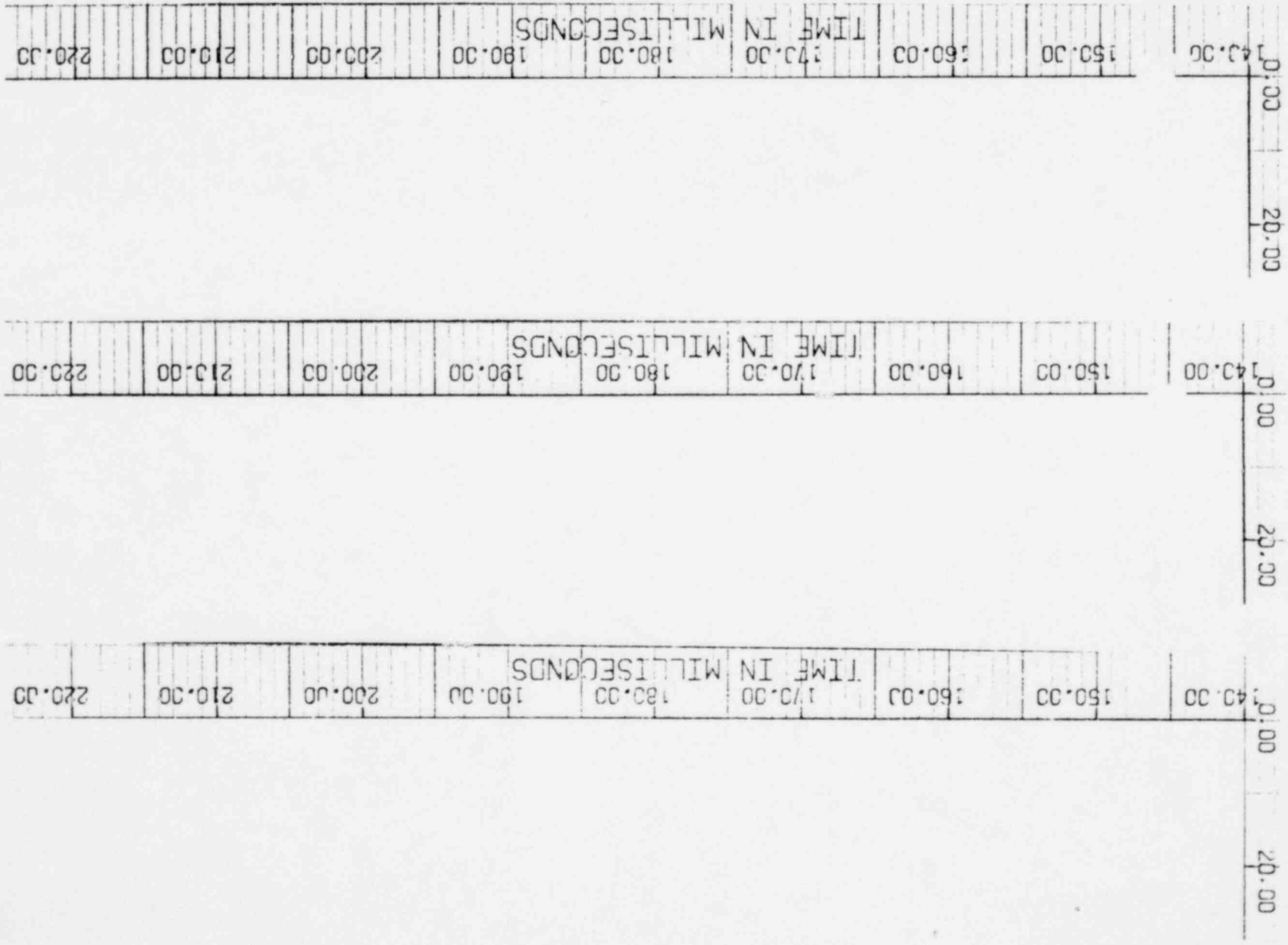
FIGURE A-130



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A-151

IMPACT PRESSURE IN PSIA

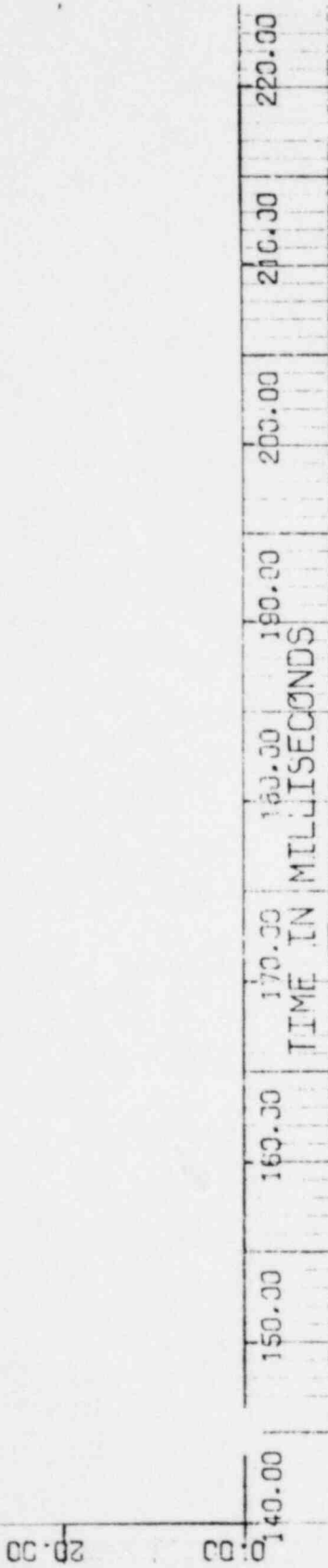


VENT HEADER IMPACT PRESSURES  
Task 5.5.3-2 Fermi 2 Test 3

FIGURE A-131

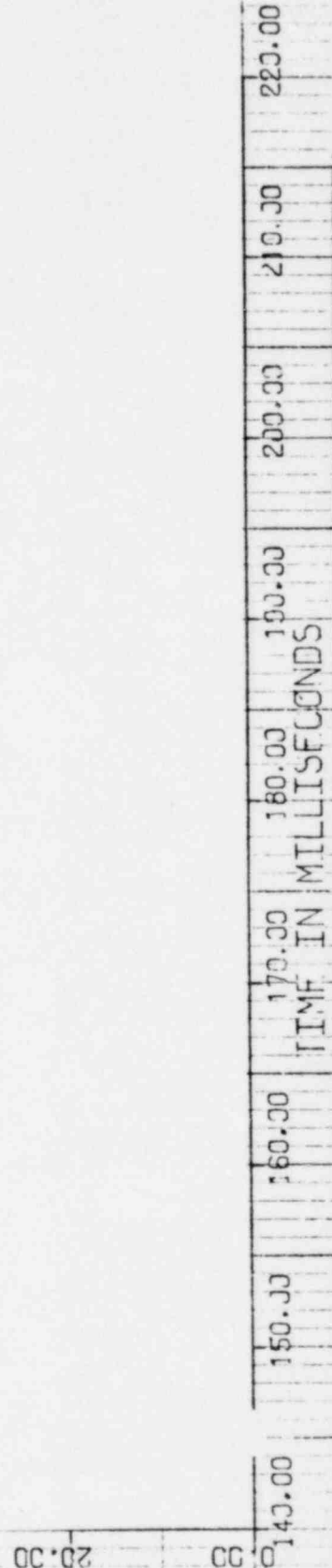
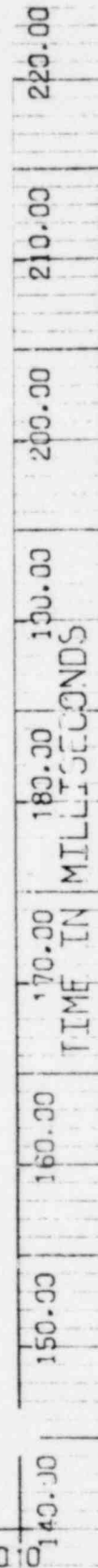
VENT HEADER IMPACT PRESSURES  
Task 5.5.3-2 Fermi 2 Test 3

FIGURE A-132



IMPACT PRESSURE IN PSIA

A-152



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FIGURE A-133

VENT HEADER IMPACT PRESSURES

Task 5.5.3-2 Fermi 2 Test 3

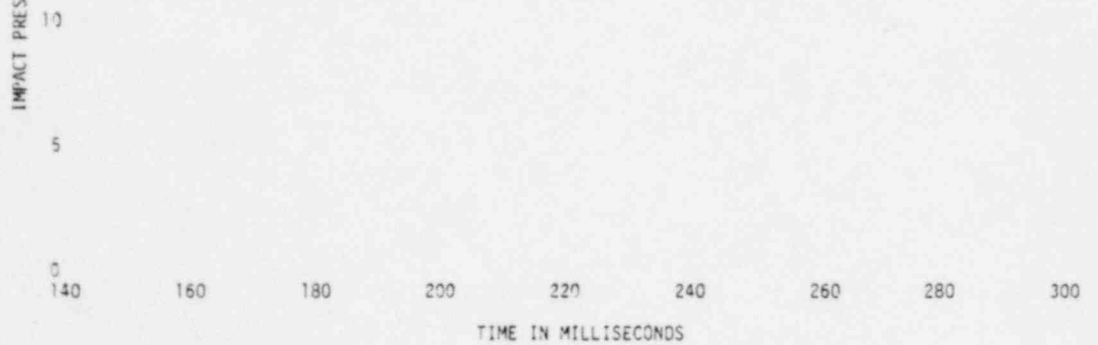
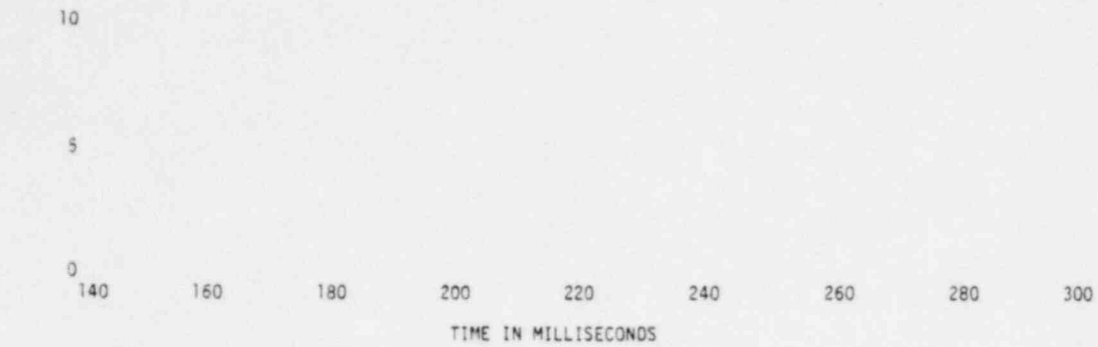
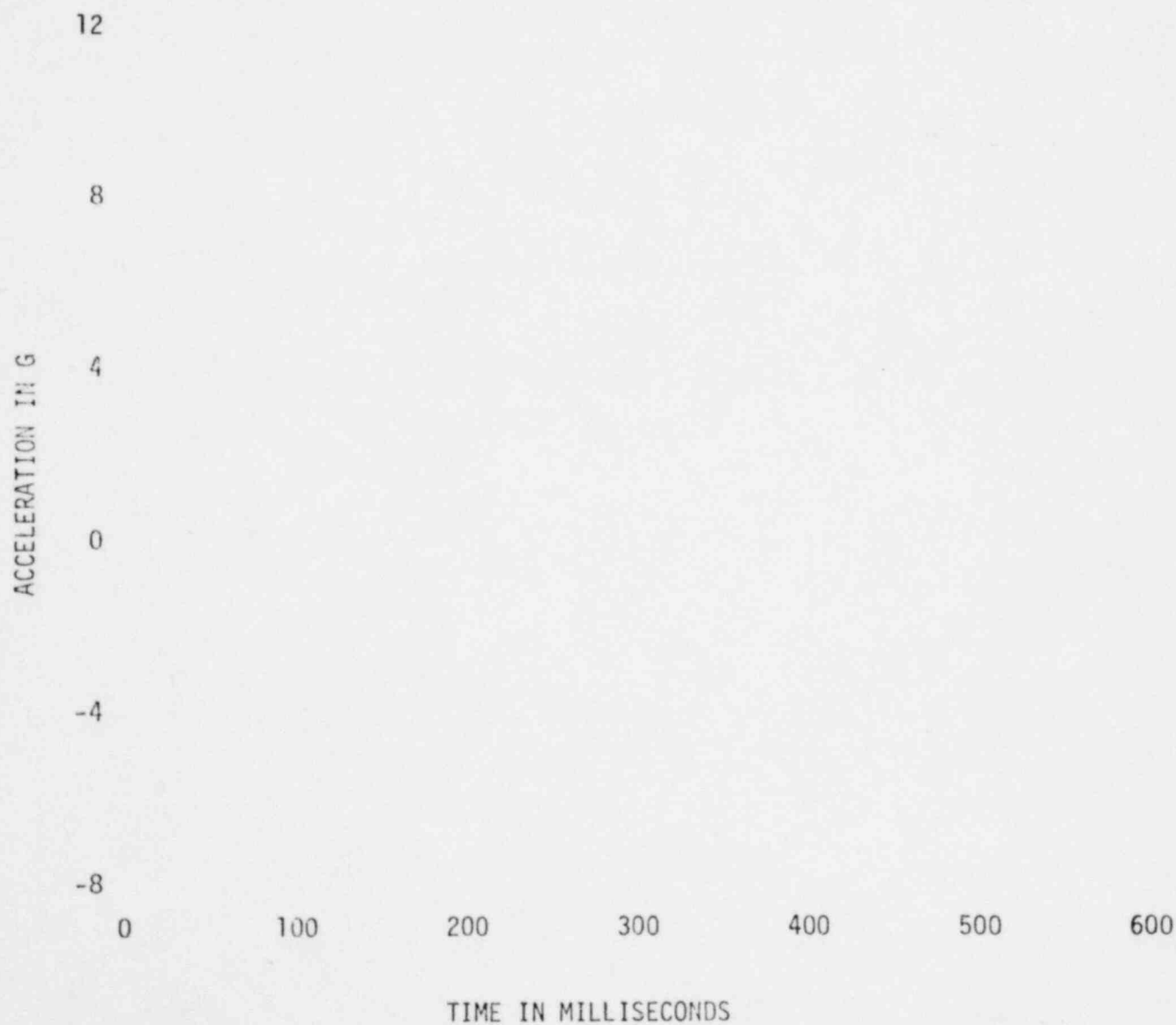


FIGURE A-134

VENT HEADER VERTICAL ACCELERATION

Task 5.5.3-2 Fermi 2 Test 3



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FIGURE A-135

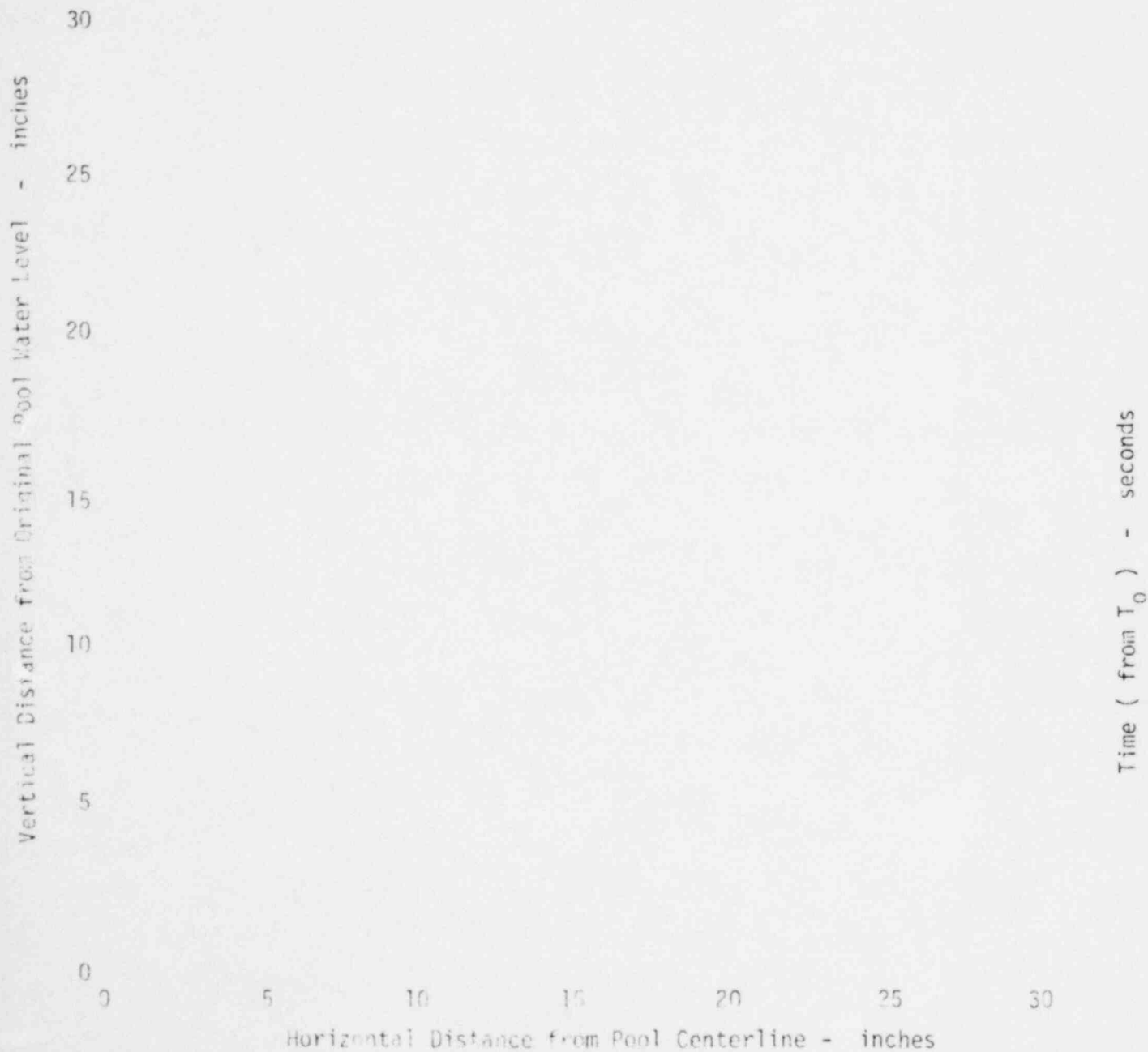
VENT HEADER VERTICAL ACCELERATION

Task 5.5.3-2 Fermi 2 Test 7



TIME HISTORY OF  
POOL DISPLACEMENT

FERMI 2, TEST 1

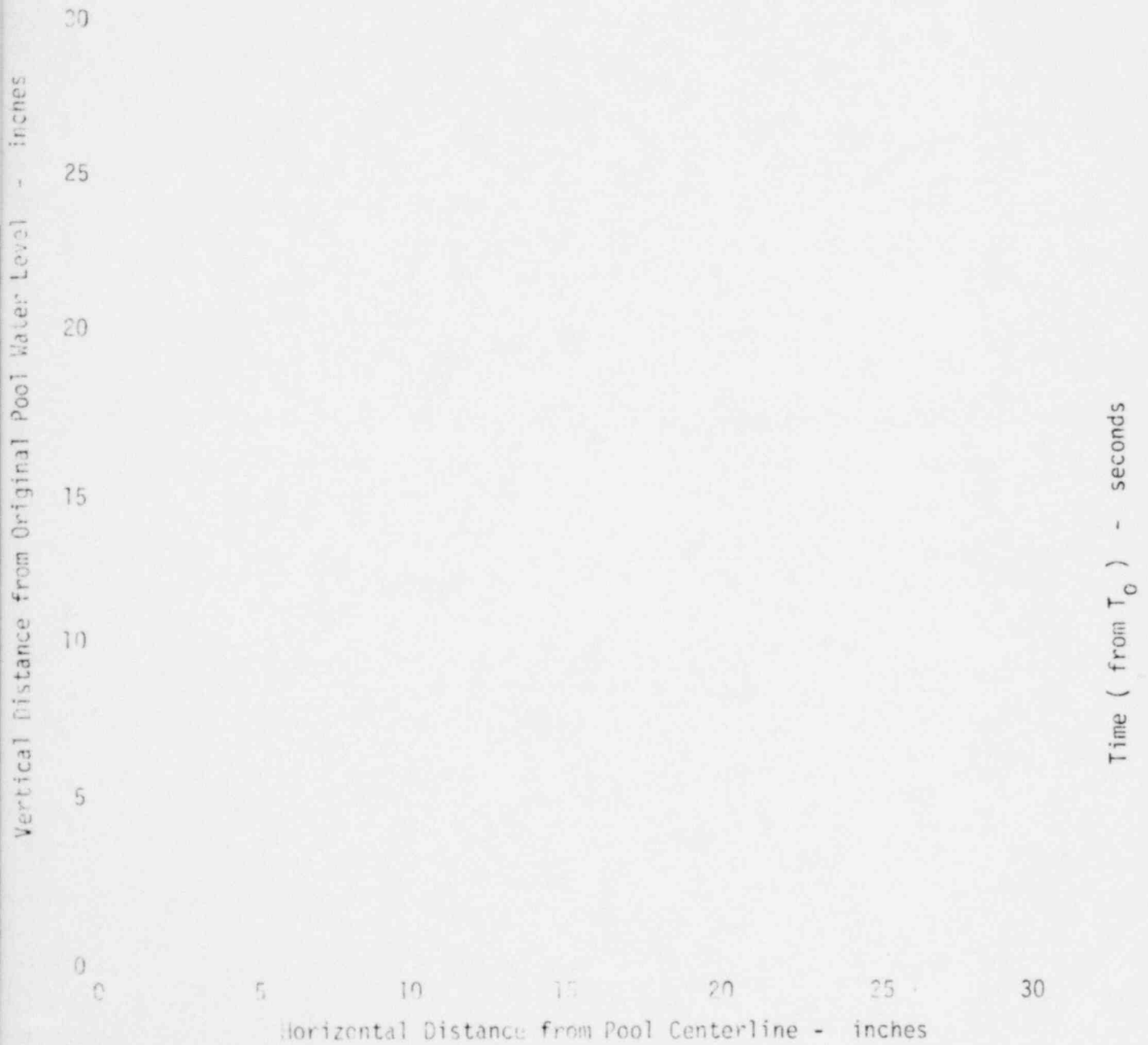


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FIGURE A-137

TIME HISTORY OF  
POOL DISPLACEMENT

FERMI 2, TEST 2

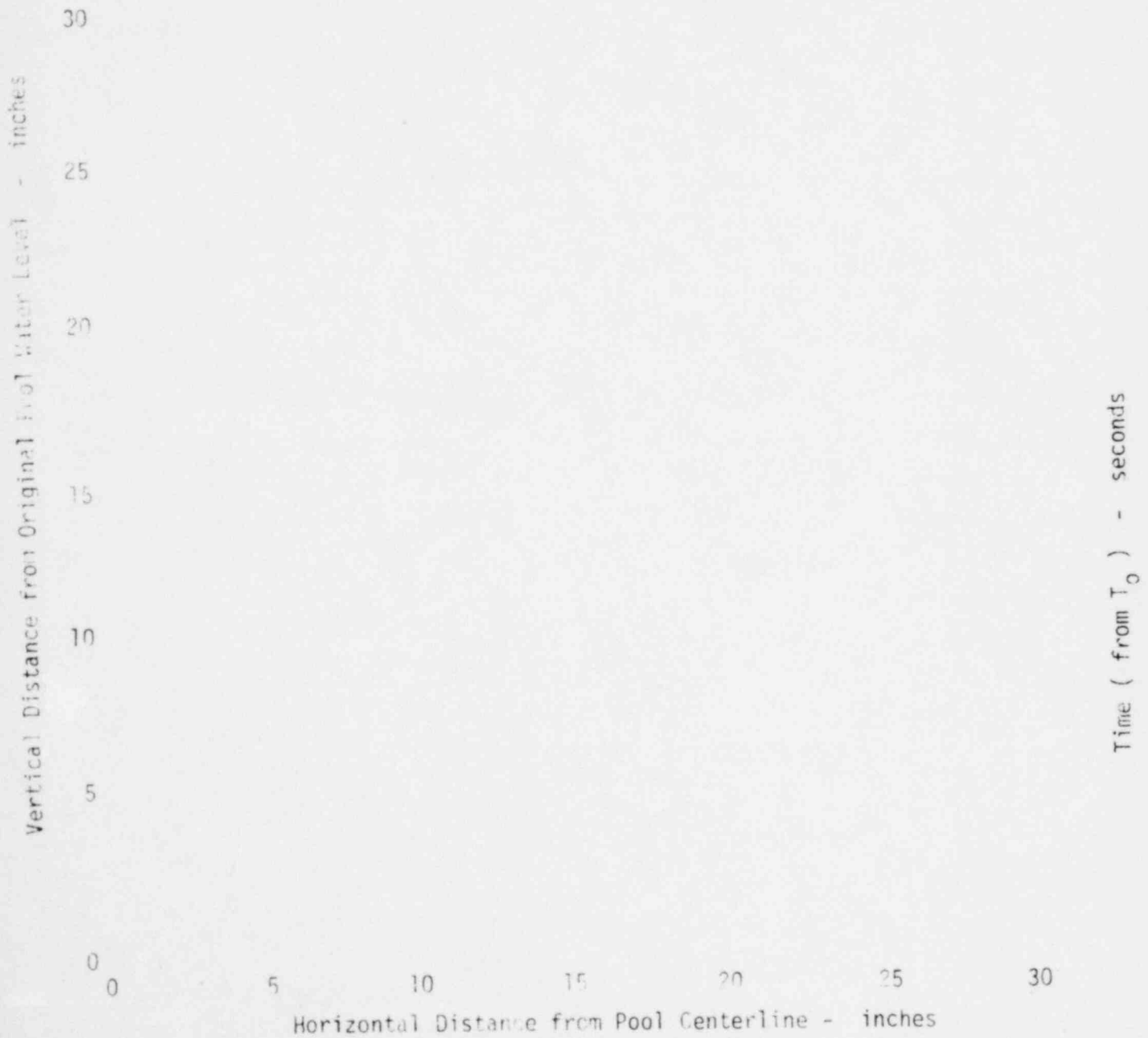


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FIGURE A-138

TIME HISTORY OF  
POOL DISPLACEMENT

FERMI 2, TEST 3



NEDO-21944  
FIGURE A-139

TIME HISTORY OF  
POOL DISPLACEMENT

FERMI 2, TEST 5

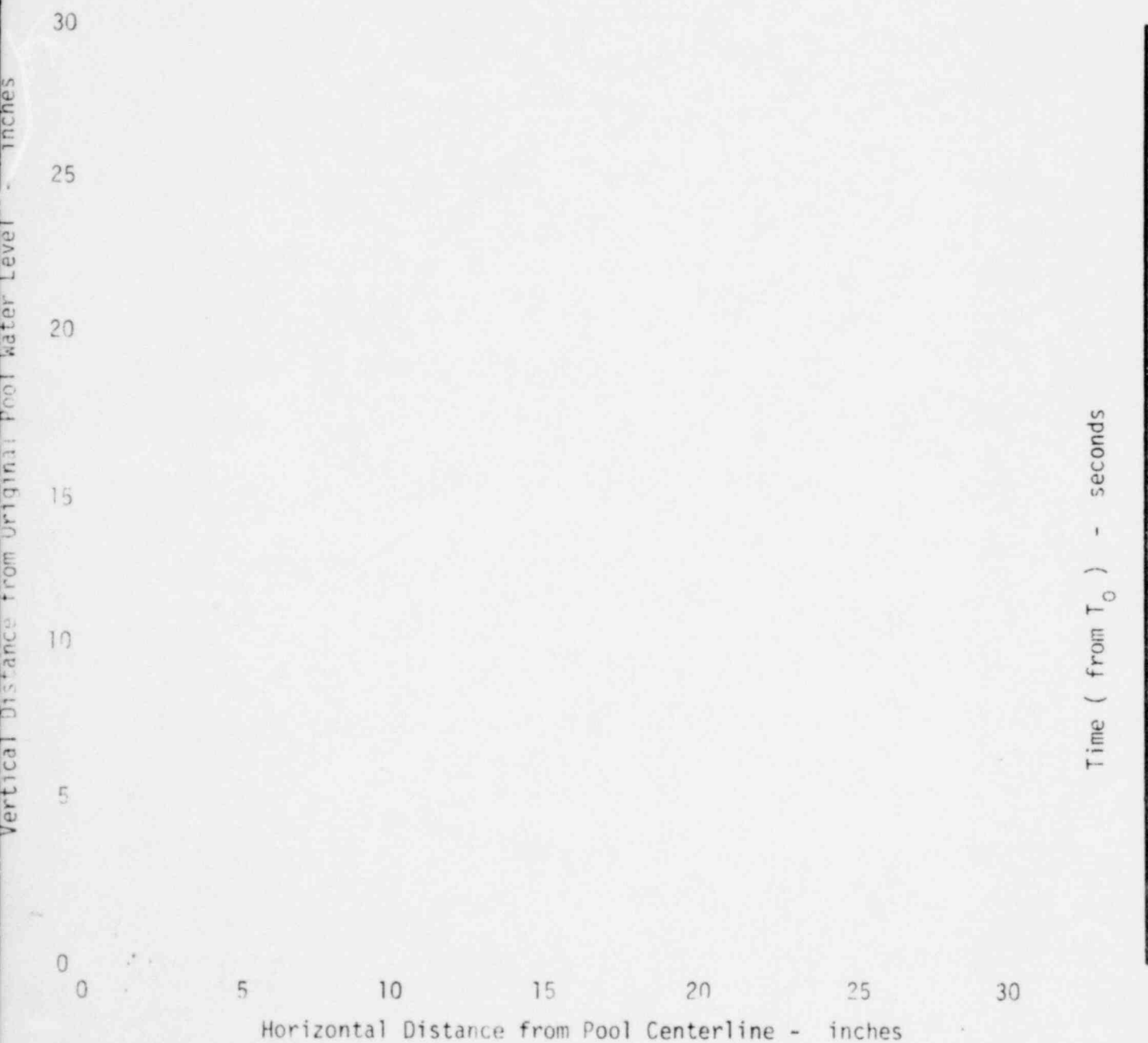


FIGURE A-140

POOL SURFACE DISPLACEMENT

FERMI, TESTS 1, 2, 3



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NUCLEAR SERVICES CORPORATION

FERMI, TESTS 1, 2, 3

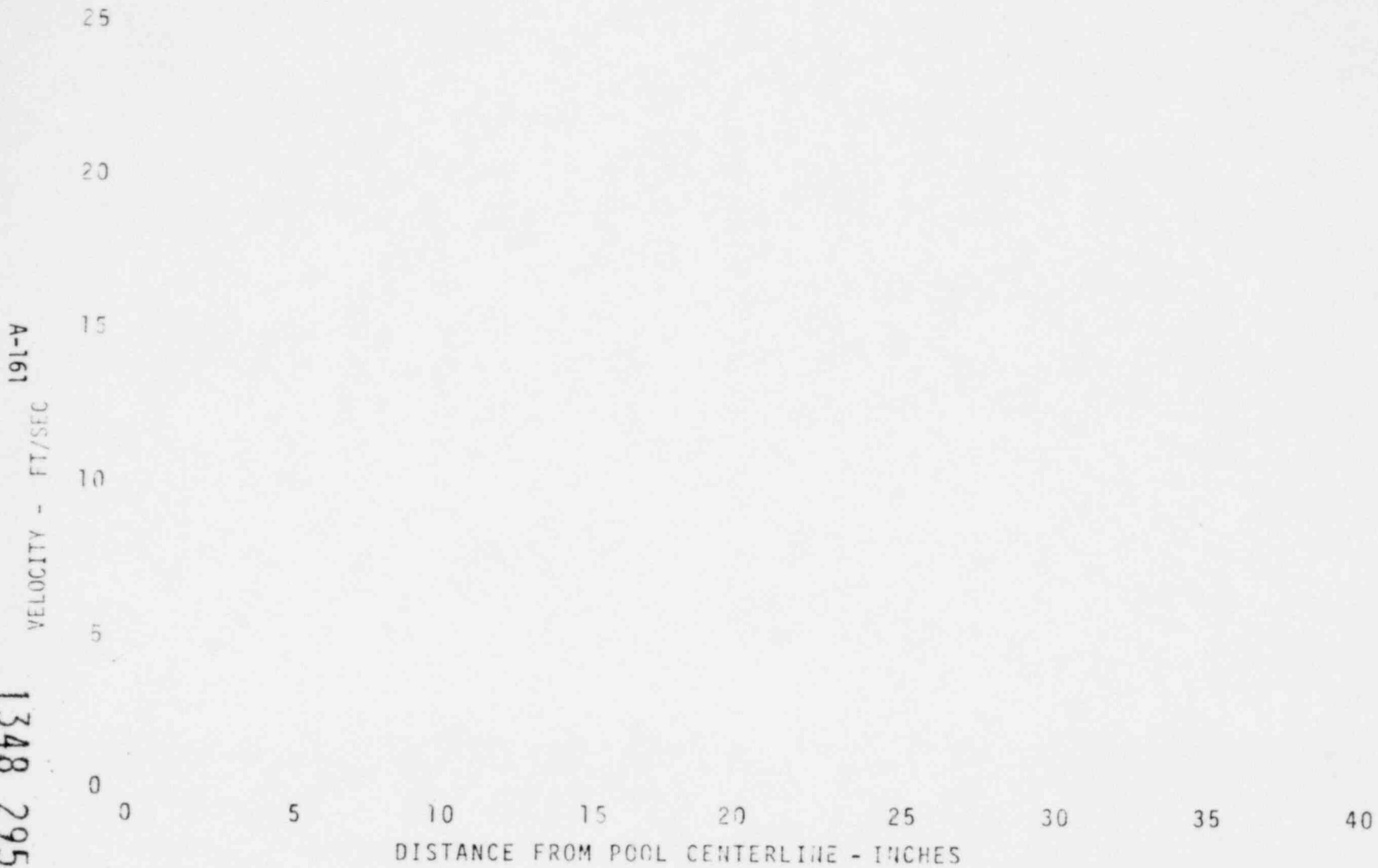
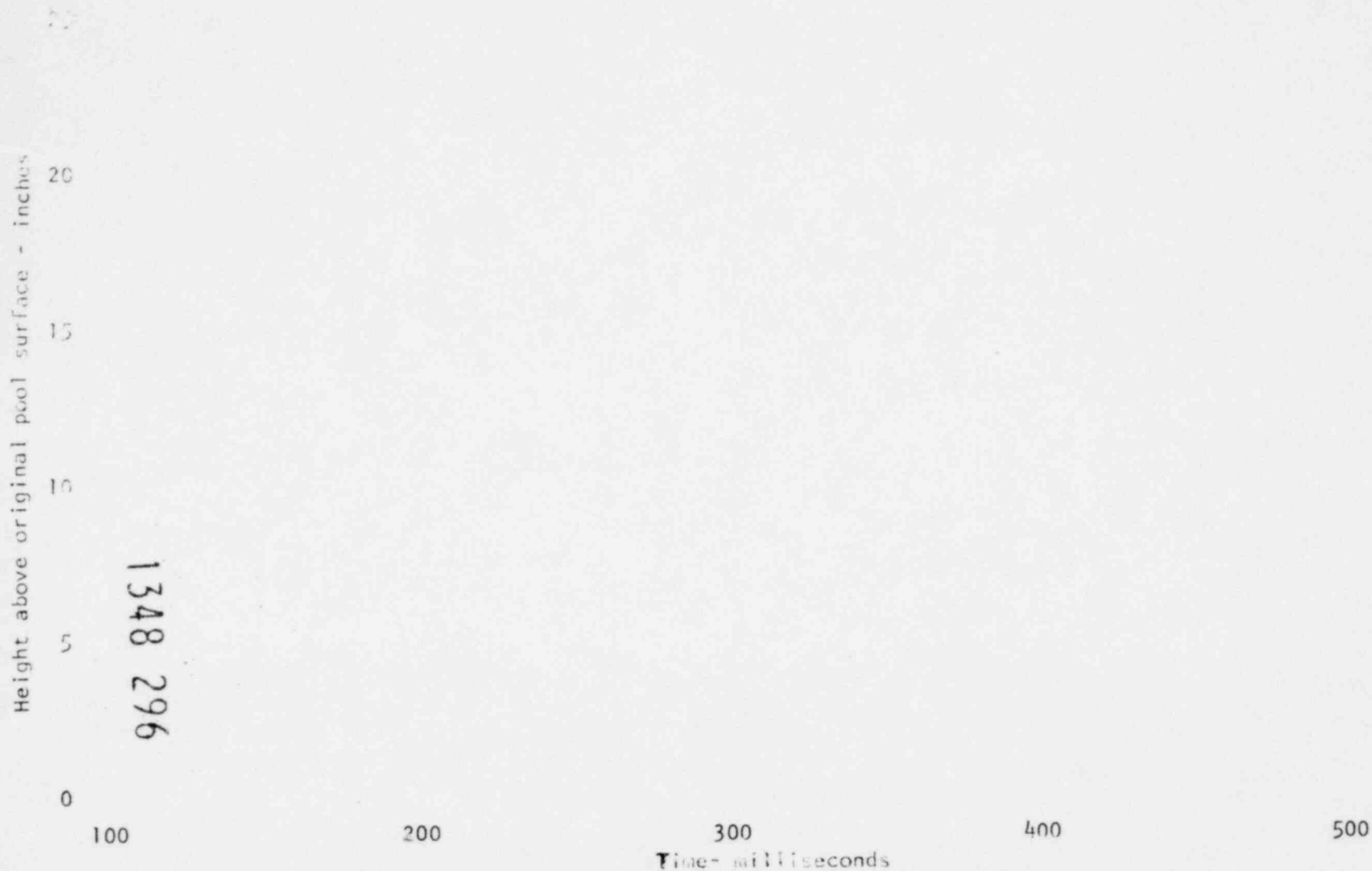


FIGURE A-142

POOL SURFACE DISPLACEMENT

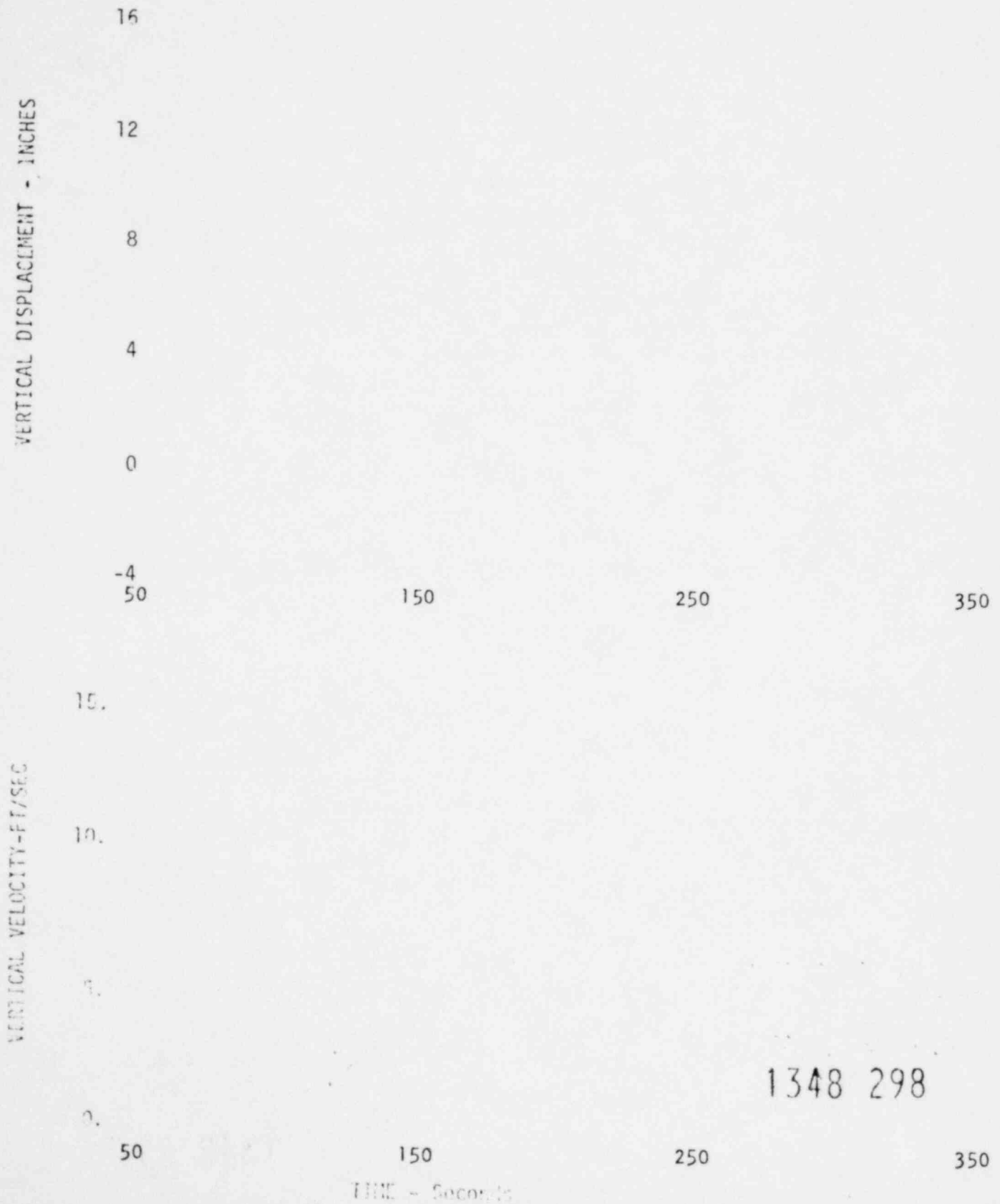
FERMI, TEST 5



FERMI, TEST 5



FERMI, TEST 4

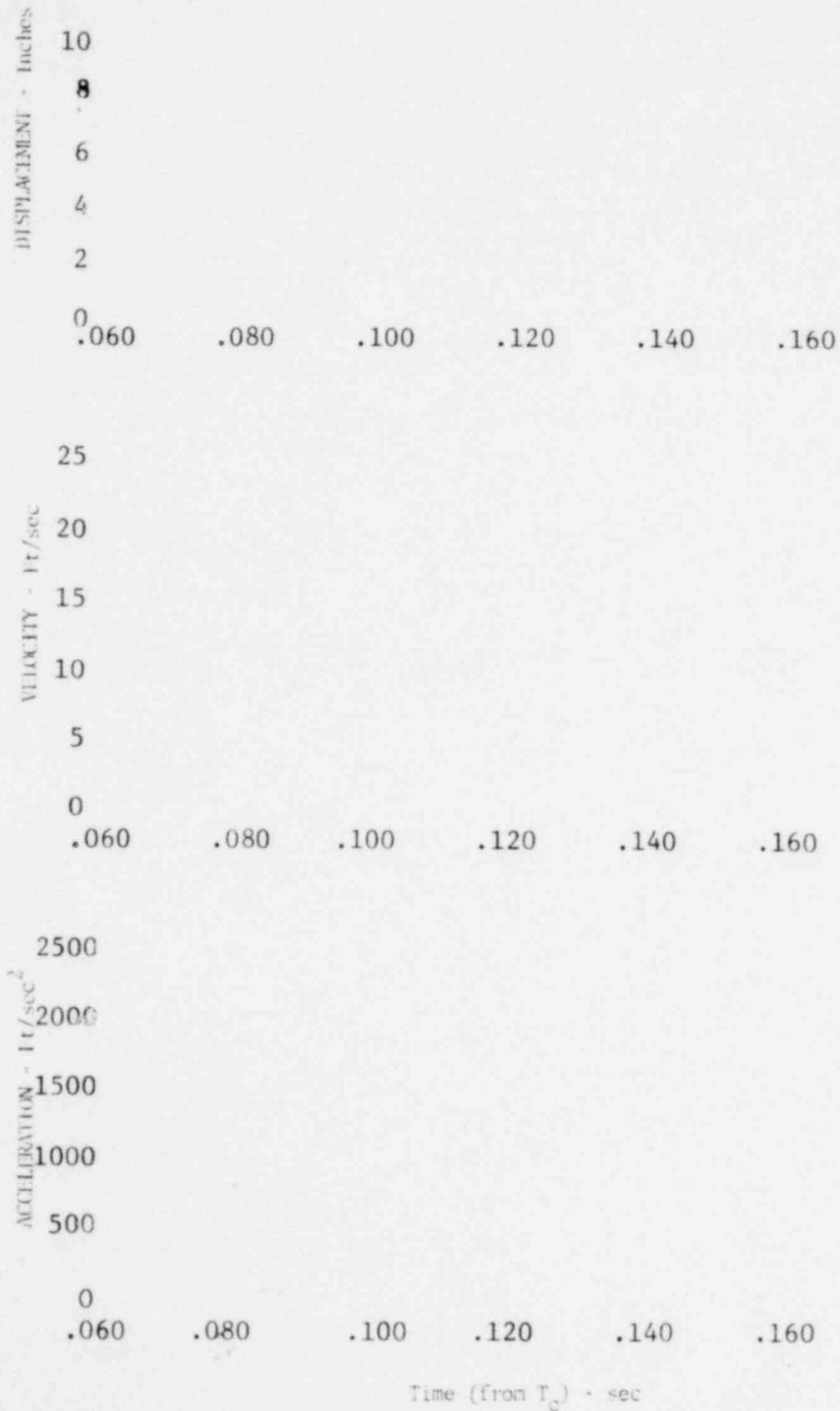


NEDO-21944

FIGURE A-145

DOWNCOMER WATER SLUG EJECTION

FERMI, TEST 3

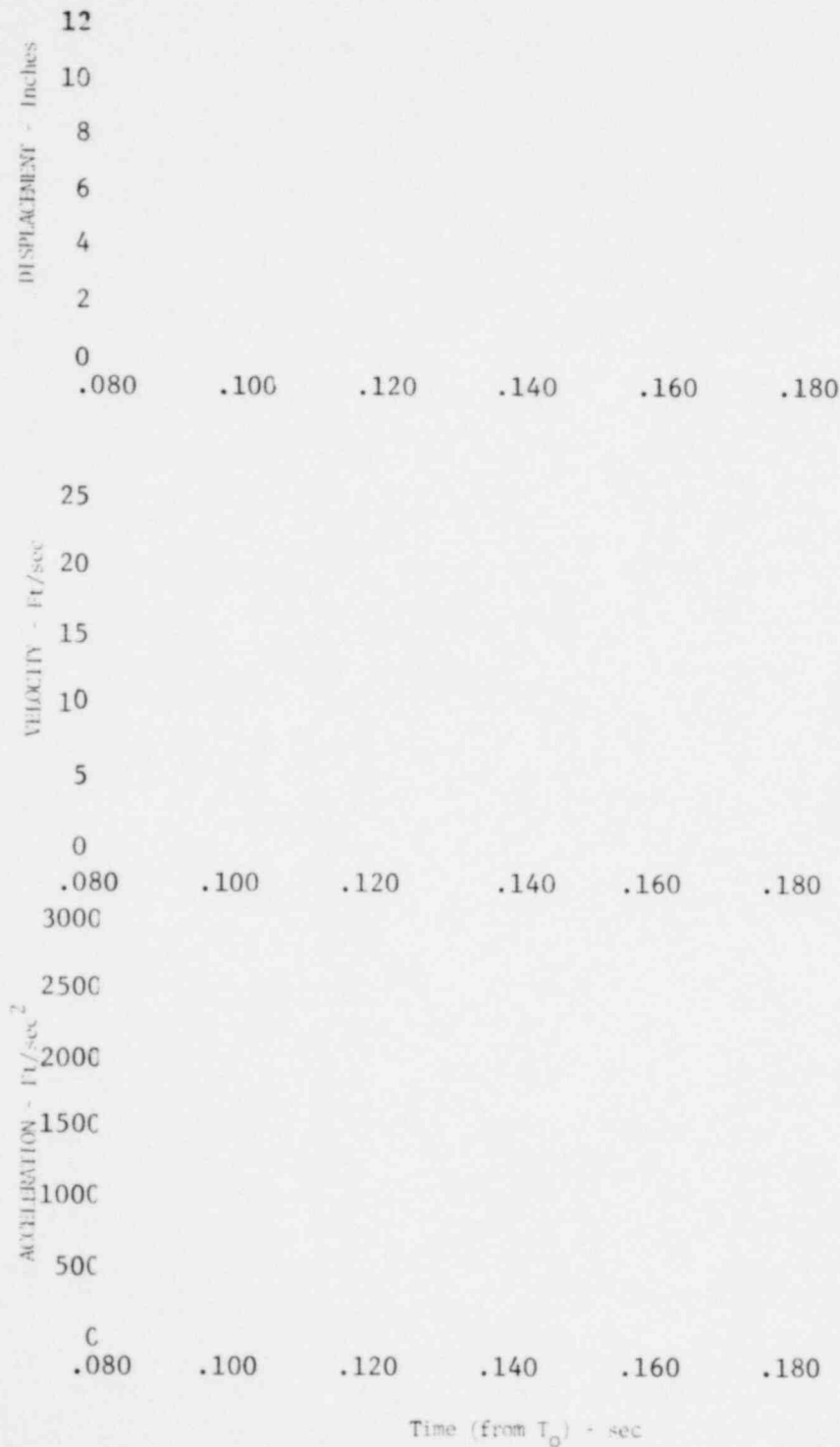


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NEDO-21944  
FIGURE A-146

DOWNCOMER WATER SLUG EJECTION

FERMI, TEST 7



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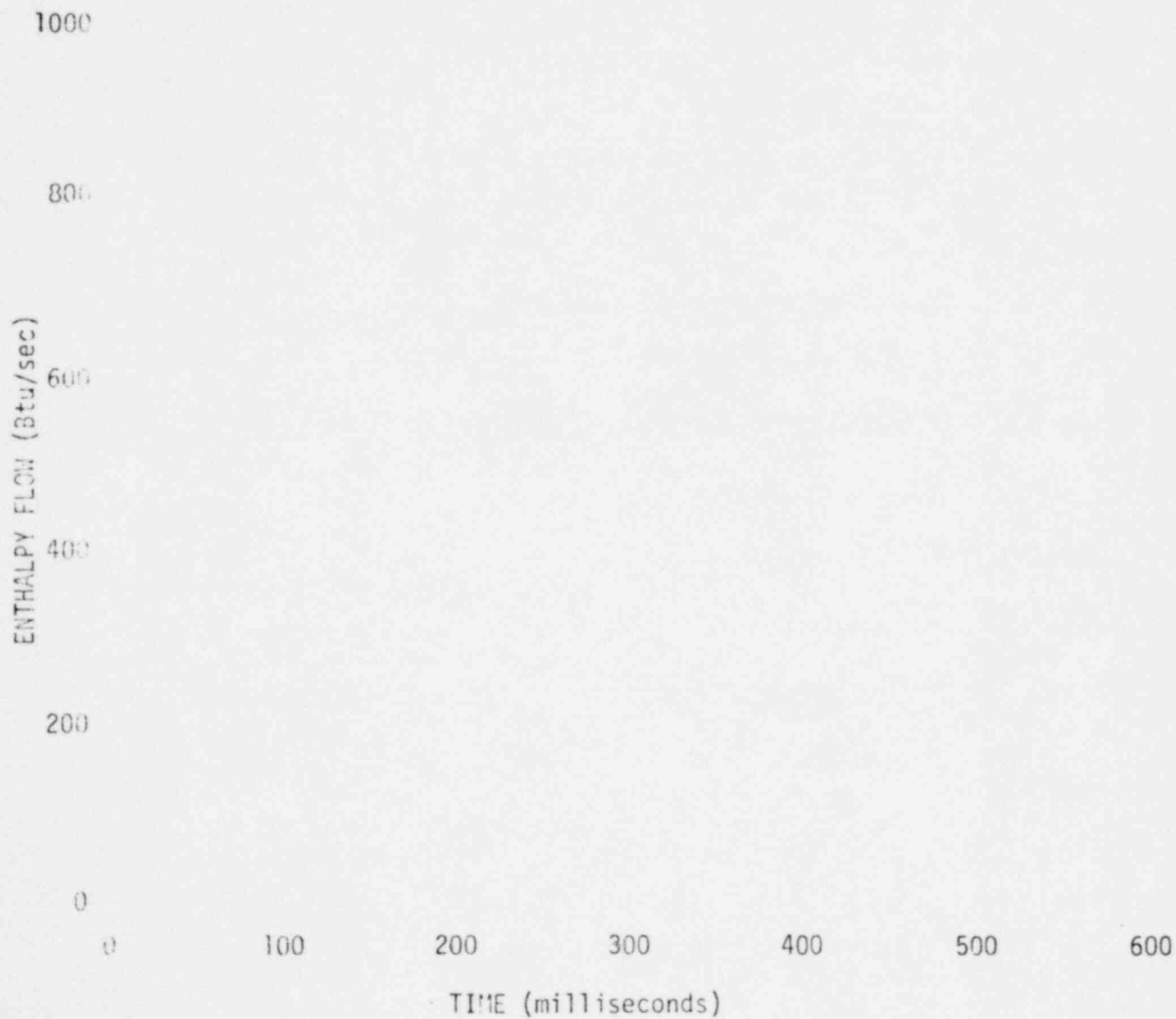
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FIGURE A-147

EFFECT OF DRYWELL/WETWELL  $\Delta P$  ON

ENTHALPY FLOW INTO POOL

Fermi 2 Tests



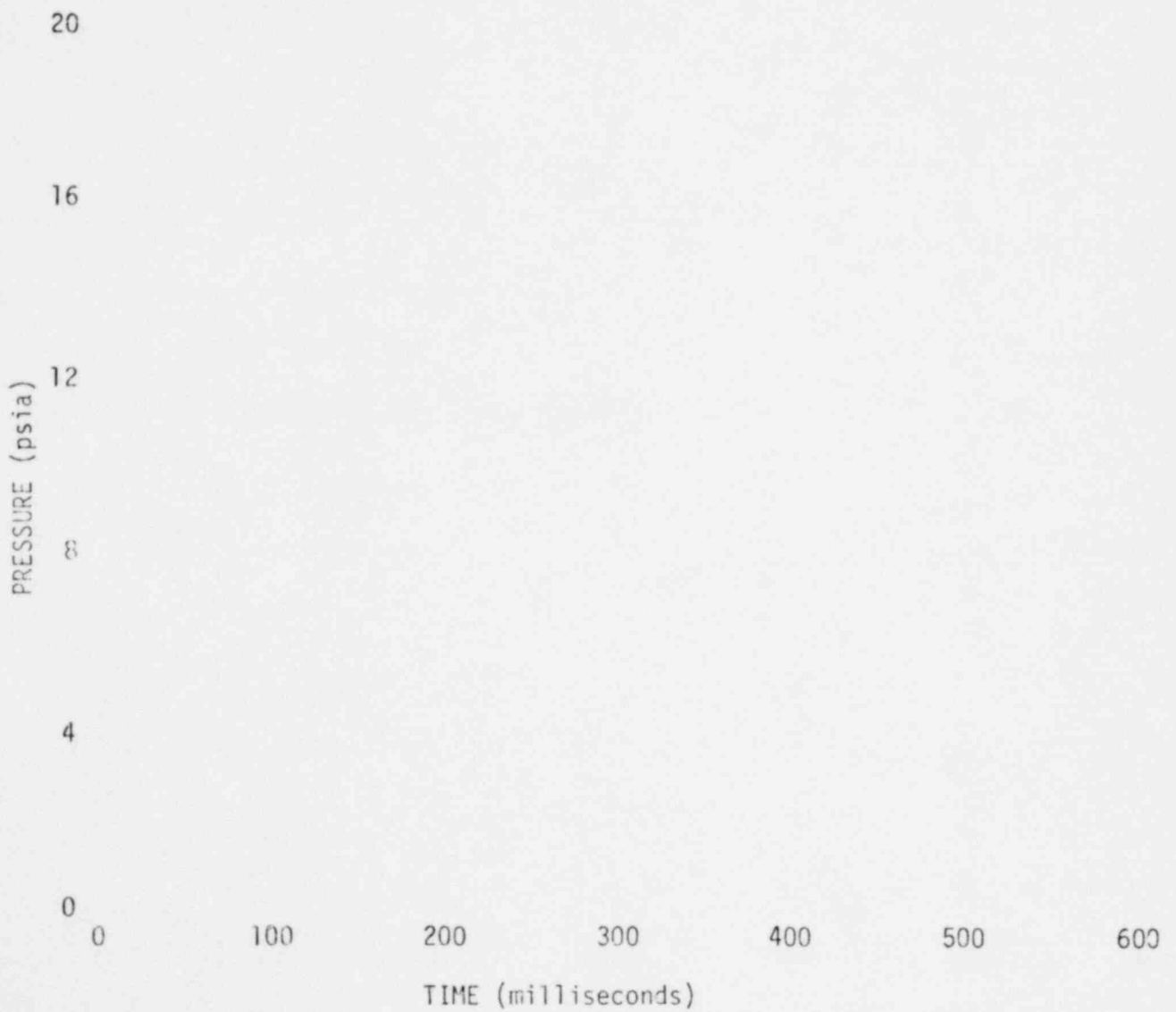
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FIGURE A-148

EFFECT OF DRYWELL/WETWELL  $\Delta P$  ON

DOWNCOMER INTERNAL PRESSURE

Fermi 2 Tests



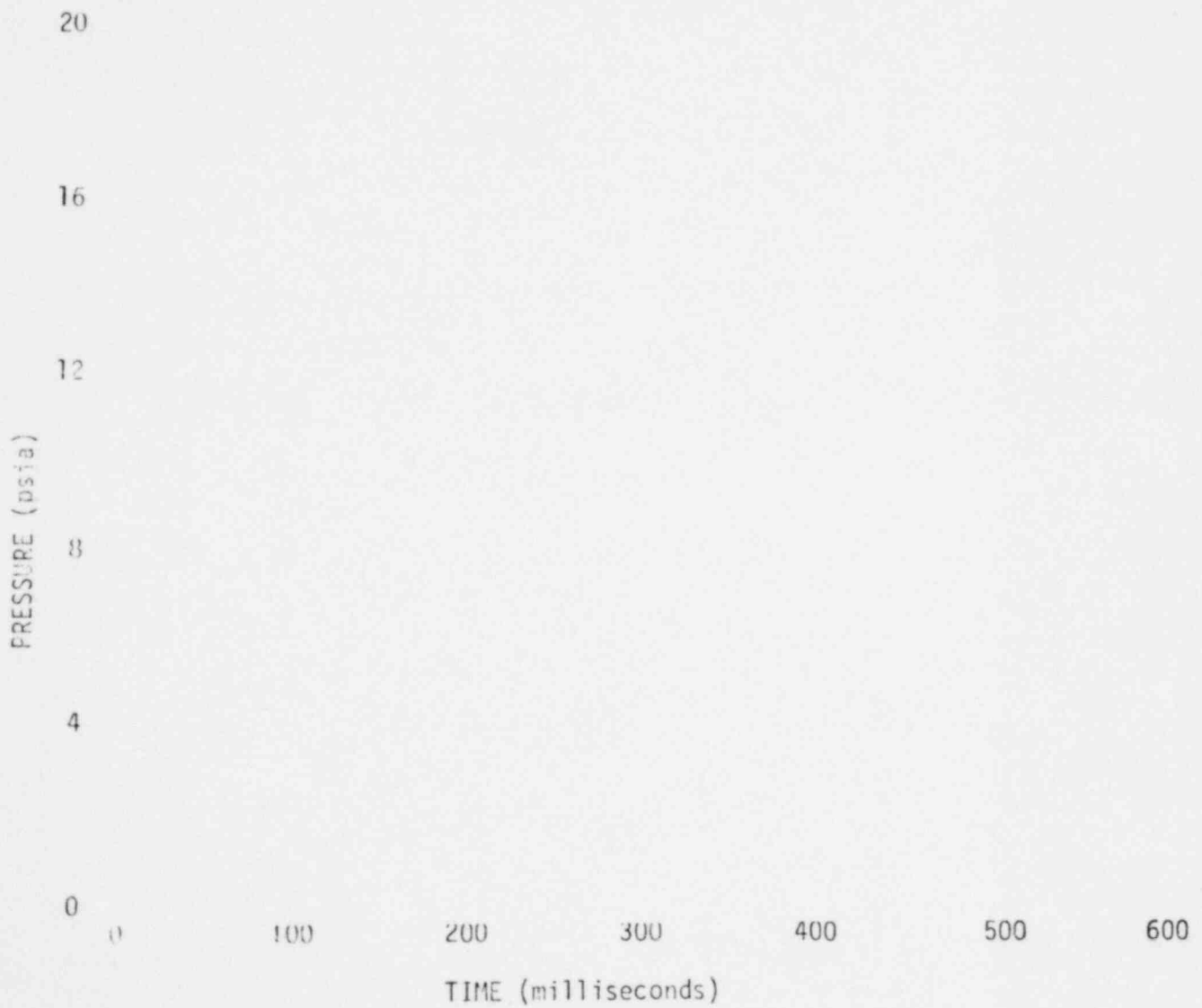
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FIGURE A-149

EFFECT OF DRYWELL/WETWELL  $\Delta P$  ON POOL PRESSURE

AT 180 DEGREE AND FREESPACE PRESSURE

Fermi 2 Tests



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TABLE A-6  
DATA FOR WETWELL VERTICAL LOADS

Task 5.5.3-2 Fermi 2 Tests

\*Vent clearing time (from  $T_0$ ) determined from the movie films.

\*\*Time difference from  $T_0$  to time of zero downforce.

—No significant downforce valley or 2nd peak downforce.

\*(1) Start-of-test reference time

Parameter	Test No.	7.03" $\Delta P$ , 6.56-inch "T" Deflector				Mean	Std. Dev.
		(1)	(2)	(3)	(4)		
$T_0$ *(1)	(sec)						
Vent Clearing Time*	(sec)						
<u>Peak Downforce</u>							
Pressure Integral:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
Corrected Pressure Integral:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
Corrected Load Cell:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
<u>Downforce Valley</u>							
Pressure Integral:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
Corrected Pressure Integral:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
Corrected Load Cell:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
<u>2nd Peak Downforce</u>							
Pressure Integral:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
Corrected Pressure Integral:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
Corrected Load Cell:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
<u>[<math>\Delta t</math>] Downforce Time**</u>							
Pressure Integral	(sec)						
Corrected Pressure Integral	(sec)						
Corrected Load Cell	(sec)						
<u>Downforce Impulse</u>							
Pressure Integral:							
Impulse	(lb-sec)						

TABLE A-6 (Continued)  
 DATA FOR WETWELL VERTICAL LOADS (continued)  
 Task 5.5.3-2 Fermi 2 Tests

Parameter	Test No.	7.03" $\Delta P$ , 6.56-inch "T" Deflector				Mean	Std. Dev.
		(1)	(2)	(3)	(4)		
<u>Peak Upforce</u>							
Pressure Integral:							
Force	(1b)						
Time (from $T_0$ )	(sec)						
Corrected Pressure Integral:							
Force	(1b)						
Time (from $T_0$ )	(sec)						
Corrected Load Cell:							
Force	(1b)						
Time (from $T_0$ )	(sec)						
<u>Upforce Valley</u>							
Pressure Integral:							
Force	(1b)						
Time (from $T_0$ )	(sec)						
Corrected Pressure Integral:							
Force	(1b)						
Time (from $T_0$ )	(sec)						
Corrected Load Cell:							
Force	(1b)						
Time (from $T_0$ )	(sec)						
<u>2nd Peak Upforce</u>							
Pressure Integral:							
Force	(1b)						
Time (from $T_0$ )	(sec)						
Corrected Pressure Integral:							
Force	(1b)						
Time (from $T_0$ )	(sec)						
Corrected Load Cell:							
Force	(1b)						
Time (from $T_0$ )	(sec)						
<u>Zero Force Time*</u>							
Pressure Integral	(sec)						
Corrected Pressure Integral	(sec)						
Corrected Load Cell	(sec)						

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TABLE A-7  
DATA FOR WETWELL VERTICAL LOADS

Task 5.5.3-2 Fermi 2 Tests

\*Vent clearing time (from  $T_0$ ) determined from the movie films.\*\*Time difference from  $T_0$  to time of zero downforce.

—No significant downforce valley or 2nd peak downforce.

\*(1) Start-of-test reference time

Parameter	Test No.	0" $\Delta P$ , 6.56-inch "T" Deflector				Mean	Std. Dev.
		(5)	(6)	(7)	(8)		
$T_0$ *(1)	(sec)						
Vent Clearing Time*	(sec)						
<u>Peak Downforce</u>							
Pressure Integral:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
Corrected Pressure Integral:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
Corrected Load Cell:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
<u>Downforce Valley</u>							
Pressure Integral:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
Corrected Pressure Integral:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
Corrected Load Cell:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
<u>2nd Peak Downforce</u>							
Pressure Integral:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
Corrected Pressure Integral:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
Corrected Load Cell:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
<u>[<math>\Delta t</math>] Downforce Time**</u>							
Pressure Integral	(sec)						
Corrected Pressure Integral	(sec)						
Corrected Load Cell	(sec)						
<u>Downforce Impulse</u>							
Pressure Integral:							
Impulse	(lb-sec)						

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TABLE A-7 (Continued)

\*Time at force is zero (from  $T_0$ )  
 —No significant 2nd peak upforce

## DATA FOR WETWELL VERTICAL LOADS (continued)

## Task 5.5.3-2 Fermi 2 Tests

Parameter	Test No.	0" $\Delta P$ , 6.56-inch "T" Deflector				Mean	Std. Dev.
		(5)	(6)	(7)	(8)		
<u>Peak Upforce</u>							
Pressure Integral:							
Force (lb)	(1b)						
Time (from $T_0$ ) (sec)	(sec)						
Corrected Pressure Integral:							
Force (lb)	(1b)						
Time (from $T_0$ ) (sec)	(sec)						
Corrected Load Cell:							
Force (lb)	(1b)						
Time (from $T_0$ ) (sec)	(sec)						
<u>Upforce Valley</u>							
Pressure Integral:							
Force (lb)	(1b)						
Time (from $T_0$ ) (sec)	(sec)						
Corrected Pressure Integral:							
Force (lb)	(1b)						
Time (from $T_0$ ) (sec)	(sec)						
Corrected Load Cell:							
Force (lb)	(1b)						
Time (from $T_0$ ) (sec)	(sec)						
<u>2nd Peak Upforce</u>							
Pressure Integral:							
Force (lb)	(1b)						
Time (from $T_0$ ) (sec)	(sec)						
Corrected Pressure Integral:							
Force (lb)	(1b)						
Time (from $T_0$ ) (sec)	(sec)						
Corrected Load Cell:							
Force (lb)	(1b)						
Time (from $T_0$ ) (sec)	(sec)						
<u>Zero Force Time*</u>							
Pressure Integral (sec)	(sec)						
Corrected Pressure Integral (sec)	(sec)						
Corrected Load Cell (sec)	(sec)						

TABLE A-8

DATA FOR VENT HEADER IMPACT LOADS

## Task 5.5.3-2 Fermi Tests

Parameter \ Test No.	7.03" $\Delta P$ , 6.56 inch "T" Deflector				0" $\Delta P$ , 6.56 inch "T" Std. Deflector	
	( 1 )	( 2 )	( 3 )	( 4 )	Mean	Dev. ( 5 )
$T_0$ (sec)						
Vent Header Impact						
Pressure Integral:						
Maximum Force (lb)						
Impulse (lb-sec)						
Duration* (sec)						
Load Cell Corrected:						
Maximum Force (lb)						
Impulse (lb-sec)						
Duration (sec)						
Pool Surface Velocity (ft/sec)						
Time (from $T_0$ )** (sec)						

\* Based on impact pressure measurements

\*\* At start of the first impact pressure recorded

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## A.4 Duane Arnold Tests

### A.4.1 Typical Data

Time-history plots of the driving conditions and pool response are presented in this section for Duane Arnold Tests 3 and 5. Test 3 was a load definition test which was conducted at a partial drywell/wetwell differential pressure of  $9.19'' \text{ H}_2\text{O } \Delta P$  and with no deflector. Test 5 was conducted without an initial drywell/wetwell differential pressure ( $0'' \Delta P$ ) and with no deflector.

#### A.4.1.1 Driving Conditions

Driving conditions for Duane Arnold Test 3 are presented in Figures A-150 through A-154. Similar plots for Test 5 are shown in Figures A-155 through A-159. Duane Arnold driving conditions had the same characteristics as the "typical" plant discussed in Section 3.0 of this report.

#### A.4.1.2 Pool Response

Downcomer internal pressure and wetwell pressures for Duane Arnold Tests 3 and 5 are presented in Figures A-160 through A-161 and A-162 through A-163, respectively. Net torus force from the pressure integral (Figures A-164 and A-165) shows some oscillations in downforce as well as in upforce. Net torus force that is determined from the torus load cell (Figures A-166 and A-168) by applying inertial correction with the torus accelerometer (Figures A-167 and A-169) is shown in Figures A-170 and A-171 and compared with net torus force determined from the pressure integral. Figures A-172 and A-173 present the net torus force based on the torus pressure integral, corrected for inertia.

The "average" pool pressures for Duane Arnold Tests 3 and 5 are shown in Figures A-174 and A-176. Figure A-175 and A-177 are the same as Figures A-172 and A-173 with force replaced by average pressure (force/torus projected area).

The vent header impact pressures for Duane Arnold Test 3 are presented in Figures A-178 through A-180. Vent header pressures for Test 5 are presented in Figures A-181 through A-183. These figures illustrate that, for the Duane Arnold single downcomer with unprotected vent header, the impact pressures are higher on the center row and decrease rapidly in the lateral direction. The maximum vent header force from the corrected load cell is somewhat lower than the maximum force from the pressure integral (Figure A-184).

The vent header impact force is not very sensitive to drywell/wetwell  $\Delta P$  for the Duane Arnold tests. Vent header impact mitigation from  $\Delta P$  may be primarily due to a reduction in the slug thickness at impact, since velocity is typically insensitive to  $\Delta P$ . Based on the review of the Duane Arnold movies, the minimum slug thickness at zero  $\Delta P$  appears to be no thicker than for partial  $\Delta P$  condition due to the presence of small bubbles (thought to originate at vent clearing) on top of the main bubble at zero  $\Delta P$ . In a two downcomer geometry these small bubbles are not directly underneath the vent header.

Vent header vertical acceleration measurements from Tests 3 and 5 are shown in Figures A-185 and A-186, respectively.

#### A.4.2 Pool Dynamics

The pool contours at various times of pool swell are shown in Figures A-187 through A-190 for Duane Arnold Tests 1, 2, 3, and 5. Pool surface displacement curves are shown in Figures A-191 and A-193. The pool surface velocity profiles are shown in Figures A-192 and A-194.

The pool surface displacement and velocity profile viewed from the side window during Test 4 are shown in Figure A-195. The downcomer water slug displacement, velocity, and acceleration versus time for Test 3 are presented in Figure A-196. Similar plots are shown in Figure A-197 for Test 5.

The movies show that the pool swell is more concentrated under the header for a single downcomer. Therefore, although the total pool momentum is reduced, the vent impact velocity is relatively high. In addition, the pool appears to be quite flat along the header centerline. This pool swell configuration gives nearly simultaneous impact along the bottom of the header which produces peak pressures comparable to reference plant values.

#### A.4.3 Data Summaries

Table A-9 presents the Duane Arnold test data for wetwell vertical forces.

Table A-10 presents the Duane Arnold test data for vent header impact forces.

#### A.4.4 Discussion and Analysis

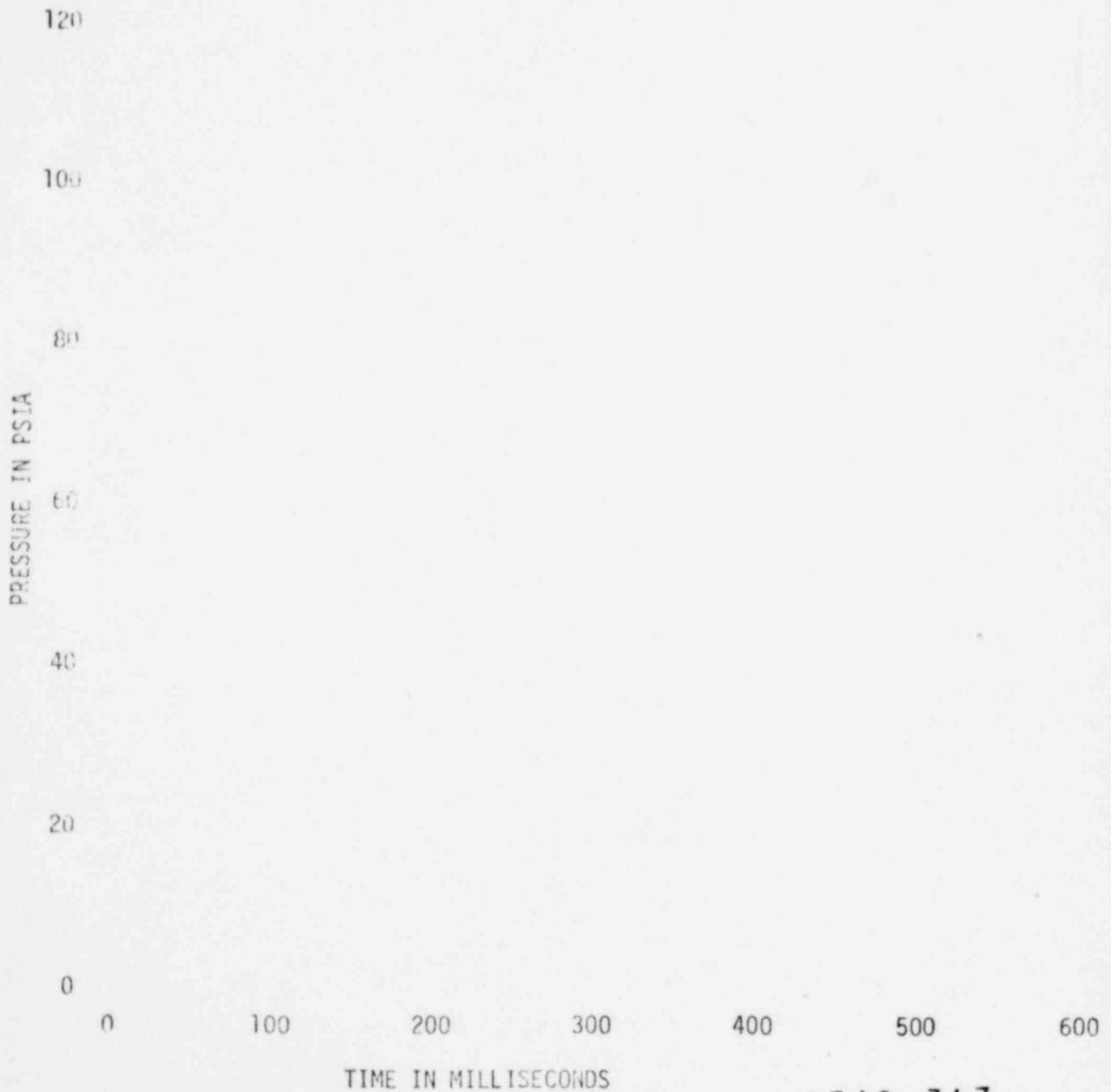
Figure A-198 presents the effect of drywell/wetwell  $\Delta P$  on the enthalpy flow into the bubbles. Effect of drywell/wetwell  $\Delta P$  on downcomer internal pressures is shown in Figure A-199. Figure A-200 presents the effect of drywell/wetwell  $\Delta P$  on pool and freespace pressures. This data for Duane Arnold parallels that for the "typical" plant in Section 3.0.

The Duane Arnold load definition tests were conducted at 9.19" H<sub>2</sub>O  $\Delta P$  with no deflector installed below the vent header. A  $\Delta P$  sensitivity test at 0"  $\Delta P$  was also conducted. The upforce as well as downforce had minor oscillations. The vent header impact force was significantly higher than for plants using deflectors.

FIGURE A-150

DRYWELL ORIFICE UPSTREAM PRESSURE

Task 5.5.3-2 Duane Arnold Test 3



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FIGURE A-151

DRYWELL PRESSURE

Task 5.5.3-2 Duane Arnold Test 3

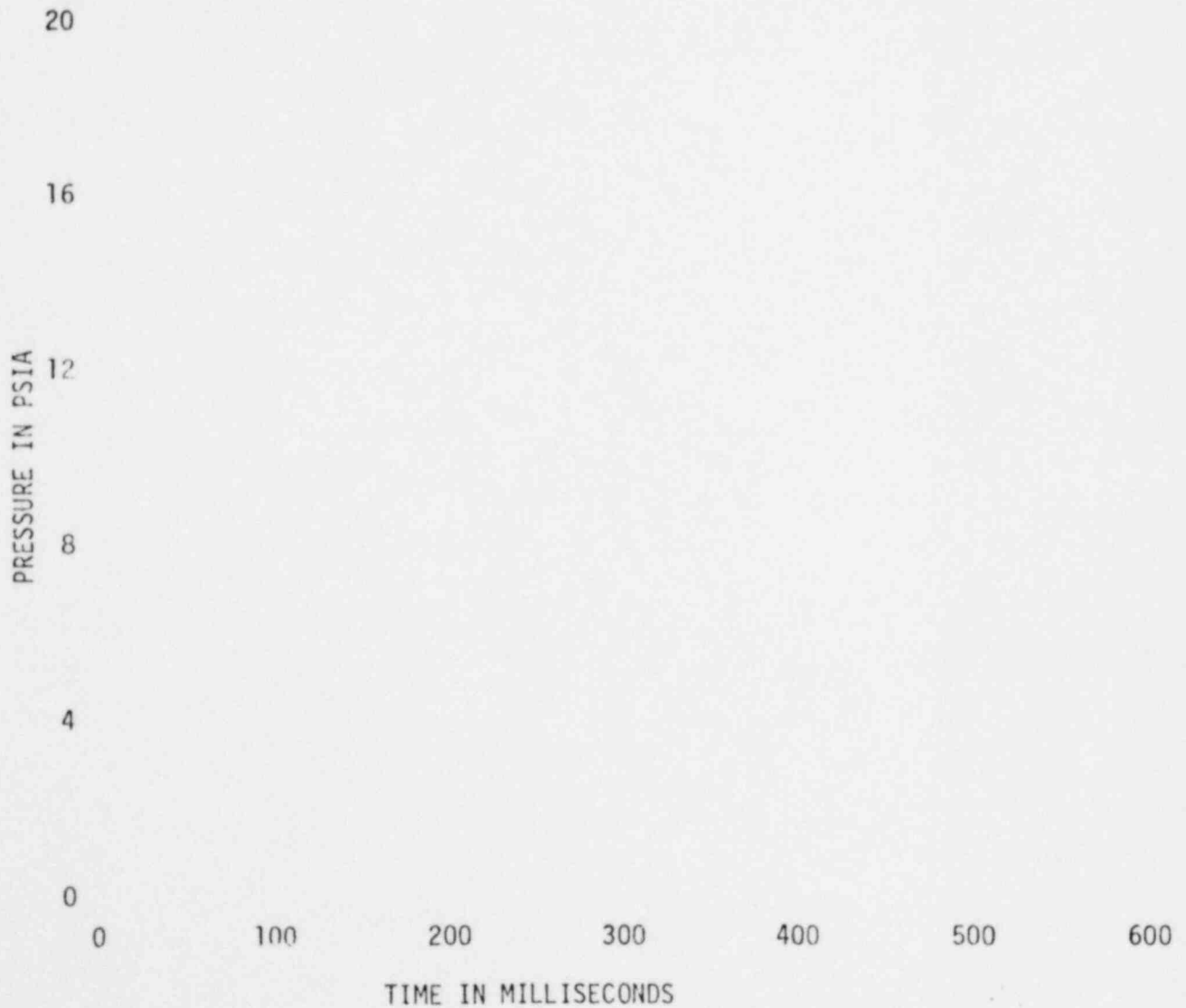


FIGURE A-152

DOWNCOMER ORIFICE DIFFERENTIAL PRESSURE

Task 5.5.3-2 Duane Arnold Test 3

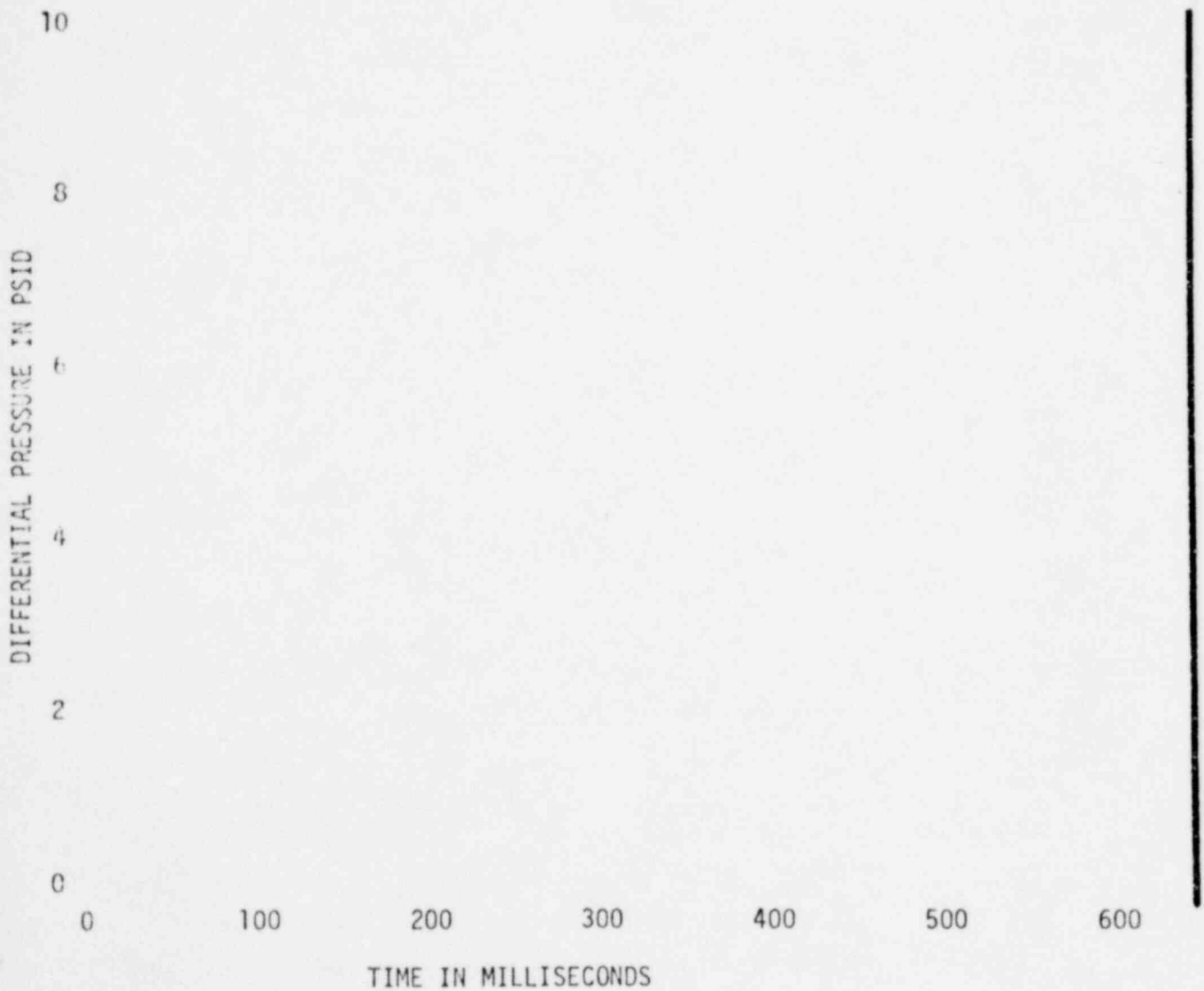


FIGURE A-153

DOWNCOMER ORIFICE UPSTREAM TEMPERATURE

Task 5.5.3-2 Duane Arnold Test 3

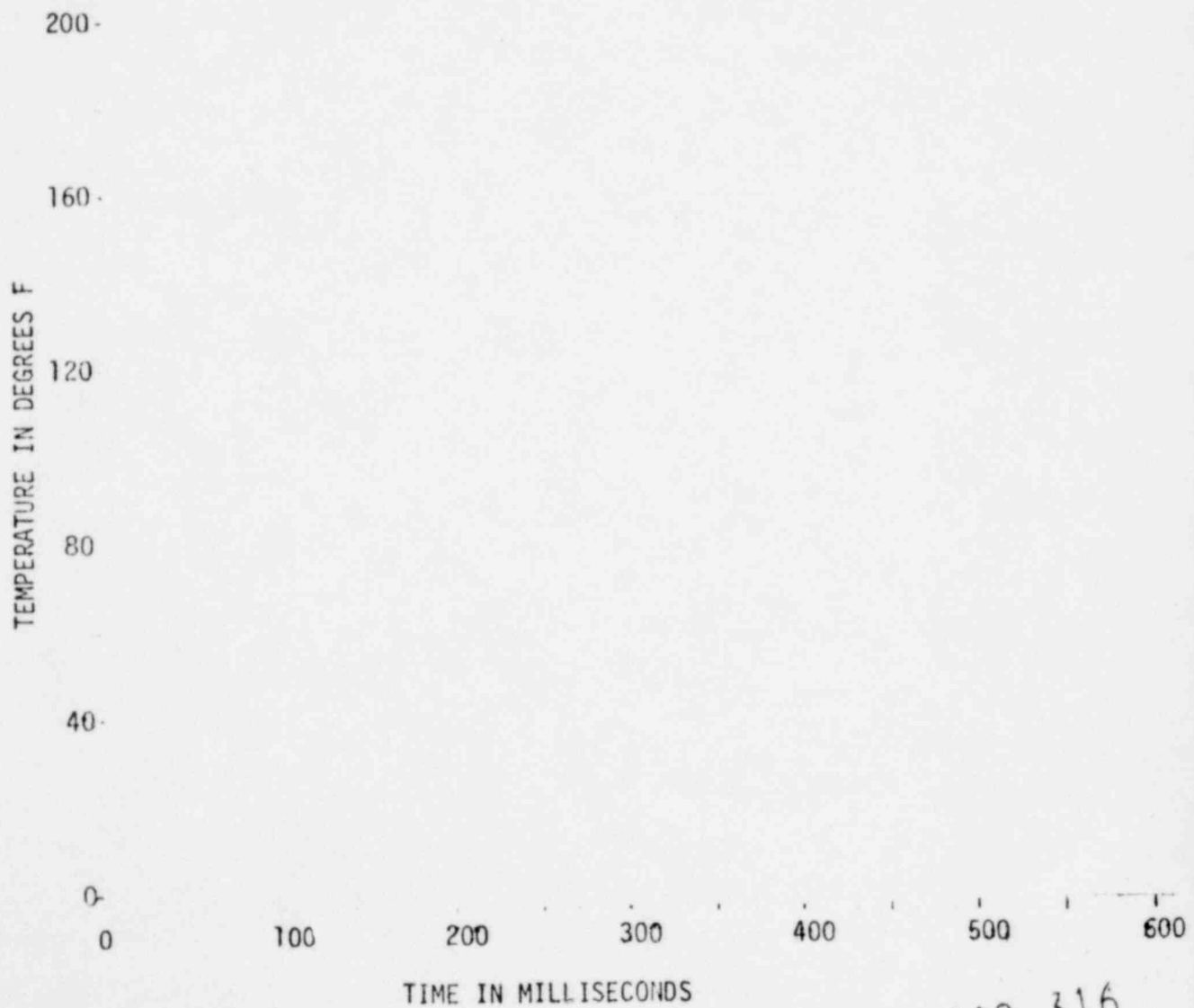
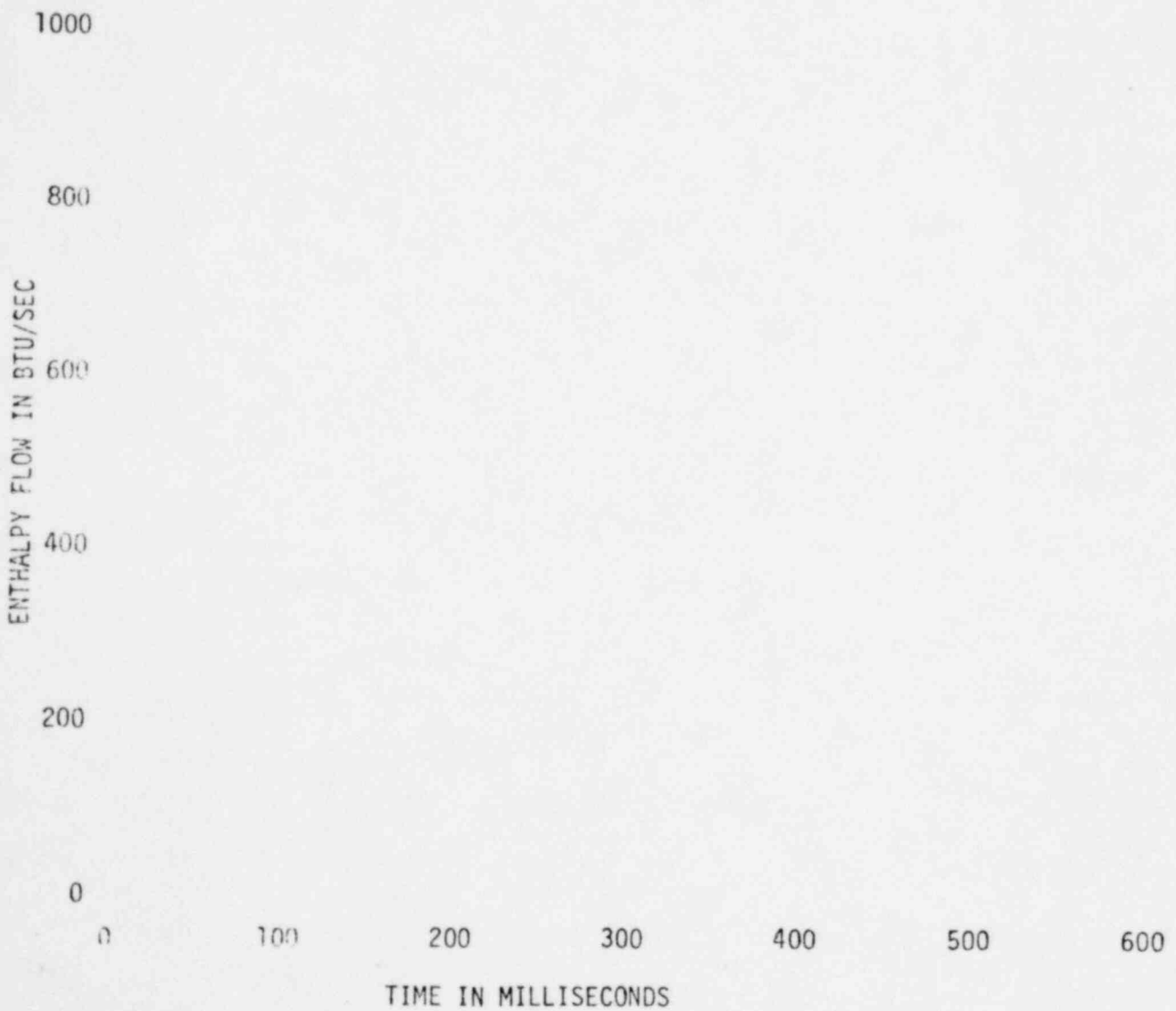


FIGURE A-154

ENTHALPY FLOW INTO POOL

Task 5.5.3-2 Duane Arnold Test 3

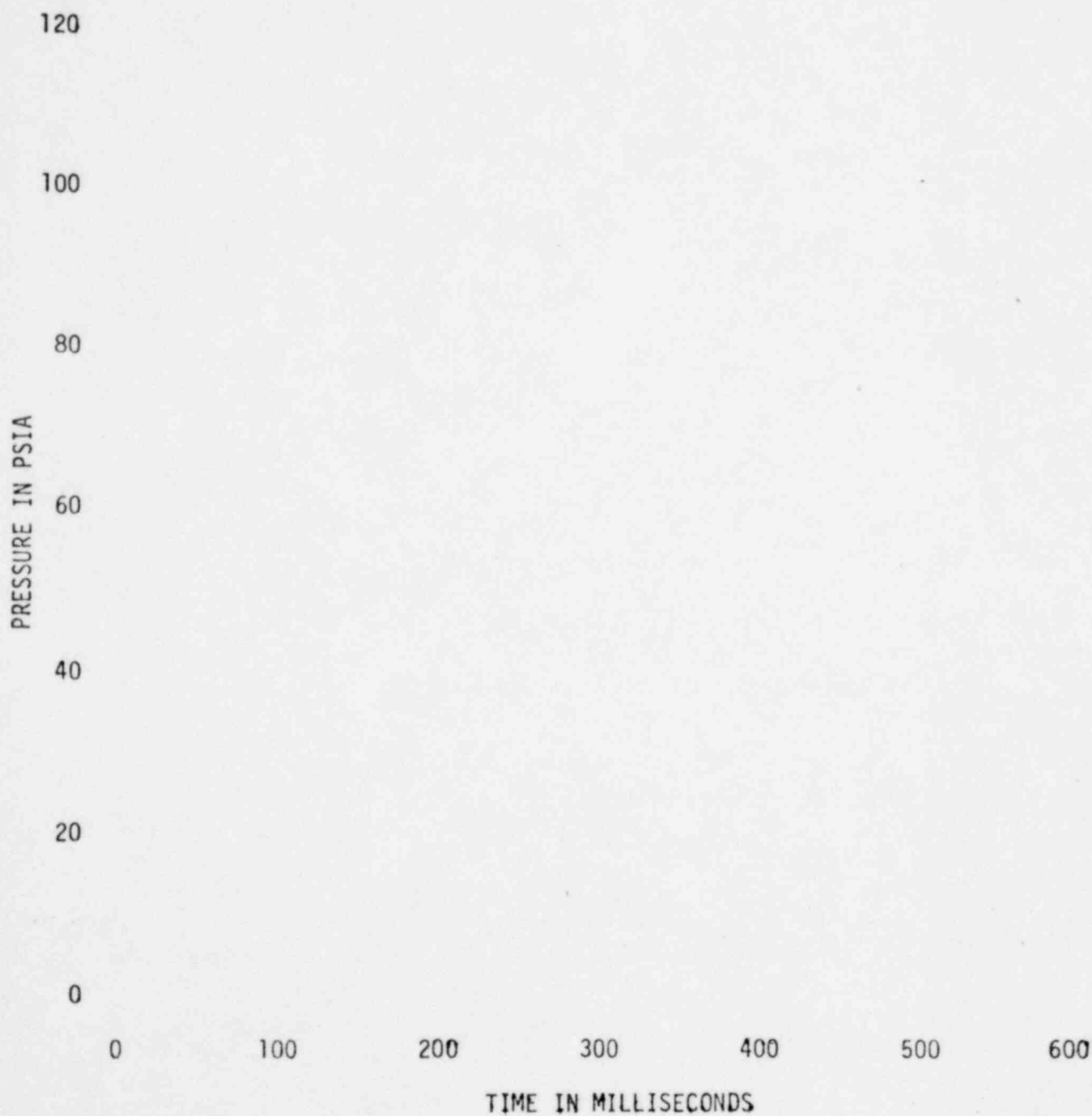


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FIGURE A-155

DRYWELL ORIFICE UPSTREAM PRESSURE

Task 5.5.3-2 Duane Arnold Test 5



1348 318

FIGURE A-156

DRYWELL PRESSURE

Task 5.5.3-2 Duane Arnold Test 5

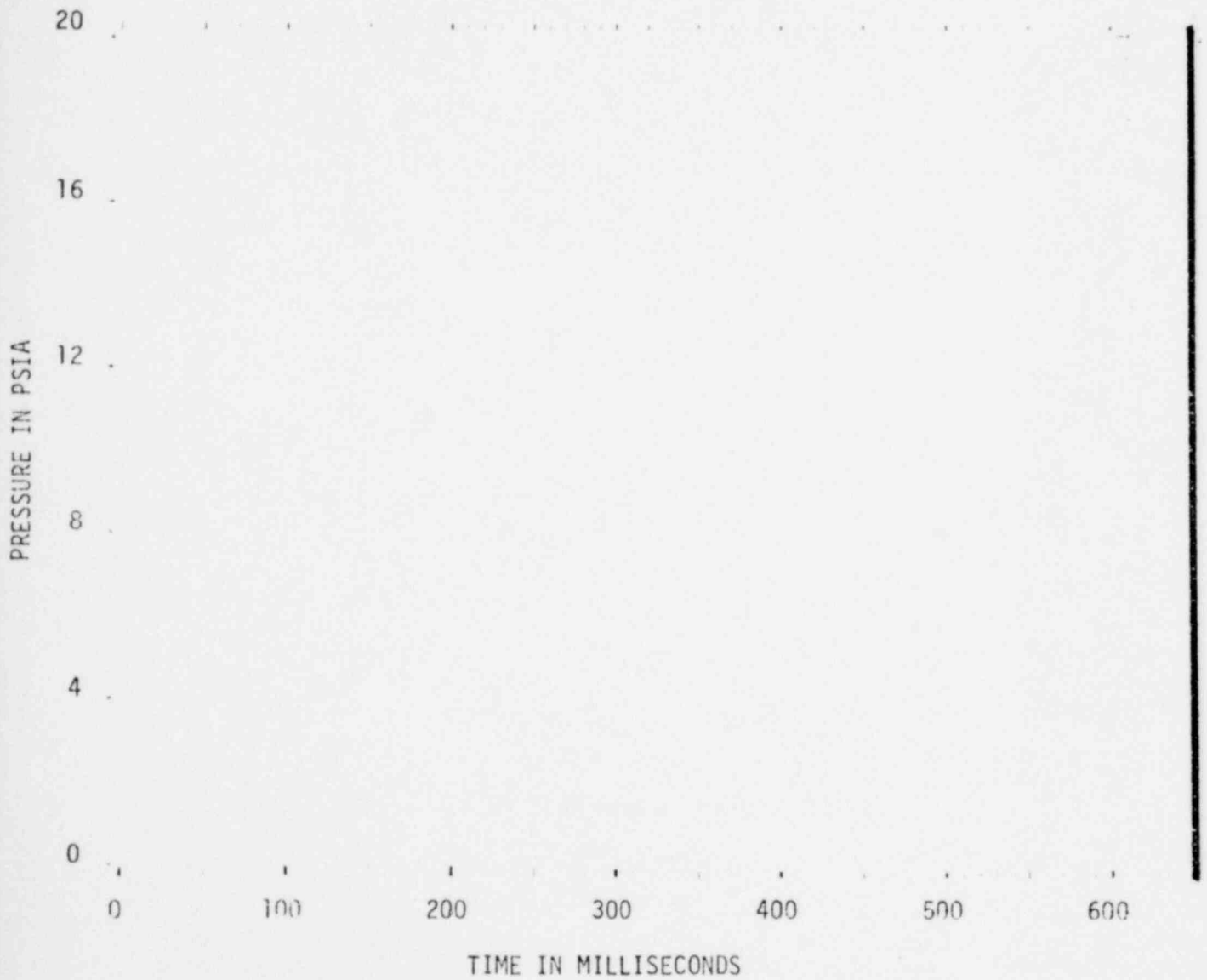


FIGURE A-157

DOWNCOMER ORIFICE DIFFERENTIAL PRESSURE

Task 5.5.3-2 Duane Arnold Test 5

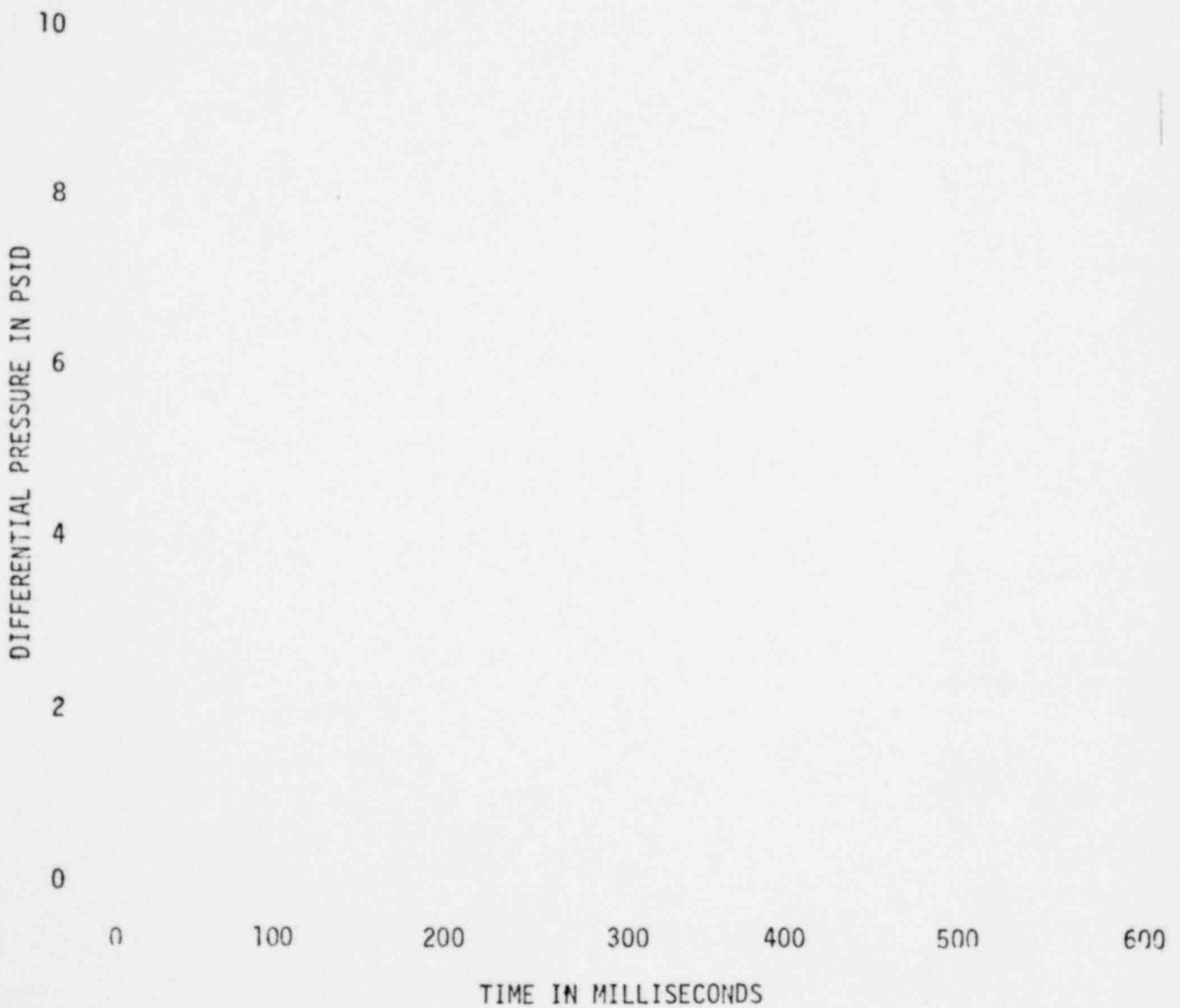


FIGURE A-158

DOWNCOMER ORIFICE UPSTREAM TEMPERATURE

Task 5.5.3-2 Duane Arnold Test 5

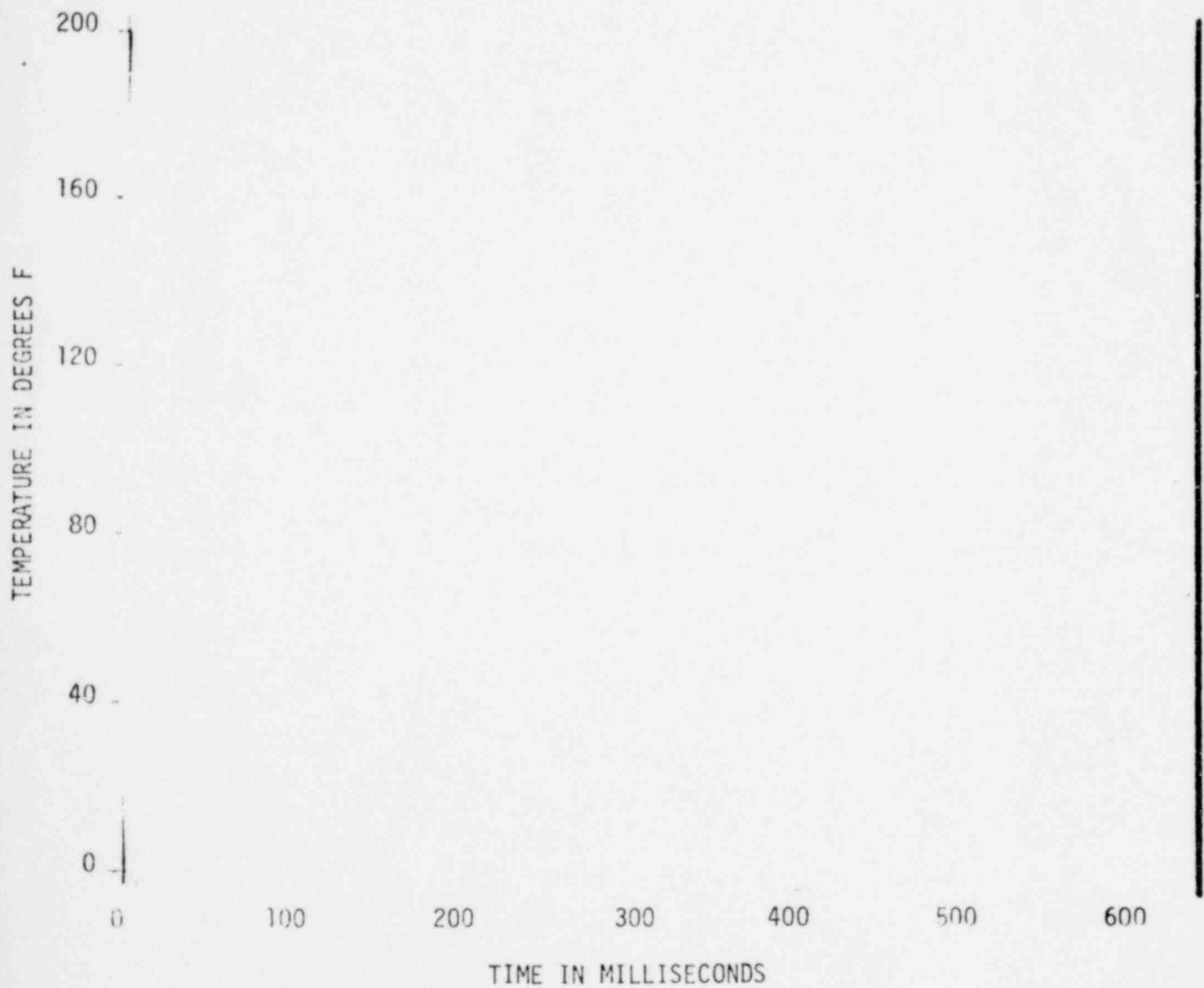


FIGURE A-159

ENTHALPY FLOW INTO POOL

Task 5.5.3-2 Duane Arnold Test 5

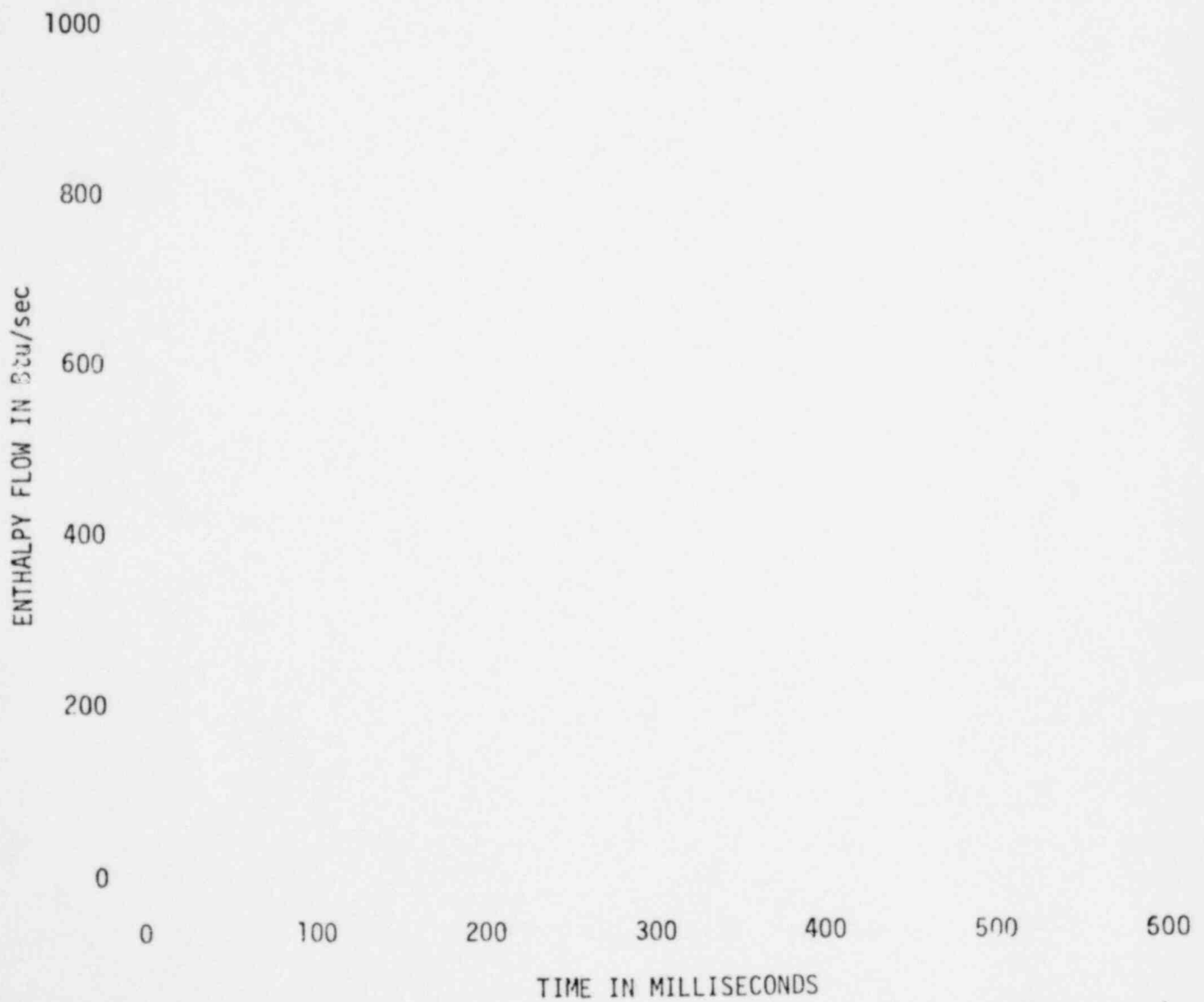


FIGURE A-160

DOWNCOMER INTERNAL PRESSURE

Task 5.5.3-2 Duane Arnold Test 3

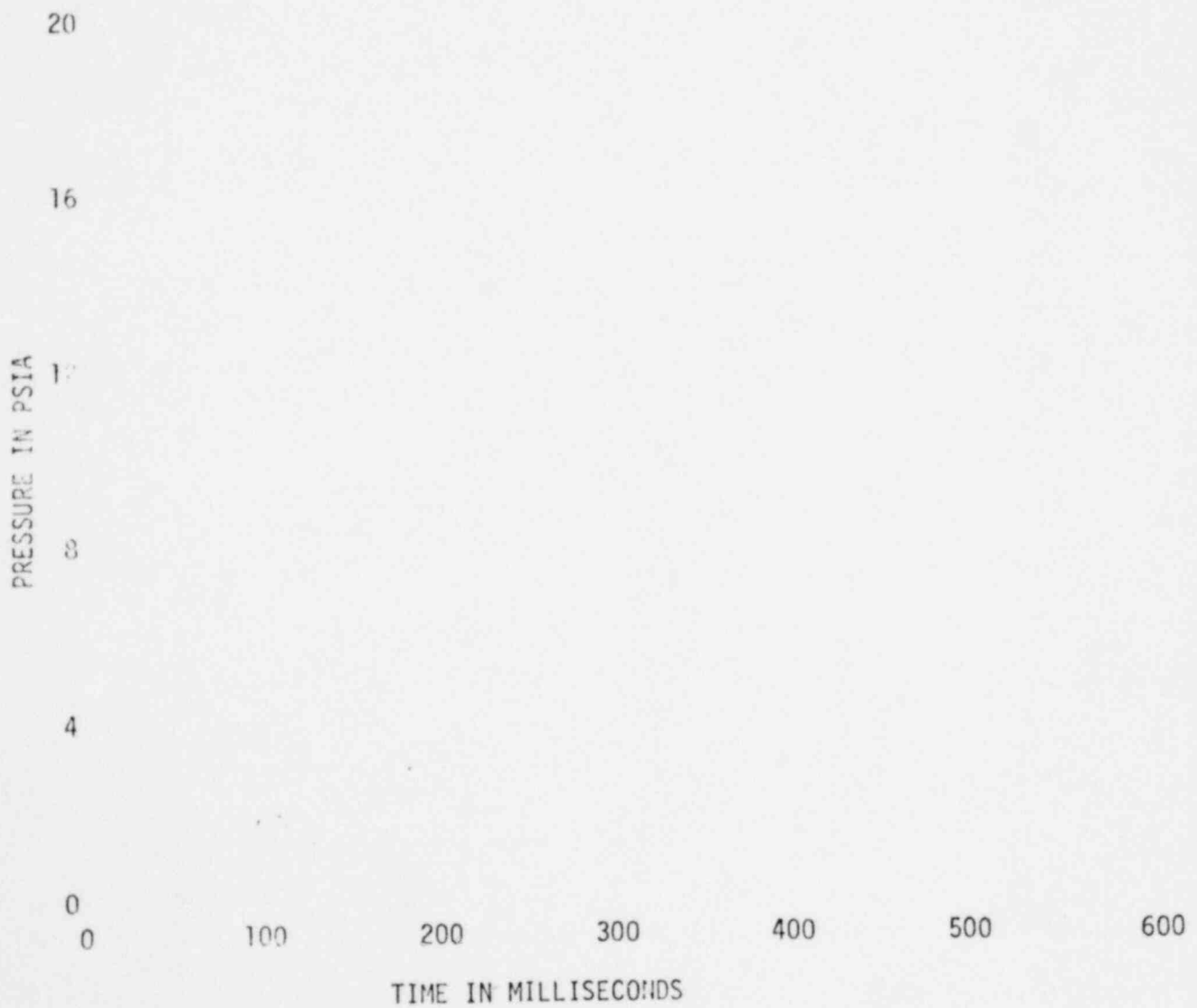


FIGURE A-161

WETWELL PRESSURES

Task 5.5.3-2 Duane Arnold Test 3

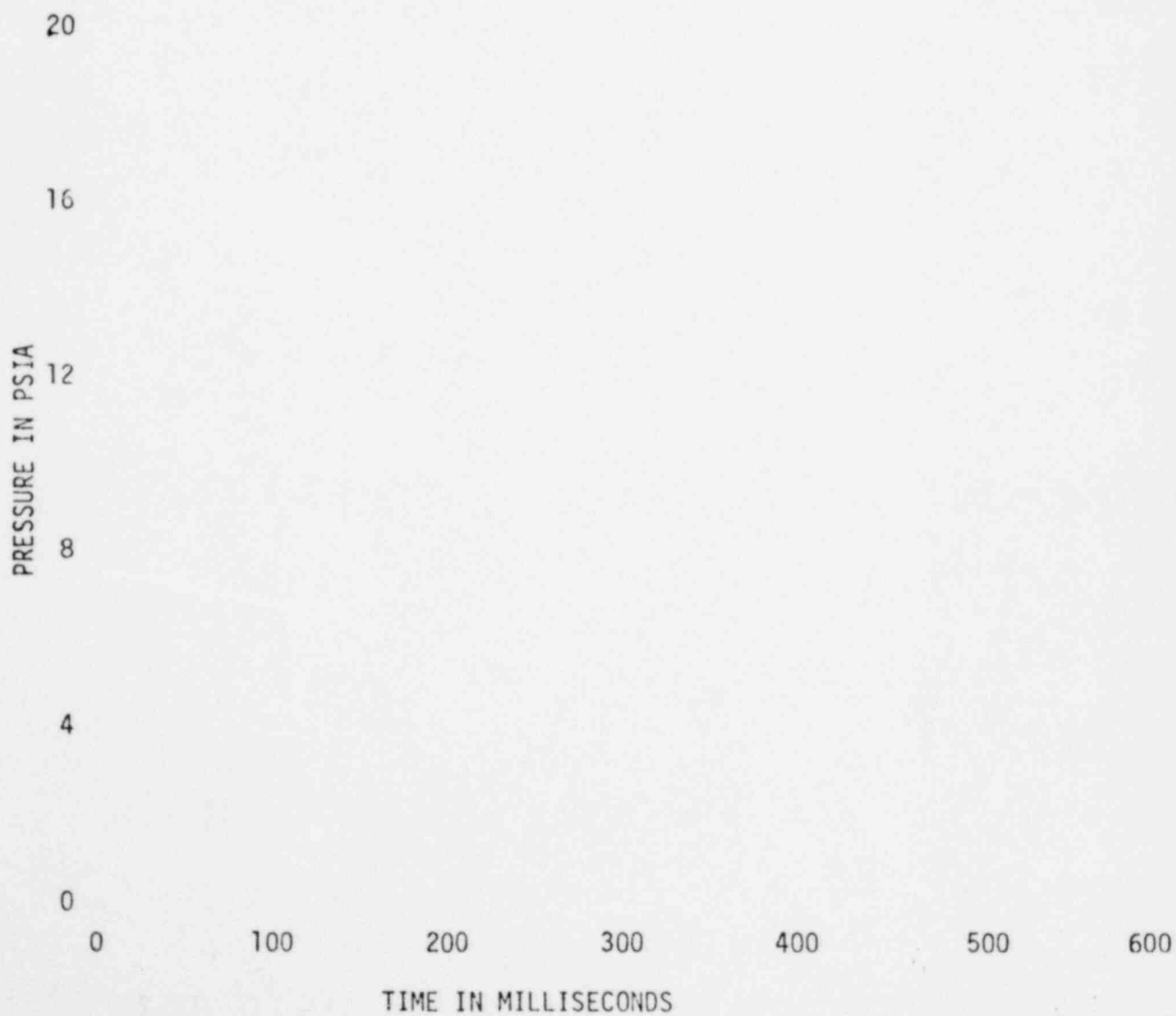
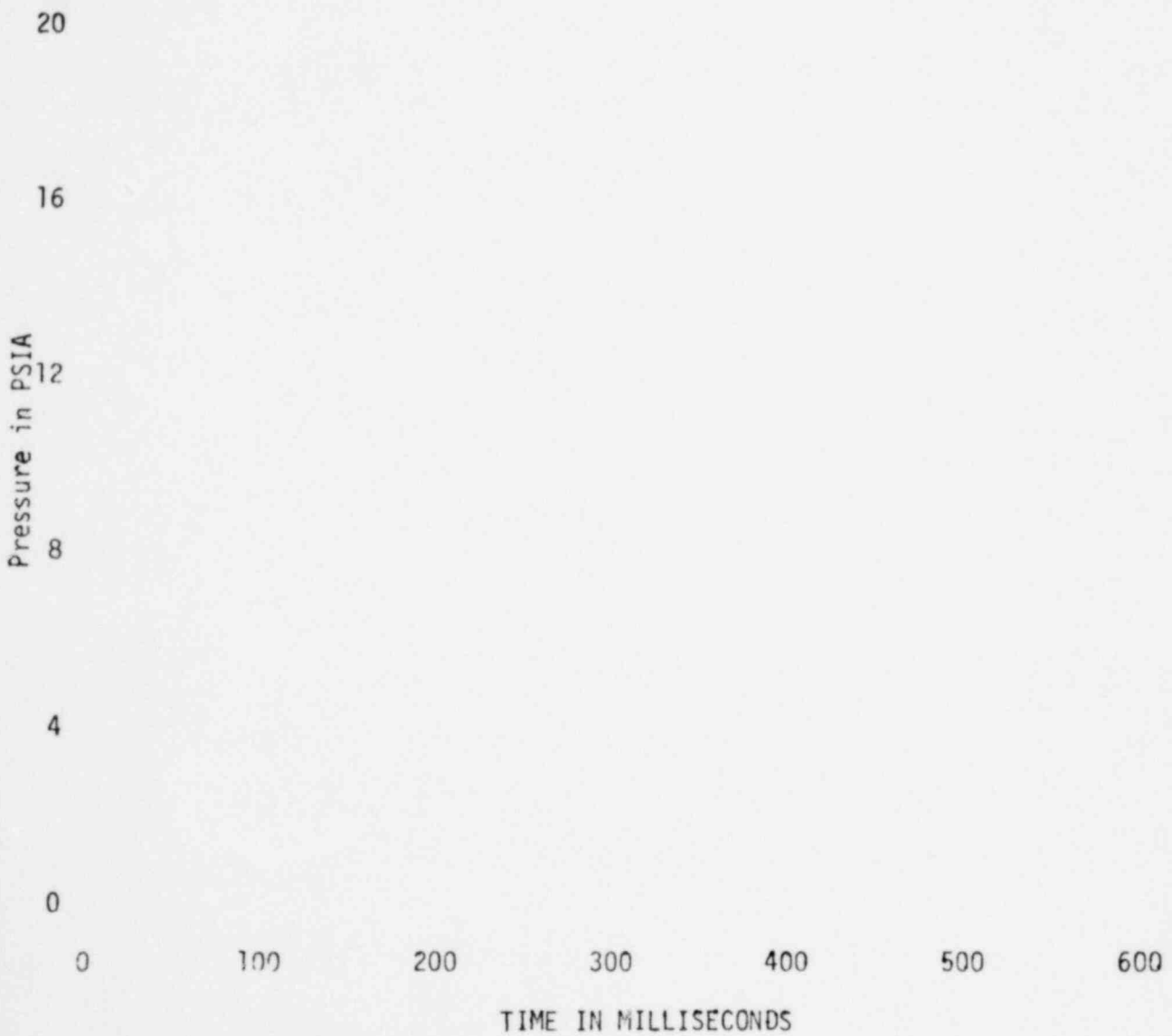


FIGURE A-162

DOWNCOMER INTERNAL PRESSURE

Task 5.5.3-2 Duane Arnold Test 5



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FIGURE A-163

WETWELL PRESSURES

Task 5.5.3-2 Duane Arnold Test 5



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FIGURE A-164

NET TORUS FORCE FROM PRESSURE INTEGRAL

Task 5.5.3-2 Duane Arnold Test 3



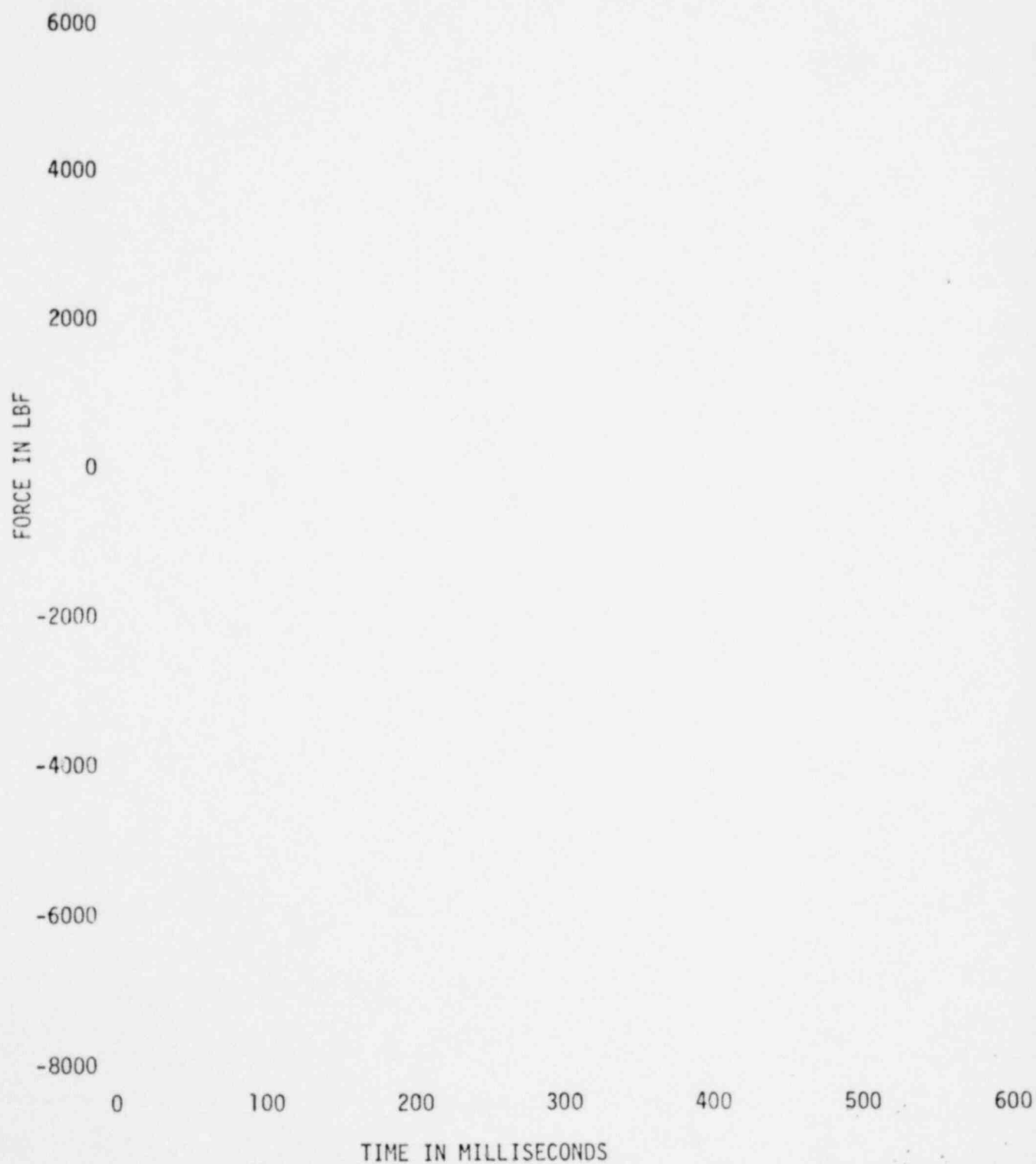
1348 327

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FIGURE A-165

NET TORUS FORCE FROM PRESSURE INTEGRAL

Task 5.5.3-2 Duane Arnold Test 5

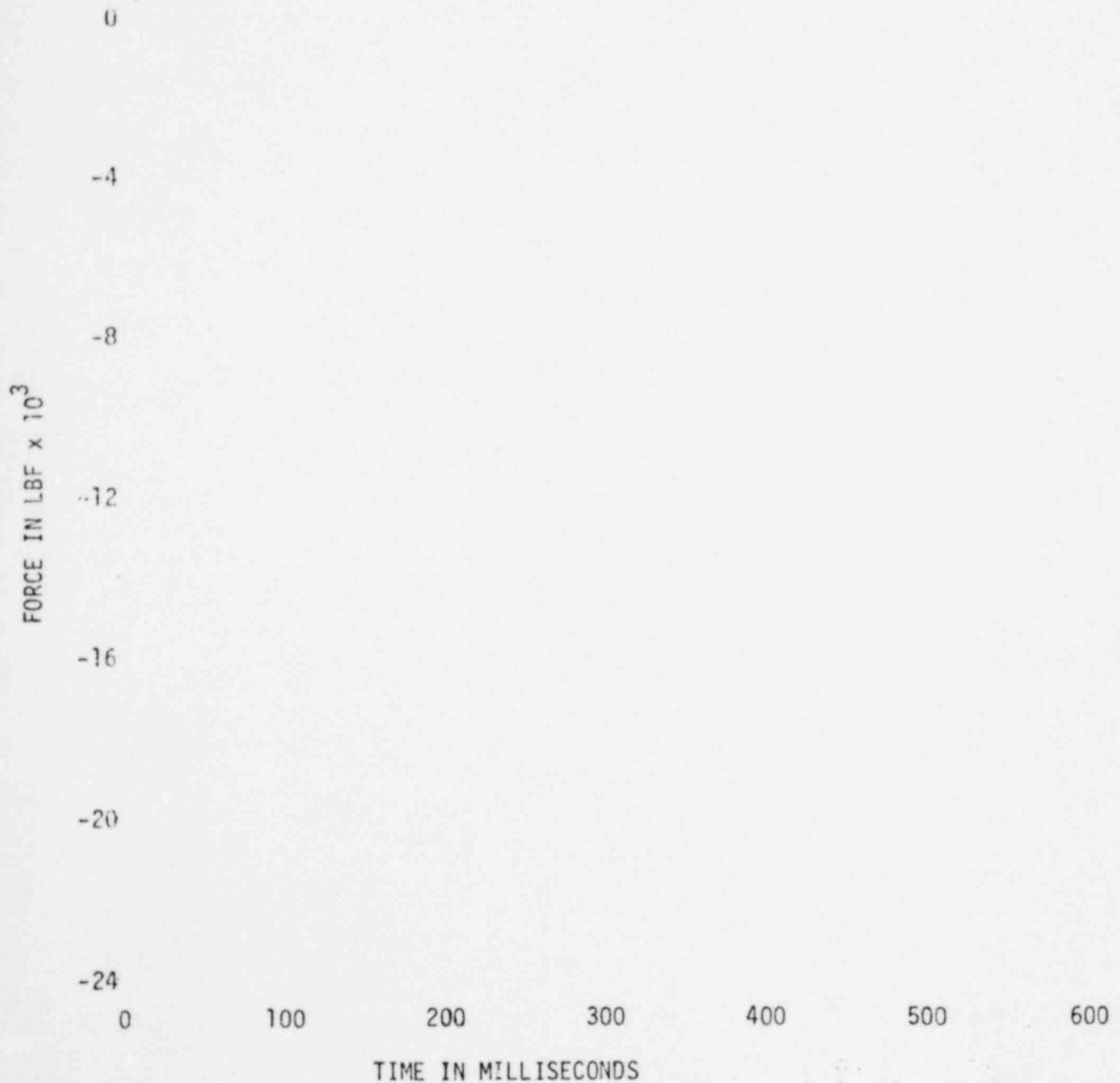


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FIGURE A-166

TORUS LOAD CELL

Task 5.5.3-2 Duane Arnold Test 3



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FIGURE A-167

TORUS VERTICAL ACCELERATION

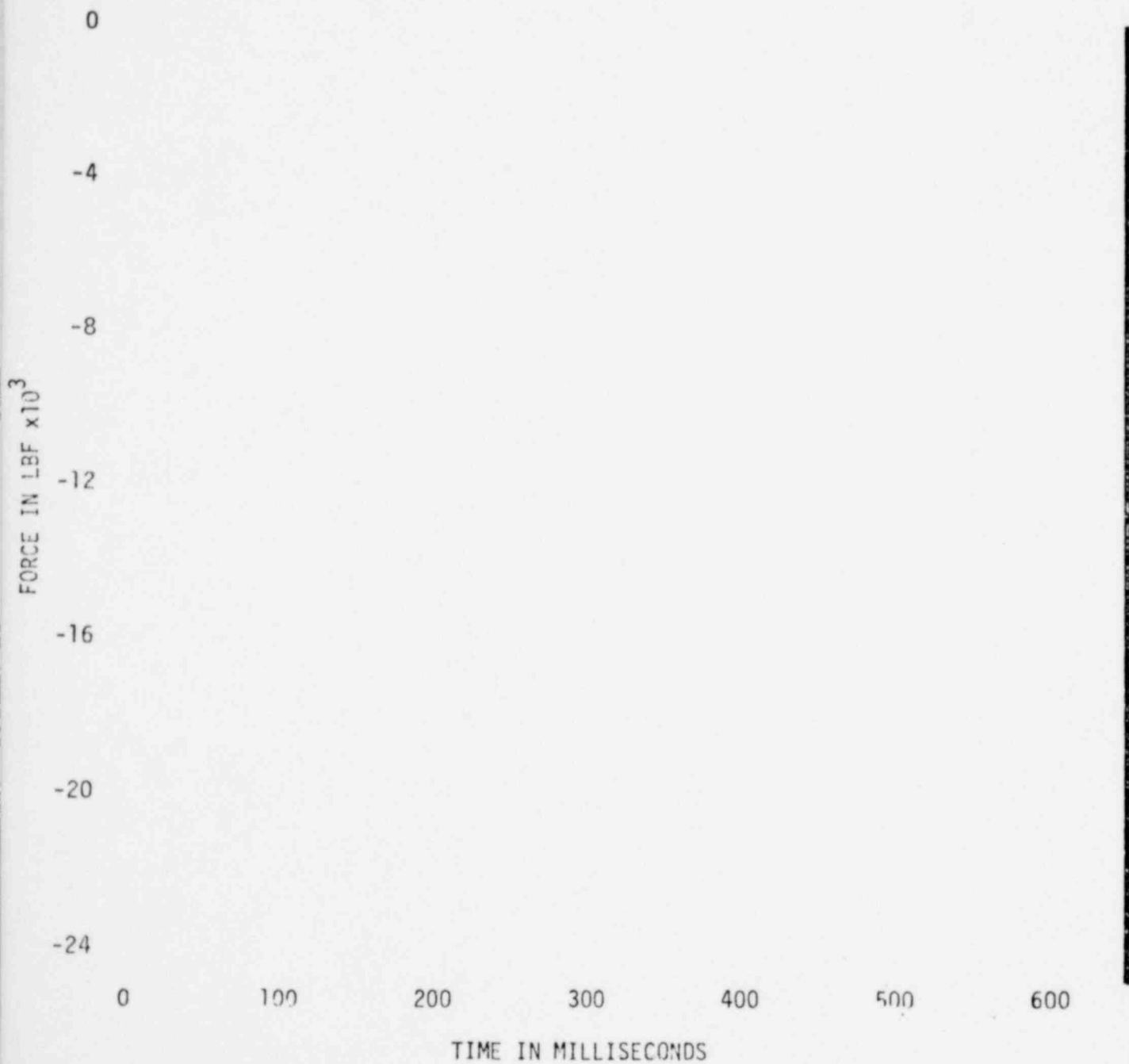
Task 5.5.3-2 Duane Arnold Test 3



FIGURE A-168

TORUS LOAD CELL

Task 5.5.3-2 Duane Arnold Test 5



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FIGURE A-169

TORUS VERTICAL ACCELERATION

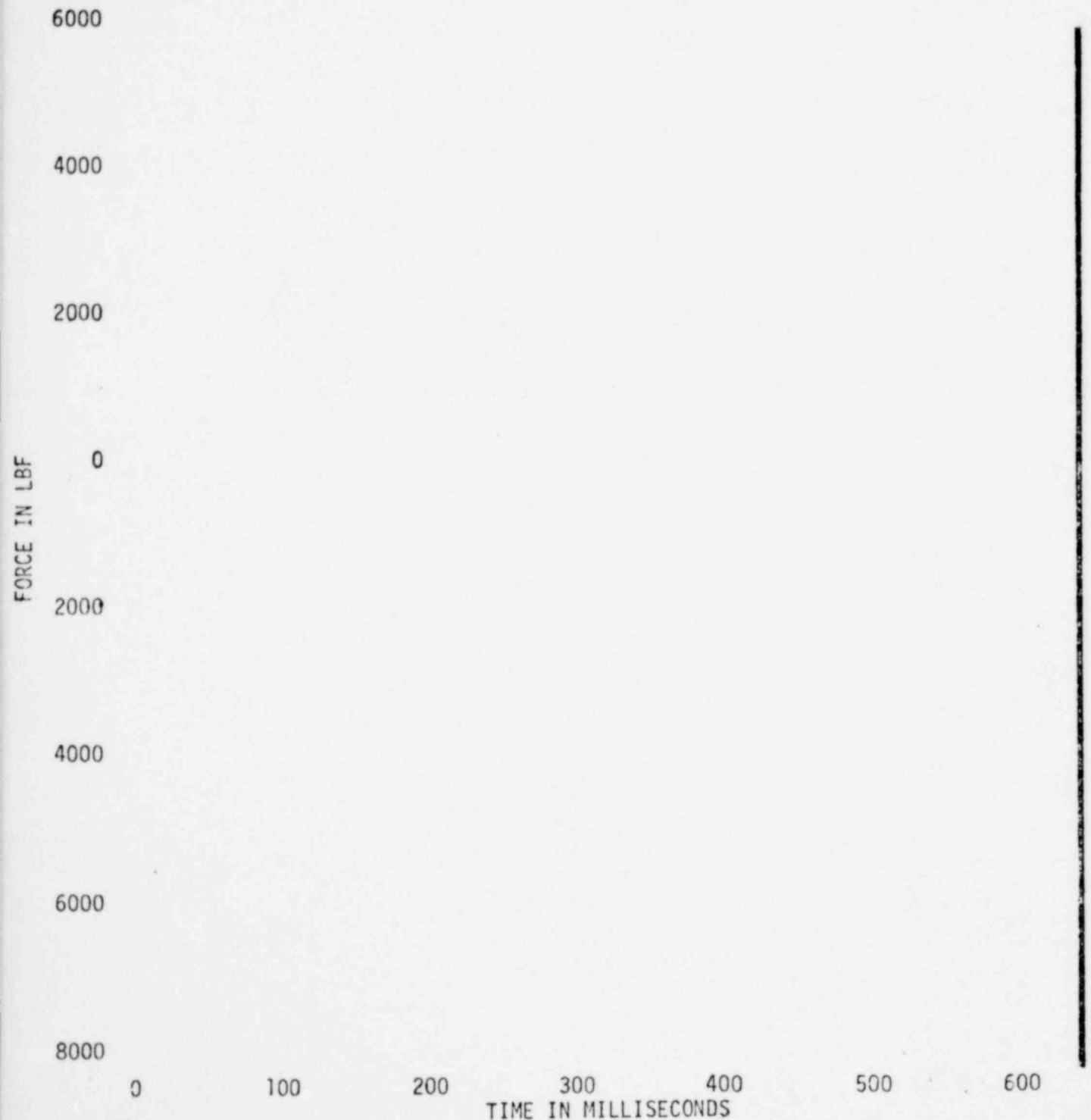
Task 5.5.3-2 Duane Arnold Test 5



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FIGURE A-170

COMPARISON OF NET TORUS FORCE FROM PRESSURE INTEGRAL  
WITH NET TORUS FORCE FROM LOAD CELL CORRECTED FOR TORUS INERTIA  
Task 5.5.3-2 Duane Arnold Test 3

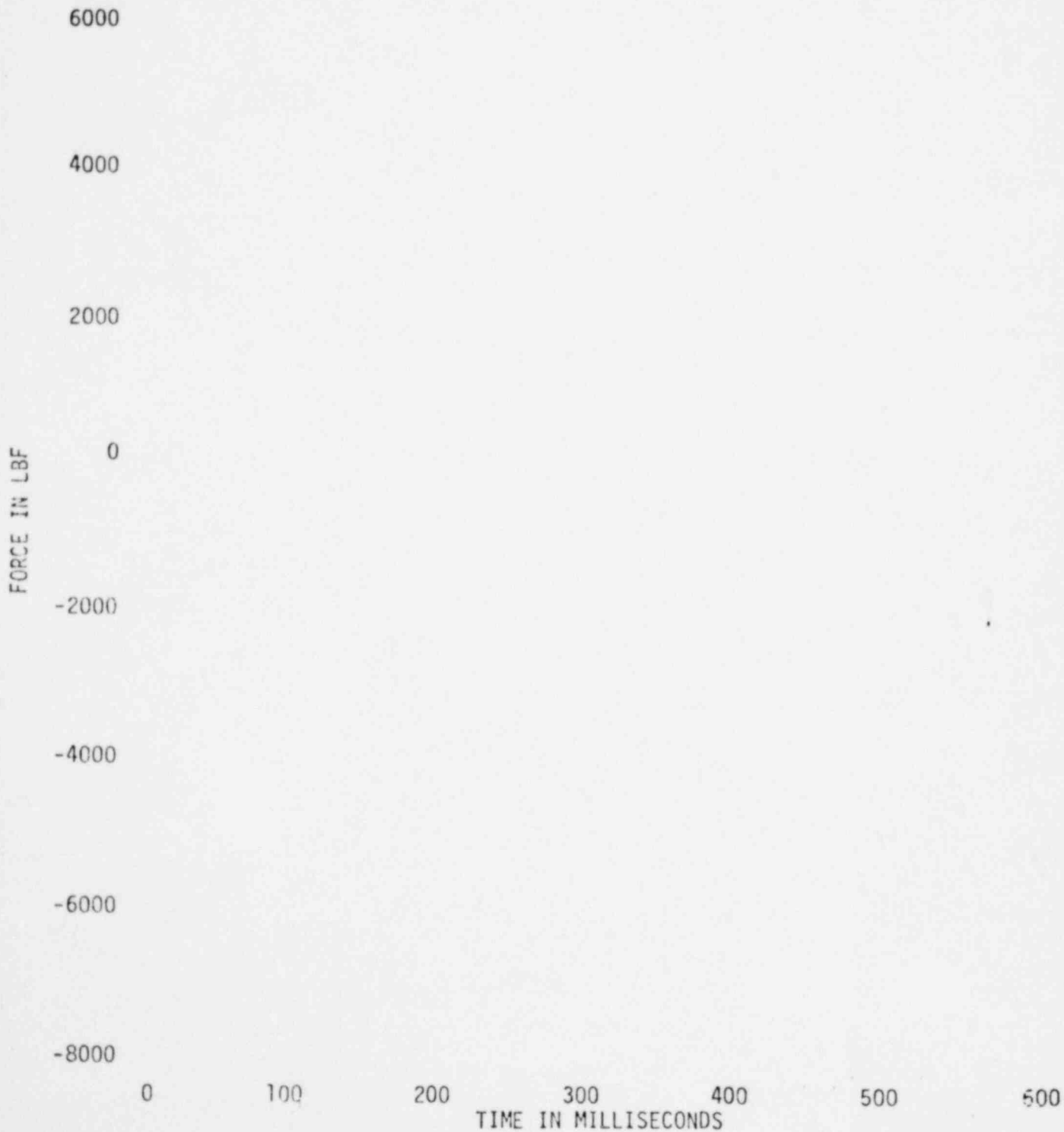


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FIGURE A-171

COMPARISON OF NET TORUS FORCE FROM PRESSURE INTEGRAL  
WITH NET TORUS FORCE FROM LOAD CELL CORRECTED FOR TORUS INERTIA

Task 5.5.3-2 Duane Arnold Test 5



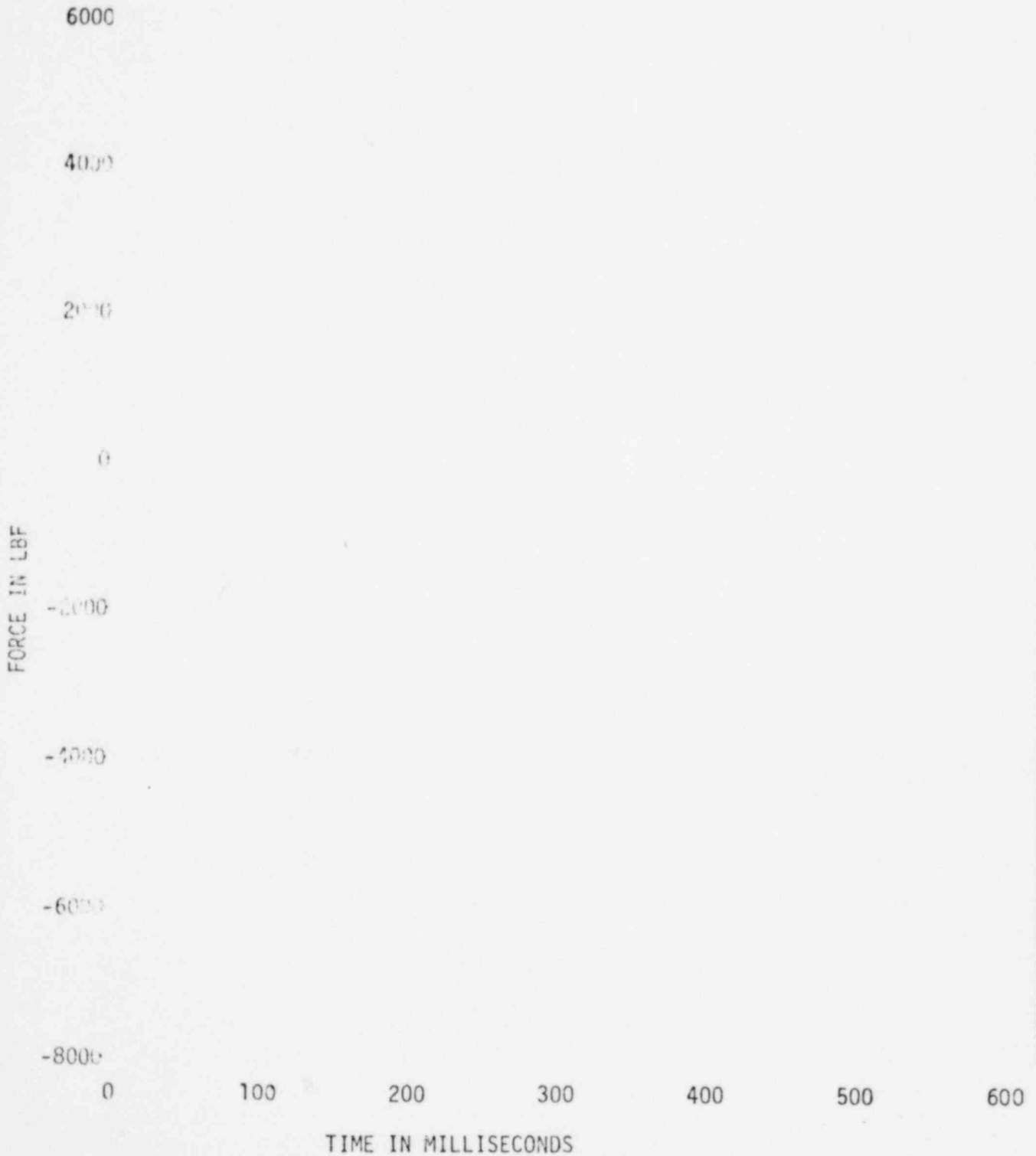
1348 334

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FIGURE A-172

NET TORUS FORCE FROM PRESSURE INTEGRAL, CORRECTED FOR WATER INERTIA

Task 5.5.3-2 Duane Arnold Test 3

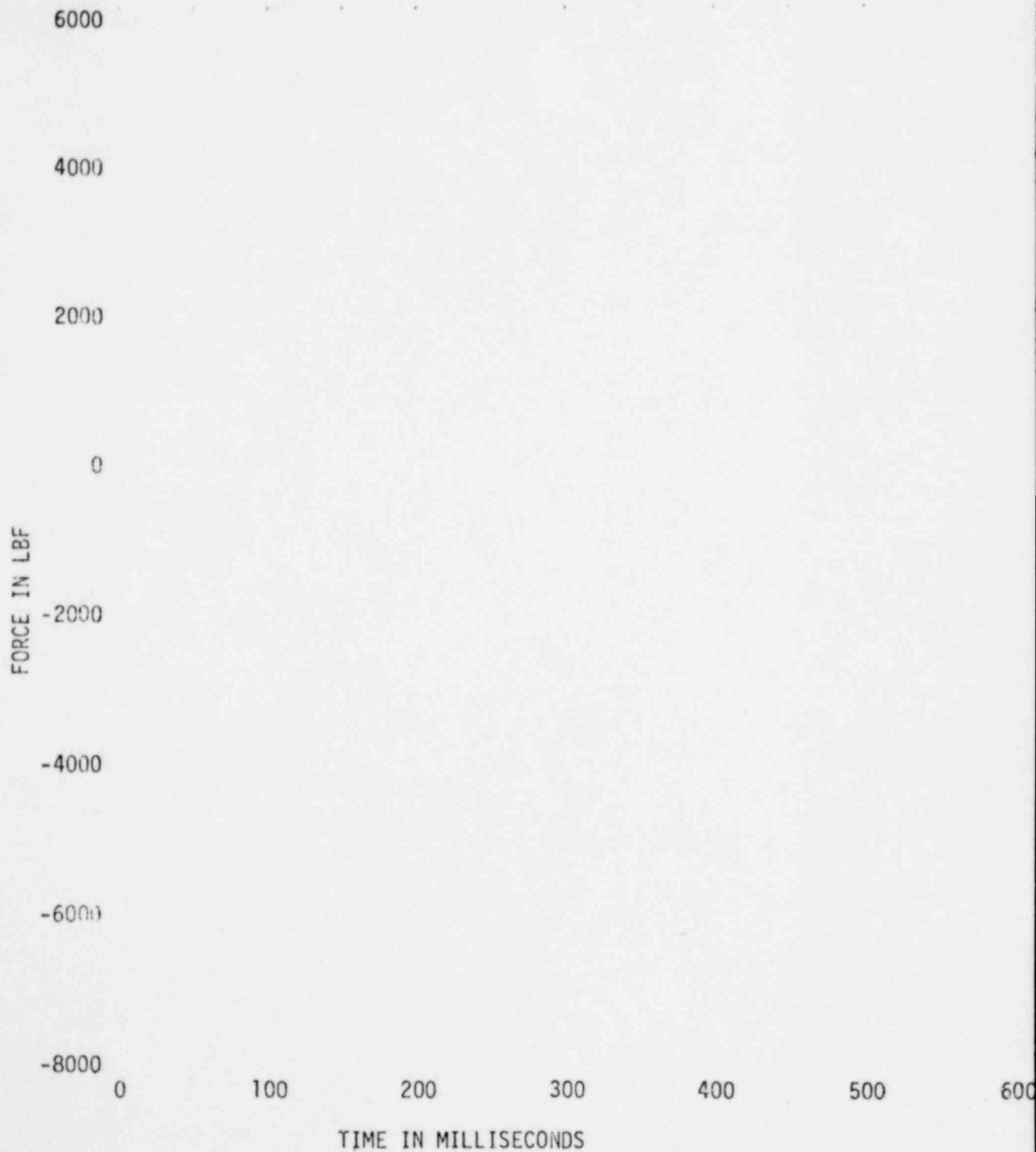


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FIGURE A-173

NET TORUS FORCE FROM PRESSURE INTEGRAL, CORRECTED FOR WATER INERTIA

Task 5.5.3-2 Duane Arnold Test 5



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FIGURE A-174

AVERAGE POOL PRESSURE, CORRECTED FOR WATER INERTIA

Task 5.5.3-2 Duane Arnold Test 3

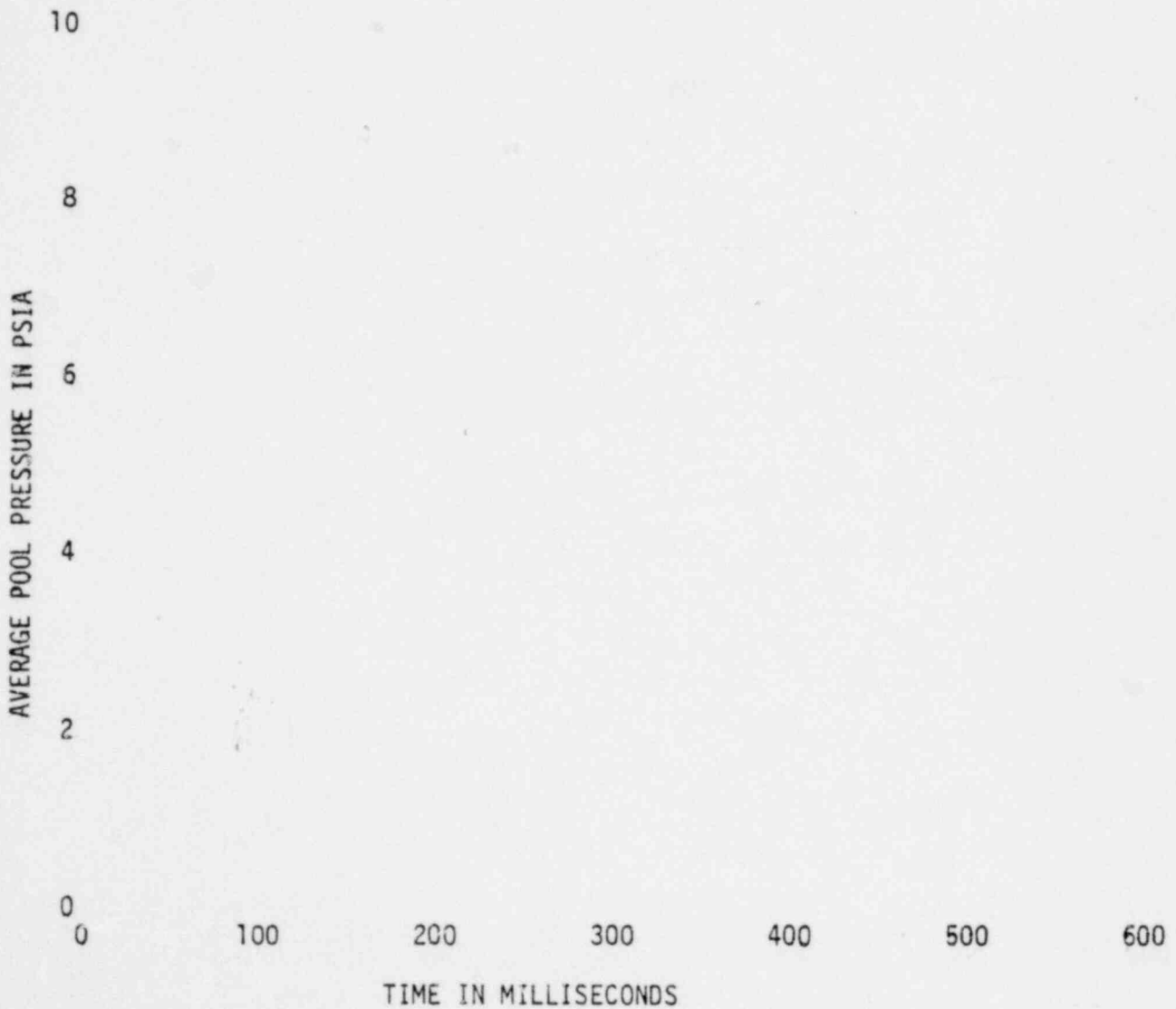


FIGURE A-175

NET AVERAGE POOL PRESSURE, CORRECTED FOR WATER INERTIA

Task 5.5.3-2 Duane Arnold Test 3

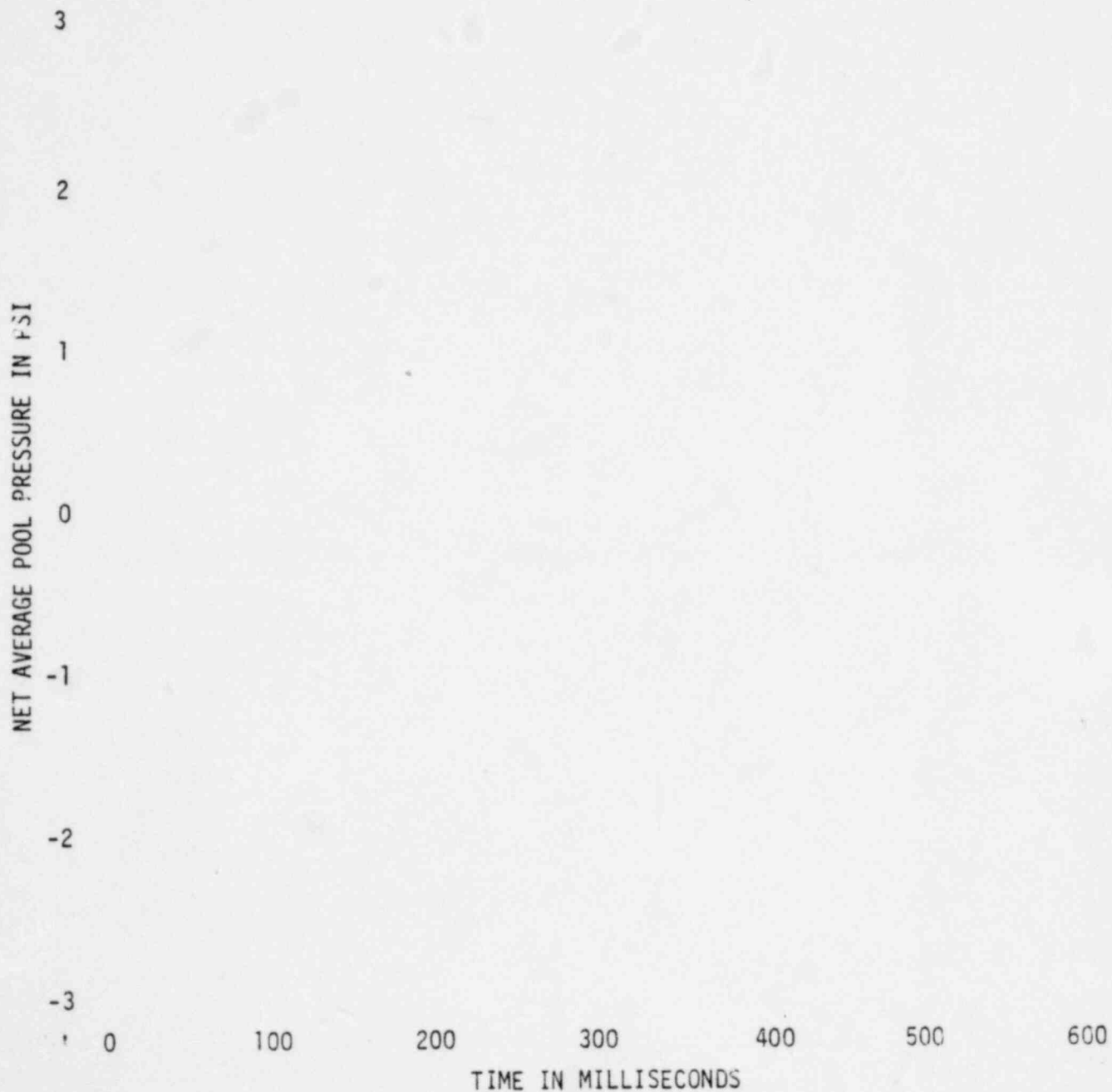
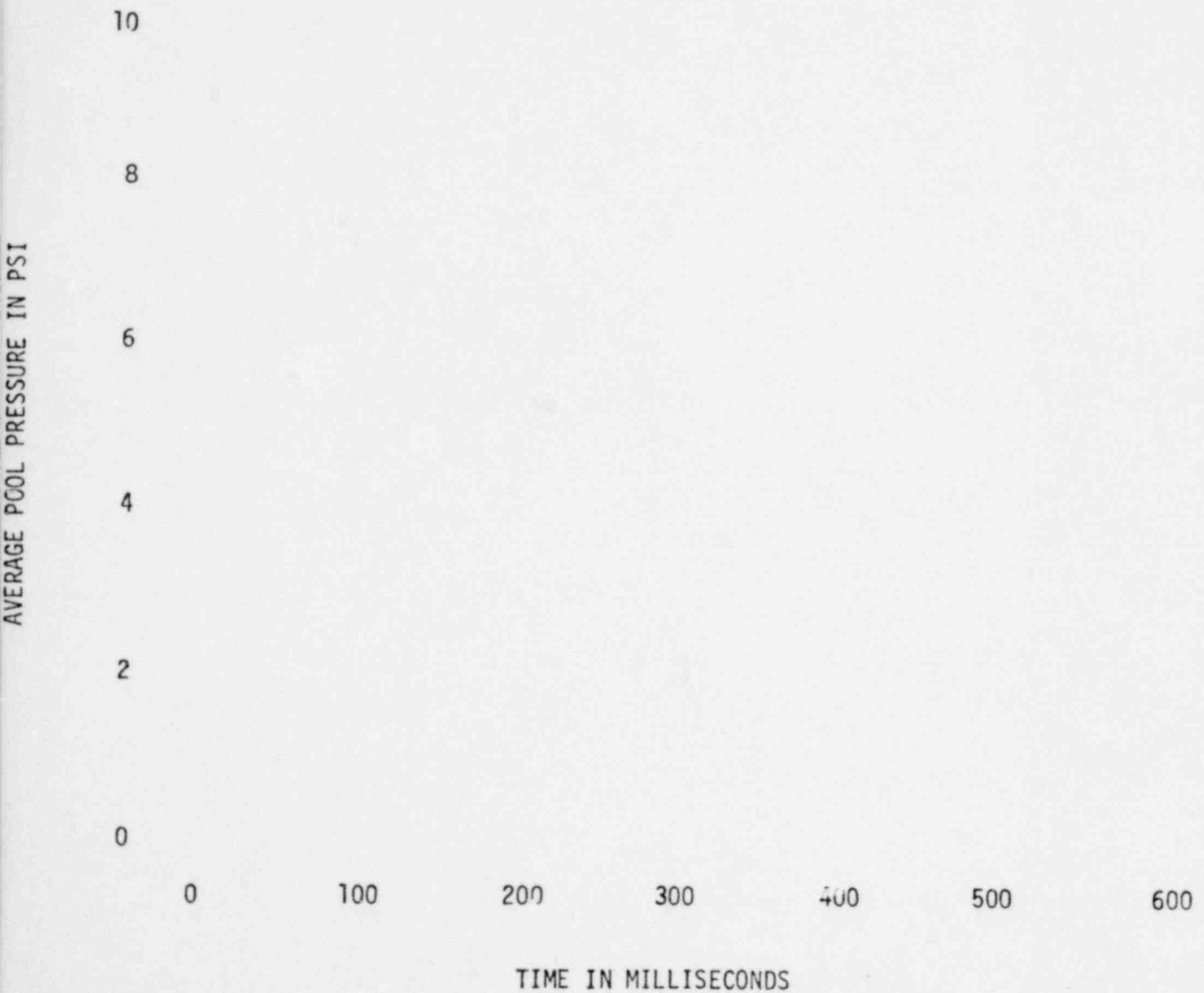


FIGURE A-176

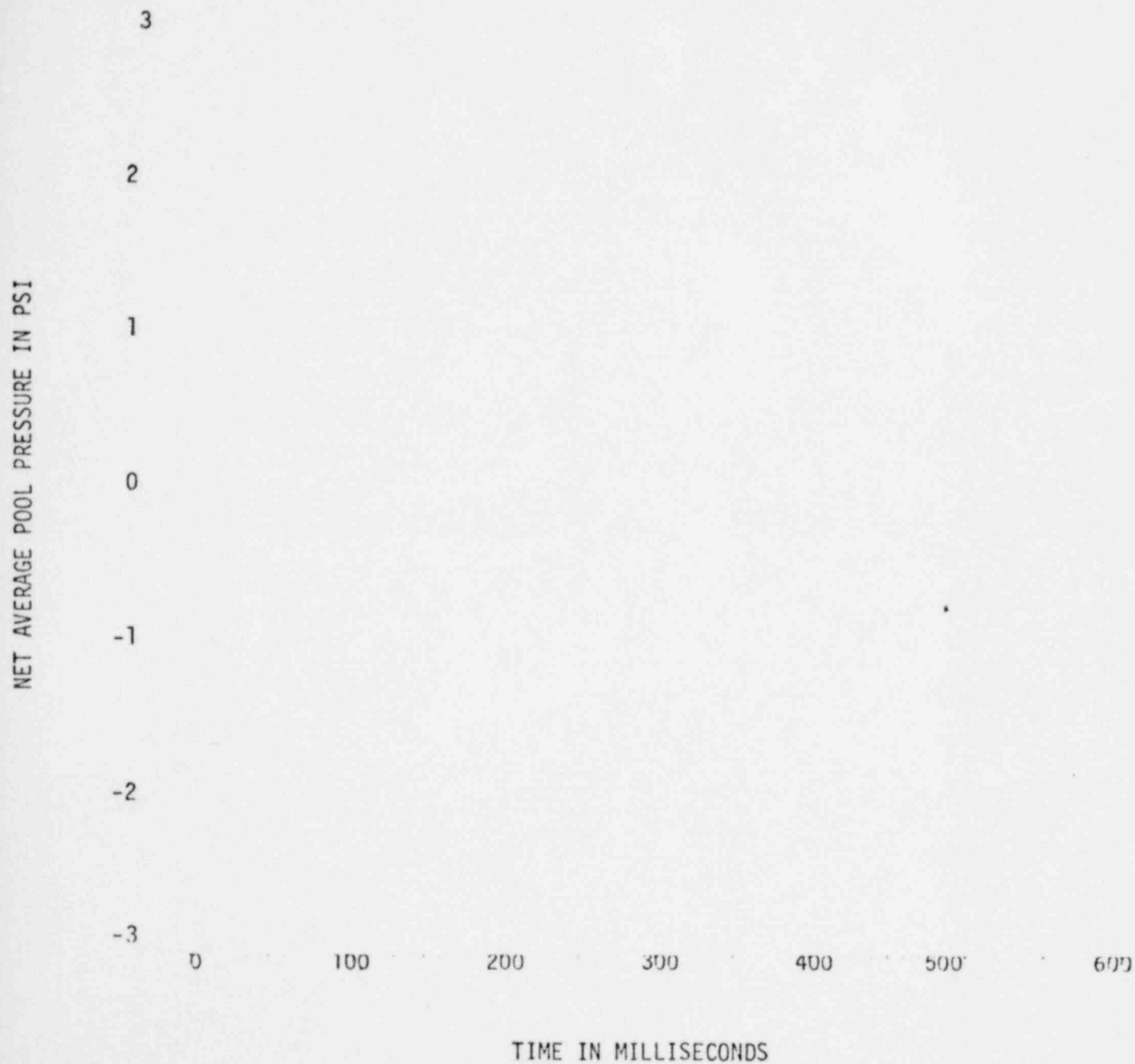
AVERAGE POOL PRESSURE, CORRECTED FOR WATER INERTIA

Task 5.5.3-2 Duane Arnold Test 5



NET AVERAGE POOL PRESSURE, CORRECTED FOR WATER INERTIA

Task 5.5.3-2 Duane Arnold Test 5



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FIGURE A-178

VENT HEADER IMPACT PRESSURES

Task 5.5.3-2 Duane Arnold Test 3

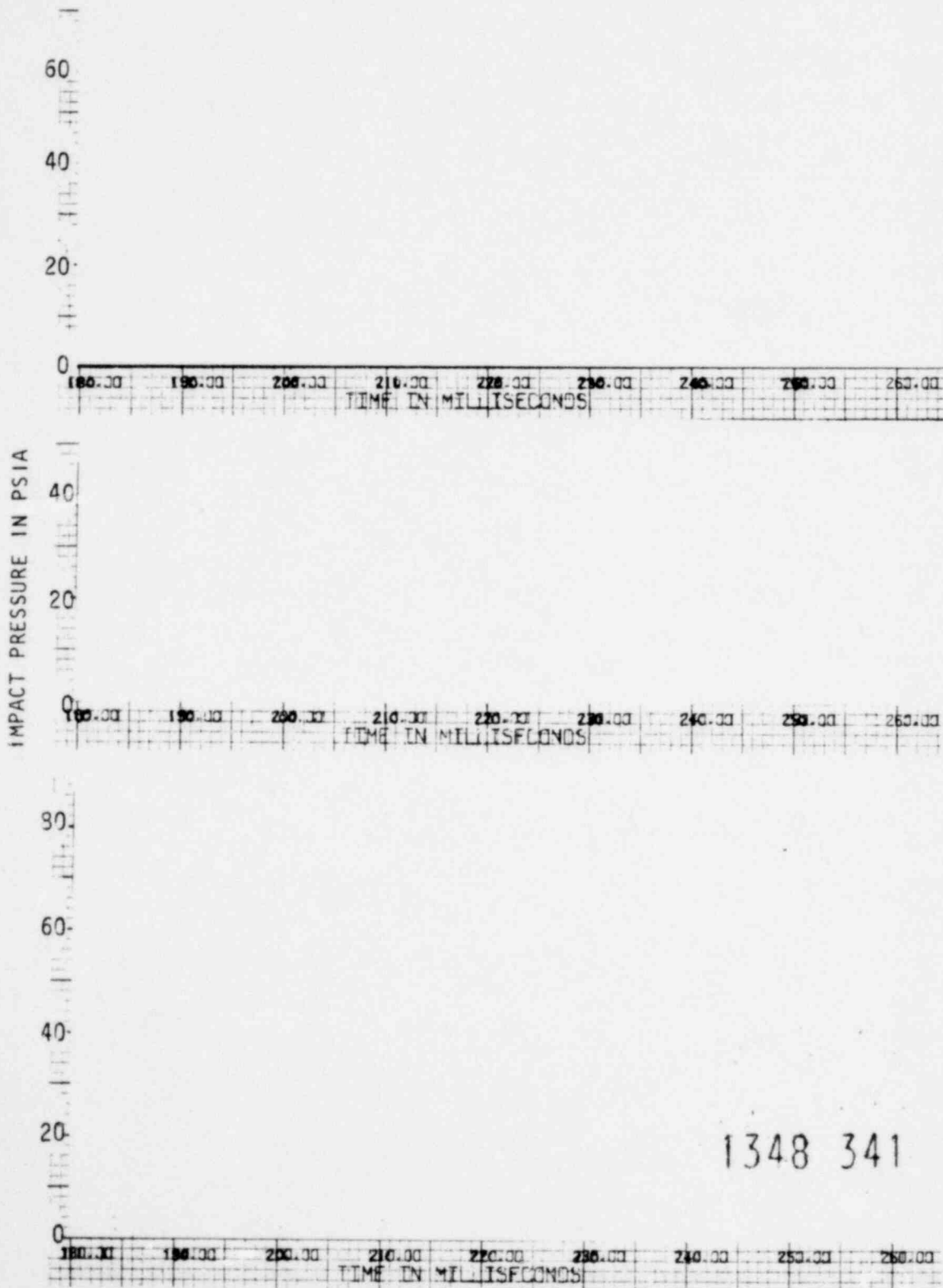
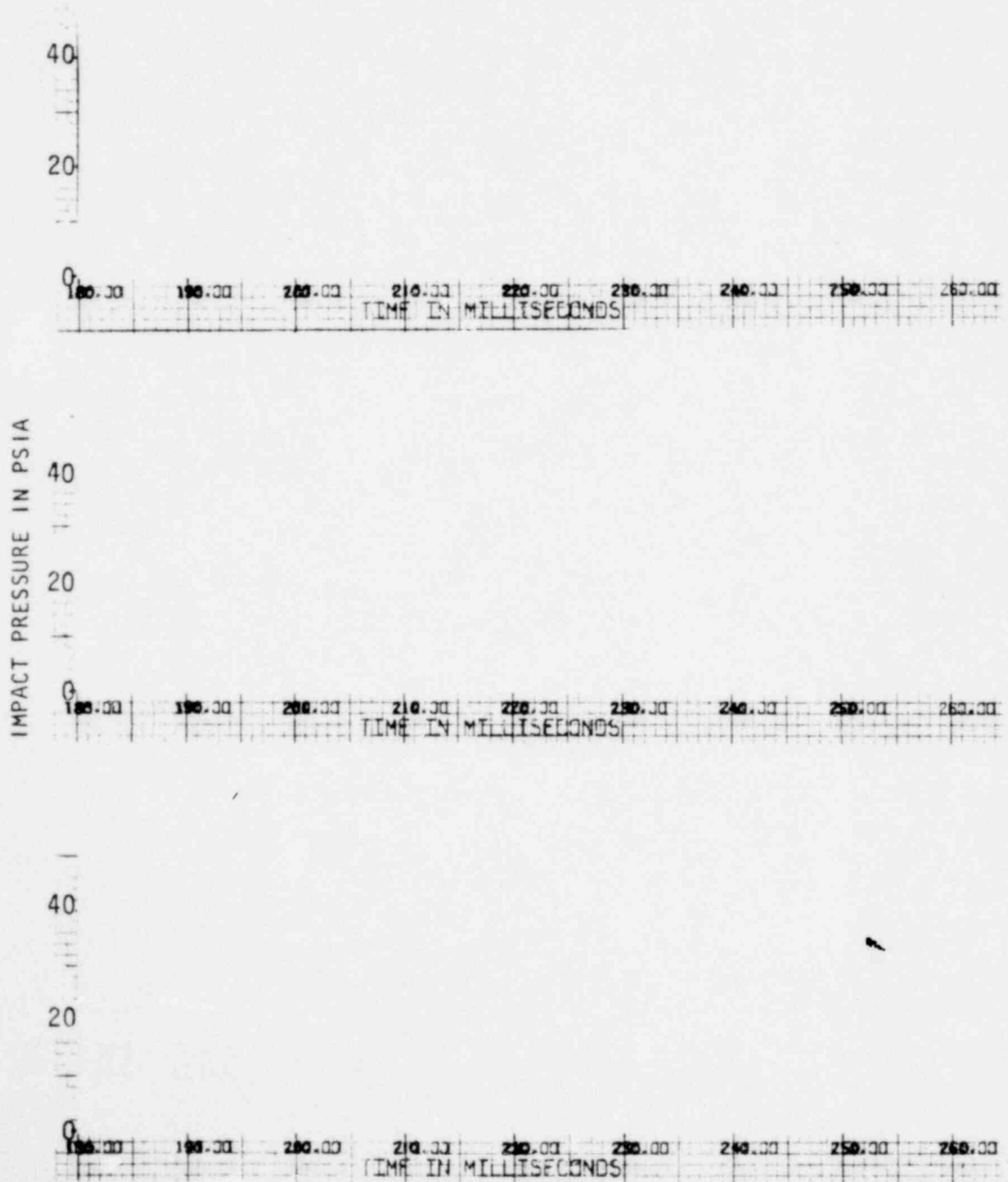


FIGURE A-179

VENT HEADER IMPACT PRESSURES

Task 5.5.3-2 Duane Arnold Test 3



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FIGURE A-180

VENT HEADER IMPACT PRESSURES

Task 5.5.3-2 Duane Arnold Test 3

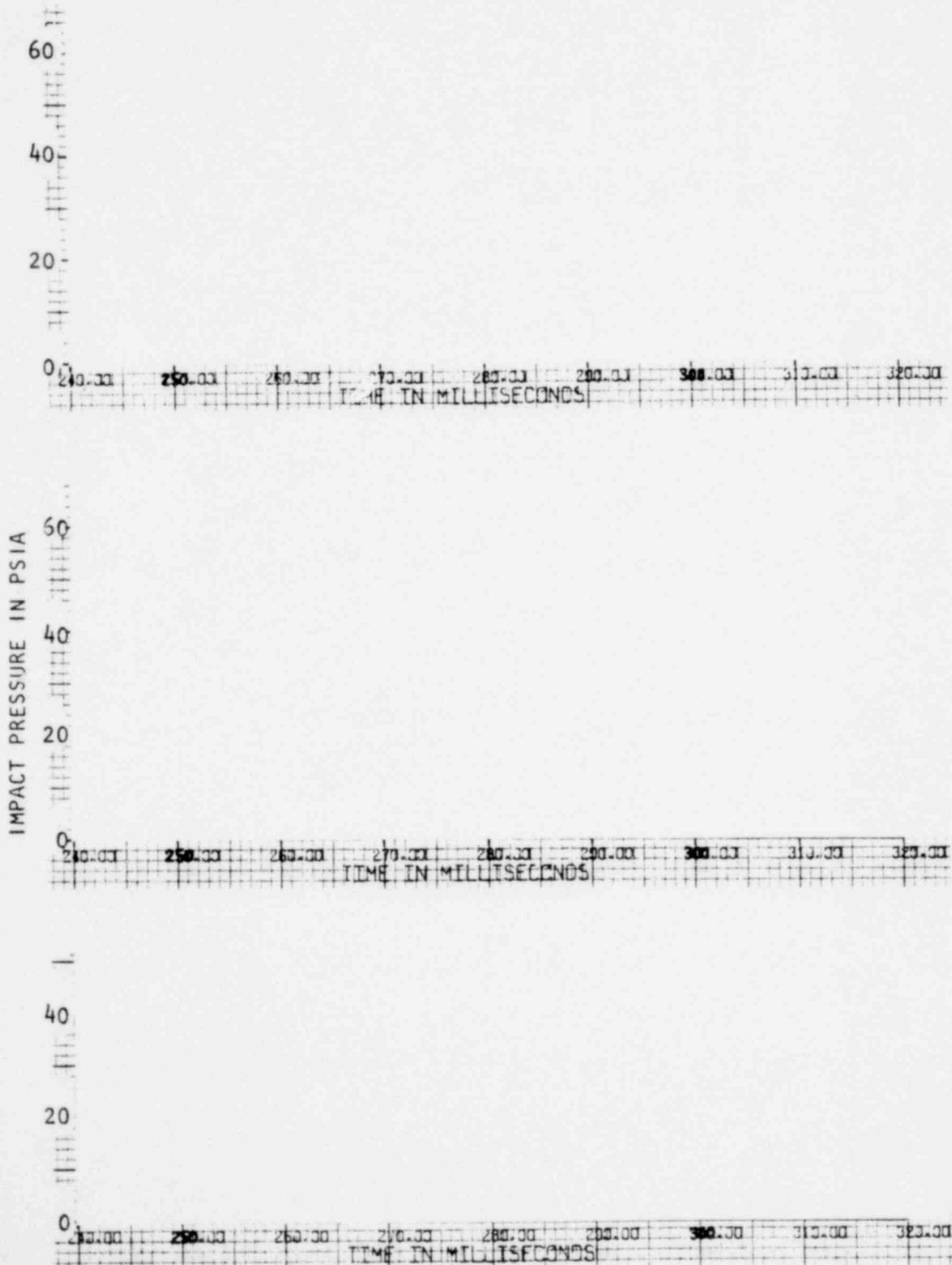


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FIGURE A-181

VENT HEADER IMPACT PRESSURES

Task 5.5.3-2 Duane Arnold Test 5

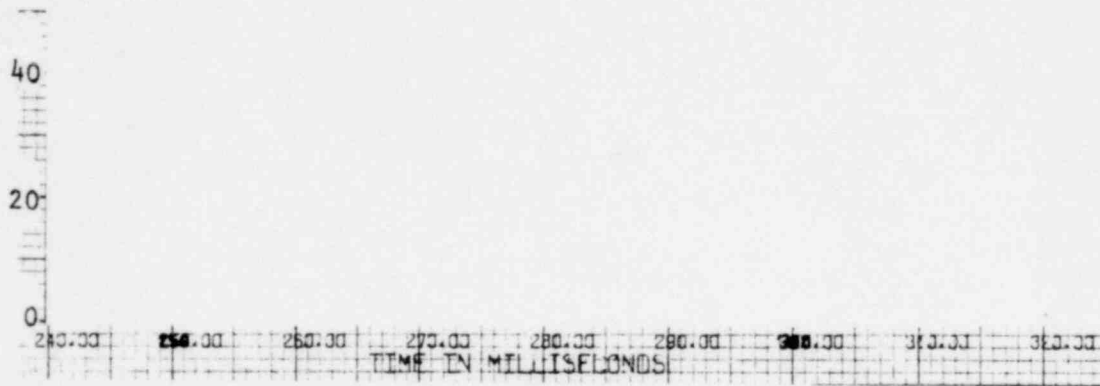


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FIGURE A-182

VENT HEADER IMPACT PRESSURES

Task 5.5.3-2 Duane Arnold Test 5



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FIGURE A-103

VENT HEADER IMPACT PRESSURES  
Task 5.5.3-2 Duane Arnold Test 5

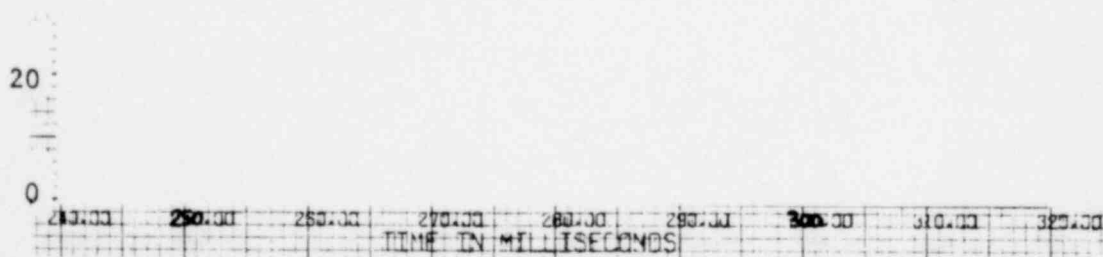
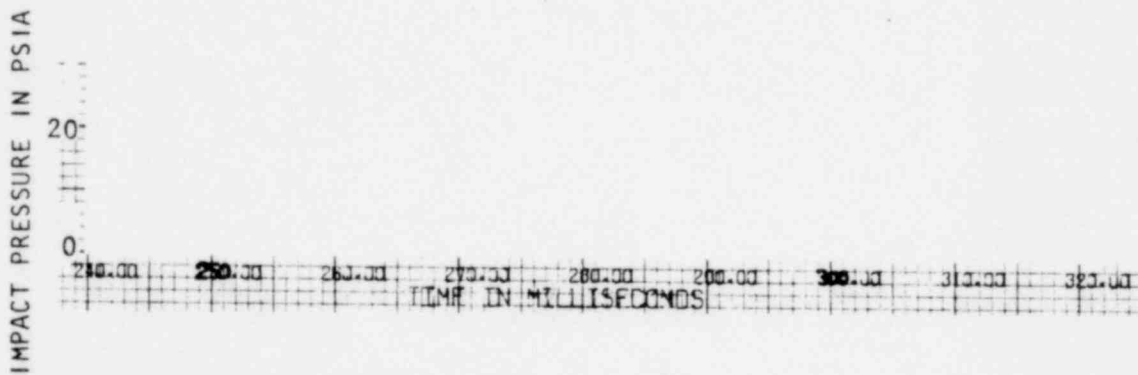
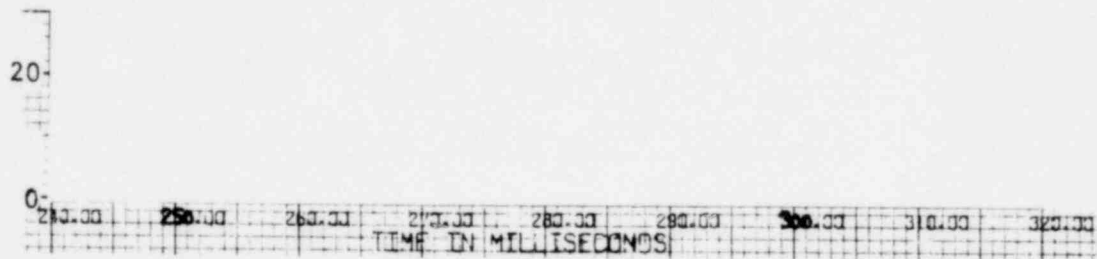
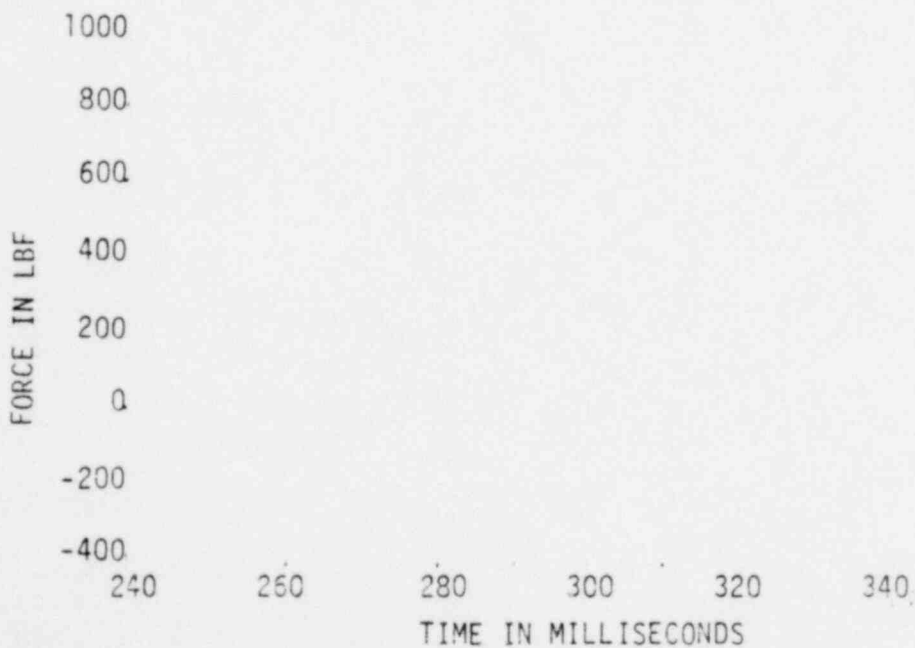
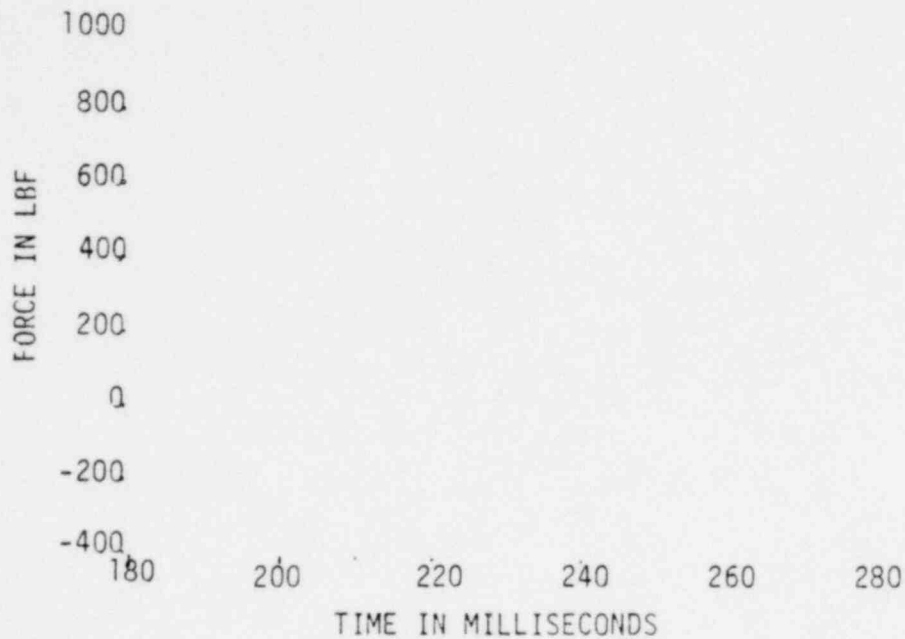


FIGURE A-184

COMPARISON OF VENT HEADER IMPACT RESULTS  
(Corrected Load Cell and Pressure Integration)  
Task 5.5.3 Duane Arnold Tests 3, 5



1348 347

FIGURE A-185

VENT HEADER VERTICAL ACCELERATION

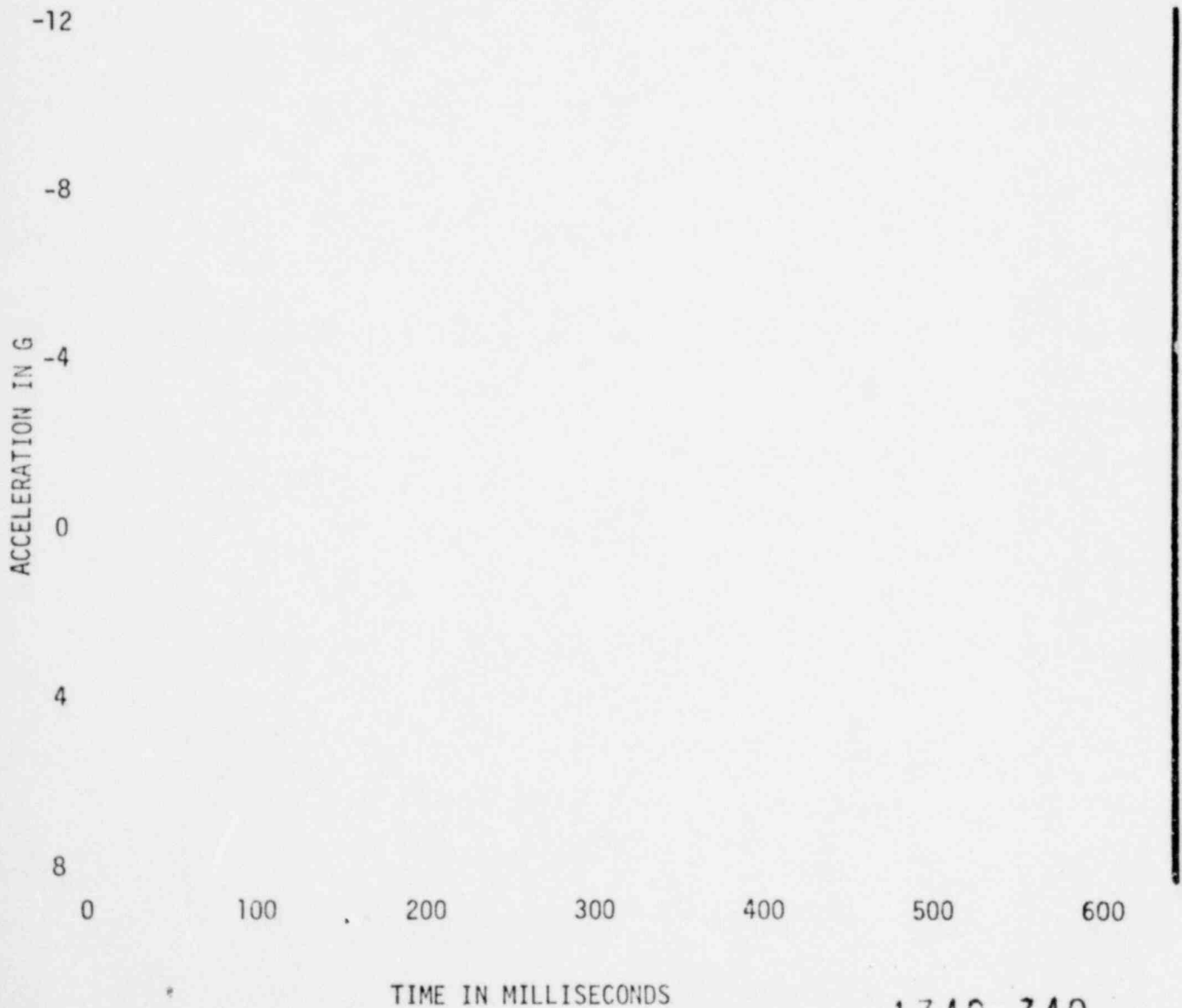
Task 5.5.3-2 Duane Arnold Test 3



FIGURE A-186

VENT HEADER VERTICAL ACCELERATION

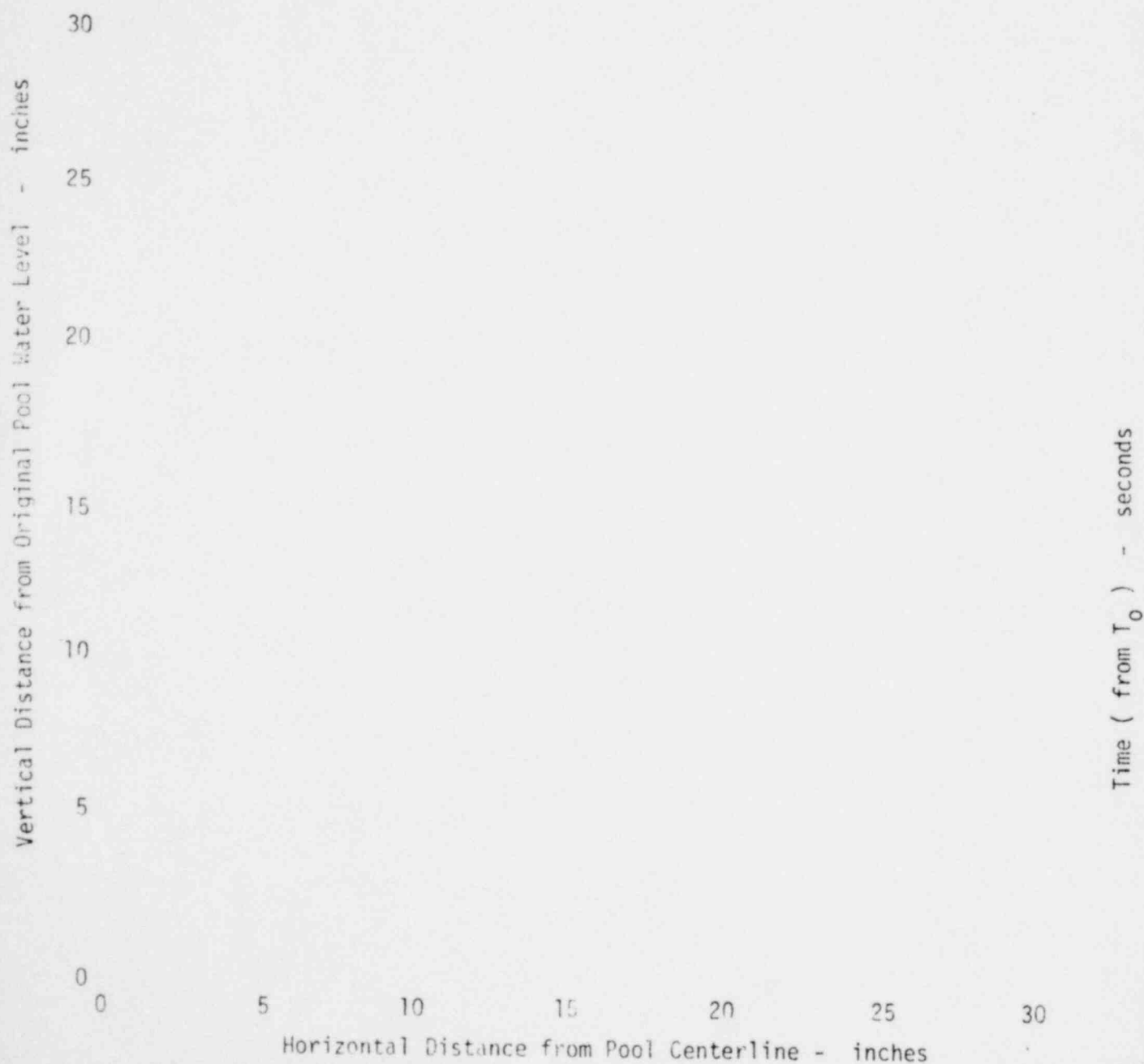
Task 5.5.3-2 Duane Arnold Test 5



1348 349

TIME HISTORY OF  
POOL DISPLACEMENT

DUANE ARNOLD, TEST 1



TIME HISTORY OF  
POOL DISPLACEMENT  
DUANE ARNOLD, TEST 2

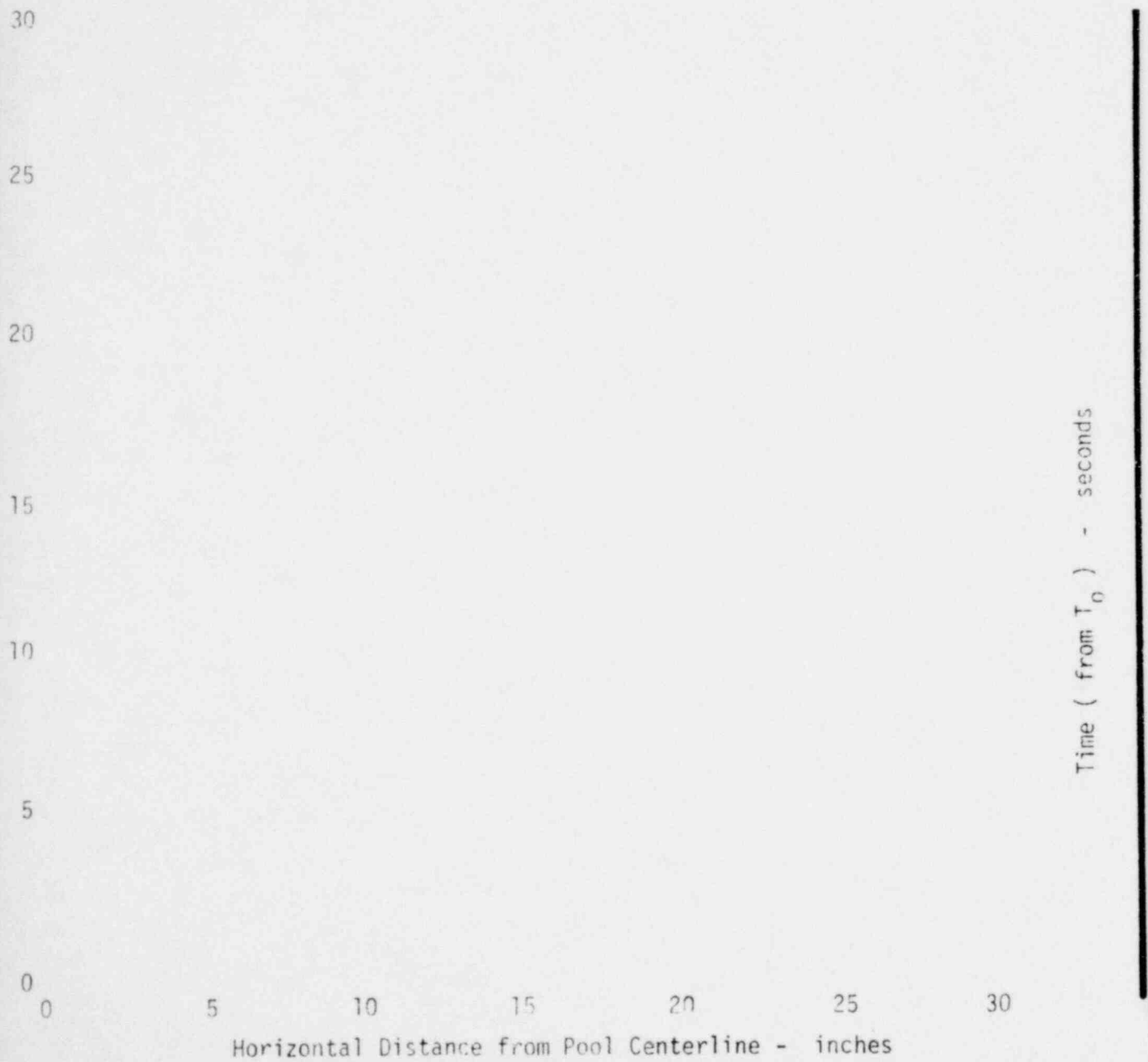
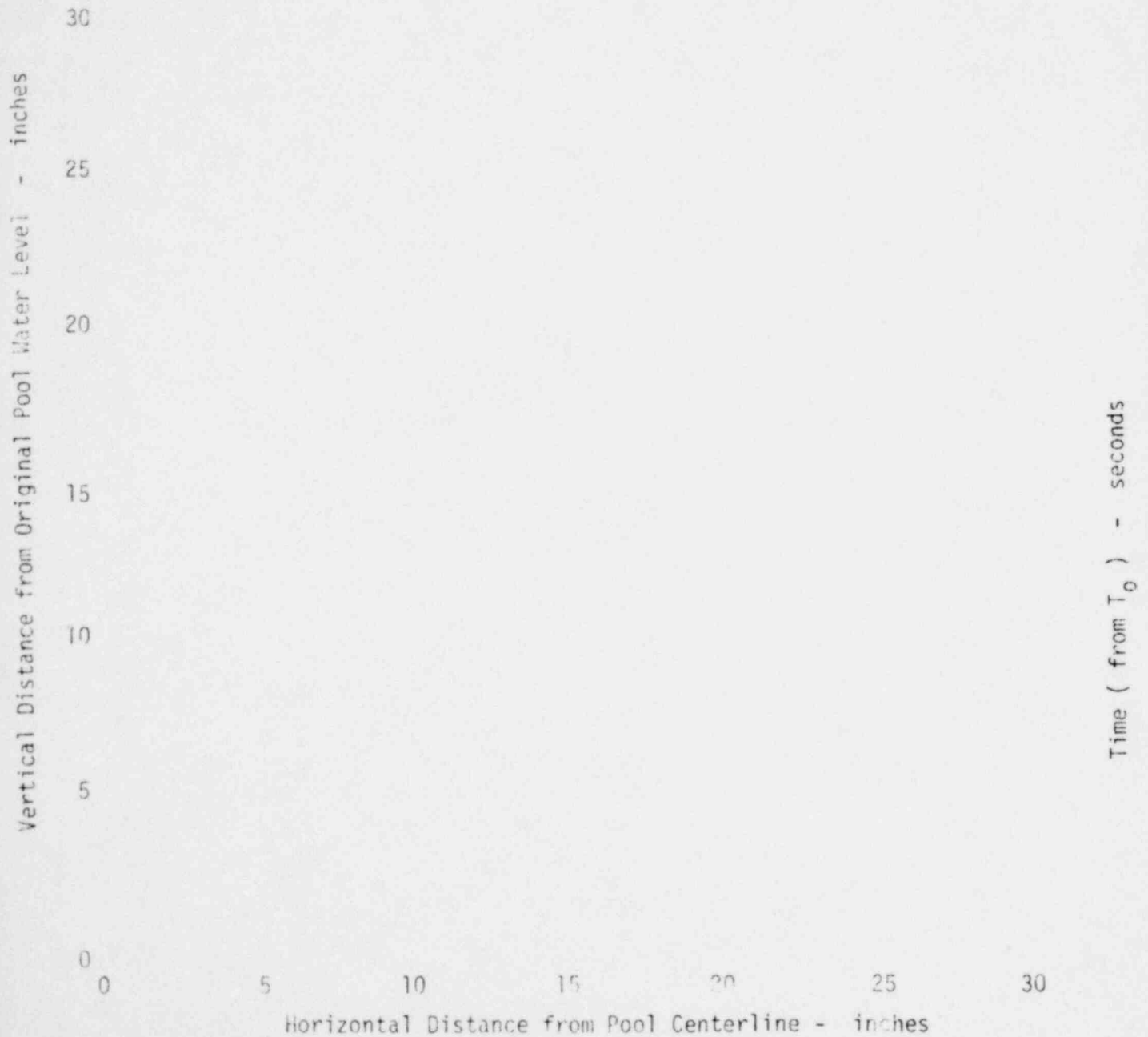


FIGURE A-189

TIME HISTORY OF  
POOL DISPLACEMENT

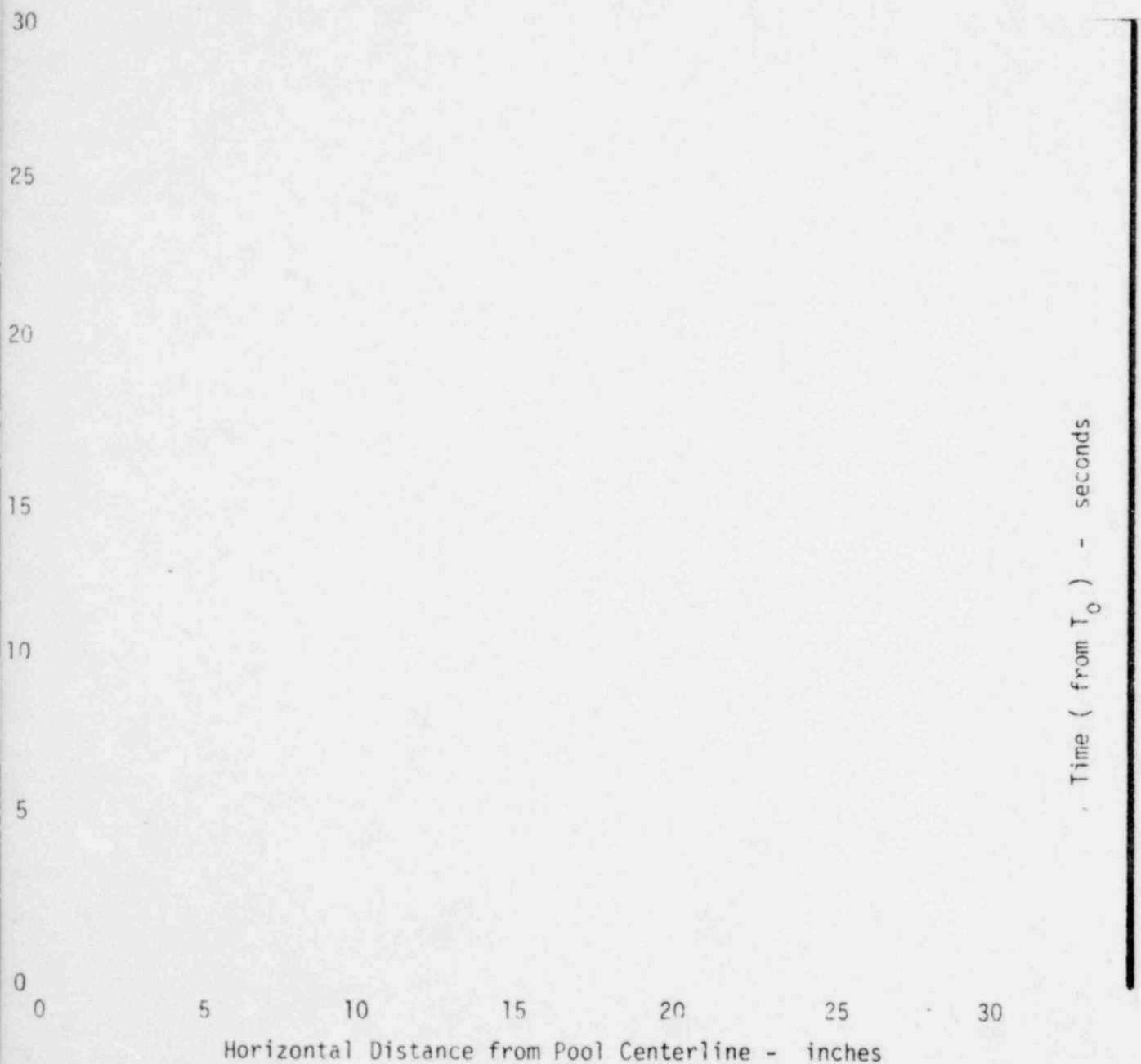
DUANE ARNOLD, TEST 3



NEDO-21944  
FIGURE A-190

TIME HISTORY OF  
POOL DISPLACEMENT

DUANE ARNOLD, TEST 5



1348 353

FIGURE A-191

POOL SURFACE DISPLACEMENT

DUANE ARNOLD, TESTS 1, 2, 3

Height - surface pool (au)iguo above original height  
A-220  
1348 354

100

200

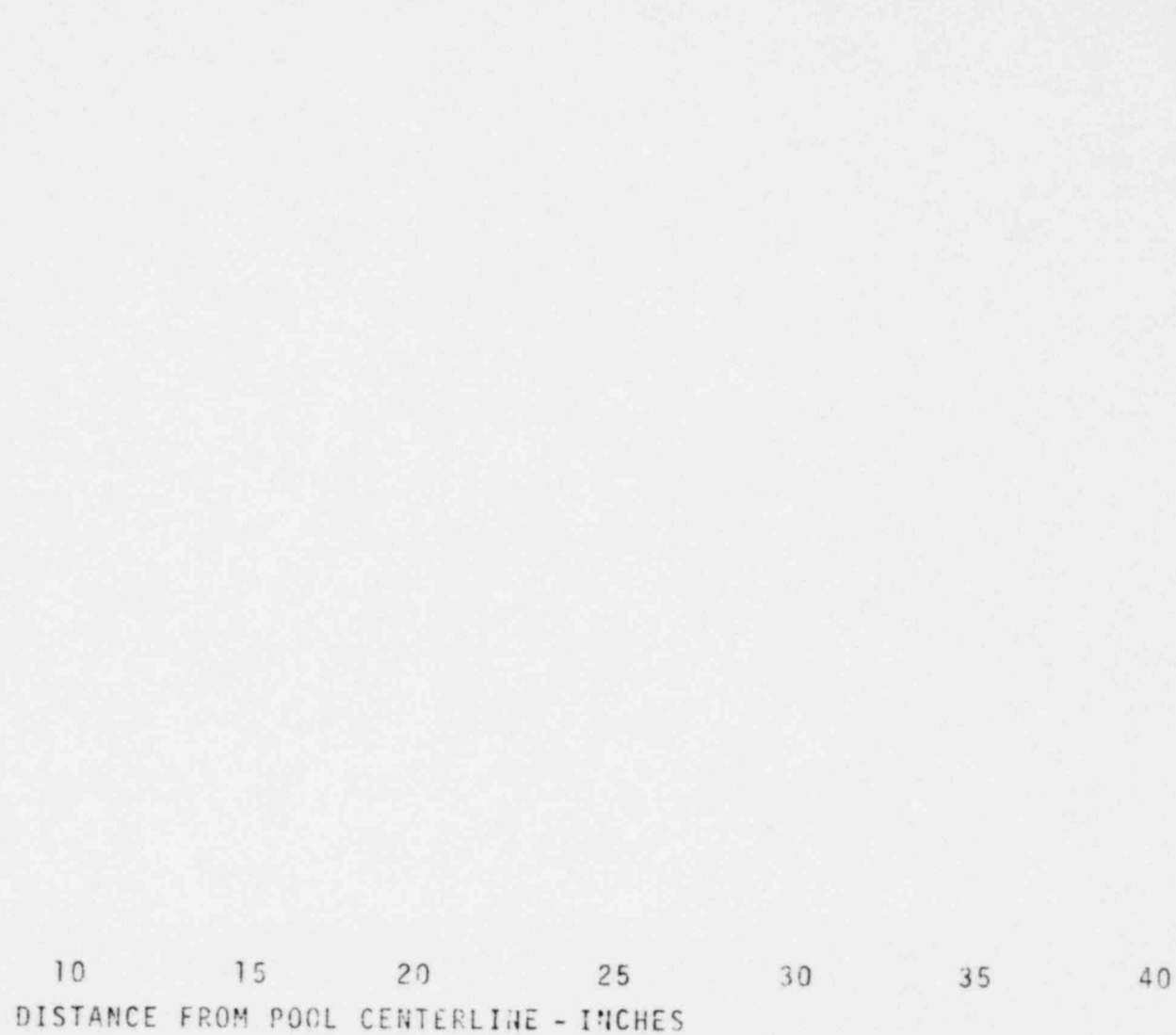
300  
Time - milliseconds

400

500

DUANE ARNOLD, TESTS 1, 2, 3

NUCLEAR SERVICES CORPORATION  
NEDO-21944



A-221

1348 355

FIGURE A-193

POOL SURFACE DISPLACEMENT

DUANE ARNOLD, TEST 5

20  
10  
0  
10  
20  
30  
40  
50  
60  
70  
80  
90  
100

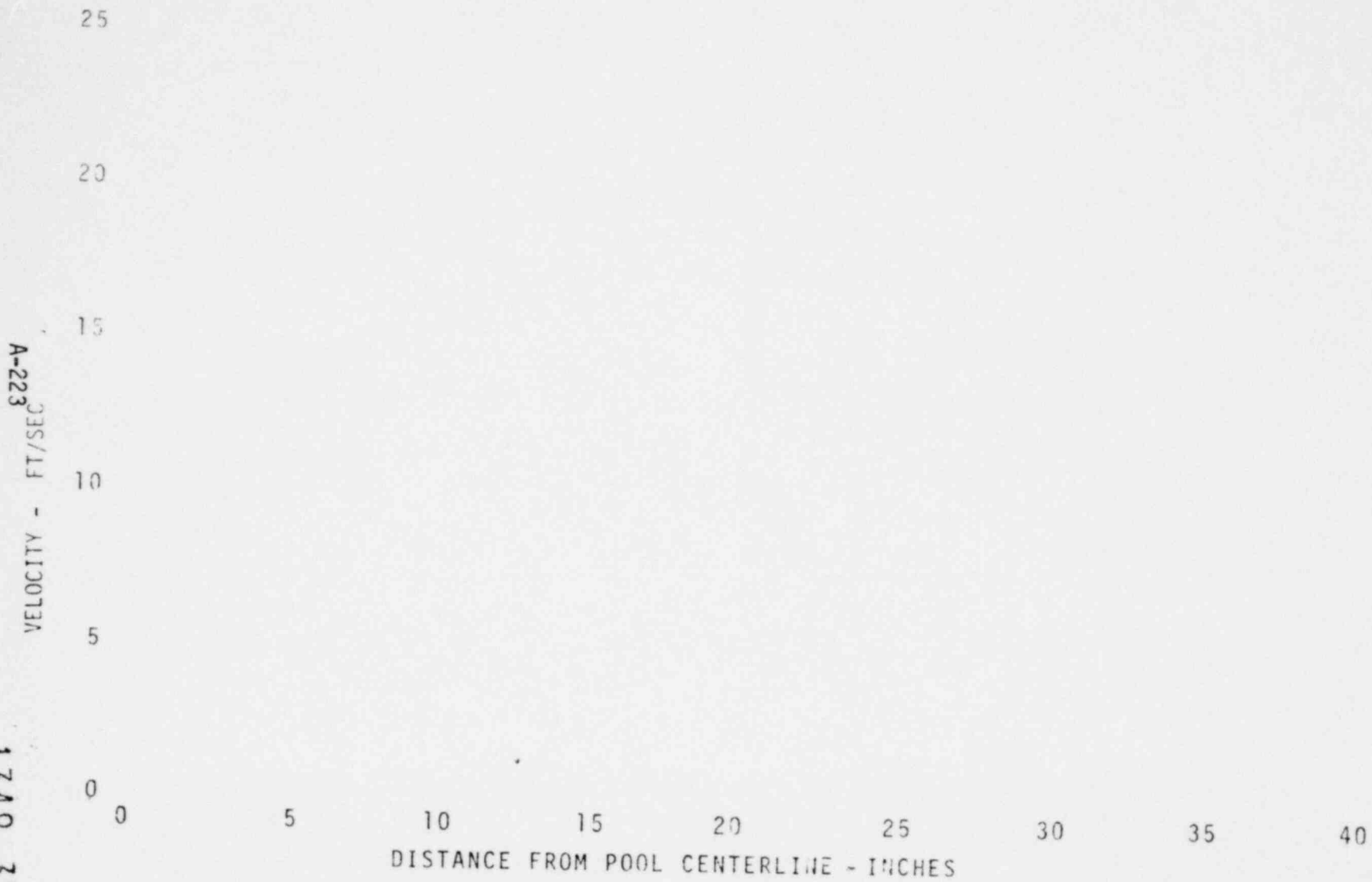
Vertical distance from pool level to top of tank

A-222

1348 356

DUANE ARNOLD, TEST 5

NEDO-21944  
NUCLEAR SERVICES CORPORATION



1348 357

FIGURE A-195

SIDE WINDOW DISPLACEMENT AND VELOCITY PROFILES

DUANE ARNOLD, TEST 4

VERTICAL DISPLACEMENT - INCHES

8

4

0

-4

-8

150

250

350

450

15.

10.

5.

0.

150

250

350

450

VERTICAL VELOCITY - FT/SEC

TIME - Seconds

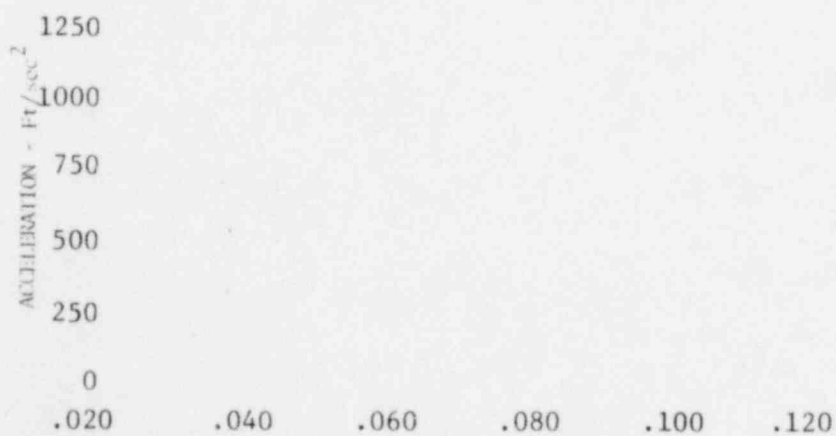
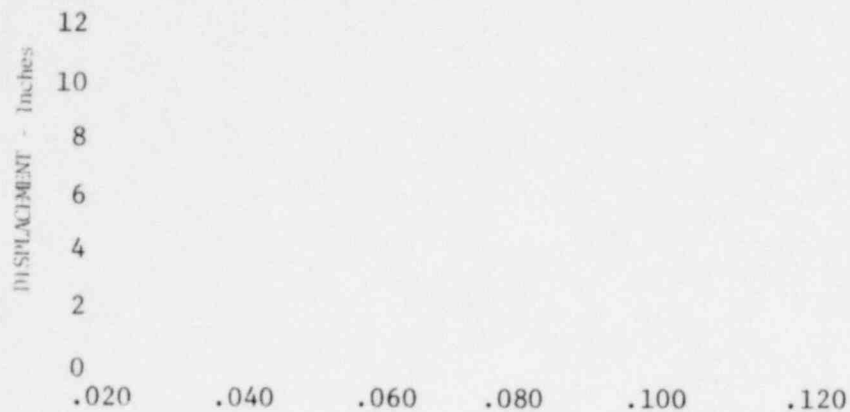
A-224

1348 358

NEDO-21944  
FIGURE A-196

DOWNCOMER WATER SLUG EJECTION

DUANE ARNOLD, TEST 3



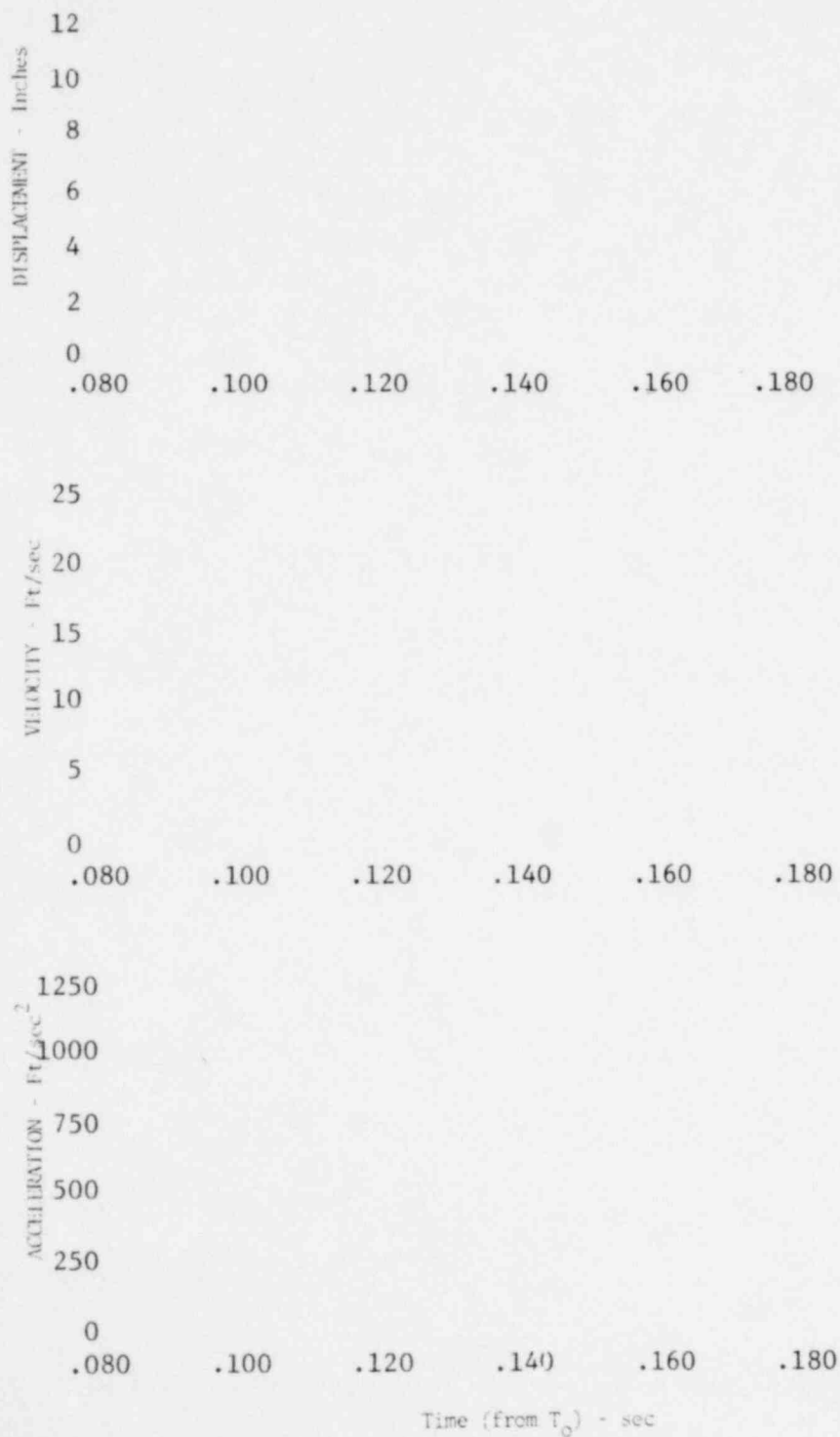
Time (from  $T_0$ ) - sec

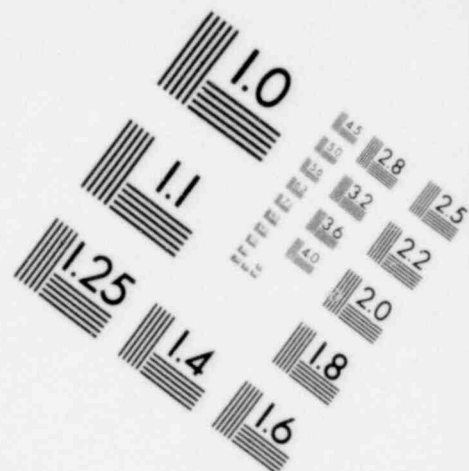
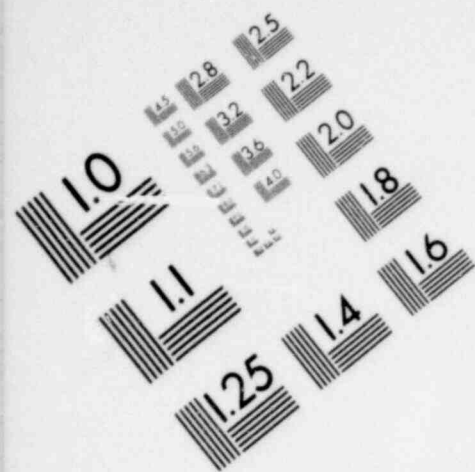
NEDO-21944

FIGURE A-197

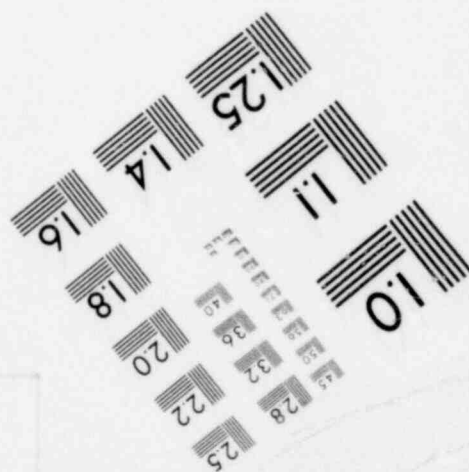
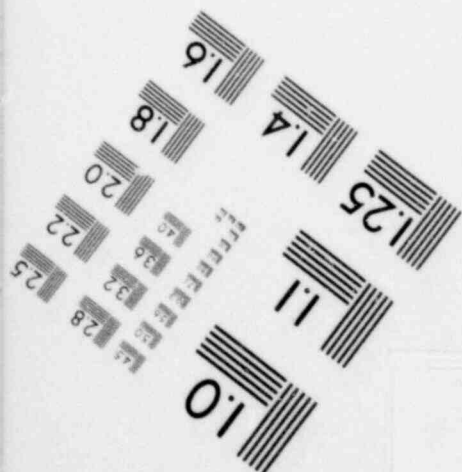
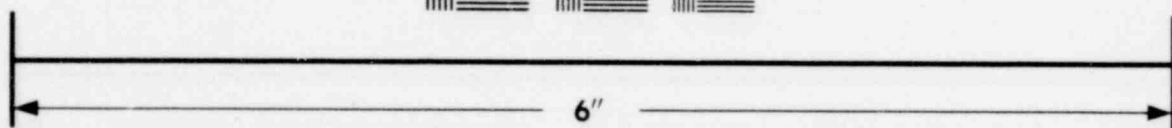
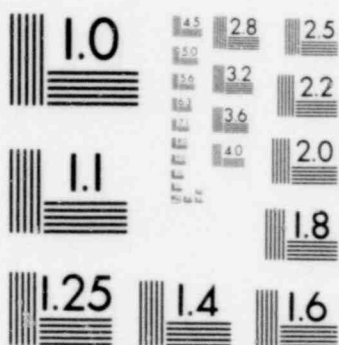
DOWNCOMER WATER SLUG EJECTION

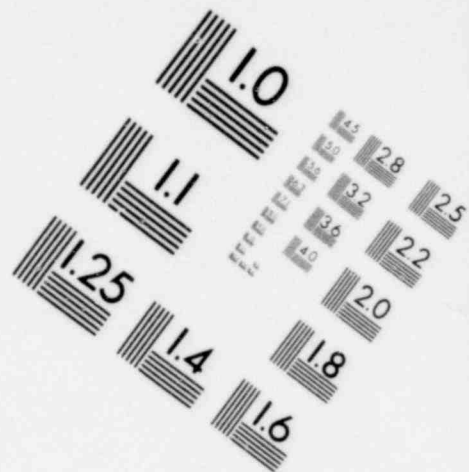
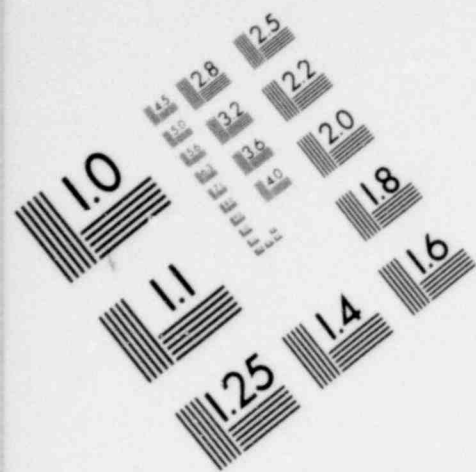
DUANE ARNOLD, TEST 5



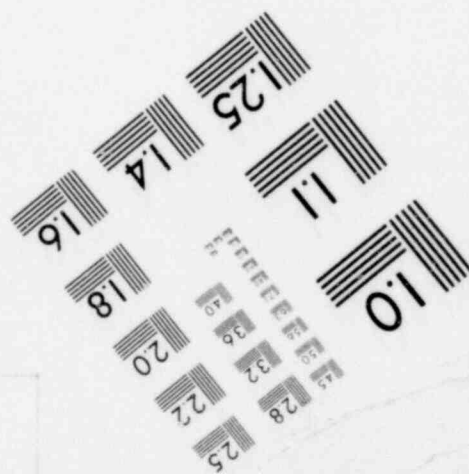
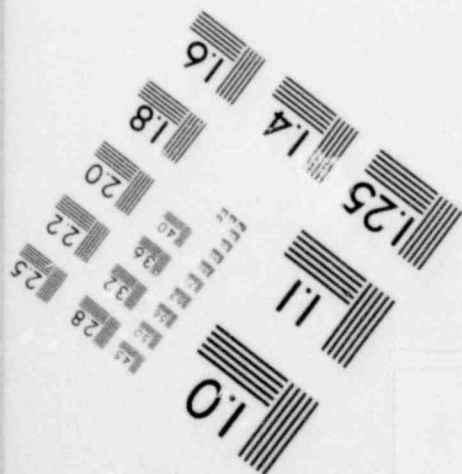
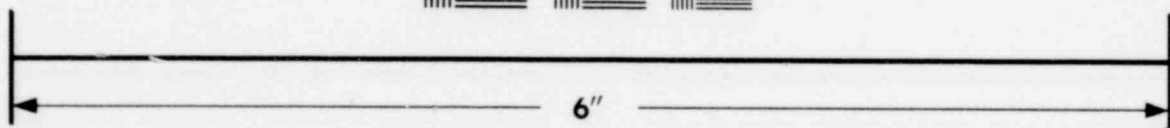
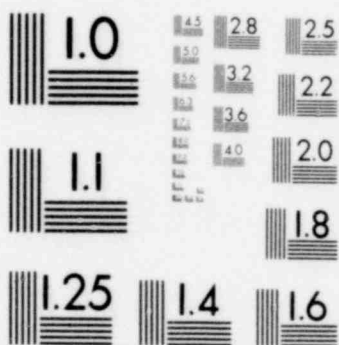


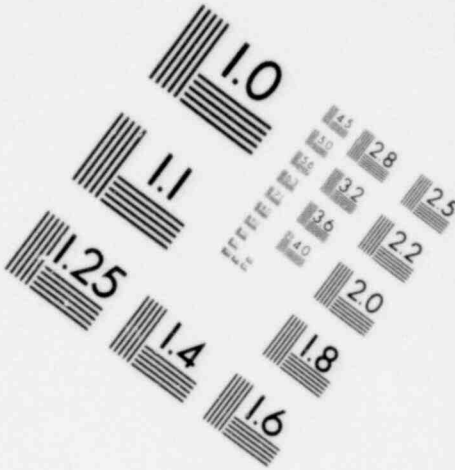
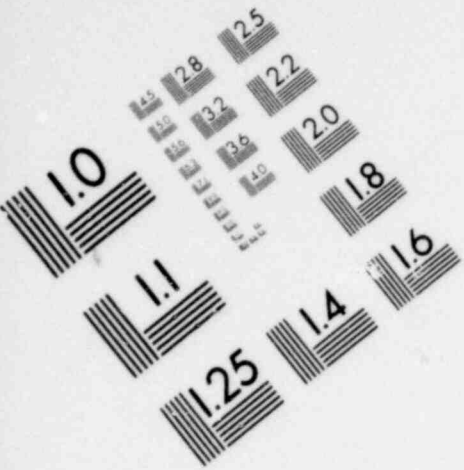
**IMAGE EVALUATION  
TEST TARGET (MT-3)**



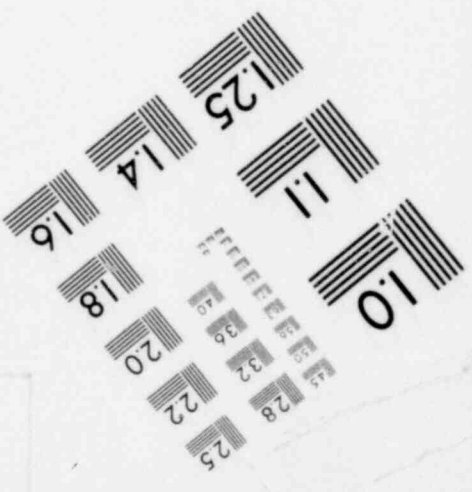
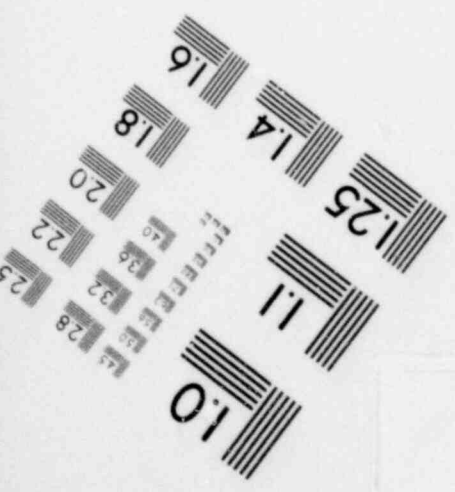
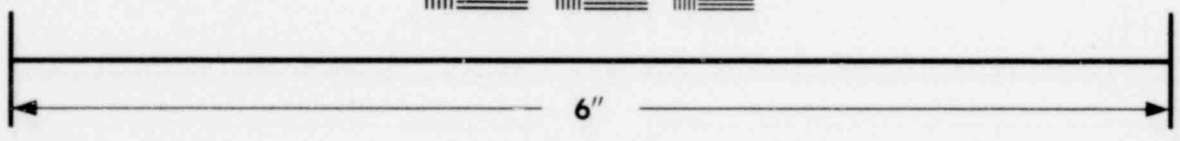
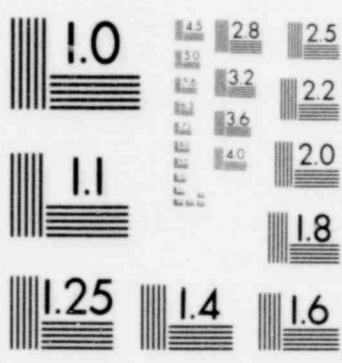


**IMAGE EVALUATION  
TEST TARGET (MT-3)**





**IMAGE EVALUATION  
TEST TARGET (MT-3)**



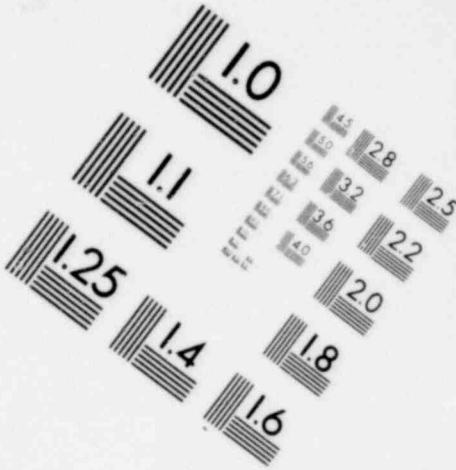
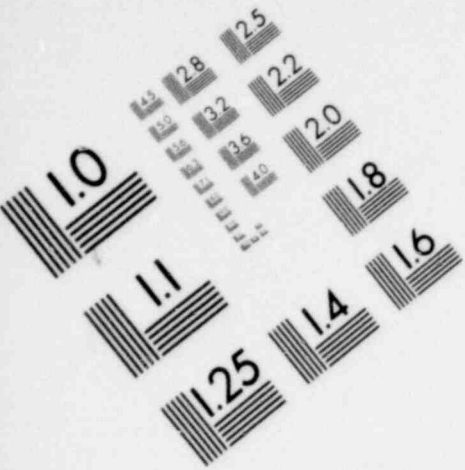
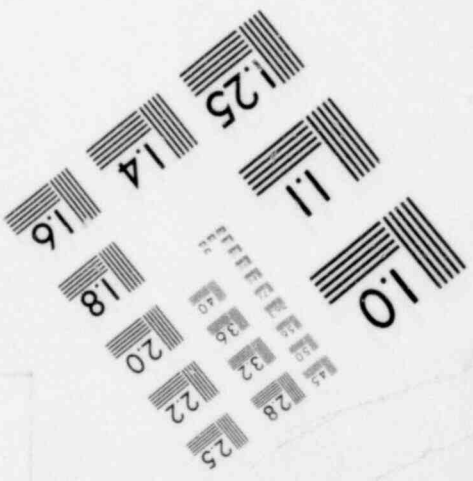
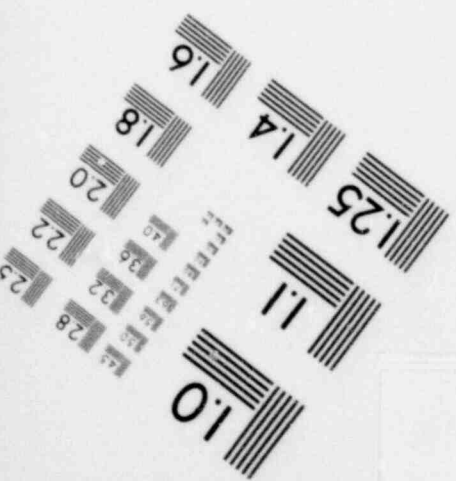
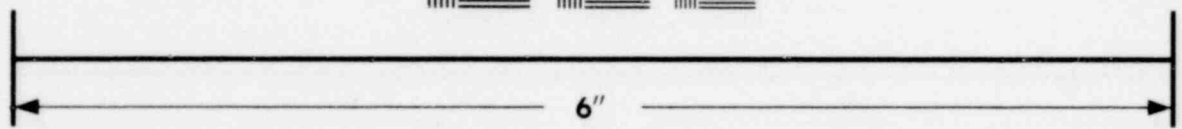
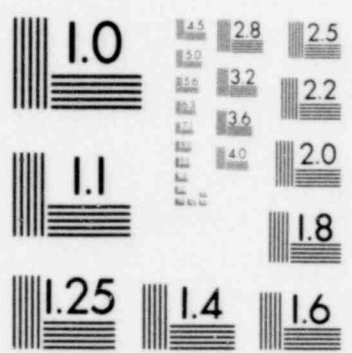


IMAGE EVALUATION  
TEST TARGET (MT-3)



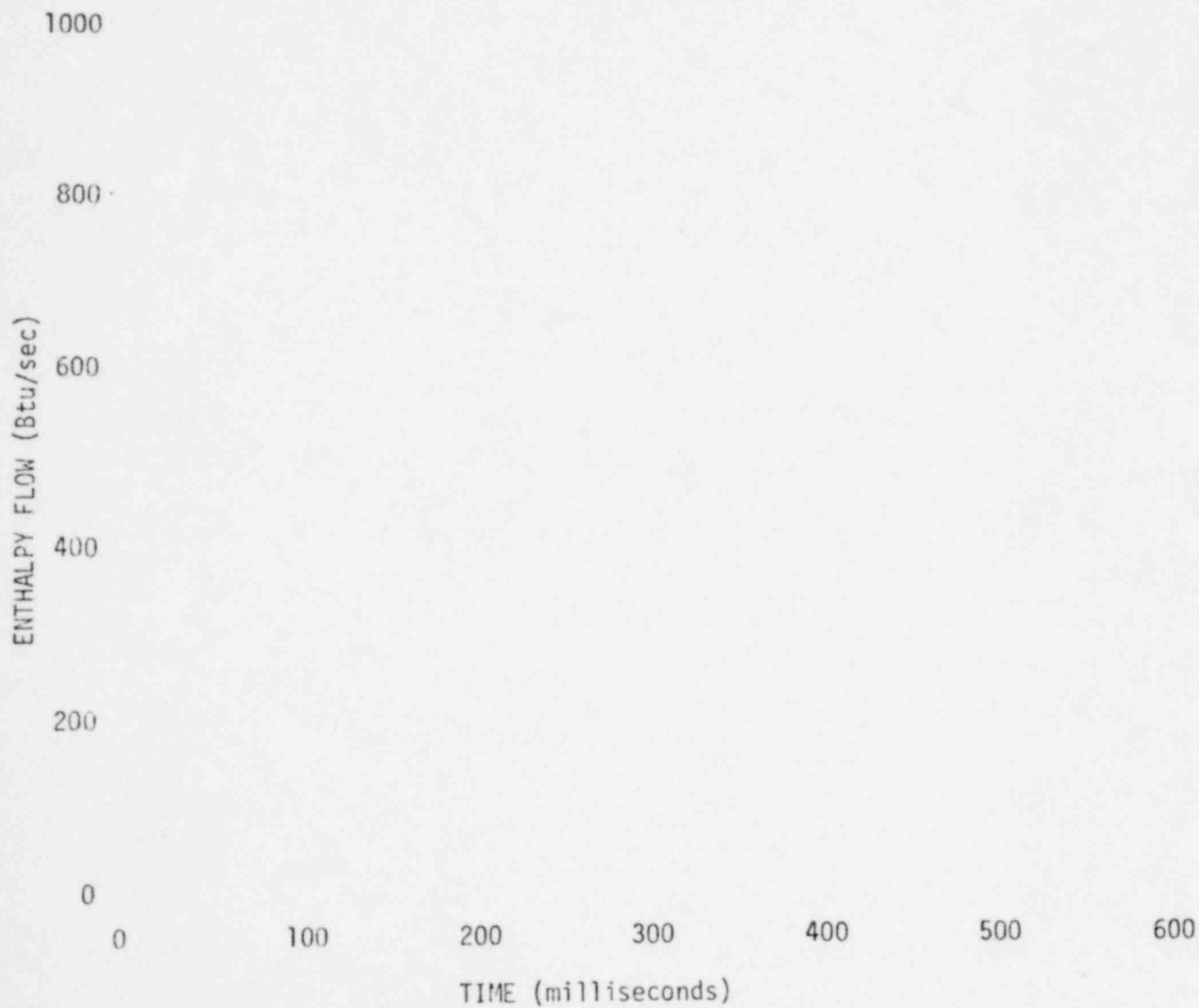
NEDO-21944

FIGURE A-198

EFFECT OF DRYWELL/WETWELL  $\Delta P$  ON

ENTHALPY FLOW INTO POOL

Duane Arnold Tests



1349 001

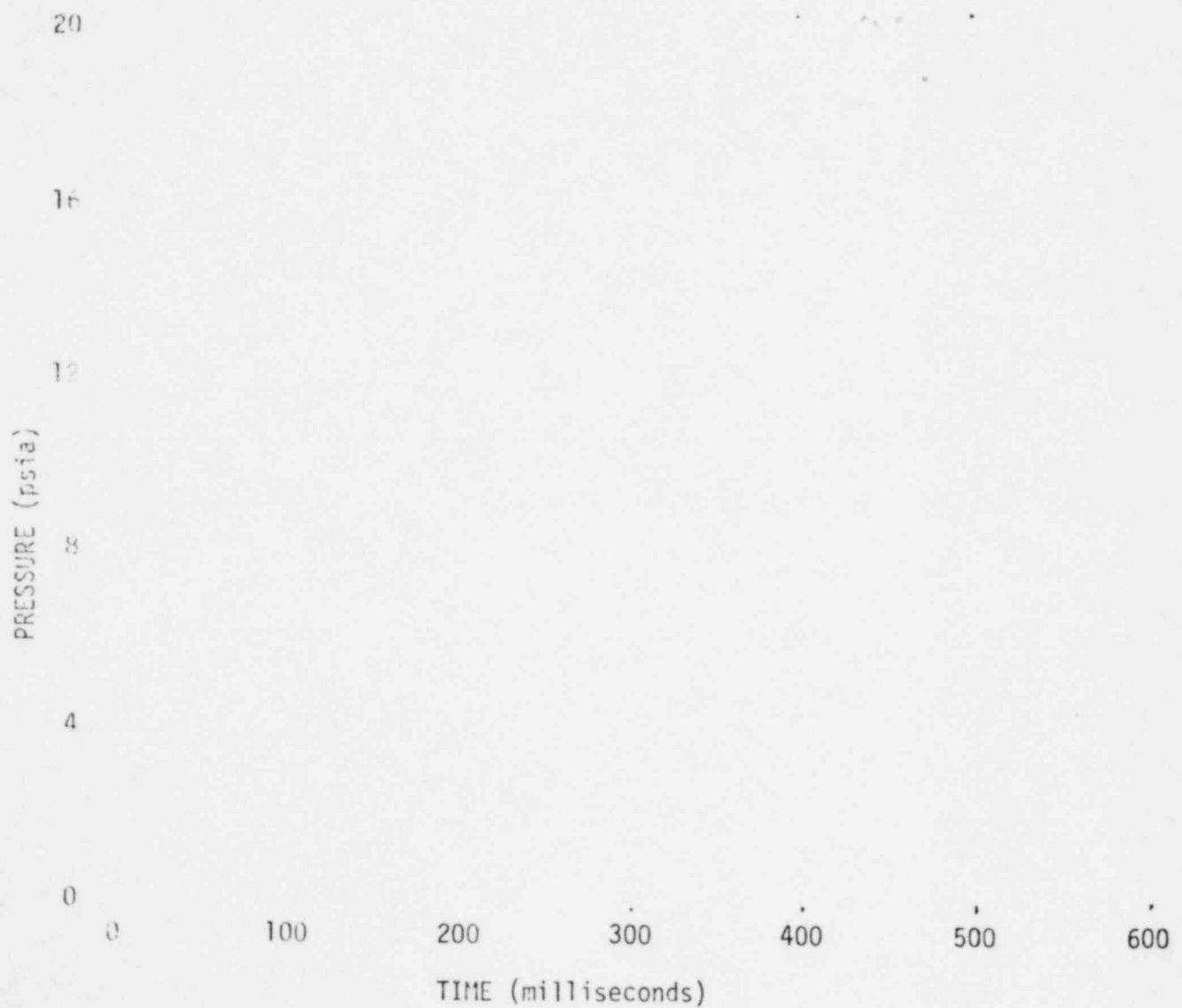
NEDO-21944

FIGURE A-199

EFFECT OF DRYWELL/WETWELL  $\Delta P$  ON

DOWNCOMER INTERNAL PRESSURE

Duane Arnold Tests



1349 002

FIGURE A-200

EFFECT OF DRYWELL/WETWELL  $\Delta P$  ON POOL PRESSURE

AT 180 DEGREE AND FREESPACE PRESSURE

Duane Arnold Tests



TABLE A-9  
DATA FOR WETWELL VERTICAL LOADS  
Task 5.5.3-2 Duane Arnold Tests

\*Vent clearing time (from  $T_0$ ) determined from the movie films.  
\*\*Time difference from  $T_0$  to time of zero downforce.  
- No significant downforce valley or 2nd peak downforce  
\*(1) Start-of-test reference time

Parameter	Test No.	9.19" $\Delta P$				Mean	Std. Dev.	0" $\Delta P$
		(1)	(2)	(3)	(4)			(5)
$T_0$ *(1)	(sec)							
Vent Clearing Time*	(sec)							
<u>Peak Downforce</u>								
Pressure Integral:								
Force	(lb)							
Time (from $T_0$ )	(sec)							
Corrected Pressure Integral:								
Force	(lb)							
Time (from $T_0$ )	(sec)							
Corrected Load Cell:								
Force	(lb)							
Time (from $T_0$ )	(sec)							
<u>Downforce Valley</u>								
Pressure Integral:								
Force	(lb)							
Time (from $T_0$ )	(sec)							
Corrected Pressure Integral:								
Force	(lb)							
Time (from $T_0$ )	(sec)							
Corrected Load Cell:								
Force	(lb)							
Time (from $T_0$ )	(sec)							
<u>2nd Peak Downforce</u>								
Pressure Integral:								
Force	(lb)							
Time (from $T_0$ )	(sec)							
Corrected Pressure Integral:								
Force	(lb)							
Time (from $T_0$ )	(sec)							
Corrected Load Cell:								
Force	(lb)							
Time (from $T_0$ )	(sec)							
<u>[<math>\Delta t</math>] Downforce Time**</u>								
Pressure Integral	(sec)							
Corrected Pressure Integral	(sec)							
Corrected Load Cell	(sec)							
<u>Downforce Impulse</u>								
Pressure Integral:								
Impulse	(lb-sec)							

TABLE A-9 (continued)

DATA FOR WETWELL VERTICAL LOADS (continued)

Task 5.5.3-2 Duane Arnold Tests

Parameter	Test No.	3.19" $\Delta P$				Std. Dev.	0" $\Delta P$
		(1)	(2)	(3)	(4)		(5)
<u>Peak Upforce</u>							
Pressure Integral:							
Force (lb)	(1b)						
Time (from $T_0$ ) (sec)	(sec)						
Corrected Pressure Integral:							
Force (lb)	(1b)						
Time (from $T_0$ ) (sec)	(sec)						
Corrected Load Cell:							
Force (lb)	(1b)						
Time (from $T_0$ ) (sec)	(sec)						
<u>Upforce Valley</u>							
Pressure Integral:							
Force (lb)	(1b)						
Time (from $T_0$ ) (sec)	(sec)						
Corrected Pressure Integral:							
Force (lb)	(1b)						
Time (from $T_0$ ) (sec)	(sec)						
Corrected Load Cell:							
Force (lb)	(1b)						
Time (from $T_0$ ) (sec)	(sec)						
<u>2nd Peak Upforce</u>							
Pressure Integral:							
Force (lb)	(1b)						
Time (from $T_0$ ) (sec)	(sec)						
Corrected Pressure Integral:							
Force (lb)	(1b)						
Time (from $T_0$ ) (sec)	(sec)						
Corrected Load Cell:							
Force (lb)	(1b)						
Time (from $T_0$ ) (sec)	(sec)						
<u>Zero Force Time*</u>							
Pressure Integral (sec)	(sec)						
Corrected Pressure Integral (sec)	(sec)						
Corrected Load Cell (sec)	(sec)						

1349 005

TABLE A-10

DATA FOR VENT R IMPACT LOADS

Task 5.5.3-2 Duane Arnold Tests

Parameter \ Test No.	9.19" $\Delta P$				Mean	Std. Dev.	0" $\Delta P$
	( 1 )	( 2 )	( 3 )	( 4 )			( 5 )
$T_0$ + (sec)							
Vent Header Impact							
Pressure Integral:							
Maximum Force (lb)							
Impulse (lb-sec)							
Duration* (sec)							
Load Cell Corrected: ++							
Maximum Force (lb)							
Impulse (lb-sec)							
Duration (sec)							
Pool Surface Velocity (ft/sec)							
Time (from $T_0$ )** (sec)							

\*(2) Offset 6" from pool centerline

\* Based on impact pressure measurements

\*\* At start of the first impact pressure recorded

+ Start of reference time

++represents peak of very noisy data (acceleration corrected); mean value would be lower

1349 006

## A.5 Nine Mile Point Tests

### A.5.1 Typical Data

Time-history plots of the driving conditions and pool response are presented in this section for Nine Mile Point Tests 3 and 5.

Test 3 was a load definition test which was conducted at a partial drywell/wetwell differential pressure of 7.94"  $\Delta P$  and with a 4.59 inch pipe deflector (16 inch full scale). Test 5 was conducted without an initial drywell/wetwell differential pressure (0"  $\Delta P$ ) and with the same 4.59 inch pipe deflector.

#### A.5.1.1 Driving Conditions

Driving conditions for Nine Mile Point Test 3 are presented in Figures A-201 through A-205. Similar plots for Nine Mile Point Test 5 are shown in Figures A-206 through A-210. Nine Mile Point's driving conditions had the same characteristics as the "typical" plant discussed in Section 3.0 of this report.

It can be seen that the downcomer orifice upstream temperature starts to drop at about 200 milliseconds in Figure A-204 and about 185 milliseconds in Figure A-209. This is the result of the condensate, which formed in the drywell during the pretest pump-down period, dripping into the downcomer and wetting the thermocouple. The corrected vent air temperature, which was based on the normal temperature runs, is shown by dash line (Figures A-204 and A-209). Correction of the air temperature on enthalpy flow into pool is negligibly small. Before the last series of the plant unique tests were conducted (August to October 1978), the thermocouple was moved up into the vent header and near the downcomer inlet. This resulted in good vent air temperature measurement.

1349 007

#### A.5.1.2 Pool Response

Downcomer internal pressure and wetwell pressures for Nine Mile Point Tests 3 and 5 are presented in Figures A-211 through A-212 and A-213 through A-214, respectively. Several spikes can be observed in one of the freespace pressures at about 400 and 565 milliseconds (Figure A-212). These spikes were caused by water splashing on the transducer, which is mounted on the top of the torus (airspace).

Figures A-215 and A-216 present net torus force based on the torus pressure integral for Nine Mile Point Tests 3 and 5, respectively. Some downforce oscillations are present, but they dampen out rapidly after the first oscillation. During the Nine Mile Point Test 3, one of the two freespace pressure transducers was splashed with water. When the outputs of both the freespace transducers are used with the pool transducer outputs to obtain net torus force, an erroneous force peak is produced at the time splashing occurs. When only that transducer which was not splashed is used to obtain net torus force, a much smoother and more accurate force-time history is obtained (Figure A-215).

The net torus force which was determined by applying the inertial correction from the torus accelerometer (Figures A-218 and A-220) to the torus load cell (Figures A-217 and A-219) is compared with the torus force obtained from the torus pressure integral in Figures A-221 and A-222. Residual oscillations are present in the corrected load cell. Figures A-223 and A-224 present the net torus force based on the torus pressure integral corrected for inertia.

The "average" pool pressures for Nine Mile Point Tests 3 and 5 are shown in Figures A-225 and A-227. Figures A-226 and A-228 are the same as Figures A-223 and A-224 with force replaced by average pressure (force/torus projected area).

1349 008

The vent header impact pressures for Nine Mile Point Test 3 are presented in Figures A-229 through A-232. Vent header pressures for Nine Mile Point Test 5 are presented in Figures A-233 through A-236. These figures indicate that the deflector was effective in reducing the peak local vent header impact pressure.

Figure A-237 presents a comparison of the vent header impact force derived from the pressure integral with that derived from the corrected load cell. Vent header vertical accelerations from Tests 3 and 5 are shown in Figures A-238 and A-239, respectively.

#### A.5.2 Pool Dynamics

The pool contours at various times of pool swell are shown in Figures A-240 through A-243 for Nine Mile Point Tests 1, 2, 3, and 5.

The pool surface displacement curves for Tests 1, 2, and 3 are shown on Figure A-244. The pool surface velocities for Tests 1, 2, and 3 are shown on Figure A-245. The pool surface displacement graph and pool surface velocity profiles for Test 5 are shown in Figures A-246 and A-247, respectively.

The pool surface displacements and velocity profile viewed from the side window during Test 4 are shown in Figure A-248. The downcomer water slug displacement, velocity, and acceleration versus time for Tests 3 and 5 are presented in Figures A-249 and 250.

#### A.5.3 Data Summaries

Table A-11 presents the Nine Mile Point Test Data for wetwell vertical forces.

Table A-12 presents the Nine Mile Point test data for vent header impact forces.

1349 009

#### A.5.4 Discussion and Analysis

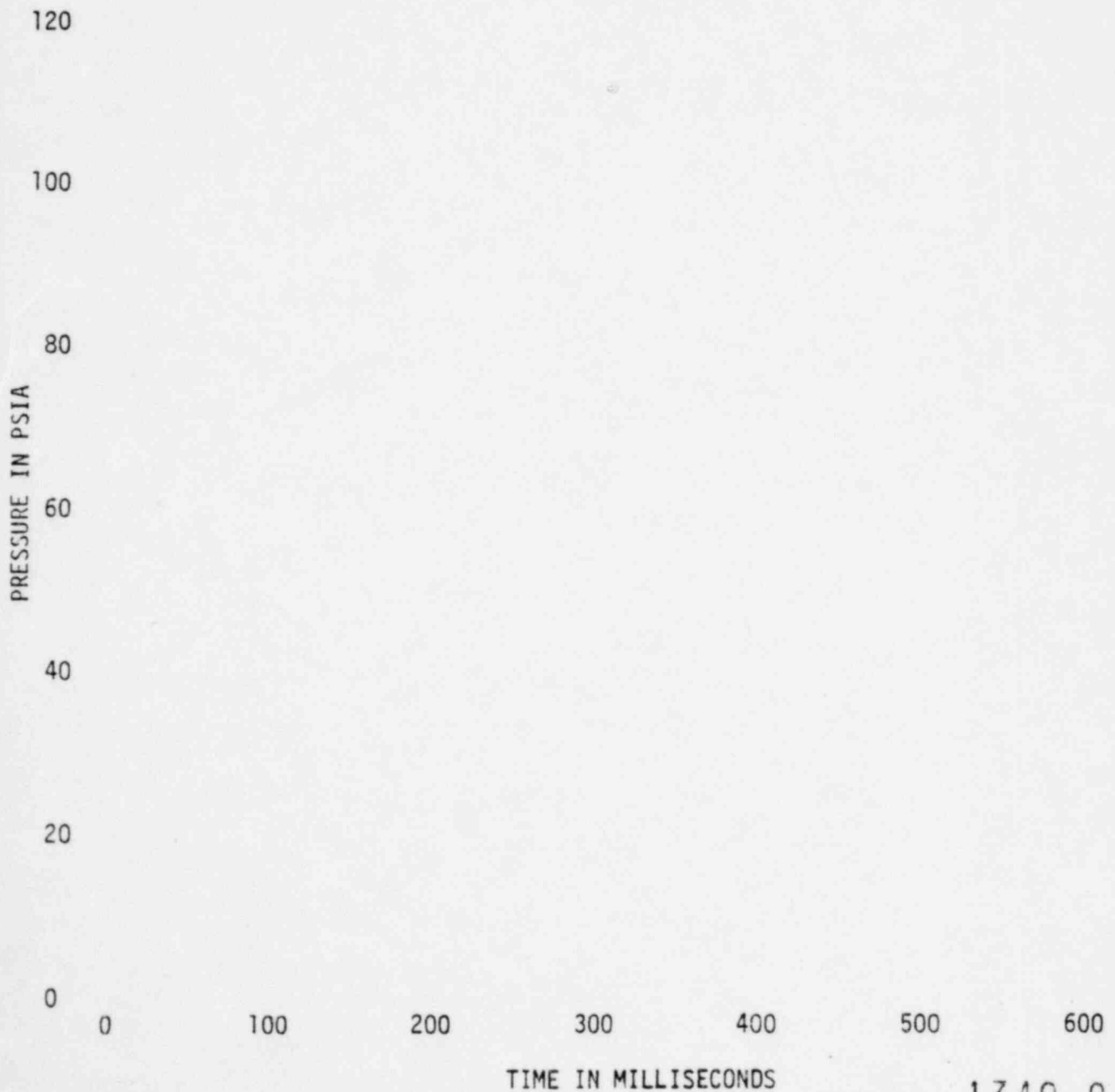
Figure A-251 presents the effect of drywell/wetwell  $\Delta P$  on enthalpy flow into the bubbles. Effect of drywell/wetwell  $\Delta P$  on downcomer internal pressure is shown in Figure A-252. Figure A-253 presents the effect of drywell/wetwell on pool and freespace pressures. The data for Nine Mile Point parallels that for the "typical" plant in Section 3.0.

The Nine Mile Point load definition tests were conducted at 7.94"  $H_2O$   $\Delta P$  and with a pipe deflector installed below the vent header. A  $\Delta P$  sensitivity test at 0"  $H_2O$   $\Delta P$  was also conducted. Some down-force oscillations were evident. The upforce was relatively smooth. Since the pipe deflector was close to the pool water level, the deflector was less effective in reducing the vent header impact force.

FIGURE A-201

DRYWELL ORIFICE UPSTREAM PRESSURE

Task 5.5.3-2 Nine Mile Point Test 3



1349 011

FIGURE A-202

DRYWELL PRESSURE

Task 5.5.3-2 Nine Mile Point Test 3

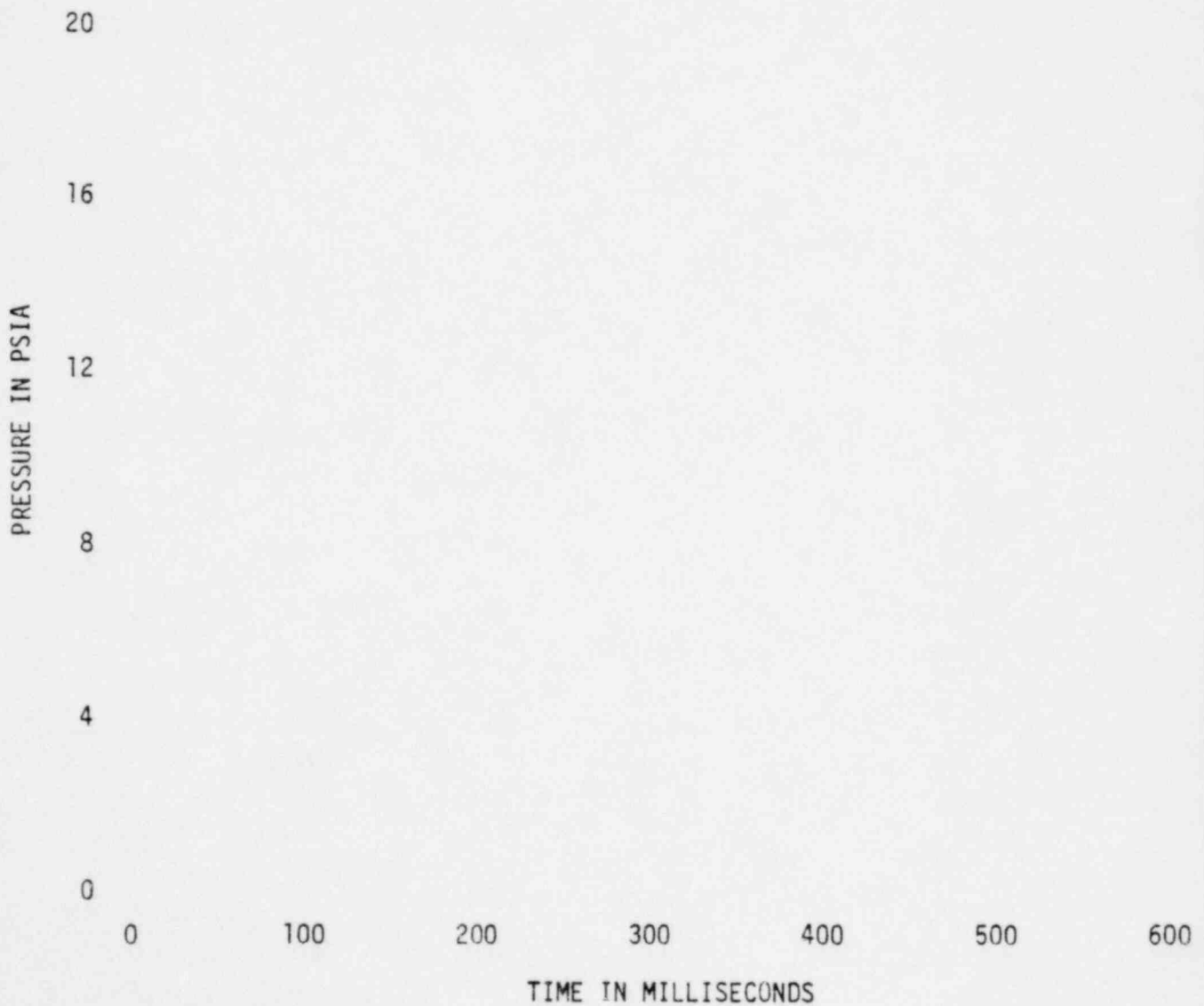


FIGURE A-203

DOWNCOMER ORIFICE DIFFERENTIAL PRESSURE

Task 5.5.3-2 Nine Mile Point Test 3



FIGURE A-204

DOWNCOMER ORIFICE UPSTREAM TEMPERATURE

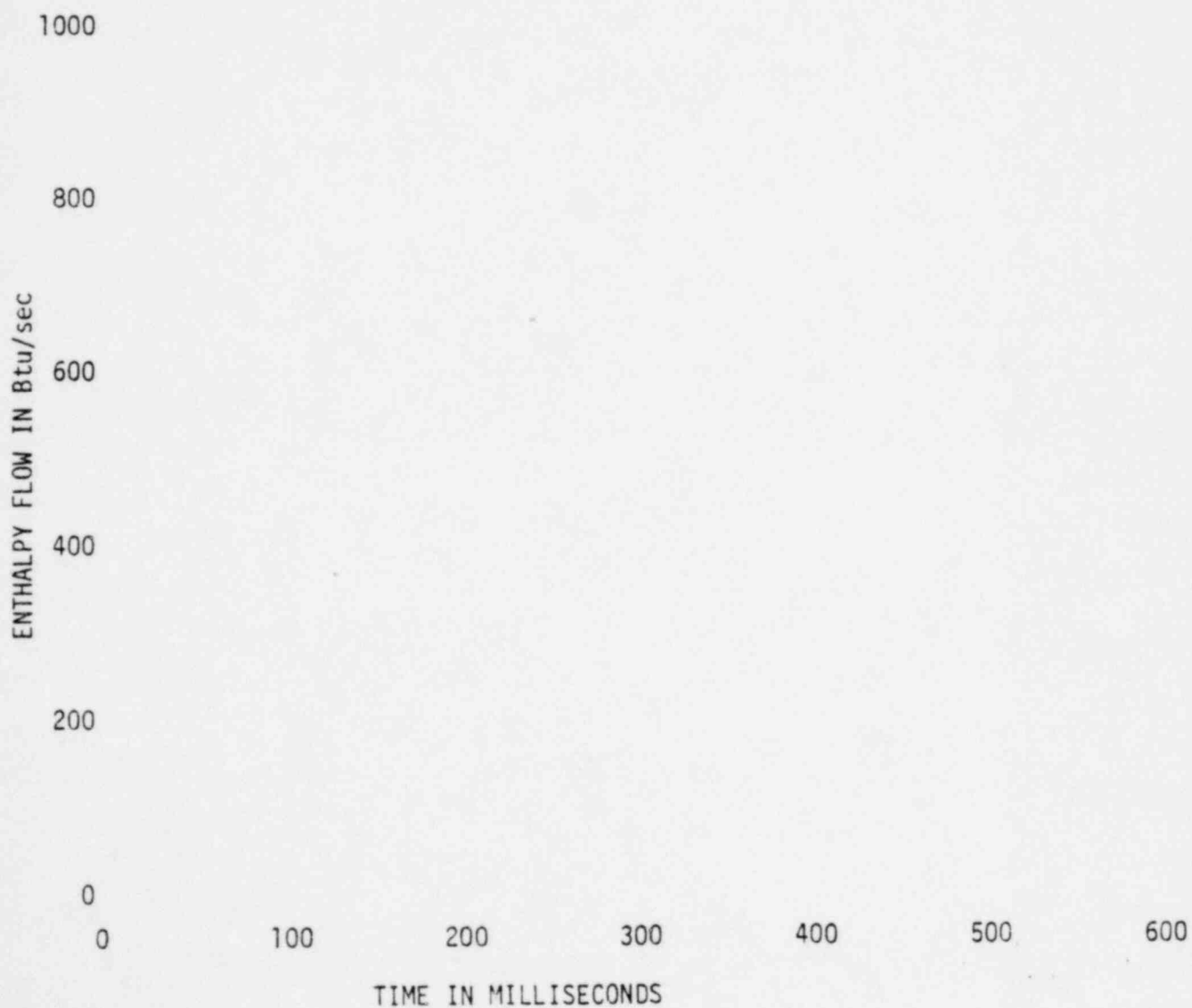
Task 5.5.3-2 Nine Mile Point Test 3



FIGURE A-205

ENTHALPY FLOW INTO POOL

Task 5.5.3-2 Nine Mile Point Test 3



1349 015

FIGURE A-206

DRYWELL ORIFICE UPSTREAM PRESSURE  
Task 5.5.3-2 Nine Mile Point Test 5

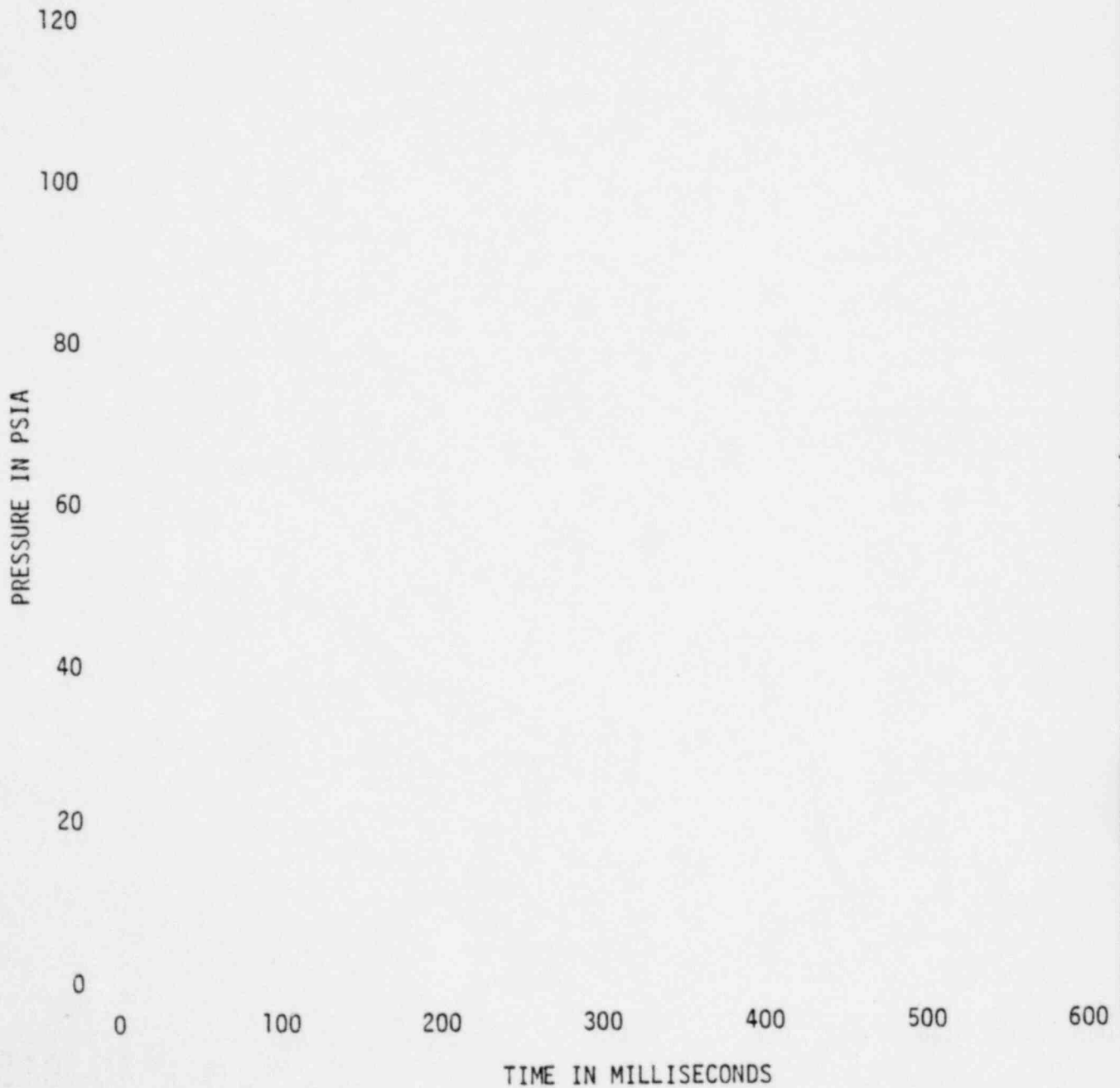


FIGURE A-207

DRYWELL PRESSURE

Task 5.5.3-2 Nine Mile Point Test 5

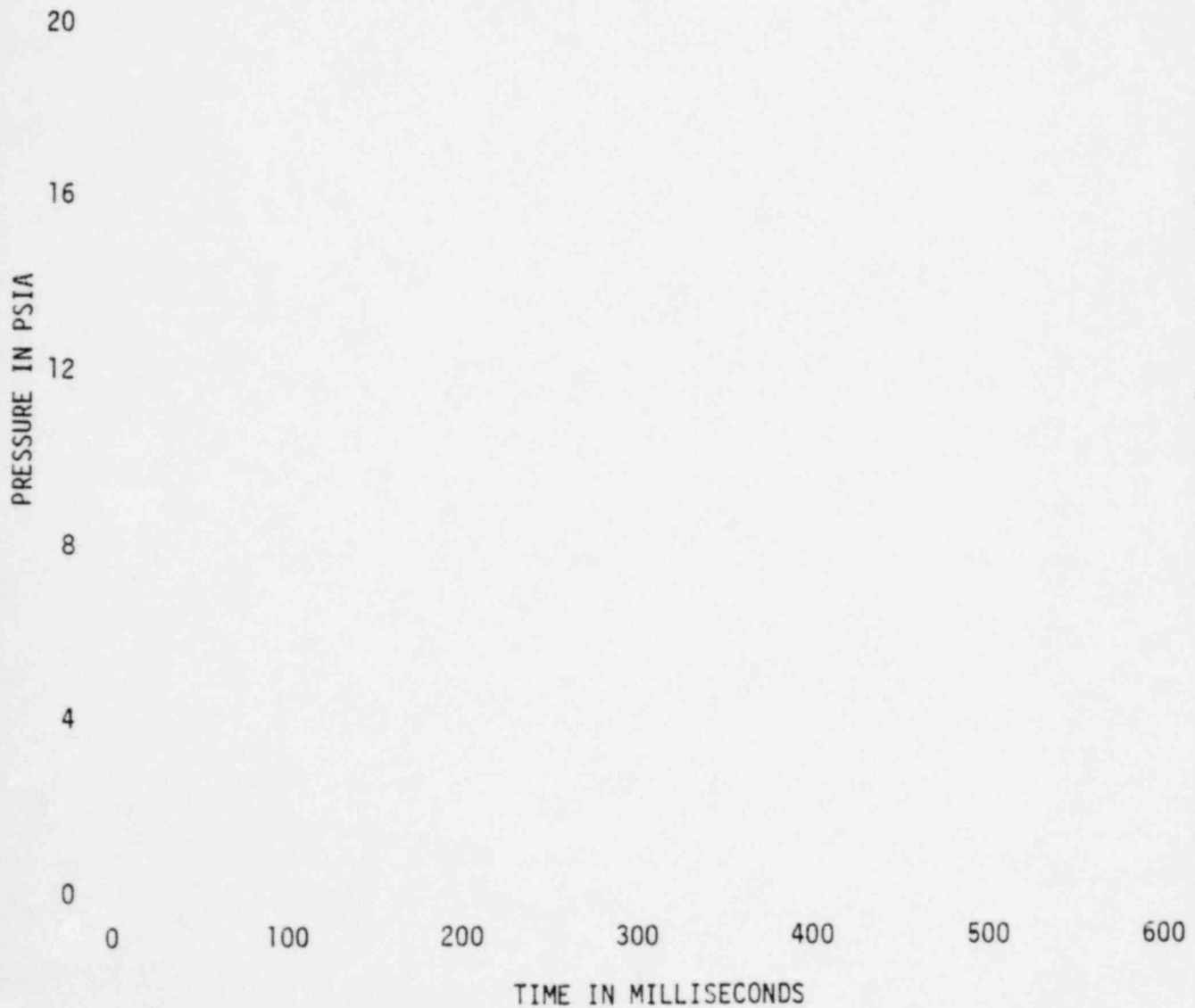


FIGURE A-208

DOWNCOMER ORIFICE DIFFERENTIAL PRESSURE

Task 5.5.3-2 Nine Mile Point Test 5



FIGURE A-209  
DOWNCOMER ORIFICE UPSTREAM TEMPERATURE  
Task 5.5.3-2 Nine Mile Point Test 5



1349 019

FIGURE A-210

ENTHALPY FLOW INTO POOL

Task 5.5.3-2 Nine Mile Point Test 5

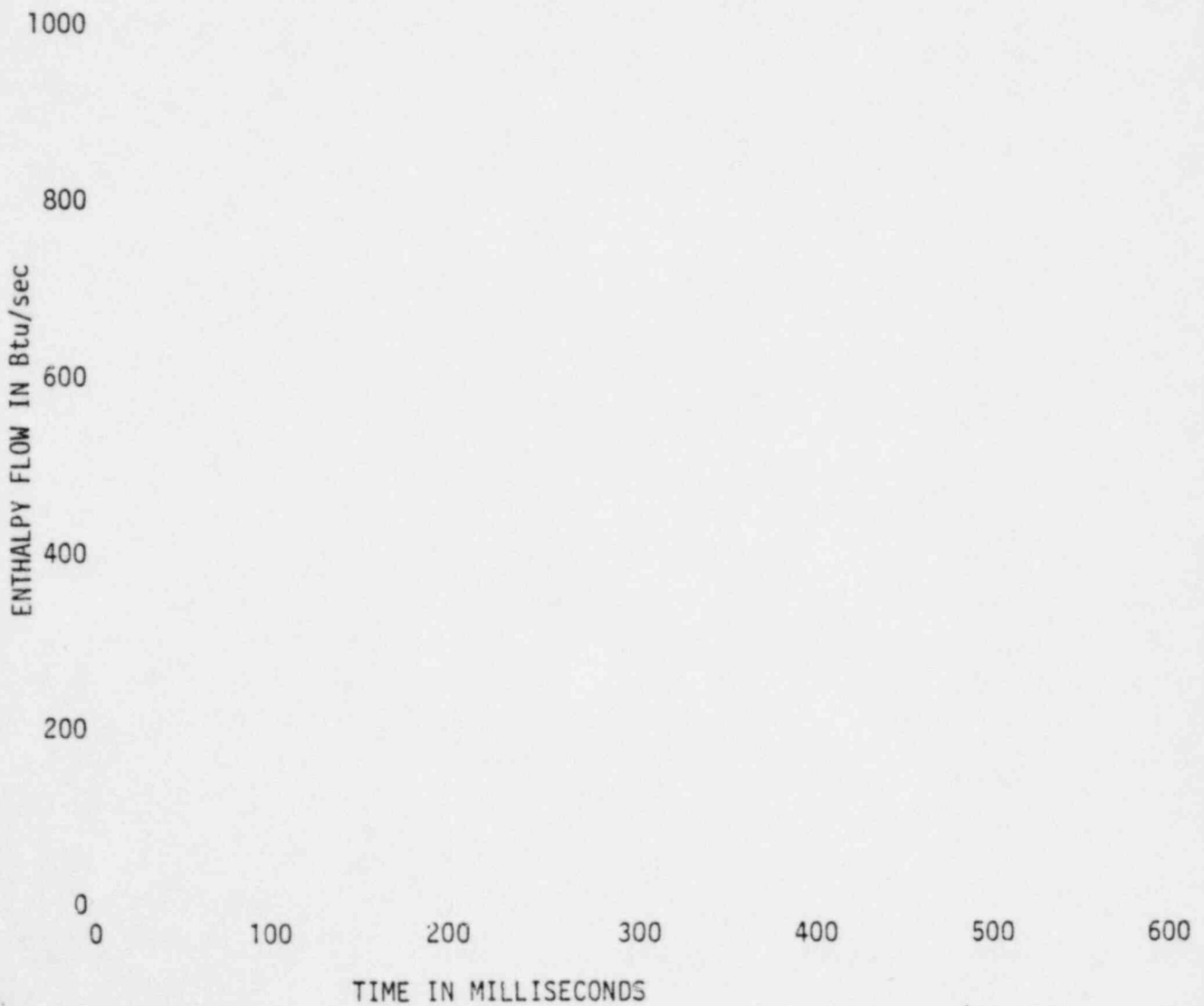


FIGURE A-211

DOWNCOMER INTERNAL PRESSURE

Task 5.5.3-2 Nine Mile Point Test 3

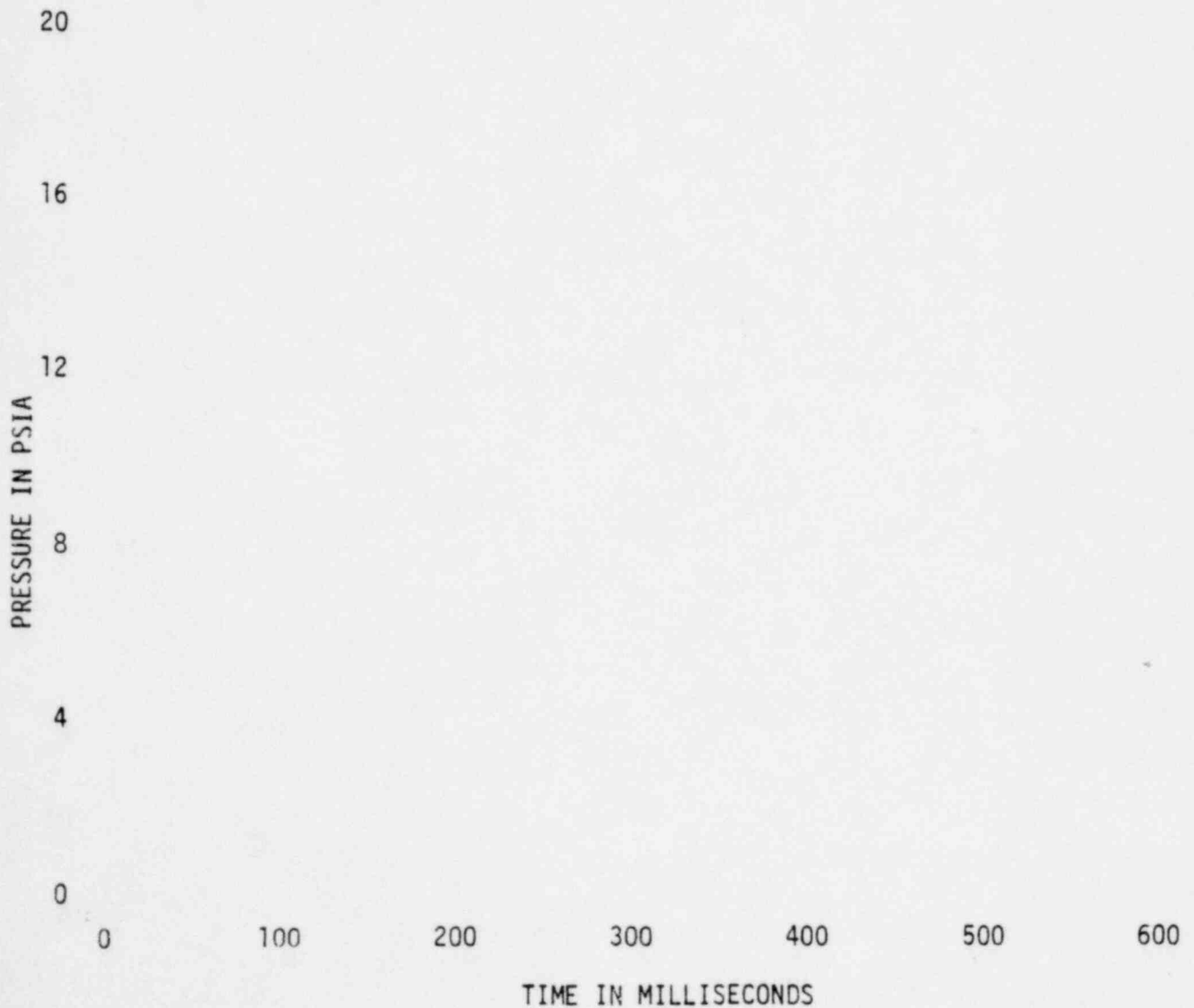


FIGURE A-212

WETWELL PRESSURES

Task 5.5.3-2 Nine Mile Point Test 3

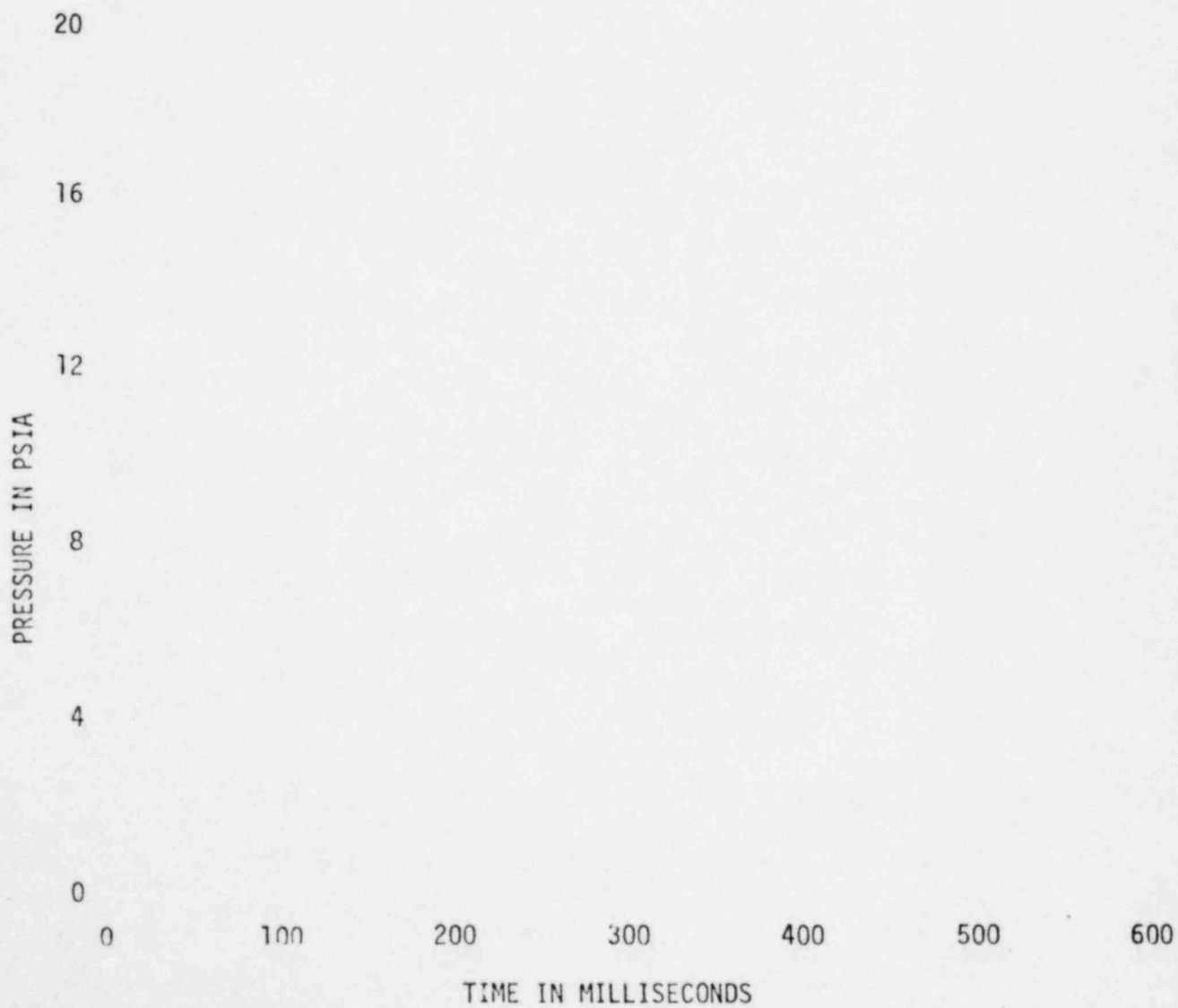
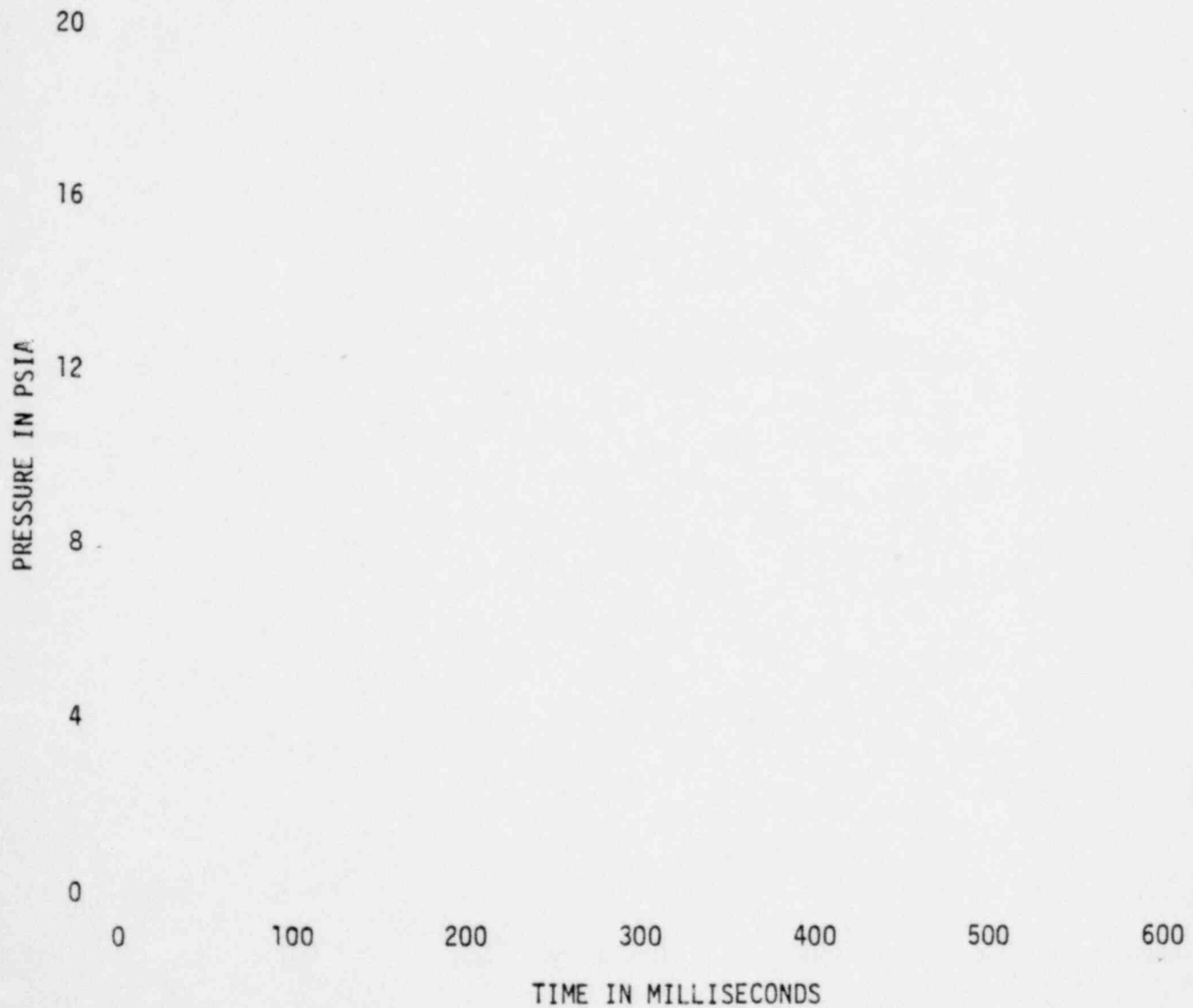


FIGURE A-213

DOWNCOMER INTERNAL PRESSURE

Task 5.5.3-2 Nine Mile Point Test 5



1349 023

FIGURE A-214

WETWELL PRESSURES

Task 5.5.3-2 Nine Mile Point Test 5

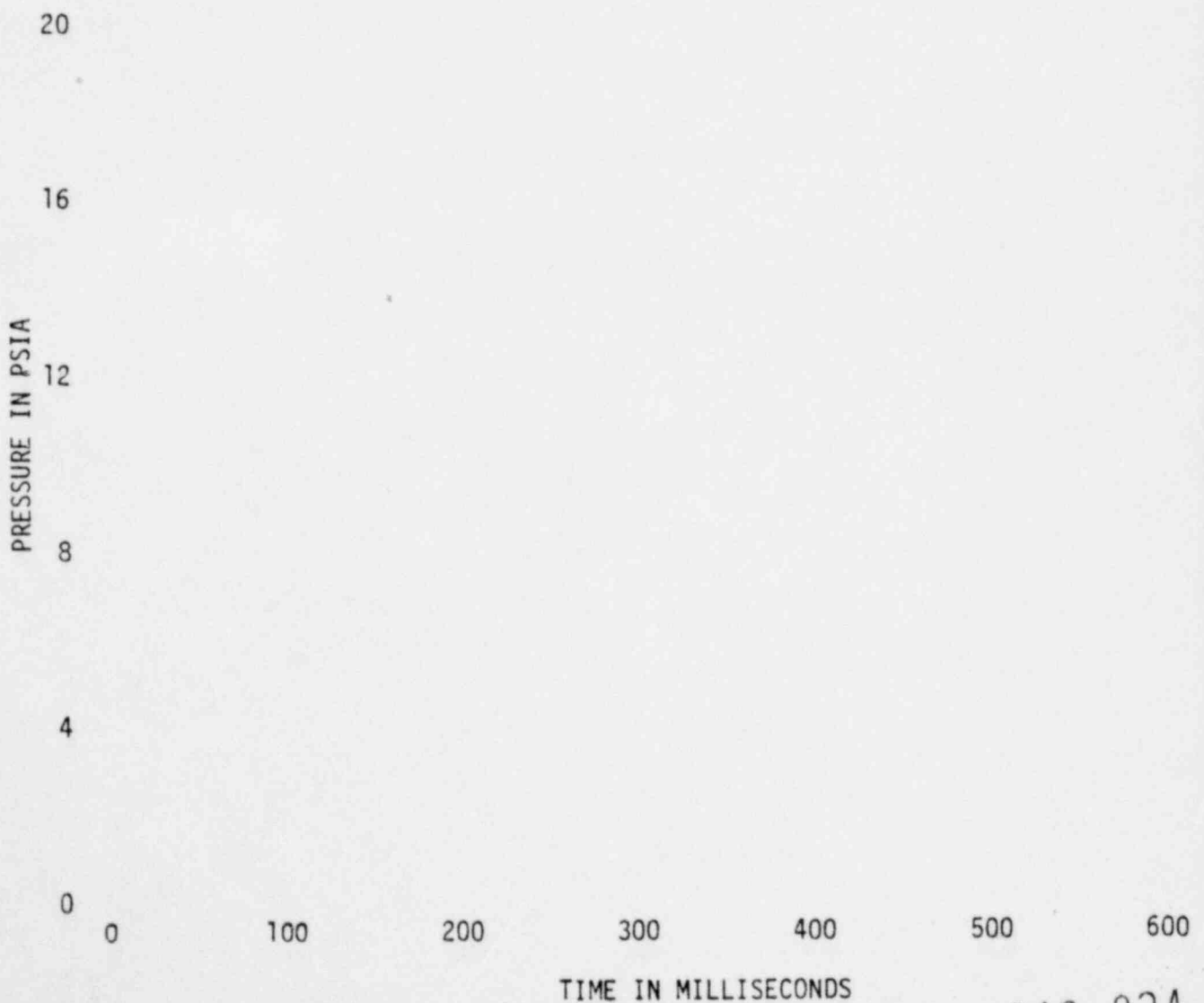


FIGURE A-215

NET TORUS FORCE FROM PRESSURE INTEGRAL

Task 5.5.3-2 Nine Mile Point Test 3



TIME IN MILLISECONDS

FIGURE A-216

NET TORUS FORCE FROM PRESSURE INTEGRAL

Task 5.5.3-2 Nine Mile Point Test 5

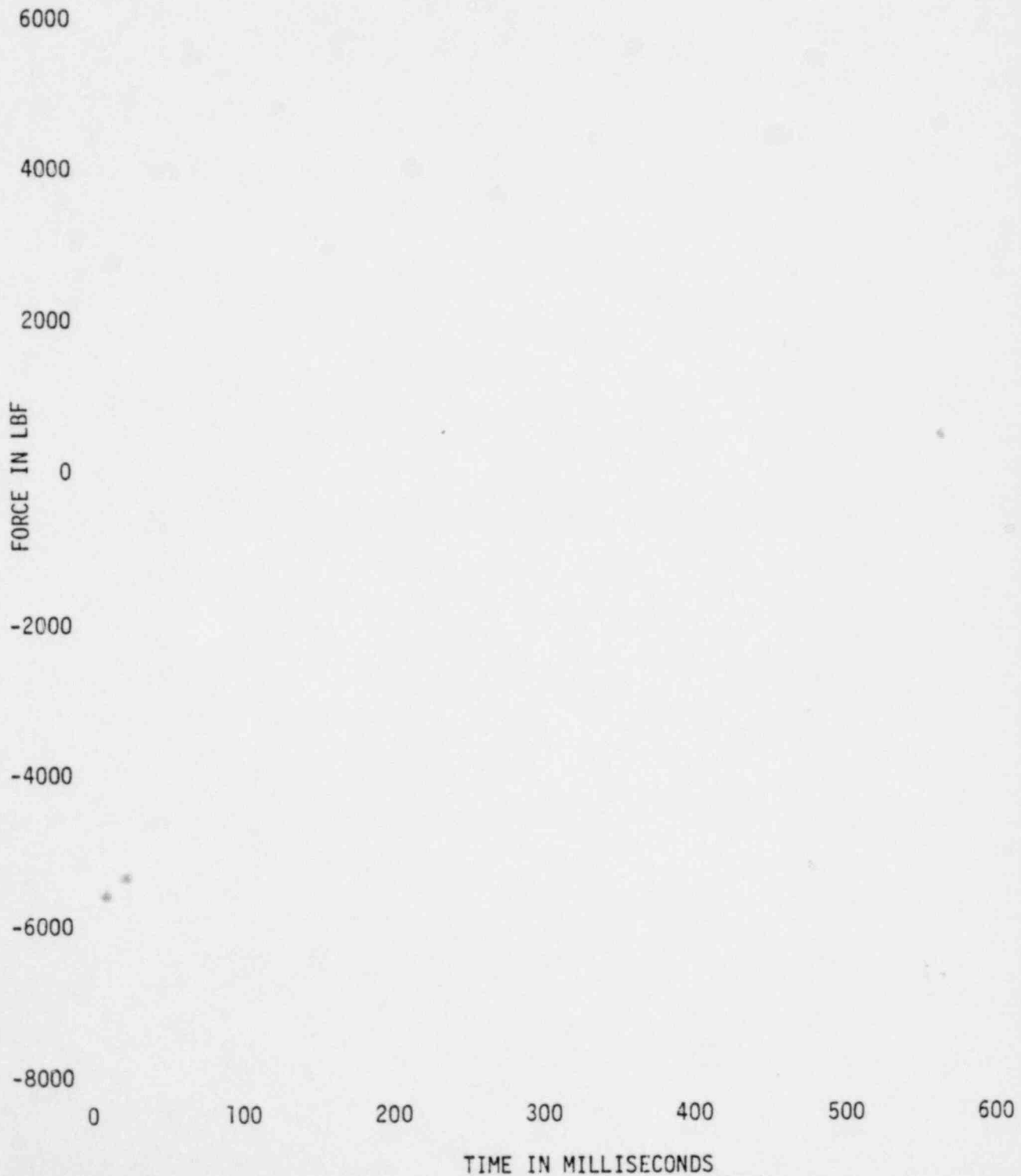


FIGURE A-217

TORUS LOAD CELL

Task 5.5.3-2 Nine Mile Point Test 3

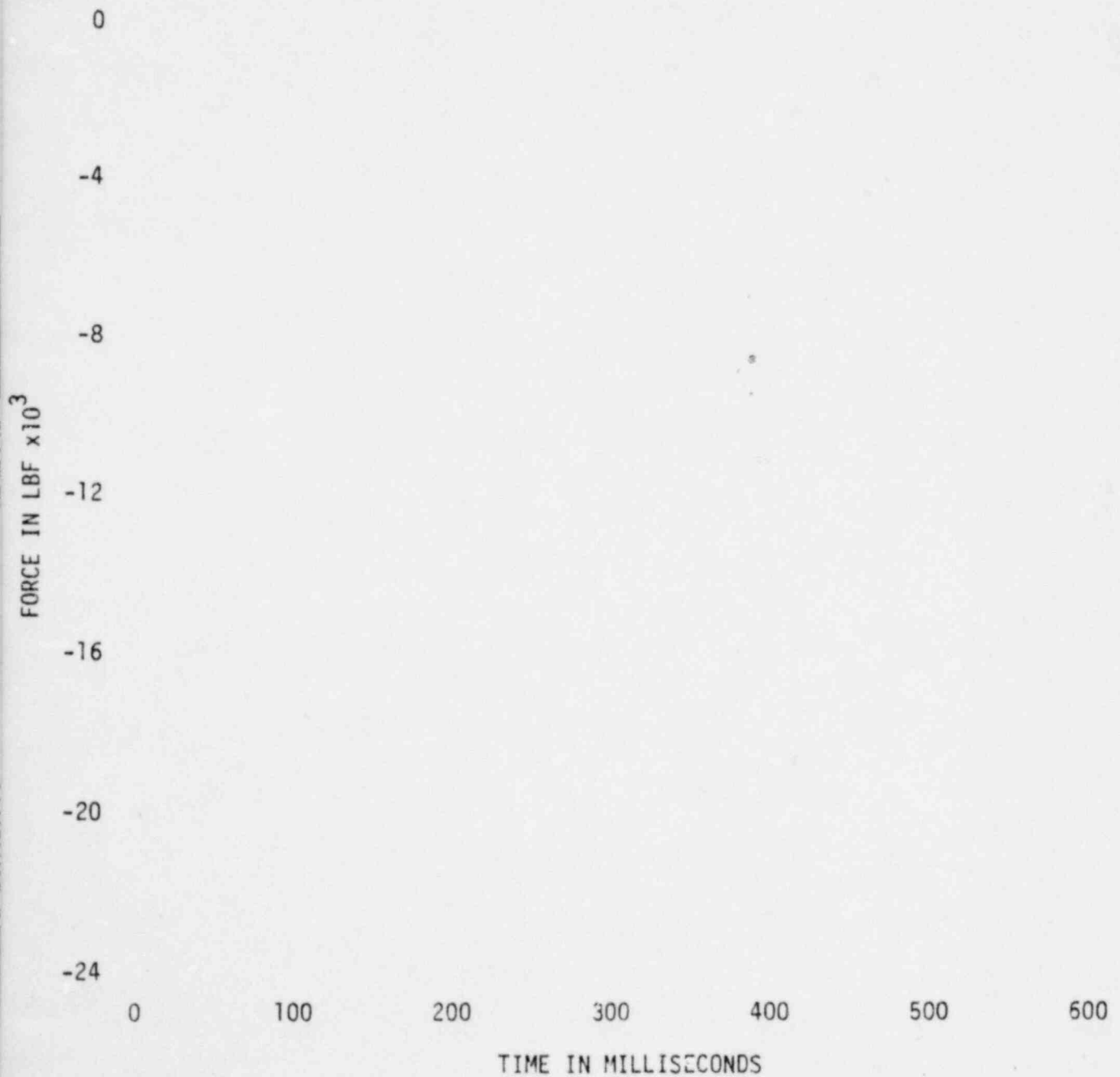


FIGURE A-218

TORUS VERTICAL ACCELERATION

Task 5.5.3-2 Nine Mile Point Test 3

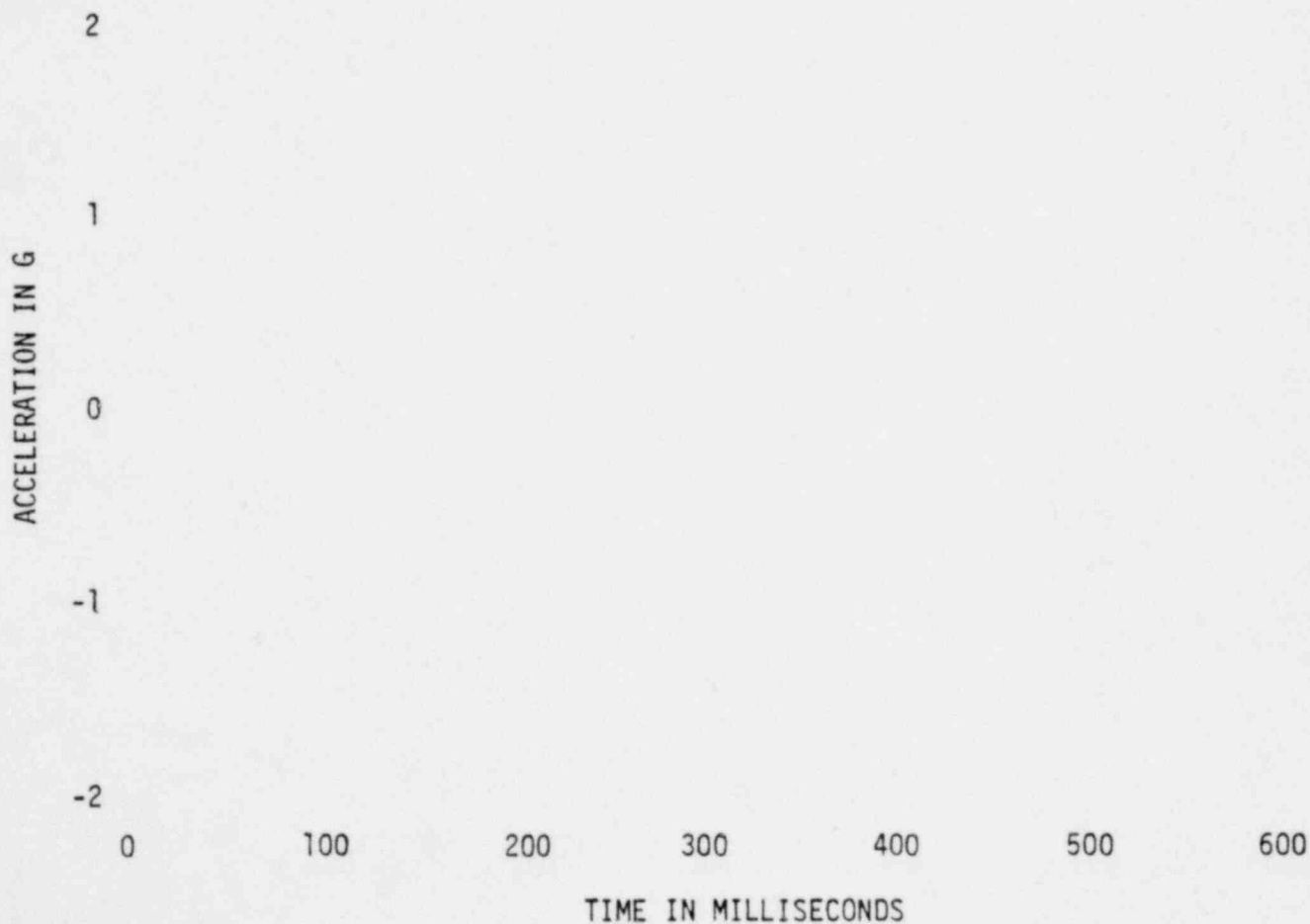


FIGURE A-219

TORUS LOAD CELL

Task 5.5.3-2 Nine Mile Point Test 5

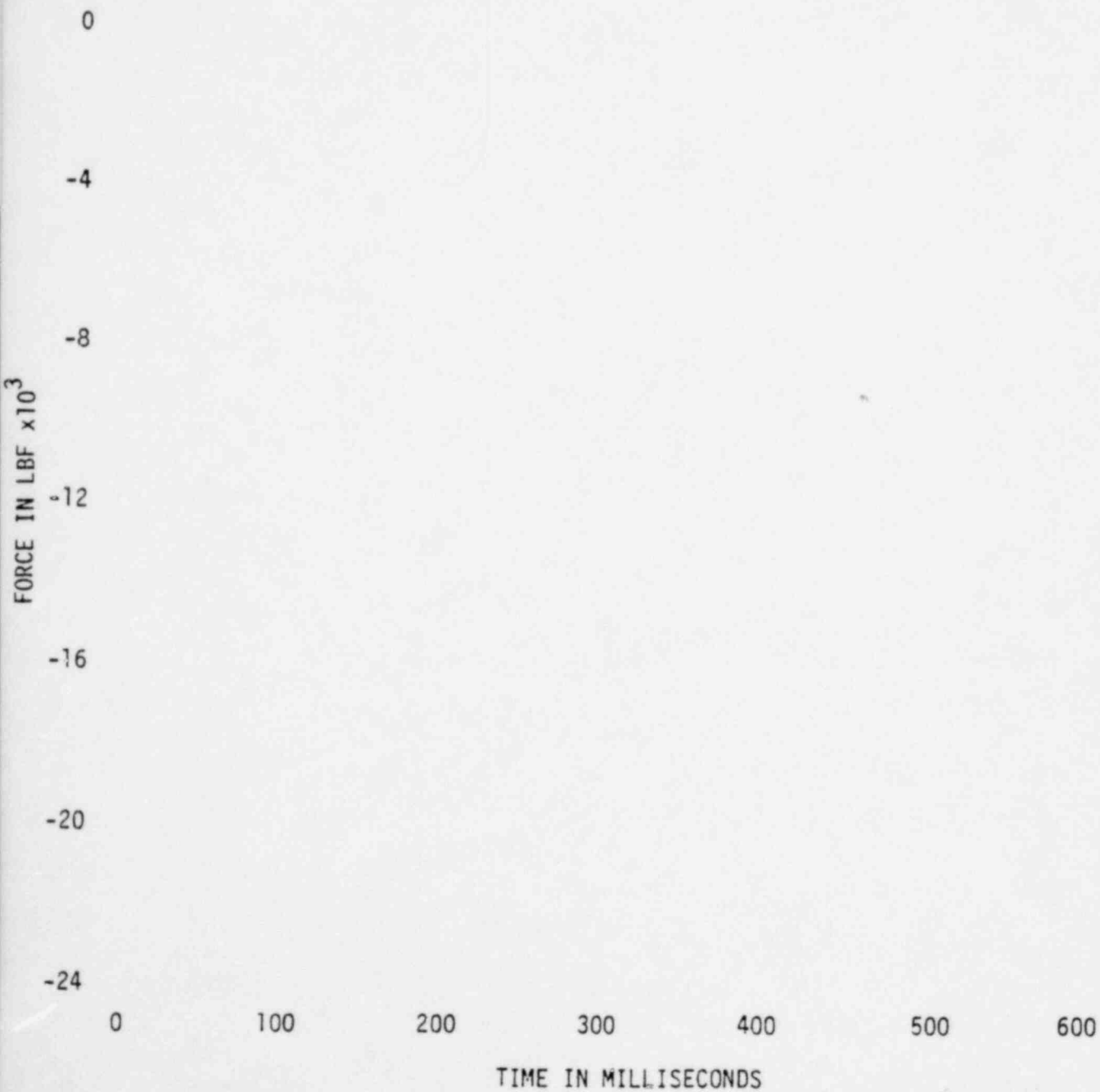
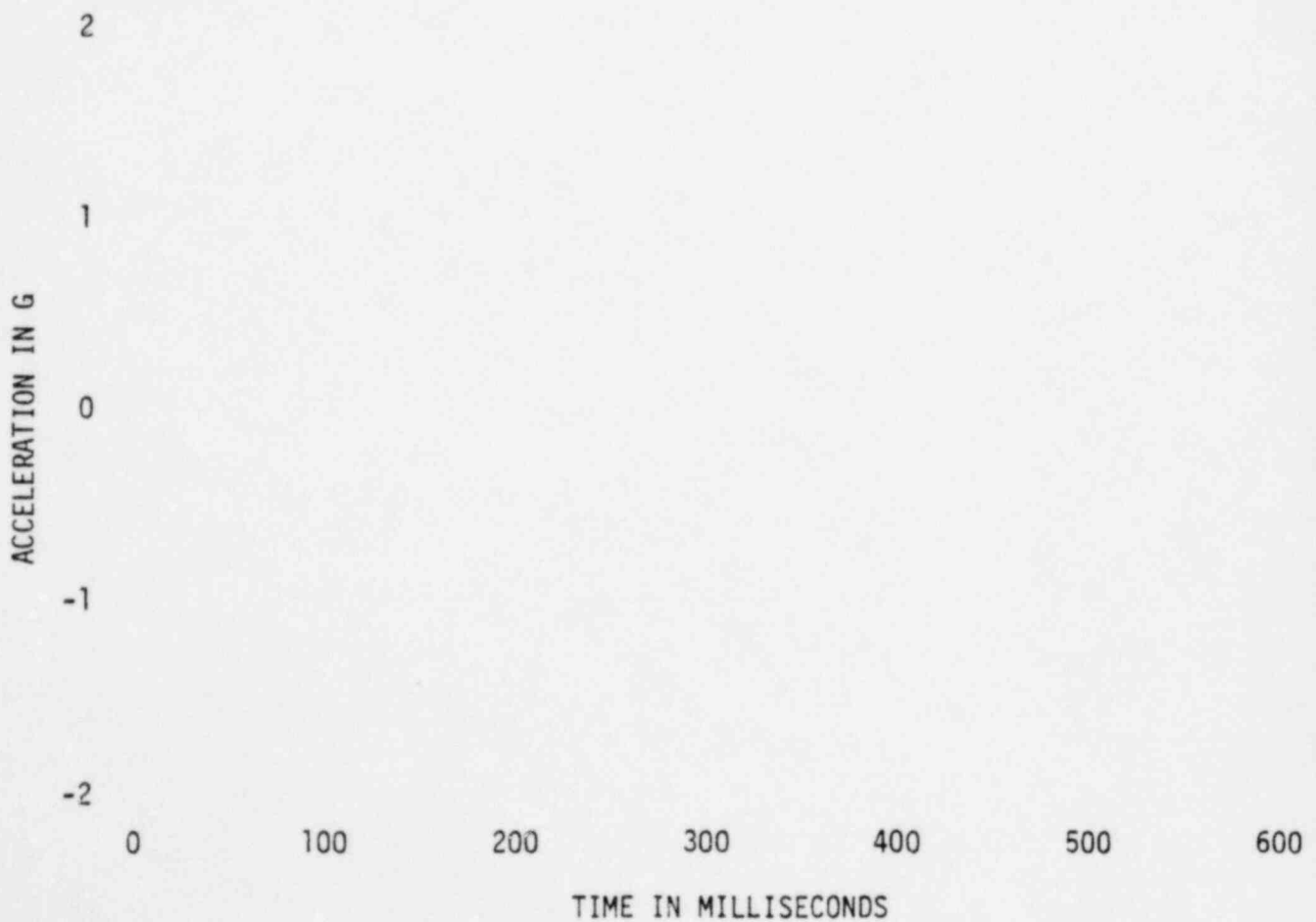


FIGURE A-220

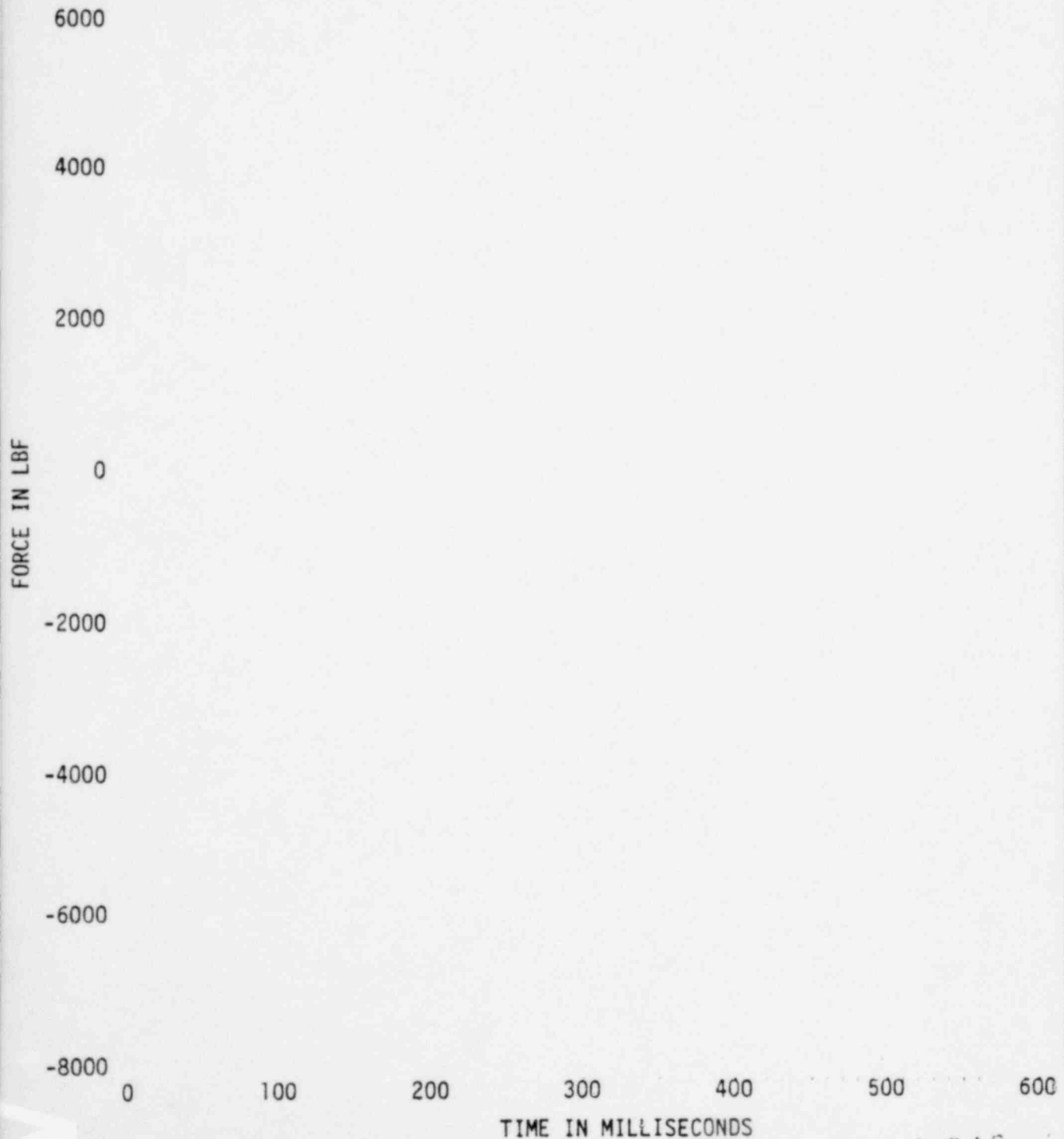
TORUS VERTICAL ACCELERATION

Task 5.5.3-2 Nine Mile Point Test 5



COMPARISON OF NET TORUS FORCE FROM PRESSURE INTEGRAL  
WITH NET TORUS FORCE FROM LOAD CELL CORRECTED FOR TORUS INERTIA

Task 5.5.3-2 Nine Mile Point Test 3

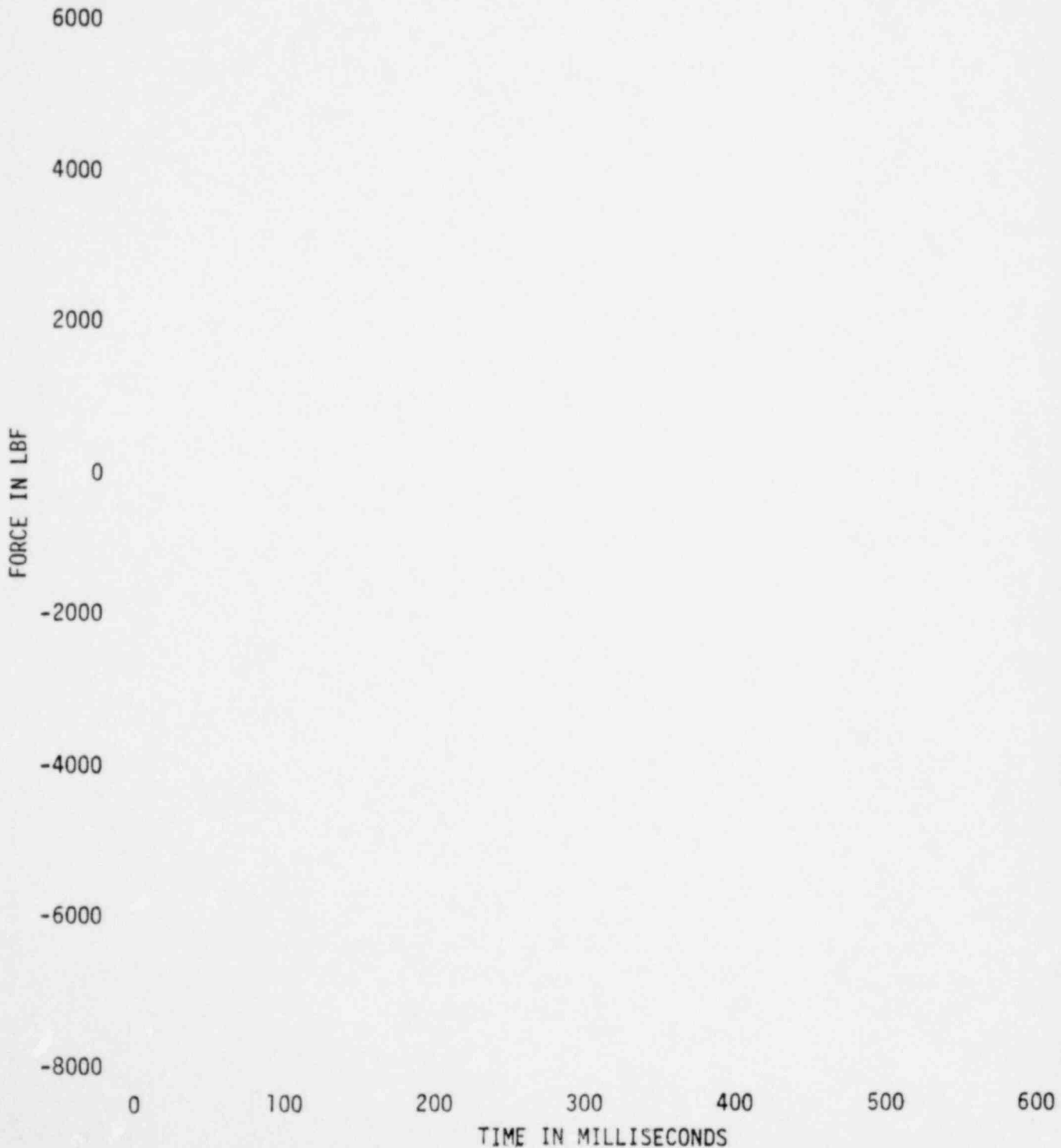


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FIGURE A-222

COMPARISON OF NET TORUS FORCE FROM PRESSURE INTEGRAL  
WITH NET TORUS FORCE FROM LOAD CELL CORRECTED FOR TORUS INERTIA

Task 5.5.3-2 Nine Mile Point Test 5

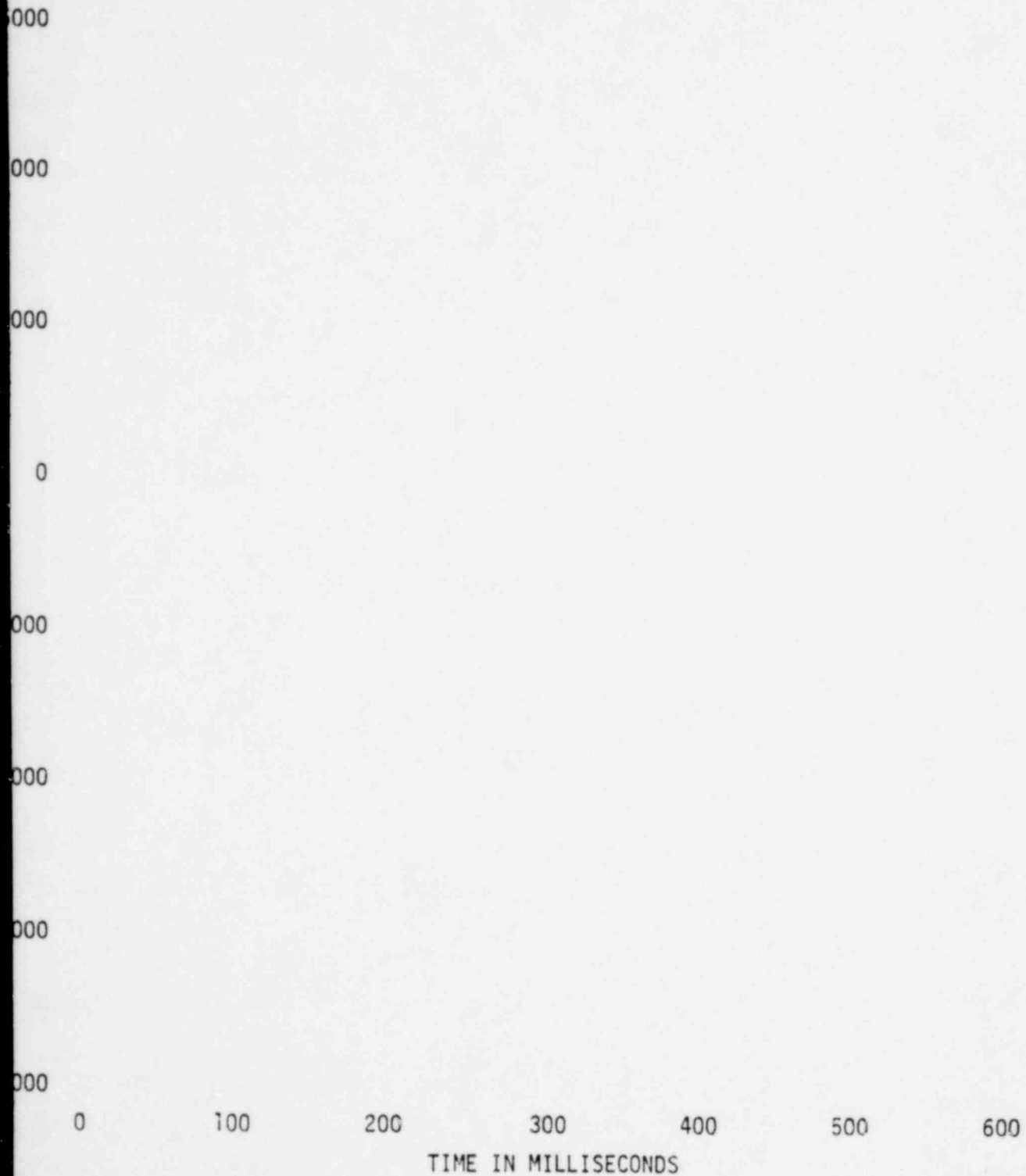


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FIGURE A-223

NET TORUS FORCE FROM PRESSURE INTEGRAL, CORRECTED FOR WATER INERTIA

Task 5.5.3-2 Nine Mile Point Test 3



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FIGURE A-224

NET TORUS FORCE FROM PRESSURE INTEGRAL, CORRECTED FOR WATER INERTIA

Task 5.5.3-2 Nine Mile Point Test 5

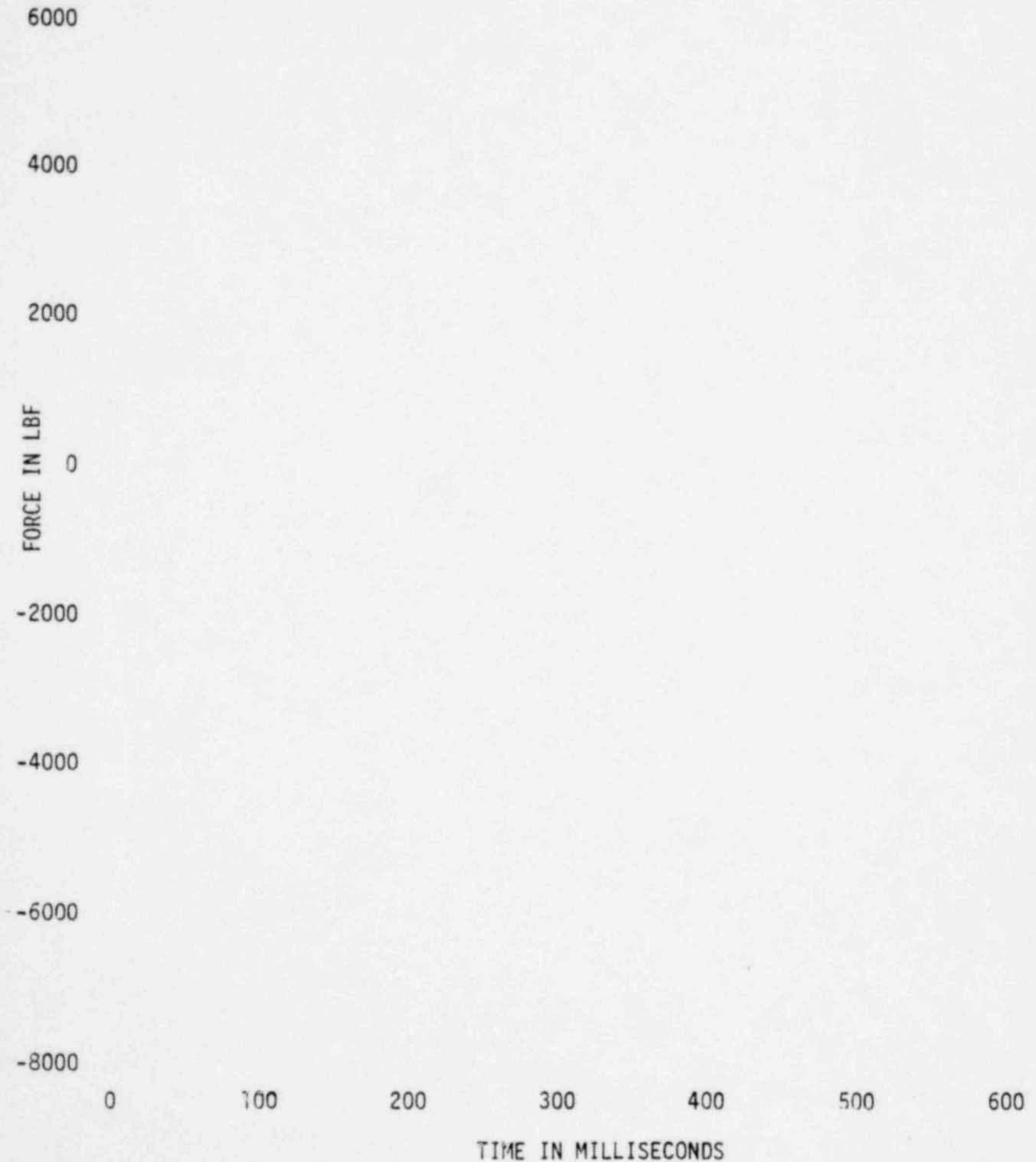


FIGURE A-225

AVERAGE POOL PRESSURE, CORRECTED FOR WATER INERTIA

Task 5.5.3-2 Nine Mile Point Test 3



FIGURE A-226

NET AVERAGE POOL PRESSURE, CORRECTED FOR WATER INERTIA

Task 5.5.3-2 Nine Mile Point Test 3

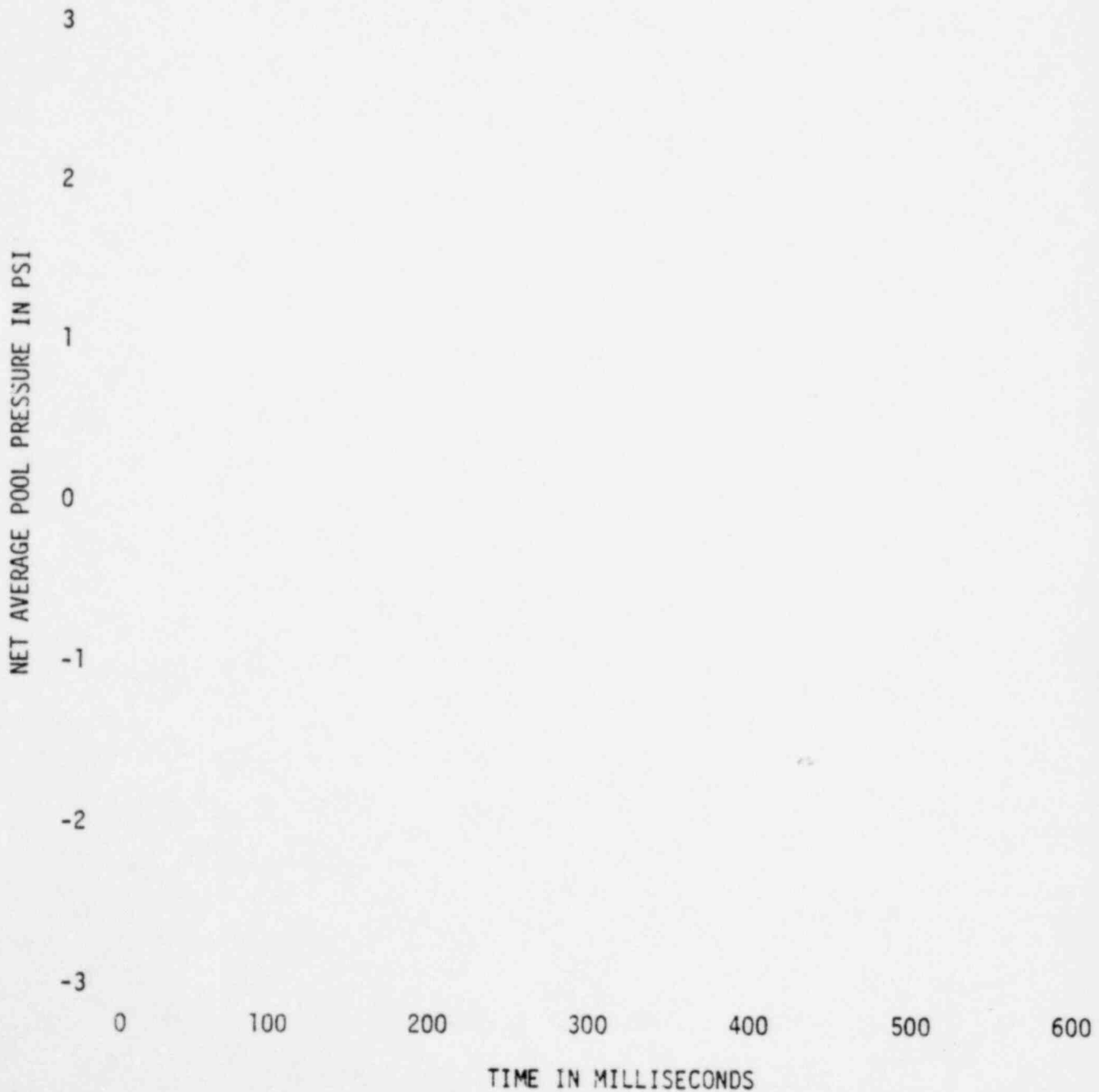
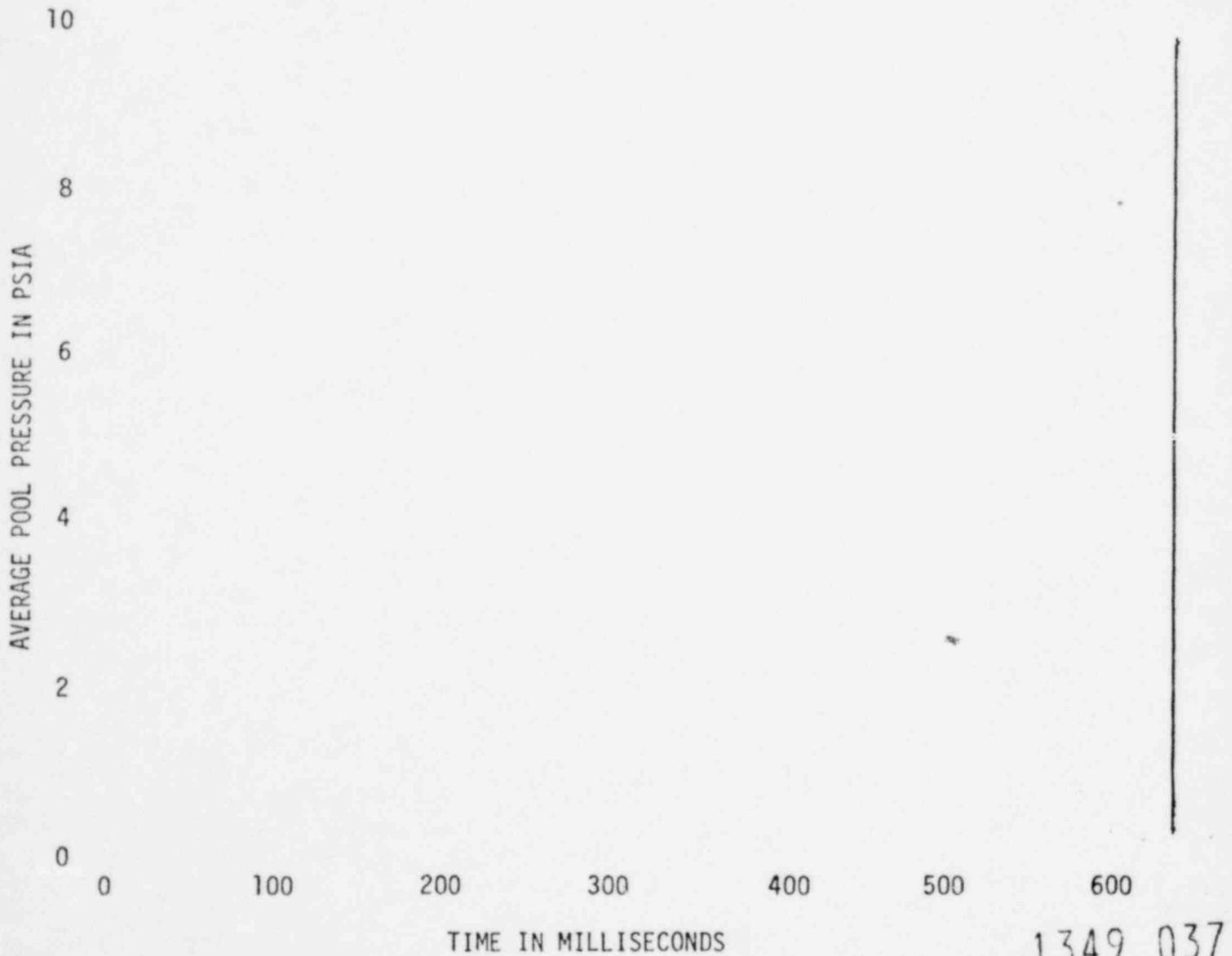


FIGURE A-227

AVERAGE POOL PRESSURE, CORRECTED FOR WATER INERTIA

Task 5.5.3-2 Nine Mile Point Test 5

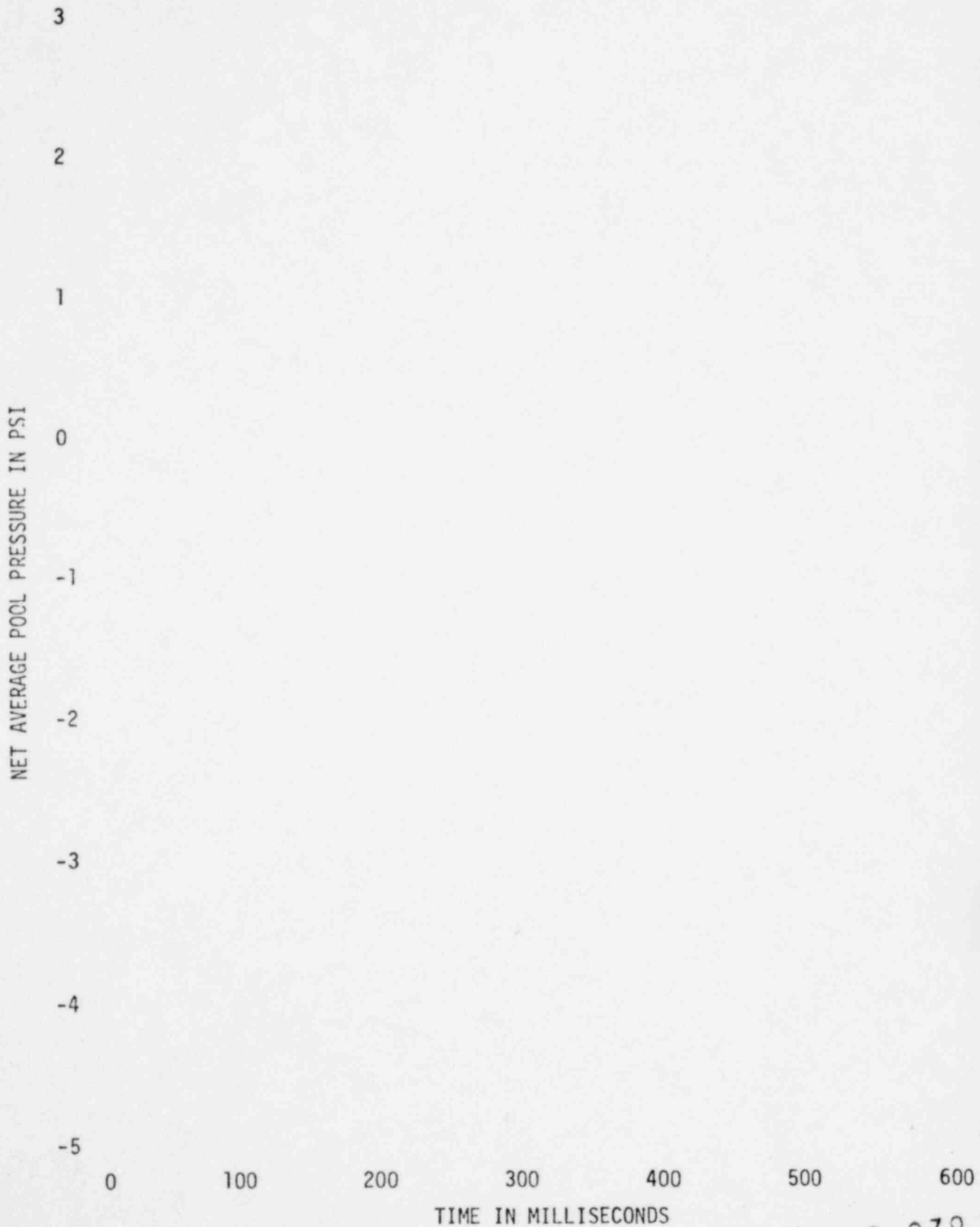


1349 037

FIGURE A-228

NET AVERAGE POOL PRESSURE, CORRECTED FOR WATER INERTIA

Task 5.5.3-2 Nine Mile Point Test 5



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Task 5.5.3-2 Nine Mile Point Test 3

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A-265

IMPACT PRESSURE IN PSIA

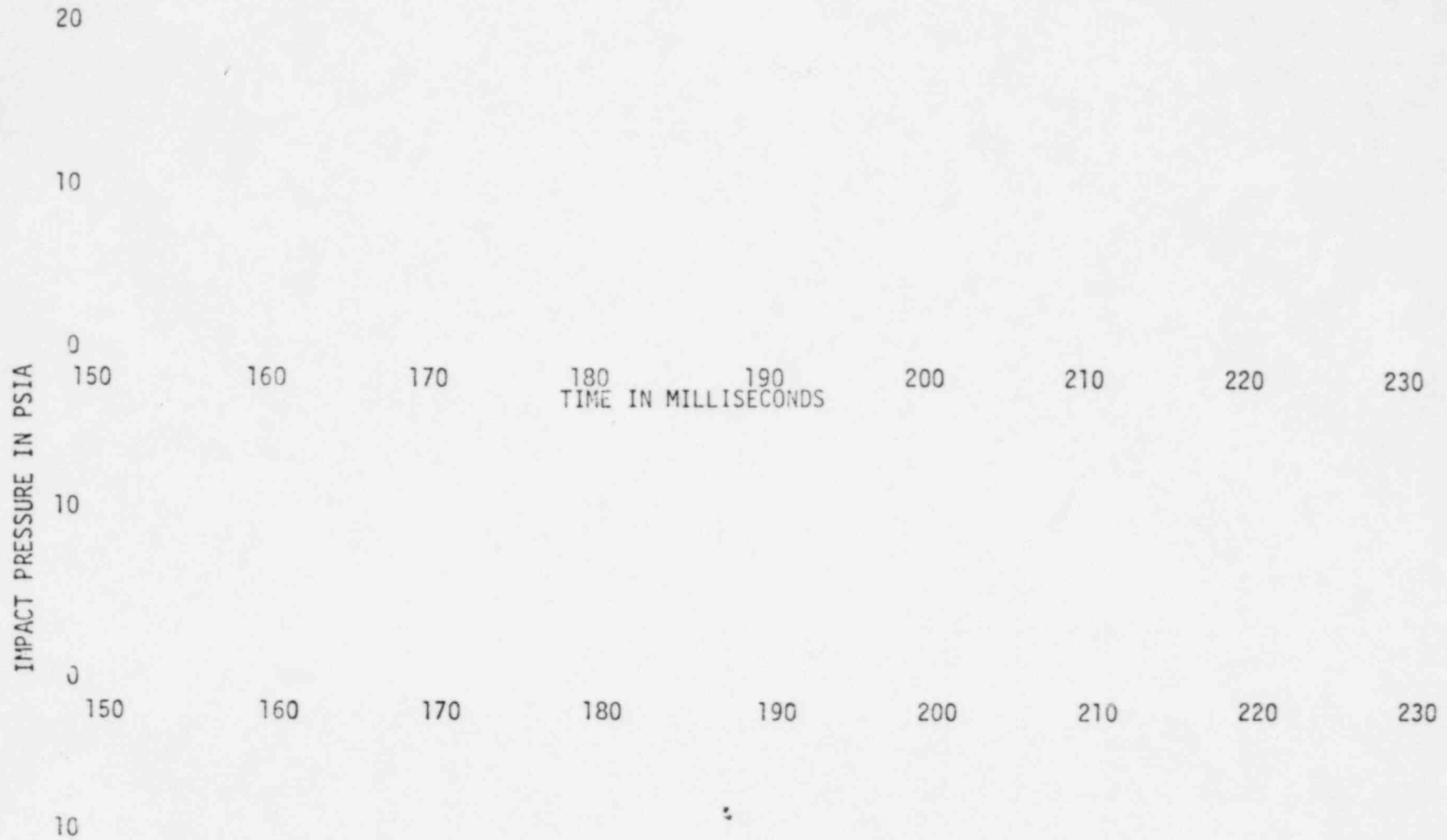
TIME IN MILLISECONDS

1349 03

FIGURE A-230

VENT HEADER IMPACT PRESSURES

Task 5.5.3-2 Nine Mile Point Test 3

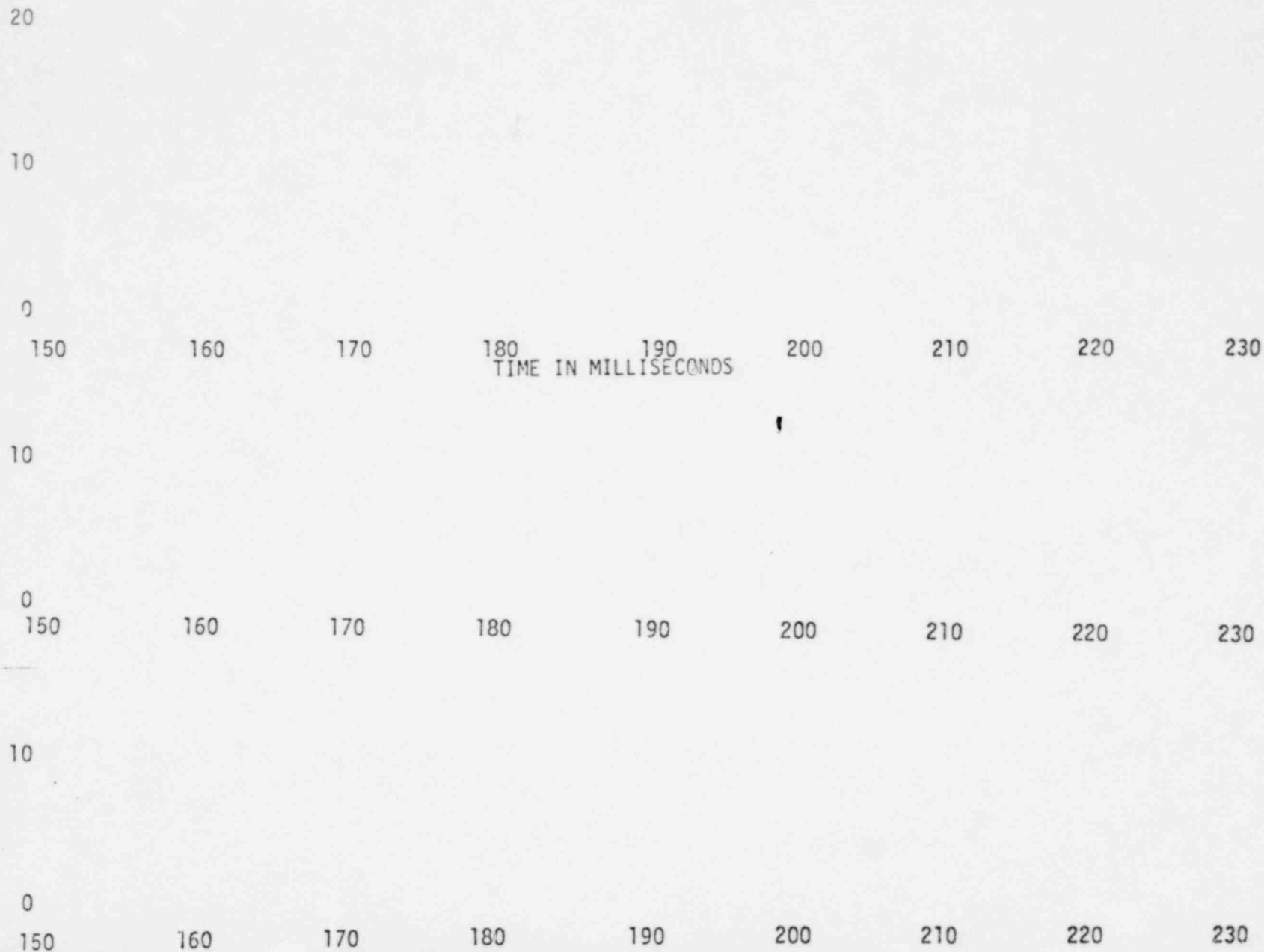


A-266

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# Task 5.5.3-2 Nine Mile Point Test 3



A-267

IMPACT PRESSURE IN PSIA

1349 041

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FIGURE A-232

VENT HEADER IMPACT PRESSURES

Task 5.5.3-2 Nine Mile Point Test 3



VENT HEADER IMPACT PRESSURES  
Task 5.5.3-2 Nine Mile Point Test 5

IMPACT PRESSURE IN PSIA

FIGURE A-234

VENT HEADER IMPACT PRESSURES

Task 5.5.3-2 Nine Mile Point Test 5

IMPACT PRESSURE IN PSIA

A-270

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VENT HEADER IMPACT PRESSURES  
Task 5.5.3-2 Nine Mile Point Test 5

IMPACT PRESSURE IN PSIA

1349 045

FIGURE A-236

VENT HEADER IMPACT PRESSURES

Task 5.5.3-2 Nine Mile Point Test 5

NEDO-21944

IMPACT PRESSURE IN PSIA

A-272

1349 046

FIGURE A-237

COMPARISON OF VENT HEADER IMPACT RESULTS  
(Corrected Load Cell and Pressure Integration)  
Task 5.5.3 Nine Mile Point Tests 3, 5

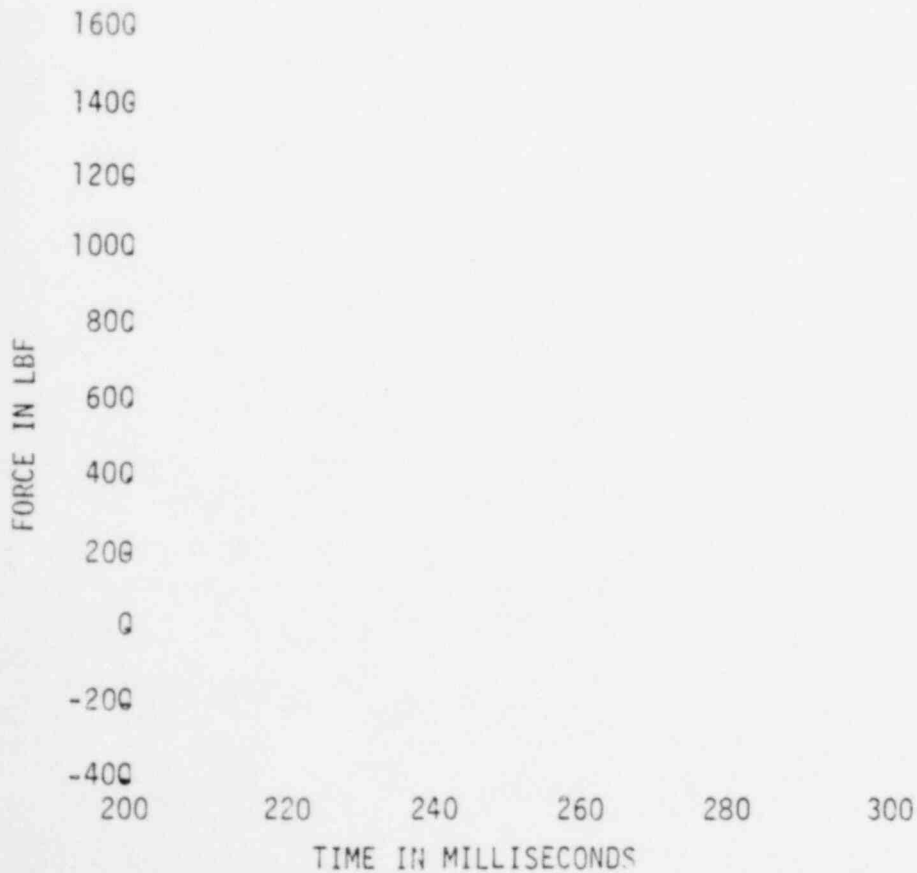
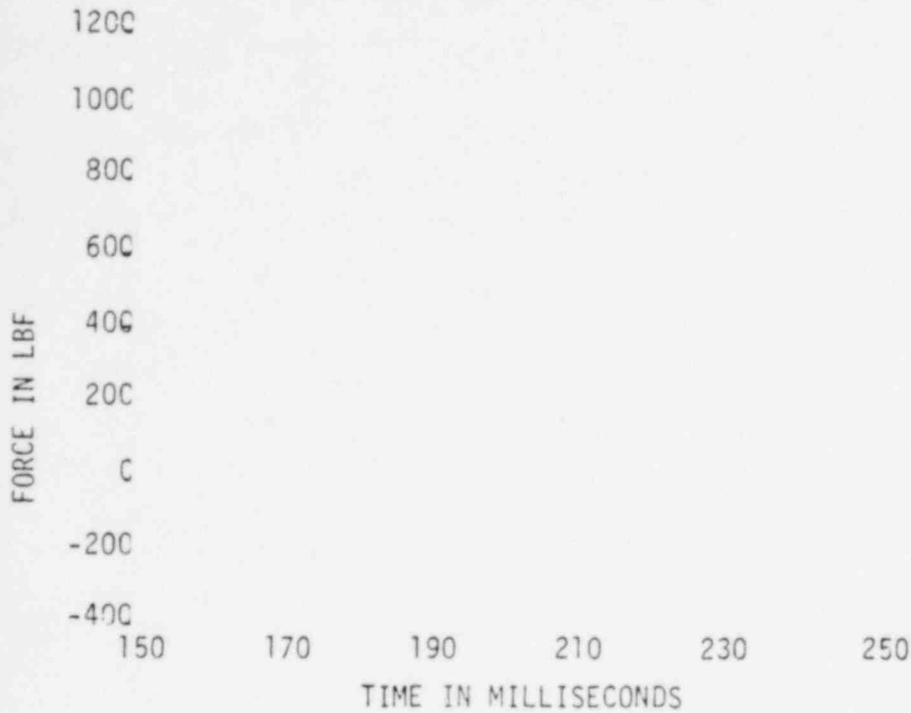


FIGURE A-238

VENT HEADER VERTICAL ACCELERATION

Task 5.5.3-2 Nine Mile Point Test 3

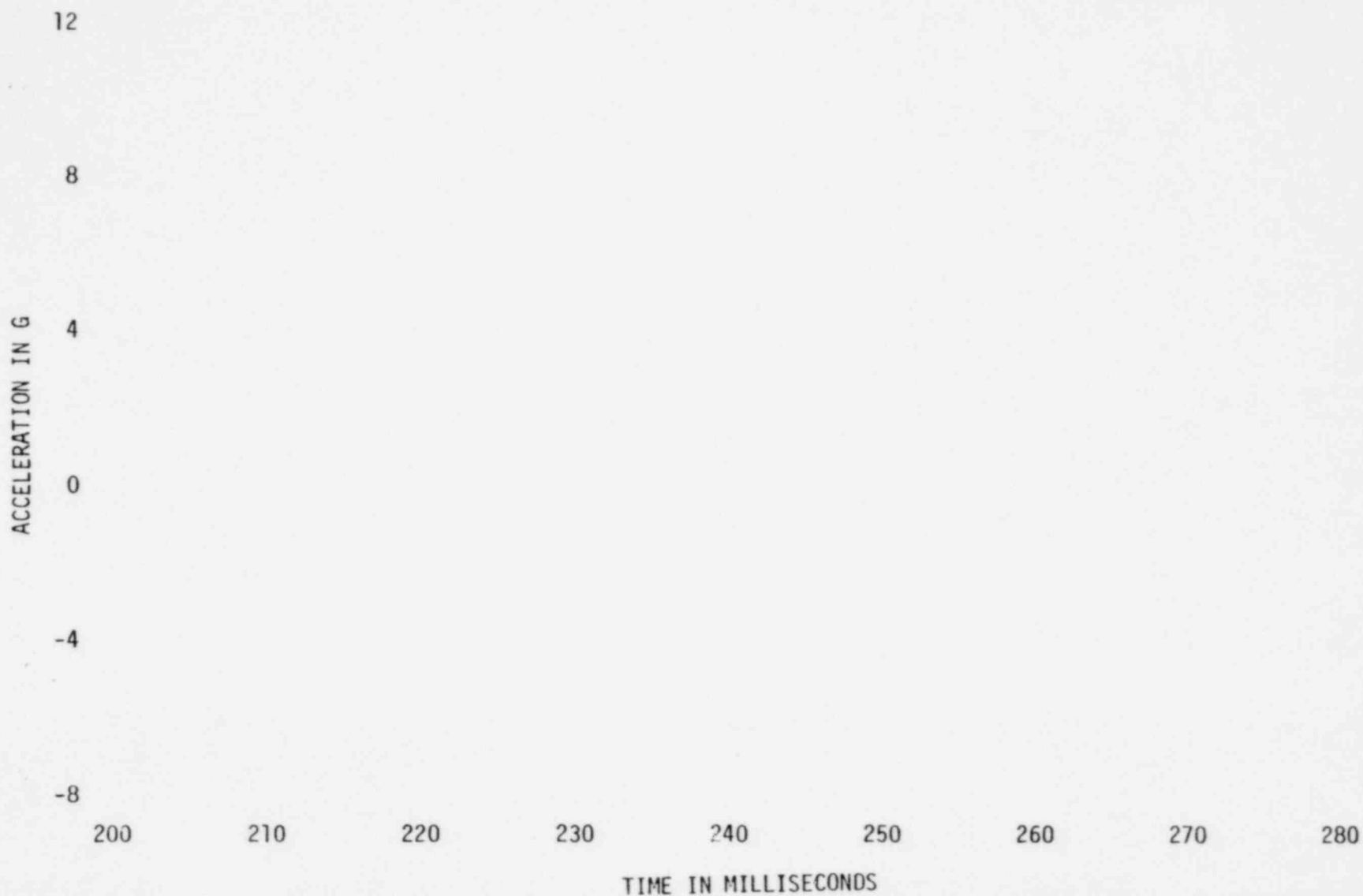


A-274

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VENT HEADER VERTICAL ACCELERATION  
Task 5.5.3-2 Nine Mile Point Test 5



A-275

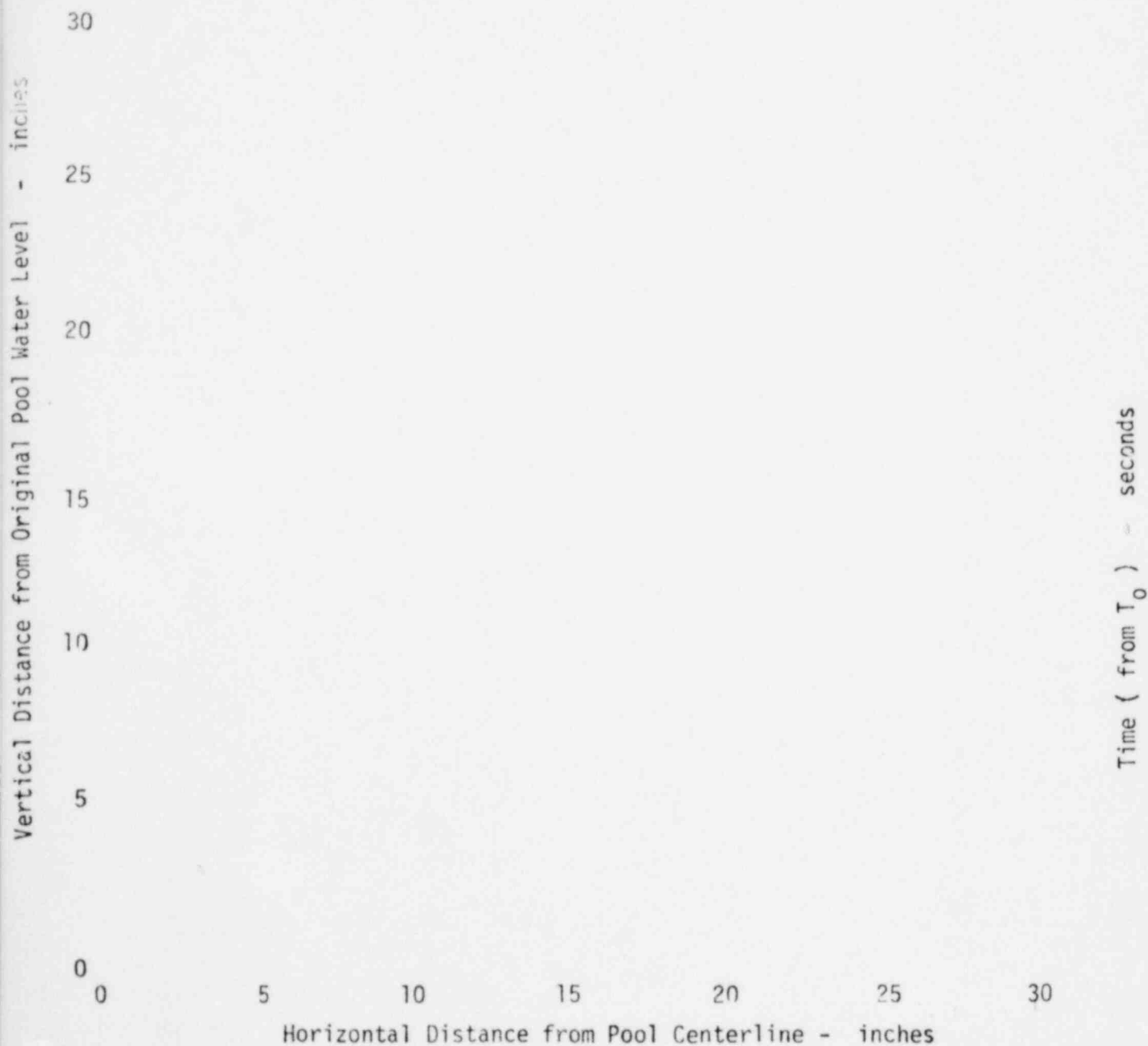
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NEDO-21944  
FIGURE A-240

TIME HISTORY OF  
POOL DISPLACEMENT

NINE MILE POINT, TEST 1



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FIGURE A-241

TIME HISTORY OF  
POOL DISPLACEMENT  
NINE MILE POINT, TEST 2

Time ( from  $T_0$  ) - seconds

5 10 15 20 25 30  
Horizontal Distance from Pool Centerline - inches

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FIGURE A-242

TIME HISTORY OF  
POOL DISPLACEMENT

NINE MILE POINT, TEST 3

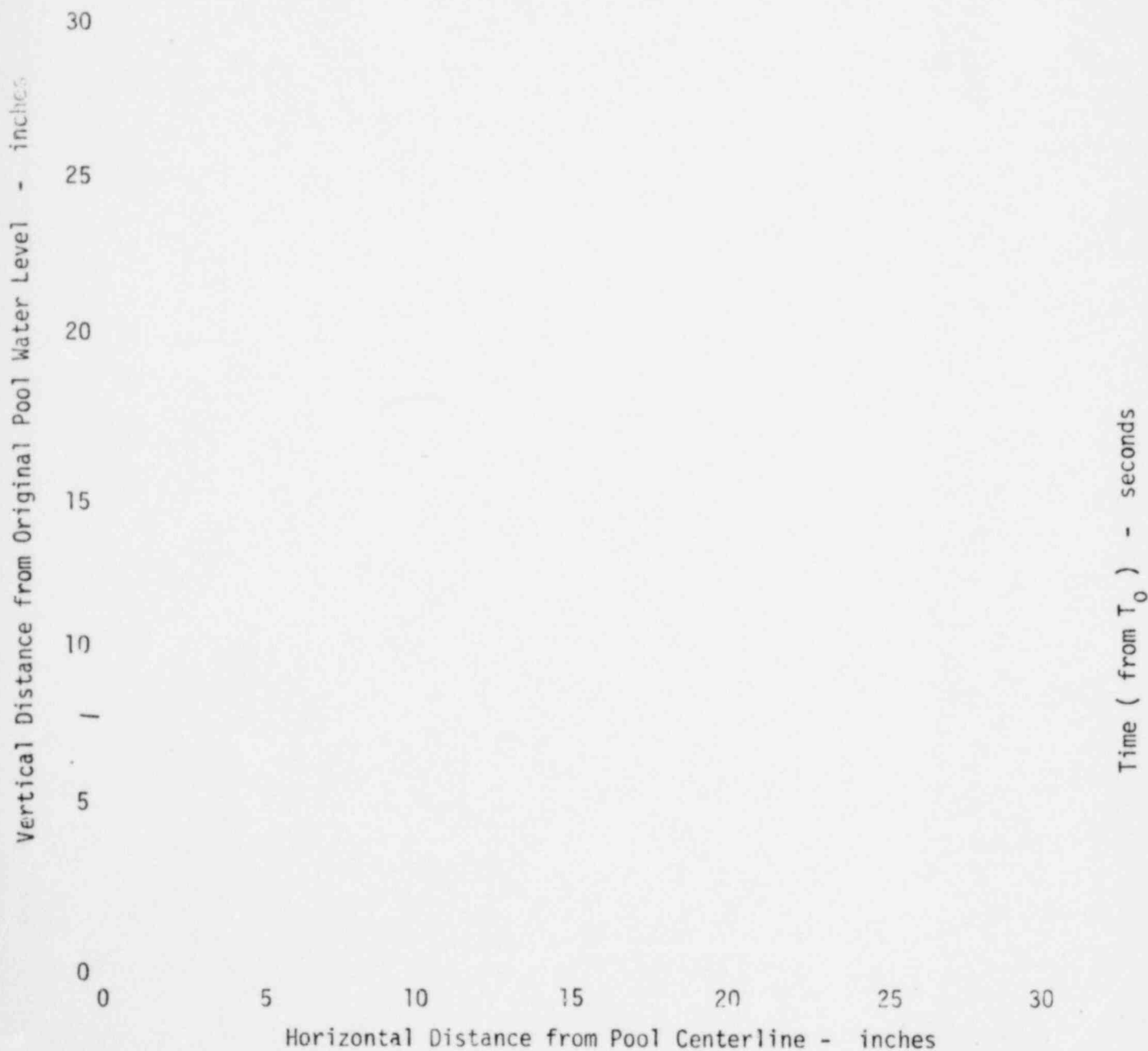


FIGURE A-243

TIME HISTORY OF  
POOL DISPLACEMENT

NINE MILE POINT, TEST 5

Time ( from  $T_0$  ) - seconds

0 5 10 15 20 25 30

Horizontal Distance from Pool Centerline - inches

1349 053

FIGURE A-244

POOL SURFACE DISPLACEMENT

NINE MILE POINT, TESTS 1, 2, 3

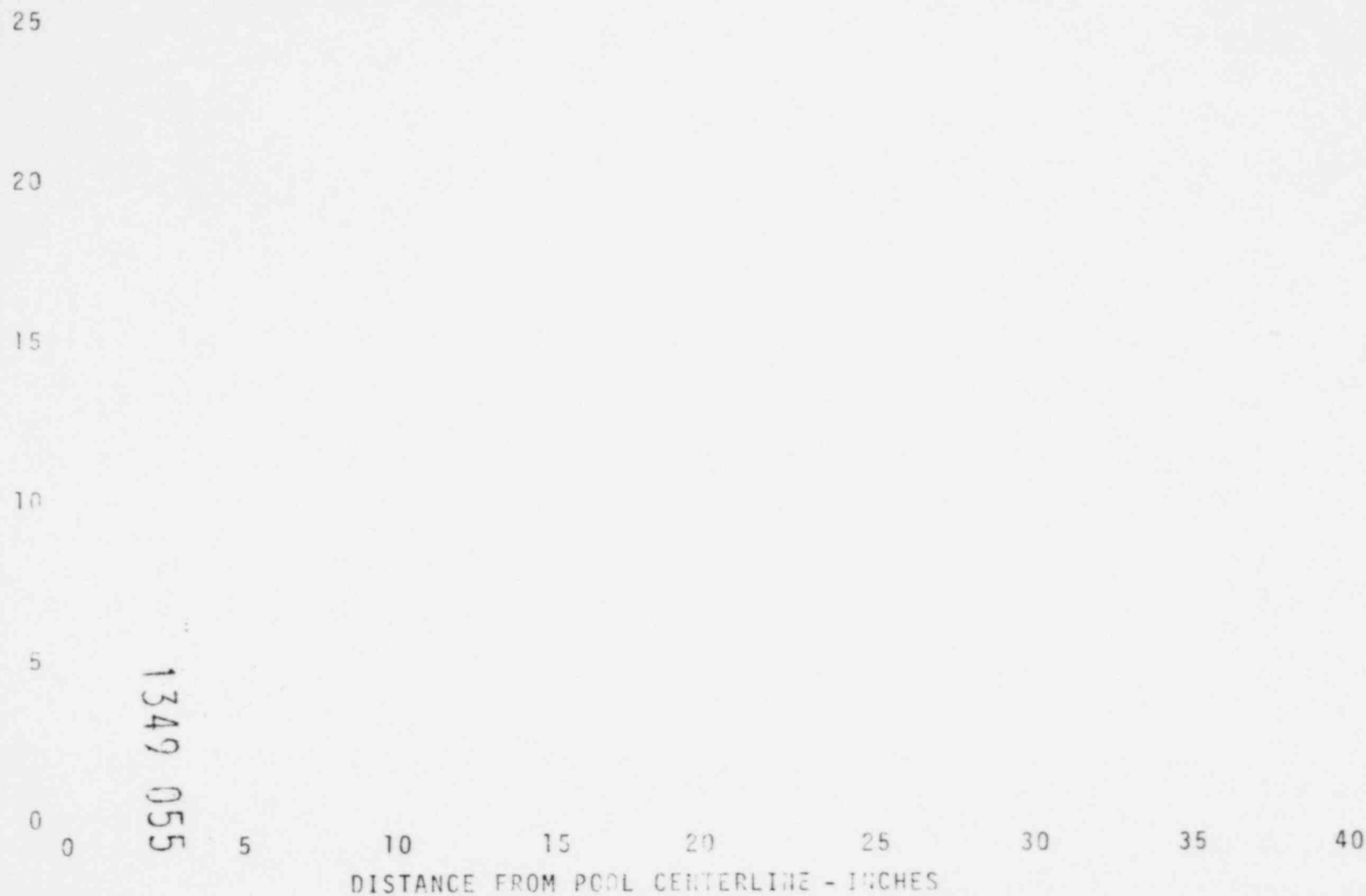


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POOL SURFACE VELOCITY PROFILES

FIGURE A-245

NINE MILE POINT, TESTS 1, 2, 3

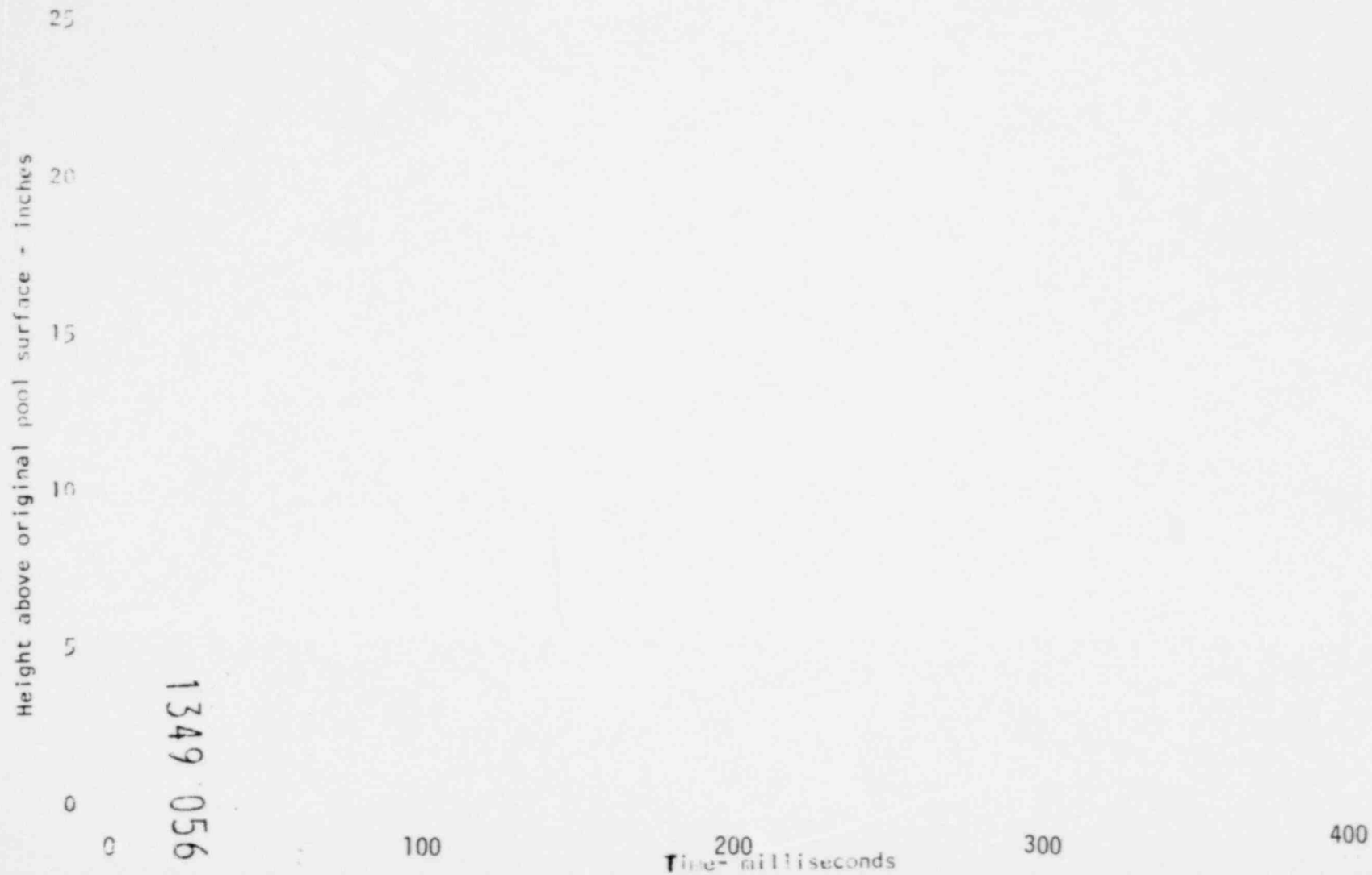


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POOL SURFACE DISPLACEMENT

FIGURE A-246

NINE MILE POINT, TEST 5



POOL SURFACE VELOCITY PROFILES

FIGURE A-247

NINE MILE POINT, TEST 5

25

20

15

10

5

0

0

5

10

15

20

25

30

35

40

DISTANCE FROM POOL CENTERLINE - INCHES

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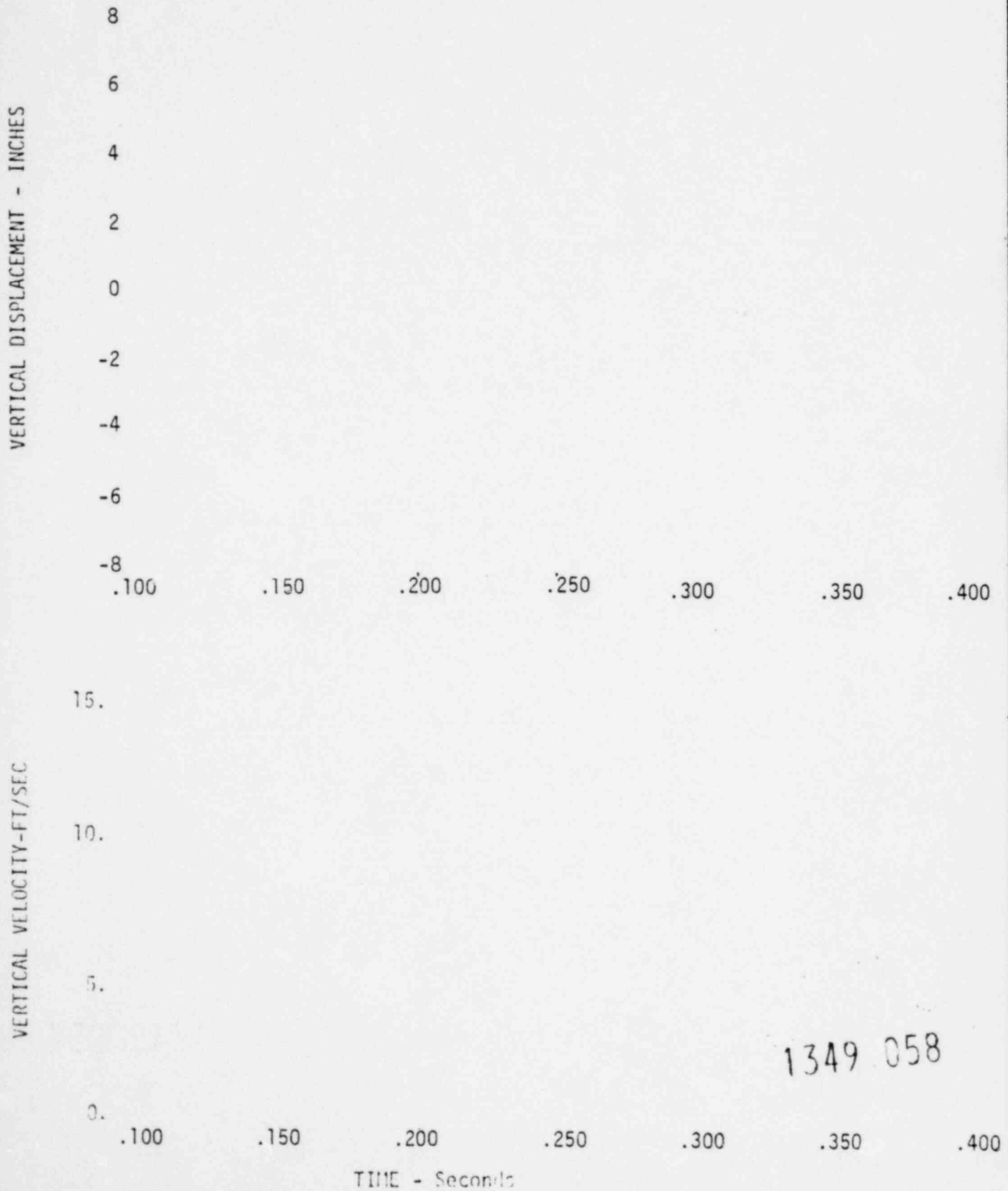
NEDO-21944

A-283  
VELOCITY - FT/SEC

FIGURE A-248

SIDE WINDOW DISPLACEMENT AND VELOCITY PROFILES

NINE MILE POINT, TEST 4

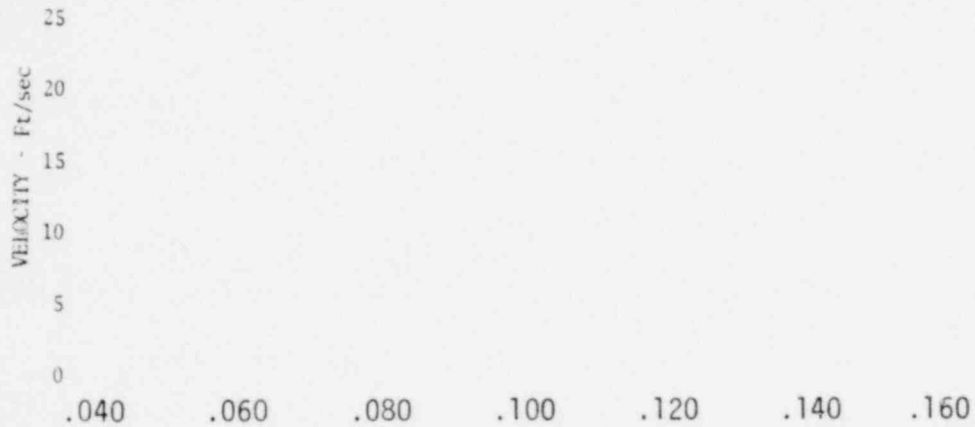
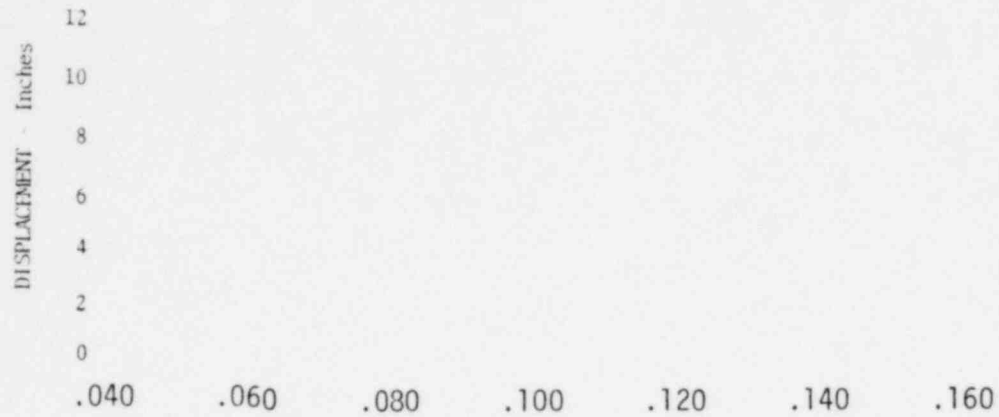


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FIGURE A-249

DOWNCOMER WATER SLUG EJECTION

NINE MILE POINT, TEST 3



Time (from  $T_0$ ) - sec

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DOWNCOMER WATER SLUG EJECTION

NINE MILE POINT, TEST 5

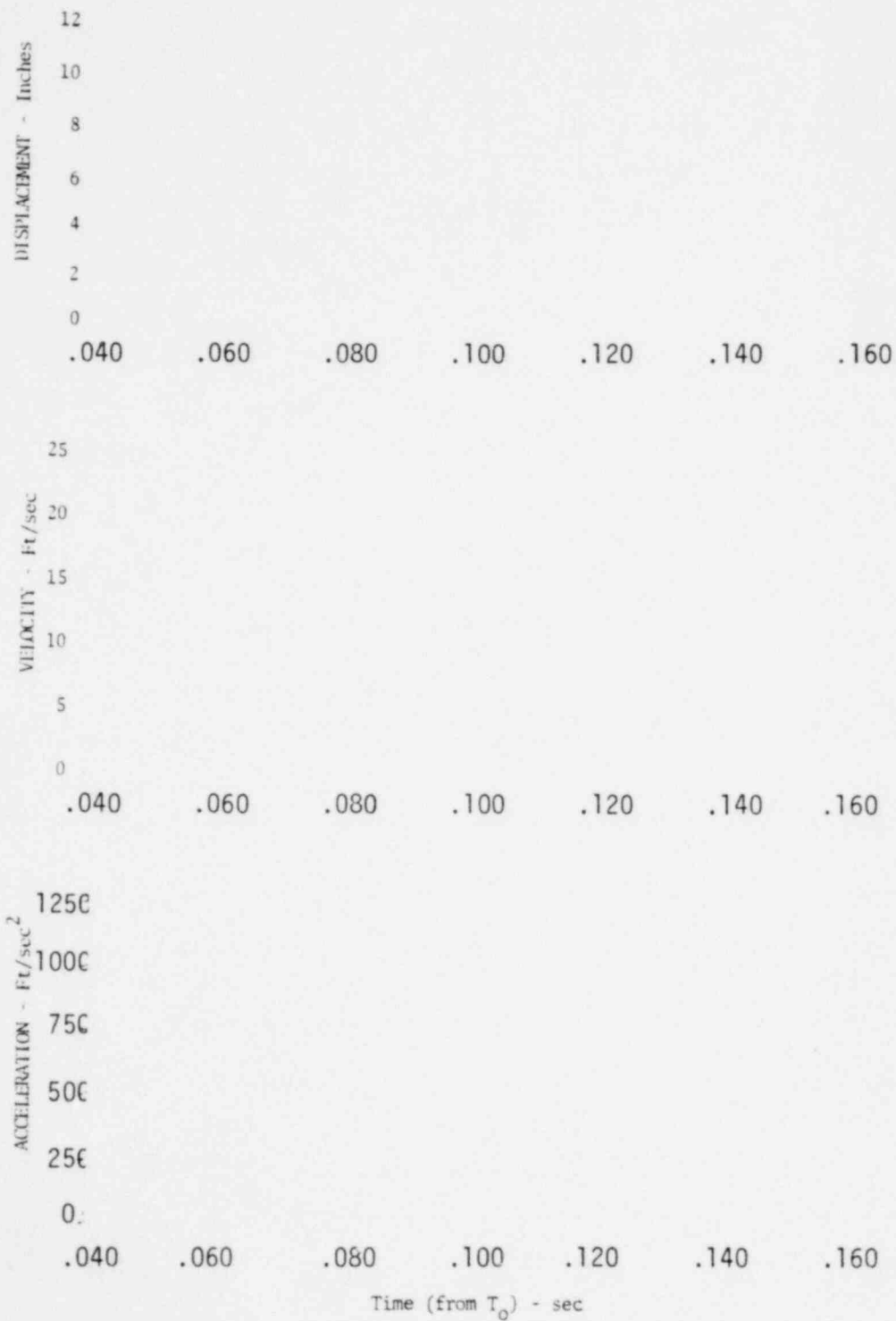


FIGURE A-251  
EFFECT OF DRYWELL/WETWELL  $\Delta P$  ON  
ENTHALPY FLOW INTO POOL  
Nine Mile Point Tests

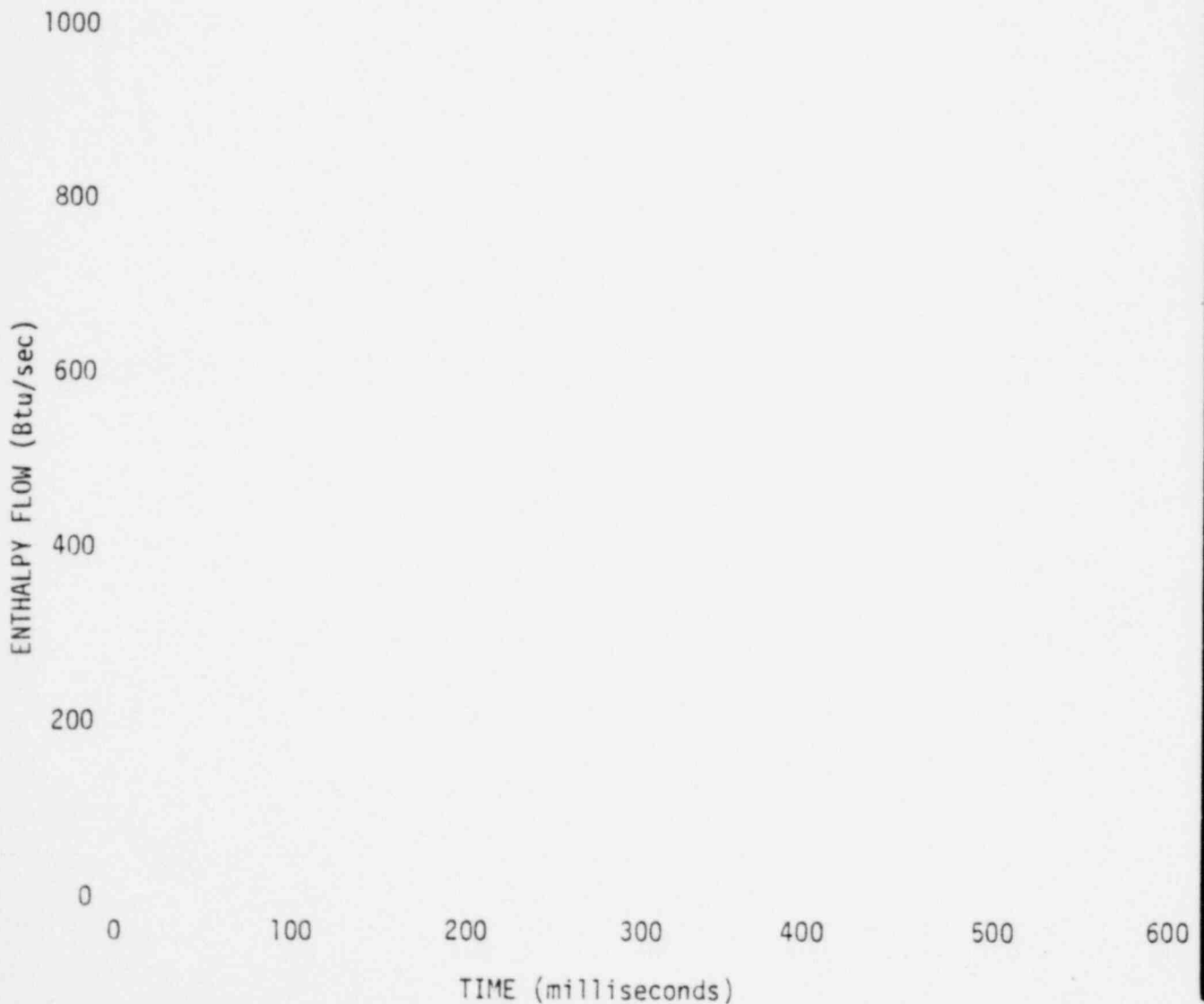


FIGURE A-252

EFFECT OF DRYWELL/WETWELL  $\Delta P$  ON  
DOWNCOMER INTERNAL PRESSURE  
Nine Mile Point Tests

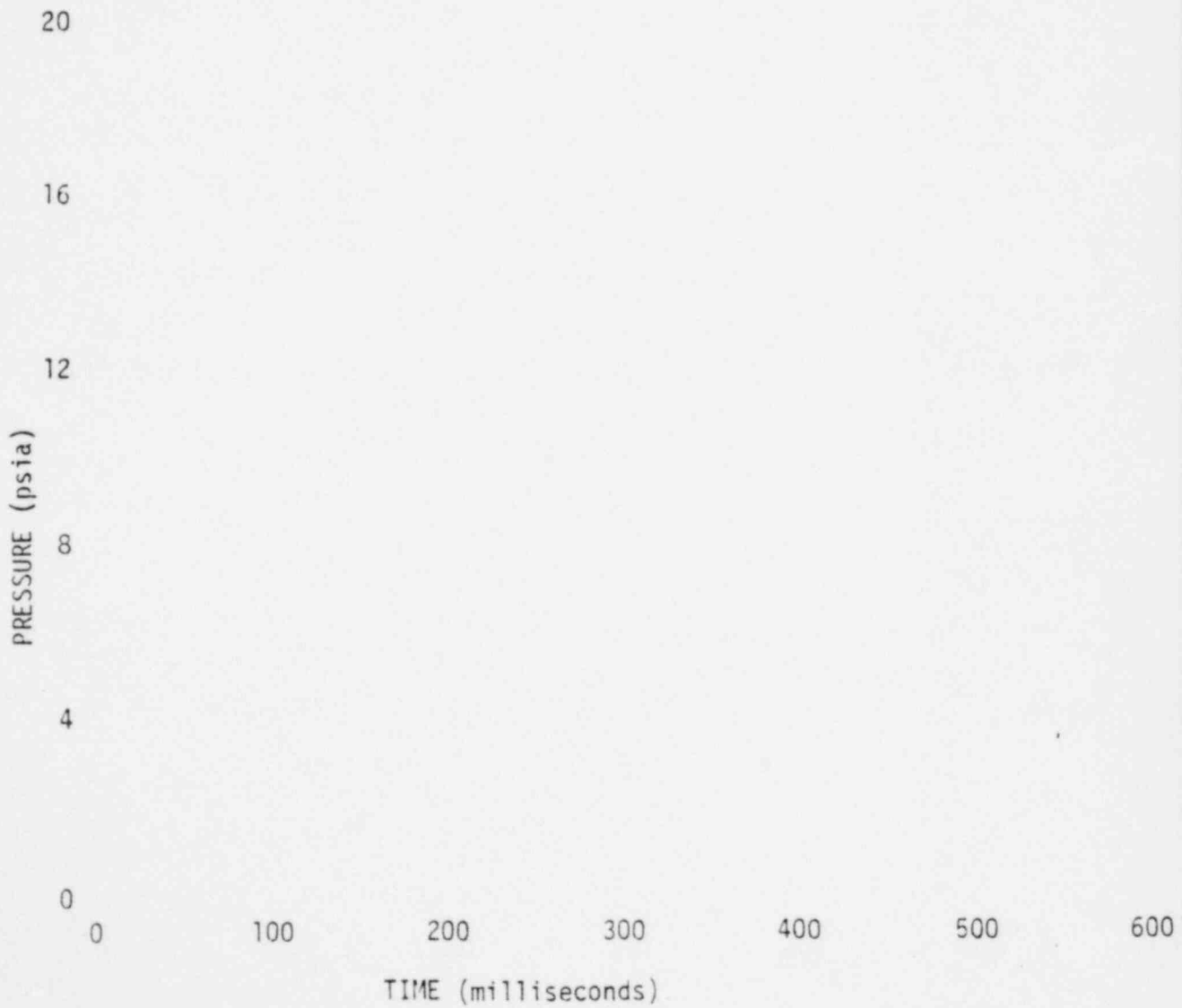


FIGURE A-253

EFFECT OF DRYWELL/WETWELL  $\Delta P$  ON POOL PRESSURE

AT 180 DEGREE AND FREESPACE PRESSURE

Nine Mile Point Tests

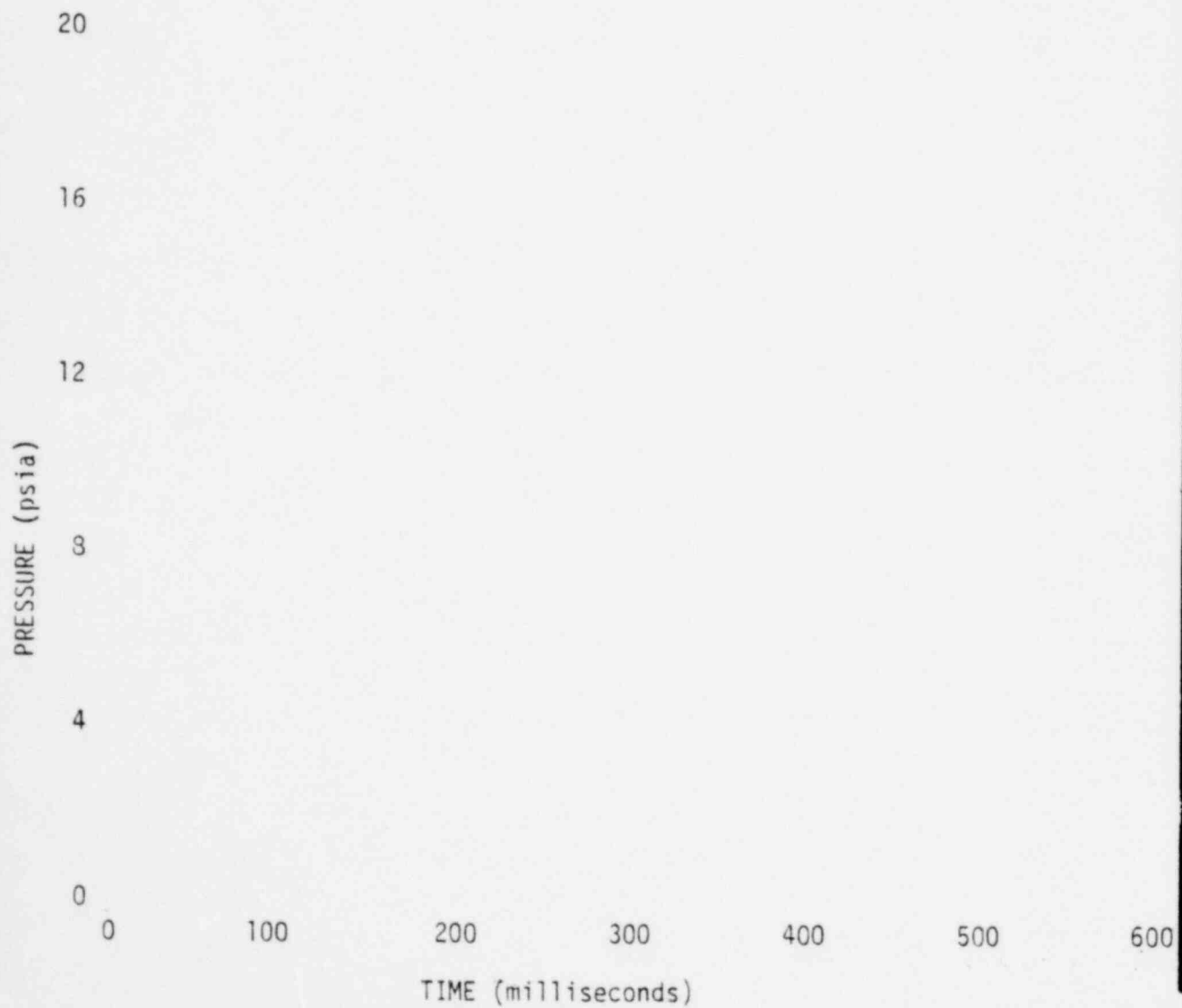


TABLE A-11

## DATA FOR WETWELL VERTICAL LOADS

Task 5.5.3-2 Nine Mile Point Tests

\*Vent clearing time (from  $T_0$ ) determined from the movie films.\*\*Time difference from  $T_0$  to time of zero downforce.

\*(1) Start-of-test reference time

Parameter	Test No.	7.94" $\Delta P$ , 4.55" Pipe Deflector (16" Full Scale)				Std. Dev.	$\frac{0'' \Delta P}{(5)}$
		(1)	(2)	(3)	(4)	Mean	
*(1)							
$T_0$	(sec)						
Vent Clearing Time*	(sec)						
Peak Downforce							
Pressure Integral:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
Corrected Pressure Integral:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
Corrected Load Cell:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
Downforce Valley							
Pressure Integral:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
Corrected Pressure Integral:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
Corrected Load Cell:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
2nd Peak Downforce							
Pressure Integral:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
Corrected Pressure Integral:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
Corrected Load Cell:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
[ $\Delta t$ ] Downforce Time**							
Pressure Integral	(sec)						
Corrected Pressure Integral	(sec)						
Corrected Load Cell	(sec)						
Downforce Impulse							
Pressure Integral:							
Impulse	(lb-sec)						

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TABLE A-11

\*Time at force is zero (from  $T_0$ )

DATA FOR WETWELL VERTICAL LOADS (continued)

Task 5.5.3-2 Nine Mile Point Tests

Parameter	Test No.	7.94" ΔP, 4.59" Pipe Deflector (16" Full Scale)					Std.	0" ΔP
		(1)	(2)	(3)	(4)	Mean	Dev.	(5)
<u>Peak Upforce</u>								
Pressure Integral:								
Force	(1b)							
Time (from T <sub>0</sub> )	(sec)							
Corrected Pressure Integral:								
Force	(1b)							
Time (from T <sub>0</sub> )	(sec)							
Corrected Load Cell:								
Force	(1b)							
Time (from T <sub>0</sub> )	(sec)							
<u>Upforce Valley</u>								
Pressure Integral:								
Force	(1b)							
Time (from T <sub>0</sub> )	(sec)							
Corrected Pressure Integral:								
Force	(1b)							
Time (from T <sub>0</sub> )	(sec)							
Corrected Load Cell:								
Force	(1b)							
Time (from T <sub>0</sub> )	(sec)							
<u>2nd Peak Upforce</u>								
Pressure Integral:								
Force	(1b)							
Time (from T <sub>0</sub> )	(sec)							
Corrected Pressure Integral:								
Force	(1b)							
Time (from T <sub>0</sub> )	(sec)							
Corrected Load Cell:								
Force	(1b)							
Time (from T <sub>0</sub> )	(sec)							
<u>Zero Force Time*</u>								
Pressure Integral	(sec)							
Corrected Pressure Integral	(sec)							
Corrected Load Cell	(sec)							

TABLE A-12

DATA FOR VENT HEADER IMPACT LOADS

Task 5.5.3-2 Nine Mile Point Tests

Parameter \ Test No.	<u>7.94" <math>\Delta P</math>, 4.60" Deflector</u>				Mean	<u>0" <math>\Delta P</math></u>	
	( 1 )	( 2 )	( 3 )	( 4 )		Std. Dev.	( 5 )
$T_0^+$ (sec)							
<u>Vent Header Impact</u>							
Pressure Integral:							
Maximum Force (lb)							
Impulse (lb-sec)							
Duration* (sec)							
Load Cell Corrected: $^{++}$							
Maximum Force (lb)							
Impulse (lb-sec)							
Duration (sec)							
Pool Surface Velocity (ft/sec)							
Time (from $T_0$ )** (sec)							

\*Based on impact pressure measurements

\*\*At start of the first impact pressure recorded.

 $^+$ Start of test reference time $^{++}$ represents peak of very noisy data (acceleration corrected); mean value would be lower

## A.6 Brunswick Tests

### A.6.1 Typical Data

Time-history plots of the driving conditions and pool response are presented in this section for Brunswick Test 3. Test 3 was a load definition test, conducted without an initial drywell/wetwell differential pressure (0"  $\Delta P$ ) and with a 5.34 inch pipe deflector (20 inch full scale).  $\Delta P$  sensitivity test was not conducted for Brunswick.

#### A.6.1.1 Driving Conditions

Driving conditions for Brunswick Test 3 are presented in Figures A-254 through A-258. Brunswick's driving conditions had the same characteristics as the "typical" plant discussed in Section 3.0 of this report.

#### A.6.1.2 Pool Response

Downcomer internal pressure and wetwell pressures for Brunswick Test 3 are presented in Figures A-259 and A-260. These pressure plots have the same characteristics as the "typical" plant in Section 3.0.

Figure A-261 presents net torus force based on the torus pressure integral for Brunswick Test 3. The net torus force shows relatively smooth downforce except for the first oscillation and shows some upforce oscillation.

The net torus force which was determined by applying the inertial correction from the torus accelerometer (Figure A-262) to the torus load cell (Figure A-263) is compared with the torus force obtained from the torus pressure integral in Figure A-264. Figure A-265 presents the net torus force based on the torus pressure integral corrected for inertia.

The "average" pool pressure for Brunswick Test 3 is shown in Figure A-266. Figure A-267 is the same as Figure A-265 with force replaced by average pressure (force/torus projected area).

The vent header impact pressures for Brunswick Test 3 are presented in Figures A-268 through A-271. These figures indicate that the deflector was effective in reducing the peak local vent header impact pressure.

Figure A-272 presents a comparison of the vent header impact force derived from the pressure integral with that derived from the corrected load cell. Vent header vertical acceleration is shown in Figure A-273.

#### A.6.2 Pool Dynamics

The pool contours at various times of pool swell are shown in Figures A-274 through A-276 for Brunswick Tests 1, 2, and 3.

The pool surface displacement curves for Tests 1, 2, and 3 are shown on Figure A-277. The pool surface velocities for Tests 1, 2, and 3 are shown on Figure A-278.

The pool surface displacements and velocity profile viewed from the side window during Test 4 are shown in Figure A-279. The down comer water slug displacement, velocity, and acceleration versus time for Test 3 are presented in Figure A-280.

Brunswick pool dynamics are similar to those of the "typical" plant discussed in Section 3.0.

#### A.6.3 Data Summaries

Table A-13 presents the Brunswick Test Data for wetwell vertical forces.

Table A-14 presents the Nine Mile Point test data for vent header impact forces.

#### A.6.4 Discussion and Analysis

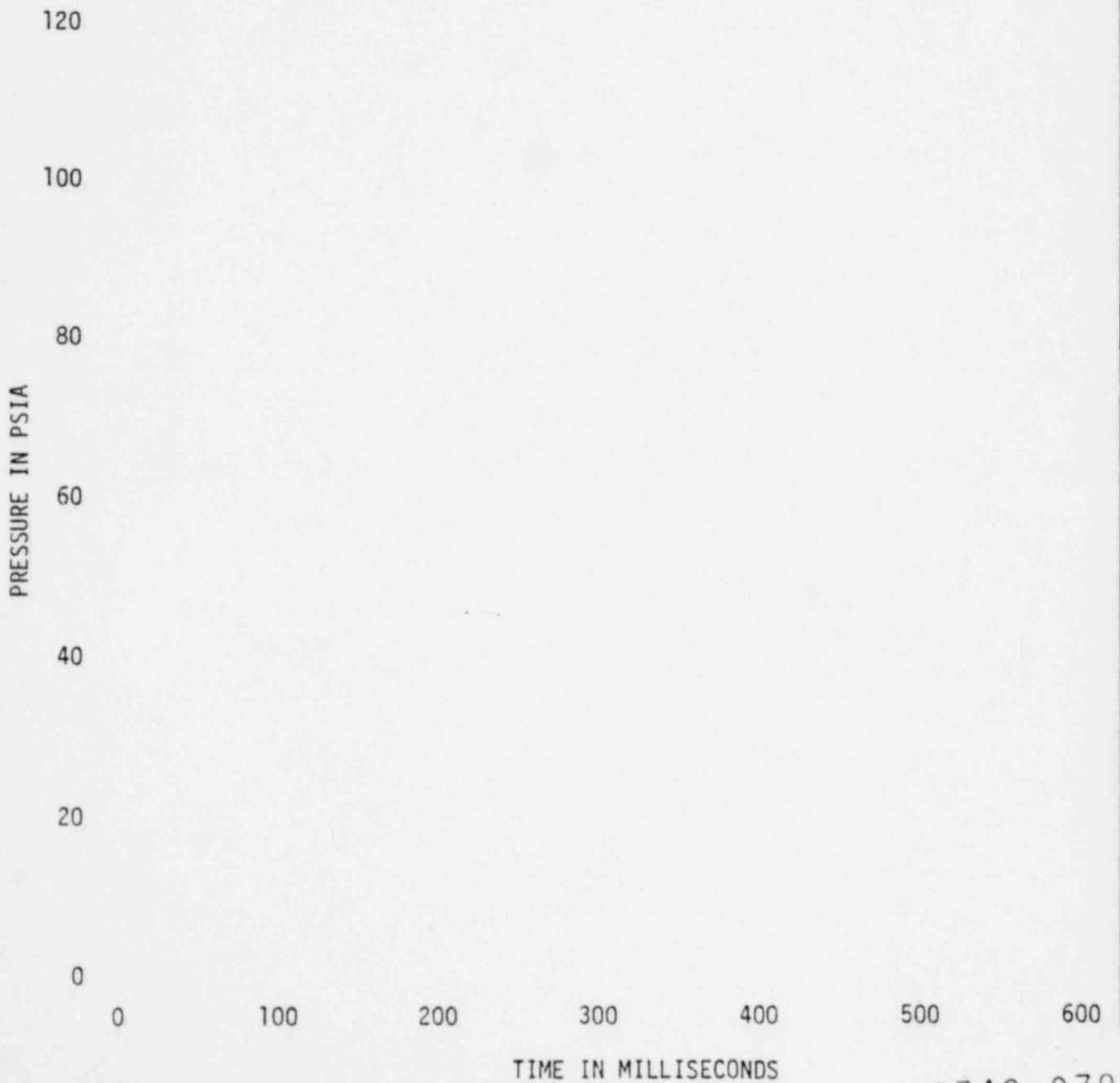
The load definition tests were conducted at zero  $\Delta P$  and with a pipe deflector installed below the vent header.  $\Delta P$  sensitivity test (at a partial or full  $\Delta P$ ) was not conducted for Brunswick. The downforce was relatively smooth except for the first oscillation. The upforce showed some oscillation, which is a characteristic of the type II (30° bend) downcomers. The pipe deflector (20 inch full scale) effectively reduced the vent header impact force.

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FIGURE A-254

DRYWELL ORIFICE UPSTREAM PRESSURE

Task 5.5.3-2 Brunswick Test 3



1349 070

FIGURE A-255

DRYWELL PRESSURE

Task 5.5.3-2 Brunswick Test 3



FIGURE A-256

DOWNCOMER ORIFICE DIFFERENTIAL PRESSURE

Task 5.5.3-2 Brunswick Test 3

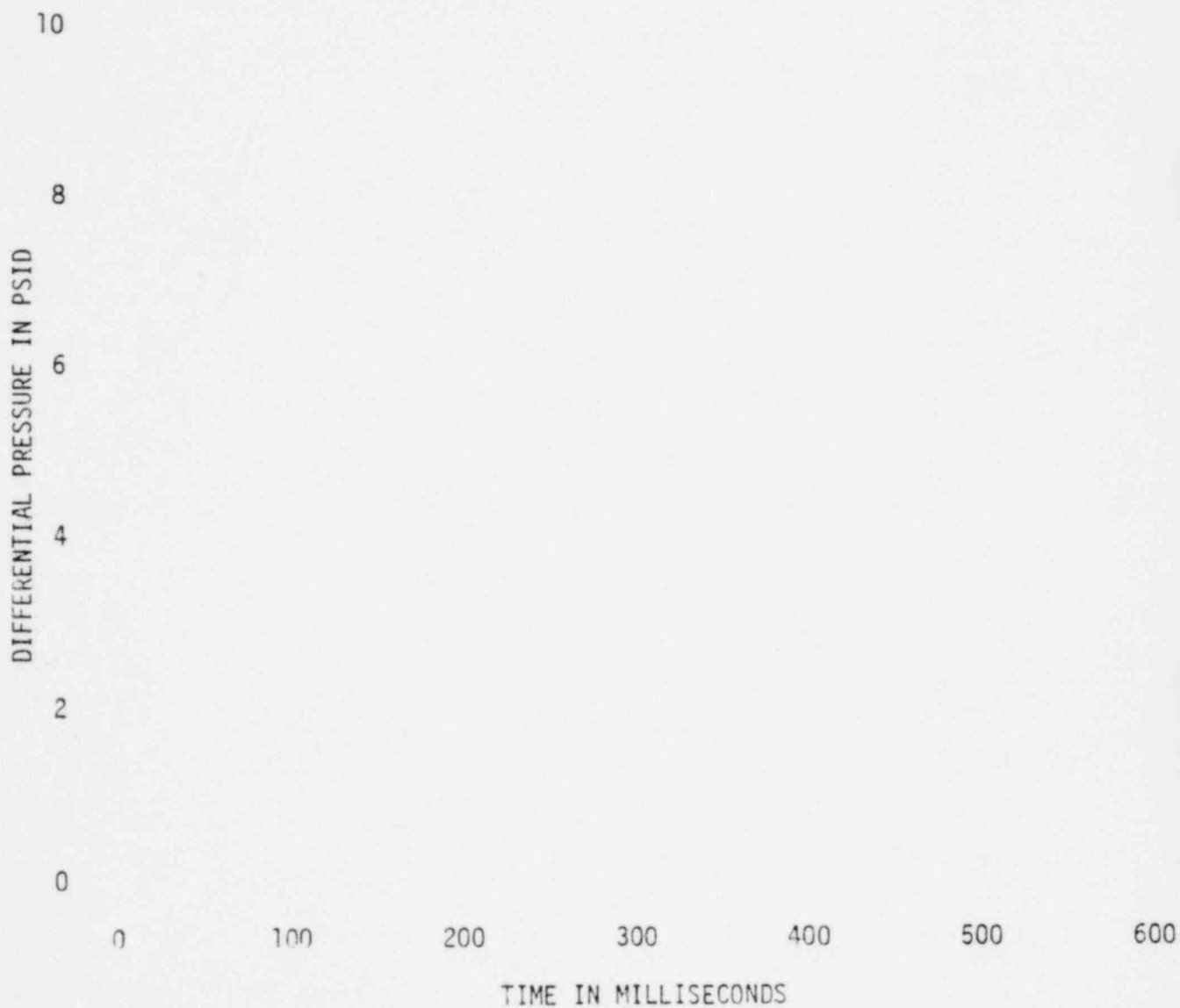
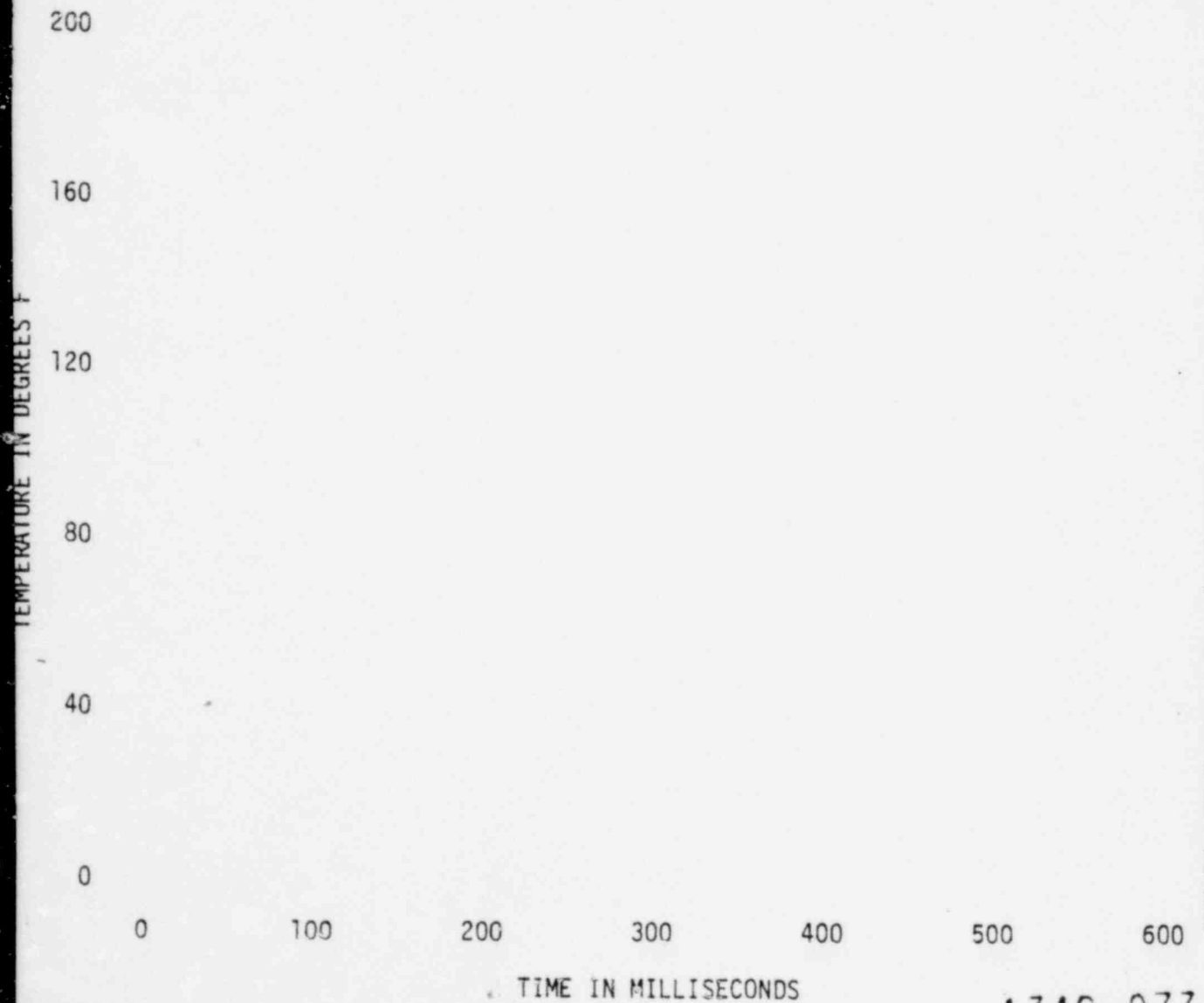


FIGURE A-257

DOWNCOMER ORIFICE UPSTREAM TEMPERATURE

Task 5.5.3-2 Brunswick Test 3



1349 073

FIGURE A-258

ENTHALPY FLOW INTO POOL

Task 5.5.3-2 Brunswick Test 3

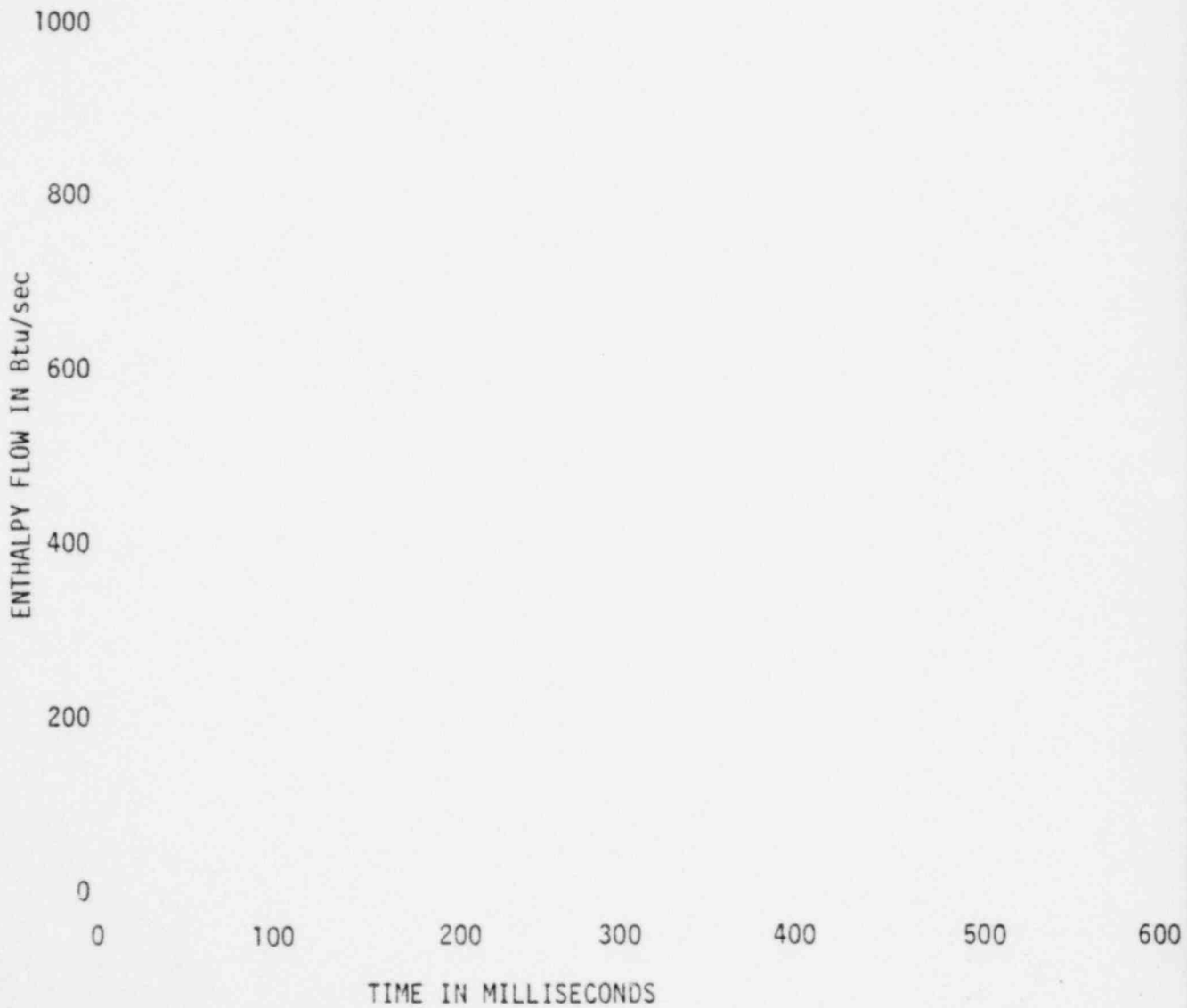


FIGURE A-259

DOWNCOMER INTERNAL PRESSURE

Task 5.5.3-2 Brunswick Test 3



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FIGURE A-260

WETWELL PRESSURES

Task 5.5.3-2 Brunswick Test 3

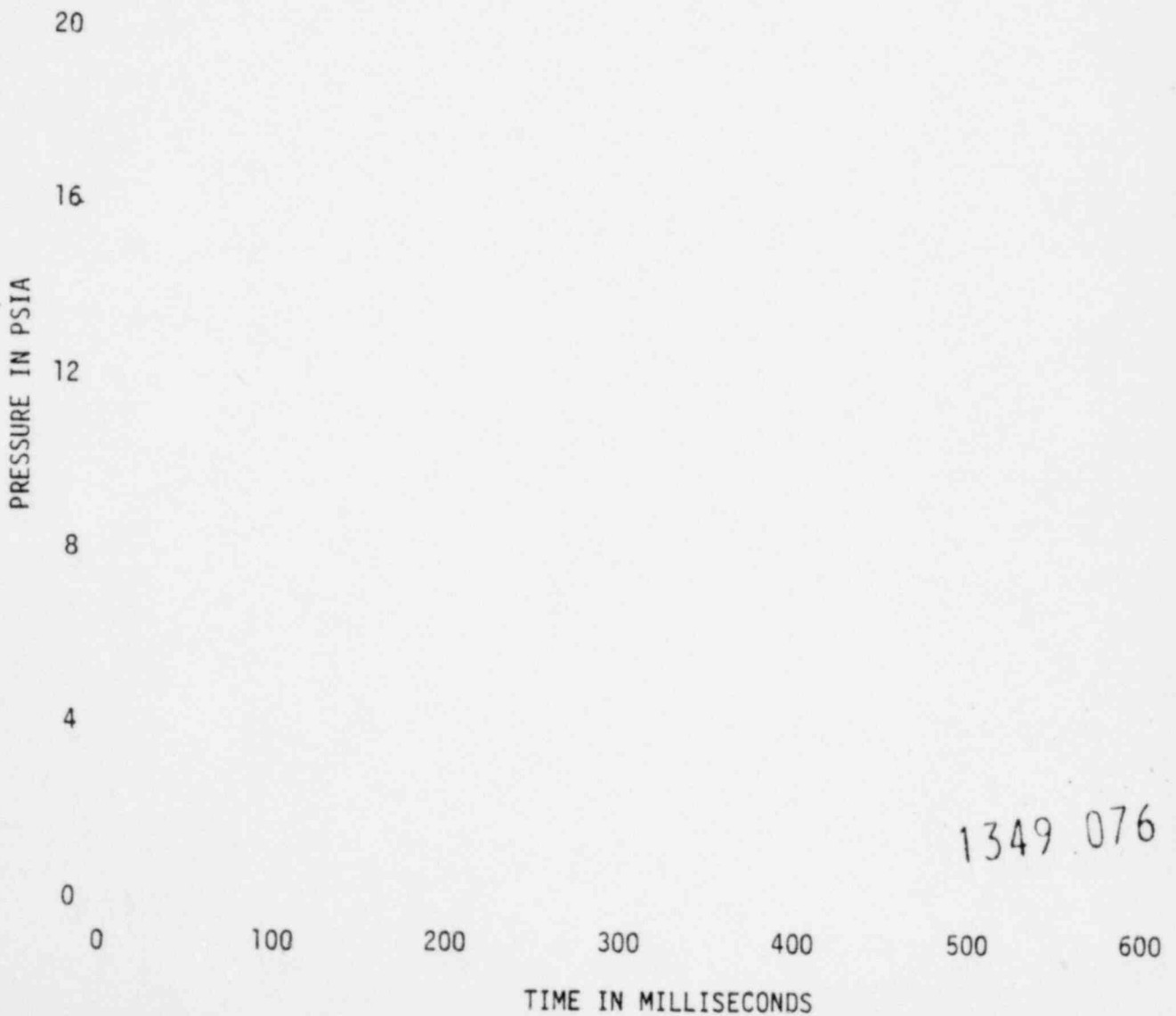


FIGURE A-261

NET TORUS FORCE FROM PRESSURE INTEGRAL

Task 5.5.3-2 Brunswick Test 3

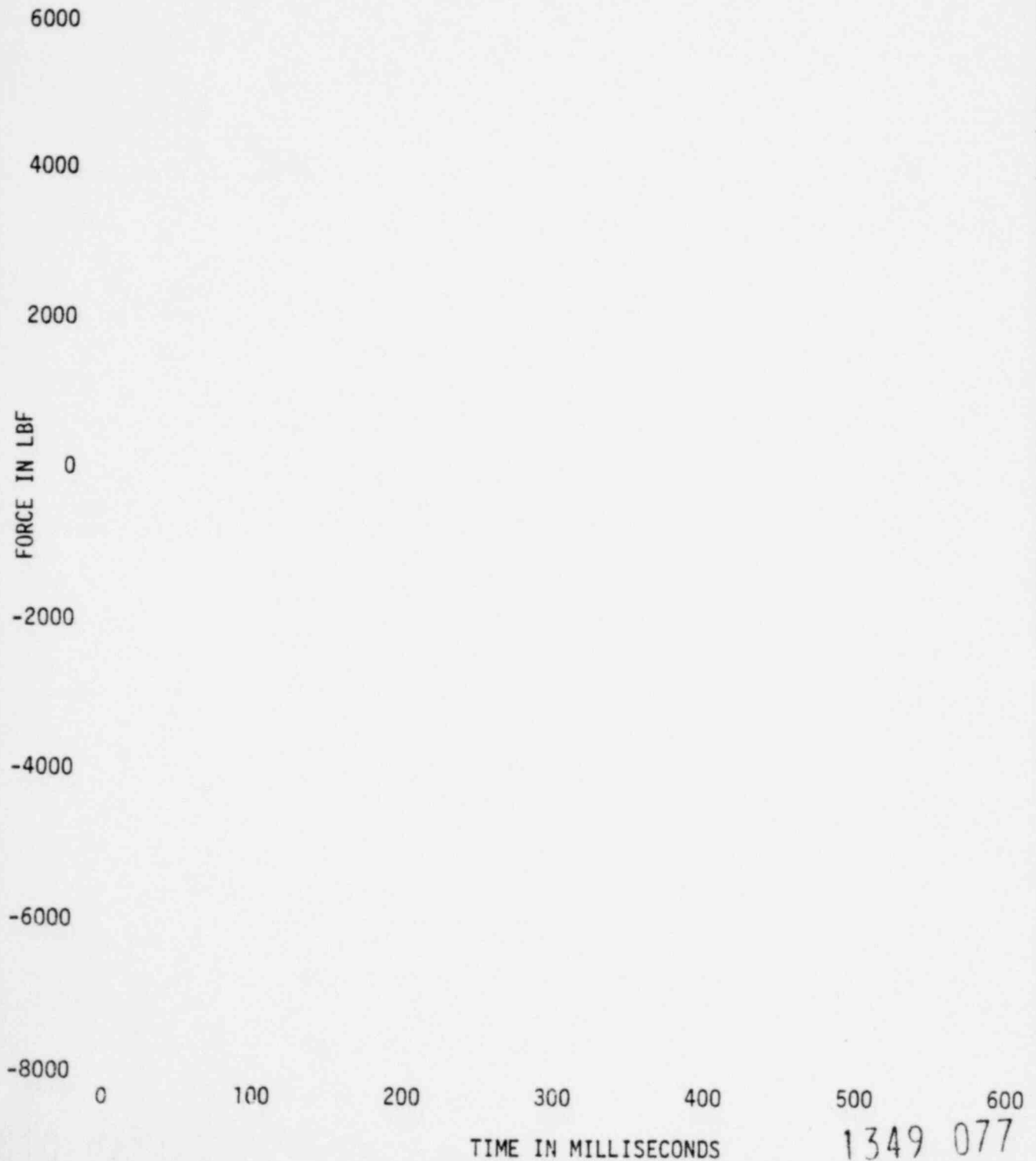
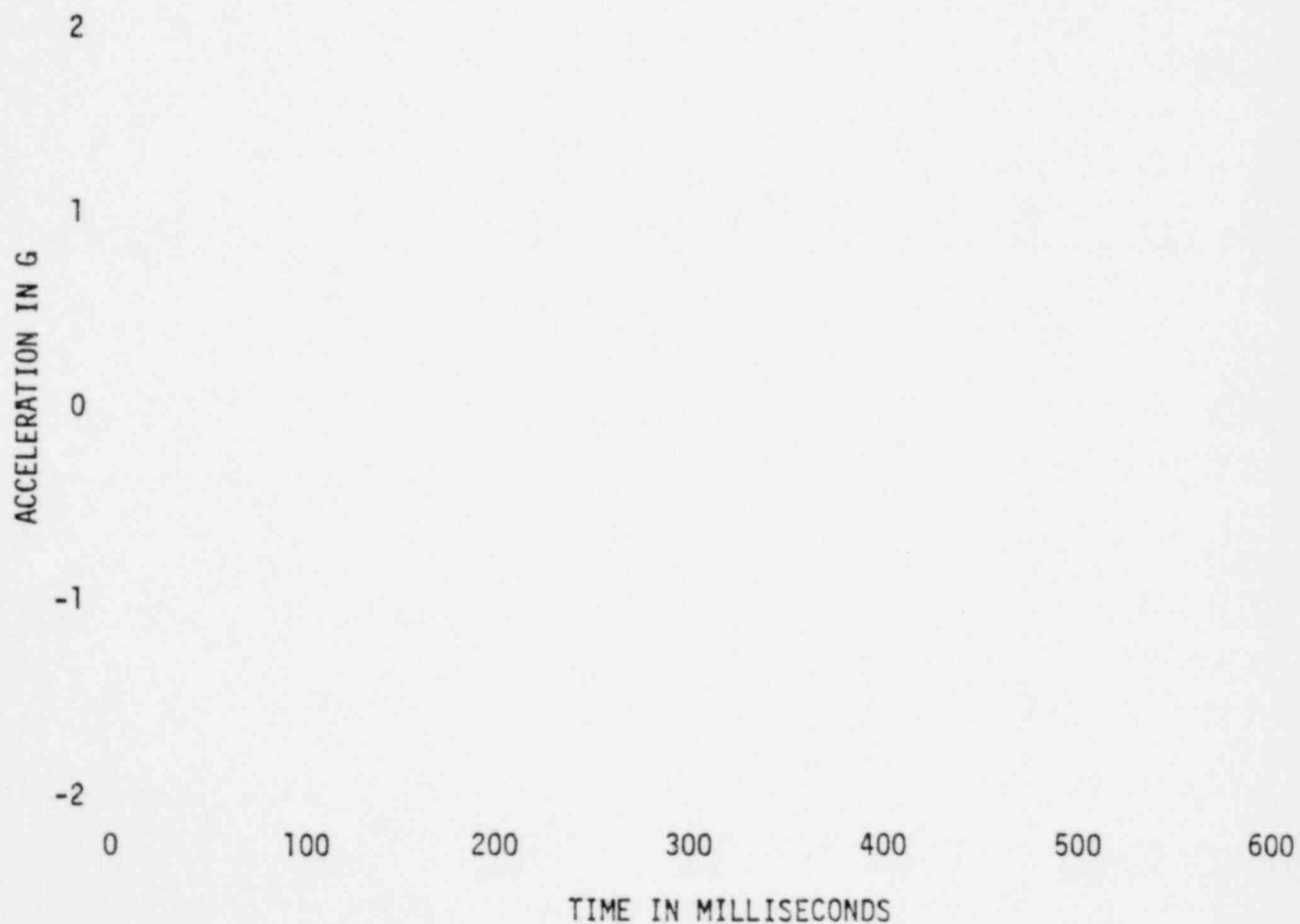


FIGURE A-262

TORUS VERTICAL ACCELERATION

Task 5.5.3-2 Brunswick Test 3

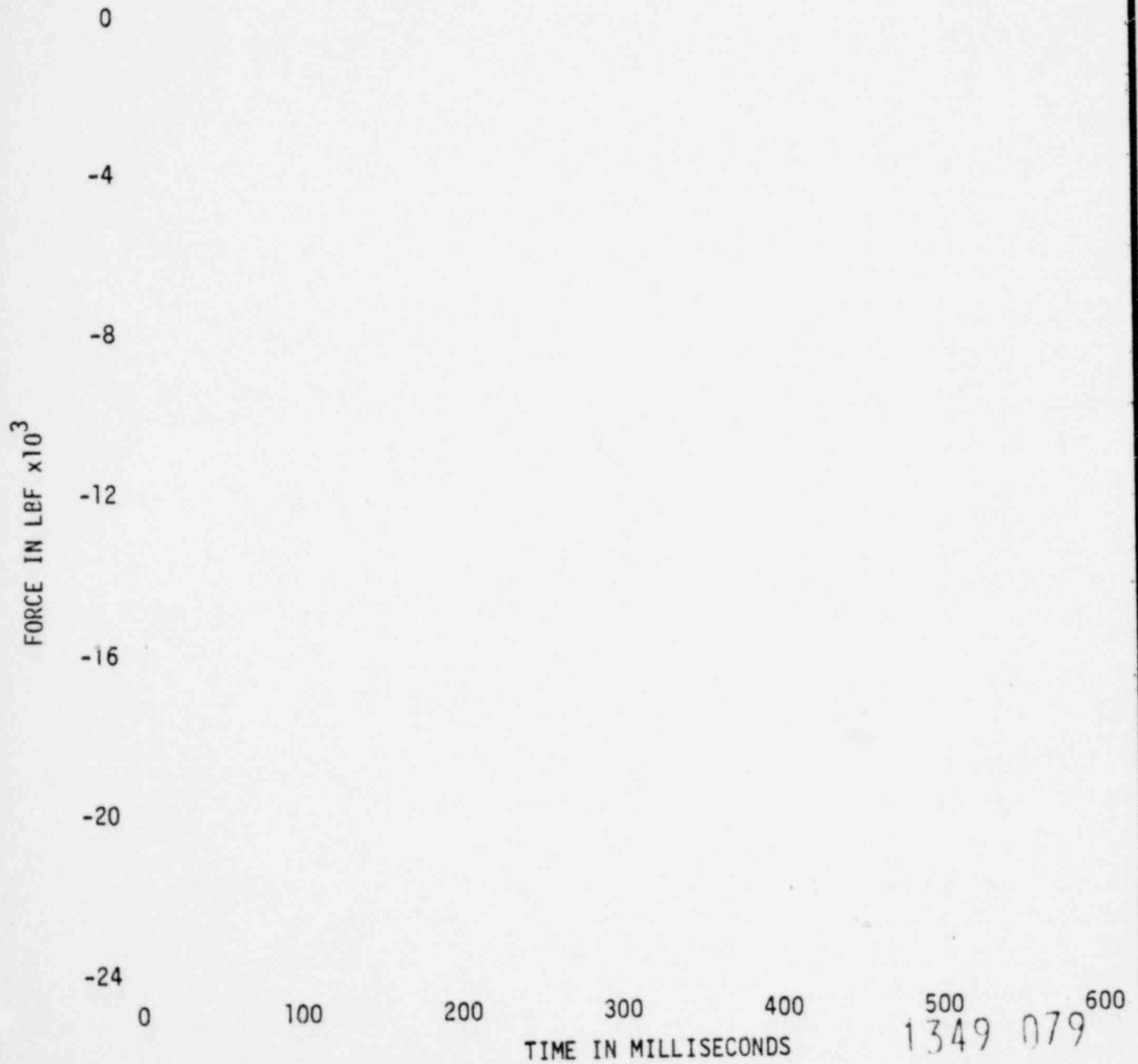


1349 078

FIGURE A-263

TORUS LOAD CELL

Task 5.5.302 Brunswick Test 3

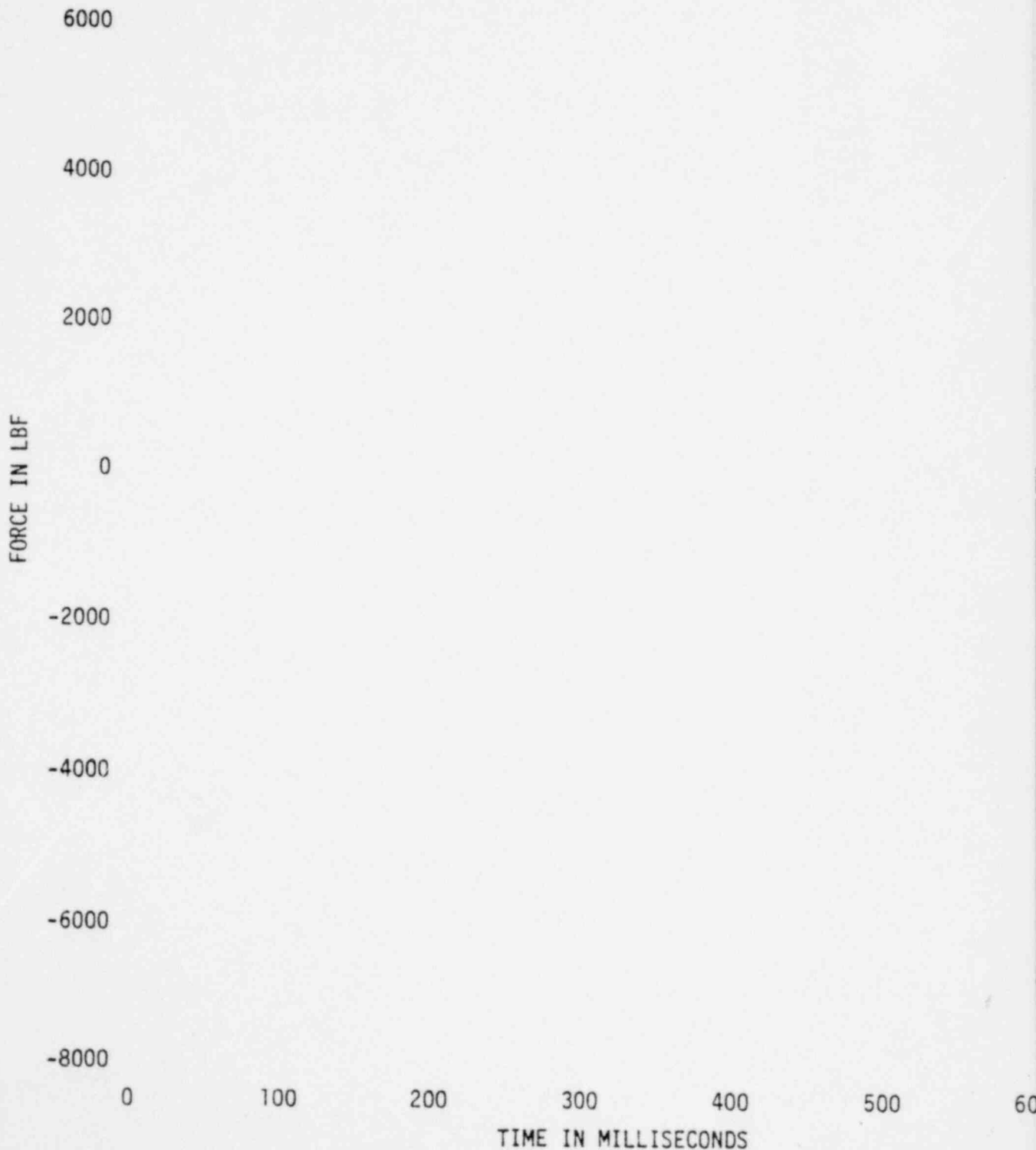


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FIGURE A-264

COMPARISON OF NET TORUS FORCE FROM PRESSURE INTEGRAL  
WITH NET TORUS FORCE FROM LOAD CELL CORRECTED FOR TORUS INERTIA

Task 5.5.3-2 Brunswick Test 3



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FIGURE A-265

NET TORUS FORCE FROM PRESSURE INTEGRAL, CORRECTED FOR WATER INERTIA

Task 5.5.3-2 Brunswick Test 3



A-307

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FIGURE A-266

AVERAGE POOL PRESSURE, CORRECTED FOR WATER INERTIA

Task 5.5.3-2 Brunswick Test 3

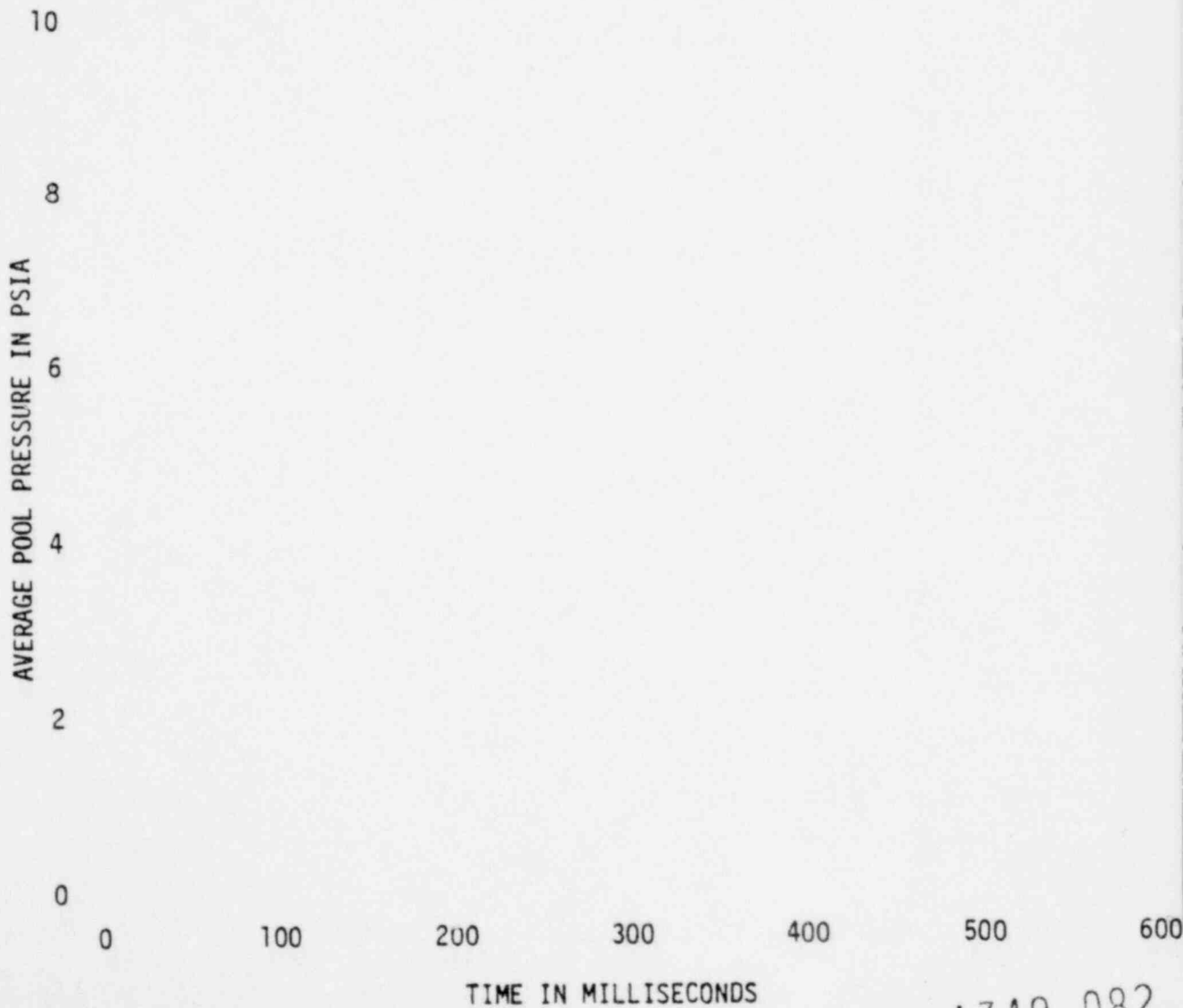
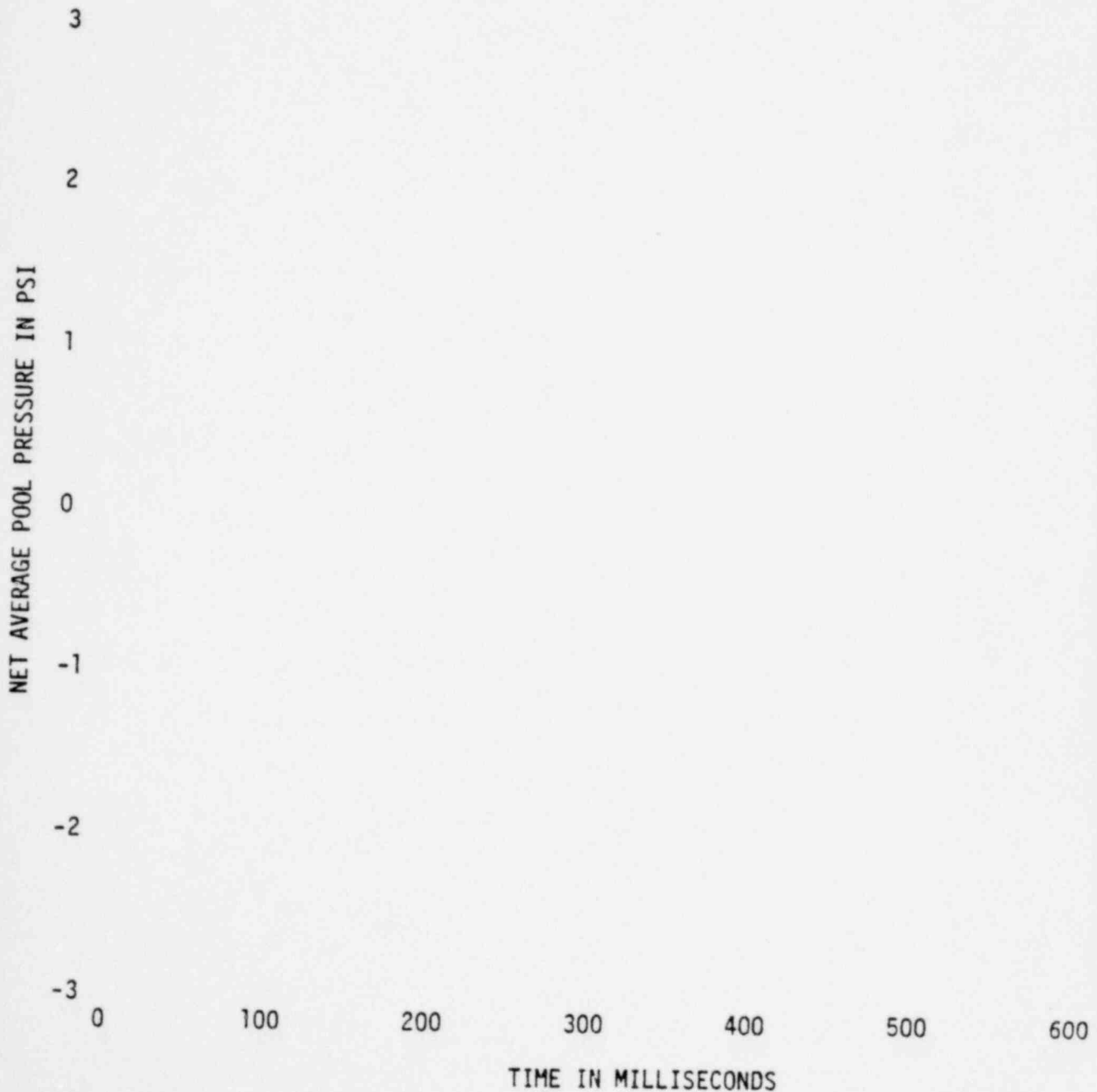


FIGURE A-267

NET AVERAGE POOL PRESSURE, CORRECTED FOR WATER INERTIA

Task 5.5.3-2 Brunswick Test 3

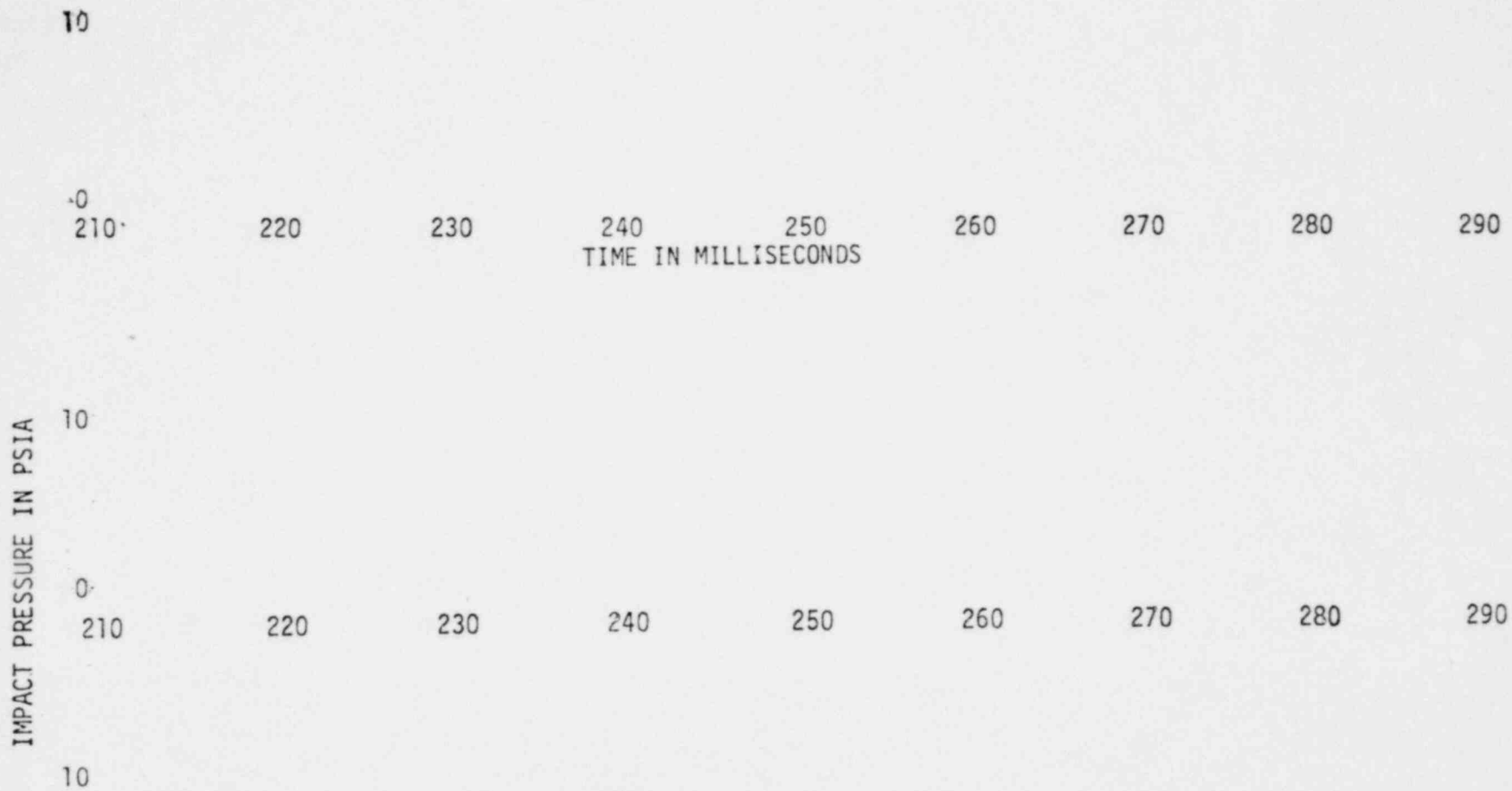


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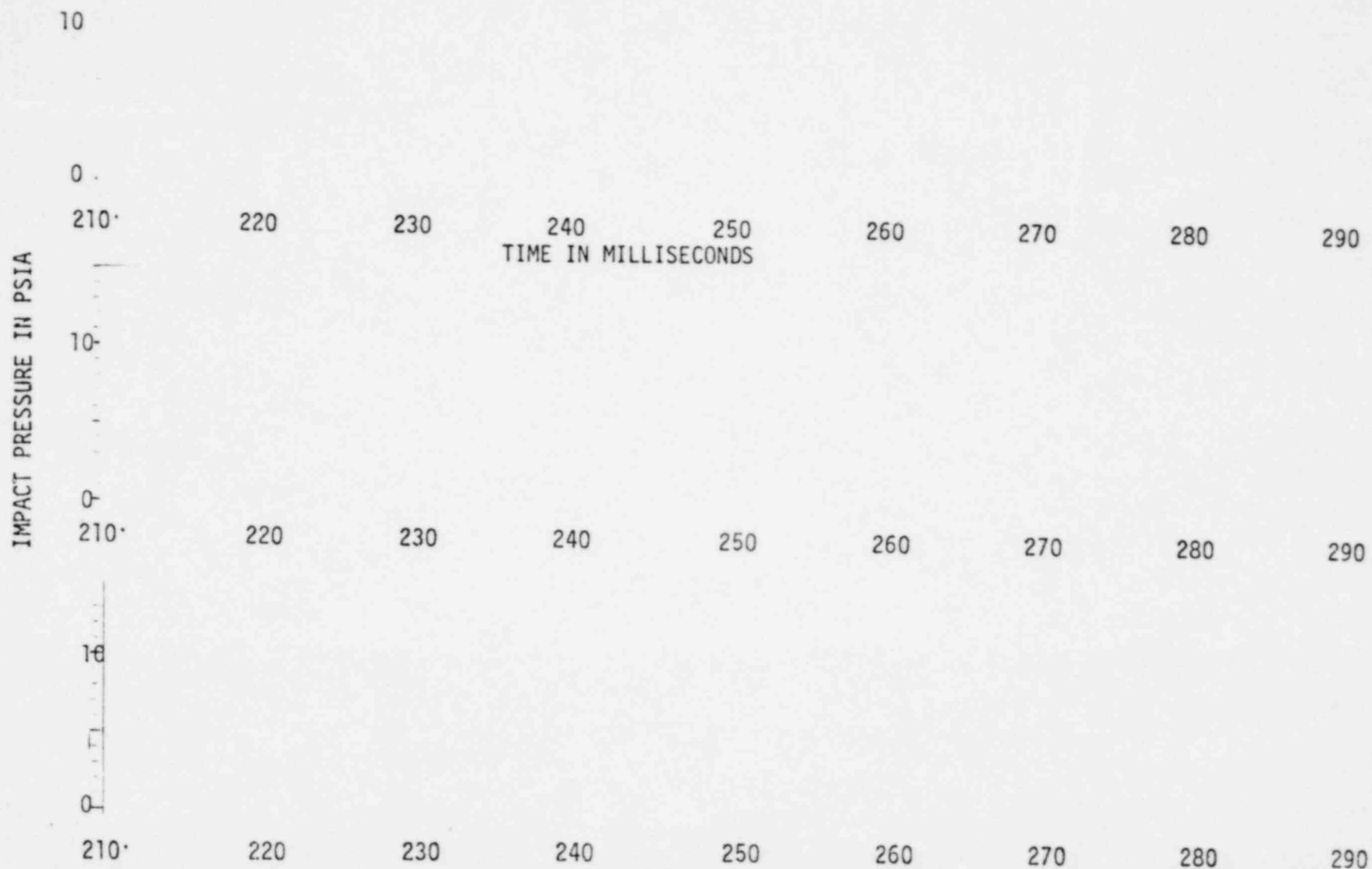
FIGURE A-268

VENT HEADER IMPACT PRESSURES

Task 5.5.3-2 Brunswick Test 3



VENT HEADER IMPACT PRESSURES  
Task 5.5.3-2 Brunswick Test 3



A-311

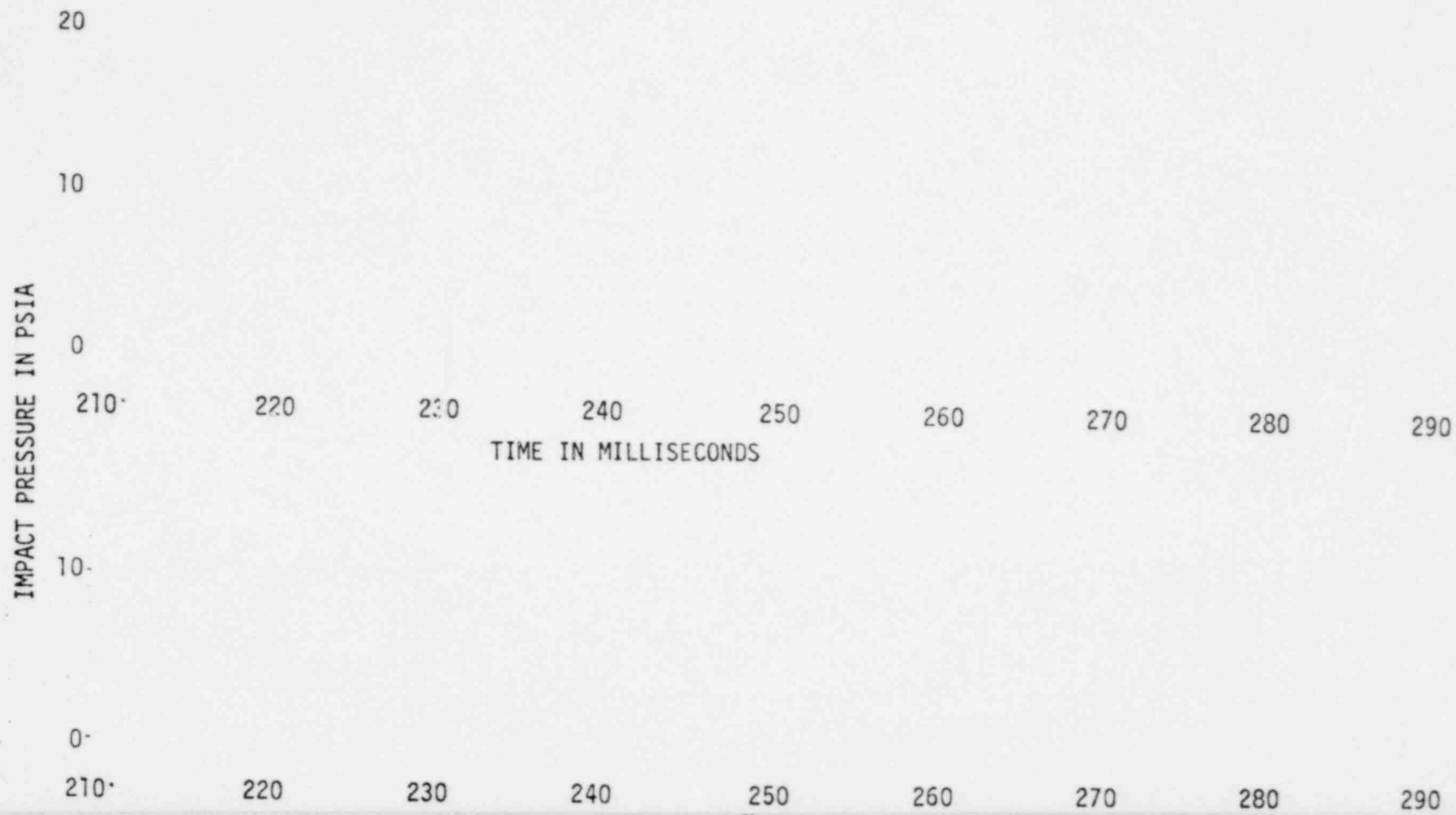
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FIGURE A-270

VENT HEADER IMPACT PRESSURES

Task 5.5.3-2 Brunswick Test 3



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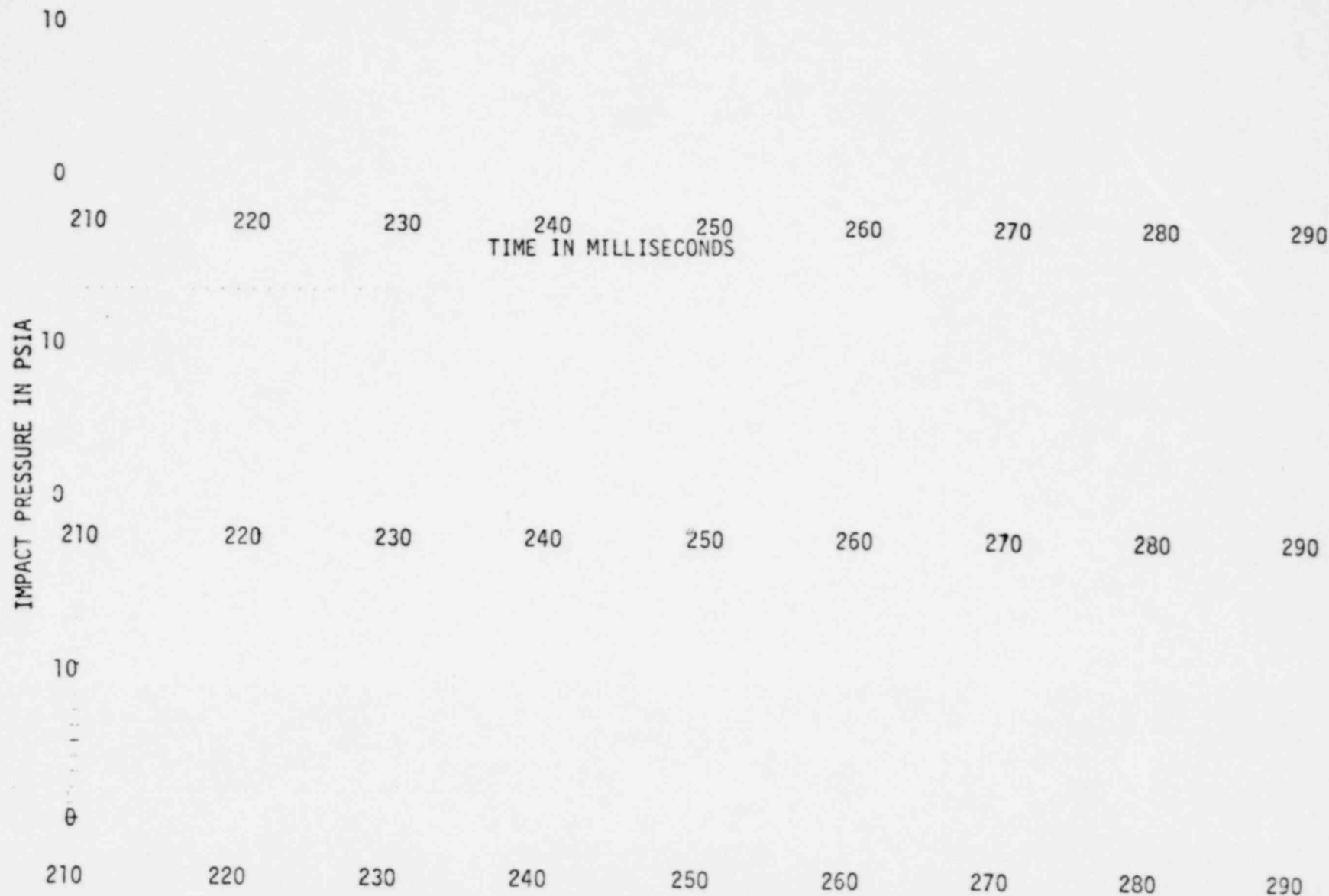
A-312

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VENT HEADER IMPACT PRESSURES  
Task 5.5.3-2 Brunswick Test 3

A-313

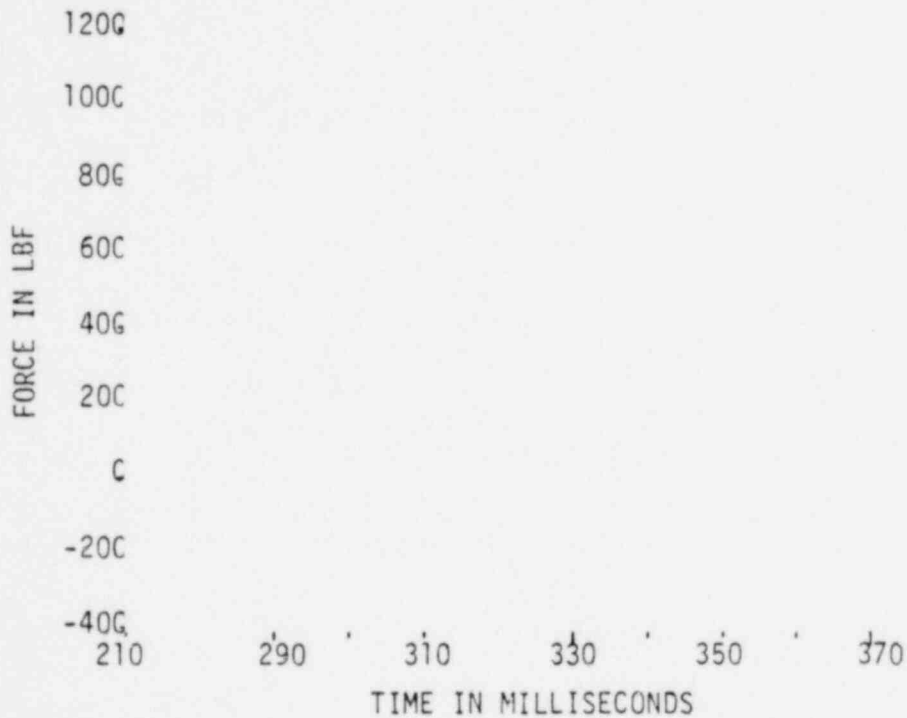
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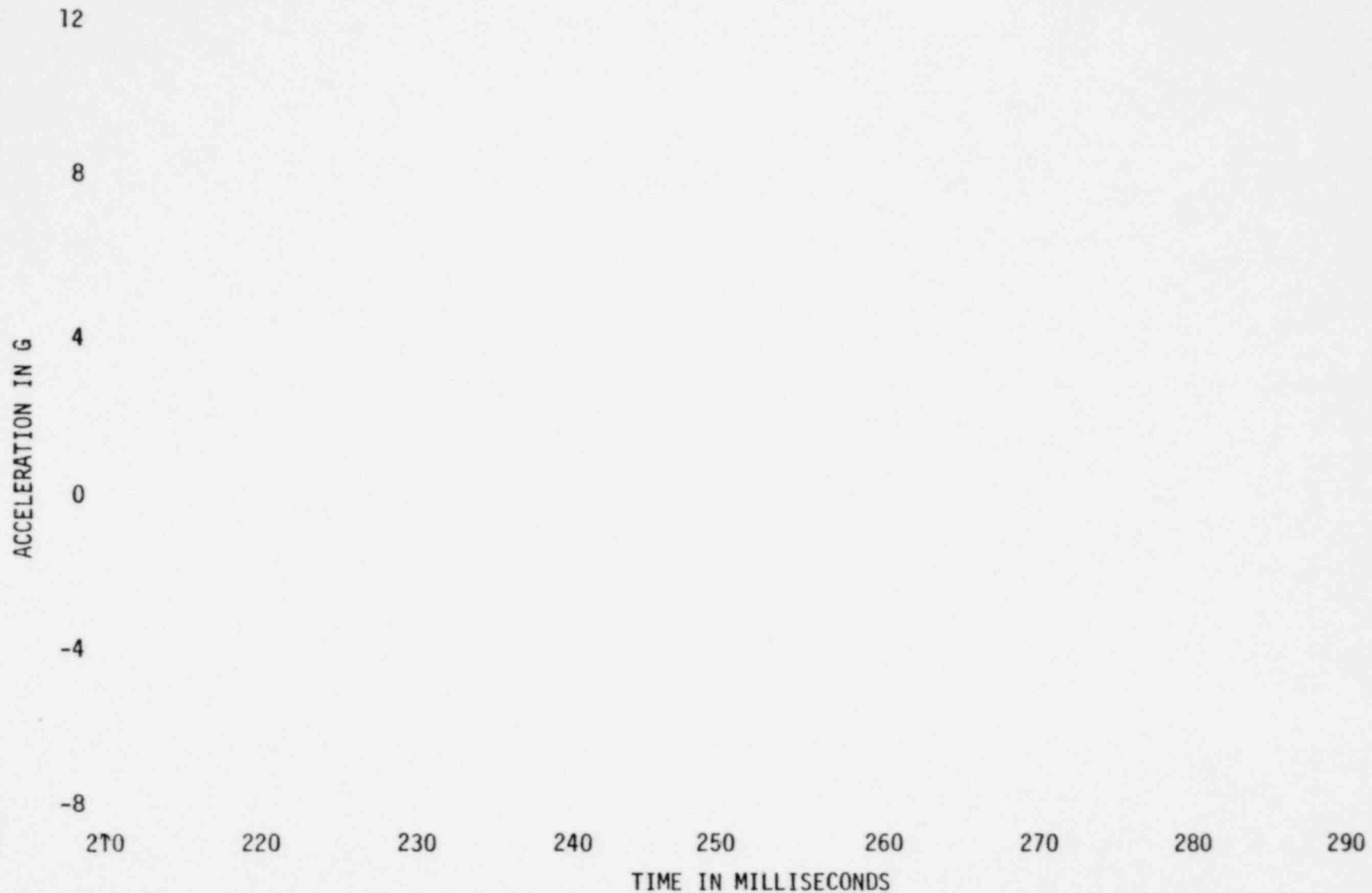
FIGURE A-272

COMPARISON OF VENT HEADER IMPACT RESULTS  
(Corrected Load Cell and Pressure Integration)  
Task 5.5.3 Brunswick Test 3



VENT HEADER VERTICAL ACCELERATION

Task 5.5.3-2 Brunswick Test 3



A-315

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FIGURE A-274  
TIME HISTORY OF  
POOL DISPLACEMENT

BRUNSWICK, TEST 1

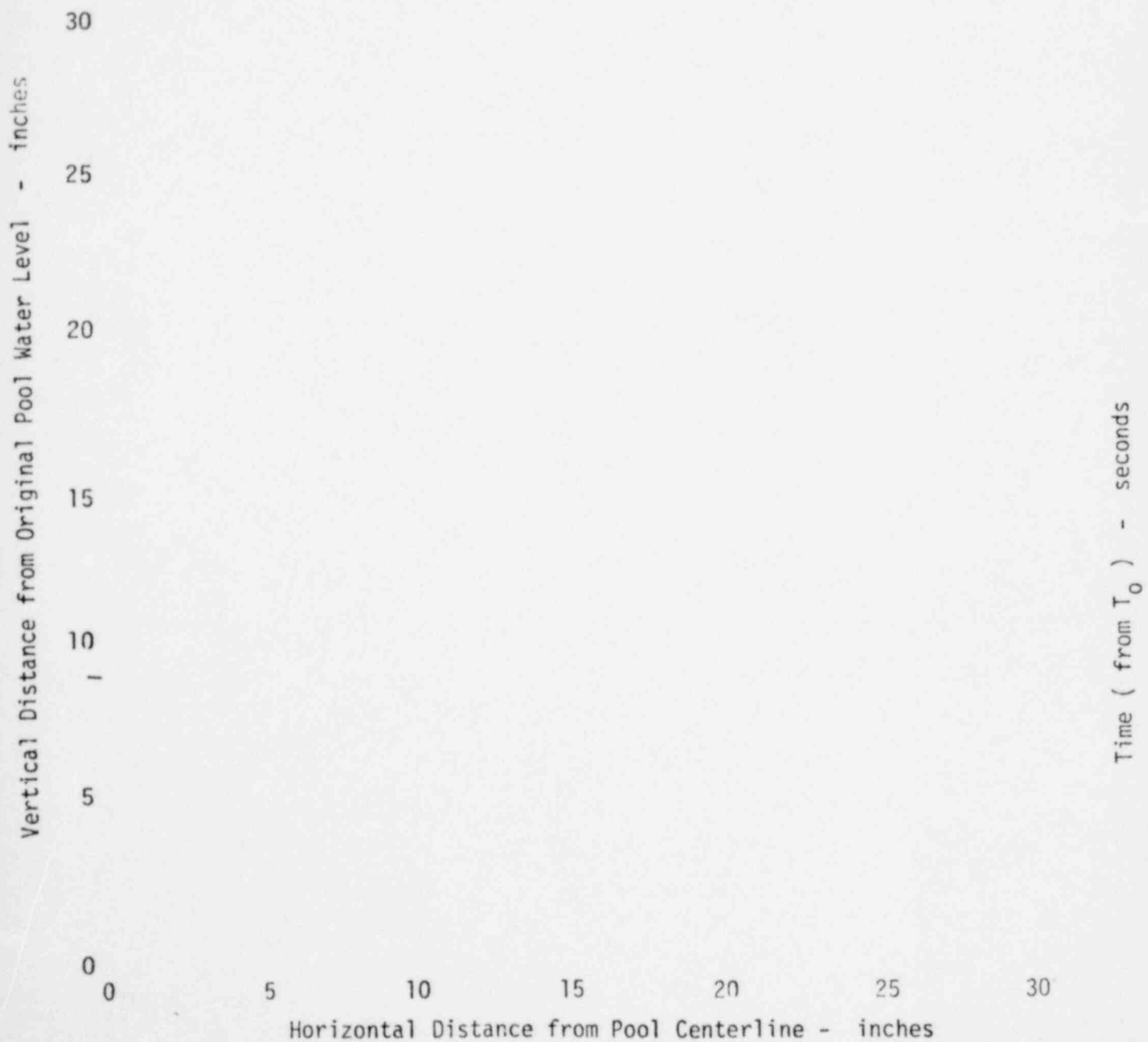


FIGURE A-275

TIME HISTORY OF  
POOL DISPLACEMENT

BRUNSWICK, TEST 2

30

25

0

5

0

5

0

0

5

10

15

20

25

30

Horizontal Distance from Pool Centerline - inches

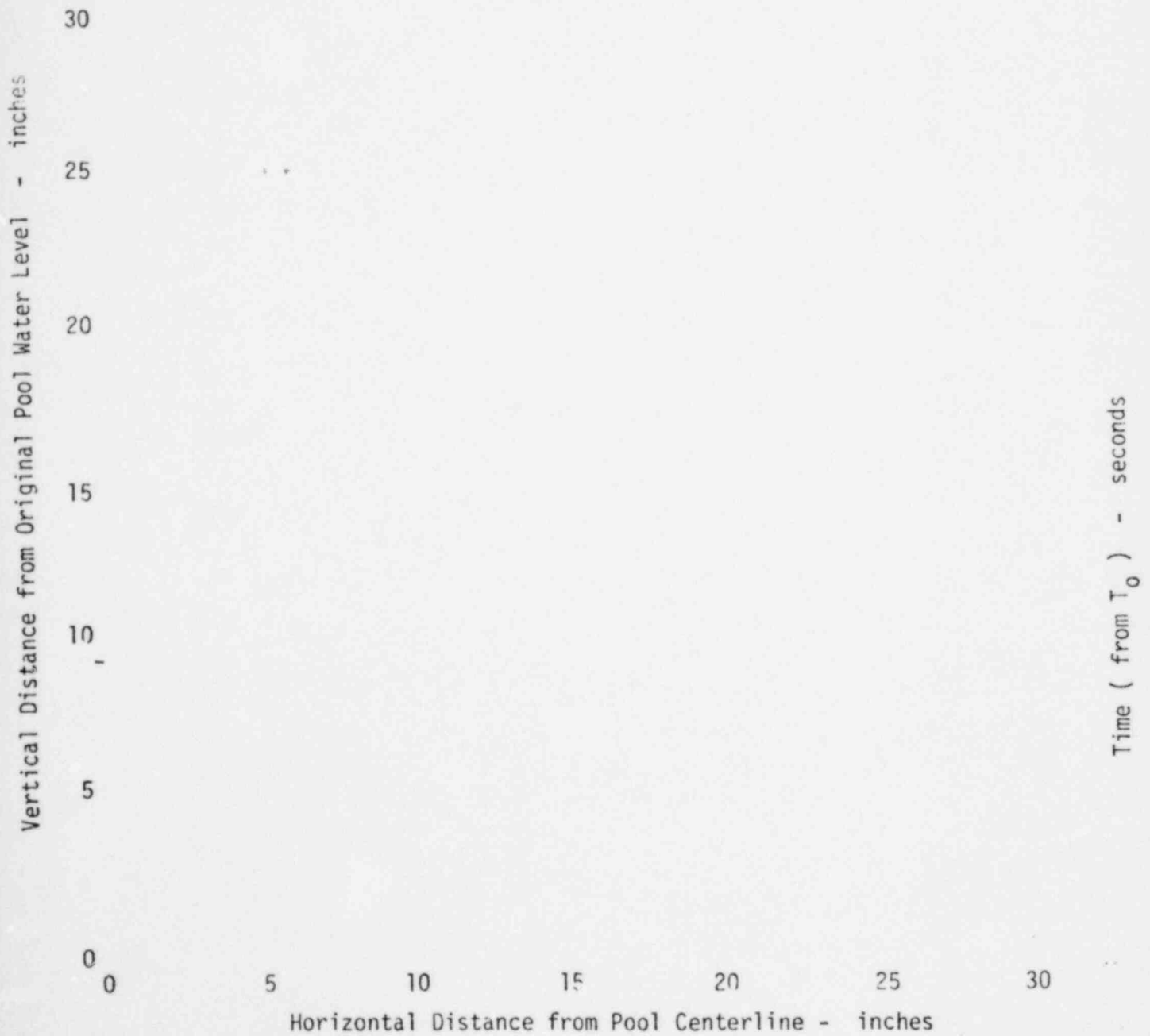
Time ( from  $T_0$  ) - seconds

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FIGURE A-276

TIME HISTORY OF  
POOL DISPLACEMENT

BRUNSWICK, TEST 3



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POOL SURFACE DISPLACEMENT

FIGURE A-277

BRUNSWICK, TESTS 1, 2, 3

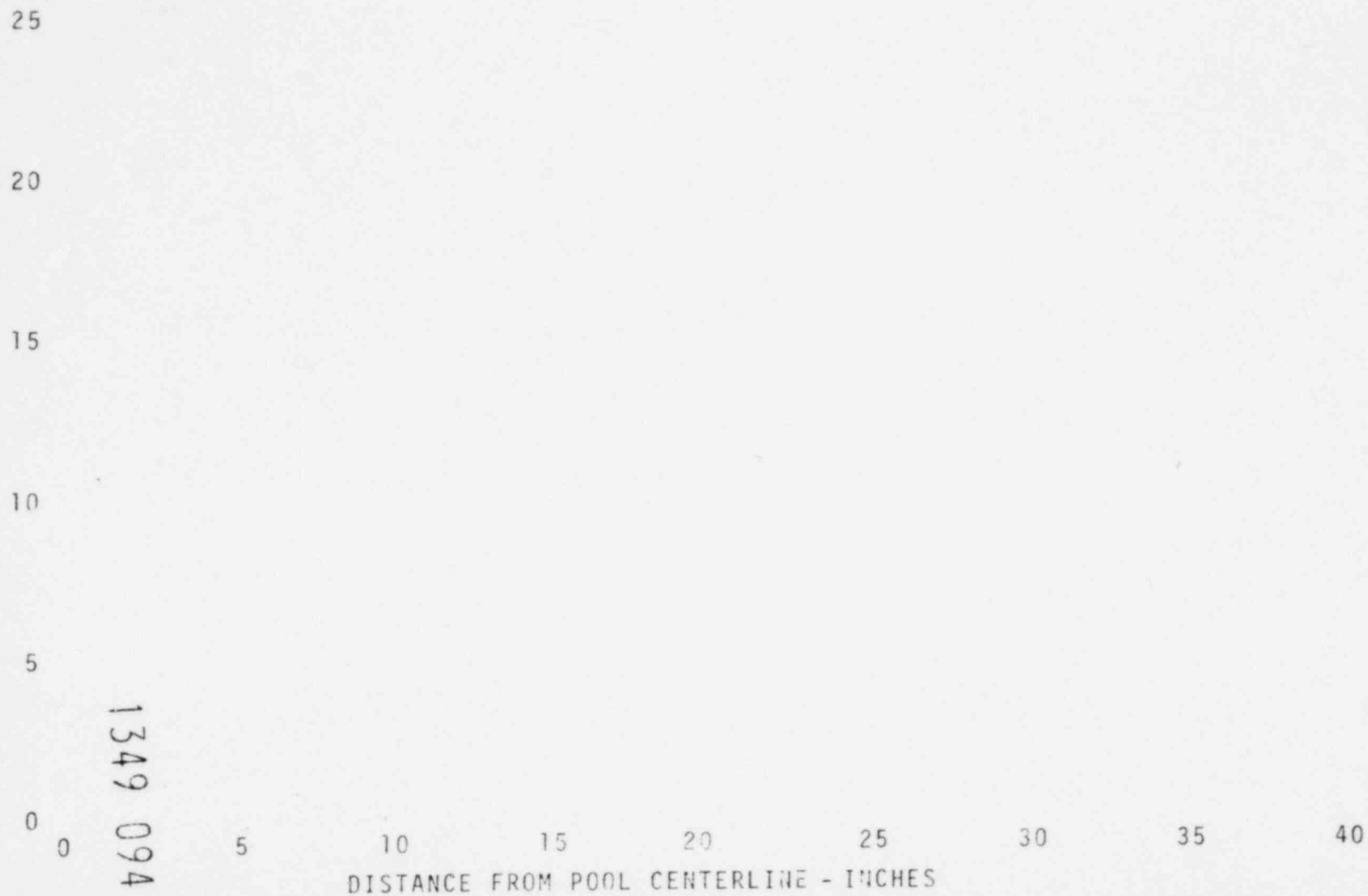


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POOL SURFACE VELOCITY PROFILES

FIGURE A-278

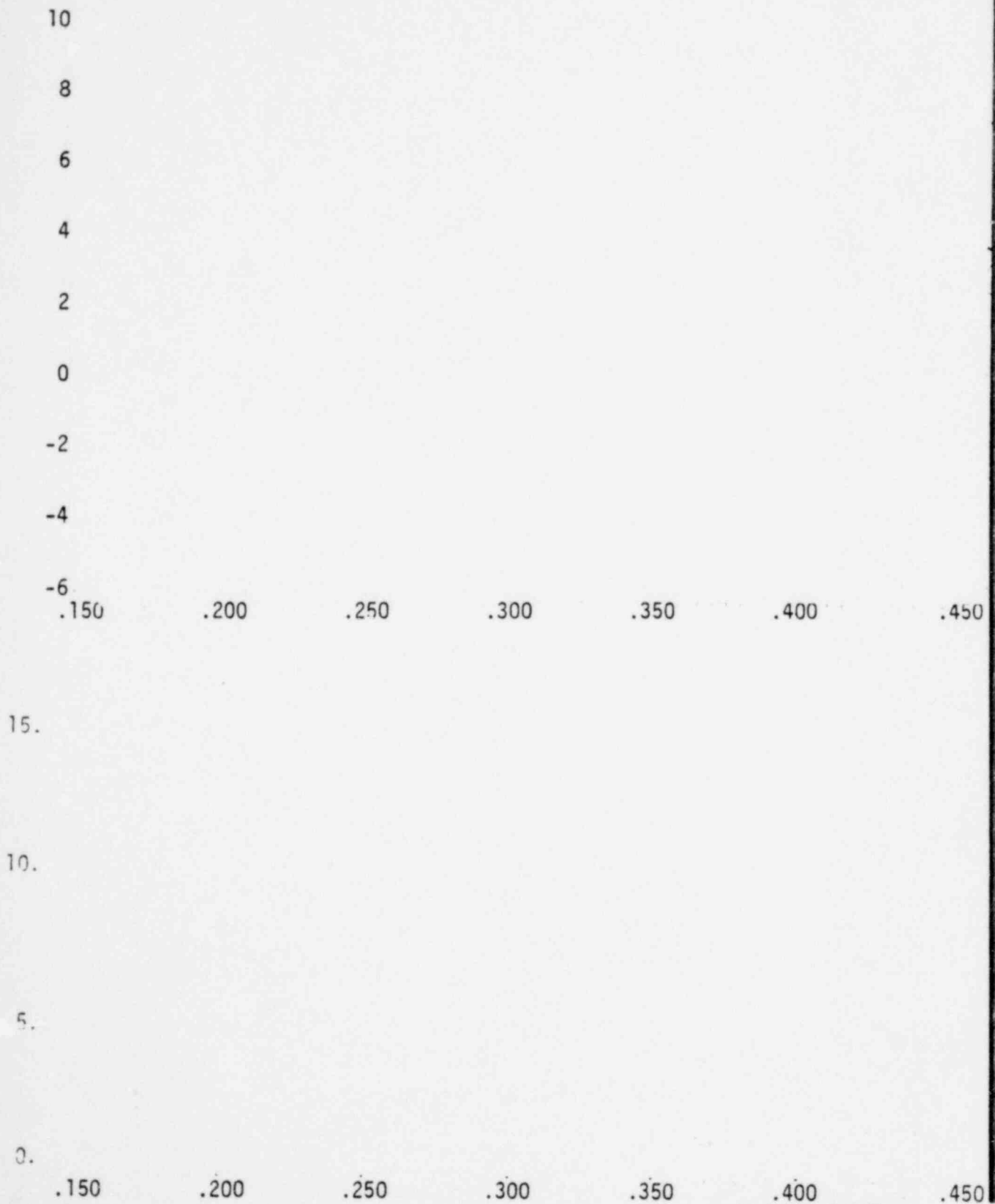
BRUNSWICK, TESTS 1, 2, 3



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SIDE WINDOW DISPLACEMENT AND VELOCITY PROFILES

BRUNSWICK, TEST 4



TIME - Seconds

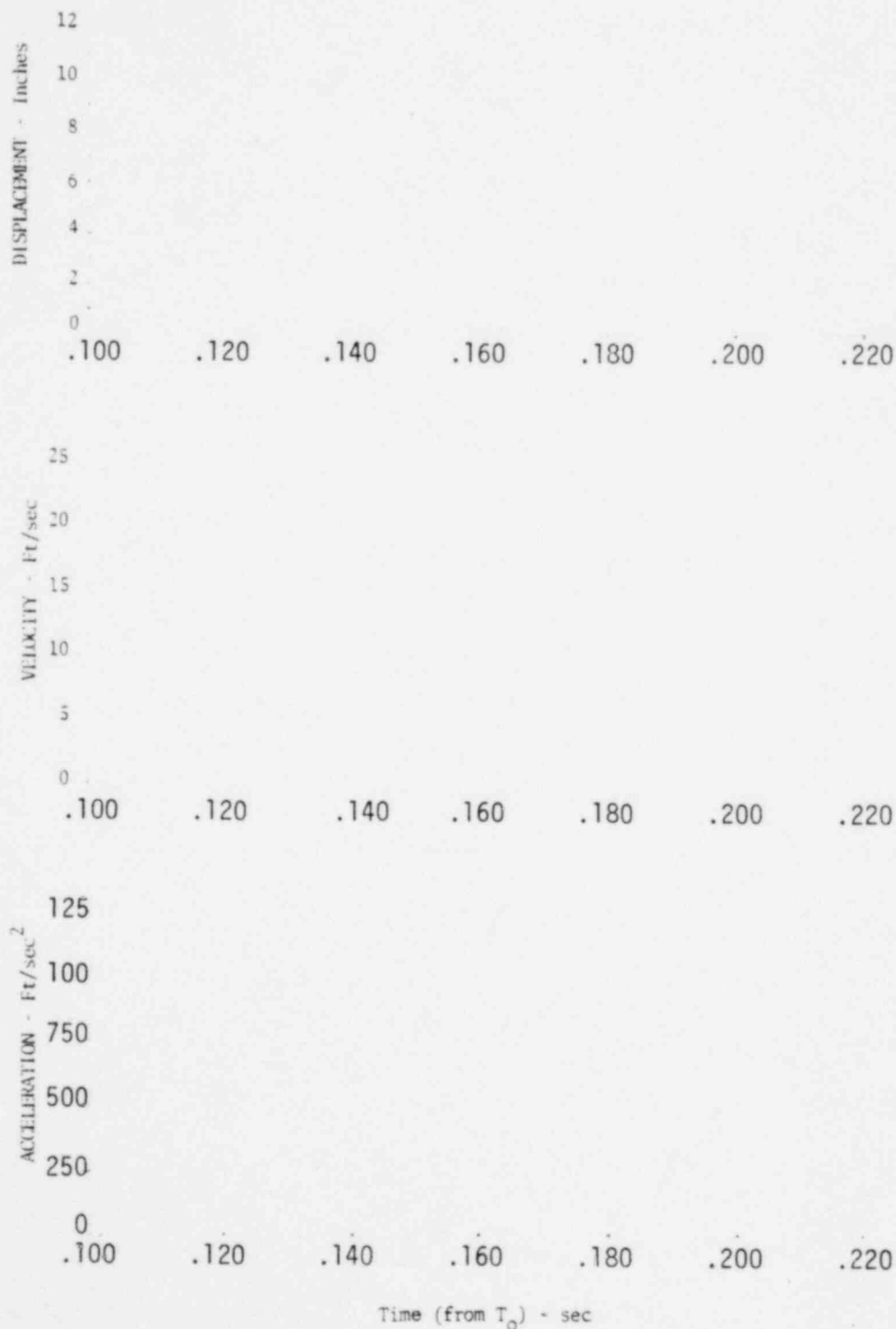
1349 095

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FIGURE A-280

DOWNCOMER WATER SLUG EJECTION

BRUNSWICK, TEST 3



1349 096

TABLE A-13

\*Vent clearing time (from  $T_0$ ) determined from the movie films.\*\*Time difference from  $T_0$  to time of zero downforce.DATA FOR WETWELL VERTICAL LOADS

Task 5.5.3-2 Brunswick Tests

\*(1) Start-of-test reference time

Parameter	Test No.	0" $\Delta P$ , 5.34" Pipe Deflector (20" Full Scale)					Std. Dev.
		(1)	(2)	(3)	(4)	Mean	
* (1)							
$T_0$	(sec)						
Vent Clearing Time*	(sec)						
<u>Peak Downforce</u>							
Pressure Integral:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
Corrected Pressure Integral:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
Corrected Load Cell:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
<u>Downforce Valley</u>							
Pressure Integral:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
Corrected Pressure Integral:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
Corrected Load Cell:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
<u>2nd Peak Downforce</u>							
Pressure Integral:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
Corrected Pressure Integral:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
Corrected Load Cell:							
Force	(lb)						
Time (from $T_0$ )	(sec)						
<u>[<math>\Delta t</math>] Downforce Time**</u>							
Pressure Integral	(sec)						
Corrected Pressure Integral	(sec)						
Corrected Load Cell	(sec)						
<u>Downforce Impulse</u>							
Pressure Integral:							
Impulse	(lb-sec)						

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TABLE A-13

\*Time at force is zero (from  $T_0$ )

## DATA FOR WETWELL VERTICAL LOADS (continued)

Task 5.5.3-2 Brunswick Tests

Parameter	Test No.	0"ΔP, 5.34" Pipe Deflector (20" Full Scale)					Std. Dev.
		(1)	(2)	(3)	(4)	Mean	
<u>Peak Upforce</u>							
Pressure Integral:							
Force (lb)	(1b)						
Time (from $T_0$ ) (sec)	(sec)						
Corrected Pressure Integral:							
Force (lb)	(1b)						
Time (from $T_0$ ) (sec)	(sec)						
Corrected Load Cell:							
Force (lb)	(1b)						
Time (from $T_0$ ) (sec)	(sec)						
<u>Upforce Valley</u>							
Pressure Integral:							
Force (lb)	(1b)						
Time (from $T_0$ ) (sec)	(sec)						
Corrected Pressure Integral:							
Force (lb)	(1b)						
Time (from $T_0$ ) (sec)	(sec)						
Corrected Load Cell:							
Force (lb)	(1b)						
Time (from $T_0$ ) (sec)	(sec)						
<u>2nd Peak Upforce</u>							
Pressure Integral:							
Force (lb)	(1b)						
Time (from $T_0$ ) (sec)	(sec)						
Corrected Pressure Integral:							
Force (lb)	(1b)						
Time (from $T_0$ ) (sec)	(sec)						
Corrected Load Cell:							
Force (lb)	(1b)						
Time (from $T_0$ ) (sec)	(sec)						
<u>Zero Force Time*</u>							
Pressure Integral (sec)	(sec)						
Corrected Pressure Integral (sec)	(sec)						
Corrected Load Cell (sec)	(sec)						

TABLE A-14

DATA FOR VENT HEADER IMPACT LOADS

Task 5.5.3-2 Brunswick Tests

Parameter	Test No.	0" $\Delta P$ , 5.34" Deflector					Std. Dev.	( 5 )
		( 1 )	( 2 )	( 3 )	( 4 )	Mean		
$T_0^+$	(sec)							
<u>Vent Header Impact</u>								
Pressure Integral:								
Maximum Force	(lb)							
Impulse	(lb-sec)							
Duration*	(sec)							
Load Cell Corrected:††								
Maximum Force	(lb)							
Impulse	(lb-sec)							
Duration	(sec)							
Pool Surface Velocity	(ft/sec)							
Time (from $T_0$ )**	(sec)							

\*Based on impact pressure measurements.

\*\*At start of the first impact pressure recorded.

\*\*\*Only the mean velocity (for tests 1, 2, 3) at a position 6" off the facility centerline is calculate.

†Start of reference time

††represents peak of very noisy data (acceleration corrected); mean value would be lower

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## A.7 Cooper Station Tests

### A.7.1 Typical Data

Time-history plots of the driving conditions and pool response are presented in this section for Cooper Station Tests 3 and 5. Test 3 was a load definition test which was conducted at a partial drywell/wetwell differential pressure of 7.46"  $\Delta P$ . Test 5 was conducted without an initial drywell/wetwell differential pressure (0"  $\Delta P$ ). The Cooper Station tests were conducted with no vent header deflector.

#### A.7.1.1 Driving Conditions

Driving conditions for Cooper Station Test 3 are presented in Figures A-281 through A-285. Similar plots for Cooper Station Test 5 are shown in Figures A-286 through A-290. Cooper Station's driving conditions had the same characteristics as the "typical" plant discussed in Section 3.0 of this report.

#### A.7.1.2 Pool Response

Downcomer internal pressure and wetwell pressures for Cooper Station Tests 3 and 5 are presented in Figures A-291 through A-292 and A-293 through A-294, respectively. These pressure plots have the same characteristics as the "typical" plant in Section 3.0.

Figures A-295 and A-296 present net torus force based on the torus pressure integral for Cooper Station Tests 3 and 5, respectively. Some downforce oscillations are present, but they dampen out rapidly after the first oscillation. The upforce also shows some oscillation.

The net torus force which was determined by applying the inertial correction from the torus accelerometer (Figures A-298 and A-300) to the torus load cell (Figures A-297 and A-299) is compared with

1349 100

the torus force obtained from the torus pressure integral in Figures A-301 and A-302. Figures A-303 and A-304 present the net torus force based on the torus pressure integral corrected for inertia.

The "average" pool pressures for Cooper Station Tests 3 and 5 are shown in Figures A-305 and A-307. Figures A-306 and A-308 are the same as Figures A-303 and A-304 with force replaced by average pressure (force/torus projected area).

The vent header impact pressures for Cooper Station Test 3 are presented in Figures A-309 through A-312. Vent header pressures for Cooper Station Test 5 are presented in Figures A-313 through A-316.

Figure A-317 presents a comparison of the vent header impact force derived from the pressure integral with that derived from the corrected load cell. Vent header vertical accelerations from Tests 3 and 5 are shown in Figures A-318 and A-319, respectively.

#### A.7.2 Pool Dynamics

The pool contours at various times of pool swell are shown in Figures A-320 through A-323 for Cooper Station Tests 1, 2, 3, and 5.

The pool surface displacement curves for Tests 1, 2, and 3 are shown on Figure A-324. The pool surface velocities for Tests 1, 2, and 3 are shown on Figure A-325. The pool surface displacement graph and pool surface velocity profiles for Test 5 are shown in Figures A-326 and A-327, respectively.

The pool surface displacements and velocity profile viewed from the side window during Test 4 are shown in Figure A-328. The downcomer water slug displacement, velocity, and acceleration versus time for Tests 3 and 5 are presented in Figures A-329 and A-330.

#### A.7.3 Data Summaries

Table A-15 presents the Cooper Station test data for wetwell vertical forces.

Table A-16 presents the Cooper Station test data for vent header impact forces.

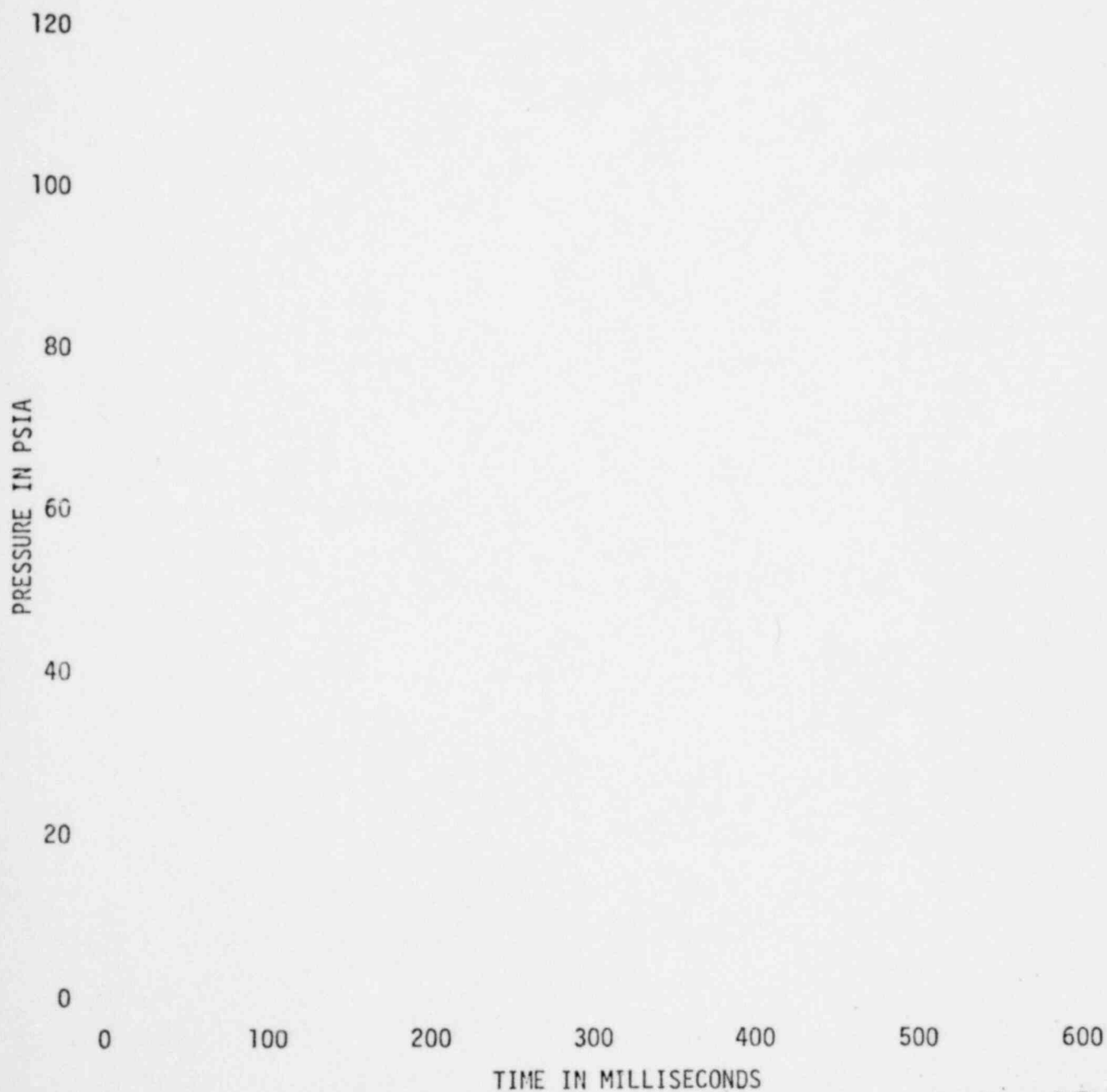
#### A.7.4 Discussion and Analysis

Figure A-331 presents the effect of drywell/wetwell  $\Delta P$  on enthalpy flow into the bubbles. Effect of drywell/wetwell  $\Delta P$  on downcomer internal pressure is shown in Figure A-332. Figure A-333 presents the effect of drywell/wetwell  $\Delta P$  on pool and freespace pressures. The data for Cooper Station parallels that for the "typical" plant in Section 3.0.

The Cooper Station load definition tests were conducted at 7.46"  $H_2O$   $\Delta P$  and with no vent header deflector. A  $\Delta P$  sensitivity test at 0"  $H_2O$   $\Delta P$  was also conducted. Some downforce oscillations were evident. The upforce also showed oscillation. The vent header impact force was significantly higher than for plants using deflectors.

FIGURE A-281

DRYWELL ORIFICE UPSTREAM PRESSURE  
Task 5.5.3-2 Cooper Station Test 3

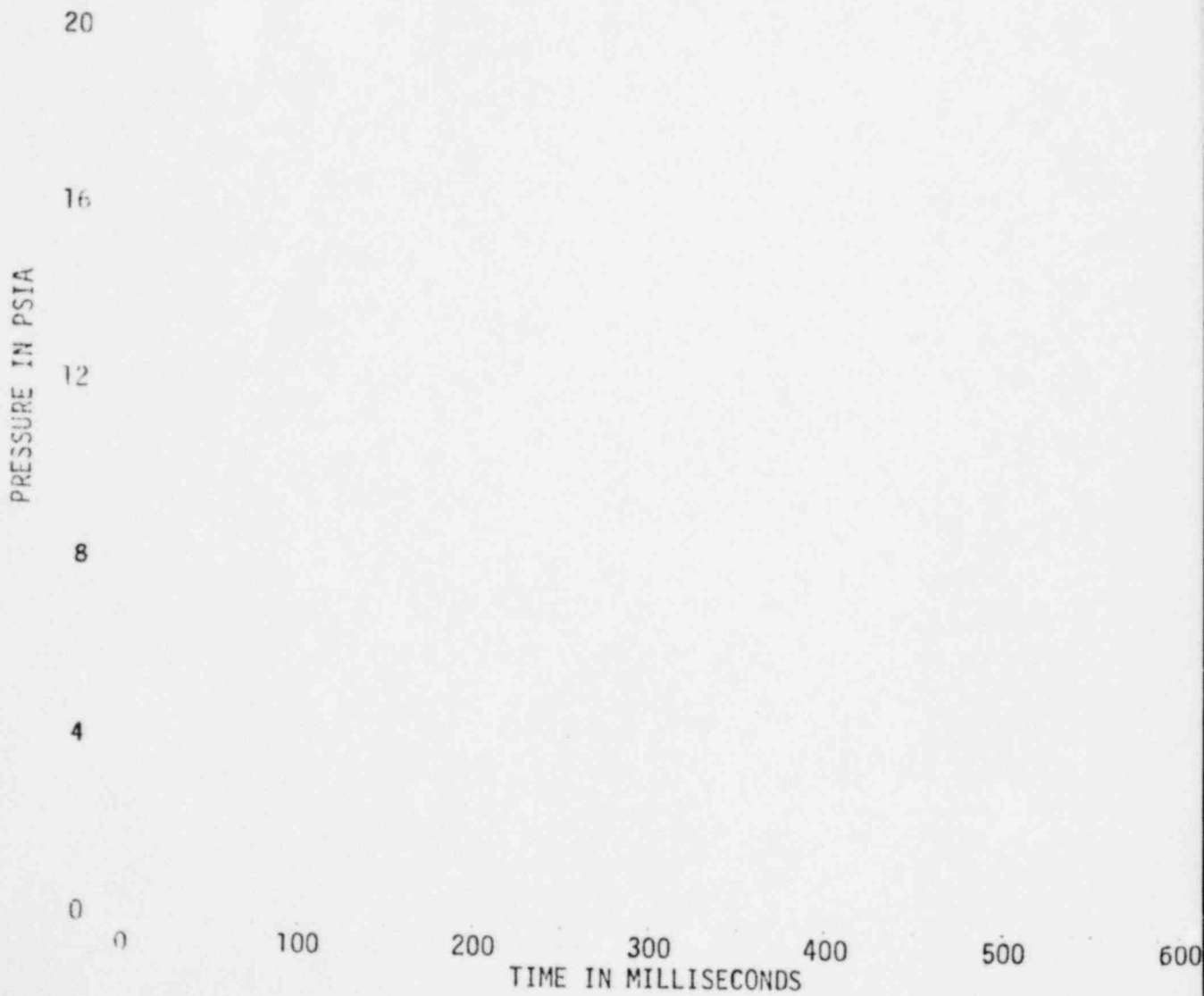


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FIGURE A-282

DRYWELL PRESSURE

Task 5.5.3-2 Cooper Station Test 3

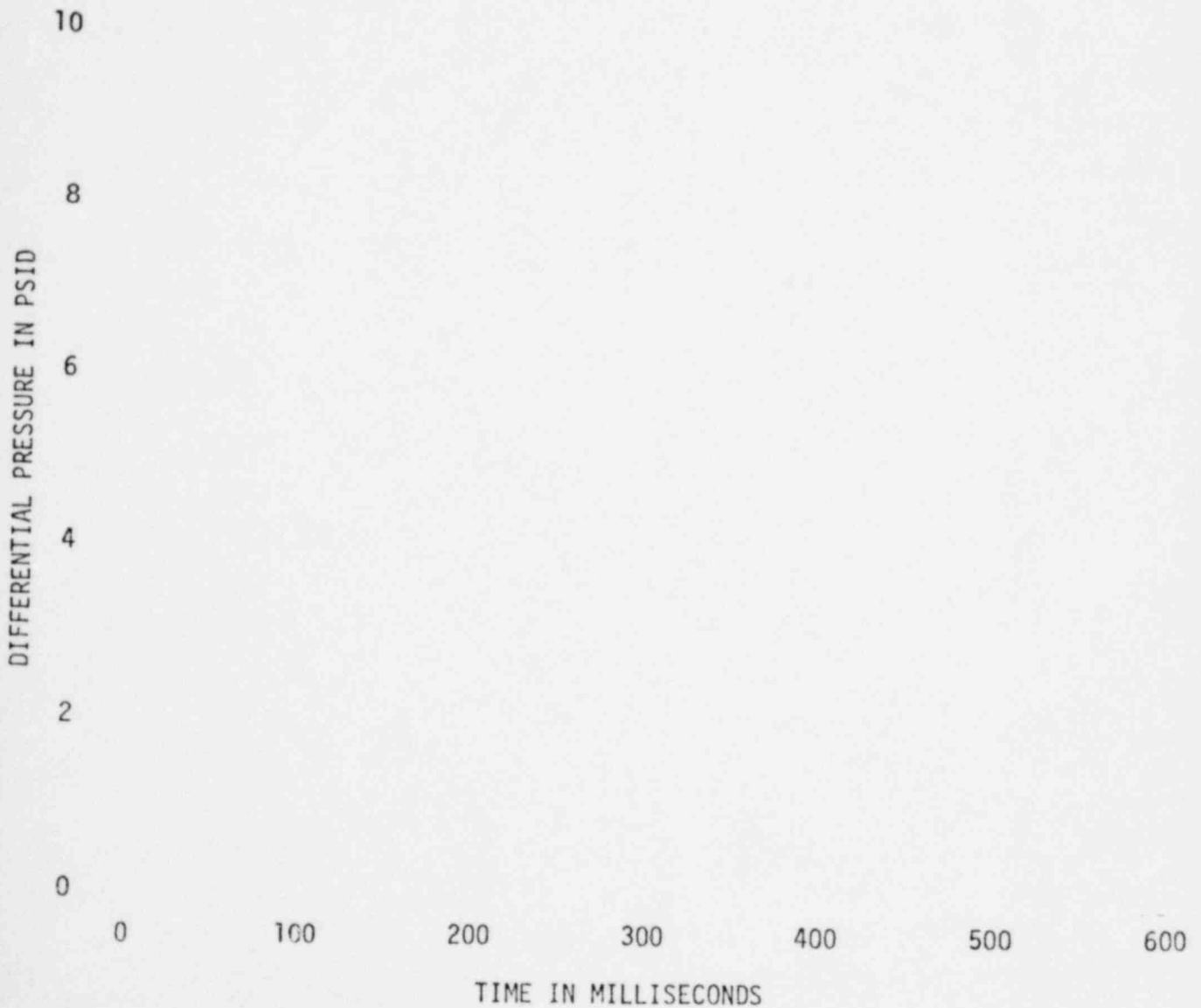


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FIGURE A-283

DOWNCOMER ORIFICE DIFFERENTIAL PRESSURE

Task 5.5.3-2 Cooper Station Test 3



1349 105

FIGURE A-284

DOWNCOMER ORIFICE UPSTREAM TEMPERATURE

Task 5.5.3-2 Cooper Station Test 3

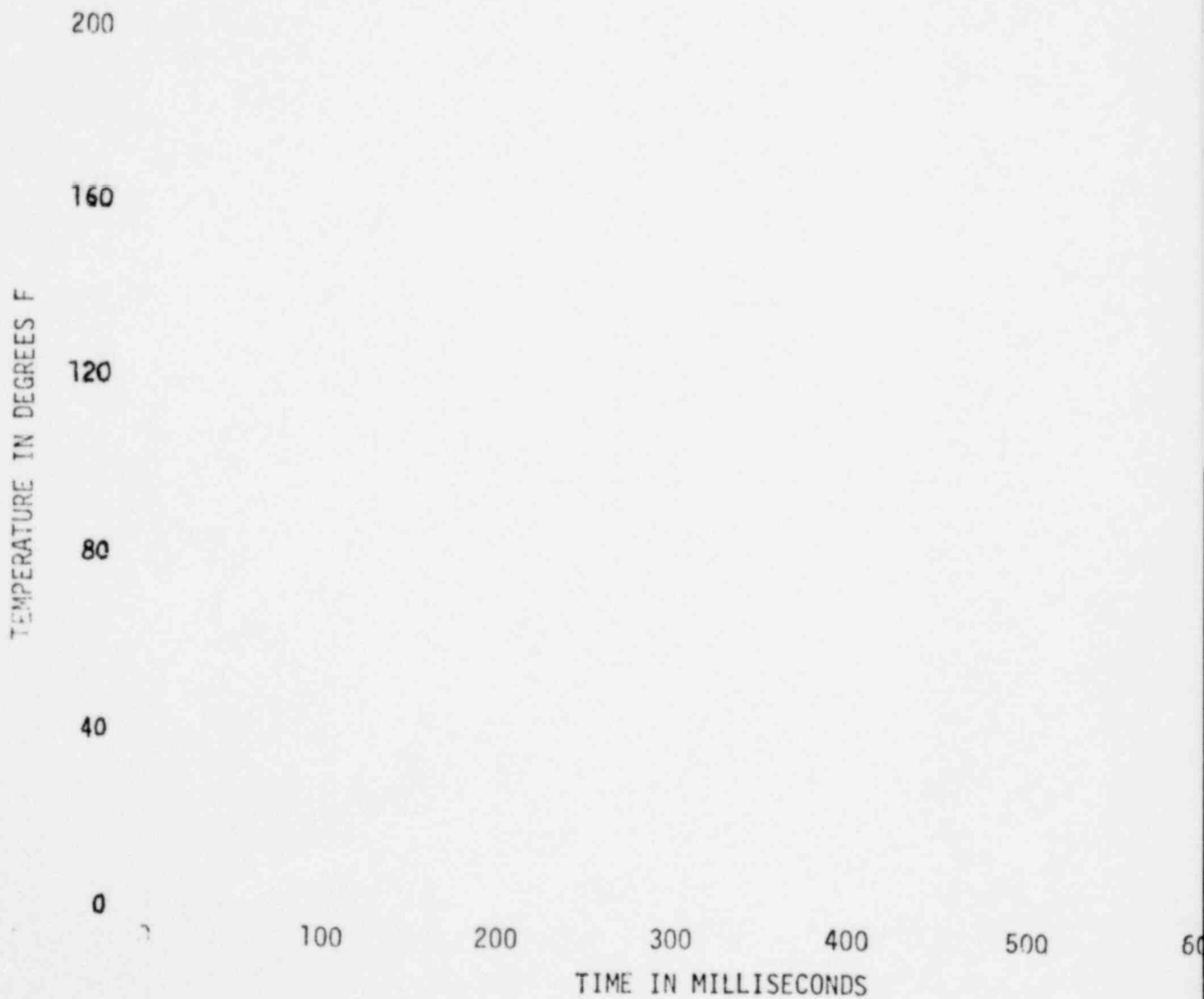


FIGURE A-285

ENTHALPY FLOW INTO POOL

Task 5.5.3-2 Cooper Station Test 3

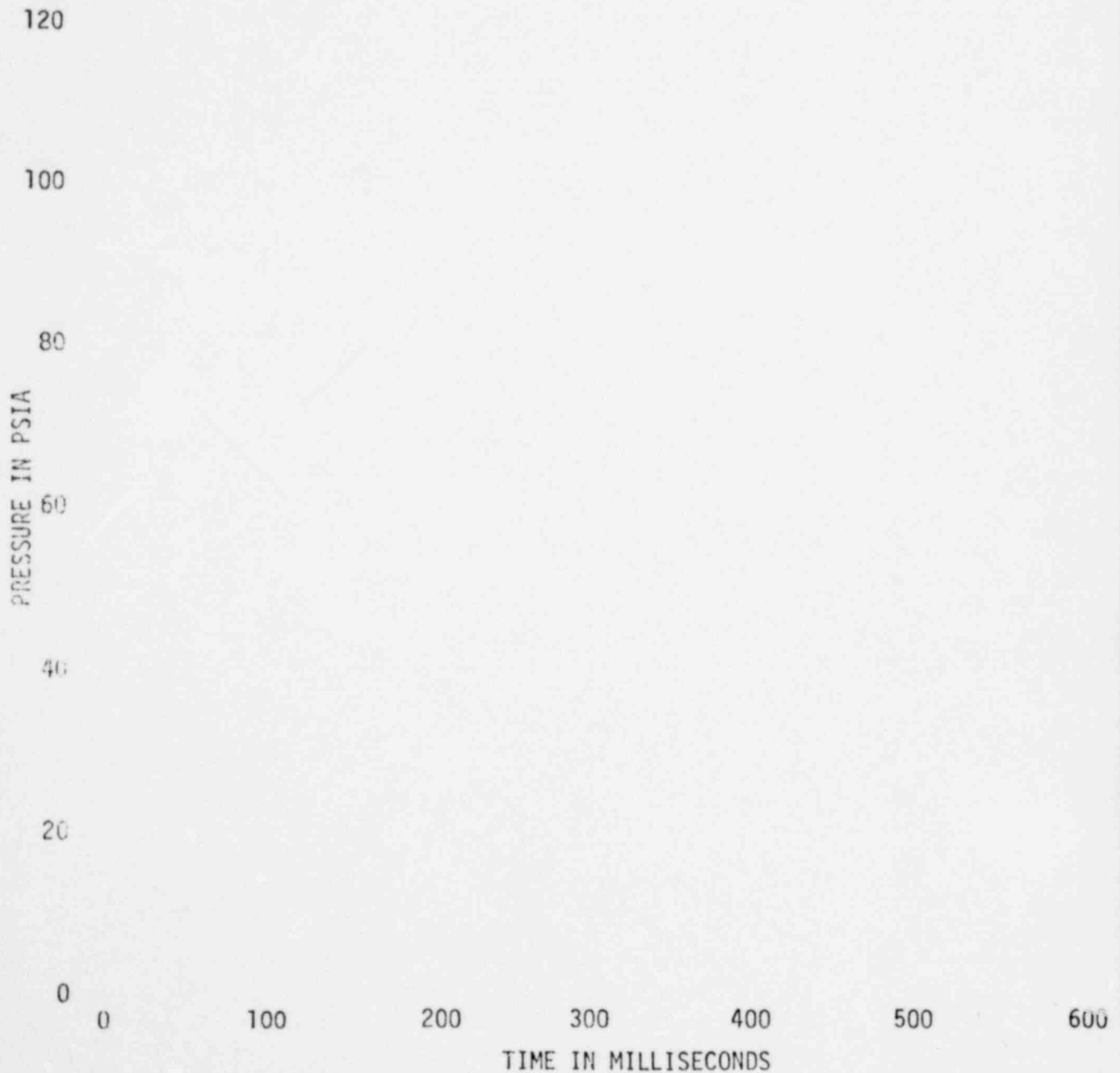


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FIGURE A-286

DRYWELL ORIFICE UPSTREAM PRESSURE

Task 5.5.3-2 Cooper Station Test 5

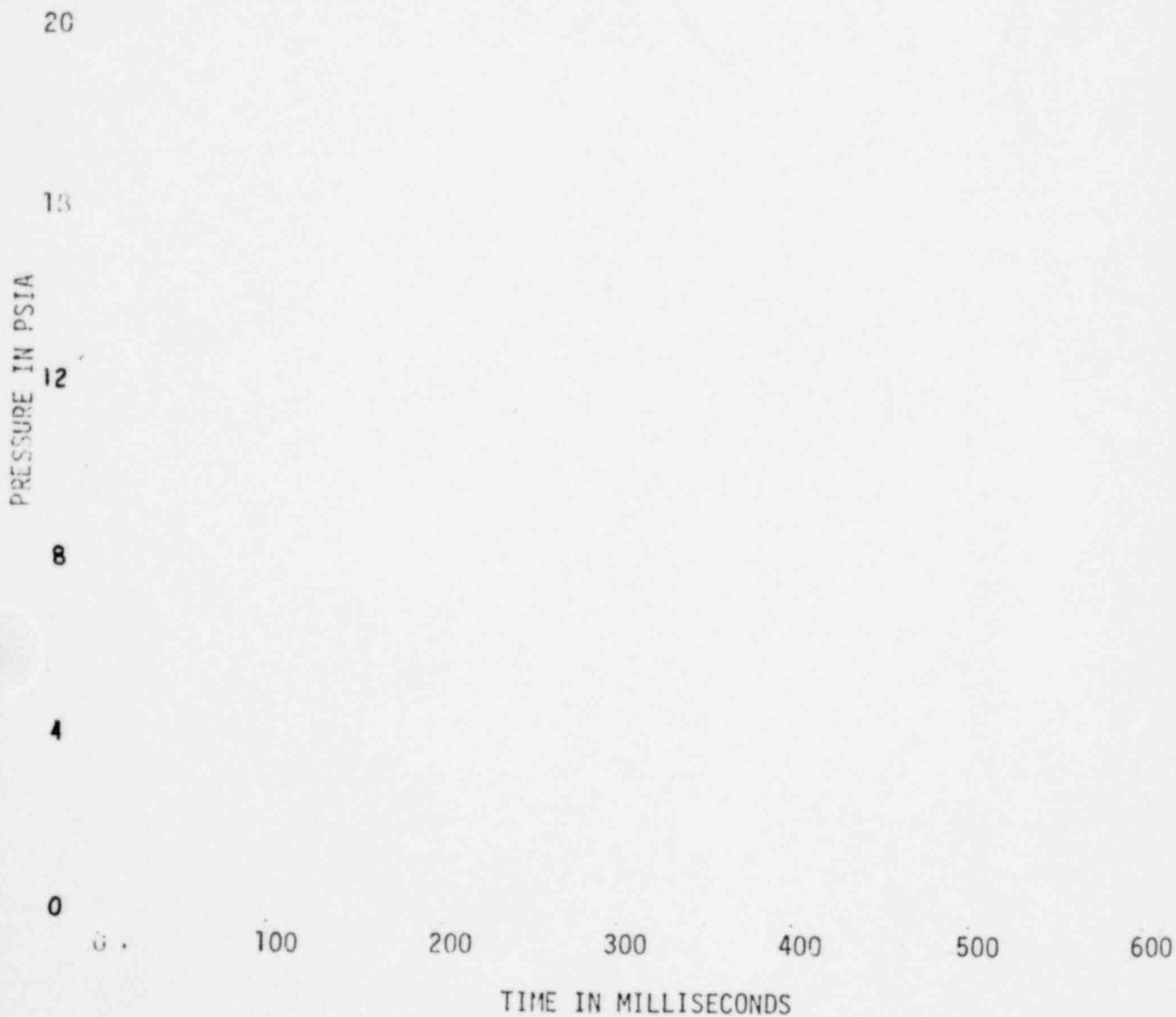


1349 108

FIGURE A-287

DRYWELL PRESSURE

Task 5.5.3-2 Cooper Station Test 5



1349 109

FIGURE A-288  
DOWNCOMER ORIFICE DIFFERENTIAL PRESSURE  
Task 5.5.3-2 Cooper Station Test 5

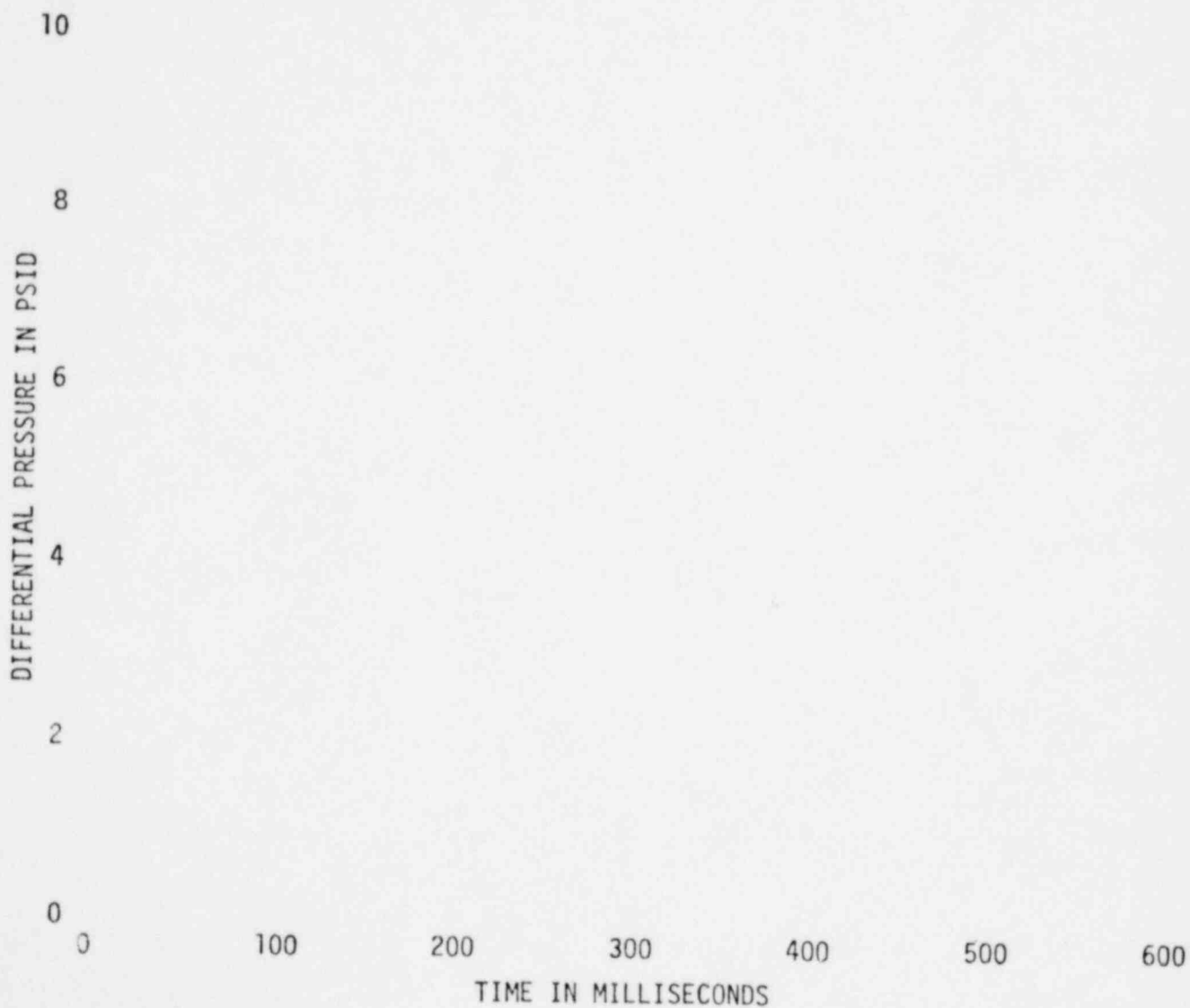


FIGURE A-289

DOWNCOMER ORIFICE UPSTREAM TEMPERATURE

Task 5.5.3-2 Cooper Station Test 5



1349 111

FIGURE A-290

ENTHALPY FLOW INTO POOL

Task 5.5.3-2 Cooper Station Test 5

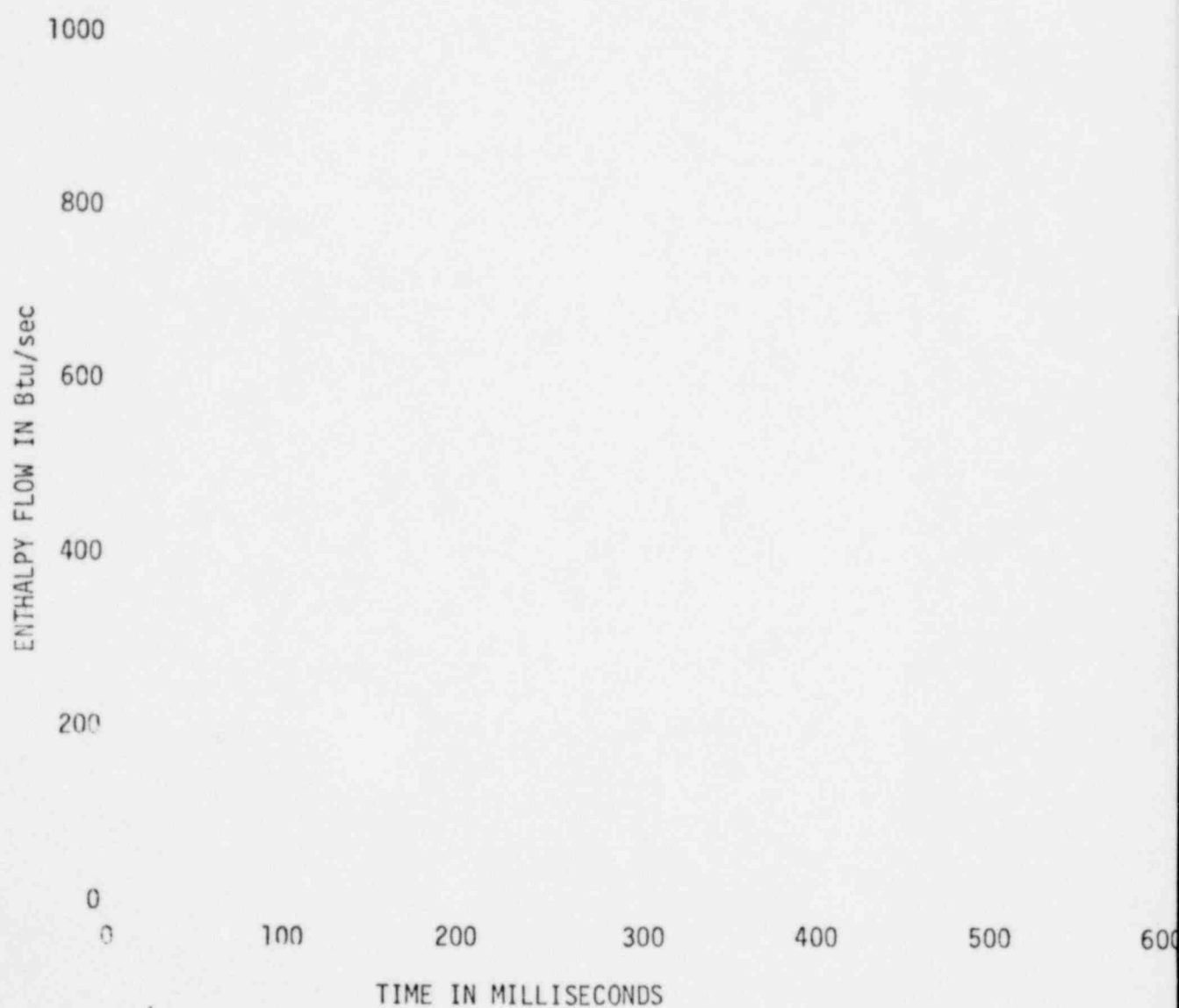


FIGURE A-291

DOWNCOMER INTERNAL PRESSURE

Task 5.5.3-2 Cooper Station Test 3



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FIGURE A-292

WETWELL PRESSURES

Task 5.5.3-2 Cooper Station Test 3

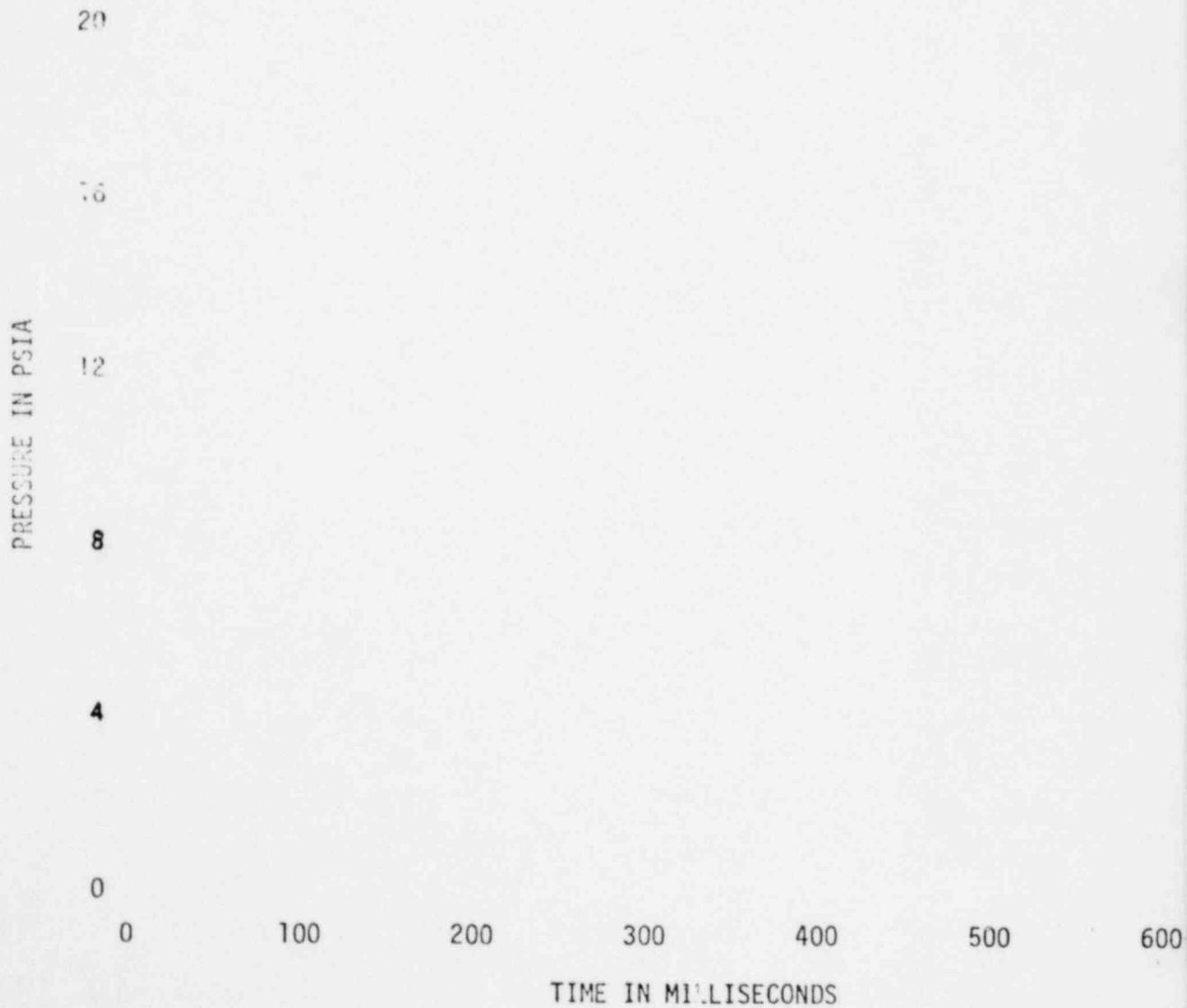
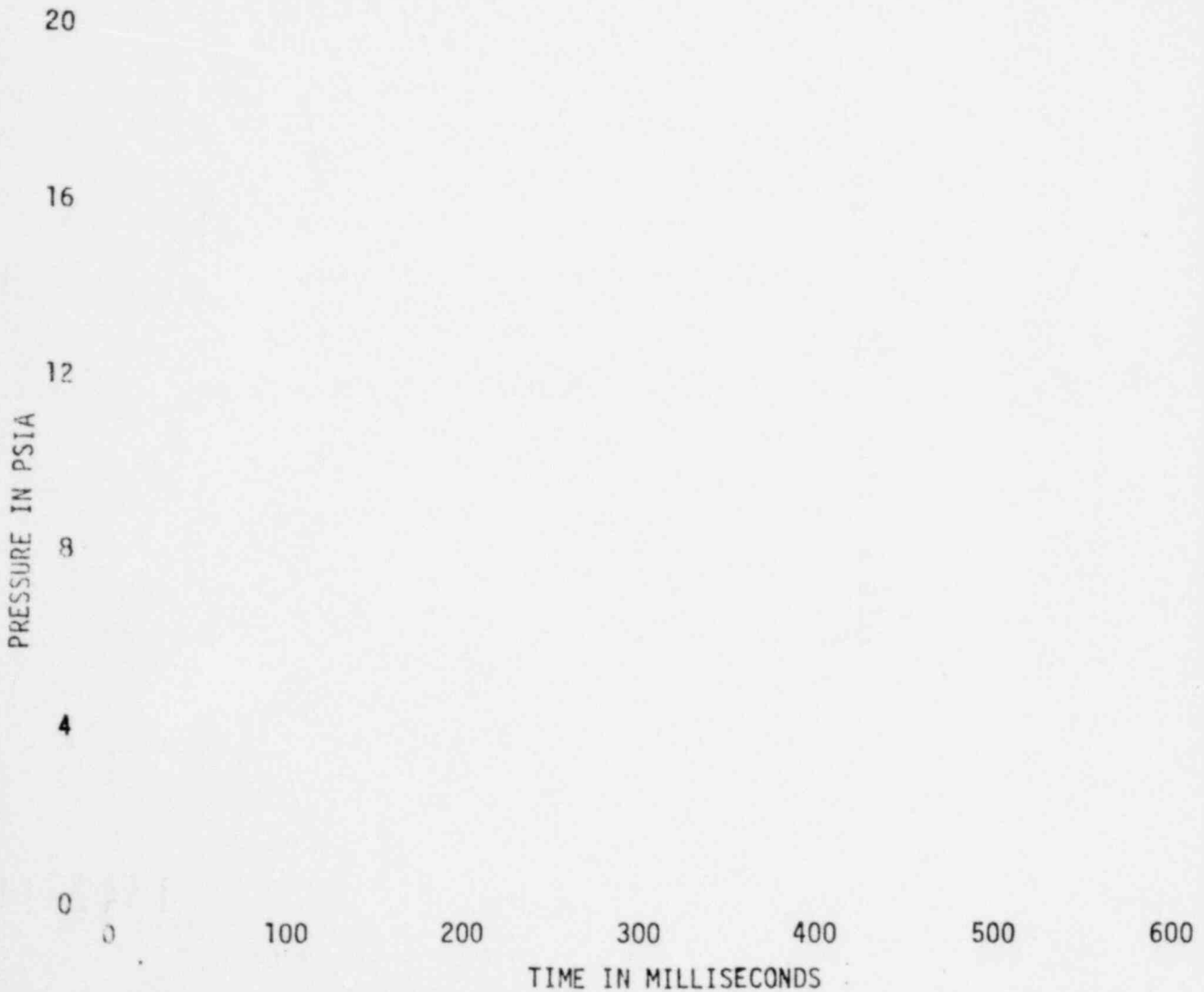


FIGURE A-293

DOWNCOMER INTERNAL PRESSURE

Task 5.5.3-2 Cooper Station Test 5



1349 115

FIGURE A-294

WETWELL PRESSURES

Task 5.5.3-2 Cooper Station Test 5

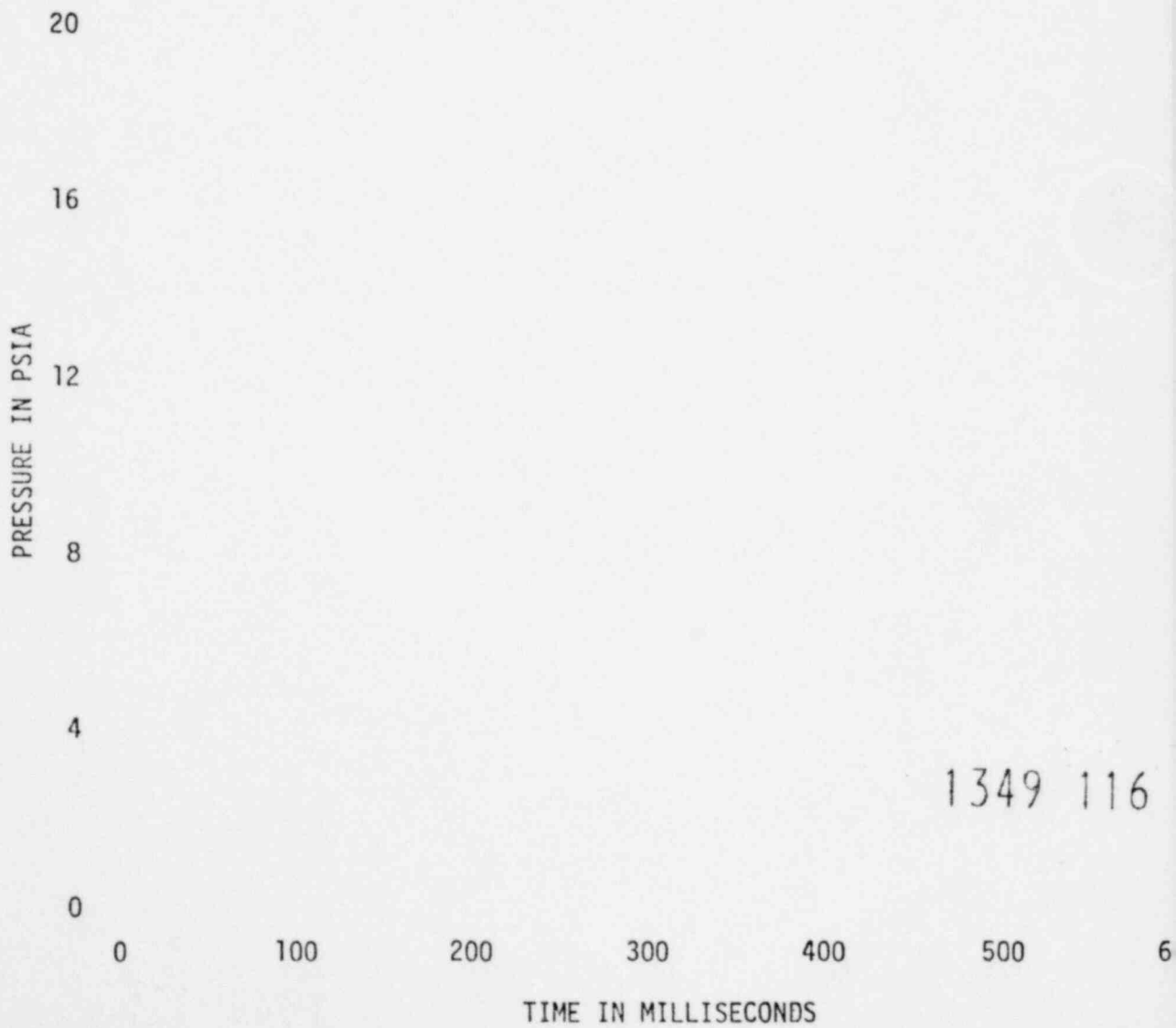


FIGURE A-295  
NET TORUS FORCE FROM PRESSURE INTEGRAL  
Task 5.5.3-2 Cooper Station Test 3

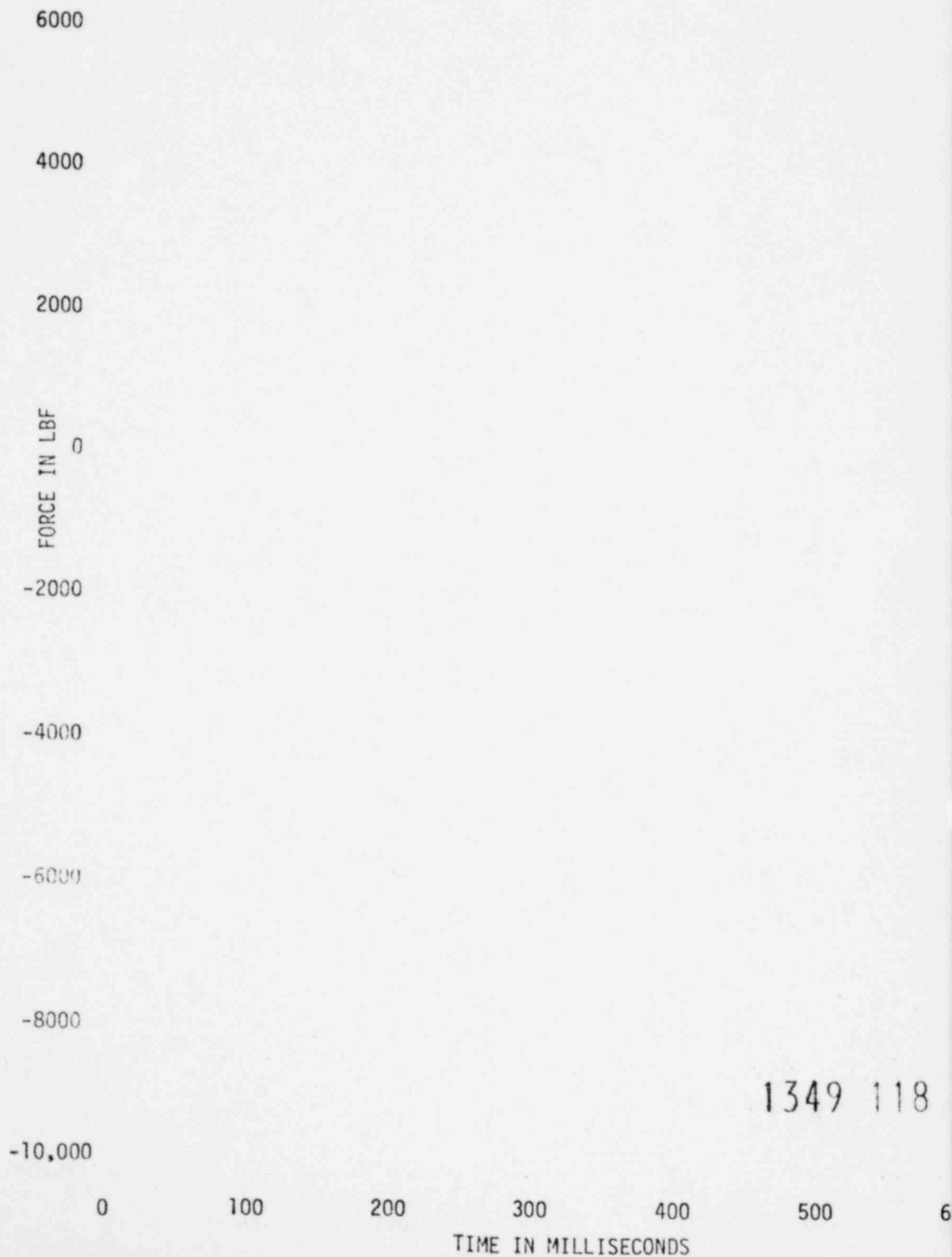


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FIGURE A-296

NET TORUS FORCE FROM PRESSURE INTEGRAL

Task 5.5.3-2 Cooper Station Test 5



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FIGURE A-297

TORUS LOAD CELL

Task 5.5.3-2 Cooper Station Test 3

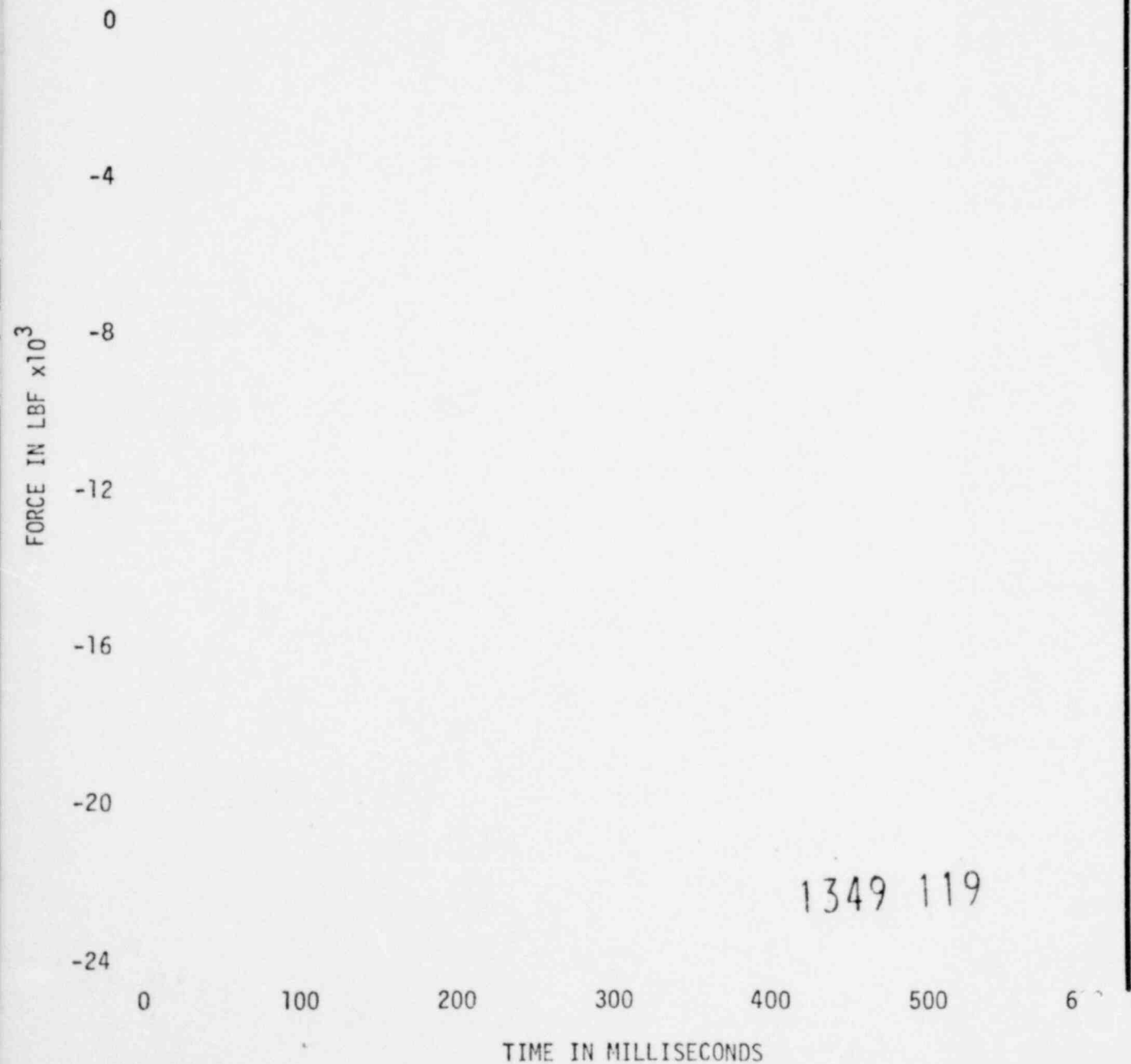
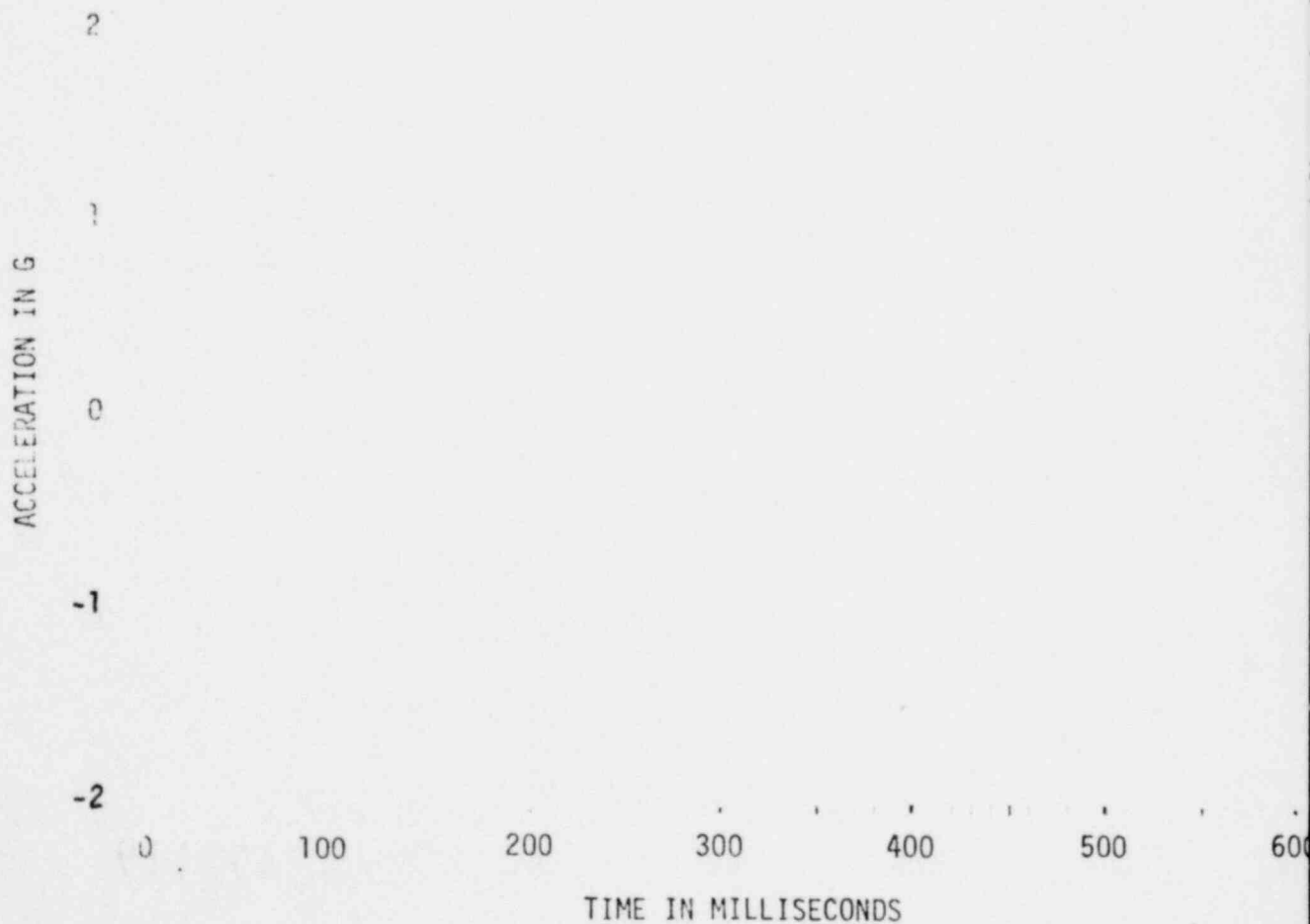


FIGURE A-298

TORUS VERTICAL ACCELERATION

Task 5.5.3-2 Cooper Station Test 3



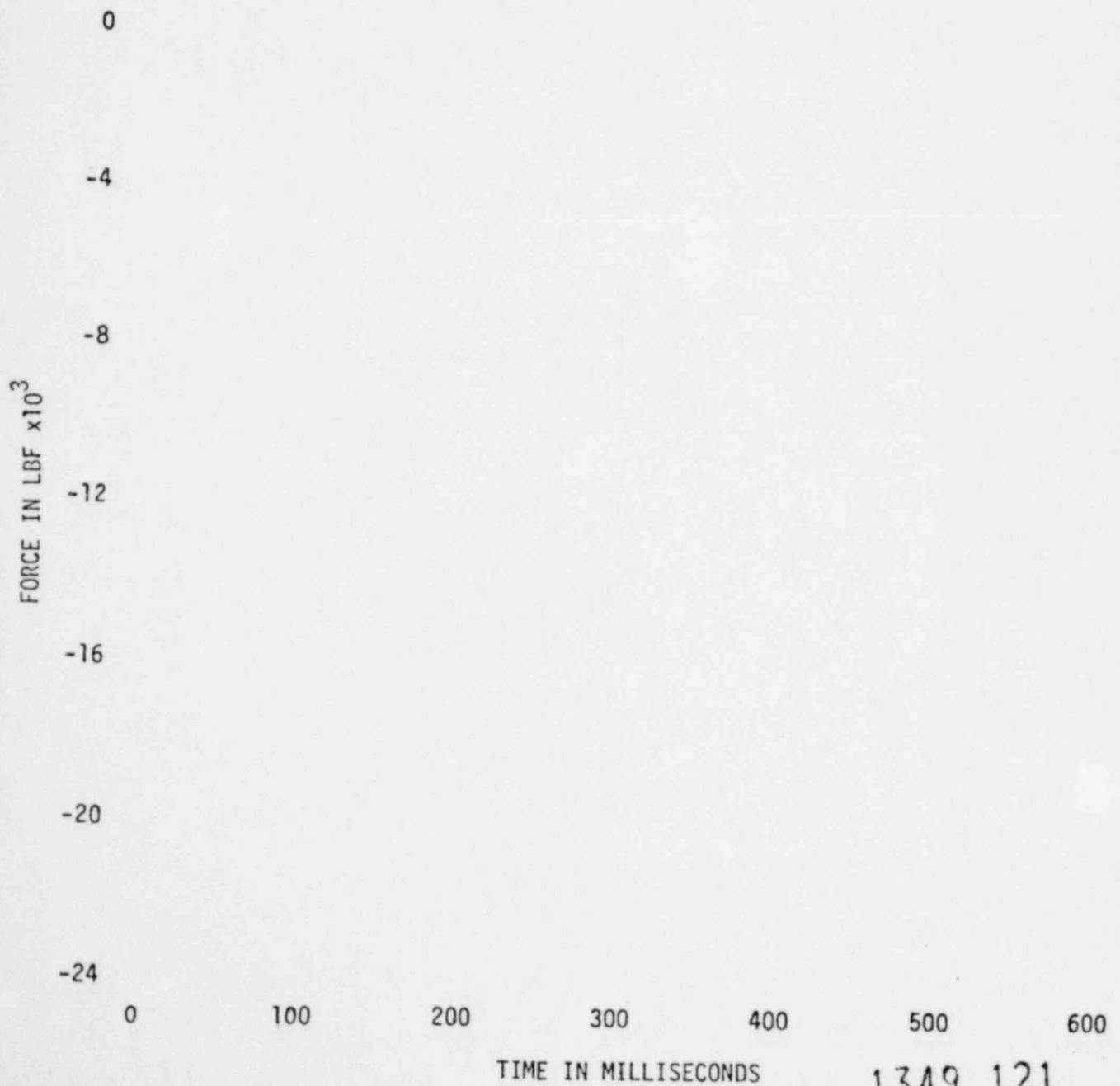
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FIGURE A-299

TORUS LOAD CELL

Task 5.5.3-2 Cooper Station Test 5

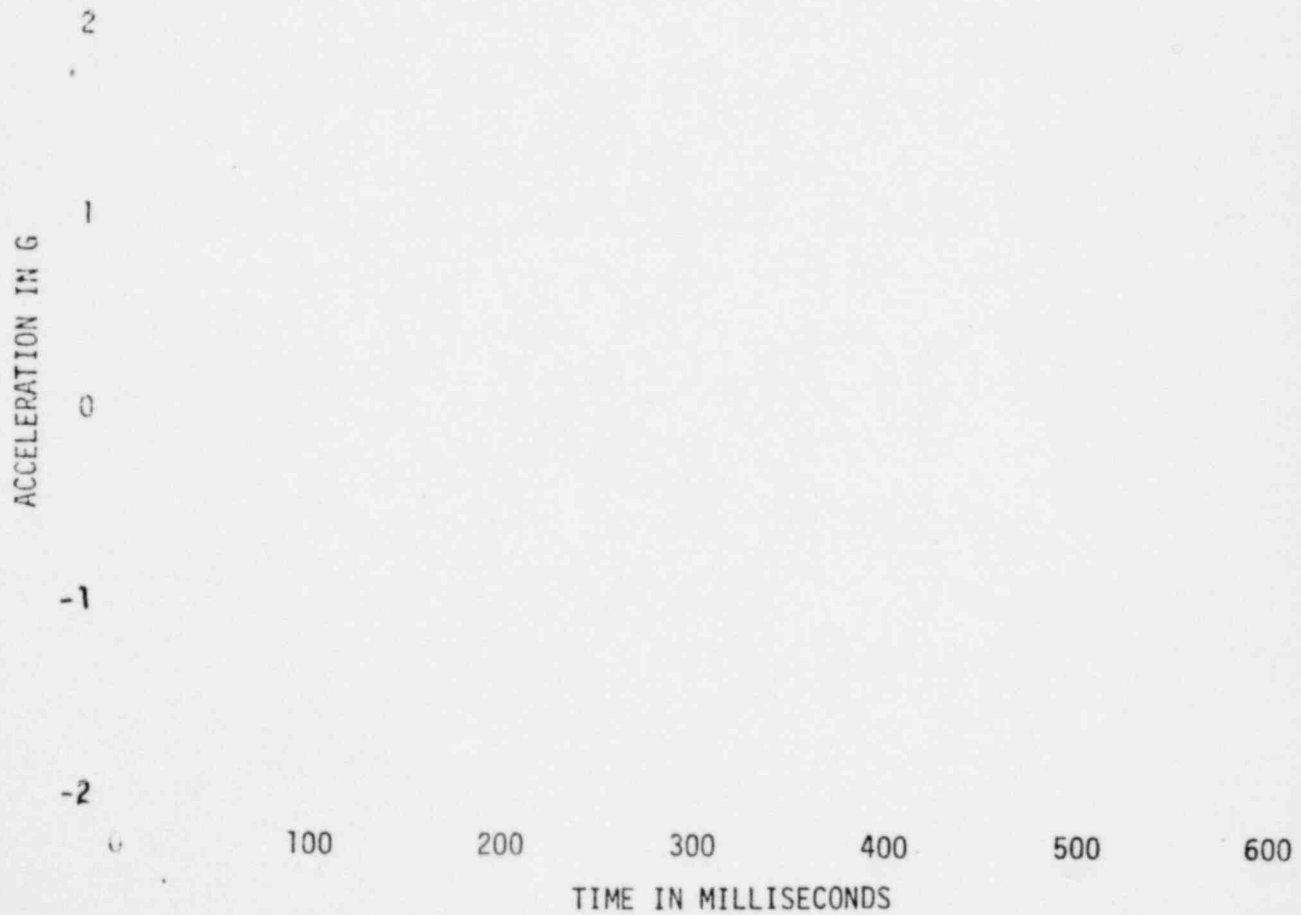


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FIGURE A-300

TORUS VERTICAL ACCELERATION

Task 5.5.3-2 Cooper Station Test 5



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FIGURE A-301

COMPARISON OF NET TORUS FORCE FROM PRESSURE INTEGRAL  
WITH NET TORUS FORCE FROM LOAD CELL CORRECTED FOR TORUS INERTIA

Task 5.5.3-2 Cooper Station Test 3



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COMPARISON OF NET TORUS FORCE FROM PRESSURE INTEGRAL  
WITH NET TORUS FORCE FROM LOAD CELL CORRECTED FOR TORUS INERTIA  
Task 5.5.3-2 Cooper Station Test 5



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FIGURE A-303

NET TORUS FORCE FROM PRESSURE INTEGRAL, CORRECTED FOR WATER INERTIA

Task 5.5.3-2 Cooper Station Test 3



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FIGURE A-304

NET TORUS FORCE FROM PRESSURE INTEGRAL, CORRECTED FOR WATER INERTIA

Task 5.5.3-2 Cooper Station Test 5

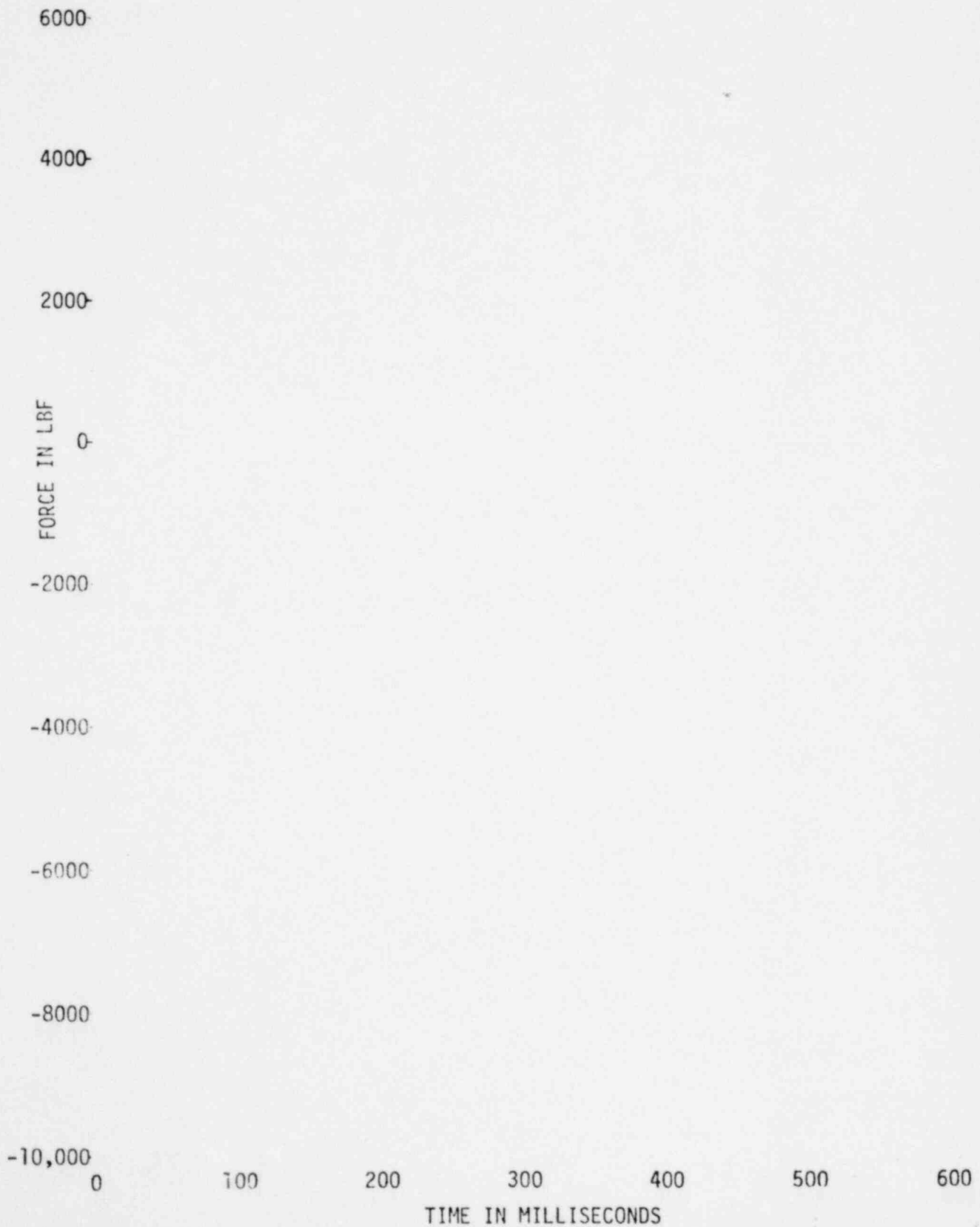


FIGURE A-305

AVERAGE POOL PRESSURE, CORRECTED FOR WATER INERTIA

Task 5.5.3-2 Cooper Station Test 3

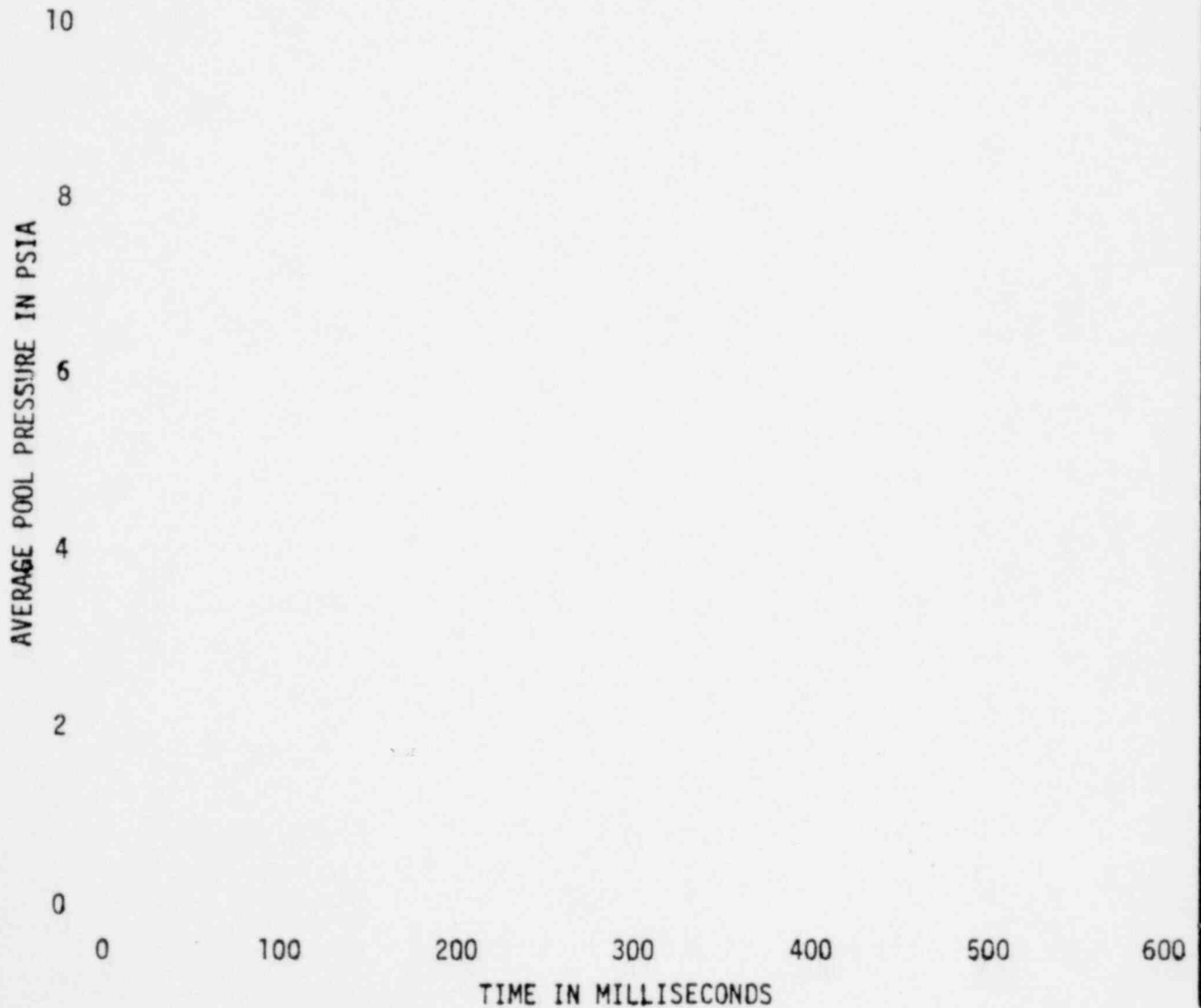


FIGURE A-306

NET AVERAGE POOL PRESSURE, CORRECTED FOR WATER INERTIA

Task 5.5.3-2 Cooper Station Test 3

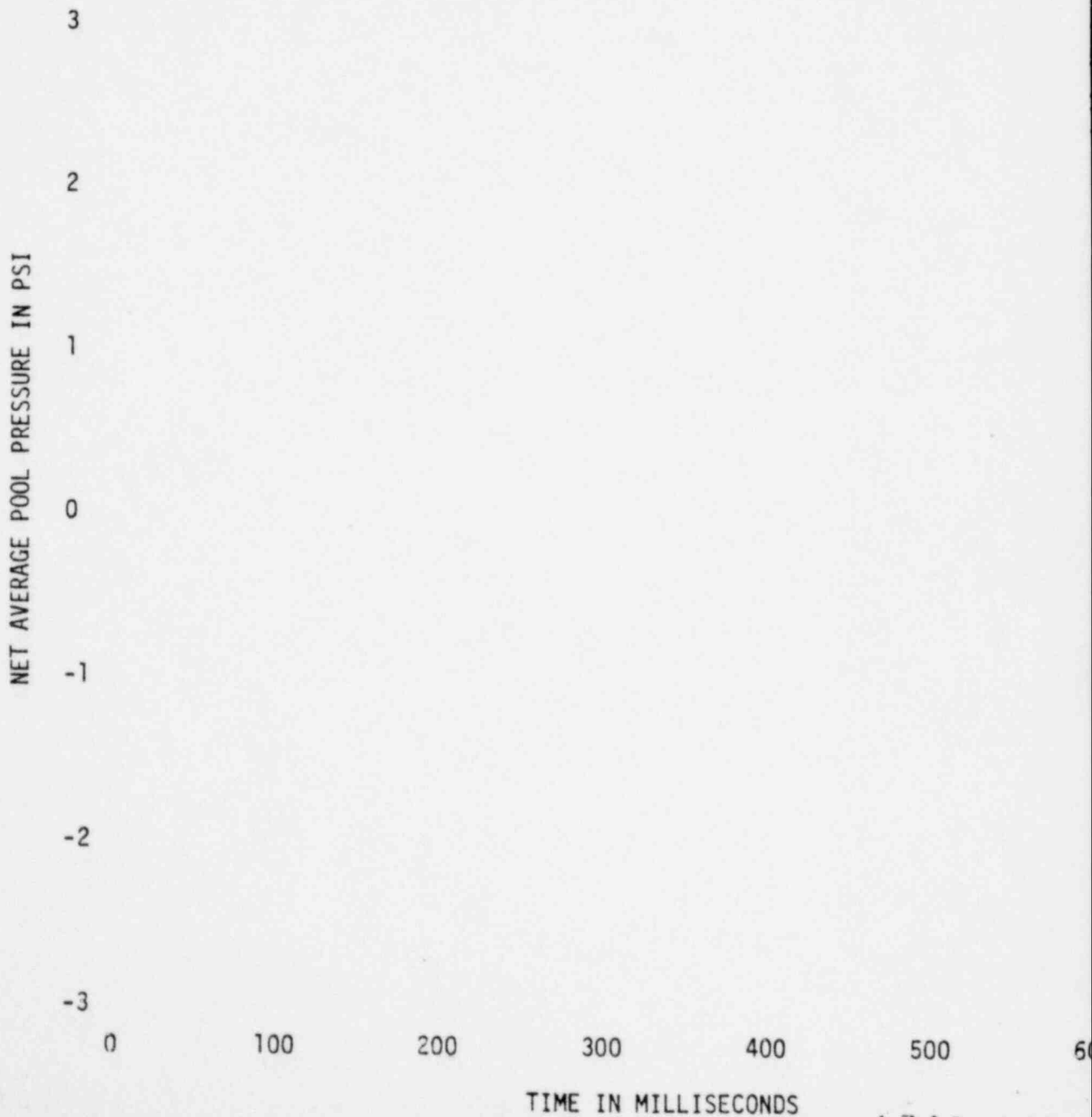
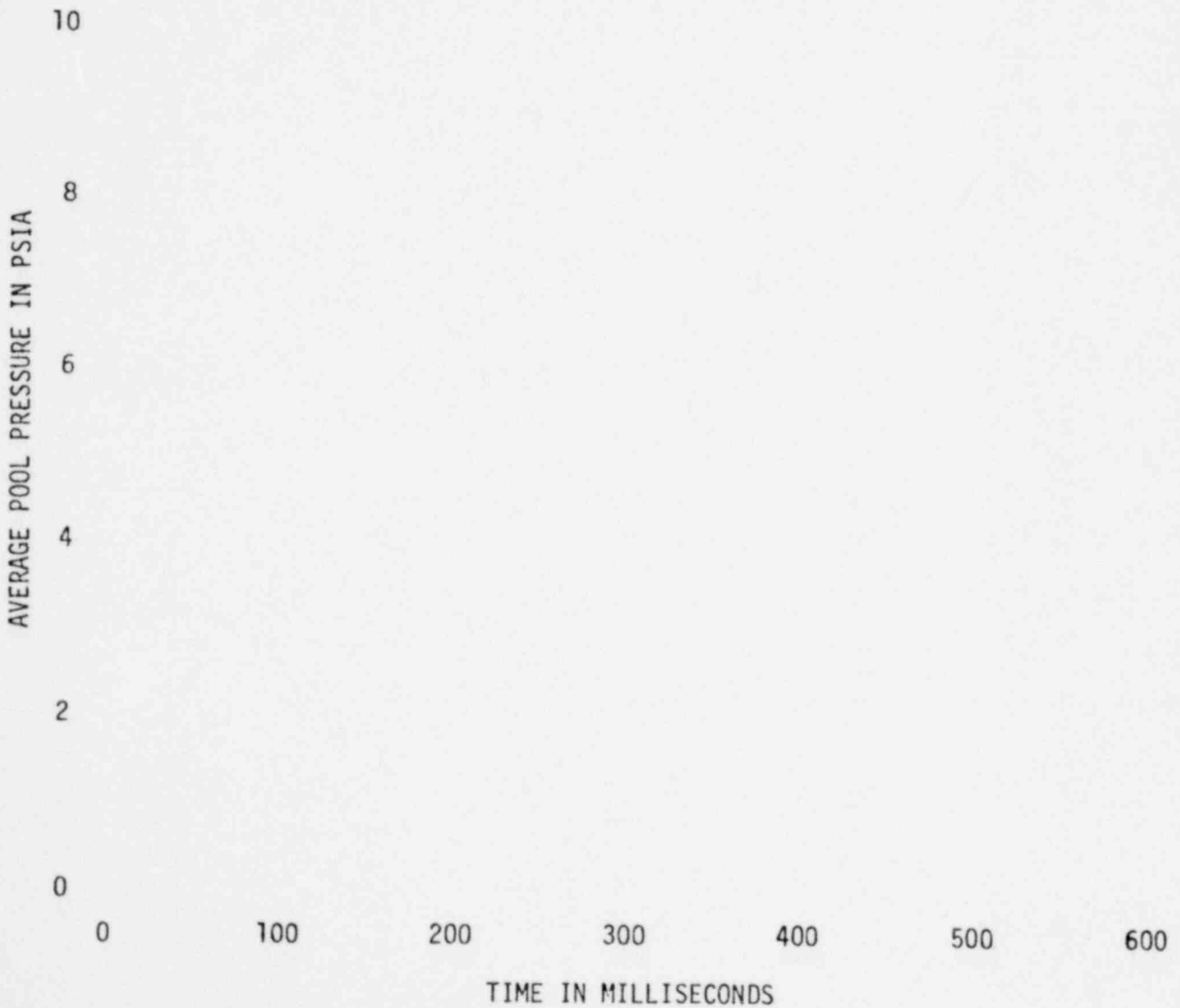


FIGURE A-307

AVERAGE POOL PRESSURE, CORRECTED FOR WATER INERTIA

Task 5.5.3-2 Cooper Station Test 5



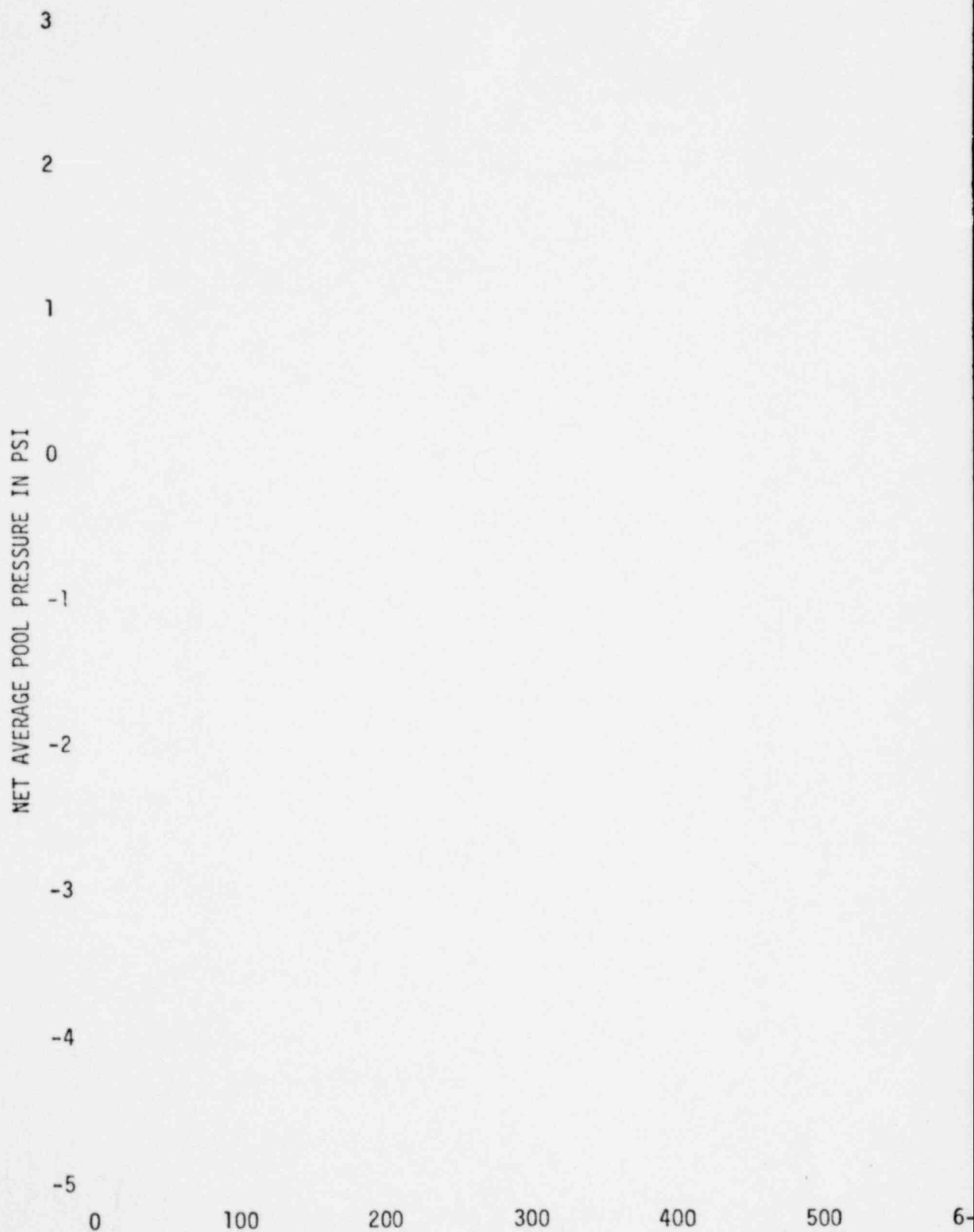
1349 129

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FIGURE A-308

NET AVERAGE POOL PRESSURE, CORRECTED FOR WATER INERTIA

Task 5.5.3-2 Cooper Station Test 5



TIME IN MILLISECONDS

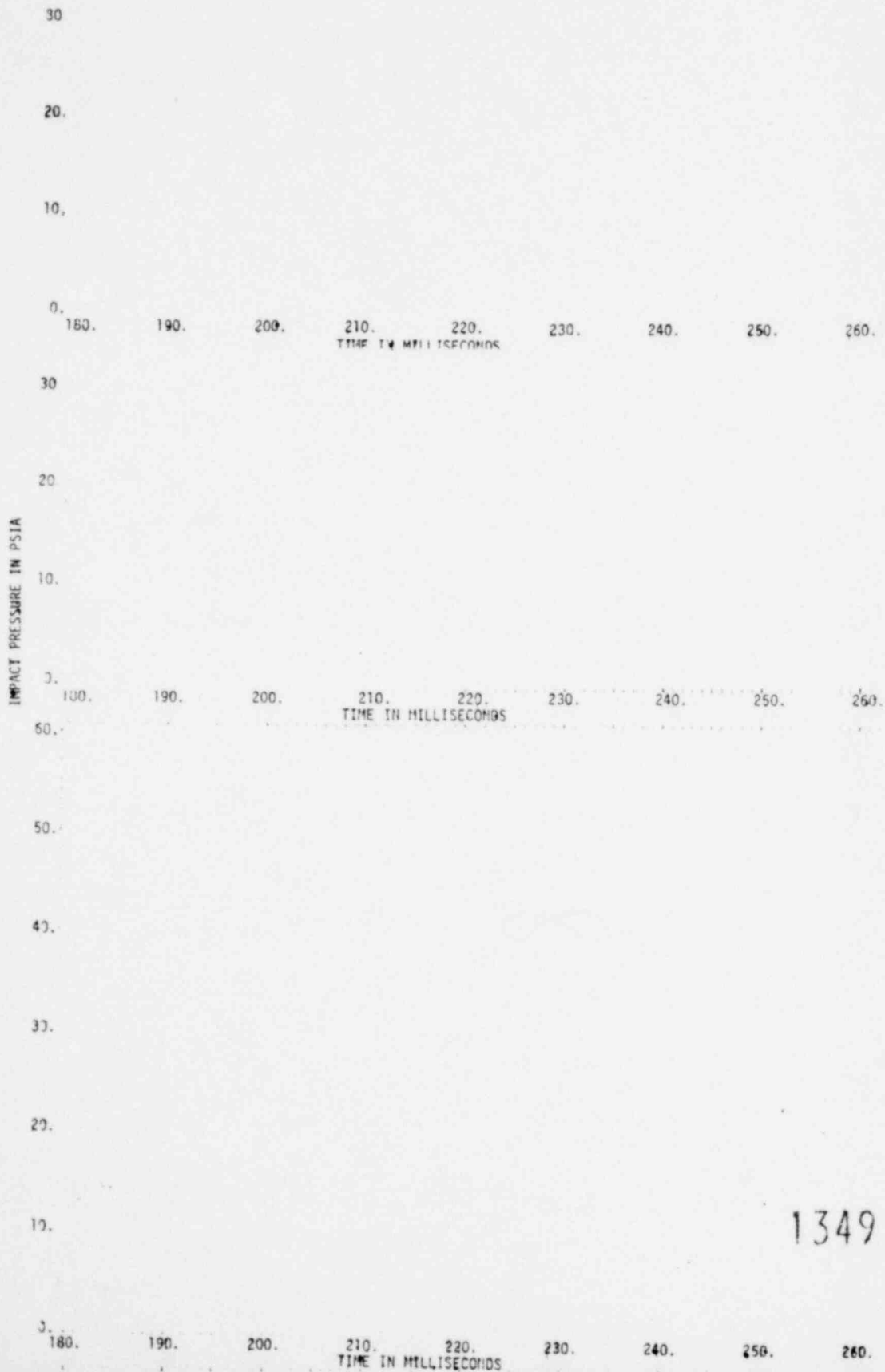
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FIGURE A-309

VENT HEADER IMPACT PRESSURES  
Task 5.5.3-2 Cooper Station Test 3

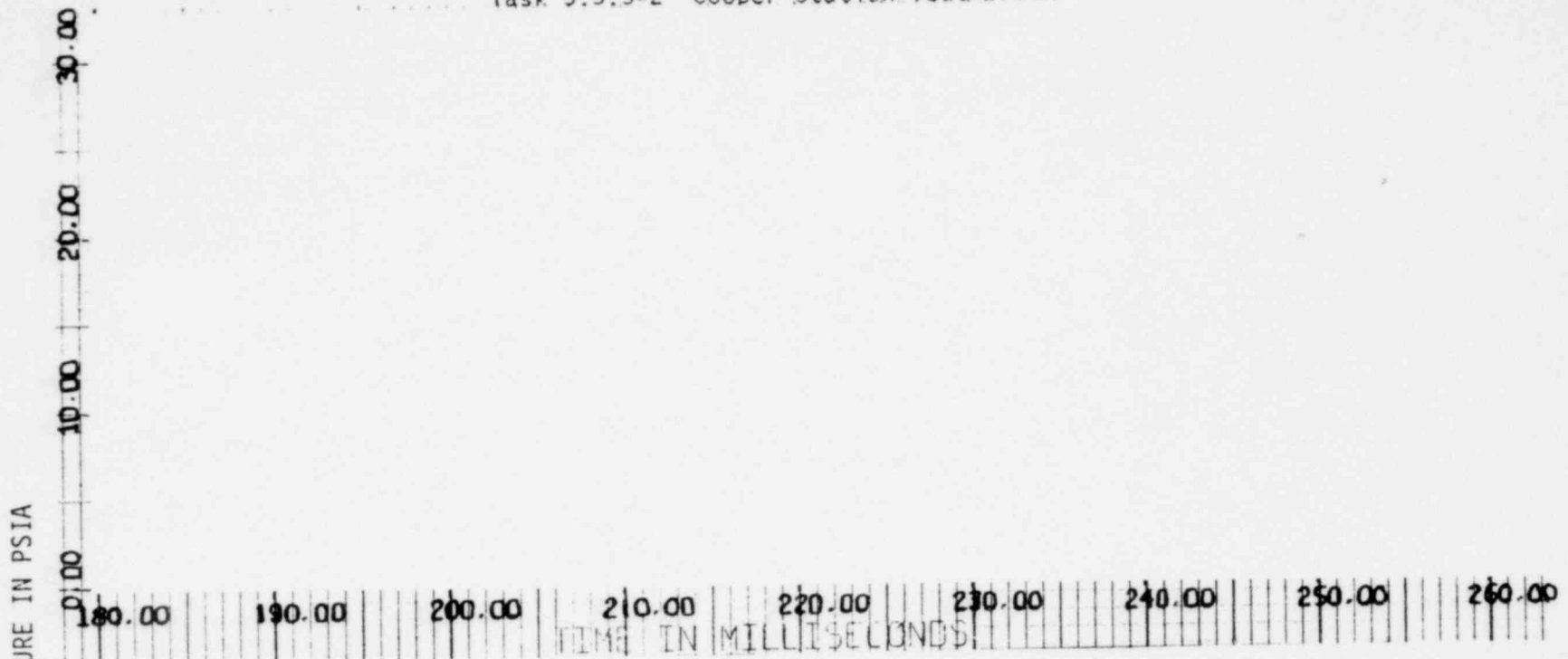


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FIGURE A-310

VENT HEADER IMPACT PRESSURES

Task 5.5.3-2 Cooper Station Test 3



No Data for Transducer (T7)

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# VENT HEADER IMPACT PRESSURES

Task 5.5.3-2 Cooper Station Test 3

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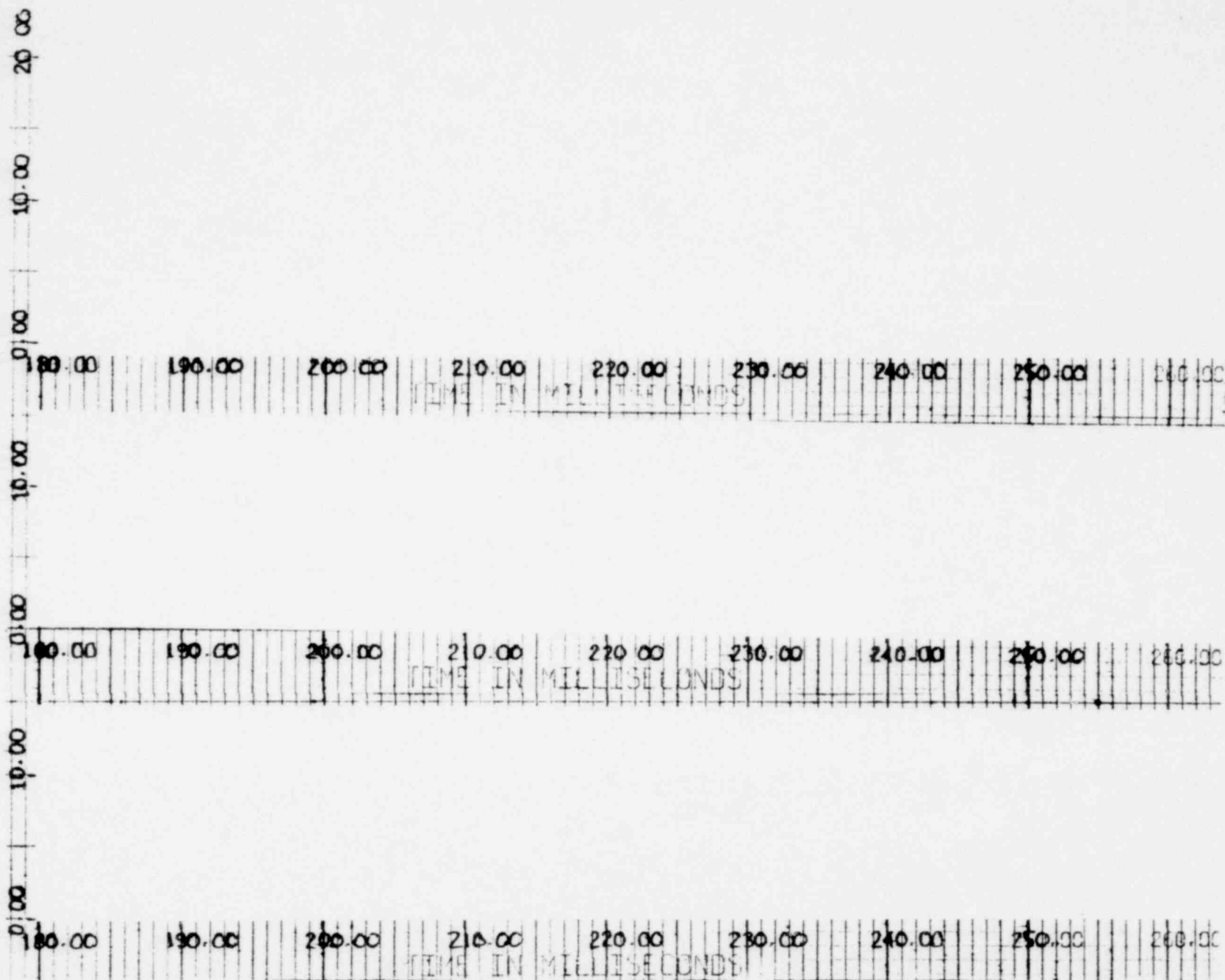


FIGURE A-312

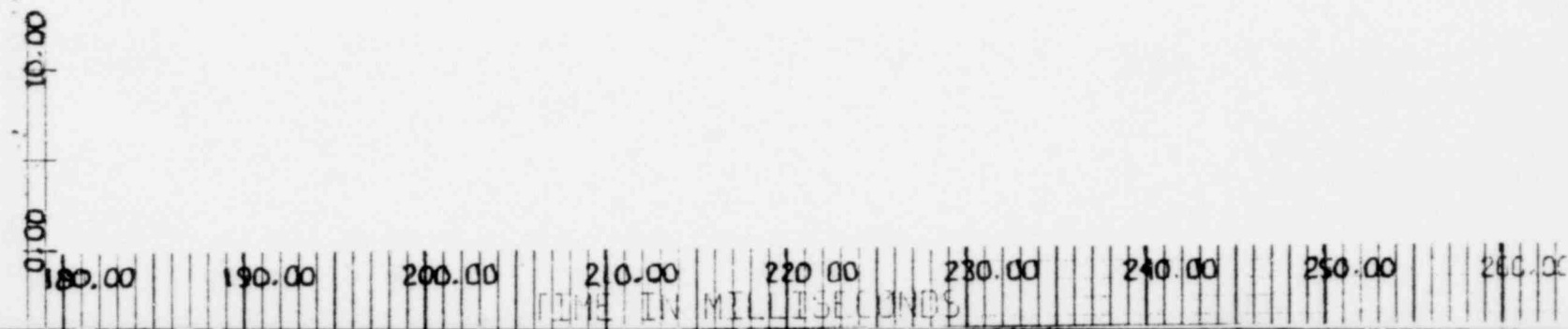
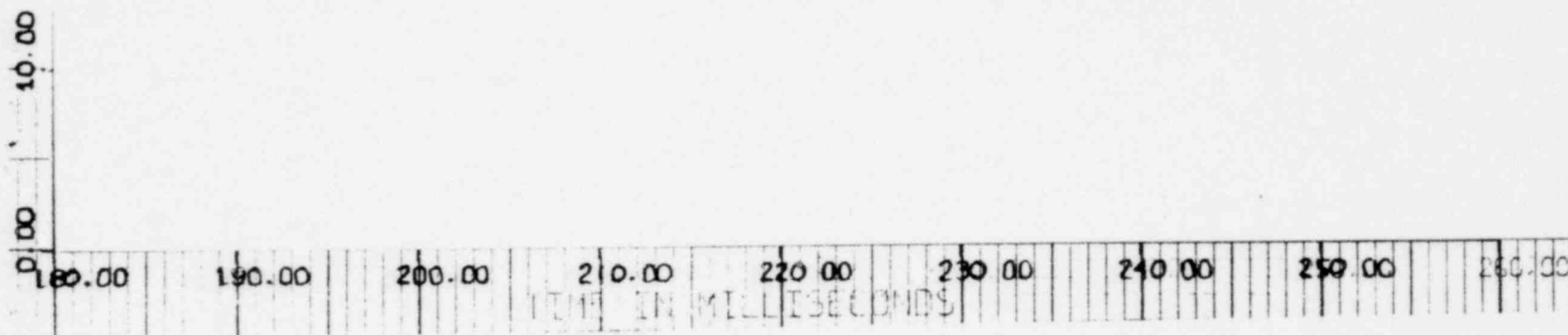
VENT HEADER IMPACT PRESSURES

Task 5.5.3-2 Cooper Station Test 3

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# VENT HEADER IMPACT PRESSURES

Task 5.5.3-2 Cooper Station Test 3

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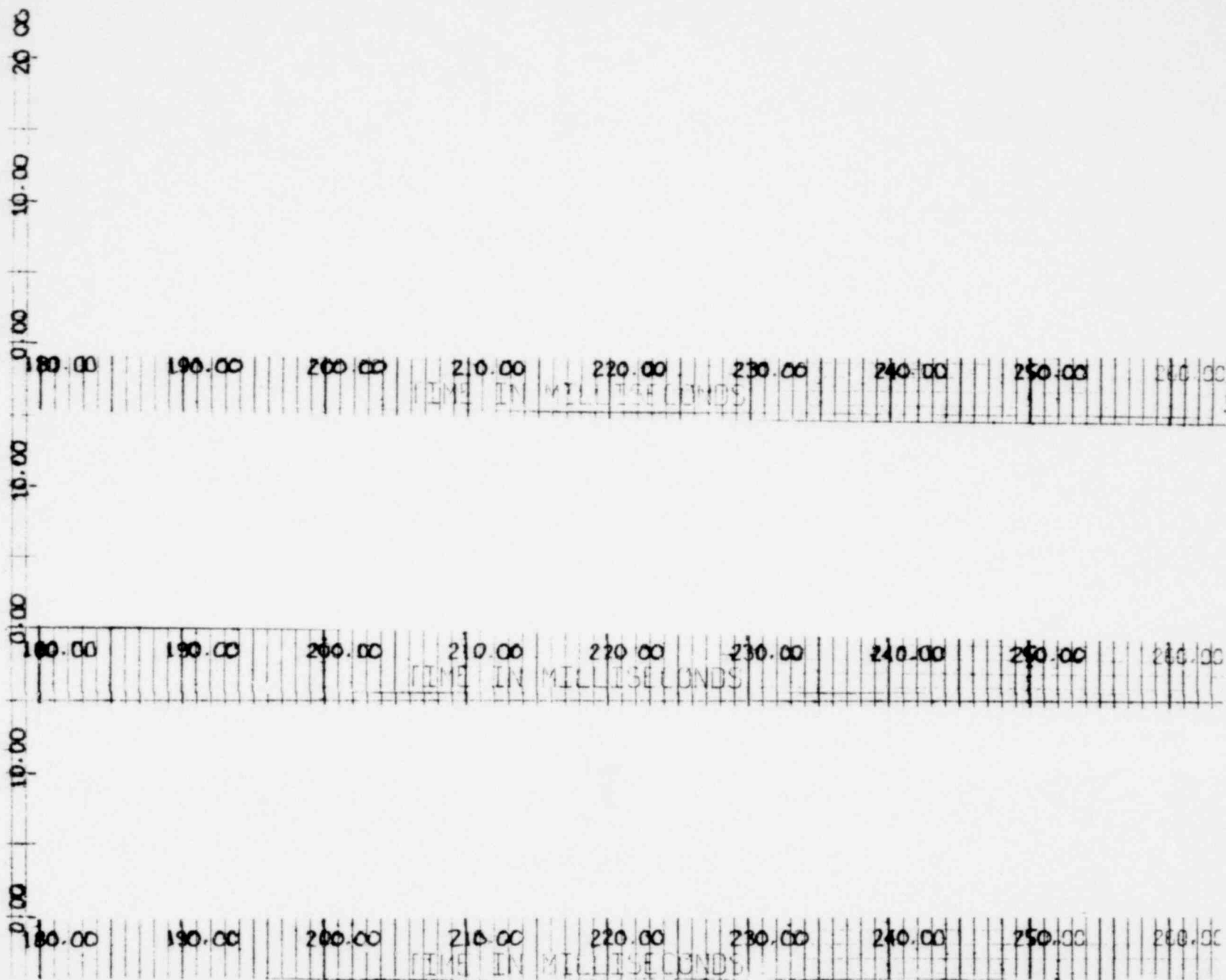
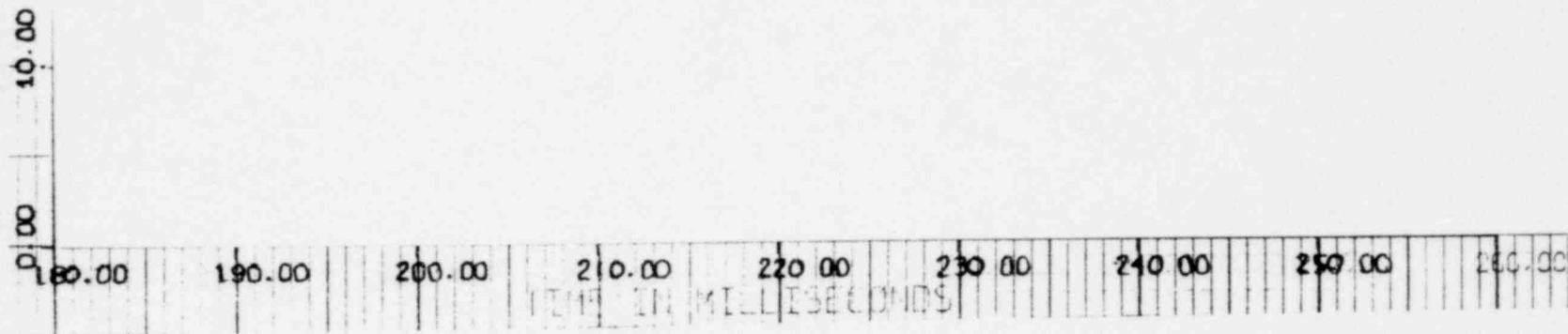


FIGURE A-312

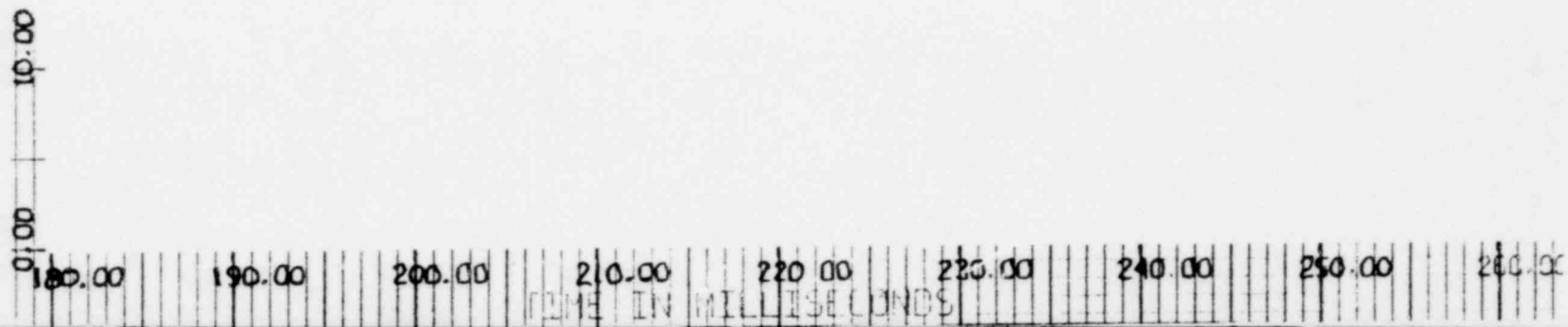
VENT HEADER IMPACT PRESSURES

Task 5.5.3-2 Cooper Station Test 3

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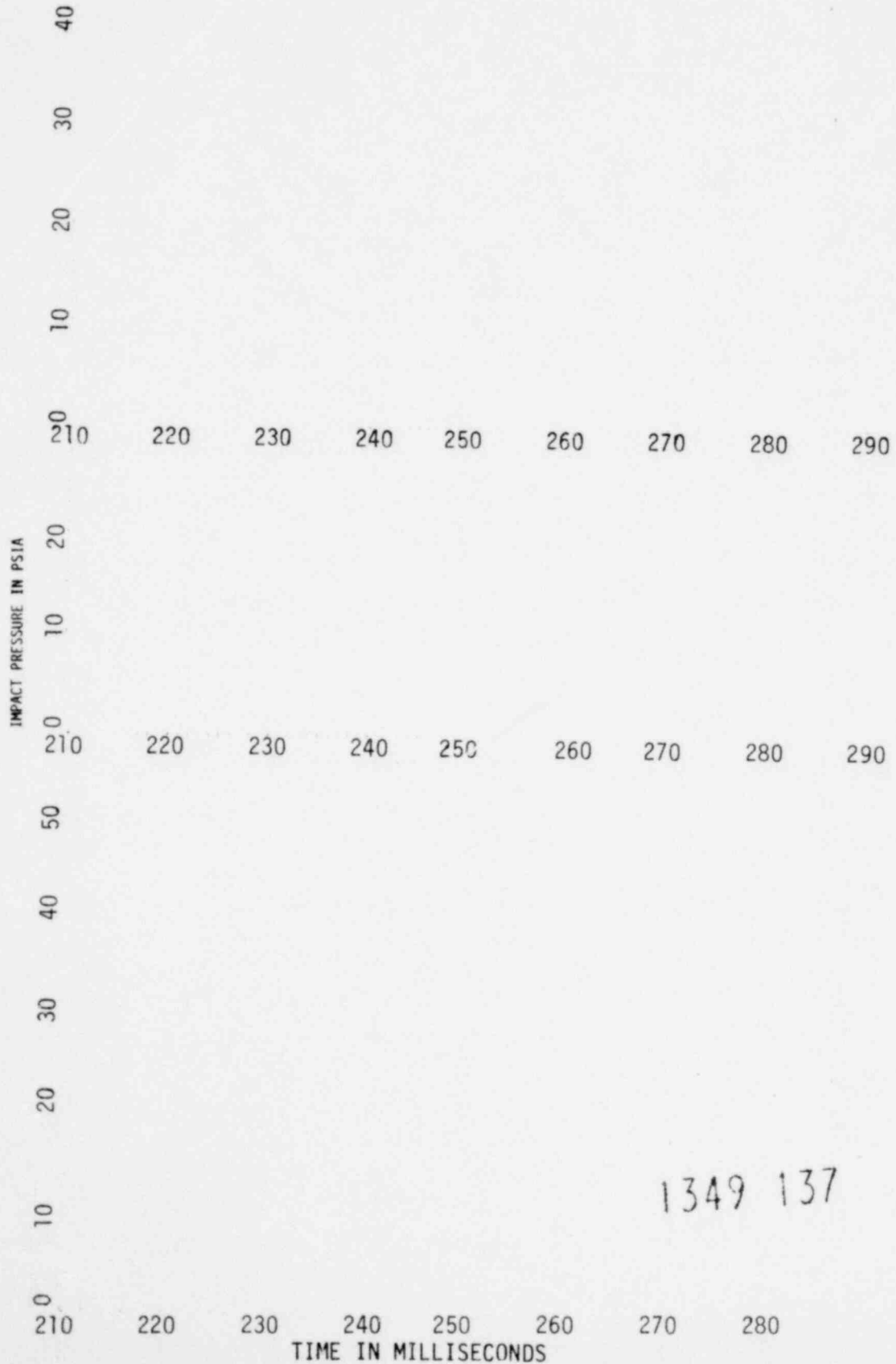
1349 136

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FIGURE A-313

VENT HEADER IMPACT PRESSURES

Task 5.5.3-2 Cooper Station Test 5



VENT HEADER IMPACT PRESSURES

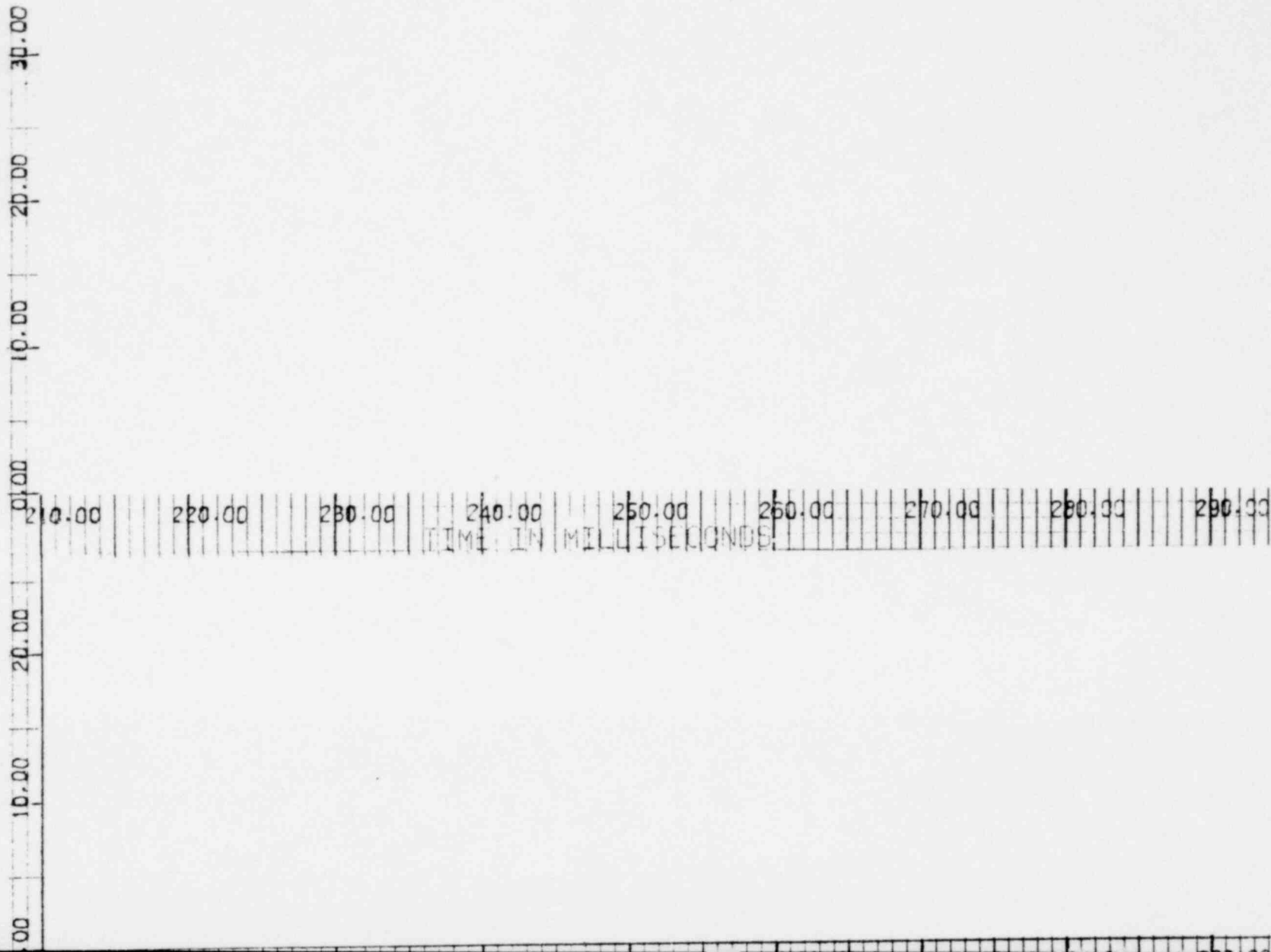
FIGURE A-314

Task 5.5.3-2 Cooper Station Test 5

A-362

IMPACT PRESSURE IN PSIA

1349 138



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FIGURE A-315

VENT HEADER IMPACT PRESSURES

Task 5.5.3-2 Cooper Station Test 5

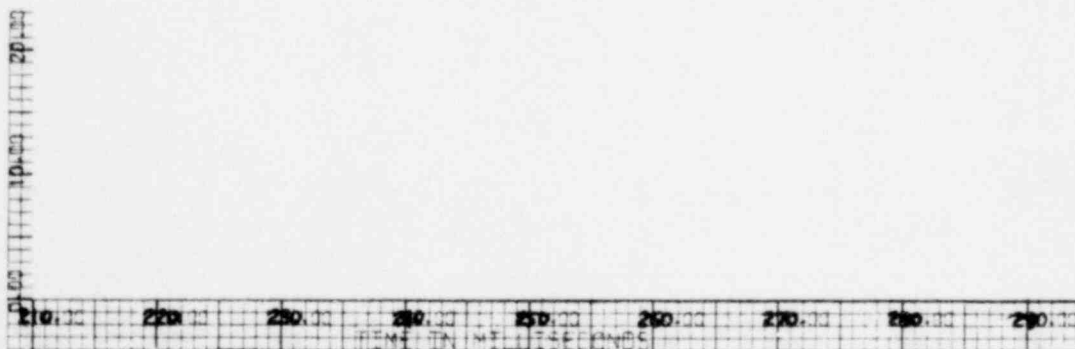
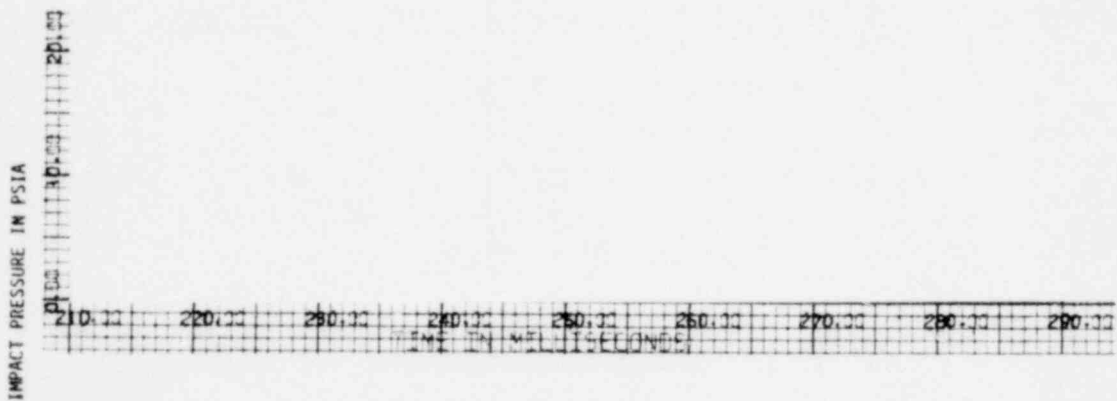
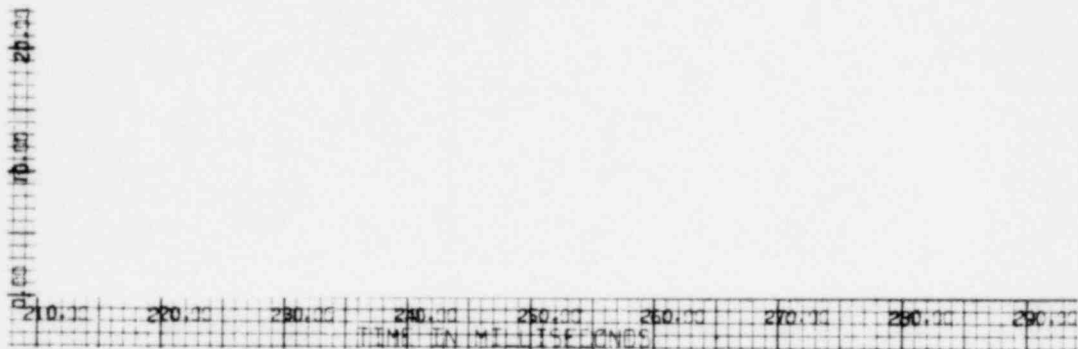
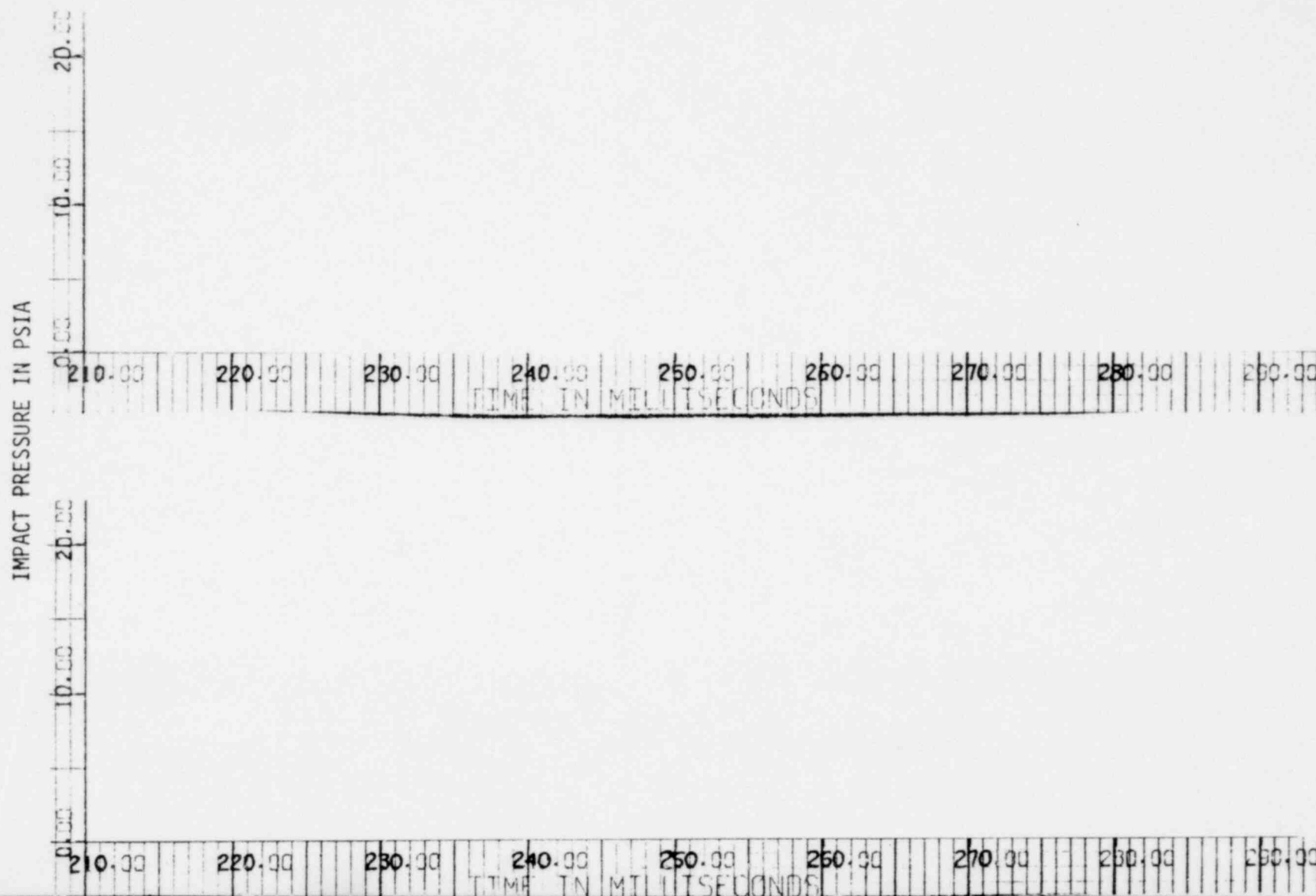


FIGURE A-316

VENT HEADER IMPACT PRESSURES

Task 5.5.3-2 Cooper Station Test 5



A-364

1349 140

NEDO-21944

FIGURE A-317

COMPARISON OF VENT HEADER IMPACT RESULTS  
(Corrected Load Cell and Pressure Integration)  
Task 5.5.3 Cooper Station Tests 3, 5

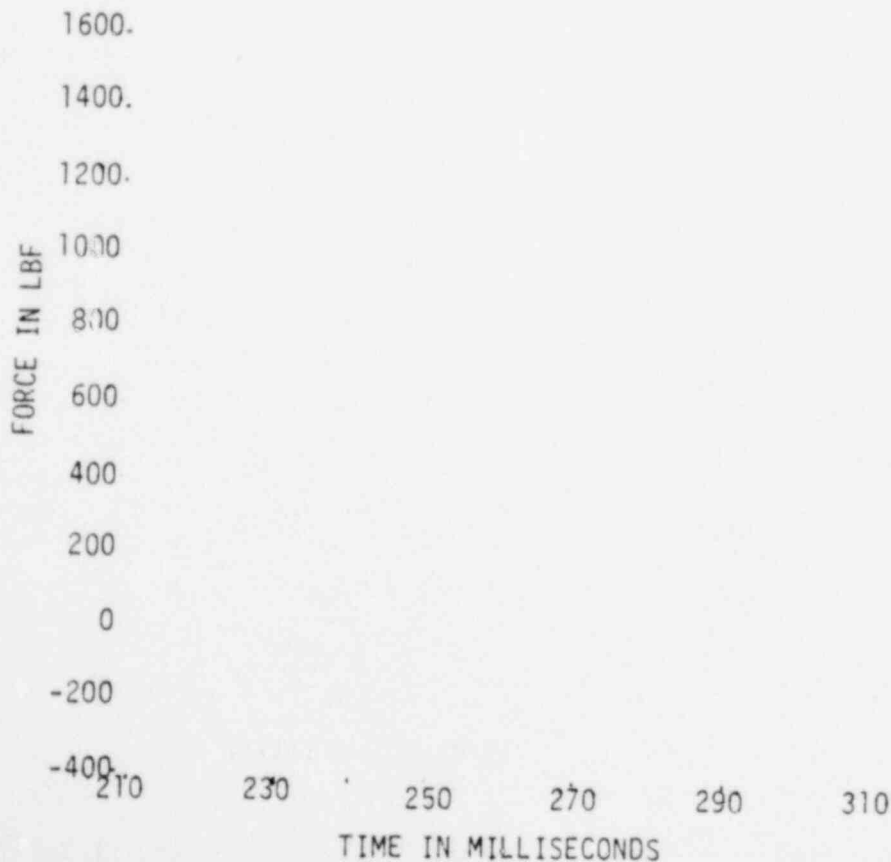
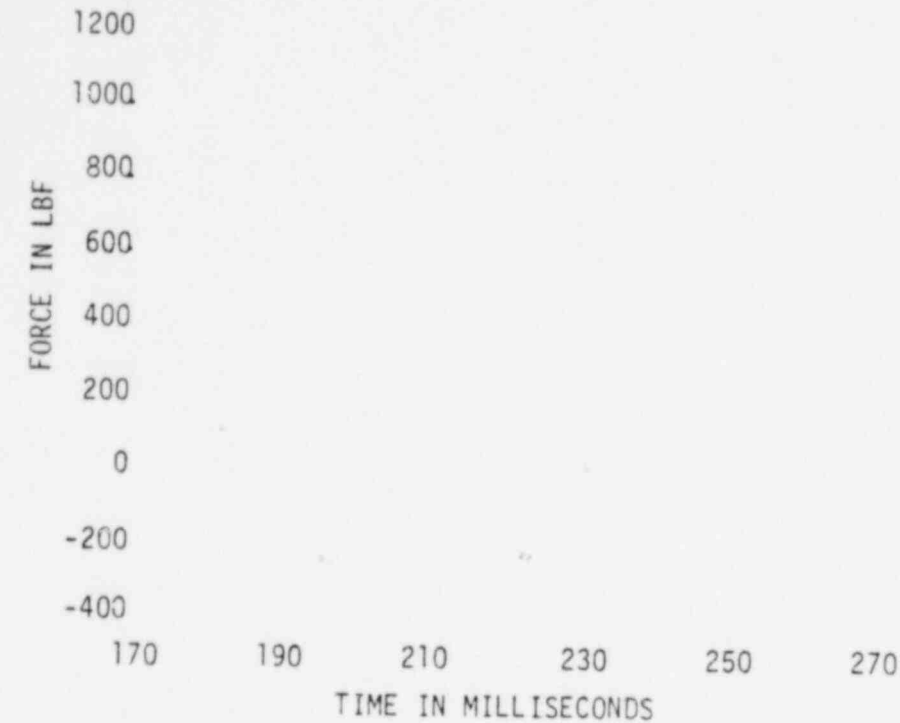
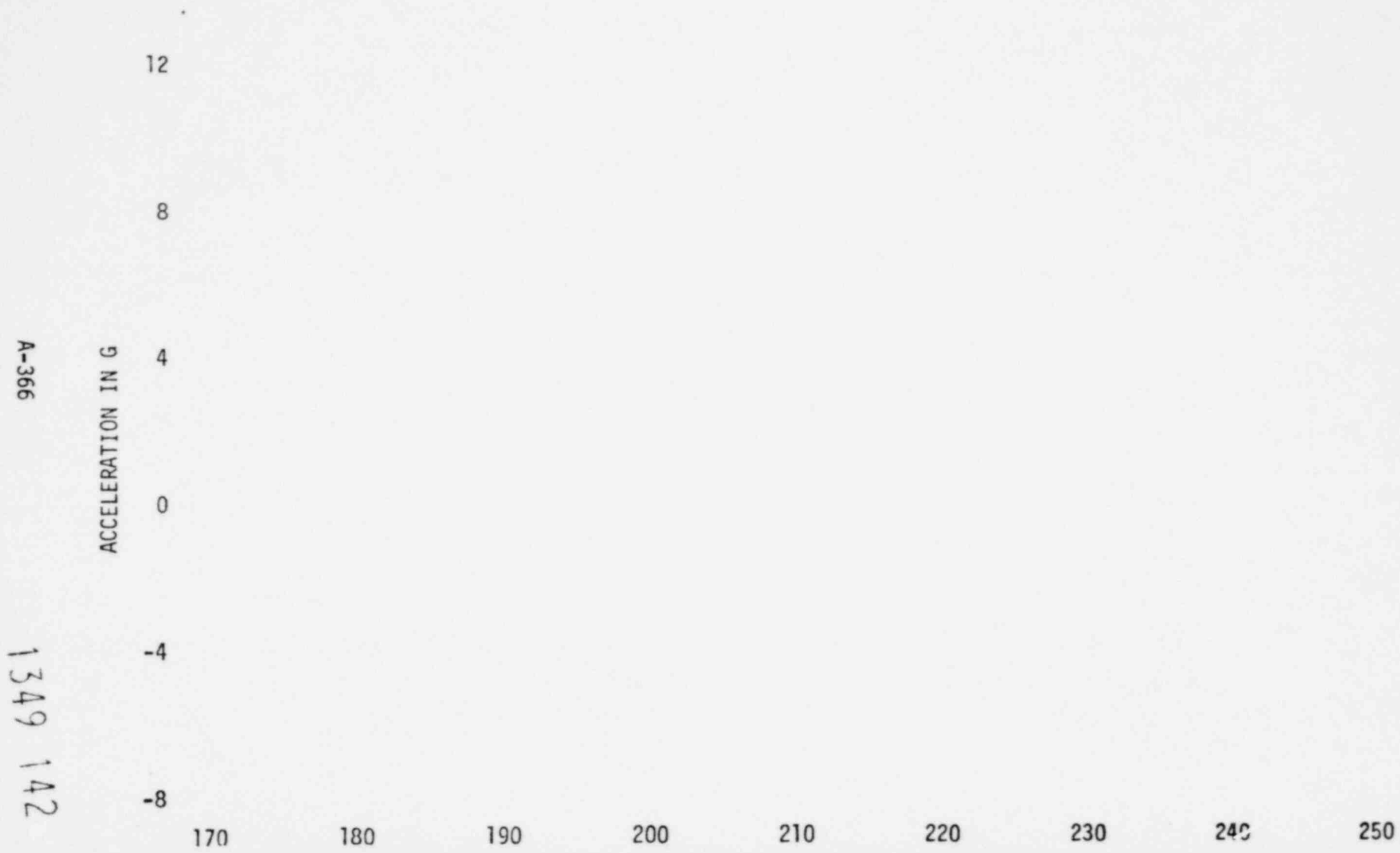


FIGURE A-318

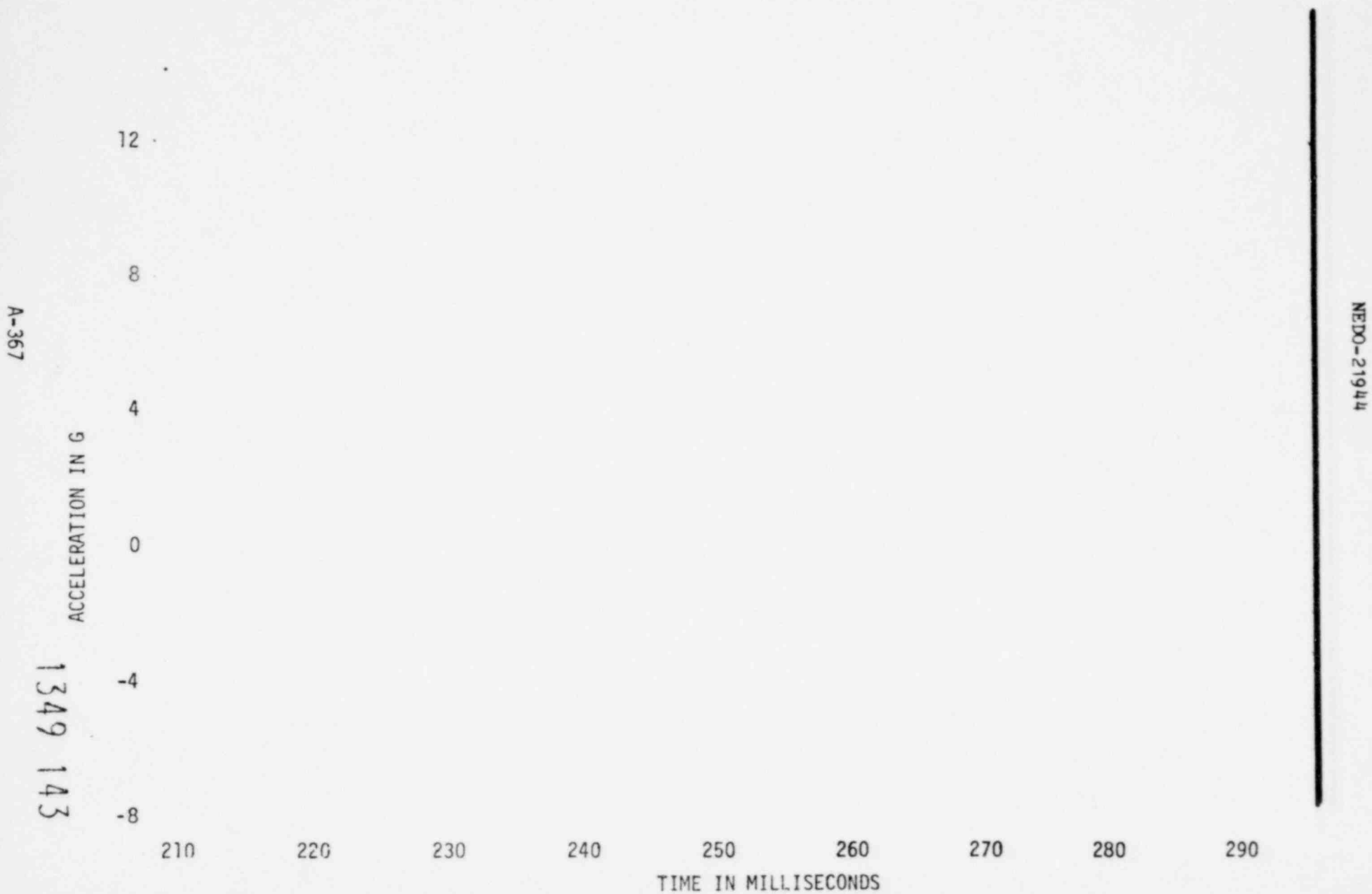
VENT HEADER VERTICAL ACCELERATION  
Task 5.5.3-2 Cooper Station Test 3



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VENT HEADER VERTICAL ACCELERATION  
Task 5.5.3-2 Cooper Station Test 5

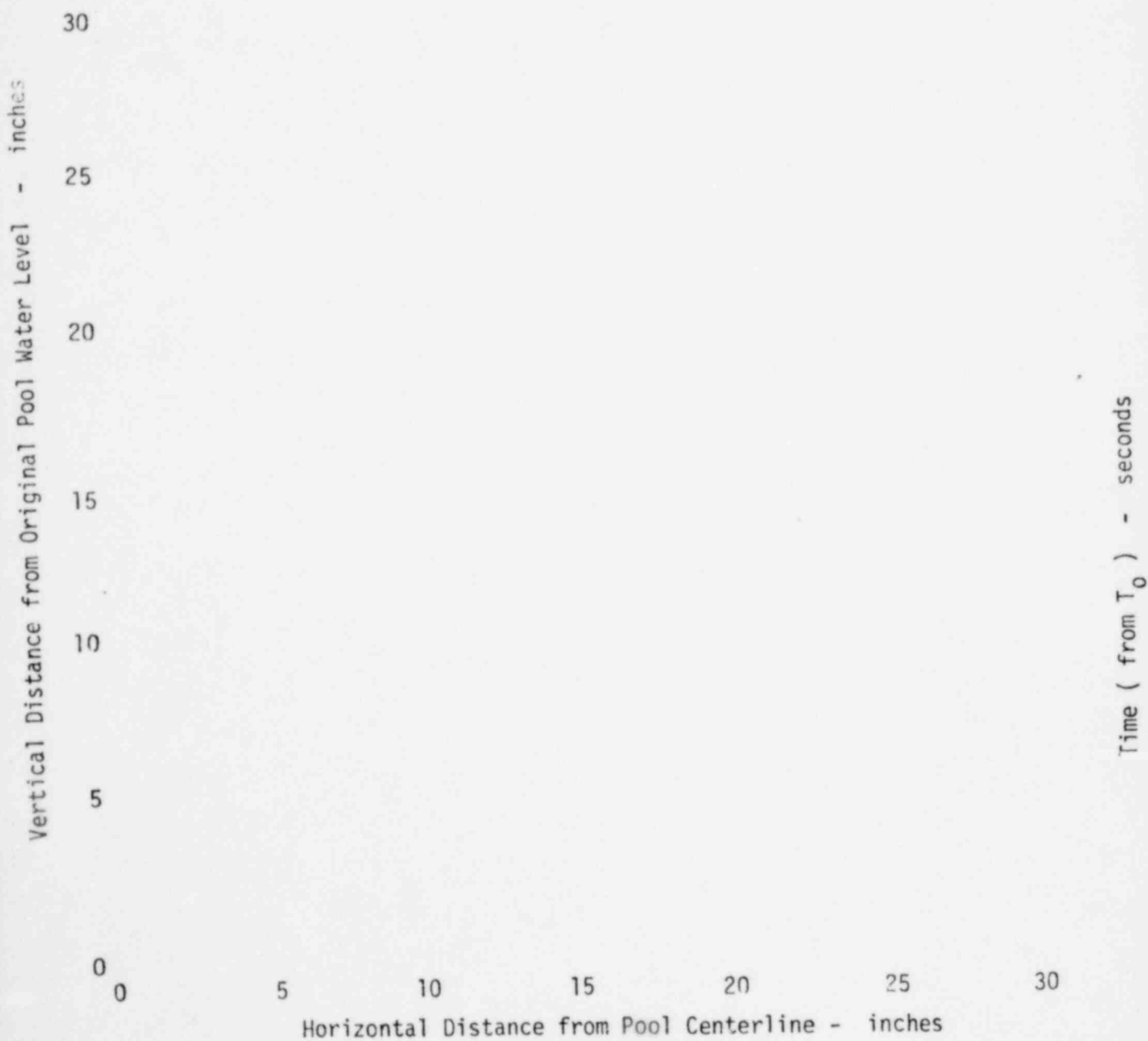


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FIGURE A-320

TIME HISTORY OF  
POOL REPLACEMENT

COOPER STATION, TEST 1



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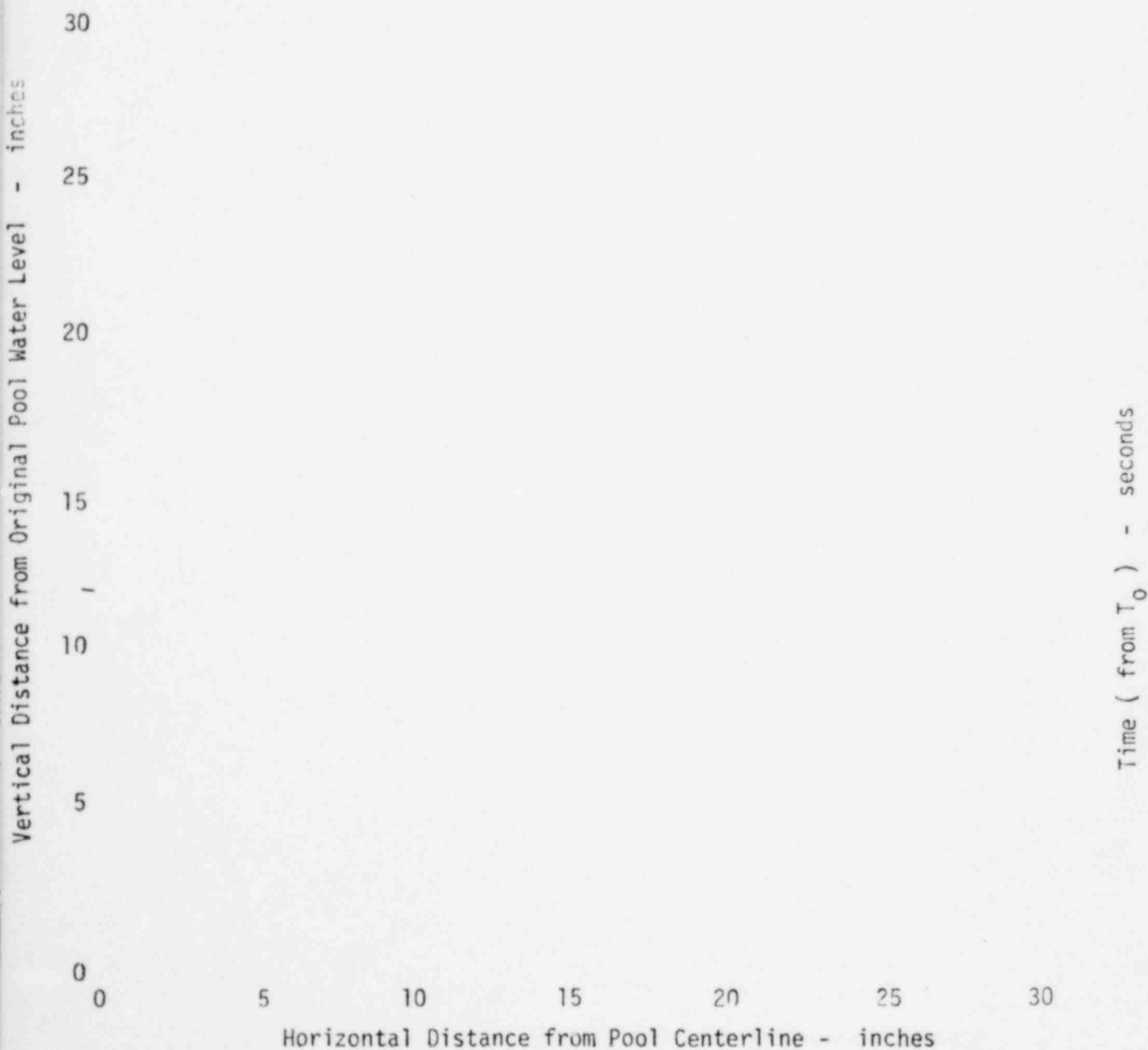
1349 144

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FIGURE A-321

TIME HISTORY OF  
POOL DISPLACEMENT

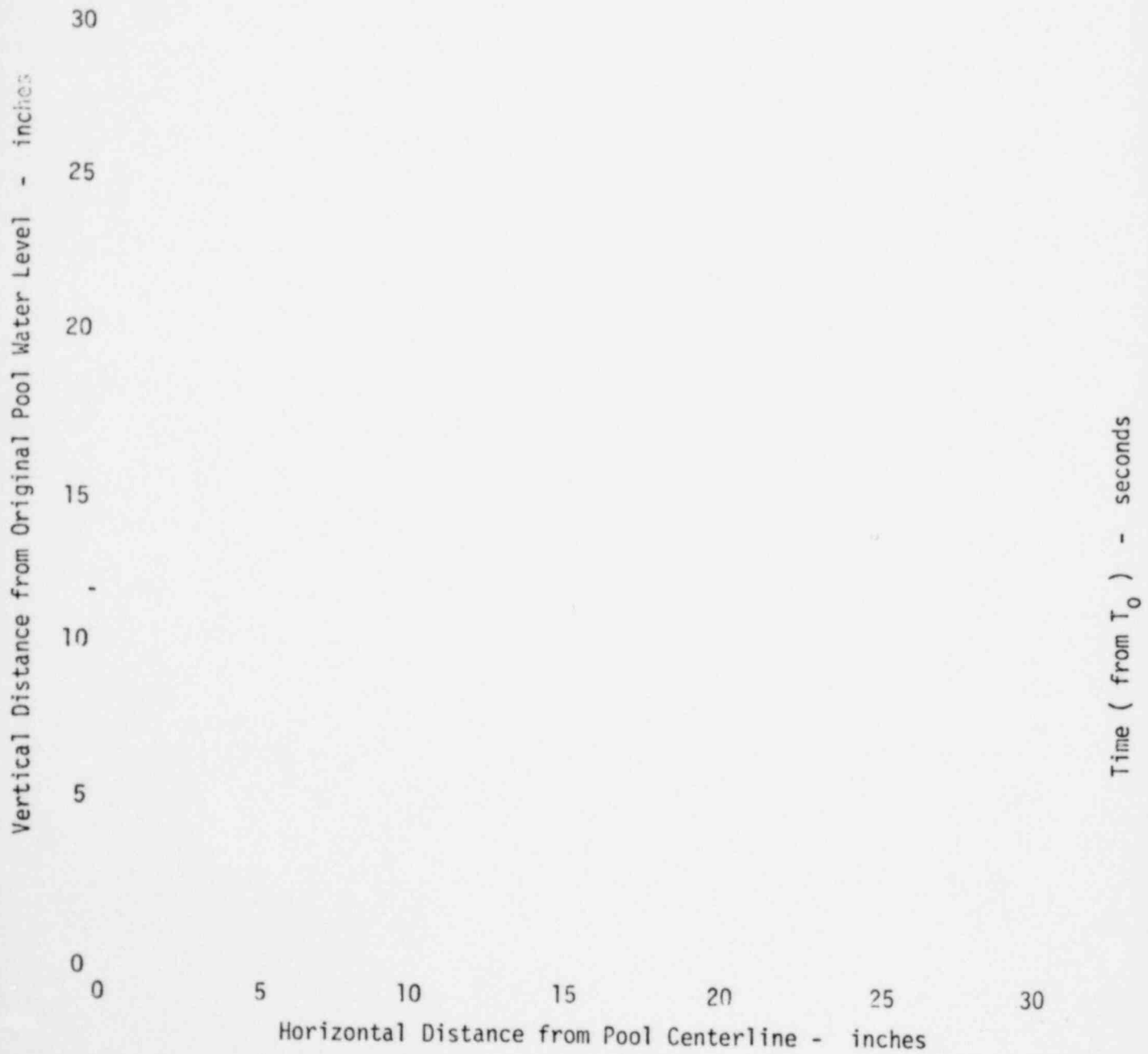
COOPER STATION, TEST 2



NEDO-21944  
FIGURE A-322

TIME HISTORY OF  
POOL DISPLACEMENT

COOPER STATION, TEST 3

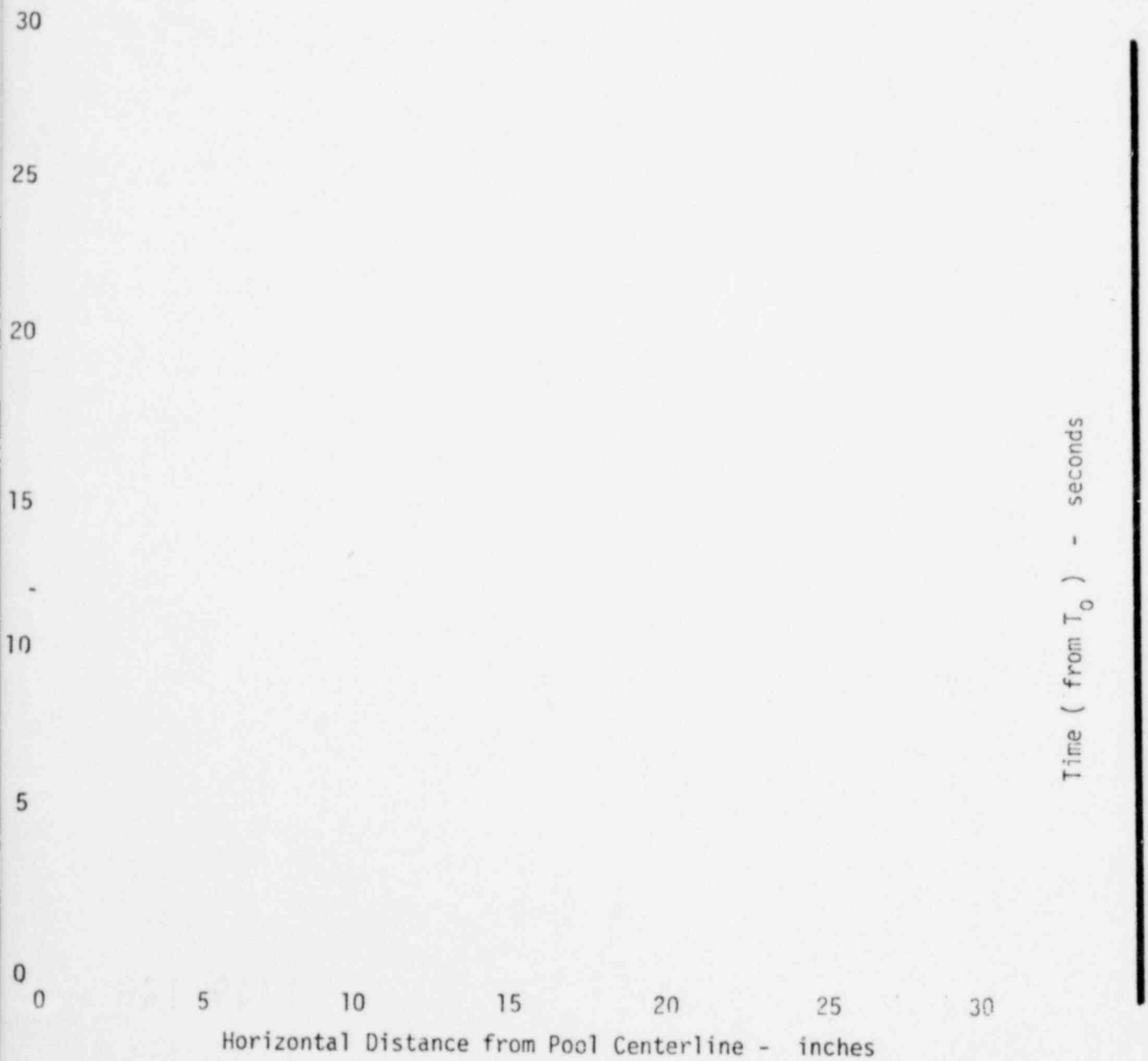


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FIGURE A-323

TIME HISTORY OF  
POOL DISPLACEMENT

COOPER STATION, TEST 5



POOL SURFACE DISPLACEMENT

FIGURE A-324

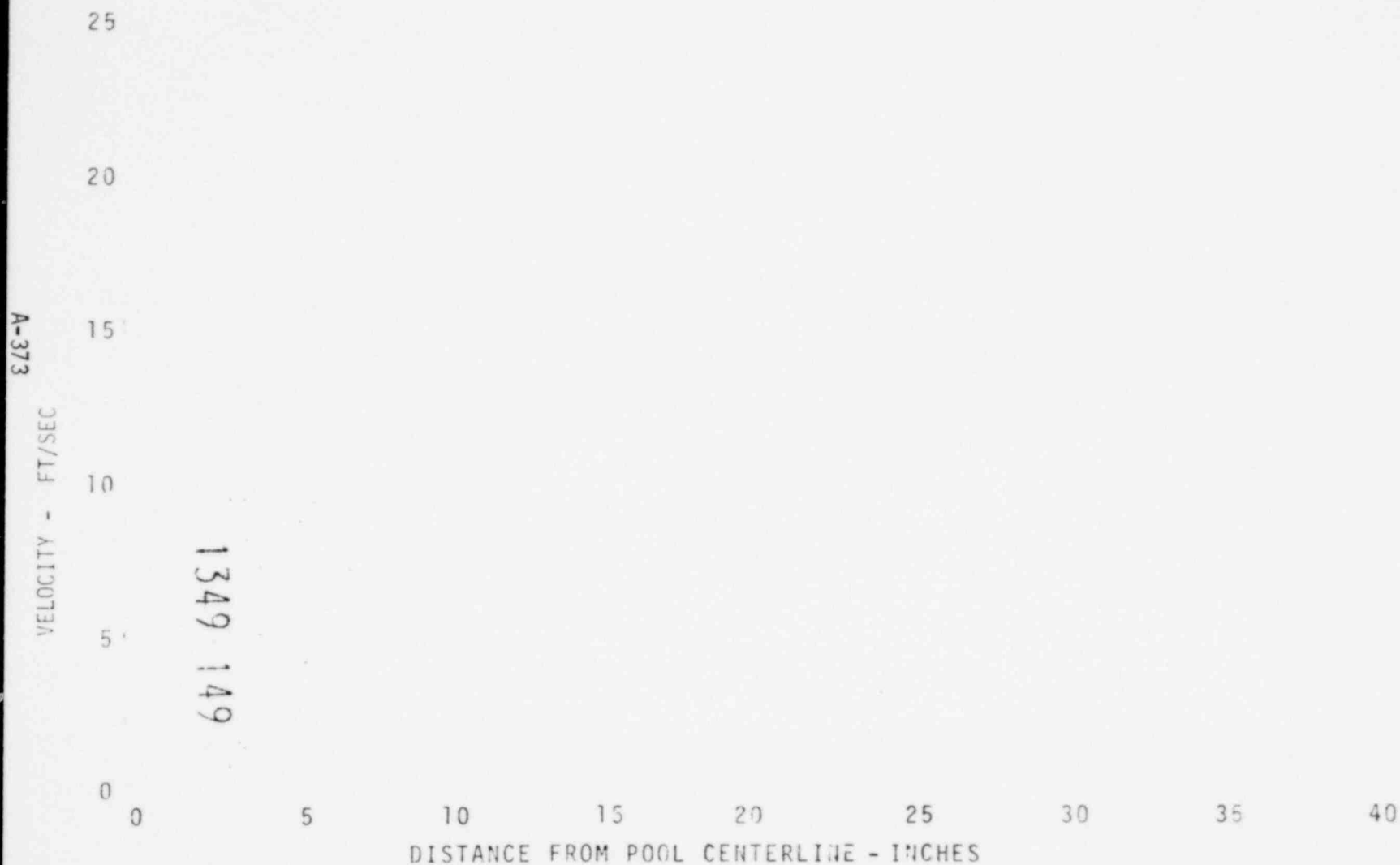
COOPER STATION, TESTS 1, 2, 3



FIGURE A-325

POOL SURFACE VELOCITY PROFILES

COOPER STATION TESTS 1, 2, 3



NUCLEAR SERVICES CORPORATION

NEED-21944

NUCLEAR SERVICES CORPORATION

POOL SURFACE DISPLACEMENT

FIGURE A-326

COOPER STATION, TEST 5

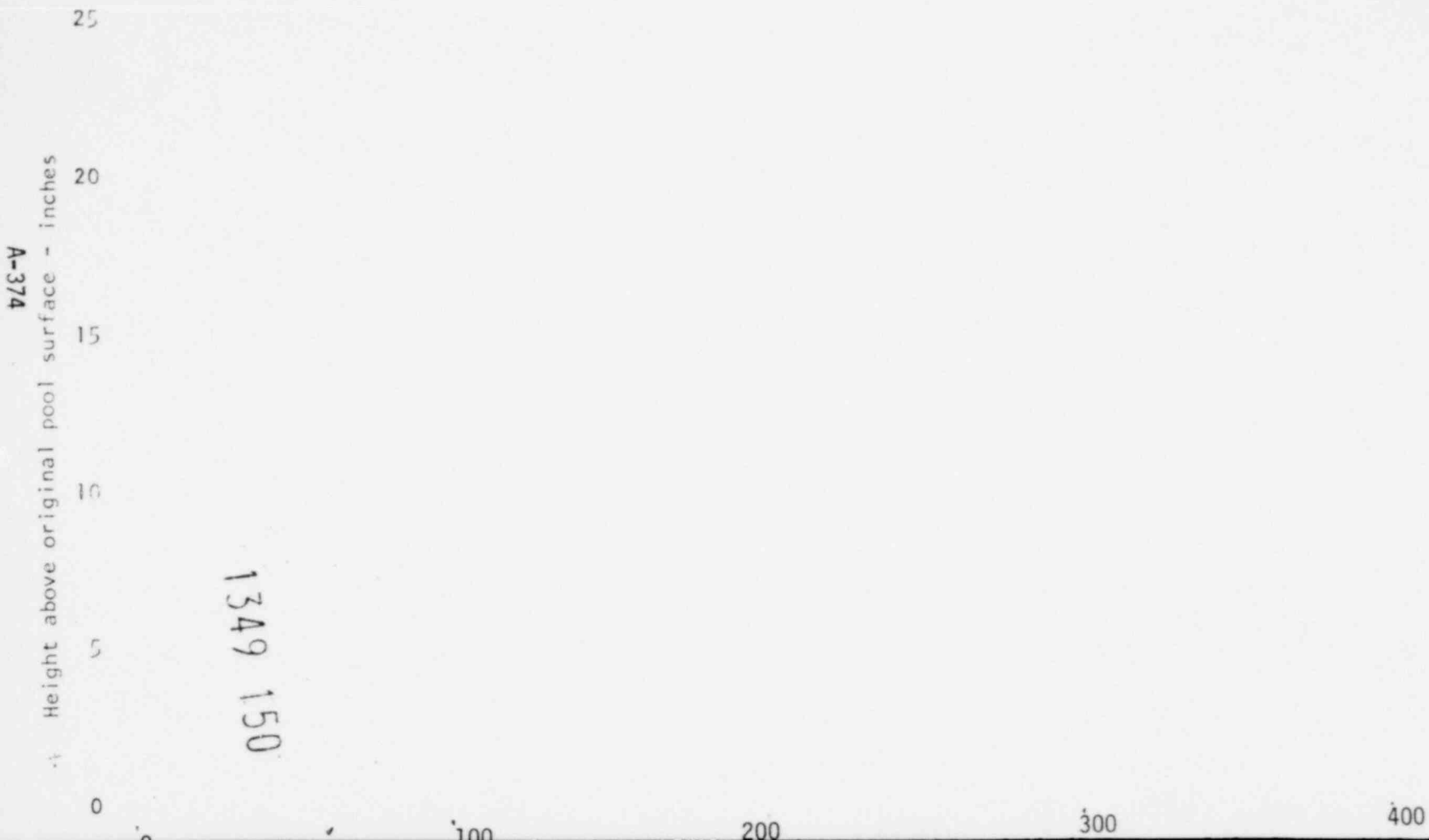
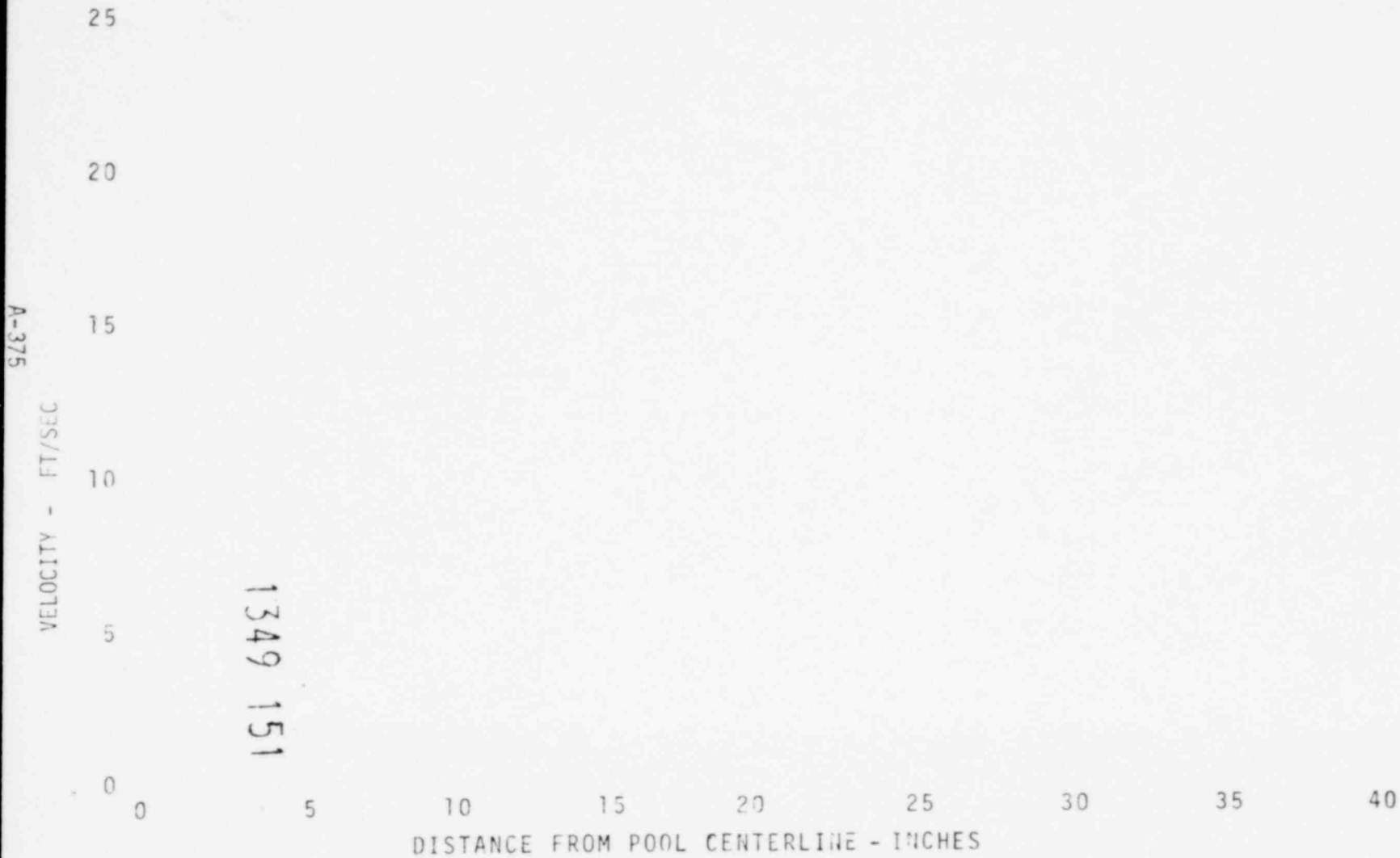


FIGURE A-327

COOPER STATION, TEST 5



NUCLEAR SERVICES CORPORATION

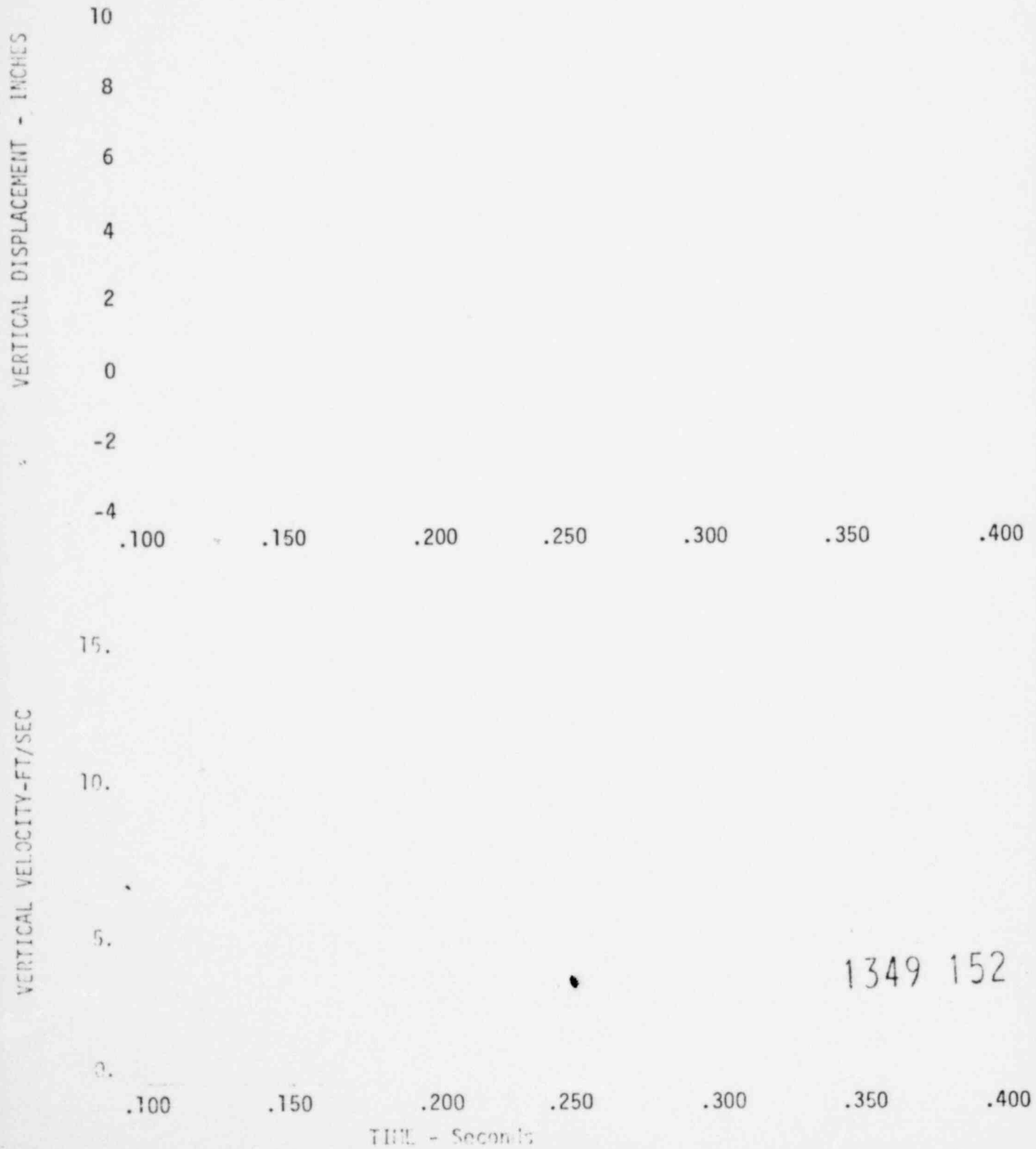
NEDO-21944

NEDO-21944

FIGURE A-328

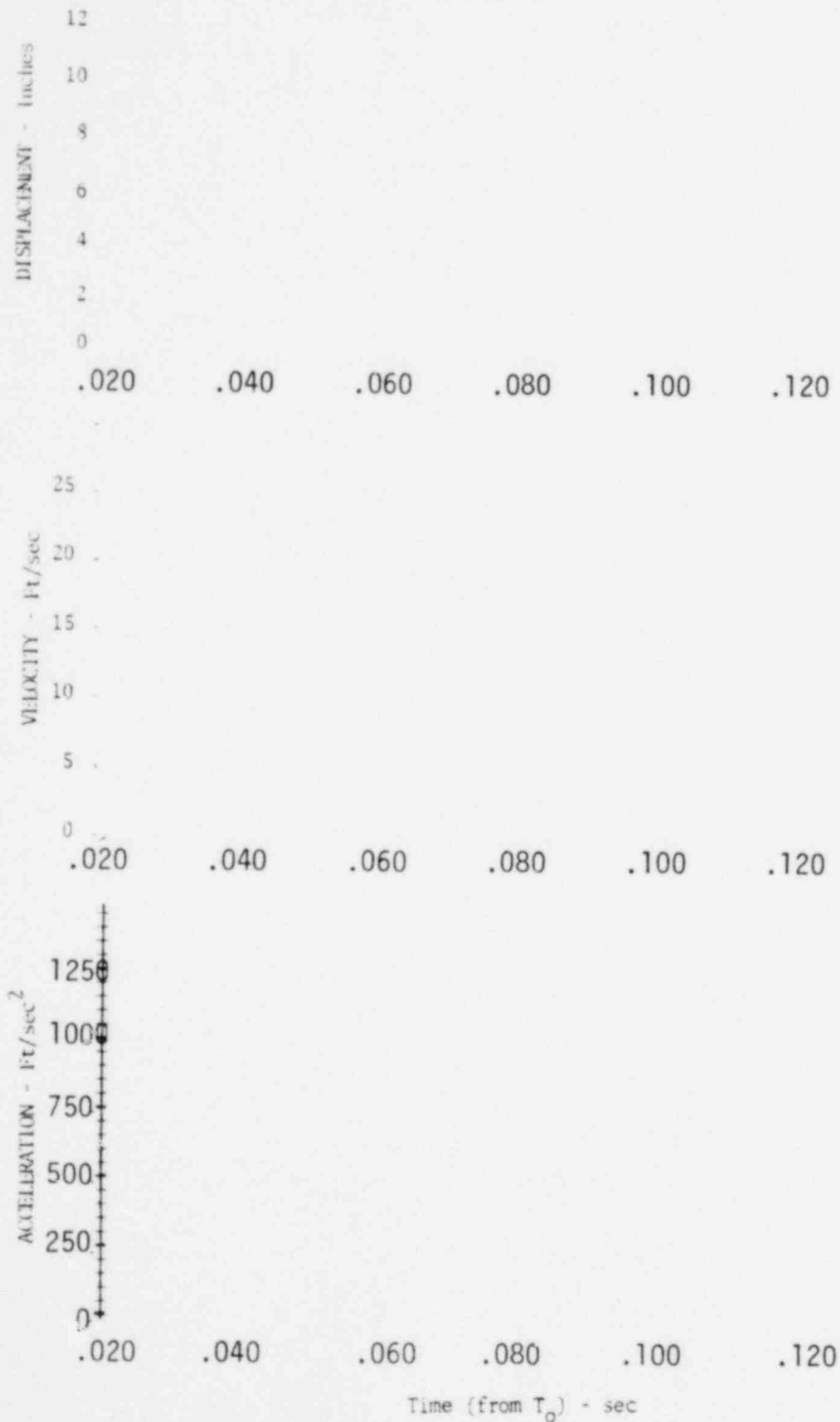
SIDE WINDOW DISPLACEMENT AND VELOCITY PROFILES

COOPER STATION, TEST 4



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## COOPER STATION, TEST 3

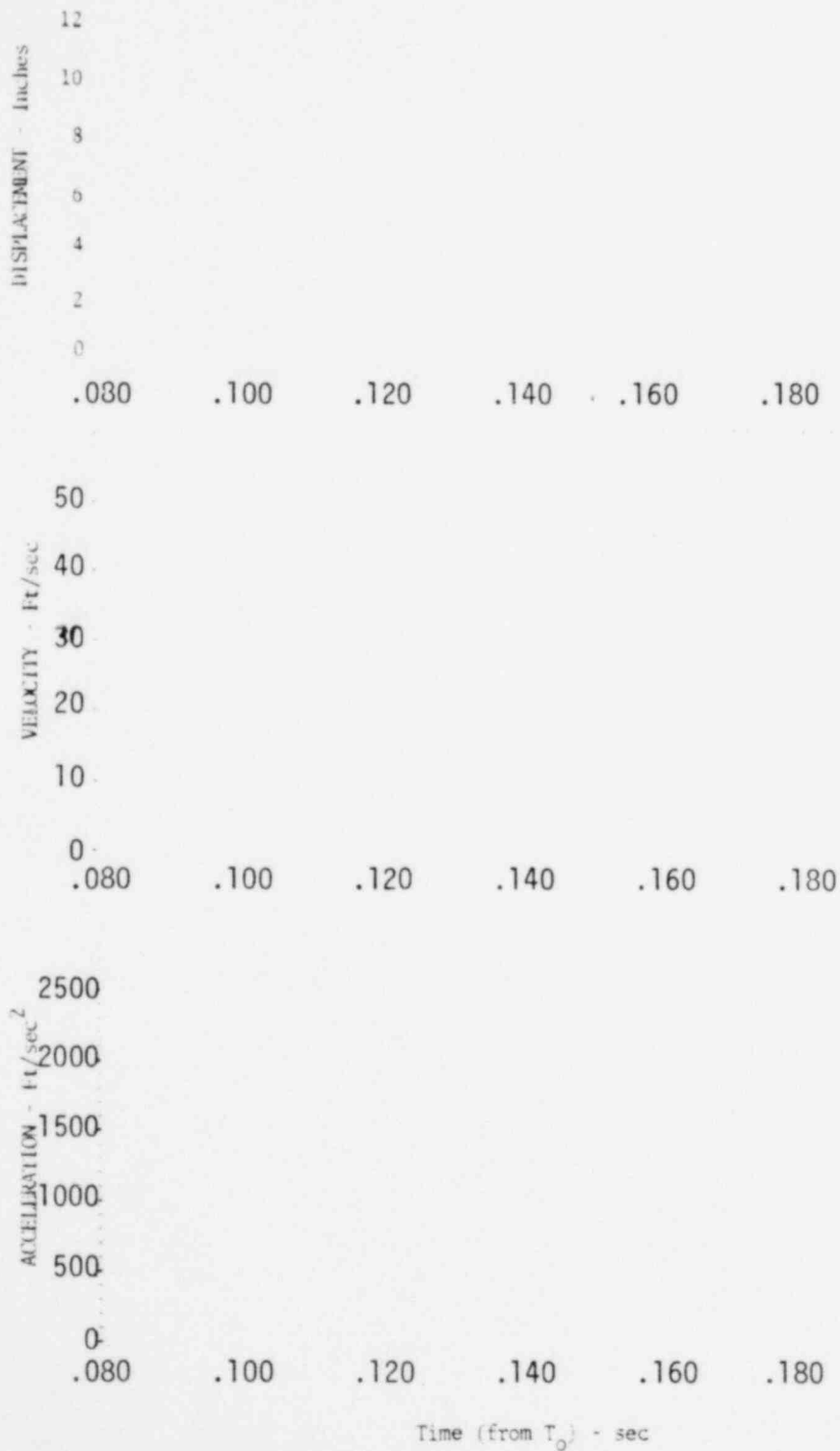


1349 153

FIGURE A-330

DOWNCOMER WATER SLUG EJECTION

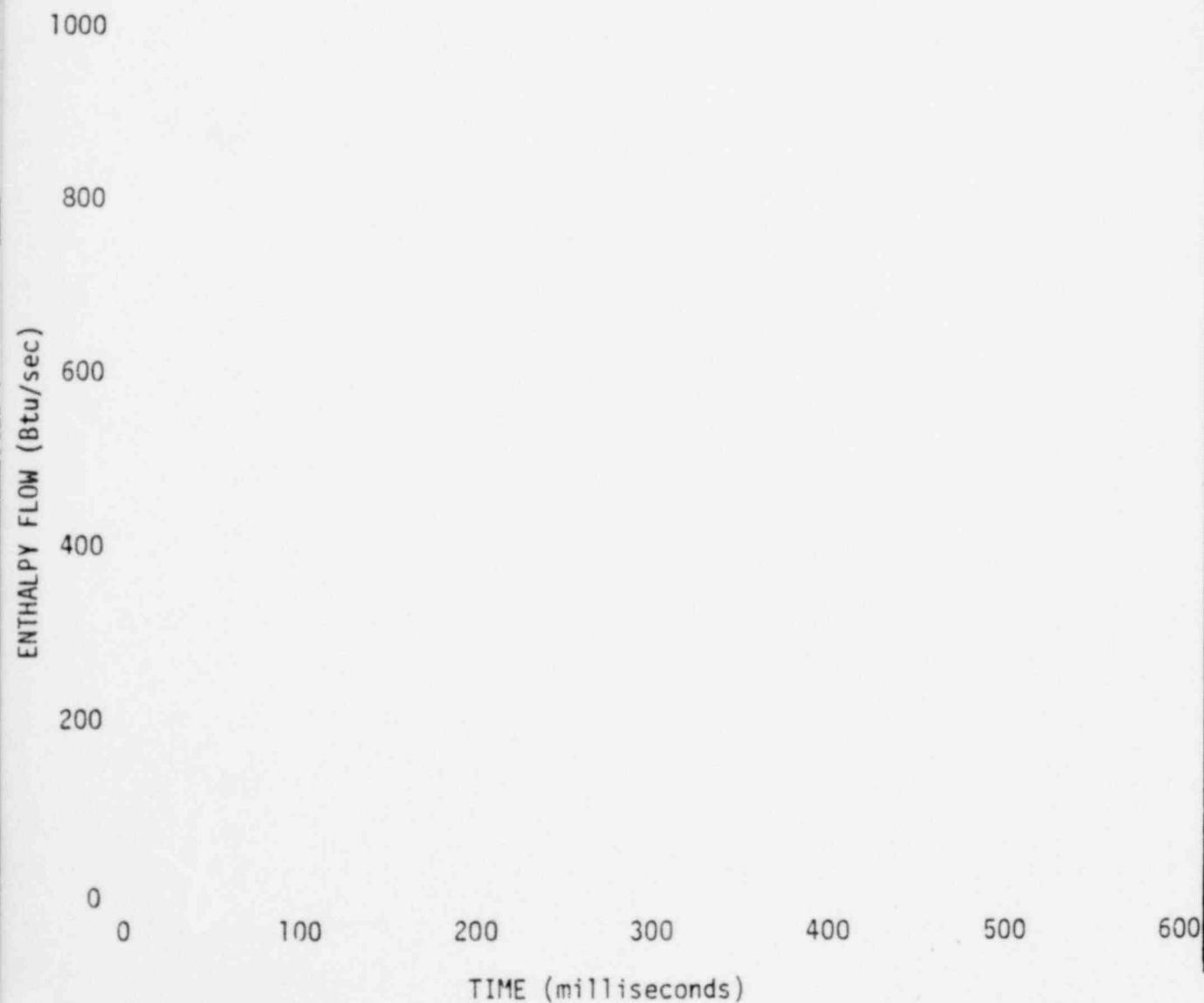
COOPER STATION, TEST 5



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FIGURE A-331

EFFECT OF DRYWELL/WETWELL  $\Delta P$  ON  
ENTHALPY FLOW INTO POOL  
Cooper Station Tests



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FIGURE A-332

EFFECT OF DRYWELL/WETWELL  $\Delta P$  ON

DOWNCOMER INTERNAL PRESSURE

Cooper Station Tests

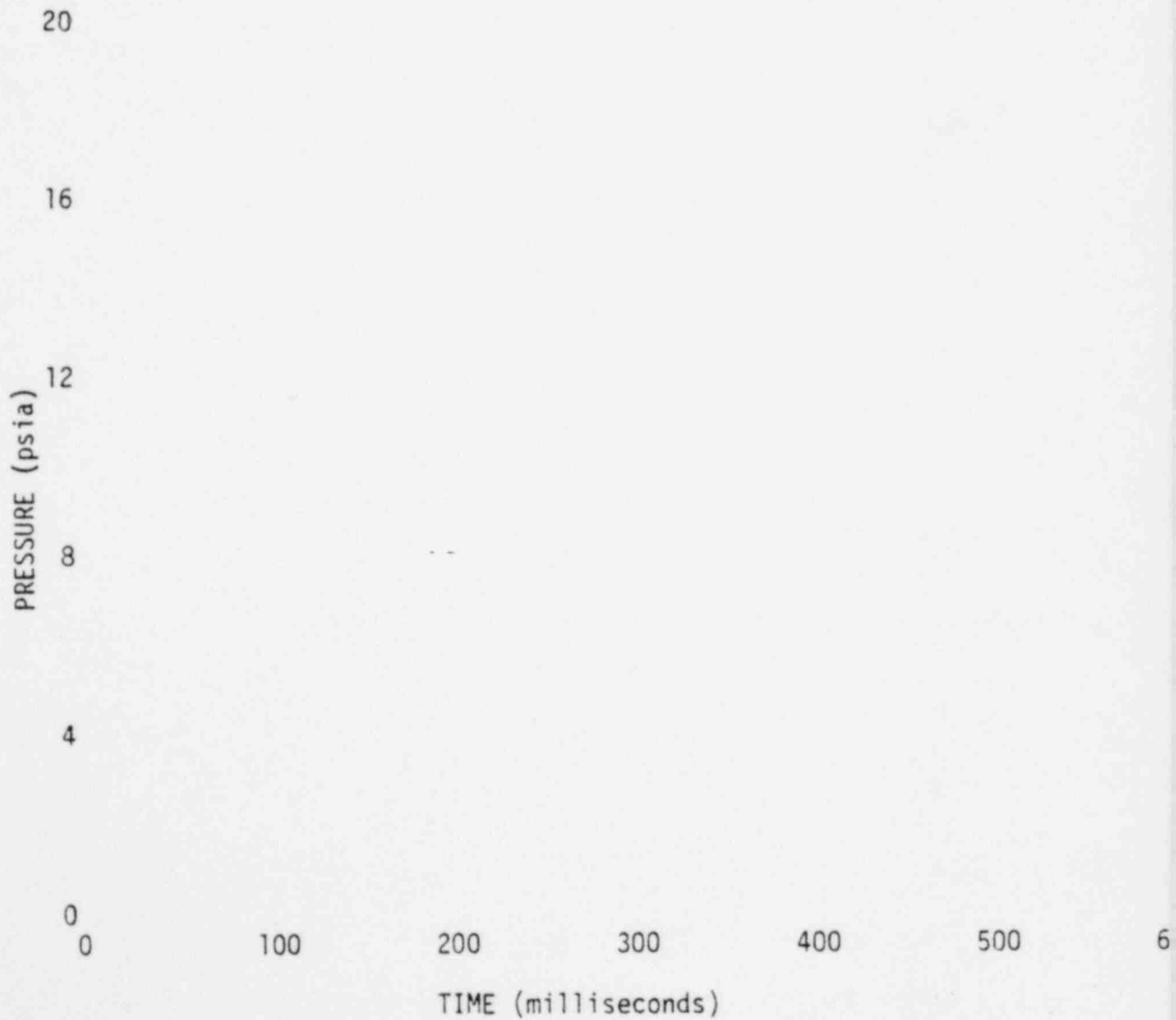
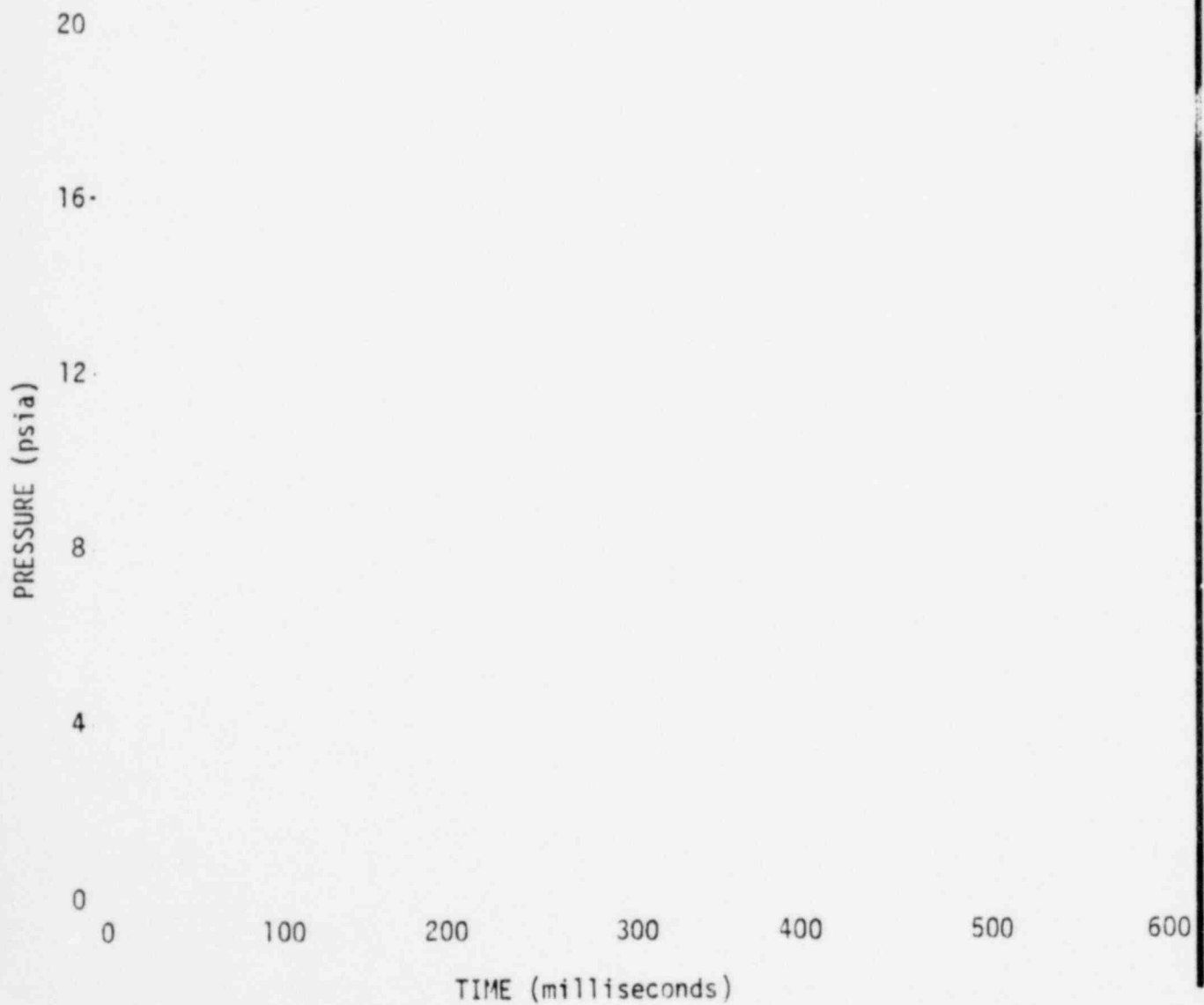


FIGURE A -333

EFFECT OF DRYWELL/WETWELL  $\Delta P$  ON POOL PRESSURE

AT 180 DEGREE AND FREESPACE PRESSURE

Cooper Station Tests



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TABLE A-15

## DATA FOR WETWELL VERTICAL LOADS

Task 5.5.3-2 Cooper Station Test.

\*Vent clearing time (from  $T_0$ ) determined from the movie films.\*\*Time difference from  $T_0$  to time of zero downforce.

\*(1) Start-of-test reference time

Parameter	Test No.	7.46" $\Delta P$ (No Deflector)				Mean	Std. Dev.	$\frac{Q}{A} \Delta P$ (5)
		(1)	(2)	(3)	(4)			
*(1)								
$T_0$	(sec)							
Vent Clearing Time*	(sec)							
<u>Peak Downforce</u>								
Pressure Integral:								
Force	(lb)							
Time (from $T_0$ )	(sec)							
Corrected Pressure Integral:								
Force	(lb)							
Time (from $T_0$ )	(sec)							
Corrected Load Cell:								
Force	(lb)							
Time (from $T_0$ )	(sec)							
<u>Downforce Valley</u>								
Pressure Integral:								
Force	(lb)							
Time (from $T_0$ )	(sec)							
Corrected Pressure Integral:								
Force	(lb)							
Time (from $T_0$ )	(sec)							
Corrected Load Cell:								
Force	(lb)							
Time (from $T_0$ )	(sec)							
<u>2nd Peak Downforce</u>								
Pressure Integral:								
Force	(lb)							
Time (from $T_0$ )	(sec)							
Corrected Pressure Integral:								
Force	(lb)							
Time (from $T_0$ )	(sec)							
Corrected Load Cell:								
Force	(lb)							
Time (from $T_0$ )	(sec)							
<u>[<math>\Delta t</math>] Downforce Time**</u>								
Pressure Integral	(sec)							
Corrected Pressure Integral	(sec)							
Corrected Load Cell	(sec)							
<u>Downforce Impulse</u>								
Pressure Integral:								
Impulse	(lb-sec)							

Table A-15

\*Time at force is zero (from  $T_0$ )DATA FOR WETWELL VERTICAL LOADS (continued)

Task 5.5.3-2 Cooper Station Tests

Parameter	Test No.	7.46" $\Delta P$ (No Deflector)				Mean	Std. Dev.	$0'' \Delta P$ (5)
		(1)	(2)	(3)	(4)			
<u>Peak Upforce</u>								
Pressure Integral:								
Force (lb)	(1b)							
Time (from $T_0$ ) (sec)	(sec)							
Corrected Pressure Integral:								
Force (lb)	(1b)							
Time (from $T_0$ ) (sec)	(sec)							
Corrected Load Cell:								
Force (lb)	(1b)							
Time (from $T_0$ ) (sec)	(sec)							
<u>Force Valley</u>								
Pressure Integral:								
Force (lb)	(1b)							
Time (from $T_0$ ) (sec)	(sec)							
Corrected Pressure Integral:								
Force (lb)	(1b)							
Time (from $T_0$ ) (sec)	(sec)							
Corrected Load Cell:								
Force (lb)	(1b)							
Time (from $T_0$ ) (sec)	(sec)							
<u>Peak Upforce</u>								
Pressure Integral:								
Force (lb)	(1b)							
Time (from $T_0$ ) (sec)	(sec)							
Corrected Pressure Integral:								
Force (lb)	(1b)							
Time (from $T_0$ ) (sec)	(sec)							
Corrected Load Cell:								
Force (lb)	(1b)							
Time (from $T_0$ ) (sec)	(sec)							
<u>to Force Time*</u>								
Pressure Integral (sec)	(sec)							
Corrected Pressure Integral (sec)	(sec)							
Corrected Load Cell (sec)	(sec)							

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TABLE A-16

DATA FOR VENT HEADER IMPACT LOADS

## Task 5.5.3-2 Cooper Station Tests

Parameter \ Test No.	7.46" $\Delta P$				Mean	Std. Dev.	0" $\Delta P$ ( 5 )
	( 1 )	( 2 )	( 3 )	( 4 )			
$T_0^+$ (sec)							
<u>Vent Header Impact</u>							
Pressure Integral:							
Maximum Force (lb)							
Impulse (lb-sec)							
Duration* (sec)							
Load Cell Corrected:††							
Maximum Force (lb)							
Impulse (lb-sec)							
Duration (sec)							
Pool Surface Velocity (ft/sec)							
Time (from $T_0$ )** (sec)							

\*Based on impact pressure measurements.

\*\*At start of the first impact pressure recorded.

†Start-of-test reference time.

††represents peak of very noisy data (acceleration corrected); mean value would be lower.

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## A.8 Dresden Tests

The plant input for Dresden and Quad Cities showed that with the same deflector geometry both plants had identical QSTF test parameters except that Dresden had a slightly higher (0.8%) drywell pressurization rate. Therefore the Dresden test data is applicable to Quad Cities.

### A.8.1 Typical Data

Time-history plots of the driving conditions and pool response are presented in this section for Dresden Tests 3 and 5. Test 3 was a load definition test which was conducted at a partial drywell/wetwell differential pressure of 7.15"  $\Delta P$  and with a 5.17 inch pipe deflector (20 inch full scale). Test 5 was conducted without an initial drywell/wetwell differential pressure (0"  $\Delta P$ ) and with the same 5.17 inch pipe deflector.

#### A.8.1.1 Driving Conditions

Driving conditions for Dresden Test 3 are presented in Figures A-334 through A-338. Similar plots for Dresden Test 5 are shown in Figures A-339 through A-343. Dresden's driving conditions had the same characteristics as the "typical" plant discussed in Section 3.0 of this report.

#### A.8.1.2 Pool Response

Downcomer internal pressure and wetwell pressures for Dresden Tests 3 and 5 are presented in Figures A-344 through A-345 and A-346 through A-347, respectively. These pressure plots have the same characteristics as the "typical" plant in Section 3.0.

Figure A-348 and A-349 present net torus force based on the torus pressure integral for Dresden Tests 3 and 5, respectively. Some downforce oscillations are present.

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The net torus force which was determined by applying the inertial correction from the torus accelerometer (Figures A-351 and A-353) to the torus load cell (Figures A-350 and A-352) is compared with the torus force obtained from the torus pressure integral in Figures A-354 and A-355. Residual oscillations are present in the corrected load cell. Figures A-356 and A-357 present the net torus force based on the torus pressure integral corrected for inertia. Smoothed downforce is also shown in these figures, using the filtering technique described in Appendix I. Refer to Appendix H for detailed comparison of filtered and unfiltered downforce transients.

The "average" pool pressures for Dresden Tests 3 and 5 are shown in Figures A-358 and A-360. Figures A-359 and A-361 are the same as Figures A-356 and A-357 with force replaced by average pressure (force/torus projected area).

The vent header impact pressures for Dresden Test 3 are presented in Figures A-362 through A-365. Vent header pressures for Dresden Test 5 are presented in Figures A-366 through A-369. These figures indicate that the deflector was effective in reducing the peak local vent header impact pressure.

Figure A-370 presents a comparison of the vent header impact force derived from the pressure integral with that derived from the corrected load cell. Vent header vertical accelerations from Tests 3 and 5 are shown in Figures A-371 and A-372, respectively.

#### A.8.2 Pool Dynamics

The pool contours at various times of pool swell are shown in Figures A-373 through A-376 for Dresden Tests 1, 2, 3, and 5.

The pool surface displacement curves for Tests 1, 2, and 3 are shown on Figure A-377. The pool surface velocities for Tests 1, 2,

and 3 are shown on Figure A-378. The pool surface displacement graph and pool surface velocity profiles for Test 5 are shown in Figures A-379 and A-380, respectively.

The pool surface displacements and velocity profile viewed from the side window during Test 4 are shown in Figure A-381. The downcomer water slug displacement, velocity, and acceleration versus time for Tests 3 and 5 are presented in Figures A-382 and A-383.

#### A.8.3 Data Summaries

Table A-17 presents the Dresden test data for wetwell vertical forces.

Table A-18 presents the Dresden test data for vent header impact forces.

#### A.8.4 Discussion and Analysis

Figure A-384 presents the effect of drywell/wetwell  $\Delta P$  on enthalpy flow into the bubbles. Effect of drywell/wetwell  $\Delta P$  on downcomer internal pressure is shown in Figure A-385. Figure A-386 presents the effect of drywell/wetwell  $\Delta P$  on pool and freespace pressures. The data for Dresden parallels that for the "typical" plant in Section 3.0.

The Dresden load definition tests were conducted at 7.15"  $H_2O$   $\Delta P$  and with a pipe deflector installed below the vent header. A  $\Delta P$  sensitivity test at 0"  $H_2O$   $\Delta P$  was also conducted. Some downforce oscillations were evident. The upforce also showed some oscillation. The pipe deflector (20 inch full-scale) effectively reduced vent header impact force.

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FIGURE A-334

DRYWELL ORIFICE UPSTREAM PRESSURE

Task 5.5.3-2 Dresden Test 3

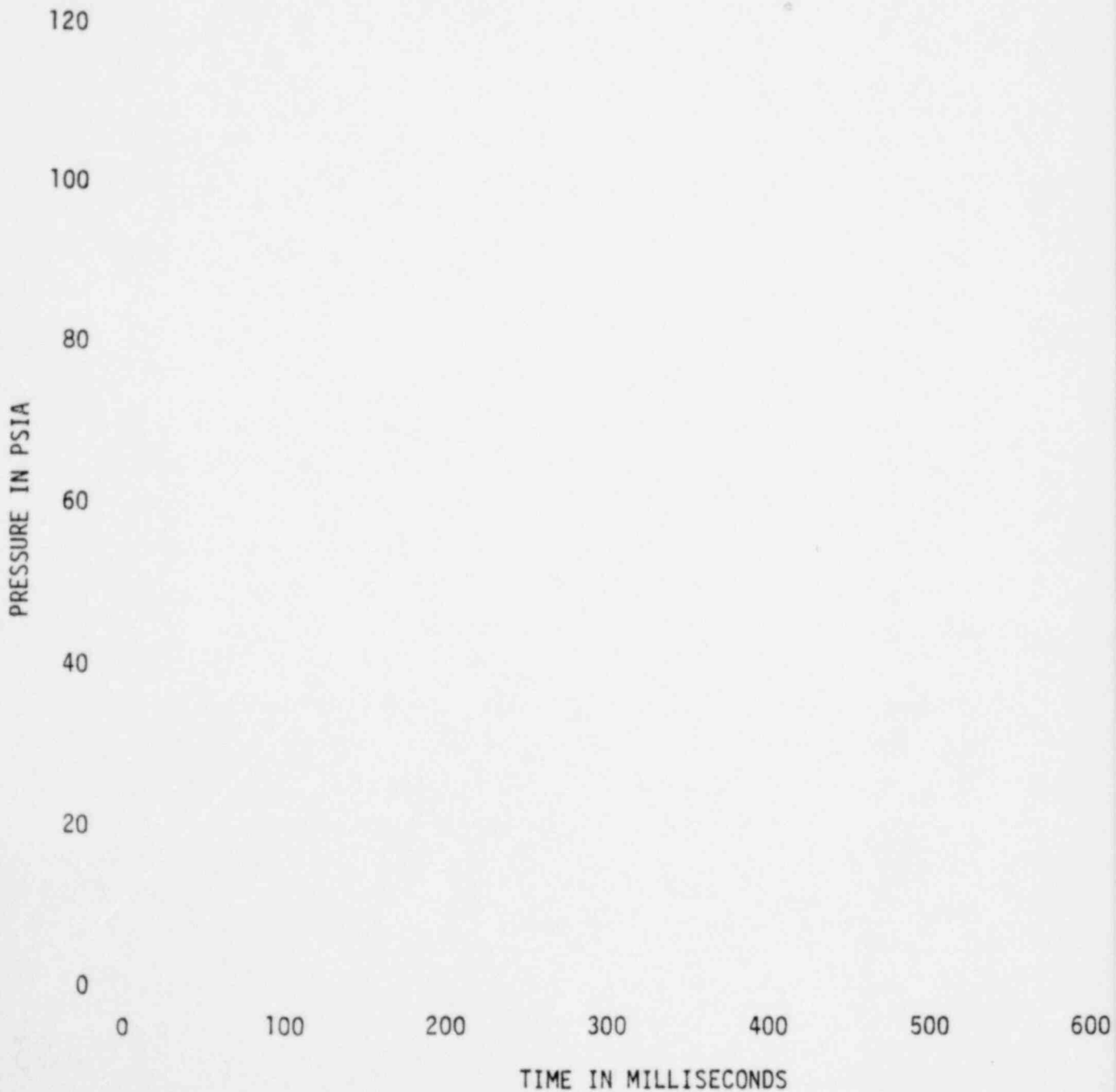


FIGURE A-335

DRYWELL PRESSURE

Task 5.5.3-2 Dresden Test 3

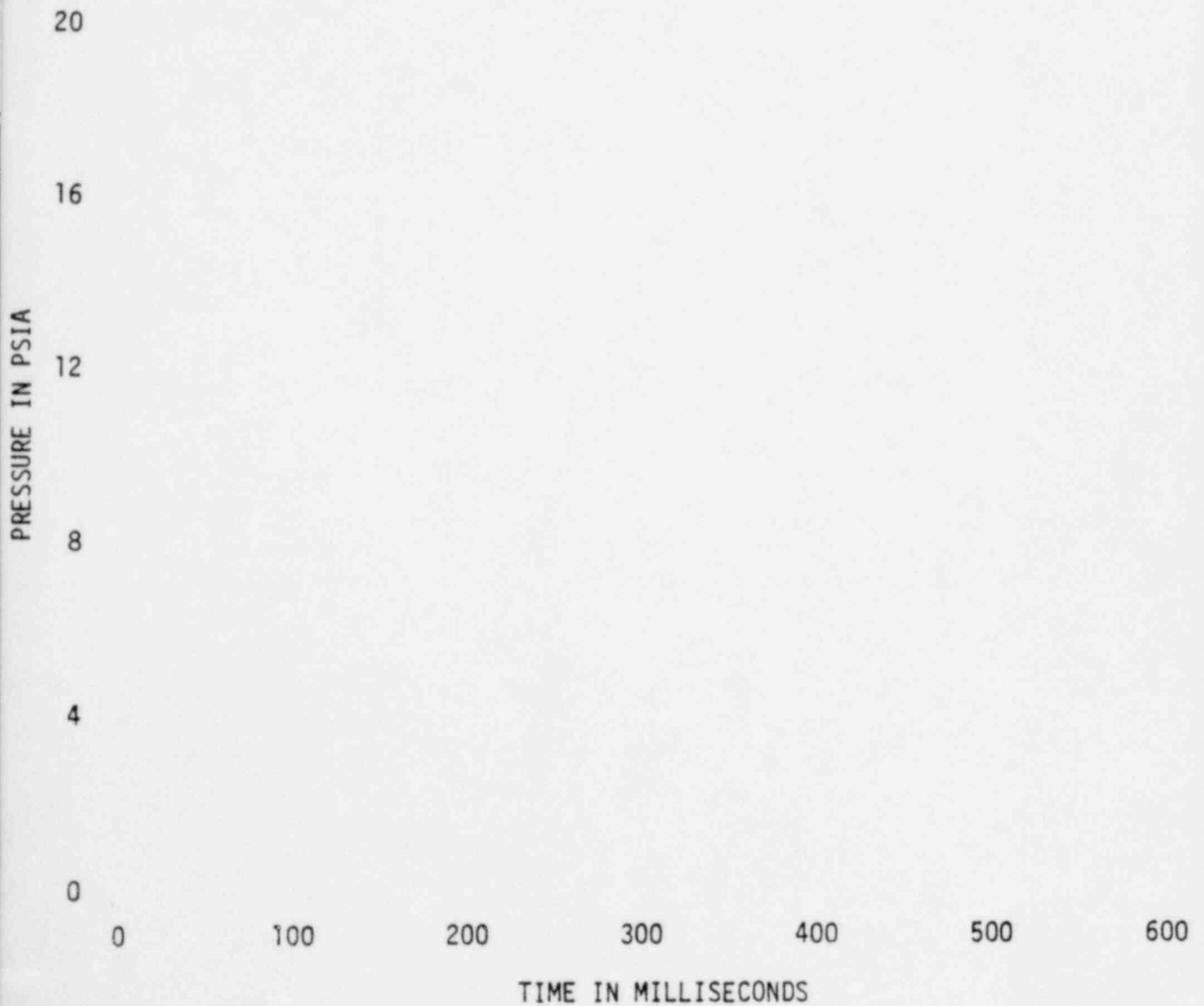


FIGURE A-336

DOWNCOMER ORIFICE DIFFERENTIAL PRESSURE

Task 5.5.3-2 Dresden Test 3

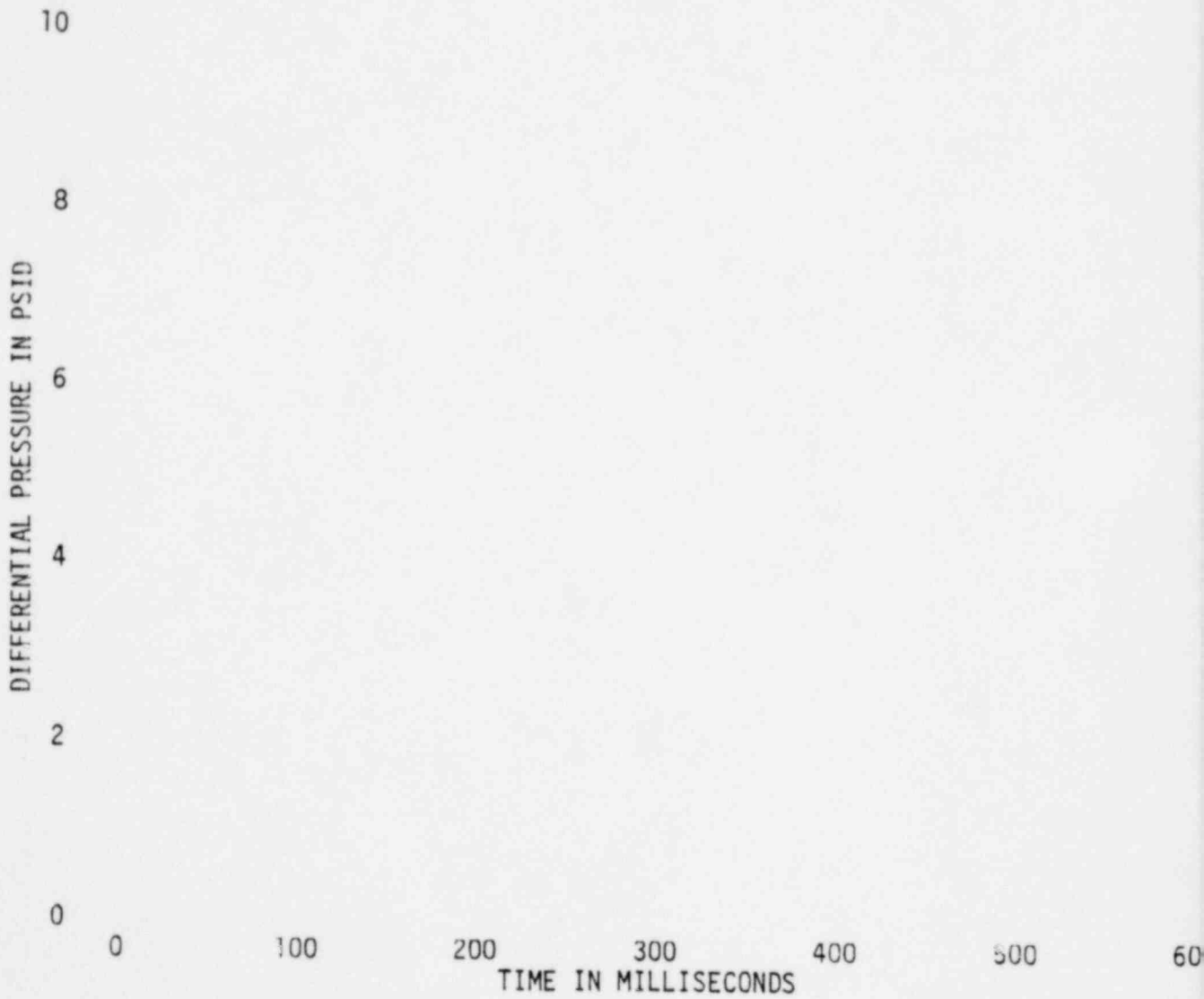
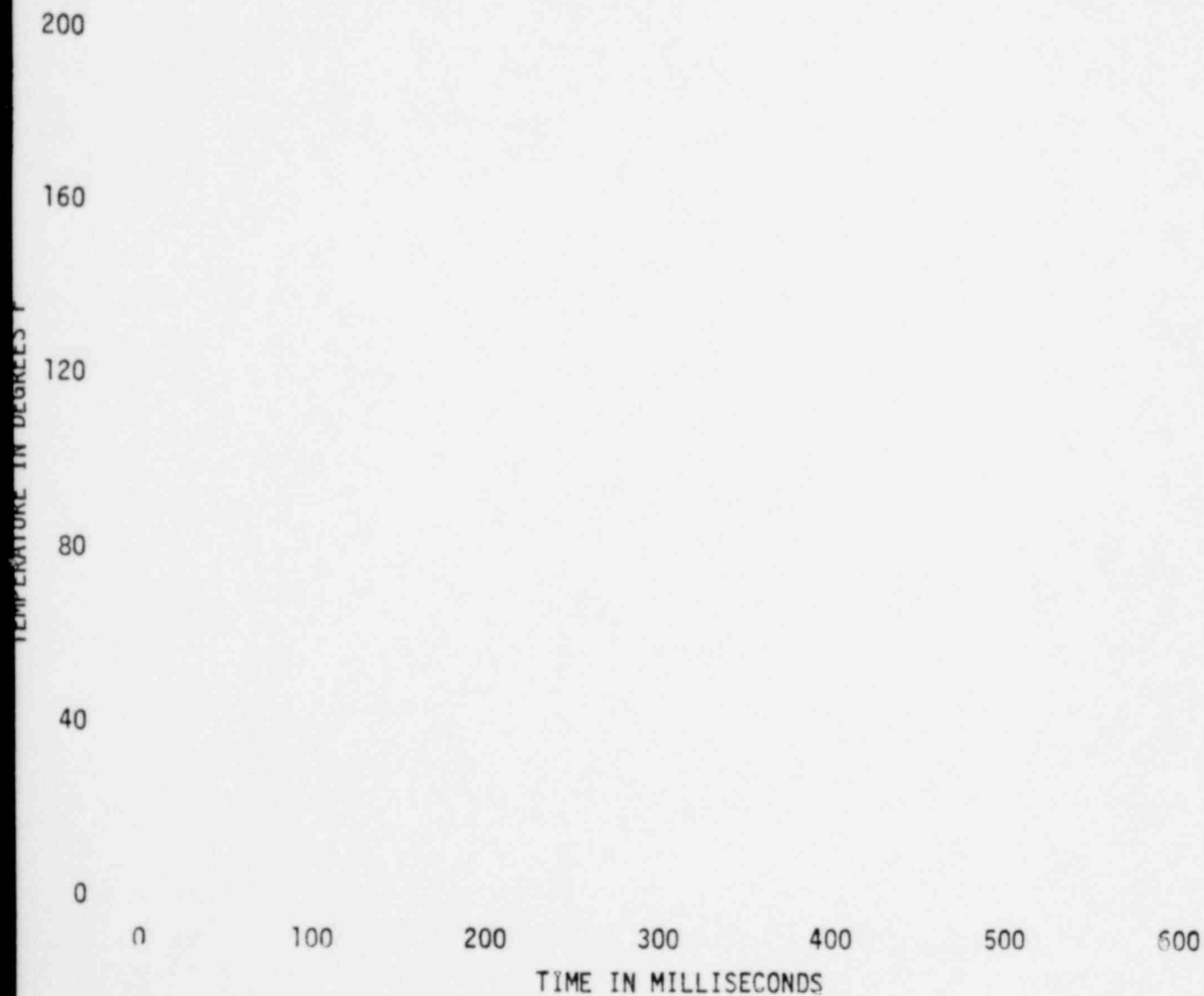


FIGURE A-337

DOWNCOMER ORIFICE UPSTREAM TEMPERATURE

Task 5.5.3-2 Dresden Test 3

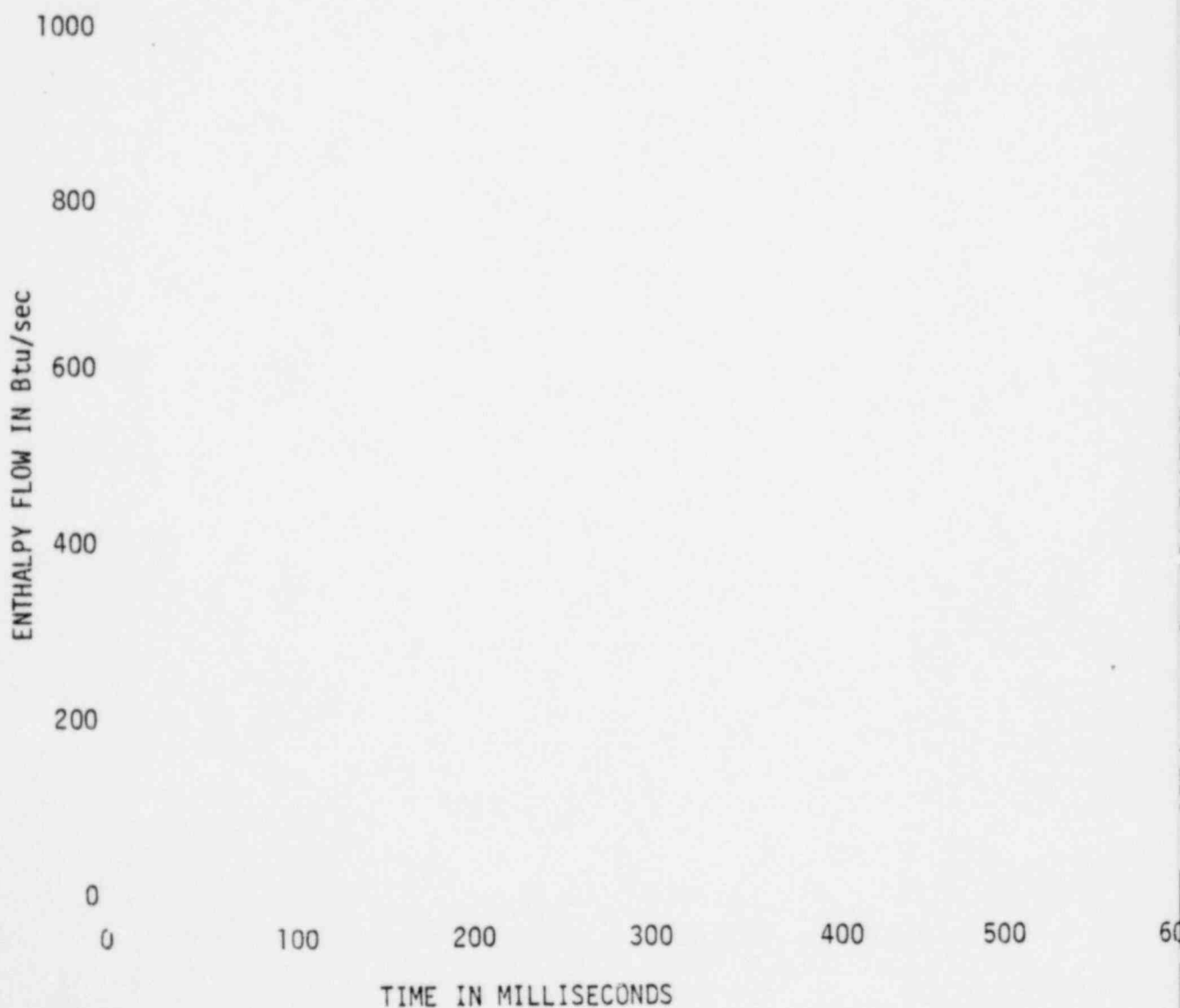


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FIGURE A-338

ENTHALPY FLOW INTO POOL

Task 5.5.3-2 Dresden Test 3



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FIGURE A-339

DRYWELL ORIFICE UPSTREAM PRESSURE

Task 5.5.3-2 Dresden Test 5

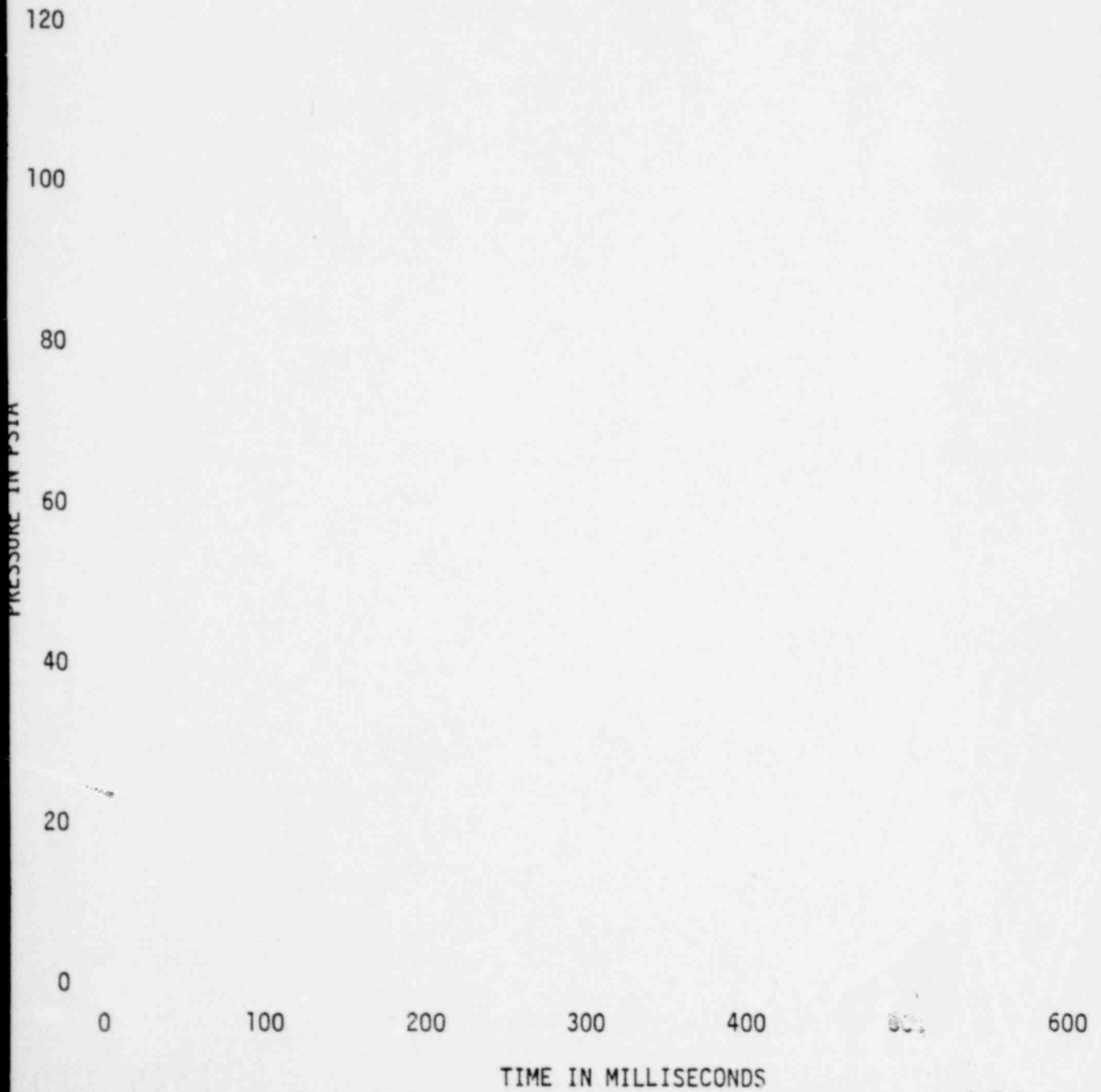


FIGURE A-340

DRYWELL PRESSURE

Task 5.5.3-2 Dresden Test 5

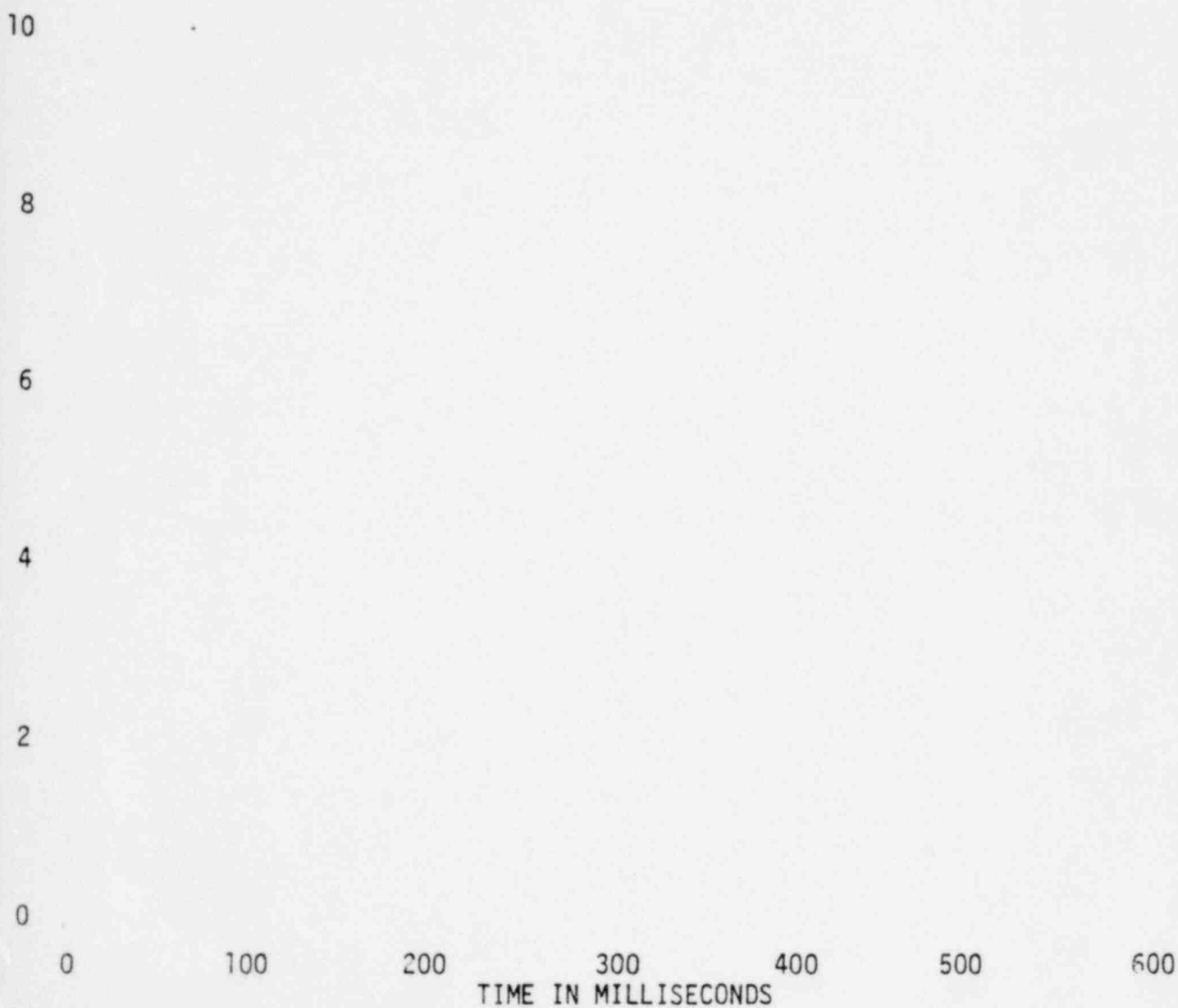


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FIGURE A-341

DOWNCOMER ORIFICE DIFFERENTIAL PRESSURE

Task 5.5.3-2 Dresden Test 5



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FIGURE A-342  
DOWNCOMER ORIFICE UPSTREAM TEMPERATURE  
Task 5.5.3-2 Dresden Test 5



FIGURE A-343

ENTHALPY FLOW INTO POOL

Task 5.5.3-2 Dresden Test 5

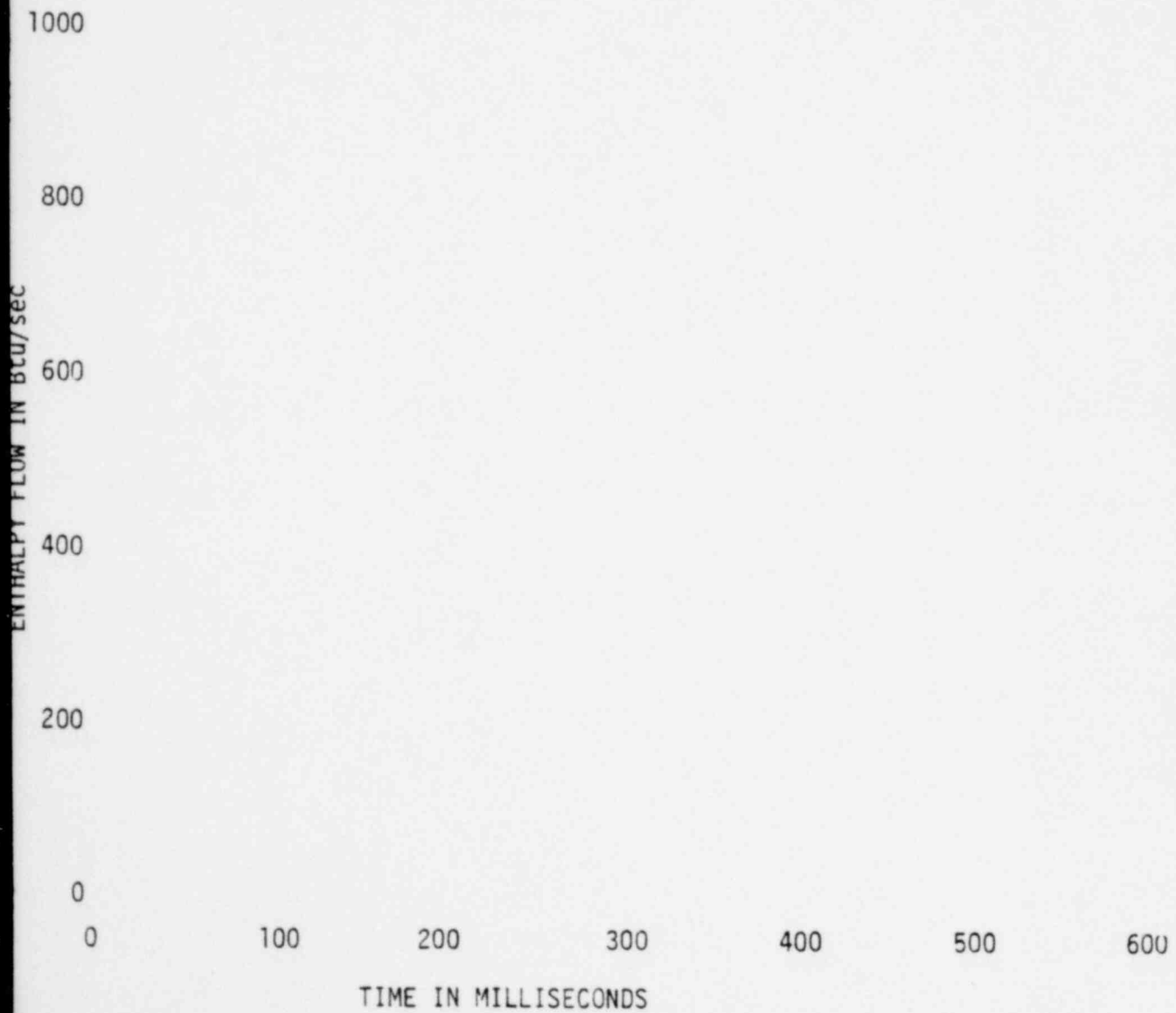


FIGURE A-344

DOWNCOMER INTERNAL PRESSURE  
Task 5.5.3-2 Dresden Test 3

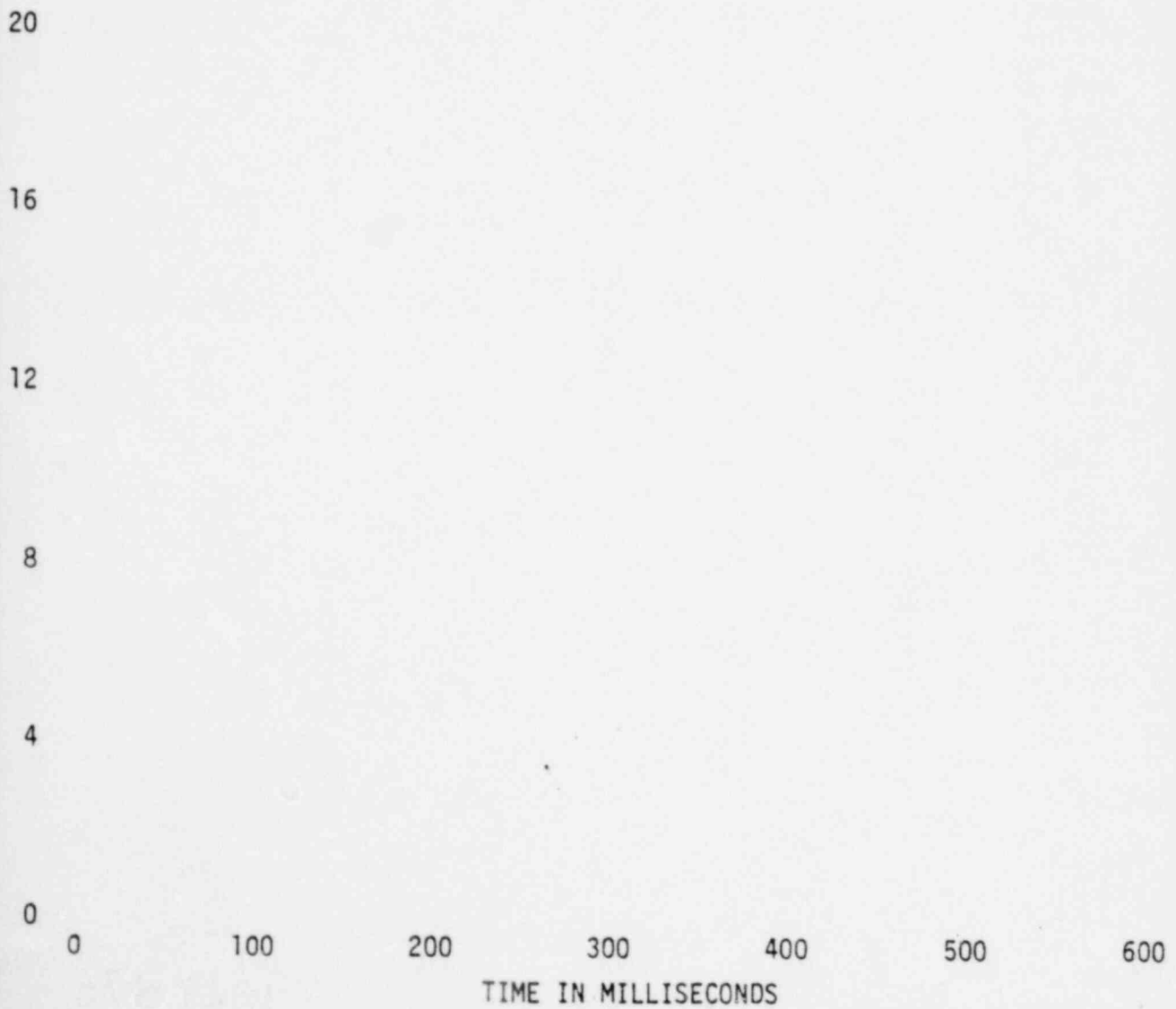


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FIGURE A-345

WETWELL PRESSURES

Task 5.5.3-2 Dresden Test 3



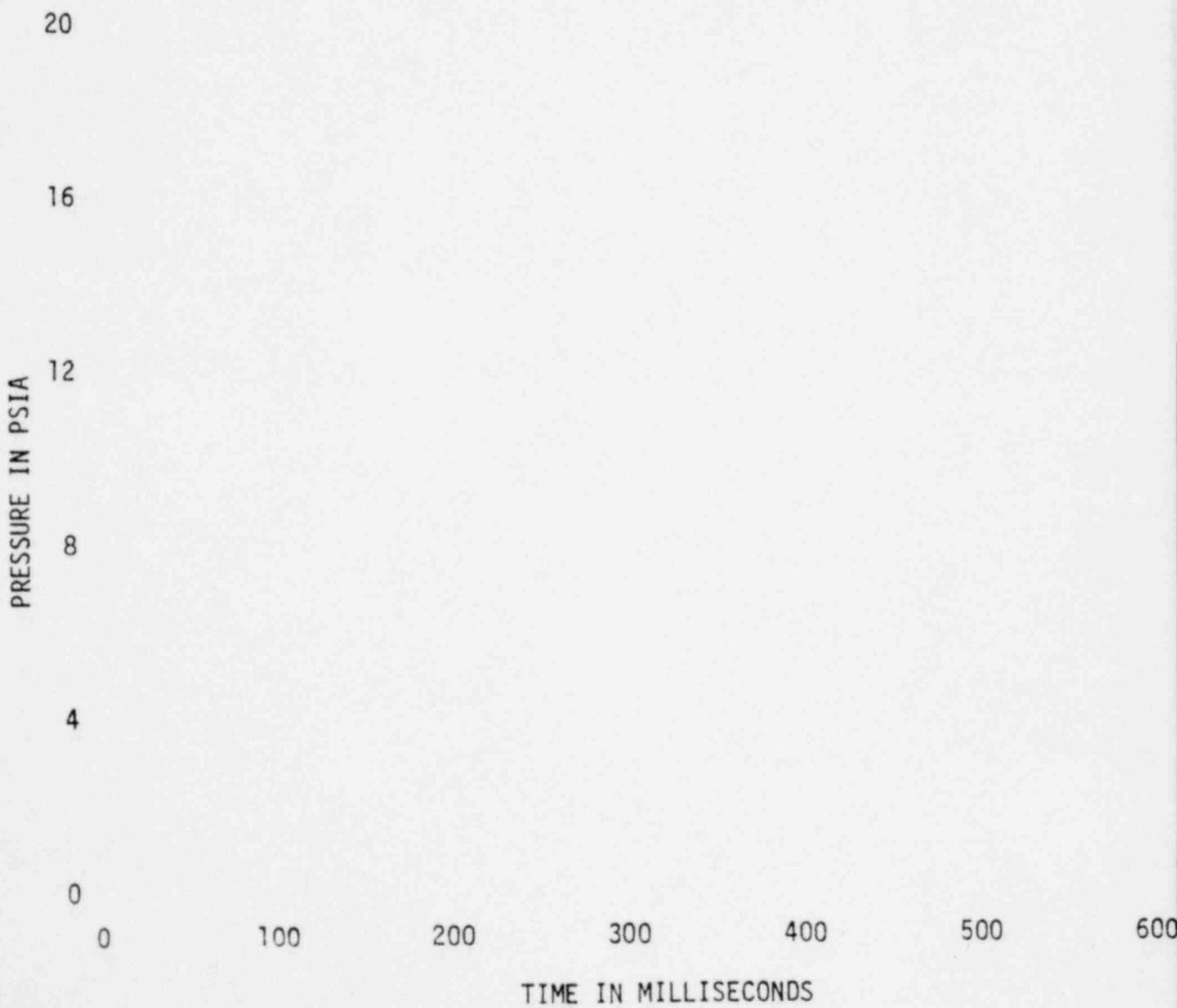
1349 175

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FIGURE A-346

DOWNCOMER INTERNAL PRESSURE

Task 5.5.3-2 Dresden Test 5



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FIGURE A-347

WETWELL PRESSURES

Task 5.5.3-2 Dresden Test 5



TIME IN MILLISECONDS

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FIGURE A-348

NET TORUS FORCE FROM PRESSURE INTEGRAL

Task 5.5.3-2 Dresden Test 3

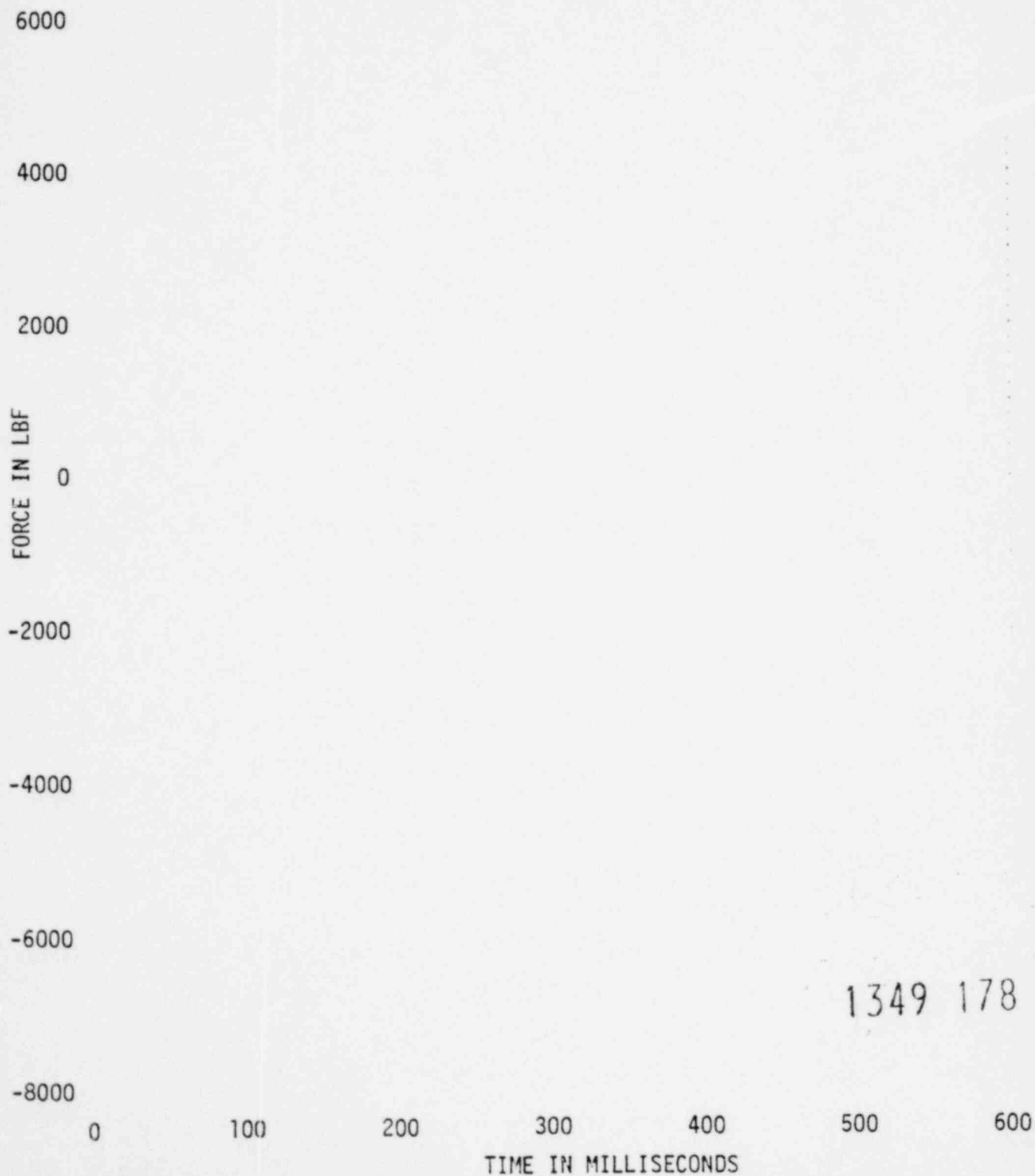


FIGURE A-349

NET TORUS FORCE FROM PRESSURE INTEGRAL

Task 5.5.3-2 Dresden Test 5



FIGURE A-350

TORUS LOAD CELL

Task 5.5.3-2 Dresden Test 3

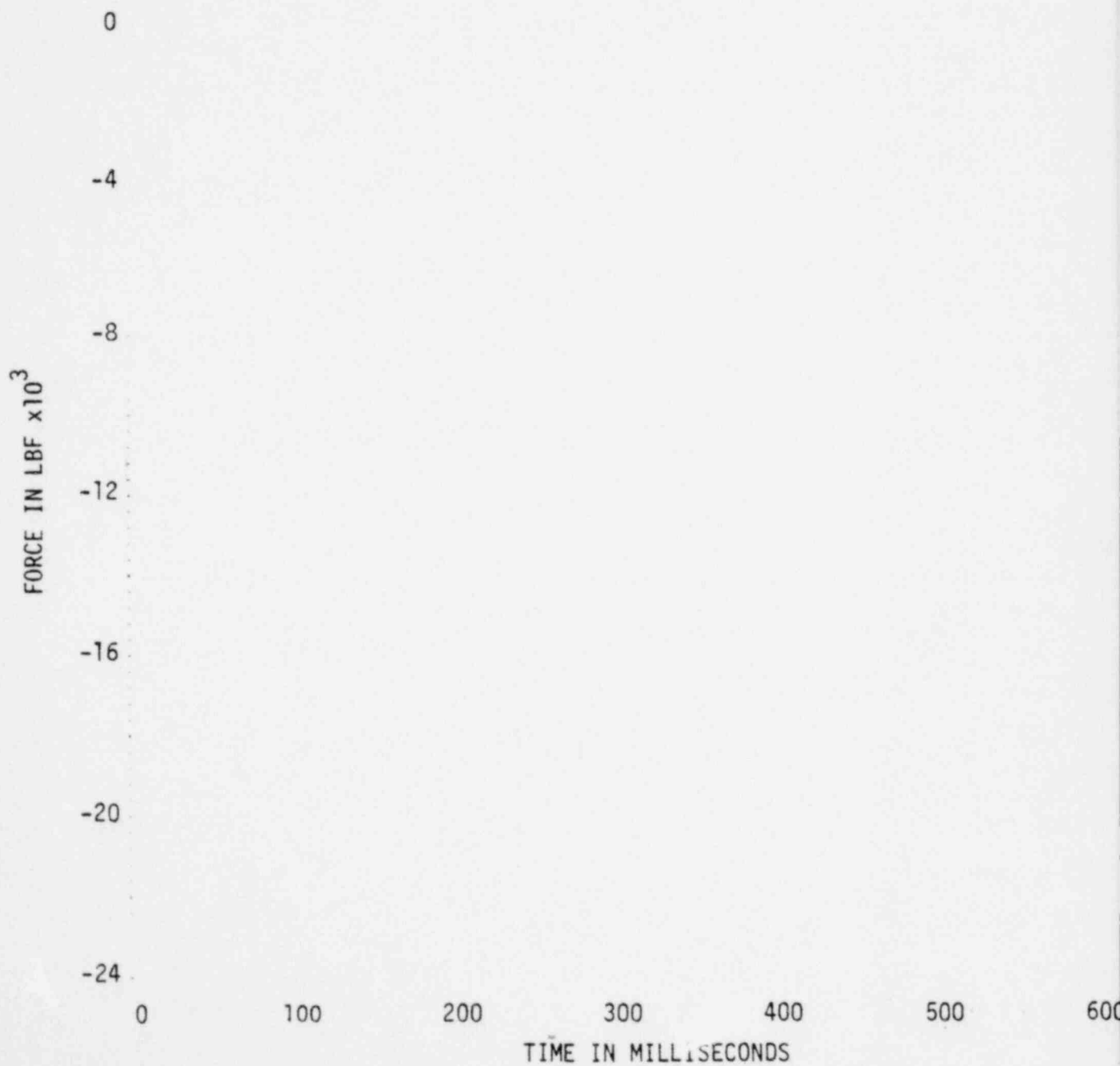
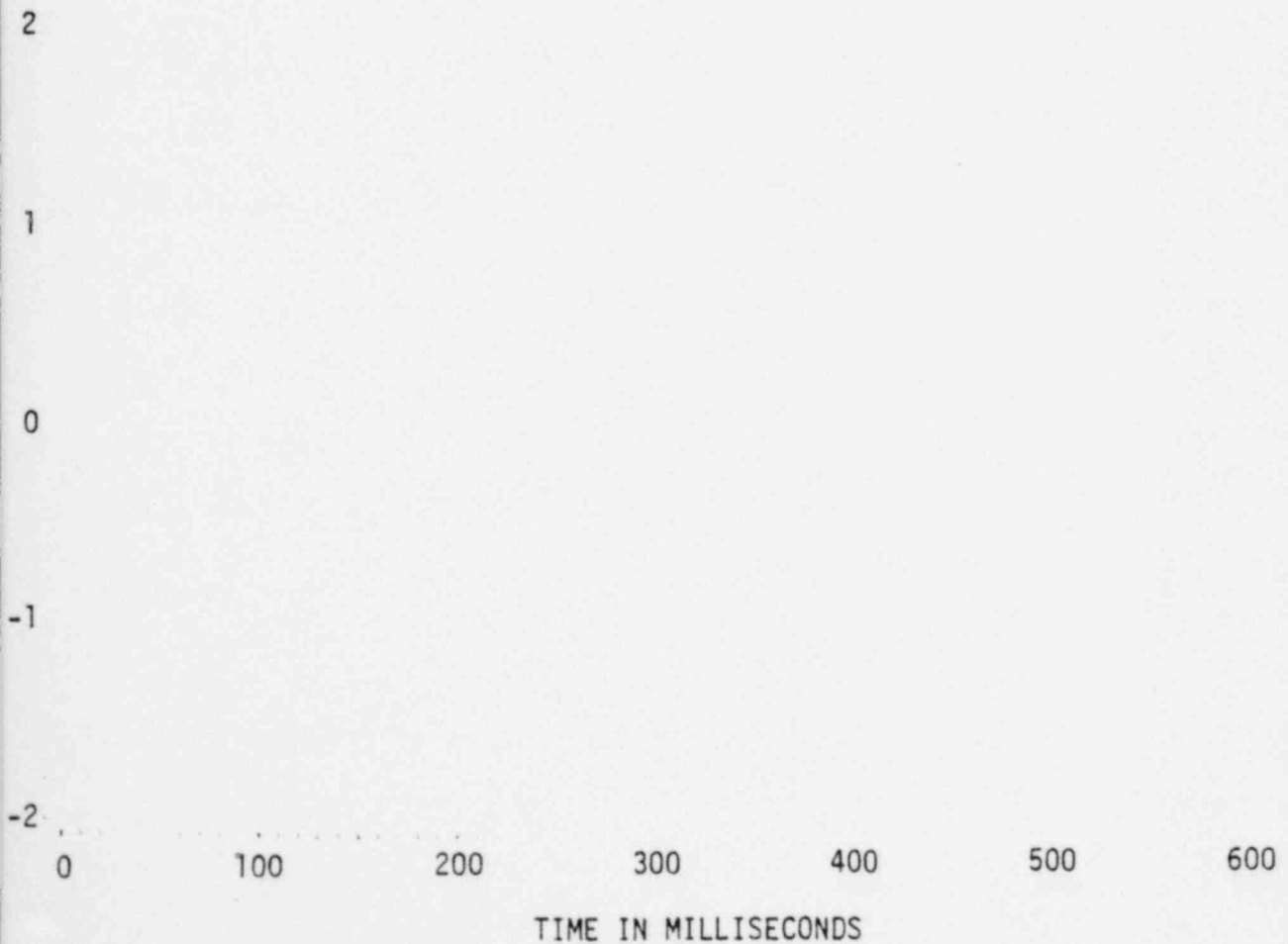


FIGURE A-351

TORUS VERTICAL ACCELERATION

Task 5.5.3-2 Dresden Test 3



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FIGURE A-352

TORUS LOAD CELL

Task 5.5.3-2 Dresden Test 5

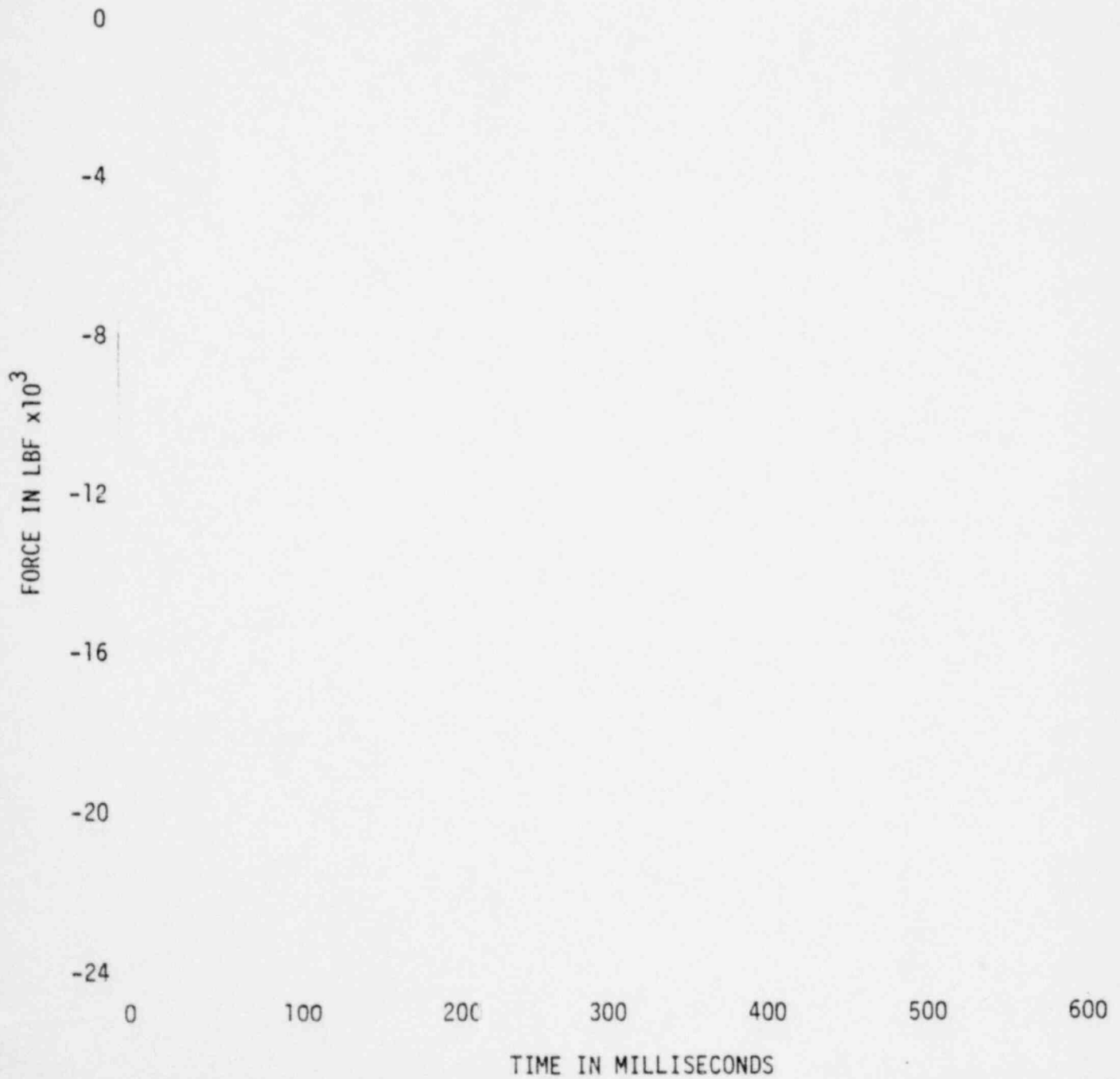
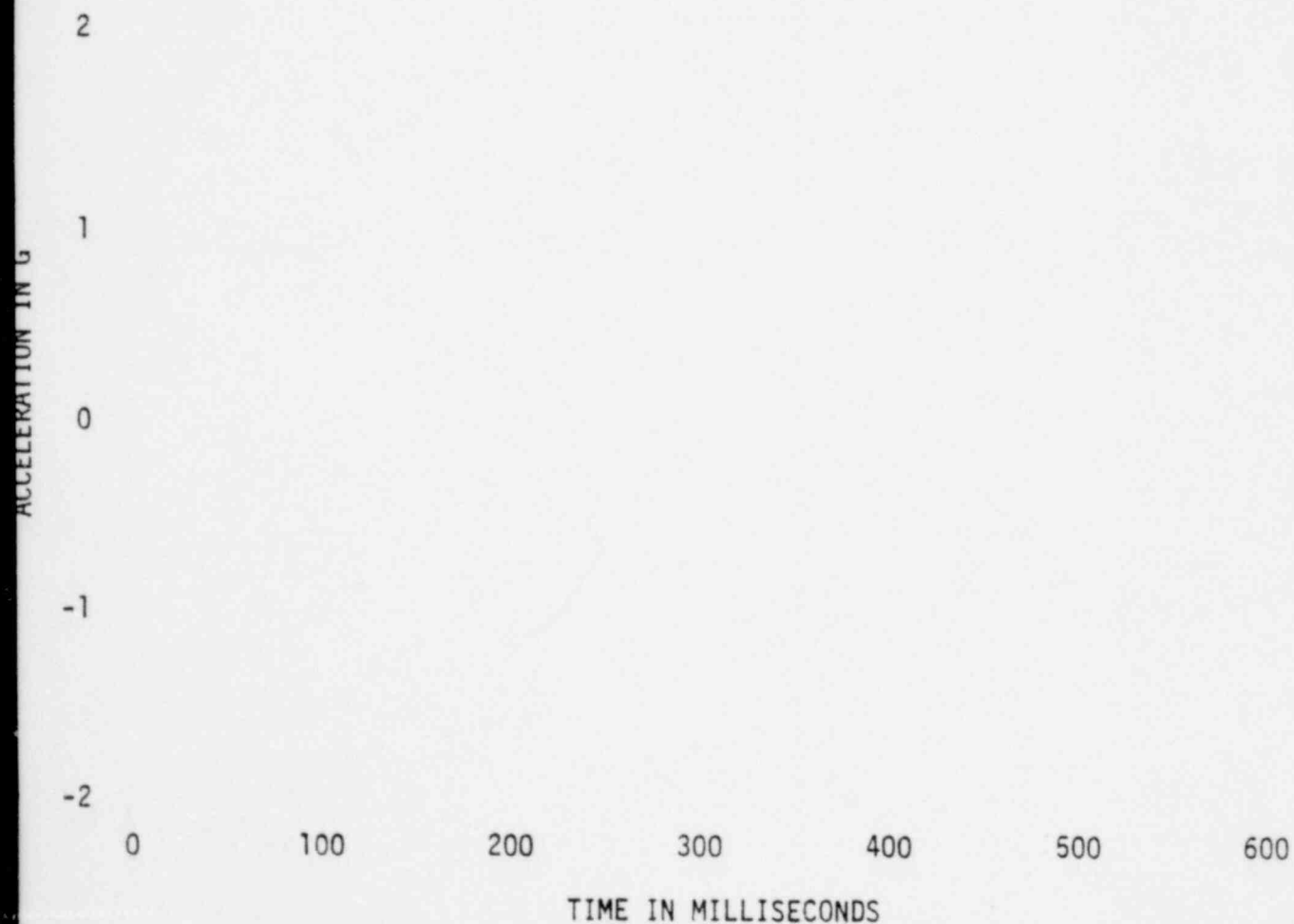


FIGURE A-353

TORUS VERTICAL ACCELERATION  
Task 5.5.3-2 Dresden Test 5



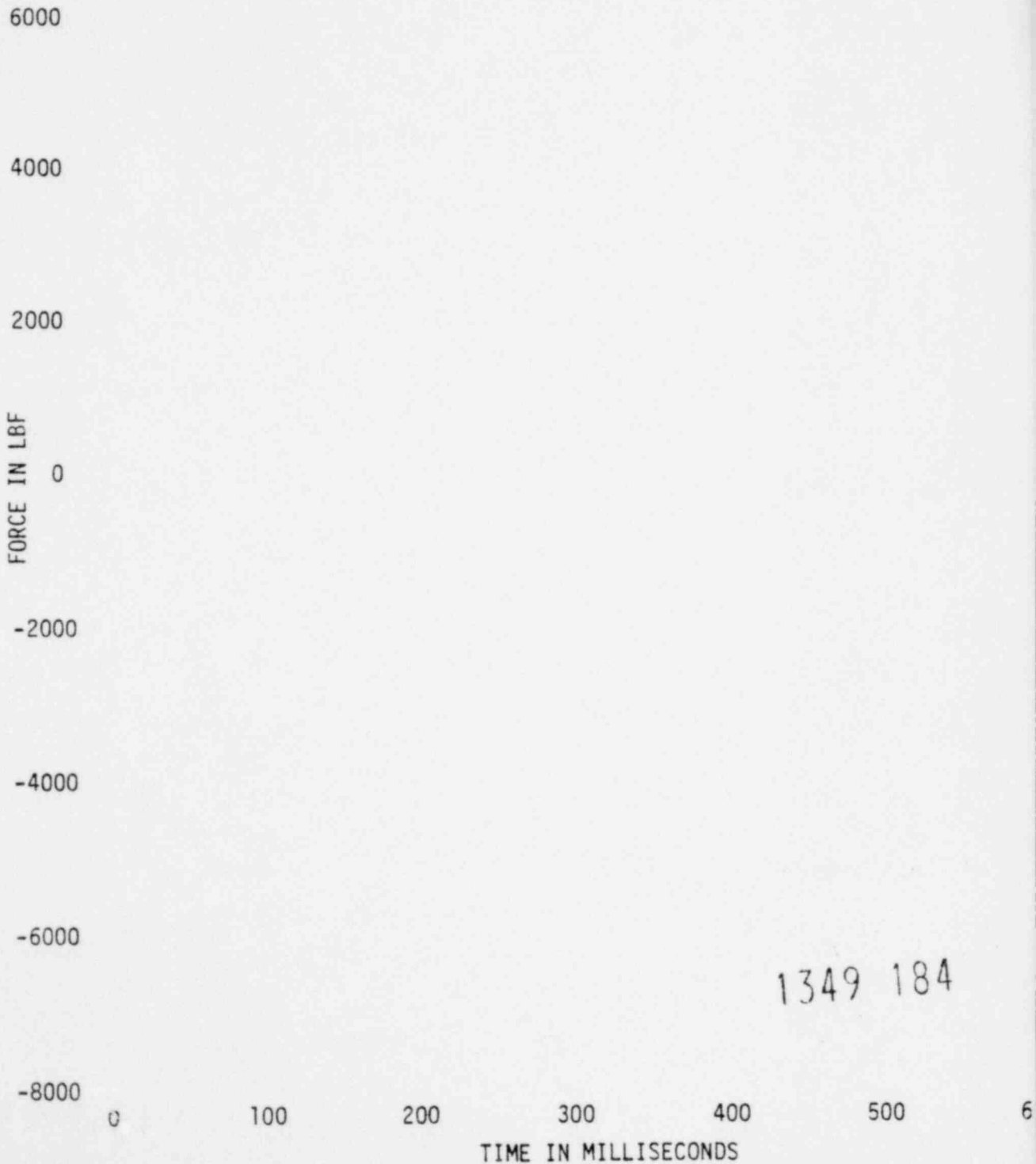
1349 183

NEDO-21944

FIGURE A-354

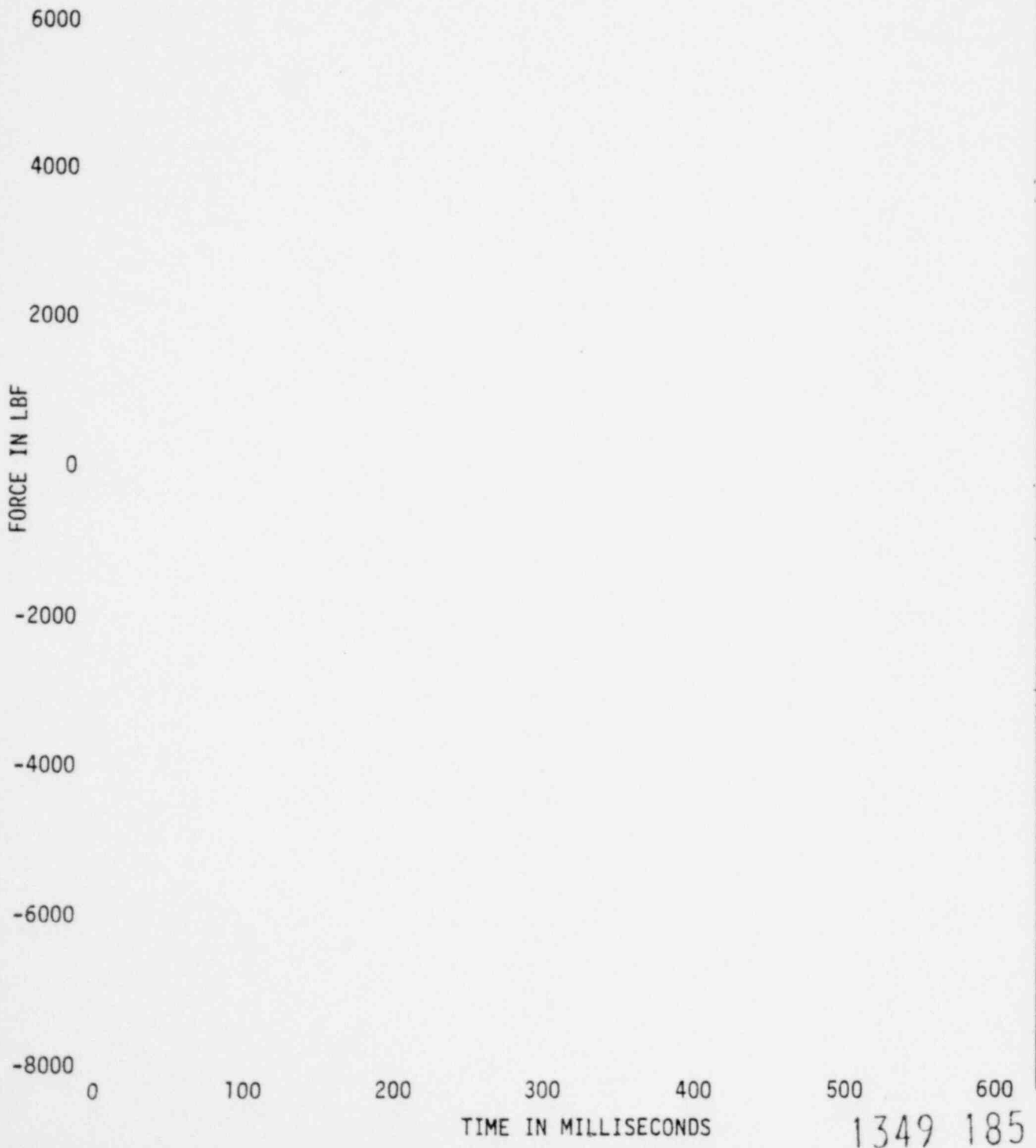
COMPARISON OF NET TORUS FORCE FROM PRESSURE INTEGRAL  
WITH NET TORUS FORCE FROM LOAD CELL CORRECTED FOR TORUS INERTIA

Task 5.5.3-2 Dresden Test 3



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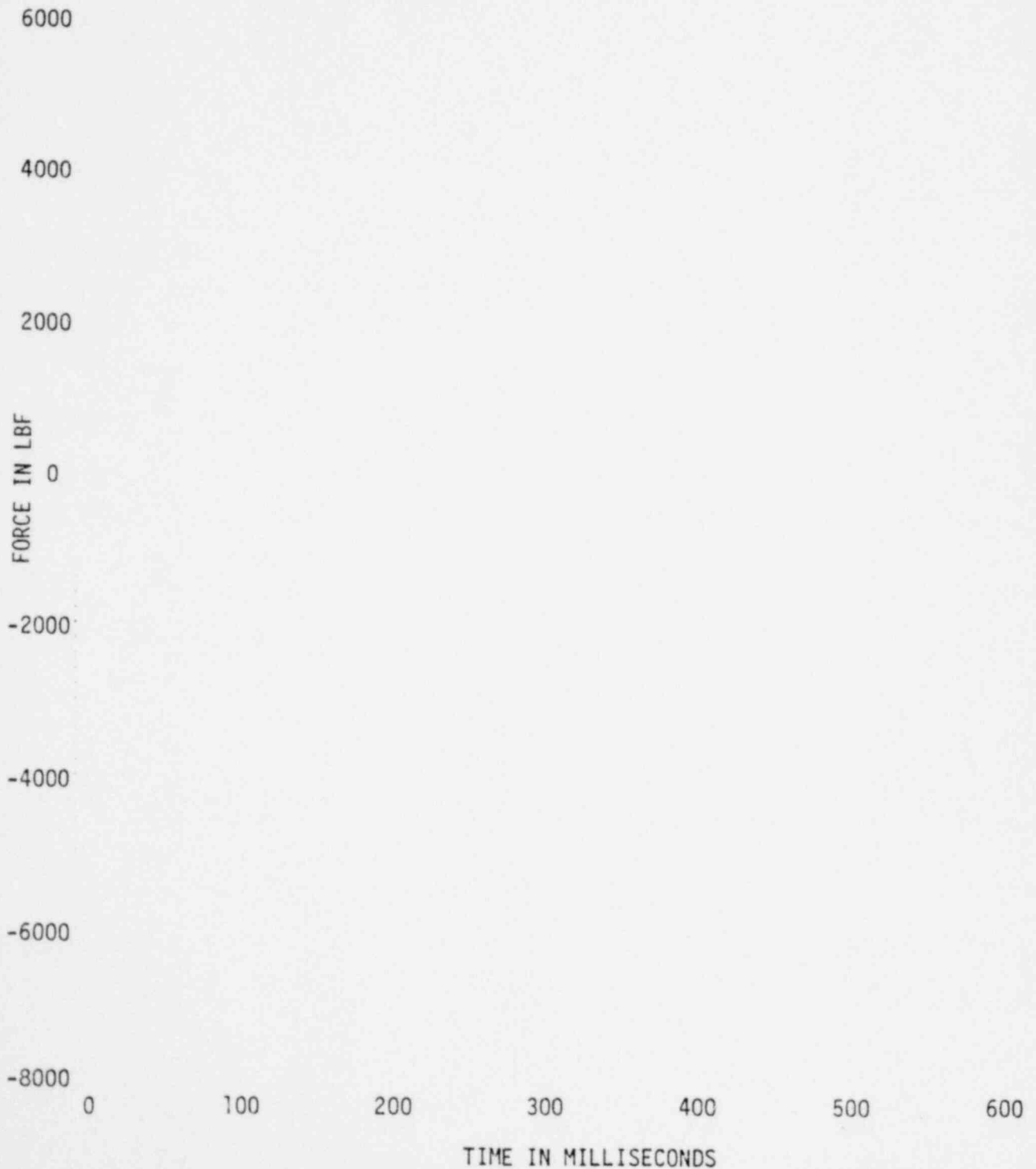
COMPARISON OF NET TORUS FORCE FROM PRESSURE INTEGRAL  
WITH NET TORUS FORCE FROM LOAD CELL CORRECTED FOR TORUS INERTIA  
Task 5.5.3-2 Dresden Test 5



NEDO-21944  
FIGURE A-356

NET TORUS FORCE FROM PRESSURE INTEGRAL, CORRECTED FOR WATER INERTIA

Task 5.5.3-2 Dresden Test 3



NEDO-21944

FIGURE A-357

NET TORUS FORCE FROM PRESSURE INTEGRAL, CORRECTED FOR WATER INERTIA

Task 5.5.3-2 Dresden Test 5



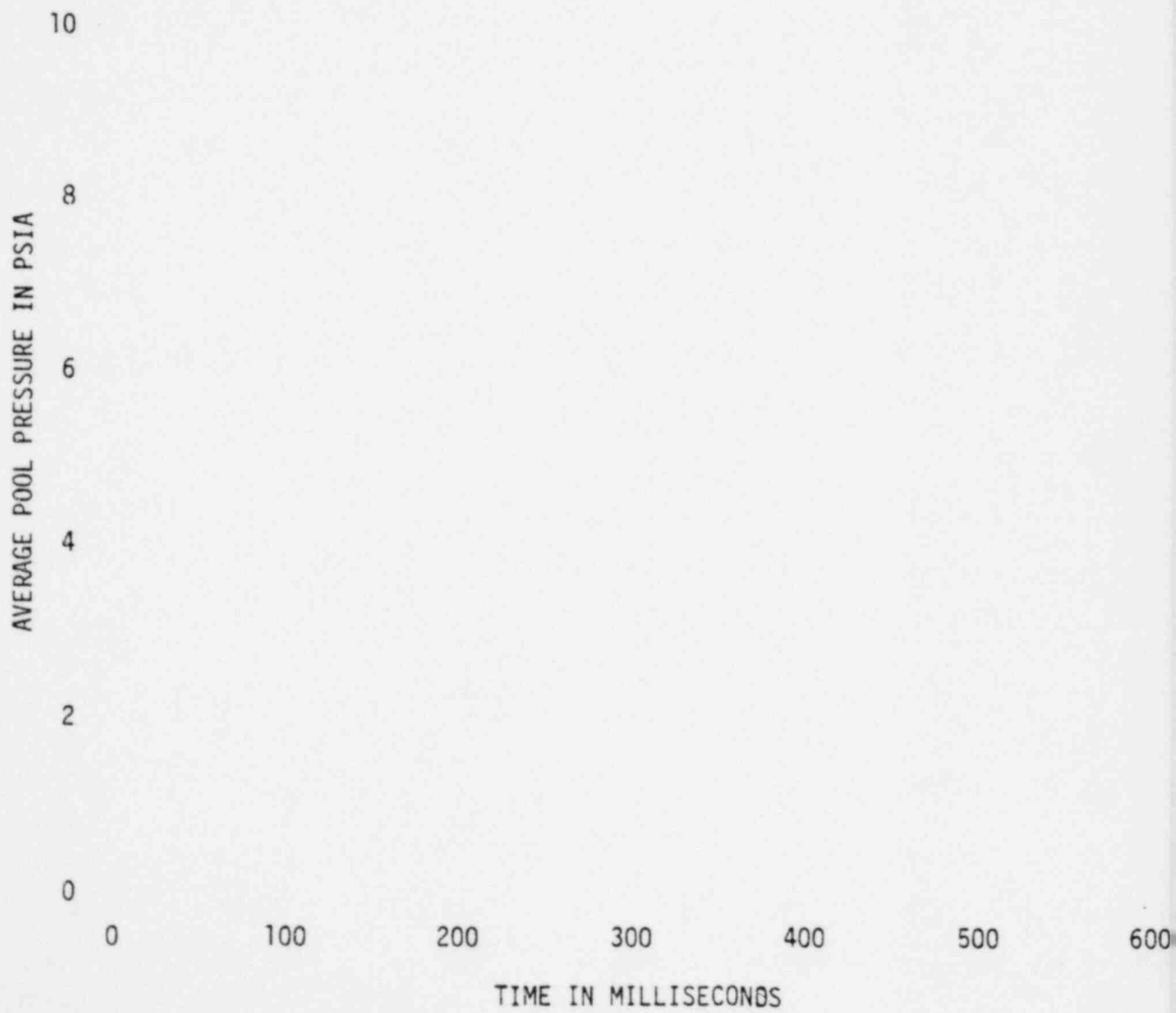
A-403

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FIGURE A-358

AVERAGE POOL PRESSURE, CORRECTED FOR WATER INERTIA

Task 5.5.3-2 Dresden Test 3

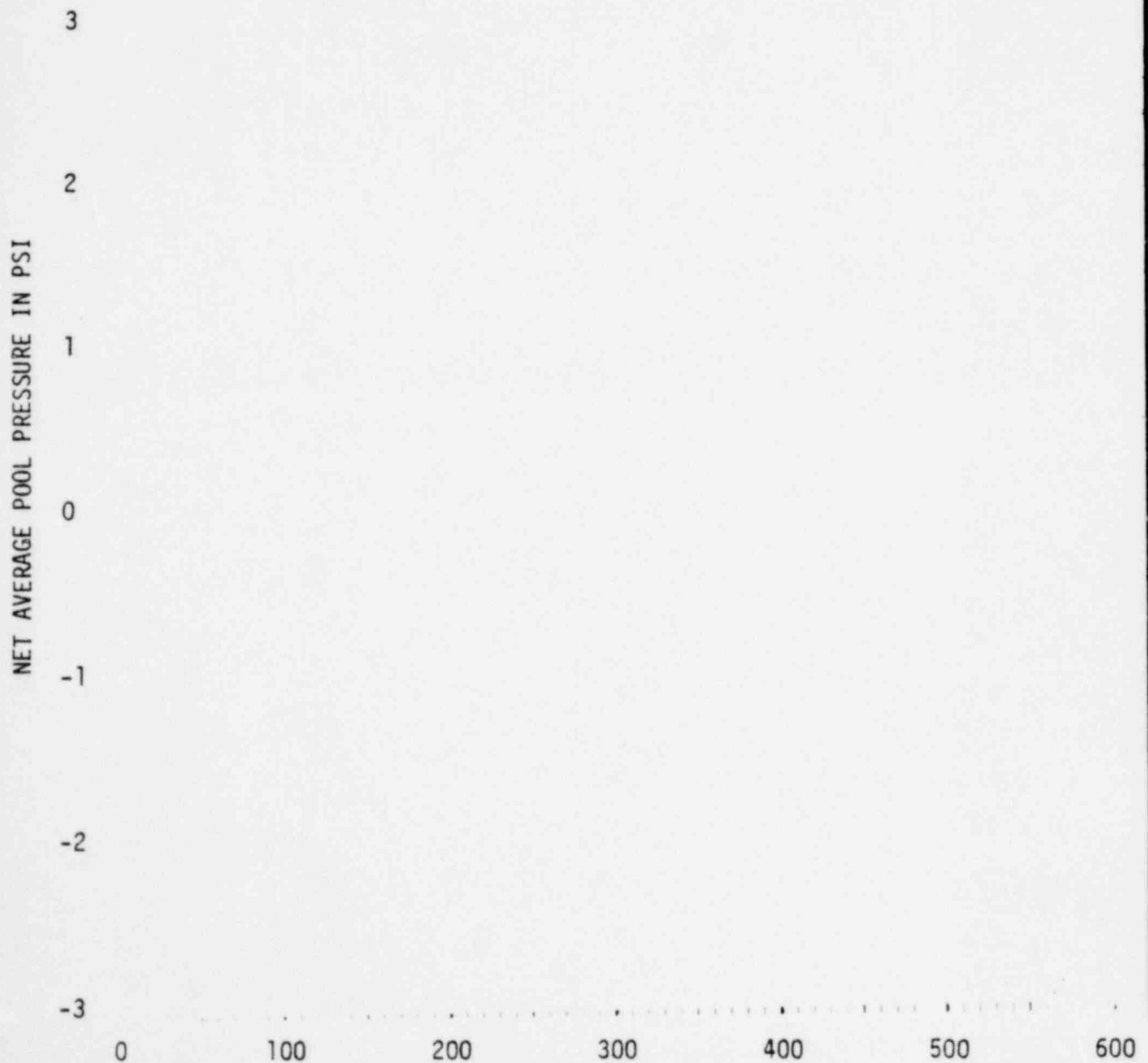


1349 188

FIGURE A-359

NET AVERAGE POOL PRESSURE, CORRECTED FOR WATER INERTIA

Task 5.5.3-2 Dresden Test 3



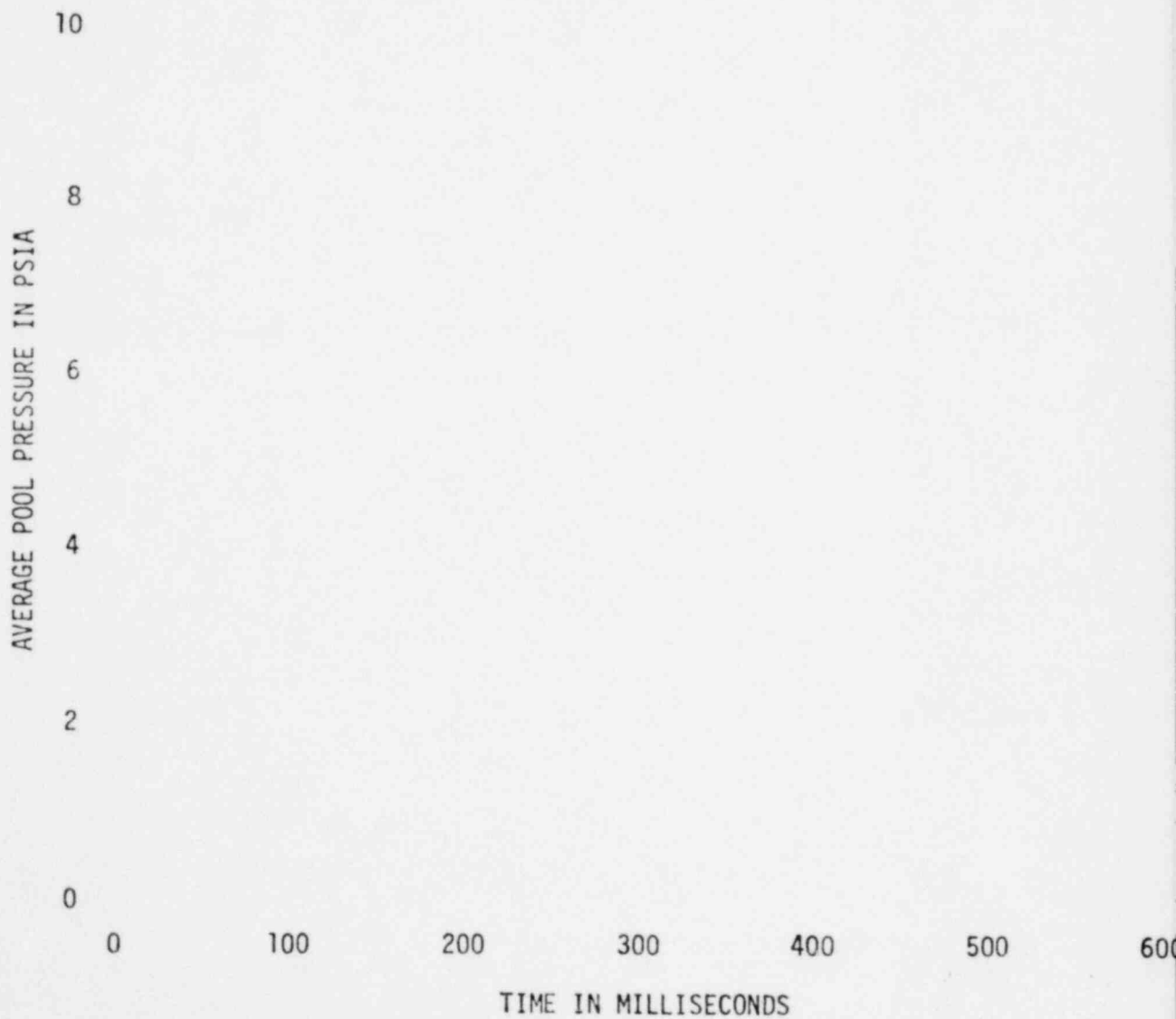
TIME IN MILLISECONDS

1349 189

FIGURE A-360

AVERAGE POOL PRESSURE, CORRECTED FOR WATER INERTIA

Task 5.5.3-2 Dresden Test 5



NEDO-21944

FIGURE A-361

NET AVERAGE PRESSURE, CORRECTED FOR WATER INERTIA

Task 5.5.3-2 Dresden Test 5

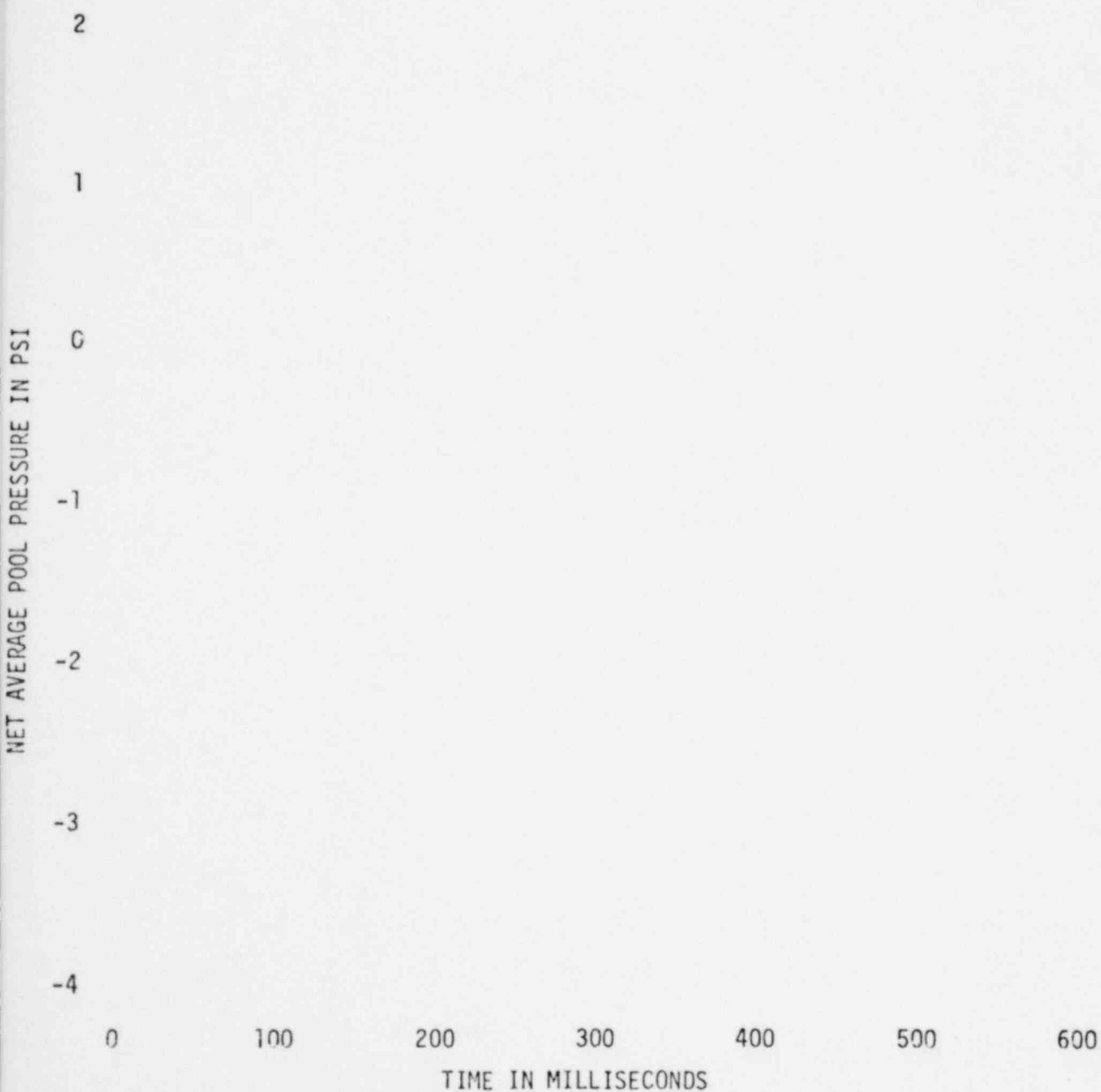
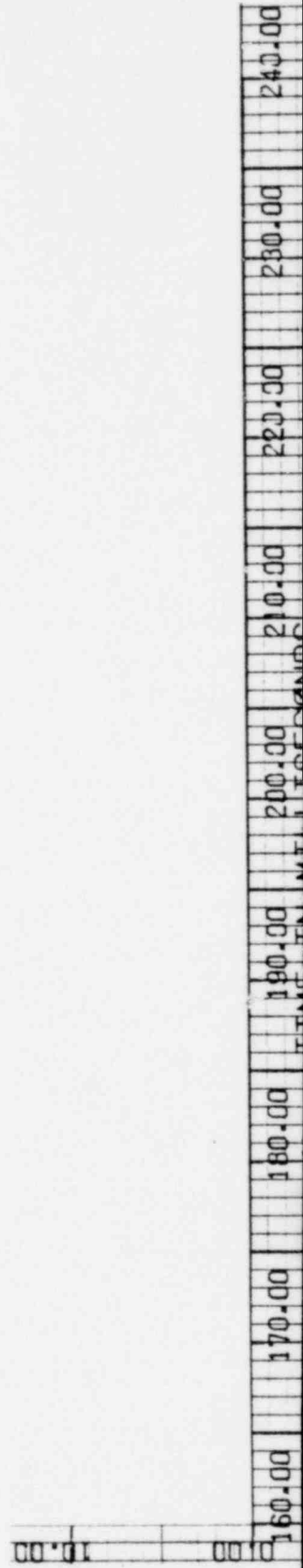
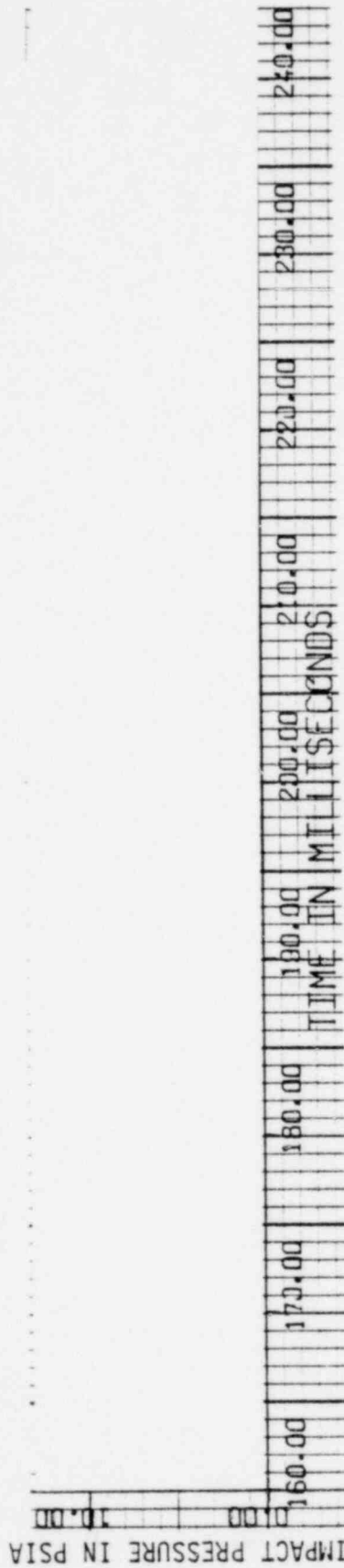


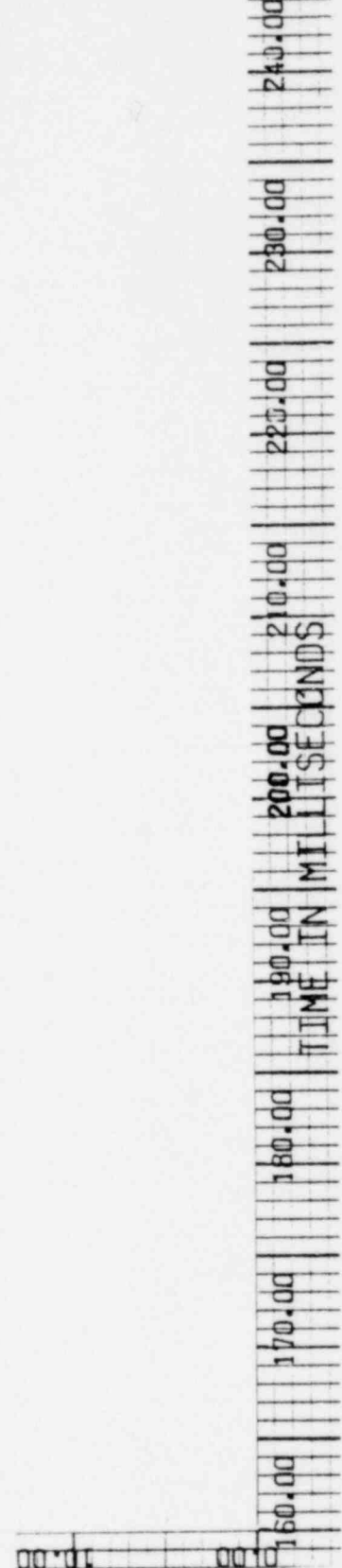
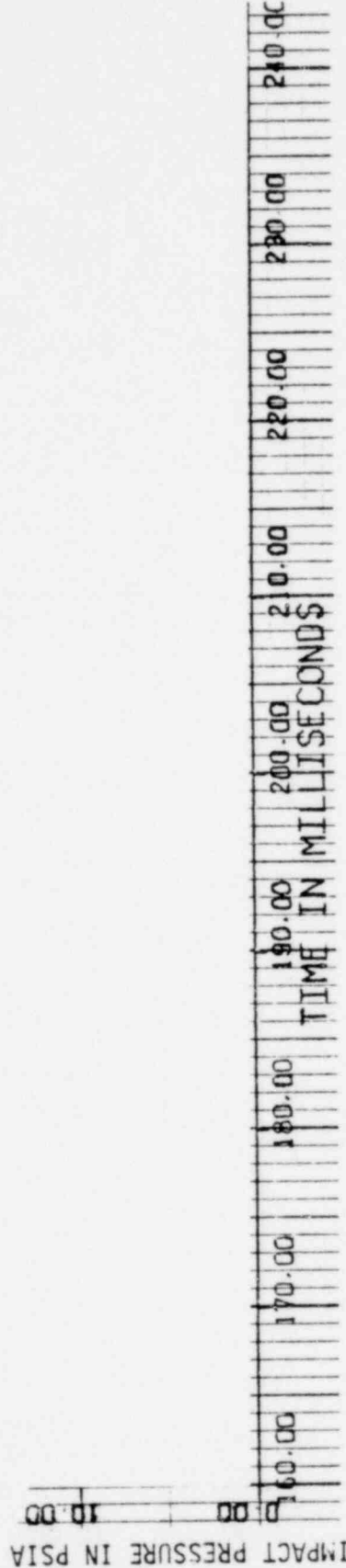
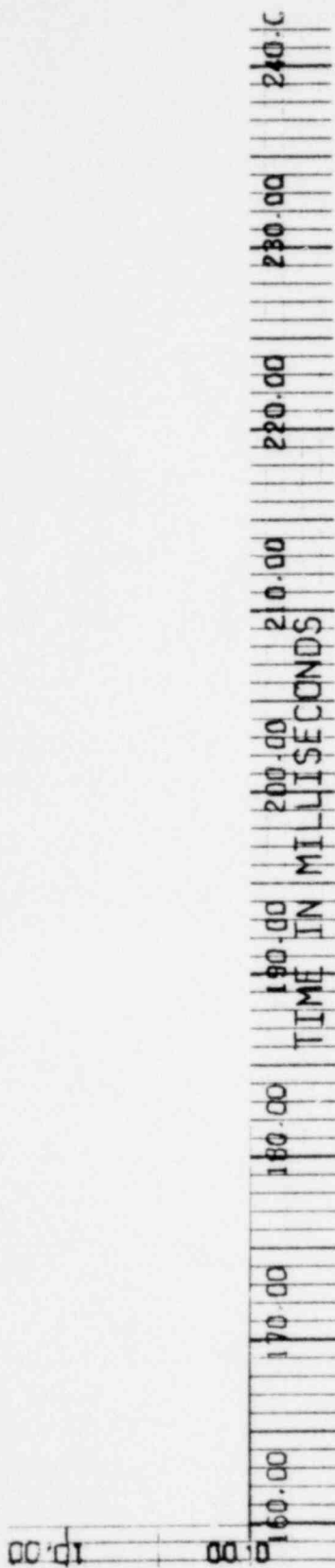
FIGURE A-362

VENT HEADER IMPACT PRESSURES

Task 5.5.3-2 Dresden Test 3



Task 5.5.3-2 Dresden Test 3



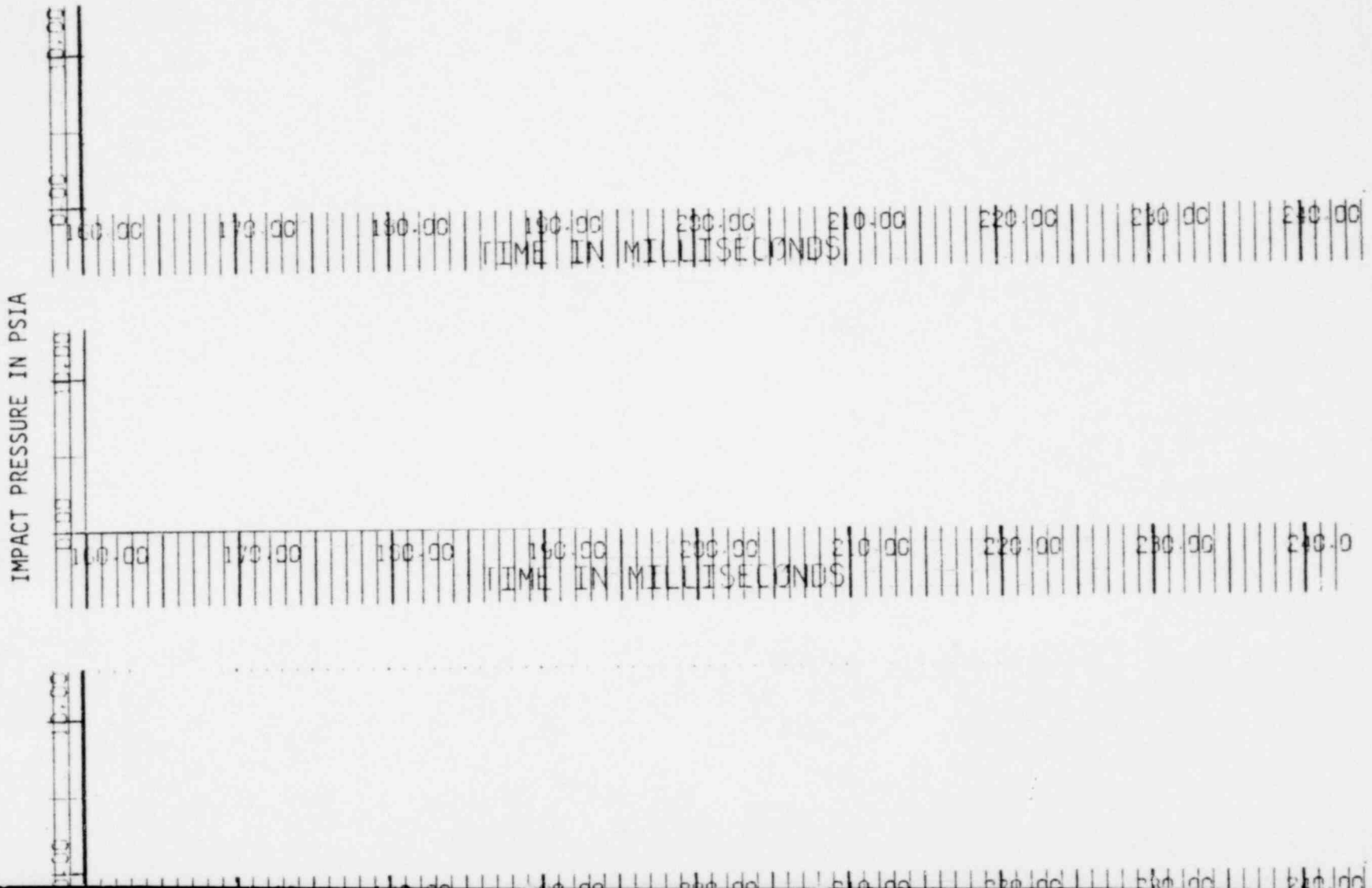
1349 193

FIGURE A-364

NEDE-21944P  
GE COMPANY PROPRIETARY  
CLASS III

VENT HEADER IMPACT PRESSURES

Task 5.5.3-2 Dresden Test 3



A-410

1349 194

NEDE-21944

## Task 5.5.3-2 Dresden Test 3

in mm

0 1 2 3 4 5 6 7 8 9 10 11 12

160.00 170.00 180.00 190.00 200.00 210.00 220.00 230.00 240.00

TIME IN MILLISECONDS

The graph displays a horizontal line at a value of 10.00 on the y-axis, which represents a constant measurement over time. The x-axis is labeled 'TIME IN MILLISECONDS' and ranges from 160.00 to 240.00 with major grid lines every 10.00 units and minor grid lines every 2.00 units. The y-axis has major grid lines at 0.00 and 10.00, with minor grid lines every 2.00 units. The constant value of 10.00 is indicated by a horizontal line that spans the entire time range shown.

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A-411

1349 195

FIGURE A-366

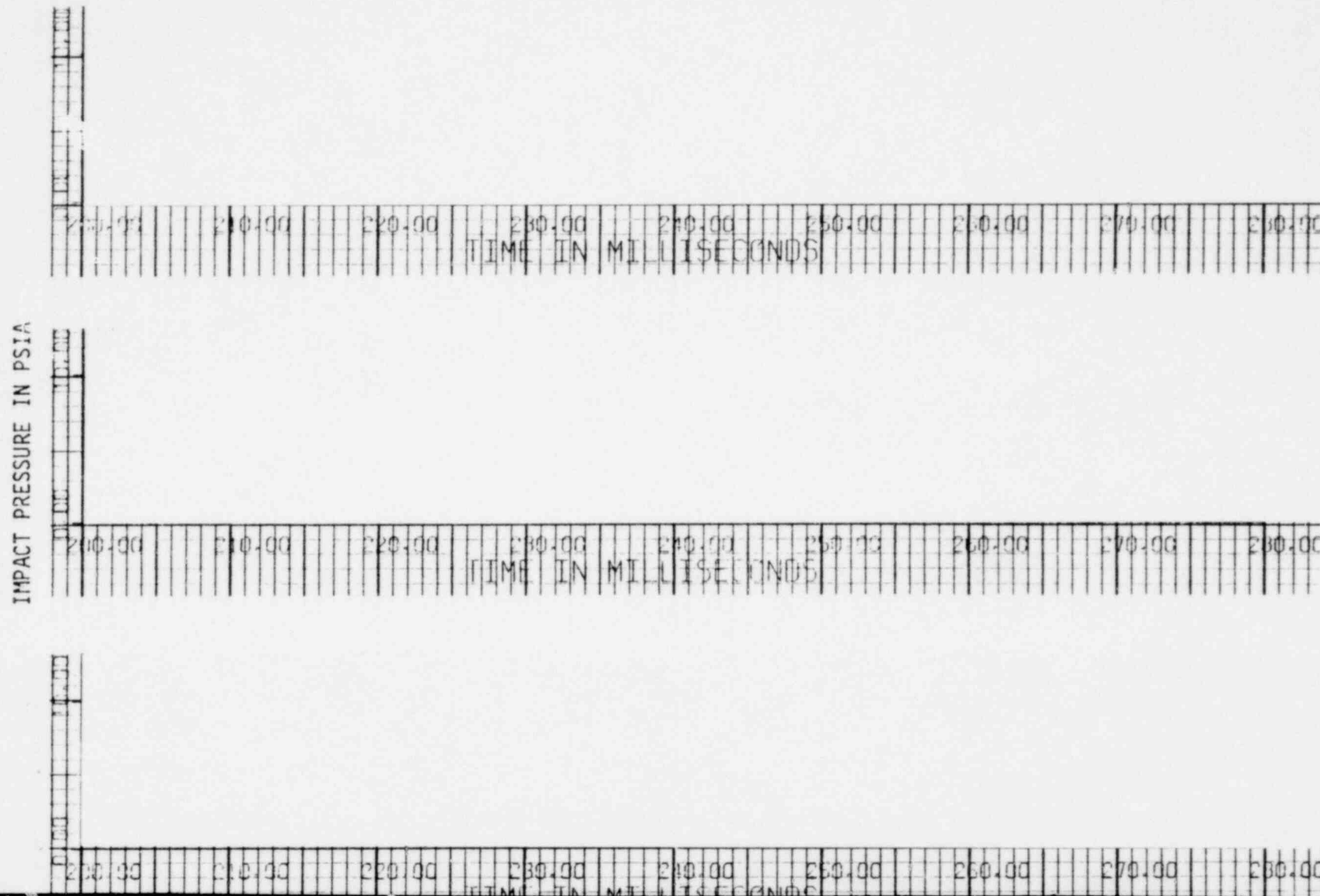
VENT HEADER IMPACT PRESSURES

Task 5.5.3-2 Dresden Test 5

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A-412

1349 196



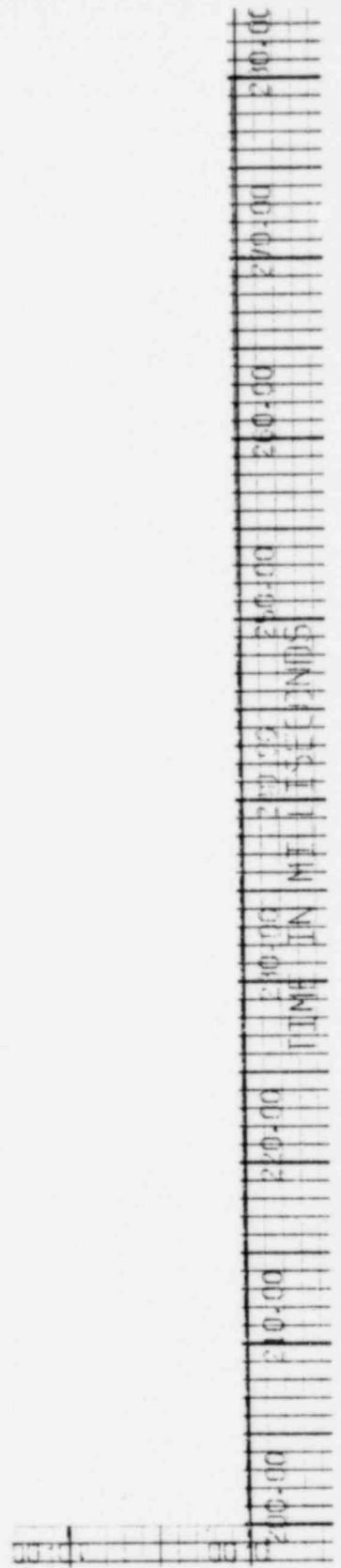
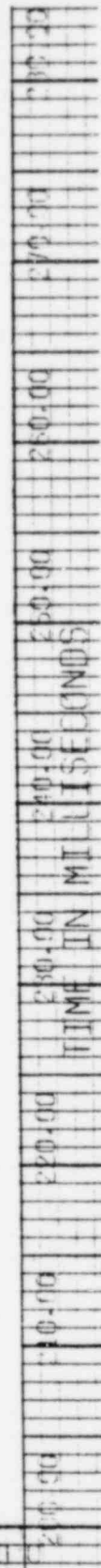
VENT HEADER IMPACT PRESSURES

Task 5.5.3-2 Dresden Test 5



IMPACT PRESSURE IN PSIA

A-413



1349 197

FIGURE A-368

VENT HEADER IMPACT PRESSURES

Task 5.5.3-2 Dresden Test 5

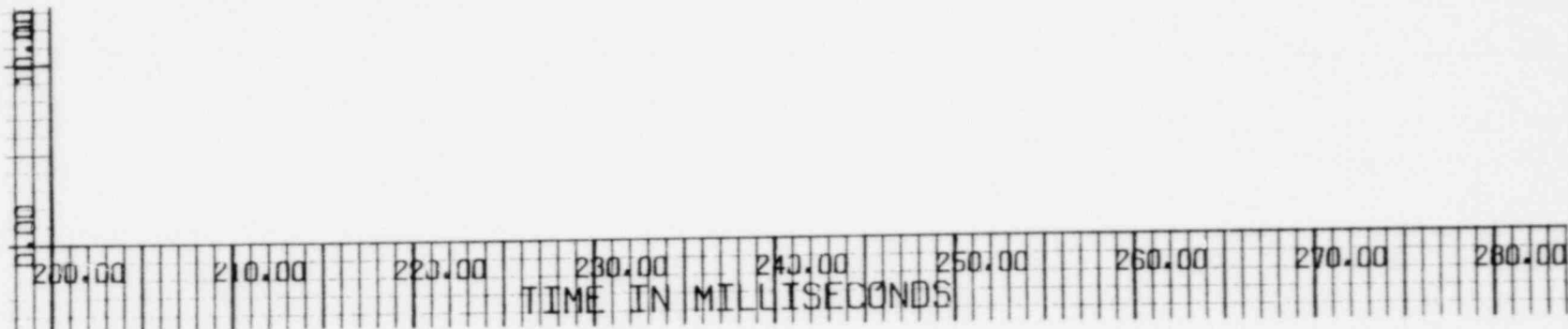


VENT HEADER IMPACT PRESSURES

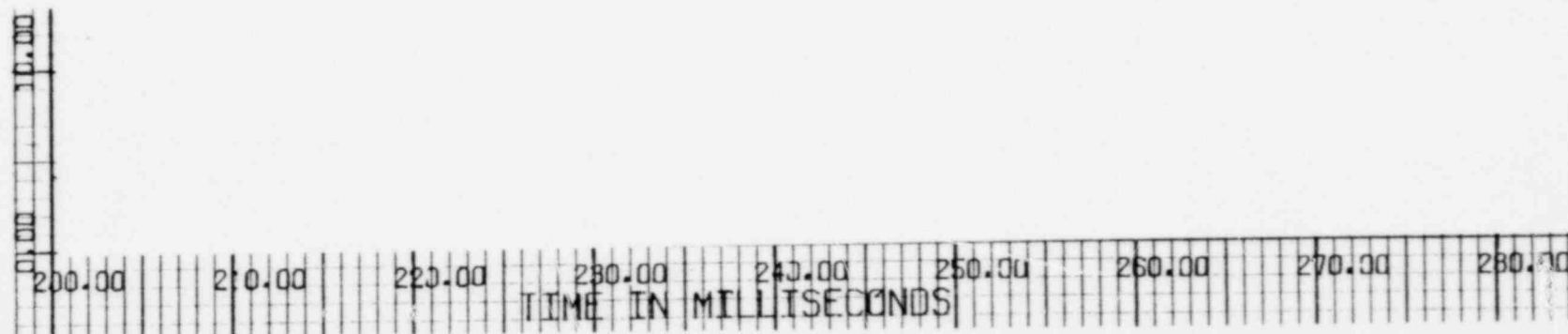
Task 5.5.3-2 Dresden Test 5

No Data for Transducer (T12)

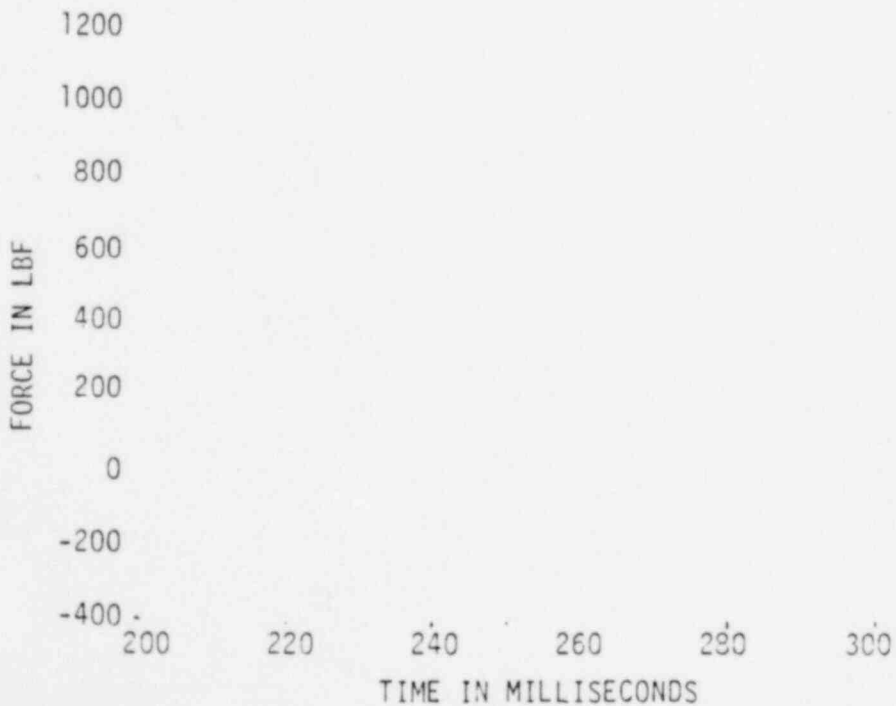
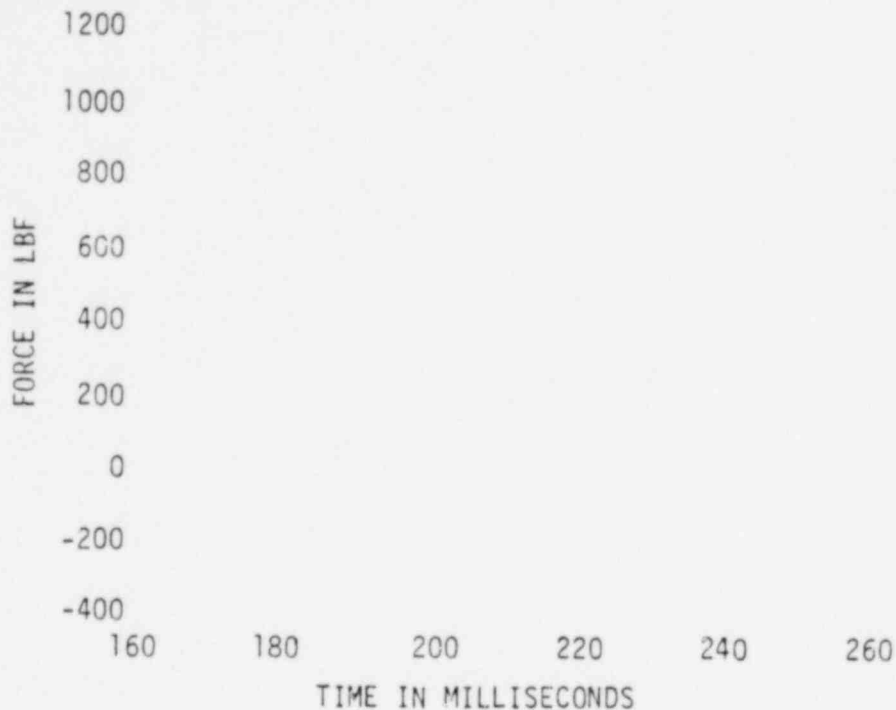
A-415



1349 199



COMPARISON OF VENT HEADER IMPACT RESULTS  
(Corrected Load Cell and Pressure Integration)  
Task 5.5.3 Dresden Tests 3, 5

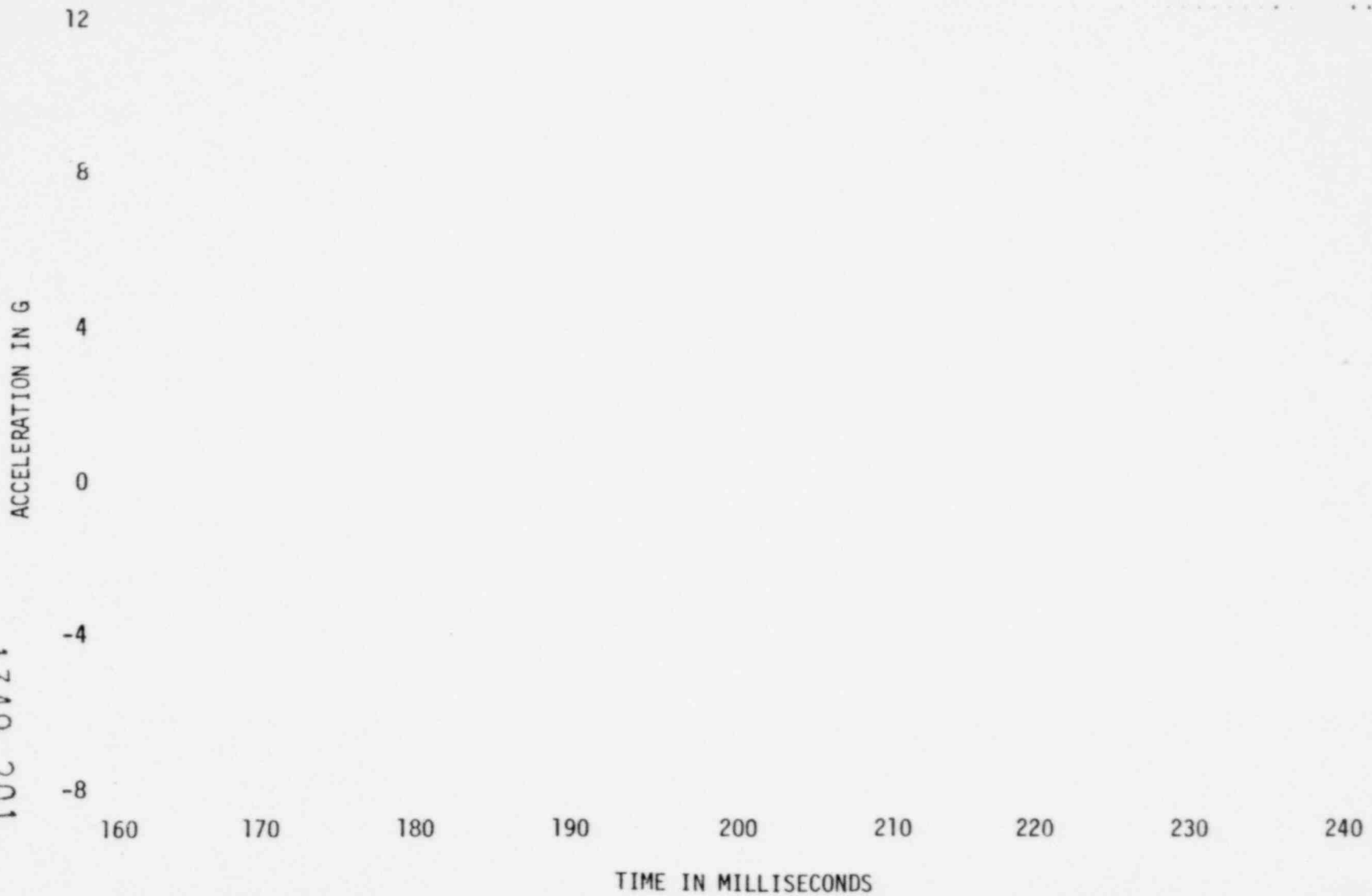


# VENT HEADER VERTICAL ACCELERATION

Task 5.5.3-2 Dresden Test 3

○ Lower Accelerometer

△ Upper Accelerometer



A-417

1349 201

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FIGURE A-372

VENT HEADER VERTICAL ACCELERATION

Task 5.5.3-2 Dresden Test 5

○ Lower Accelerometer

△ Upper Accelerometer



A-418

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NEDO-21944  
FIGURE A-373

TIME HISTORY OF  
POOL DISPLACEMENT

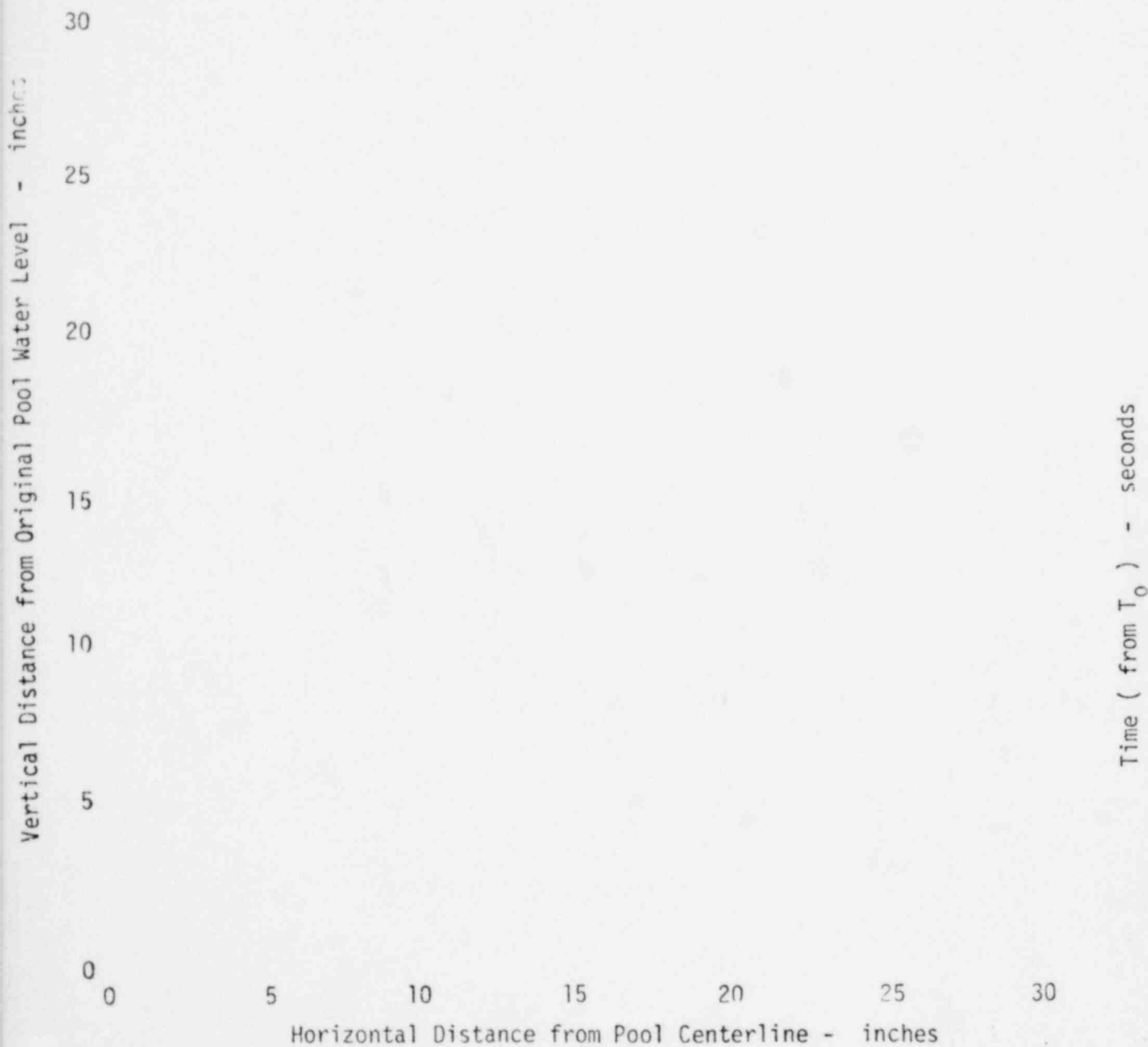
DRESDEN, TEST 1

Time ( from  $T_0$  ) - seconds

0 5 10 15 20 25 30  
Horizontal Distance from Pool Centerline - inches

1349 203

TIME HISTORY OF  
POOL DISPLACEMENT  
DRESDEN, TEST 2



NEDO-21944

FIGURE A-375

TIME HISTORY OF  
POOL DISPLACEMENT

DRESDEN, TEST 3

Time ( from  $T_0$  ) - seconds

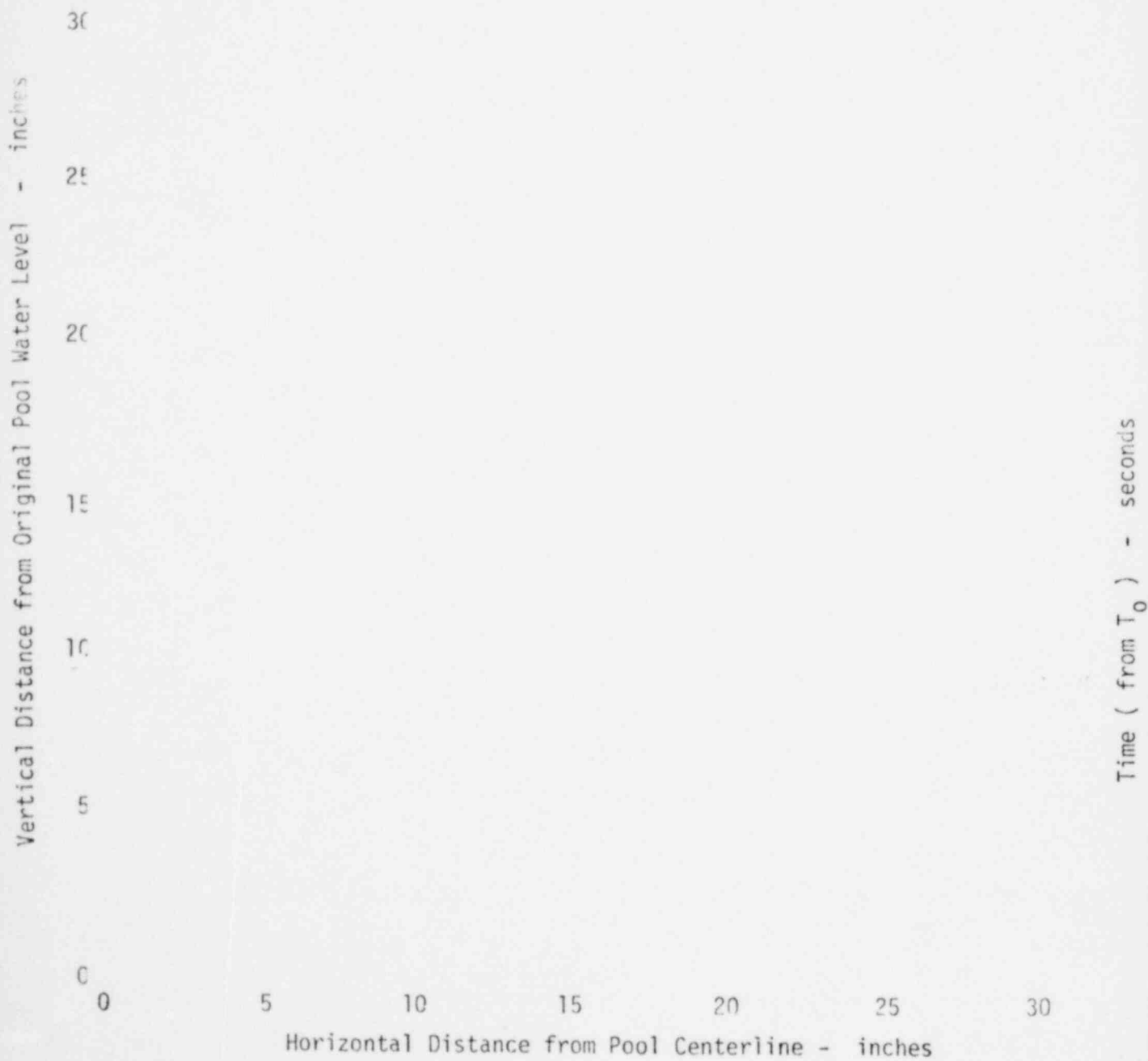
0 5 10 15 20 25 30  
Horizontal Distance from Pool Centerline - inches

1349 205

A-421

TIME HISTORY OF  
POOL DISPLACEMENT

DRESDEN, TEST 5



POOL SURFACE DISPLACEMENT

DRESDEN, TESTS 1, 2, 3

A-377

A-423  
Height above original pool surface in inches

25

20

15

10

5

0

1349 237.0

100

200

Time - milliseconds

300

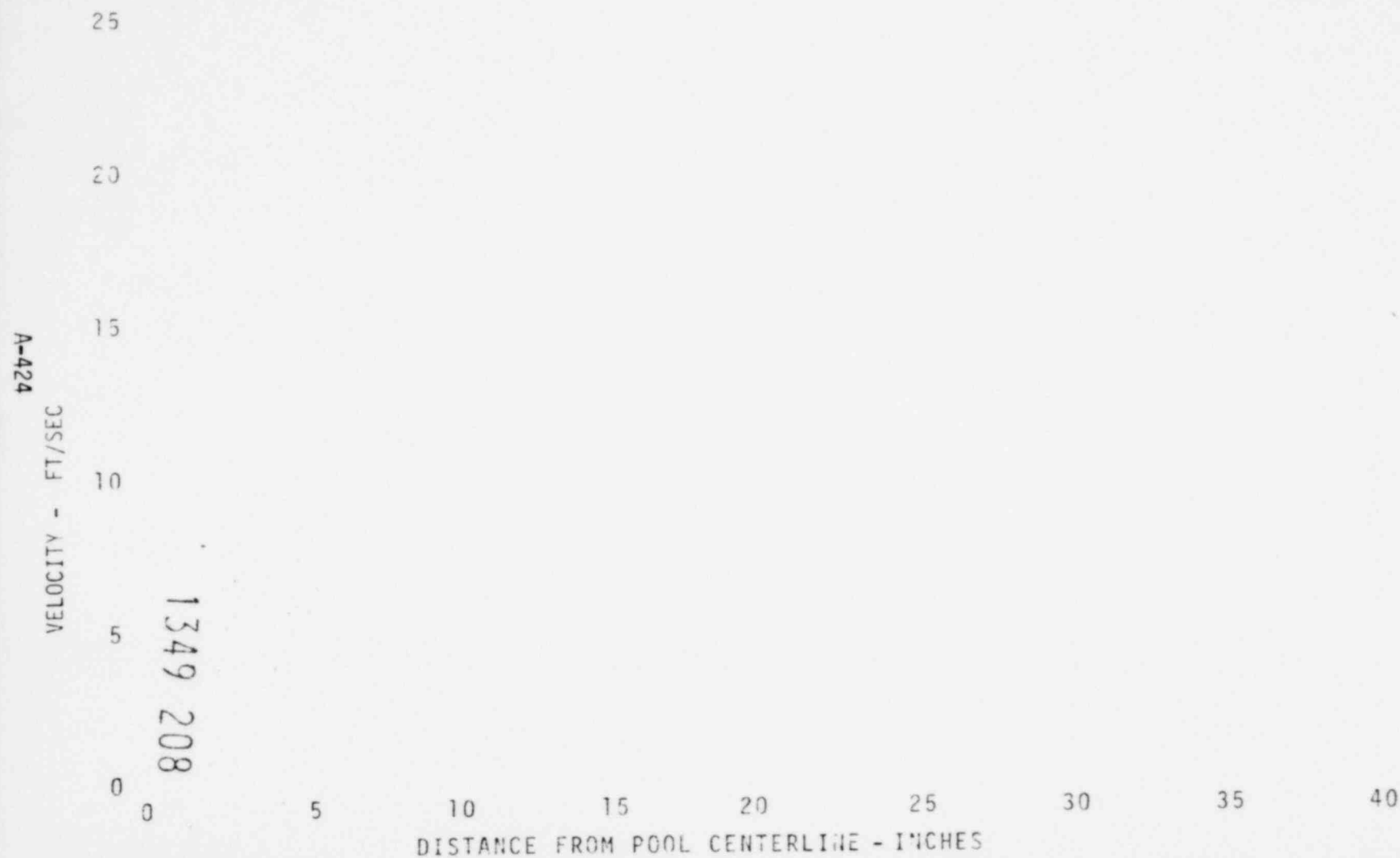
400

NEDO-21944

POOL SURFACE VELOCITY PROFILES

FIGURE A-378

DRESDEN, TESTS 1, 2, 3



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POOL SURFACE DISPLACEMENT

DRESDEN, TEST 5

FIGURE A-379

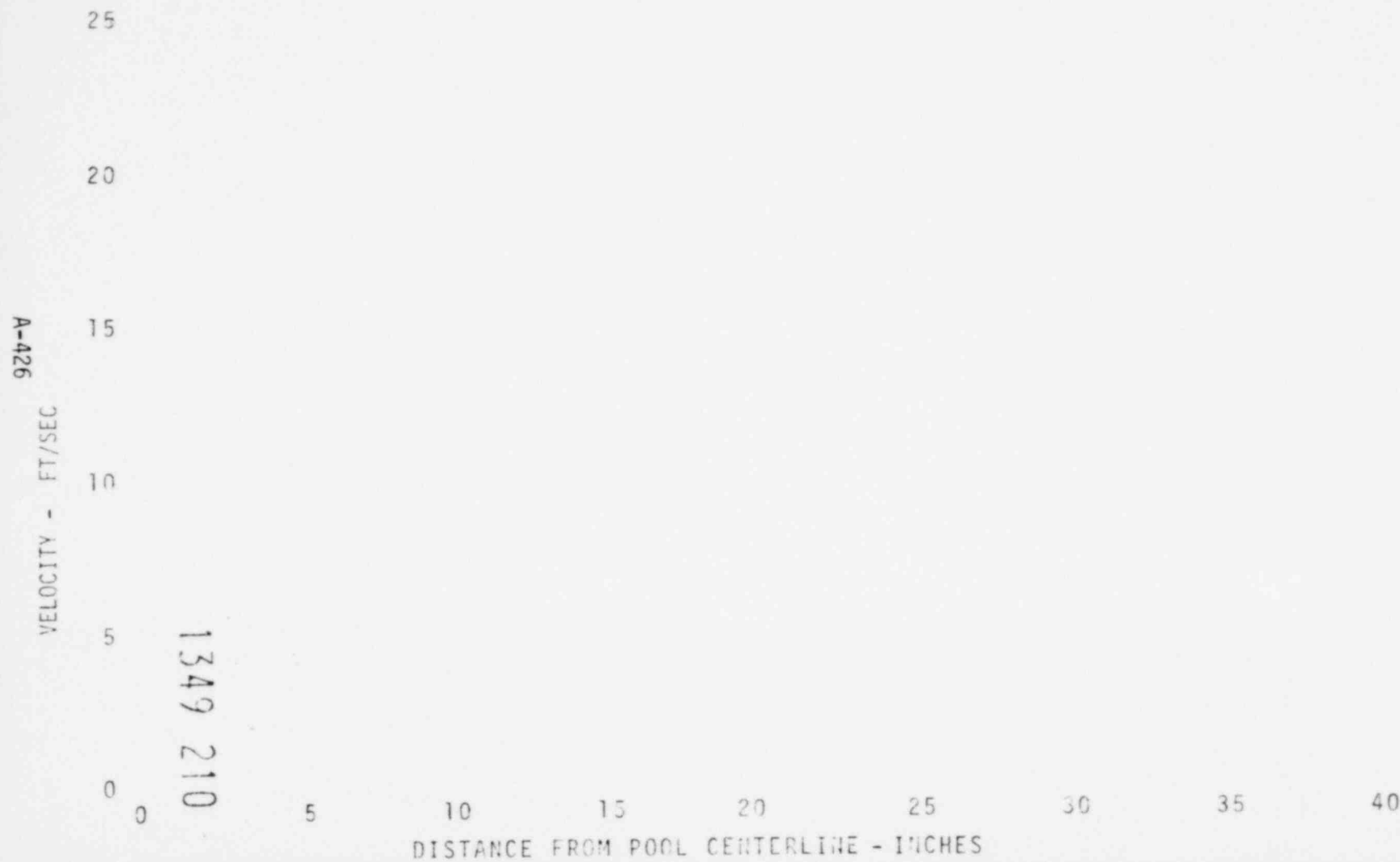


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POOL SURFACE VELOCITY PROFILES

FIGURE A-380

DRESDEN, TEST 5



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NEDO-21944

FIGURE A-381

SIDE WINDOW DISPLACEMENT AND VELOCITY PROFILES

DRESDEN, TEST 4



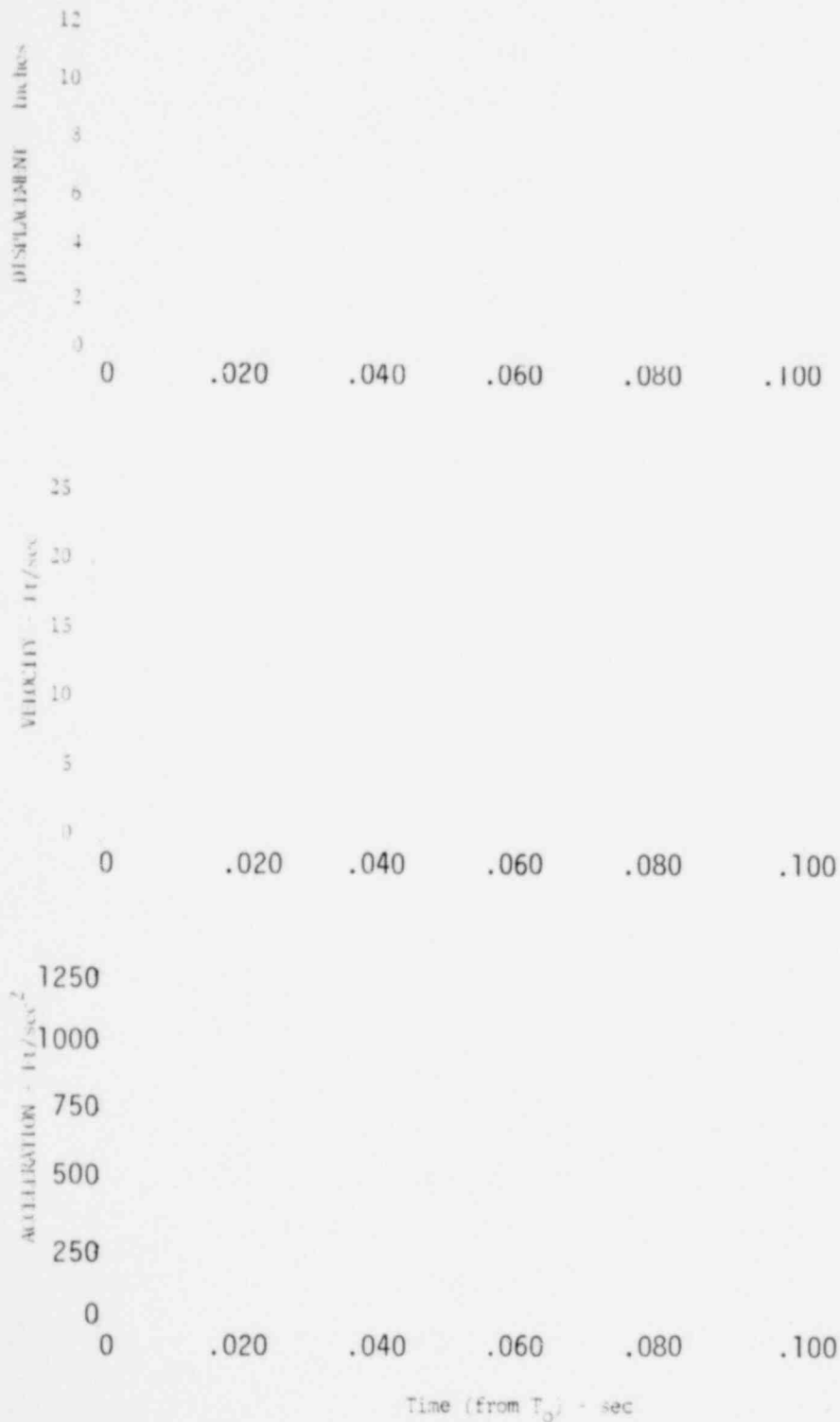
TIME - Seconds

NEDO-21944

FIGURE A-382

DOWNCOMER WATER SLUG EJECTION

DRESDEN, TEST 3



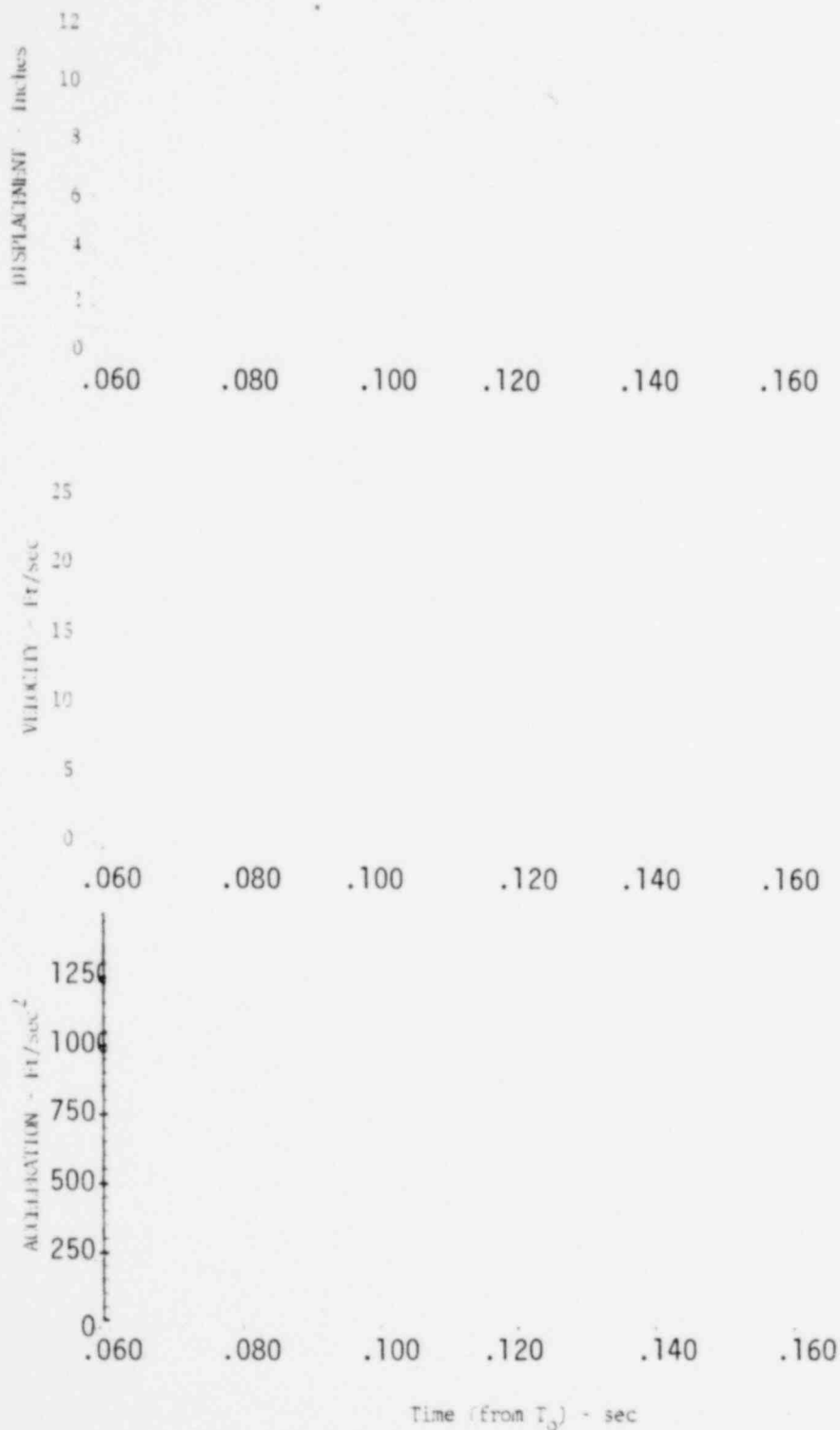
1349 212

NEDO-21944

FIGURE A-383

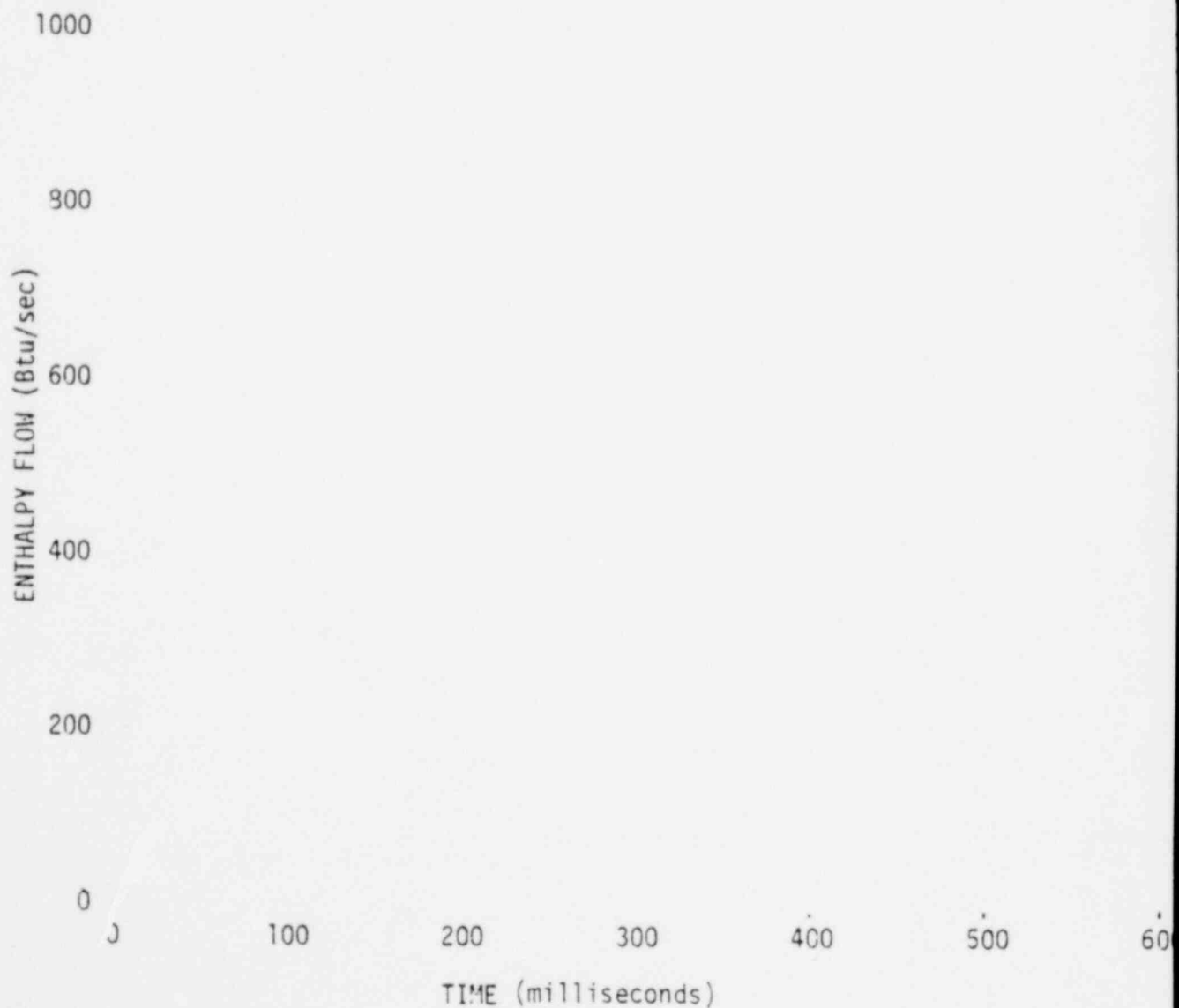
DOWNCOMER WATER SLUG EJECTION

DRESDEN, TEST 5



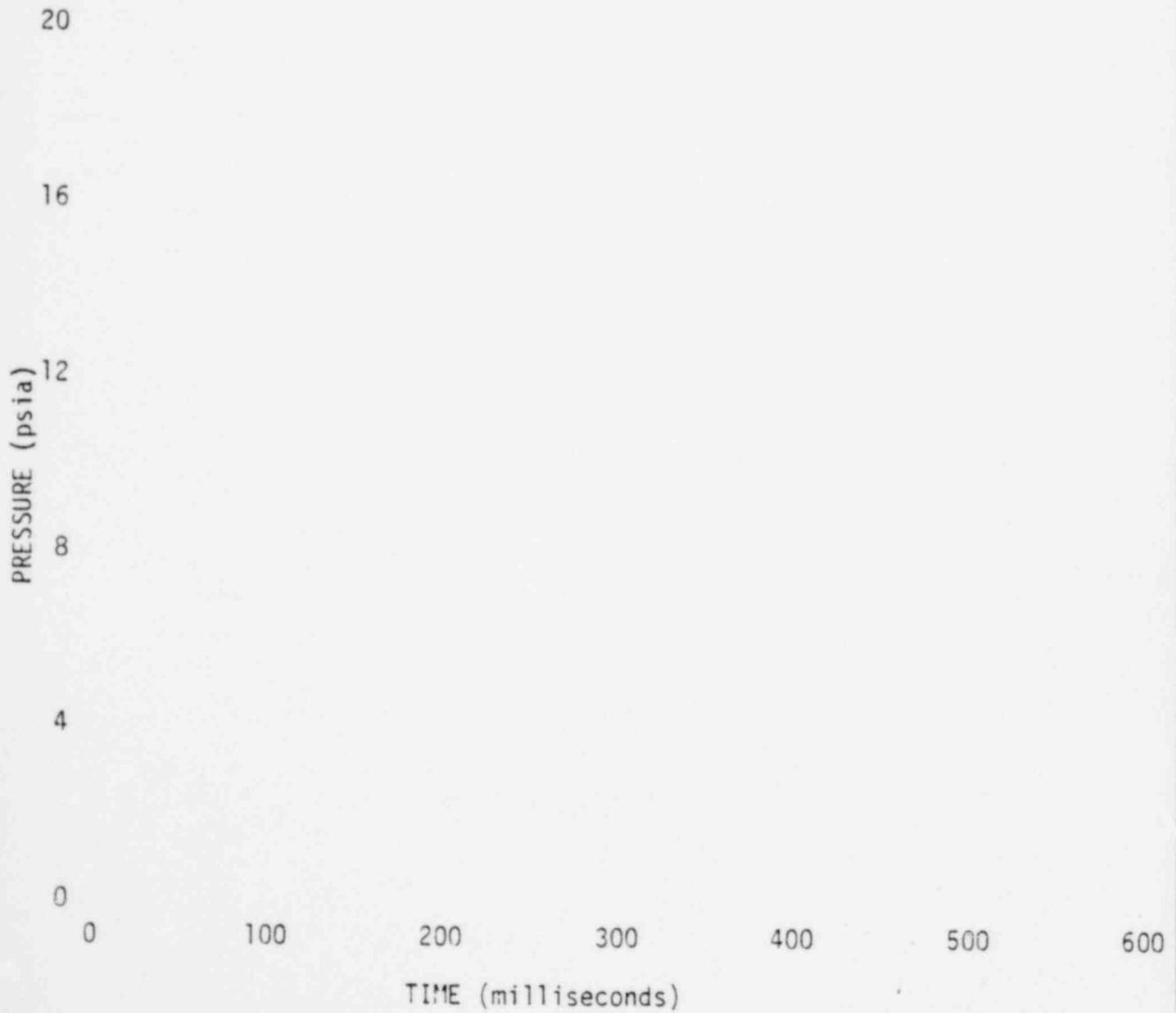
1349 213

FIGURE A-384  
EFFECT OF DRYWELL/WETWELL  $\Delta P$  ON  
ENTHALPY FLOW INTO POOL  
Dresden Tests



1349 214

FIGURE A-385  
EFFECT OF DRYWELL/WETWELL  $\Delta P$  ON  
DOWNCOMER INTERNAL PRESSURE  
Dresden Tests



1349 215

FIGURE A-386

EFFECT OF DRYWELL/WETWELL  $\Delta P$  ON POOL PRESSURE

AT 180 DEGREE AND FREESPACE PRESSURE

Dresden Tests

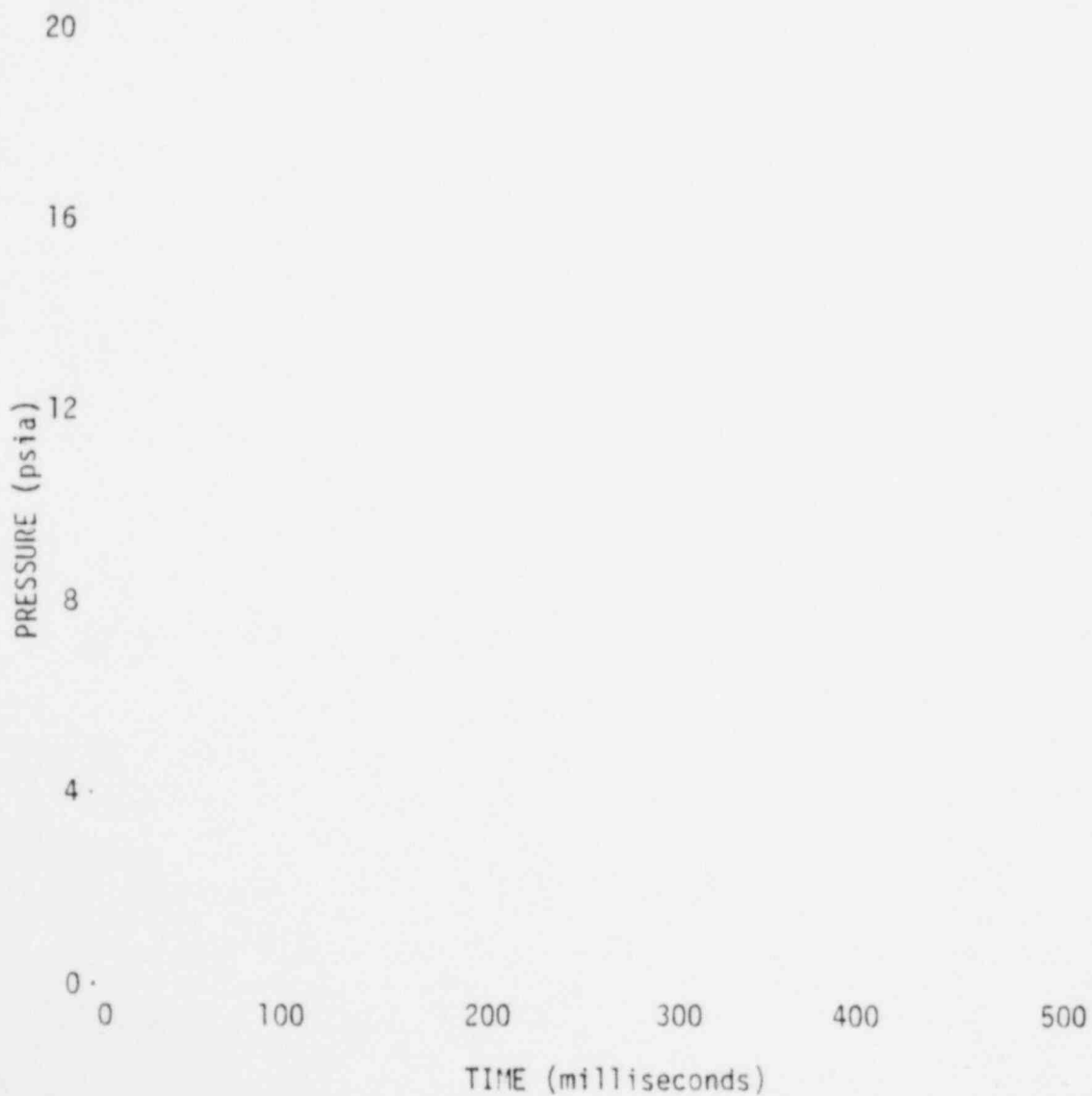


TABLE A-17

\*Time at force is zero (from  $T_0$ )

## DATA FOR WETWELL VERTICAL LOADS (continued)

## Task 5.5.3-2 Dresden Tests

Parameter	Test No.	7.15" $\Delta P$ , 5.17" Pipe Deflector (20" Full Scale)					0" $\Delta P$	
		(1)	(2)	(3)	(4)	Mean	Std. Dev.	(5)
<u>Peak Upforce</u>								
Pressure Integral:								
Force (lb)	(1b)							
Time (from $T_0$ ) (sec)	(sec)							
Corrected Pressure Integral:								
Force (lb)	(1b)							
Time (from $T_0$ ) (sec)	(sec)							
Corrected Load Cell:								
Force (lb)	(1b)							
Time (from $T_0$ ) (sec)	(sec)							
<u>Force Valley</u>								
Pressure Integral:								
Force (lb)	(1b)							
Time (from $T_0$ ) (sec)	(sec)							
Corrected Pressure Integral:								
Force (lb)	(1b)							
Time (from $T_0$ ) (sec)	(sec)							
Corrected Load Cell:								
Force (lb)	(1b)							
Time (from $T_0$ ) (sec)	(sec)							
<u>End Peak Upforce</u>								
Pressure Integral:								
Force (lb)	(1b)							
Time (from $T_0$ ) (sec)	(sec)							
Corrected Pressure Integral:								
Force (lb)	(1b)							
Time (from $T_0$ ) (sec)	(sec)							
Corrected Load Cell:								
Force (lb)	(1b)							
Time (from $T_0$ ) (sec)	(sec)							
<u>Pro Force Time*</u>								
Pressure Integral (sec)	(sec)							
Corrected Pressure Integral (sec)	(sec)							
Corrected Load Cell (sec)	(sec)							

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TABLE A-17

DATA FOR WETWELL VERTICAL LOADS

Task 5.5.3-2 Dresden Tests

\*Vent clearing time (from  $T_0$ ) determined from the movie films.

\*\*Time difference from  $T_0$  to time of zero downforce.

\*(1) Start-of-test reference time

Parameter	Test No.	7.15" $\Delta P$ , 5.17" Pipe Deflector (20" Full Scale)					Std. Dev.	0" $\Delta P$ (5)
		(1)	(2)	(3)	(4)	Mean		
* (1)								
$T_0$	(sec)							
Vent Clearing Time*	(sec)							
<u>Peak Downforce</u>								
Pressure Integral:								
Force	(lb)							
Time (from $T_0$ )	(sec)							
Corrected Pressure Integral:								
Force	(lb)							
Time (from $T_0$ )	(sec)							
Corrected Load Cell:								
Force	(lb)							
Time (from $T_0$ )	(sec)							
<u>Downforce Valley</u>								
Pressure Integral:								
Force	(lb)							
Time (from $T_0$ )	(sec)							
Corrected Pressure Integral:								
Force	(lb)							
Time (from $T_0$ )	(sec)							
Corrected Load Cell:								
Force	(lb)							
Time (from $T_0$ )	(sec)							
<u>2nd Peak Downforce</u>								
Pressure Integral:								
Force	(lb)							
Time (from $T_0$ )	(sec)							
Corrected Pressure Integral:								
Force	(lb)							
Time (from $T_0$ )	(sec)							
Corrected Load Cell:								
Force	(lb)							
Time (from $T_0$ )	(sec)							
<u>[<math>\Delta t</math>] Downforce Time**</u>								
Pressure Integral	(sec)							
Corrected Pressure Integral	(sec)							
Corrected Load Cell	(sec)							
<u>Downforce Impulse</u>								
Pressure Integral:								
Impulse	(lb-sec)							

TABLE A-18

DATA FOR VENT HEADER IMPACT LOADS

Task 5.5.3-2 Dresden Tests

Parameter \ Test No.	7.15" $\Delta P$ , 5.18" Deflector				0" $\Delta P$	
	( 1 )	( 2 )	( 3 )	( 4 )	Mean	Std. Dev. ( 5 )
$T_0^+$ (sec)						
Vent Header Impact						
Pressure Integral:						
Maximum Force (lb)						
Impulse (lb-sec)						
Duration* (sec)						
Load Cell Corrected:††						
Maximum Force (lb)						
Impulse (lb-sec)						
Duration (sec)						
Pool Surface Velocity (ft/sec)						
Time (from $T_0$ )** (sec)						

\*Based on impact pressure measurements

\*\*At start of the first impact pressure recorded.

†Start of reference time

††represents peak of very noisy data (acceleration corrected); mean value would be lower

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