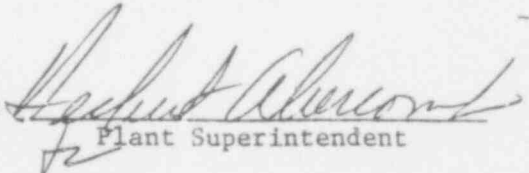


TENNESSEE VALLEY AUTHORITY  
BROWNS FERRY NUCLEAR PLANT

TECHNICAL INSTRUCTION 47

OFFSITE DOSE CALCULATION MANUAL (ODCM)

Approved: 

Plant Superintendent

Date: 

June 21, 1979

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## 1. Gaseous Effluents

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### 1.1 Alarm/Trip Setpoints

Specification 3.8.B.1 requires that the dose rate in unrestricted areas due to gaseous effluents from the site shall be limited at all times to the following values:

1. 500 mrem/y to the total body and 3,000 mrem/y to the skin from noble gases.
2. 1,500 mrem/y to any organ from radioiodines and particulates.

Specification 3.2.K.1 requires gaseous effluent monitors to have alarm/trip setpoints to ensure that the above dose rates are not exceeded. This section of the ODCM describes the methodology that will be used to determine these setpoints.

The methodology for determining alarm/trip setpoints is divided into two major parts. The first consists of backcalculating from a dose rate to a release rate limit, in  $\mu\text{Ci/s}$ , for each nuclide and release point. The second consists of using the release rate limits to determine the physical settings on the monitors. The methodology for the latter is contained in Technical Instruction 15.

#### 1.1.1 Release Rate Limit Methodology - $\mu\text{Ci/s}$

##### Step 1

The first step involves calculating a dose rate based on the design objective source term mix used in the licensing of the plant. Historical meteorological data used are in this calculation.

Doses are determined for (1) noble gases and (2) iodines and particulates. Depending on the pathway involved, either air concentrations or ground concentrations are calculated.

- A. Equations and assumptions for calculating doses from noble gases are as follows:

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Assumptions

1. Doses to be calculated are total body and skin.
2. Exposure pathway is submersion within a cloud of noble gases.
3. Noble gas radionuclide mix is based on the expected source term given in Table 1.1.
4. Basic radionuclide data are given in Table 1.2.
5. Releases are treated as ground-level, split-level, or elevated.
6. Meteorological data are expressed as joint frequency distributions (JFD's) of wind speed, wind direction, and atmospheric stability for the period January 1974 to December 1975 (Table 1.3). Releases from the turbine building are treated as 100 percent ground level, whereas stack releases are considered 100 percent elevated. Releases from the reactor building and radwaste building are treated as split-level; i.e., partly elevated and partly ground level.
7. Raw meteorological data for ground-level releases consist of wind speed and direction measurements at 10 m and temperature measurements at 10 m and 45 m. The ground-level portion of the split-level JFD was based on wind speeds and directions measured at the 10 m level and temperature measurements at 10 and 45 m. The elevated portion of the split-level JFD was based on wind speeds and directions measured at 46 m and temperature measurements at 45 and 90 m. Wind speeds and directions for elevated releases were measured at 93 m. Stability class D was assumed to persist during the entire period for elevated releases.
8. Dose is to be evaluated at the offsite exposure point where maximum concentrations are expected to exist.
9. Potential maximum-exposure (Table 1.4) considered are the nearest site boundary points in each sector.

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10. A semi-infinite cloud model is used.
11. No credit is taken for shielding by residence.
12. Plume depletion and radioactive decay are considered.
13. Building wake effects on effluent dispersion are considered.
14. A sector-average dispersion equation is used.
15. The wind speed classes that are used are as follows:

<u>Number</u>	<u>Range (m/s)</u>	<u>Midpoint (m/s)</u>
1	<0.3	0
2	0.3-0.6	0.45
3	0.7-1.5	1.10
4	1.6-2.4	1.99
5	2.5-3.3	2.80
6	3.4-5.5	4.45
7	5.6-8.2	6.91
8	>10.9	13.00

16. The stability classes that will be used are the standard A through G classifications. The stability classes 1-7 will correspond to A=1, B=2, . . . , G=7.
17. Terrain elevations are considered.

#### Equations

To calculate the dose from radioactive effluents discharged from a given release point for any one of the 16 potential maximum-exposure points, the following equations are used.

For determining the air concentration of any radionuclide:

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$$X_i = \sum_{j=1}^9 \sum_{k=1}^7 \left( \frac{2}{\pi} \right)^{1/2} \frac{f_{jk} Q_i p}{\sum_{zk} u_j (2\pi x/n)} \exp \left( -\lambda_i \frac{x}{u_j} \right) \exp \left( -\frac{h_e^2}{2\sigma_{zk}^2} \right) \quad (1.1)$$

where

$X_i$  = air concentration of radionuclide  $i$ ,  $\mu\text{Ci}/\text{m}^3$ .

$f_{jk}$  = joint relative frequency of occurrence of winds in windspeed class  $j$ , stability class  $k$ , blowing toward this exposure point, expressed as a fraction.

$Q_i$  = average release rate of radionuclide  $i$ ,  $\mu\text{Ci}/\text{s}$ .

$p$  = fraction of radionuclide remaining in plume,

Figure 1.1.

$\Sigma_{zk}$  = vertical dispersion coefficient for stability class  $k$  which includes a building wake adjustment,  $\Sigma_{zk} = \left[ \sigma_{zk}^2 + 0.5A/\pi \right]^{1/2}$ , where  $\sigma_{zk}$  is the vertical dispersion coefficient for stability class  $k$  (m), and  $A$  is

the minimum building cross-sectional area ( $2,350 \text{ m}^2$ ), m.

$u_j$  = midpoint value of wind speed class interval  $j$ , m/s.

$x$  = downwind distance, m.

$n$  = number of sectors, 16.

$\lambda_i$  = radioactive decay coefficient of radionuclide  $i$ ,  $\text{s}^{-1}$ .

$2\pi x/n$  = sector width at point of interest, m.

$h_e$  = effective release height, m.

For effluents exhausted from release points that are higher than twice the height of adjacent structures (elevated releases) the effective release height is determined by

$$h_e = h_s + h_{pr} - h_t - c \quad (1.1a)$$

where

$c$  = correction for low relative exit velocity,  $c = 3(1.5 - W_0/\bar{u})$  d,

where  $W_0$  = vertical plume exit velocity (m/s),  $\bar{u}$  = mean windspeed (m/s), and  $d$  = inside diameter of the release point, m.

$h_{pr}$  = plume rise above release point, m.

$h_s$  = physical height of release point, m.

$h_t$  = maximum terrain height between release point and receptor location ( $h_t$  can be any real number), m.

For effluents released from points less than the height of adjacent structures, a ground level release is assumed ( $h_e = 0$ ).

For effluents released from points at the level of or above adjacent structures, but lower than elevated release points, releases are treated as follows:

Case 1 - elevated if  $W_0/\bar{u} \geq 5$

Case 2 - ground-level ( $h_e = 0$ ) if  $W_0/\bar{u} \leq 1$ .

Case 3 - split-level if  $1 < W_0/\bar{u} < 5$ .

Under Case 3 a split-level dispersion approach is implemented using a model that requires for each release point two JFD's, one for elevated releases and one for ground-level releases. The summation of the elevated and ground-level JFD's account for the total period of record. Releases are considered to be elevated  $100(1 - E_t)$  percent of the time and ground-level  $100 E_t$  percent of the time where the entrainment coefficient,  $E_t$ , is defined by

$$E_t = 2.58 - 1.58 (W_0/\bar{u}) \text{ for } 1 < W_0/\bar{u} \leq 1.5 \quad (1.1b)$$

$$E_t = 0.3 - 0.06 (W_0/\bar{u}) \text{ for } 1.5 < W_0/\bar{u} \leq 5 \quad (1.1c)$$

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For determining the total body dose rate

$$D_{TB} = 1 \times 10^6 \sum_1 X_1 DFB_1 \quad (1.2)$$

where

$D_{TB}$  = total body dose rate, mrem/y.

$X_1$  = air concentration of radionuclide 1,  $\mu\text{Ci}$

$DFB_1$  = total body dose factor due to gamma radiation, mrem/y per  $\text{pCi}/\text{m}^3$  (Table 1.5).

$1 \times 10^6$  = pCi/ $\mu\text{Ci}$  conversion factor.

For determining the skin dose rate

$$D_s = 1 \times 10^6 \sum_1 X_1 [DFS_1 + 1.11 DFY_1] \quad (1.3)$$

where

$D_s$  = skin dose rate, mrem/y.

$X_1$  = air concentration of radionuclide 1,  $\mu\text{Ci}/\text{m}^3$ .

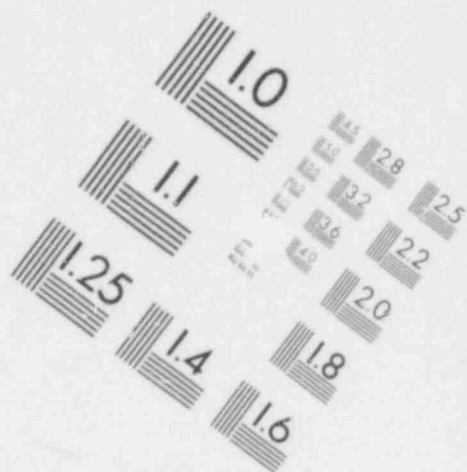
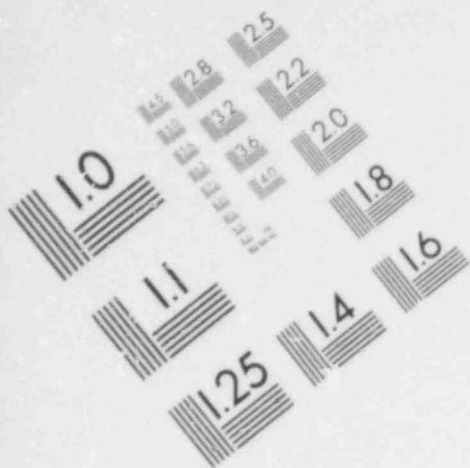
$DFS_1$  = skin dose factor due to beta radiation, mrem/y per  $\text{pCi}/\text{m}^3$  (Table 1.5).

$DFY_1$  = gamma-to-air dose factor for radionuclide 1, mrem/y per  $\text{pCi}/\text{m}^3$  (Table 1.5).

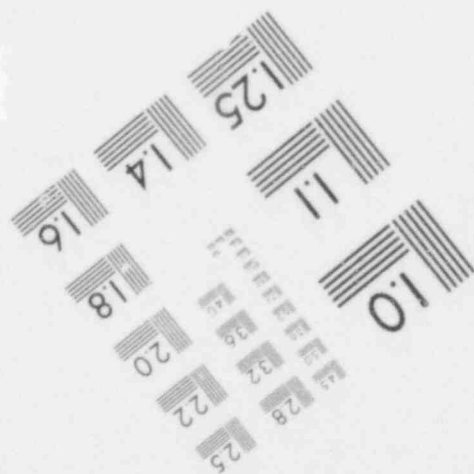
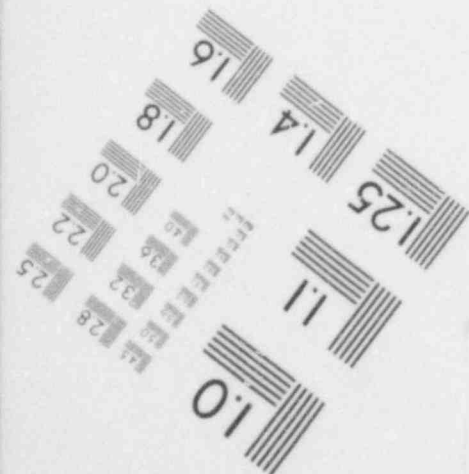
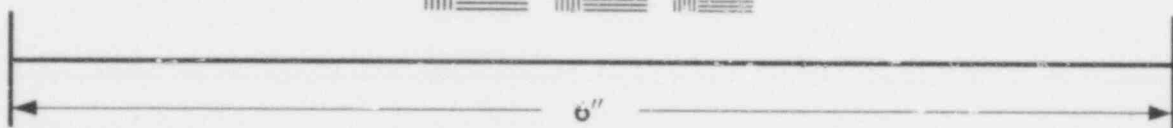
$1 \times 10^6$  = pCi/ $\mu\text{Ci}$  conversion factor.

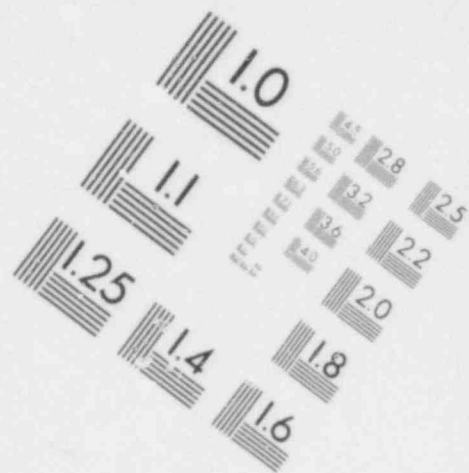
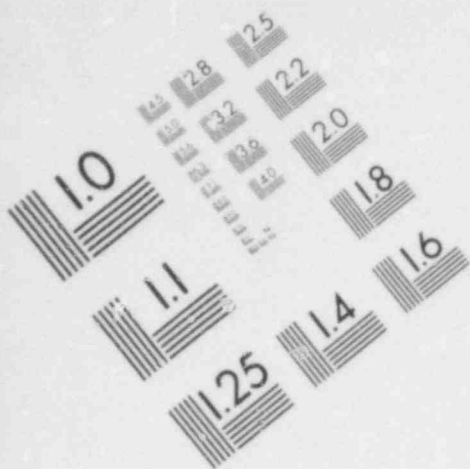
The above dose calculations are repeated for each release point (vent or stack) and then summed to obtain maximum total body and skin dose rates. The maximum total body and skin dose rates will then be used in step 2.

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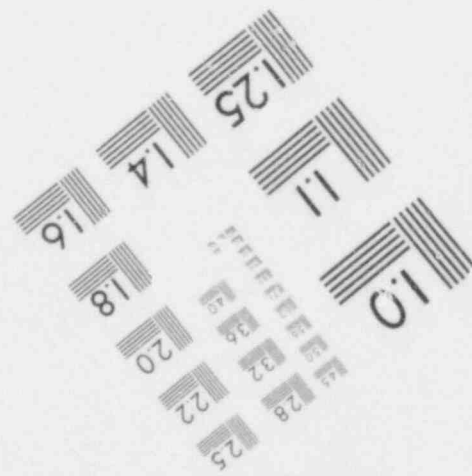
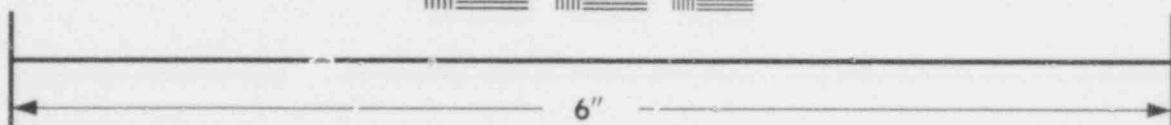


# IMAGE EVALUATION TEST TARGET (MT-3)





**IMAGE EVALUATION  
TEST TARGET (MT-3)**



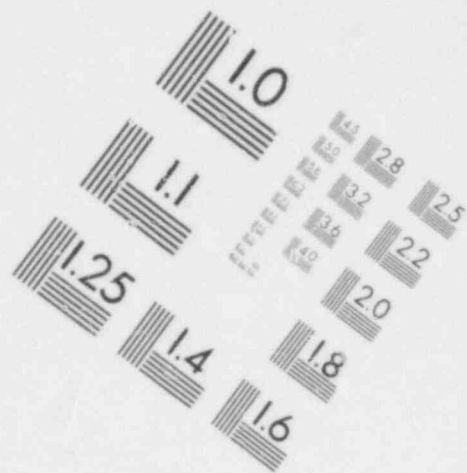
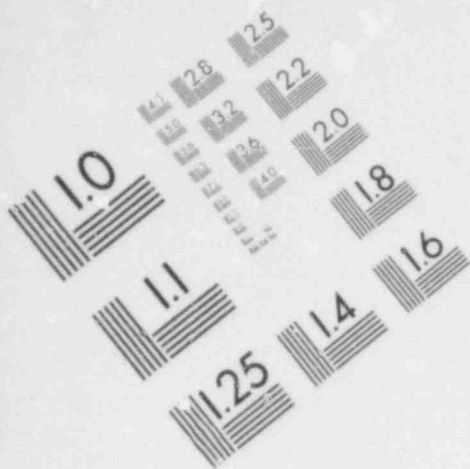
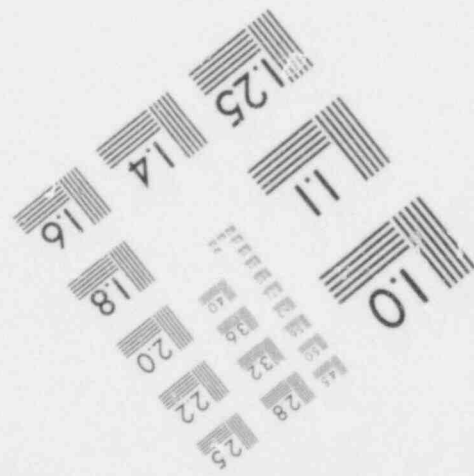
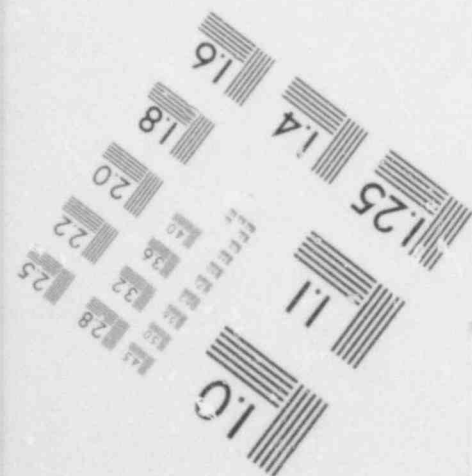
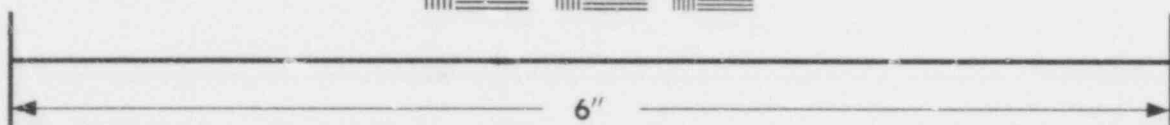
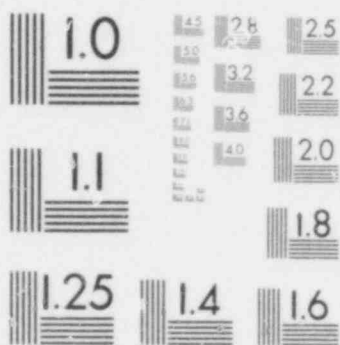


IMAGE EVALUATION  
TEST TARGET (MT-3)





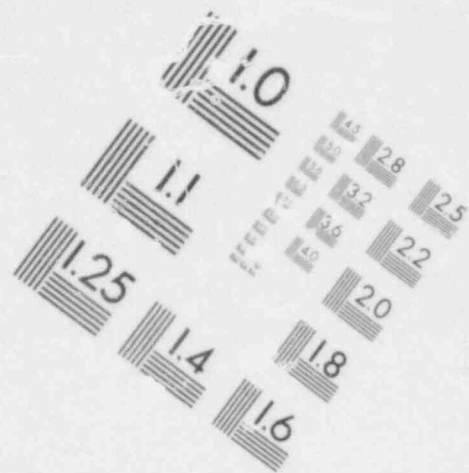
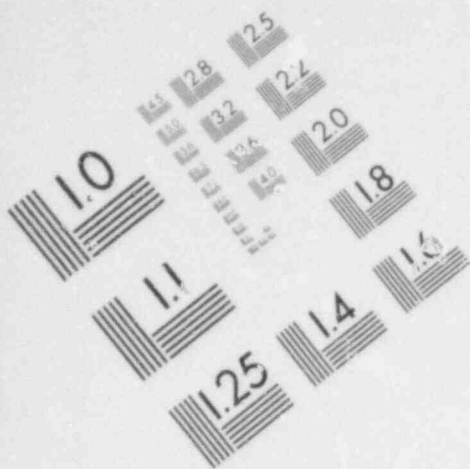
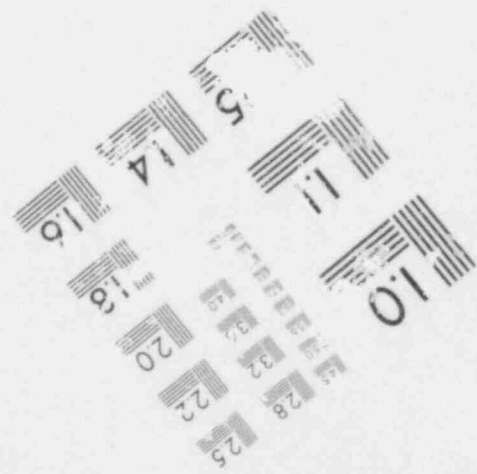
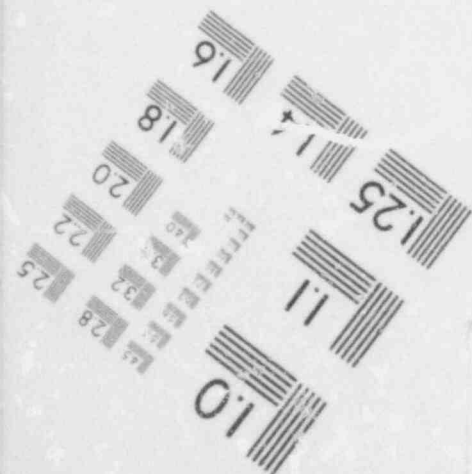
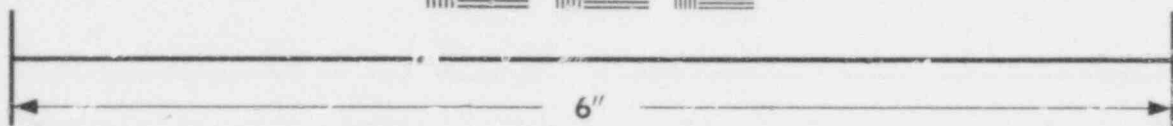


IMAGE EVALUATION  
TEST TARGET (MT-3)



- B. Equations and assumptions for calculating doses from radioiodines and particulates are as follows:

Assumptions

1. Dose is to be calculated for the critical organ, thyroid, and the critical age group, infant.
2. Exposure pathways from iodines and particulates are milk ingestion, ground contamination, and inhalation.
3. The radioiodine and particulate mix is based on the expected source term given in Table 1.1.
4. Basic radionuclide data are given in Table 1.2.
5. Releases are treated as ground-level, split-level, or elevated.
6. Meteorological data are expressed as joint frequency distributions (JFD's) of wind speed, wind direction, and atmospheric stability for the period January 1974 to December 1975 (Table 1.3). Releases from the turbine building are treated as 100 percent ground level, whereas stack releases are considered 100 percent elevated. Releases from the reactor building and rad-waste building are treated as split-level; i.e., partly elevated and partly ground level.
7. Raw meteorological data for ground-level releases consist of wind speed and direction measurements at 10 m and temperature measurements at 10 m and 45 m. The ground-level portion of the split-level JFD was based on wind speeds and directions measured at the 10 m level and temperature measurements at 10 and 45 m. The elevated portion of the split-level JFD was based on wind speeds and directions measured at 46 m and temperature measurements at 45 and 90 m. Wind speeds and directions for elevated releases

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were measured at 93 m. Stability class D was assumed to persist during the entire period for elevated releases.

8. Dose is to be evaluated at the potential offsite exposure point where maximum concentrations are expected to exist.
9. Real cow and garden locations are not considered.
10. Potential maximum-exposure points (Table 1.4) considered are the nearest site boundary points in each sector.
11. Terrain elevations are considered.
12. Building wake effects on effluent dispersion are considered.
13. Plume depletion and radioactive decay are considered for air-concentration calculations.
14. Radioactive decay is considered for ground-concentration calculations.
15. Deposition is calculated based on the curves given in Figure 1.2.
16. A milk cow obtains 100 percent of her food from pasture grass.
17. No credit is taken for shielding by residence.

#### Equations

To calculate the dose from radioactive effluents discharged from a given release point for any one of the potential maximum-exposure points, the following equations are used.

##### 1. Inhalation

Equation for calculating air concentration,  $\chi$ , is the same as in the Noble Gas Section, 1.1.1.A.

For determining the thyroid dose rate:

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$$D_{THI} = 1 \times 10^6 \sum_1 X_1 DFI_1 BR \quad (1.4)$$

where:

$D_{THI}$  = thyroid dose rate due to inhalation,  $\text{mrem/y}$ .

$X_1$  = air concentration of radionuclide i,  $\mu\text{Ci}/\text{m}^3$ .

$DFI_1$  = infant inhalation dose factor,  $\text{mrem/pCi}$  (Table 1.7).

$BR$  = infant breathing rate,  $1,400 \text{ m}^3/\text{y}$ .

$1 \times 10^6$  =  $\text{pCi}/\mu\text{Ci}$  conversion factor.

## 2. Ground Contamination

For determining the ground concentration of any nuclide:

$$G_1 = 3.15 \times 10^7 \sum_{k=1}^7 \frac{f_k Q_1 DR}{(2\pi x/n) \lambda_1} [1 - \exp^{-(\lambda_1 t_b)}] \quad (1.5)$$

where

$G_1$  = ground concentration of radionuclide i,  $\mu\text{Ci}/\text{m}^2$ .

$k$  = stability class.

$f_k$  = joint relative frequency of occurrence of winds in stability class k blowing toward this exposure point, expressed as a fraction.

$Q_1$  = average release rate of radionuclide i,  $\mu\text{Ci}/\text{s}$ .

$DR$  = relative deposition rate  $\text{m}^{-1}$  (Figure 1.2). The choice of

figure is governed by the effective release height

calculated by equation 1.1a. A linear interpolation is used

for effective release heights that fall in between the given curves.

$x$  = downwind distance,  $\text{m}$ .

$n$  = number of sectors, 16.

$2\pi x/n$  = sector width at point of interest,  $\text{m}$ .

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$\lambda_1$  = radioactive decay coefficient of radionuclide 1,  $y^{-1}$ .

$t_b$  = time for buildup of radionuclides on the ground, 35y.

$3.15 \times 10^7$  = s/y conversion factor.

For determining the thyroid dose rate from ground contamination:

$$D_{THG} = (8,760)(1 \times 10^6) \sum_1 G_1 DFG_1 \quad (1.6)$$

where:

$D_{THG}$  = thyroid dose rate due to ground contamination, mrem/y.

$G_1$  = ground concentration of radionuclide 1,  $\mu\text{Ci}/\text{m}^2$ .

$DFG_1$  = dose factor for standing on contaminated ground, mrem/h per  $\mu\text{Ci}/\text{m}^2$  (Table 1.8).

8,760 = occupation time, h/y.

$1 \times 10^6$  = pCi/ $\mu\text{Ci}$  conversion factor

### 3. Milk Ingestion

For determining the concentration of any nuclide (except C-14 and H-3) in and on vegetation:

$$CV_i = 3,600 \sum_{k=1}^7 \frac{f_k Q_i DR}{(2\pi x/n)} \left[ \frac{r[1 - \exp(-\lambda_{Ei} t_e)]}{Y_v \lambda_{Ei}} + \frac{B_{iv} [1 - \exp(-\lambda_i t_b)]}{P \lambda_i} \right] \quad (1.7)$$

where:

$CV_i$  = concentration of radionuclide i in and on vegetation,  $\mu\text{Ci}/\text{kg}$ .

$k$  = stability class.

$f_k$  = frequency of this stability class and wind direction combination, expressed as a fraction.

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$Q_1$  = average release rate of radionuclide 1,  $\mu\text{Ci/s}$ .

DR = relative deposition rate,  $\text{m}^{-1}$  (Figure 1.2. The

choice of figure is governed by the effective release

height calculated by equation 1.1a. A linear interpolation

is used for effective release heights that fall in between

the given curves.

$x$  = downwind distance, m.

$n$  = number of sectors, 16.

$2\pi x/n$  = sector width at point of interest, m.

$r$  = fraction of deposited activity retained on vegetation (1.0 for iodines, 0.2 for particulates).

$\lambda_{Ei}$  = effective removal rate constant,  $\lambda_{Ei} = \lambda_i + \lambda_w$ , where  $\lambda_i$  is the radioactive decay coefficient,  $\text{h}^{-1}$ , and  $\lambda_w$  is a measure of physical loss by weathering ( $\lambda_w = .0021 \text{ h}^{-1}$ ),  $\text{h}^{-1}$ .

$t_e$  = period over which deposition occurs, 720 h.

$Y_v$  = agricultural yield,  $0.7 \text{ kg/m}^2$ .

$B_{iv}$  = transfer factor from soil to vegetation of radionuclide  $i$  (Table 1.6).

$\lambda_i$  = radioactive decay coefficient of radionuclide  $i$ ,  $\text{h}^{-1}$ .

$t_b$  = time for buildup of radionuclides on the ground,  $3.07 \times 10^5$  h (35y).

$P$  = effective surface density of soil,  $240 \text{ kg/m}^2$ .

3,600 = s/h conversion factor.

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For determining the concentration of C-14 in vegetation:

$$CV_{14} = 1 \times 10^3 X_{14} (0.11/0.16) \quad (1.8)$$

where

$CV_{14}$  = concentration of C-14 in vegetation,  $\mu\text{Ci/kg}$ .

$X_{14}$  = air concentration of C-14,  $\mu\text{Ci/m}^3$ .

0.11 = fraction of total plant mass that is natural carbon.

0.16 = concentration of natural carbon in the atmosphere,  
 $\text{g/m}^3$ .

$1 \times 10^3$  = g/kg conversion factor.

For determining the concentration of H-3 in vegetation:

$$CV_T = 1 \times 10^3 X_T (0.75)(0.5/H) \quad (1.9)$$

where

$CV_T$  = concentration of H-3 in vegetation,  $\mu\text{Ci/kg}$ .

$X_T$  = air concentration of H-3,  $\mu\text{Ci/m}^3$ .

0.75 = fraction of total plant mass that is water.

0.5 = ratio of tritium concentration in plant water to tritium  
concentration in atmospheric water.

$H$  = absolute humidity of the atmosphere,  $\text{g/m}^3$ .

$1 \times 10^3$  = g/kg conversion factor.

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For determining the concentration of any nuclide in cow's milk:

$$CM_1 = CV_1 FM_1 Q_f \exp(-\lambda_1 t_f) \quad (1.10)$$

where

$CM_1$  = concentration of radionuclide 1 (including C-14 and H-3) in cow's milk,  $\mu\text{Ci/l}$ .

$CV_1$  = concentration of radionuclide 1 in and on vegetation,  $\mu\text{Ci/kg}$ .

$FM_1$  = transfer factor from feed to milk for radionuclide 1,  $\text{d/l}$ .

$Q_f$  = amount of feed consumed by the cow per day,  $\text{kg/d}$ .

$\lambda_1$  = radioactive decay coefficient of radionuclide 1,  $\text{d}^{-1}$ .

$t_f$  = transport time of activity from feed to milk to receptor, 2 days.

For determining the thyroid dose rate from ingestion of cow's milk:

$$D_{THM} = 1 \times 10^6 \sum_1 CM_1 DFING_1 UM \quad (1.11)$$

where

$D_{THM}$  = thyroid dose rate due to milk ingestion,  $\text{mrem/y}$ .

$CM_1$  = concentration of radionuclide 1 in cow's milk,  $\mu\text{Ci/l}$ .

$DFING_1$  = infant ingestion dose factor from Reg. Guide 1.109 (Rev. 1),  $\text{mrem/pCi}$  (Table 1.7)

$UM$  = infant ingestion rate for milk, 330  $\text{l/y}$ .

$1 \times 10^6$  =  $\text{pCi}/\mu\text{Ci}$  conversion factor.

#### 4. Total Thyroid Dose Rate

For determining the total thyroid dose rate from iodines and particulates:

$$D_{TH} = D_{THI} + D_{THG} + D_{THM} \quad (1.12)$$

where

$D_{TH}$  = total thyroid dose rate,  $\text{mrem/y}$ .

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$D_{THI}$  = thyroid dose rate due to inhalation, mrem/y.

$D_{THG}$  = thyroid dose rate due to ground contamination, mrem/y.

$D_{THM}$  = thyroid dose rate due to milk ingestion, mrem/y.

The above dose calculations are repeated for each release point and then summed to obtain thyroid dose rates. The maximum thyroid dose rate will then be used in step 2.

#### Step 2

The dose rate limits of interest (10CFR20) are

Total Body = 500 mrem/y

Skin = 3,000 mrem/y

Maximum Organ = 1,500 mrem/y

Dividing the above limits by the appropriate dose calculated in step 1 yields a useful ratio.

$$\frac{\text{Dose limit.}}{\text{Dose step 1}} = R$$

This ratio, R, represents how far above or below the guidelines the step 1 calculation was. Multiplying the original source terms by R will give release rates that should correspond to the dose limits given above.

Release rate limits in  $\mu\text{Ci/s}$  for each nuclide and release point are now available.

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## 1.2 Monthly Dose Calculations

Dose calculations will be performed monthly to determine compliance with specifications 3.8.B.3 and 3.8.B.5. These specifications require that the dose rate in unrestricted areas due to gaseous effluents from each reactor at the site shall be limited to the following values:

For noble gases,

1. During any calendar quarter, 5 mrad to air for gamma radiation and 10 mrad to air for beta radiation.
2. During any calendar year, 10 mrad to air for gamma radiation and 20 mrad to air for beta radiation.

For iodines and particulates,

1. During any calendar quarter, 7.5 mrem to any organ.
2. During any calendar year, 15 mrem to any organ.

This section of the ODCM describes the methodology that will be used to perform these monthly calculations.

Doses will first be calculated by a simplified conservative approach (step 1). If these exceed the specification limits, a more realistic calculation will be performed (step 2).

### 1.2.1 Noble Gases

#### Step 1

Doses will be calculated using the methodology described in this step. If any limits are exceeded, step 2 will be performed.

Equations and assumptions for calculating doses from releases of noble gases are as follows:

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### Assumptions

1. Doses to be calculated are gamma and beta air doses.
2. The highest annual-average  $\chi/Q$  based on licensing meteorology for ground-level releases for any offsite location will be used
3. No credit is taken for radioactive decay.
4. For gamma doses, releases of Xe-133, Xe-138, Kr-85m, and Kr-88 are considered.
5. For beta doses, releases of Xe-133, Xe-138, Kr-85m, and Kr-88 are considered.
6. Dose factors are calculated using data from TVA's nuclide library.
7. The nuclides considered are expected to contribute at least 90 percent of the total dose. However, the calculations extrapolate doses assuming that only 90 percent of total dose was contributed.
8. A semi-infinite cloud model is used.
9. Building wake effects on effluent dispersion are considered.

### Equations

For determining the gamma dose to air:

$$D_Y = \frac{(\chi/Q)}{0.9} \sum_i Q_i DFY_i \quad (1.13)$$

where:

$D_Y$  = gamma dose to air from continuous releases, mrad.

$\chi/Q$  = highest annual-average relative concentration,  $2.26 \times 10^{-6}$  s/m<sup>3</sup>

0.9 = fraction of total gamma dose expected to be contributed by these nuclides (actually 0.94).

$Q_i$  = monthly release of radionuclide i, Ci.

$DFY_i$  = gamma-to-air dose factor for radionuclide i, mrad/s per Ci/m<sup>3</sup>

(Table 1.5).

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This equation then reduces to

$$D_Y = 2.51 \times 10^{-6} \sum_1 Q_1 \text{EFY}_1 \quad (1.14)$$

For determining the beta dose to air:

$$D_\beta = \frac{(\chi/Q)}{0.9} \sum_1 Q_1 \text{DFB}_1 \quad (1.15)$$

where:

$D_\beta$  = beta dose to air, mrad.

$\chi/Q$  = highest annual-average relative concentration,  $2.26 \times 10^{-6}$  s/m<sup>3</sup>.

0.9 = fraction of total beta dose expected to be contributed by these nuclides (actually 0.90).

$Q_1$  = monthly release of radionuclide i, Ci.

$\text{DFB}_1$  = beta-to-air dose factor for radionuclide i, mrad/s per Ci/m<sup>3</sup> (Table 1.5).

This equation then reduces to:

$$D_\beta = 2.51 \times 10^{-6} \sum_1 Q_1 \text{DFB}_1 \quad (1.16)$$

## Step 2

This methodology is to be used if the calculations in Step 1 yield doses that exceed applicable limits.

Equations and assumptions for calculating doses to air from releases of noble gases are as follows:

Assumptions

1. Doses to be calculated are gamma and beta air doses.
2. Dose is to be evaluated at the nearest site boundary point in each sector.
3. Historical onsite meteorological data for the appropriate months from the period 1974-1975 will be used.
4. All measured radionuclide releases are considered.
5. A semi-infinite cloud model is used.
6. Radioactive decay is considered.
7. Building wake effects on effluent dispersion are considered.
8. Dose factors are calculated using data from TVA's radionuclide library.

Equations

Equation for calculating air concentration,  $\chi$ , is the same as in Section 1.1.1, step 1, part A. Air concentrations are calculated for the site boundary in each sector.

For determining the gamma dose to air

$$D_{\gamma n} = t_m \sum_1 \chi_{ni} DF_{\gamma i} \quad (1.24)$$

where:

$D_{\gamma n}$  = gamma dose to air for sector n, mrad.

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$X_{ni}$  = air concentration of radionuclide  $i$  in sector  $n$ ,  
 $Ci/m^3$ .

$DFY_i$  = gamma-to-air dose factor for radionuclide  $i$ , mrad/s per  
 $Ci/m^3$  (Table 1.5).

$t_n$  = time period considered (1 month, but number of s/mo is  
variable), s.

- For determining the beta dose to air:

$$D_{\beta n} = t_n \sum_i X_{ni} DF\beta_i \quad (1.25)$$

where:

$D_{\beta n}$  = beta dose to air for sector  $n$ , mrad.

$X_{ni}$  = air concentration of radionuclide  $i$  in sector  $n$ ,  $Ci/m^3$ .

$DF\beta_i$  = beta to air dose factor for radionuclide  $i$ , mrad/s per  
 $Ci/m^3$ .

$t_n$  = time period considered (number of seconds in this month),  
s.

The sector having the highest total dose is then used to check  
compliance with specification 3.8.3.3.

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### 1.2.2 Iodines and Particulates

#### Step 1

Doses will be calculated using the methodology described in this step. If any limits are exceeded, step 2 will be performed.

Equations and assumptions for calculating doses from releases of iodines and particulates are as follows:

#### - Assumptions

1. Dose is to be calculated for the critical organ, thyroid, and the critical age group, infant.
2. Exposure pathway considered is milk ingestion.
3. The highest annual-average D/Q based on licensing meteorology for ground-level releases for any real cow location will be used for I-131 and I-133 doses.
4. The highest annual-average  $\chi/Q$  based on licensing meteorology for ground-level releases for any cow location will be used for C-14 doses.
5. No credit is taken for radioactive decay.
6. Releases of I-131, I-133, and C-14 are considered.
7. The radionuclides considered are expected to contribute at least 99 percent of the total dose. However, the calculations

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extrapolate doses assuming that only 90 percent of the total dose was contributed.

8. Releases of C-14 are based on the expected source term.
9. The cow is assumed to graze on pasture grass for the whole year.

#### Equations

For determining the thyroid dose from milk ingestion of I-131 or I-133:

$$DTH_{131(133)} = \frac{Q_{131(133)} DF_{131(133)} D/Q}{3.15 \times 10^7} \quad (1.26)$$

where:

$DTH_{131(133)}$  = thyroid dose from I-131(I-133), mrem.

$Q_{131(133)}$  = monthly release of I-131(133), Ci.

$DF_{131(133)}$  = I-131(133) milk ingestion dose factor to infant, mrem/y per Ci/m<sup>2</sup>-s.

$D/Q$  = relative deposition rate,  $5.66 \times 10^{-9} \text{ m}^{-2}$ .

$3.15 \times 10^7$  = s/y.

For determining the thyroid dose from milk ingestion of C-14:

$$DTH_{14} = \frac{Q_{14} DF_{14} X/Q}{3.15 \times 10^7} \quad (1.27)$$

where:

$DTH_{14}$  = thyroid dose from C-14, mrem.

$Q_{14}$  = monthly release of radionuclide i, Ci.

$DF_{14}$  = C-14 milk ingestion dose factor, mrem/y per Ci/m<sup>3</sup>.

$X/Q$  = relative dispersion factor,  $2.26 \times 10^{-6} \text{ s/m}^3$ .

$3.15 \times 10^7$  = s/y.

For determining the total thyroid dose from releases:

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$$DTH = \frac{DTH_{131} + DTH_{133} + DTH_{14}}{0.9} \quad (1.28)$$

where:

DTH = thyroid dose, mrem.

$DTH_{131}$  = thyroid dose from release of I-131, mrem.

$DTH_{133}$  = thyroid dose from release of I-133, mrem.

$DTH_{14}$  = thyroid dose from release of C-14, mrem.

0.9 = fraction of total thyroid dose expected to be contributed by these radionuclides (actually 0.99).

## Step 2

This methodology is to be used if the calculations in step 1 yield doses that exceed applicable limits.

Doses for releases of iodines and particulates shall be calculated using the methodology in Section 1.1.1, step 1, part B, with the following exceptions:

1. All measured radionuclide releases will be used.
2. Dose will be evaluated at real cow locations and will consider actual grazing information.

The receptor having the highest total dose is then used to check compliance with specification 3.8.B.5.

## 1.3 Gaseous Radwaste Treatment System Operation

The gaseous radwaste treatment system (GRTS) described below shall be maintained and operated to keep releases ALARA.

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#### 1.3.1 System Description

A flow diagram for the GRTS is given in Figure 1. . . The system includes the subsystems that process and dispose of the gases from the main condenser air ejectors, the startup vacuum pumps, and the gland seal condensers. One gaseous radwaste treatment system is provided for each unit. The processed gases from each unit are routed to the plant stack for dilution and elevated release to the atmosphere. The air ejector off-gas line of each unit and the stack are continuously monitored by radiation monitors.

#### 1.3.2 Dose Calculations

Doses will be calculated monthly using the methodology described in Section 1.2. These doses will be used to ensure that the GRTS is operating as designed.

TABLE 1.1  
EXPECTED ANNUAL ROUTINE ATMOSPHERIC RELEASES FROM ONE UNIT AT BROWNS FERRY

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ISOTOPE	NUCLEAR PLANT (Ci/y/unit)				STACK	MVP
	REACTOR COMPLEX VENT	RADWASTE BUILDING VENT	TURBINE BUILDING VENTS	GLAND SEAL AND OFFGAS		
Kr-85m	6	<1	2	1.10 E4	0	
Kr-87	6	<1	95	873	0	
Kr-88	9	<1	102	1.22 E4	0	
Kr-89	1	34	503	0	0	
Xe-133m	0	60	0	633	0	
Xe-133	103	294	581	5.40 E4	300	
Xe-135m	111	667	464	1212	0	
Xe-135	173	328	672	868	200	
Xe-137	78	113	386	0	0	
Xe-138	12	2	1179	1483	0	
I-131 I	0.0594	0.0050	0.0156	0.0041	0.0085	
I-132 I	0.594	0.050	0.1786	0.0469	0.0973	
I-133 I	0.297	0.025	0.1231	0.0323	0.0671	
I-134 I	1.485	0.125	0.0267	0.0070	0.0145	
I-135 I	0.594	0.050	0.1231	0.0323	0.0671	
I-131 O	0.0316	0.029	0.0065	0.0332	0.2741	
I-132 O	0.316	0.290	0.0744	0.3801	3.1384	
I-133 O	0.158	0.145	0.0513	0.2619	2.1626	
I-134 O	0.790	0.725	0.0111	0.0568	0.4687	
I-135 O	0.316	0.290	0.0513	0.2619	2.1626	
Cr 51	3 E-3	9 E-4	1 E-3	1 E-4	0	
Mn 54	3 E-3	5 E-3	2 E-3	4 E-5	0	
Co 58	2 E-3	4 E-4	9 E-5	2 E-5	0	
Fe 59	1 E-4	8 E-4	4 E-4	2 E-4	0	
Co 60	3 E-2	6 E-3	3 E-3	1 E-5	0	
Zn 65	3 E-3	2 E-4	4 E-4	9 E-5	0	
Sr 89	1 E-2	3 E-1	*	*	0	
Sr 90	2 E-3	4 E-3	*	*	0	
Nb 95	3 E-4	2 E-4	9 E-6	8 E-5	0	
Zr 95	1 E-4	1 E-4	8 E-6	8 E-5	0	
Ru 103	3 E-5	1 E-4	2 E-4	1 E-4	0	
Ag 110m	7 E-6	*	*	*	0	
Sb 124	3 E-5	3 E-4	6 E-5	8 E-5	0	
Cs 134	5 E-3	3 E-4	5 E-4	2 E-5	0	
Cs 136	2 E-3	5 E-5	1 E-4	9 E-8	0	
Cs 137	7 E-3	4 E-4	2 E-3	7 E-4	0	
Ba 140	4 E-3	5 E-4	2 E-2	8 E-3	0	
Ce 141	4 E-4	2 E-4	2 E-3	2 E-5	0	
Ce 144	5 E-6	*	*	4 E-6	0	
Ar-41	25	0	0	0	0	
C-14	0	0	0	9.5	0	
H-3	0	9.5	0	0	0	

\*Not available

I denotes nonorganic iodine (elemental, particulate, HIO)  
O denotes organic iodine

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TABLE 1.2 BASIC RADIONUCLIDE DATA

NUCLIDE	HALF-LIFE (DAYS)	LAMDA (1/S)	T	C	BETA (MEV/DIS)	GAMMA (MEV/DIS)	WASH (1/S)
1 TRITIUM	101	4.49E-03	1.79E-09	2	1	5.68E-03	0.0
2 C-14	674	2.04E-06	3.84E-12	2	1	5.17E-02	0.0
3 N-13	732	6.94E-03	1.16E-03	2	1	4.91E-01	1.02E-00
4 O-19	834	3.36E-04	2.39E-02	2	1	1.02E-00	1.05E-00
5 F-18	932	7.62E-02	1.05E-04	2	1	2.41E-01	9.88E-01
6 NA-24	1704	6.33E-01	1.27E-05	5	1	5.55E-01	4.12E-00
7 P-32	1504	1.43E-01	5.61E-07	5	1	6.95E-01	0.0
8 AR-41	1805	7.63E-02	1.05E-04	2	1	3.63E-01	1.28E-00
9 CR-51	2405	2.78E-01	2.89E-07	5	1	3.75E-03	3.28E-02
10 MN-54	2508	3.03E-02	2.65E-08	5	1	4.17E-03	8.36E-01
11 MH-56	2509	1.07E-01	7.50E-05	5	1	7.93E-01	1.76E-00
12 FE-59	2604	4.50E-01	1.78E-07	5	1	1.18E-01	1.19E-00
13 CO-58	2706	7.13E-01	1.12E-07	5	1	2.05E-01	9.76E-01
14 CO-60	2708	1.92E-03	4.18E-09	5	1	9.08E-02	2.50E-00
15 ZA-69M	3007	5.75E-01	1.39E-05	5	1	0.0	4.15E-00
16 ZA-69	3006	3.96E-02	2.03E-04	5	1	3.19E-01	0.0
17 BR-84	3516	2.21E-02	3.63E-04	2	1	1.26E-00	1.68E-00
18 BR-85	3518	2.08E-03	3.86E-03	2	2	1.04E-00	8.40E-01
19 KR-85M	3611	1.83E-01	4.38E-05	1	2	2.53E-01	1.54E-01
20 KR-85	3610	3.93E-03	2.04E-09	1	1	2.51E-01	2.21E-03
21 KR-87	3612	5.28E-02	1.52E-04	1	1	1.32E-00	7.93E-01
22 KR-88	3613	1.17E-01	6.86E-05	1	1	3.75E-01	1.96E-00
23 KR-89	3614	2.21E-03	3.63E-03	1	1	1.23E-00	2.08E-00
24 RB-88	3713	1.24E-02	6.47E-04	5	1	2.06E-00	6.86E-01
25 RB-89	3714	1.07E-02	7.50E-04	5	1	0.0	2.40E-00
26 SR-89	3808	5.20E-01	1.54E-07	5	1	5.73E-01	1.36E-04
27 SR-90	3810	1.03E-04	7.79E-10	5	1	1.96E-01	0.0
28 SR-91	3811	4.03E-01	1.99E-05	5	2	6.50E-01	6.95E-01
29 SR-92	3812	1.13E-01	7.10E-05	5	1	1.45E-01	1.34E-00
30 SR-93	3813	5.56E-03	1.44E-03	5	1	1.61E-00	6.26E-01
31 Y-90	3916	2.67E-00	3.00E-06	5	1	9.36E-01	0.0
32 Y-91M	3919	3.47E-02	2.31E-04	5	1	0.0	5.56E-01
33 Y-91	3918	5.88E-01	1.36E-07	5	1	6.06E-01	3.61E-03
34 Y-92	3920	1.47E-01	5.46E-05	5	1	1.44E-00	2.50E-01
35 Y-93	3921	4.29E-01	1.87E-05	5	1	1.17E-00	8.94E-02
36 ZR-95	4014	6.50E-01	1.23E-07	5	2	1.20E-01	7.35E-01
37 NB-95M	4115	3.75E-00	2.14E-06	5	1	2.85E-01	5.47E-02
38 NB-95	4114	3.50E-01	2.29E-07	5	1	4.50E-02	7.64E-01
39 MO-99	4209	2.79E-00	2.87E-06	5	2	3.96E-01	1.62E-01
40 TC-99M	4314	2.50E-01	3.21E-05	5	1	4.65E-03	1.43E-01
41 TC-99	4313	7.74E-07	1.04E-13	5	1	8.38E-02	0.0
42 TC-104	4320	1.25E-02	6.42E-04	5	1	0.0	0.0
43 RU-106	4407	3.67E-02	2.19E-08	5	1	1.01E-02	0.0
44 TE-132	5223	3.24E-00	2.48E-06	5	1	1.00E-01	2.05E-01
45 I-129	5315	6.21E-09	1.29E-15	3	1	4.02E-02	3.77E-03
46 I-131	5317	8.05E-00	9.96E-07	3	2	1.94E-01	3.81E-01
47 MI-131	15317	8.05E-00	9.96E-07	4	2	1.94E-01	3.81E-01
48 I-132	5318	9.58E-02	8.37E-05	3	1	5.14E-01	2.33E-00
49 MI-132	15318	9.58E-02	8.37E-05	4	1	5.14E-01	2.33E-00
50 I-133	5319	8.75E-01	9.17E-06	3	2	4.08E-01	6.10E-01
51 MI-133	15319	8.75E-01	9.17E-06	4	2	4.08E-01	6.10E-01
52 I-134	5320	3.61E-02	2.22E-04	3	1	6.10E-01	2.54E-00
53 MI-134	15320	3.61E-02	2.22E-04	4	1	6.10E-01	2.54E-00
54 I-135	5321	2.79E-01	2.87E-05	3	2	3.68E-01	1.58E-00
55 MI-135	15321	2.79E-01	2.87E-05	4	2	3.68E-01	1.58E-00
56 XE-131M	5412	1.18E-01	6.80E-07	1	1	1.43E-01	2.01E-02
57 XE-133M	5414	2.26E-00	3.55E-06	1	1	1.90E-01	4.16E-02
58 XE-133	5413	5.27E-00	1.52E-06	1	1	1.35E-01	4.54E-02
59 XE-135M	5416	1.08E-02	7.43E-04	1	1	9.50E-02	4.32E-01
60 XE-135	5415	3.82E-01	2.09E-05	1	1	3.17E-01	2.47E-01
61 XE-137	5417	2.71E-03	2.96E-03	1	1	1.64E-00	1.94E-01
62 XE-138	5418	1.18E-02	6.80E-04	1	1	6.06E-01	1.18E-00
63 CS-134	5510	7.48E-02	1.07E-08	5	1	1.57E-01	1.04E-00
64 CS-135	5512	1.10E-09	7.29E-15	5	1	5.74E-02	0.0
65 CS-136	5514	1.30E-01	6.17E-07	5	1	1.01E-01	2.20E-00
66 CS-137	5515	1.10E-04	7.29E-10	5	1	2.52E-01	5.97E-01
67 CS-138	5516	2.24E-02	3.58E-04	5	1	1.23E-00	2.30E-00
68 BA-139	5615	5.76E-02	1.34E-04	5	1	6.54E-01	5.05E-02
69 BA-140	5616	1.28E-01	6.27E-07	5	1	3.15E-01	1.95E-01
70 LA-140	5715	1.68E-00	4.77E-06	5	1	5.40E-01	2.31E-00
71 CE-144	5815	2.84E-02	2.82E-08	5	1	4.13E-02	3.24E-02
72 PR-143	5912	1.36E-01	5.90E-07	5	1	3.14E-01	0.0
73 PR-144	5913	1.20E-02	6.68E-04	5	1	1.23E-00	3.10E-02
74 NP-239	9310	2.35E-00	3.41E-06	5	1	1.24E-01	2.08E-00

POOR ORIGINAL

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Table 1.3

JOINT PERCENTAGE FREQUENCIES OF WIND DIRECTION AND WIND SPEED  
- FOR DIFFERENT STABILITY CLASSES -

STABILITY CLASS A  
DELTA T = -1.9 DEG. C/100M

BROWNS FERRY NUCLEAR PLANT METEOROLOGICAL FACILITY

JAN 1, 74 - DEC 31, 75

WIND DIRECTION	WIND SPEED (MPH)										TOTAL
	0.0-1.4	1.5-3.4	3.5-5.4	5.5-7.4	7.5-12.4	12.5-18.4	18.5-24.4	24.5-30.4	30.5-36.4	36.5-42.4	
N	0.0	0.0	0.11	0.17	0.20	0.04	0.0	0.0	0.0	0.0	0.52
NNE	0.0	0.04	0.13	0.15	0.25	0.04	0.0	0.0	0.0	0.0	0.61
NE	0.0	0.04	0.10	0.07	0.02	0.0	0.0	0.0	0.0	0.0	0.23
ENE	0.0	0.01	0.04	0.02	0.0	0.0	0.0	0.0	0.0	0.0	0.07
E	0.0	0.01	0.03	0.02	0.0	0.0	0.0	0.0	0.0	0.0	0.06
ESE	0.0	0.05	0.19	0.14	0.05	0.0	0.0	0.0	0.0	0.0	0.43
SE	0.0	0.26	1.35	0.38	0.10	0.0	0.0	0.0	0.0	0.0	2.09
SSE	0.0	0.23	0.80	0.09	0.02	0.0	0.0	0.0	0.0	0.0	1.14
S	0.01	0.15	0.50	0.12	0.02	0.0	0.0	0.0	0.0	0.0	0.80
SSW	0.0	0.02	0.07	0.01	0.01	0.0	0.0	0.0	0.0	0.0	0.11
SW	0.0	0.02	0.10	0.01	0.01	0.0	0.0	0.0	0.0	0.0	0.14
WSW	0.0	0.02	0.13	0.09	0.05	0.0	0.0	0.0	0.0	0.0	0.29
W	0.0	0.01	0.06	0.06	0.04	0.0	0.01	0.0	0.0	0.0	0.18
WNW	0.0	0.02	0.04	0.12	0.18	0.07	0.01	0.0	0.0	0.0	0.46
NW	0.0	0.0	0.02	0.12	0.26	0.14	0.01	0.0	0.0	0.0	0.55
NNW	0.0	0.0	0.02	0.03	0.09	0.12	0.0	0.0	0.0	0.0	0.26
SURTOTAL	0.01	0.88	3.71	1.60	1.30	0.41	0.03	0.0	0.0	0.0	7.94
CALM =	0.01										

1337 STABILITY CLASS A OCCURRENCES OUT OF TOTAL 1659 VALID TEMPERATURE DIFFERENCE READINGS

1296 VALID WIND DIRECTION - WIND SPEED READINGS OUT OF TOTAL 1337 STABILITY CLASS A OCCURRENCES

ALL COLUMNS AND CALM TOTAL 100 PERCENT OF ALL VALID READINGS

METEOROLOGICAL FACILITY LOCATED 0.78 MILES ESE OF BROWNS FERRY NUCLEAR PLANT  
TEMPERATURE INSTRUMENTS 33 AND 150 FEET ABOVE GROUND  
RADWASTE BUILDING-GROUND LEVEL RELEASE 33 FEET WIND INFORMATION.

POOR ORIGINAL

Table 1.3 (Continued)

JOINT PERCENTAGE FREQUENCIES OF WIND DIRECTION AND WIND SPEED  
FOR DIFFERENT STABILITY CLASSES

STABILITY CLASS B

-1.7 < DELTA-T < -1.7 DEG. C/100M

BROWNS FERRY NUCLEAR PLANT METEOROLOGICAL FACILITY\*

JAN 1, 74 - DEC 31, 75

WIND DIRECTION	WIND SPEED (MPH)										TOTAL
	0.5-1.4	1.5-3.4	3.5-5.4	5.5-7.4	7.5-12.4	12.5-18.4	18.5-24.4	24.5-30.4	30.5-36.4	36.5-42.4	
N	0.0	0.03	0.15	0.11	0.23	0.02	0.0	0.0	0.0	0.0	0.54
NNE	0.0	0.06	0.12	0.12	0.16	0.01	0.0	0.0	0.0	0.0	0.47
NE	0.0	0.03	0.1	0.06	0.01	0.0	0.0	0.0	0.0	0.0	0.17
ENE	0.0	0.02	0.04	0.01	0.01	0.0	0.0	0.0	0.0	0.0	0.08
E	0.0	0.03	0.02	0.03	0.0	0.0	0.0	0.0	0.0	0.0	0.08
ESE	0.0	0.07	0.06	0.04	0.01	0.0	0.0	0.0	0.0	0.0	0.18
SE	0.0	0.35	0.53	0.08	0.04	0.0	0.0	0.0	0.0	0.0	1.00
SSE	0.01	0.26	0.23	0.02	0.01	0.0	0.0	0.0	0.0	0.0	0.53
S	0.0	0.13	0.31	0.05	0.01	0.0	0.0	0.0	0.0	0.0	0.50
SSW	0.0	0.04	0.07	0.03	0.0	0.0	0.0	0.0	0.0	0.0	0.14
SW	0.0	0.07	0.11	0.01	0.01	0.0	0.0	0.0	0.0	0.0	0.20
WSW	0.0	0.04	0.24	0.07	0.09	0.01	0.0	0.0	0.0	0.0	0.45
W	0.0	0.01	0.12	0.12	0.09	0.02	0.01	0.0	0.0	0.0	0.37
WNW	0.0	0.02	0.13	0.20	0.33	0.09	0.02	0.0	0.0	0.0	0.79
NW	0.0	0.01	0.11	0.15	0.40	0.10	0.01	0.0	0.0	0.0	0.78
NNW	0.0	0.01	0.03	0.12	0.34	0.11	0.01	0.0	0.0	0.0	0.62
SURTOTAL	0.01	1.18	2.34	1.22	1.74	0.36	0.05	0.0	0.0	0.0	6.90
CALM =	0.0										

1147 STABILITY CLASS B OCCURRENCES OUT OF TOTAL 16559 VALID TEMPERATURE DIFFERENCE READINGS

1119 VALID WIND DIRECTION - WIND SPEED READINGS OUT OF TOTAL 1147 STABILITY CLASS B OCCURRENCES

ALL COLUMNS AND CALM TOTAL 100 PERCENT OF NET VALID READINGS

\*METEOROLOGICAL FACILITY LOCATED 0.78 MILES ESE OF BROWNS FERRY NUCLEAR PLANT  
TEMPERATURE INSTRUMENTS 33 AND 150 FEET ABOVE GROUND  
RAHWASTE BUILDING-GROUND LEVEL RELEASE 33 FEET WIND INFORMATION.

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Table 1.3 (Continued)

JOINT PERCENTAGE FREQUENCIES OF WIND DIRECTION AND WIND SPEED  
FOR DIFFERENT STABILITY CLASSES

STABILITY CLASS C  
-1.7 < DELTA-T < -1.5 DEG. C/100M

BROWNS FERRY NUCLEAR PLANT METEOROLOGICAL FACILITY\*

JAN 1, 74 - DEC 31, 75

WIND DIRECTION	WIND SPEED (MPH)								TOTAL
	0.5-1.4	1.5-3.4	3.5-5.4	5.5-7.4	7.5-12.4	12.5-18.4	18.5-24.4	25-24.5	
N	0.0	0.02	0.08	0.09	0.17	0.04	0.0	0.0	0.40
NNE	0.0	0.04	0.07	0.07	0.07	0.02	0.0	0.0	0.26
NE	0.0	0.03	0.04	0.01	0.0	0.0	0.0	0.0	0.08
ENE	0.0	0.01	0.03	0.01	0.0	0.0	0.0	0.0	0.05
E	0.0	0.01	0.04	0.01	0.0	0.0	0.0	0.0	0.06
ESE	0.0	0.04	0.10	0.06	0.01	0.0	0.0	0.0	0.21
SE	0.0	0.28	0.21	0.05	0.02	0.0	0.0	0.0	0.56
SSE	0.0	0.12	0.12	0.01	0.0	0.0	0.0	0.0	0.34
S	0.0	0.15	0.12	0.01	0.0	0.0	0.0	0.0	0.28
SSW	0.0	0.02	0.04	0.01	0.0	0.0	0.0	0.0	0.07
SW	0.0	0.02	0.07	0.0	0.01	0.0	0.0	0.0	0.10
WSW	0.0	0.02	0.10	0.06	0.02	0.0	0.0	0.0	0.20
W	0.0	0.0	0.14	0.09	0.07	0.06	0.0	0.0	0.36
WNW	0.0	0.05	0.11	0.13	0.12	0.08	0.04	0.0	0.53
NW	0.0	0.01	0.09	0.07	0.23	0.08	0.01	0.0	0.49
NNW	0.0	0.02	0.06	0.10	0.27	0.15	0.01	0.0	0.61
SUBTOTAL	0.0	0.93	1.42	0.77	0.99	0.43	0.06	0.0	4.60
CALM =	0.0								

757 STABILITY CLASS C OCCURRENCES OUT OF TOTAL 16559 VALID TEMPERATURE DIFFERENCE READINGS

739 VALID WIND DIRECTION - WIND SPEED READINGS OUT OF TOTAL 757 STABILITY CLASS C OCCURRENCES

ALL COLUMNS AND CALM TOTAL 1.0 PERCENT OF NET VALID READINGS

\*METEOROLOGICAL FACILITY LOCATED 0.78 MILES ESE OF BROWNS FERRY NUCLEAR PLANT  
TEMPERATURE INSTRUMENTS 33 AND 150 FEET ABOVE GROUND  
RADWASTE BUILDING-GROUND LEVEL RELEASE 33 FEET WIND INFORMATION.

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302 022



Table 1.3 (Continued)

WIND DIRECTION - FREQUENCIES OF WIND DIRECTION AND WIND SPEED  
- BY DIFFERENT STABILITY CLASSES

STABILITY CLASS D

-1.5x DELTA-T = -0.5 DEG. C/100M

BROWNS FERRY NUCLEAR PLANT METEOROLOGICAL FACILITY\*

JAN 1, 74 - DEC 31, 75

WIND DIRECTION	045-144	145-244	245-344	345-444	445-544	545-644	645-744	745-844	845-944	945-1044	1045-1144	1145-1244	1245-1344	1345-1444	1445-1544	1545-1644	1645-1744	1745-1844	1845-1944	1945-2044	2045-2144	2145-2244	2245-2344	2345-2444	TOTAL
N	0.04	0.31	0.41	0.53	0.38	0.12	0.02	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	2.30
NNE	0.01	0.42	0.48	0.38	0.35	0.02	0.01	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	1.66
NE	0.01	0.40	0.30	0.12	0.04	0.01	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.90
ENE	0.02	0.36	0.22	0.02	0.03	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.65
E	0.02	0.23	0.22	0.04	0.02	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.53
ESE	0.01	0.51	0.74	0.36	0.28	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	1.90
SE	0.05	1.44	1.45	0.58	0.35	0.03	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	3.90
SSE	0.01	0.97	0.54	0.13	0.04	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	1.69
S	0.01	1.06	0.75	0.18	0.02	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	2.02
SSW	0.01	0.33	0.23	0.07	0.01	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.65
SW	0.02	0.33	0.23	0.03	0.01	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.62
WSW	0.01	0.54	0.64	0.27	0.23	0.12	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	1.81
W	0.00	0.35	0.88	0.56	0.57	0.15	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	2.51
WNW	0.00	0.18	0.42	0.42	0.62	0.36	0.05	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	2.06
NW	0.01	0.10	0.24	0.48	0.85	0.40	0.03	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	2.04
NNW	0.01	0.26	0.36	0.36	1.26	0.50	0.01	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	2.76
SUBTOTAL	0.24	7.79	8.11	4.45	5.59	1.71	0.09	0.02	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	28.00
CALM =	0.01																								

4648 STABILITY CLASS D OCCURRENCES OUT OF TOTAL 16559 VALID TEMPERATURE DIFFERENCE READINGS

4564 VALID WIND DIRECTION - WIND SPEED READINGS OUT OF TOTAL 4648 STABILITY CLASS D OCCURRENCES

ALL COLUMNS AND CALM TOTAL 100 PERCENT OF NET VALID READINGS

\*METEOROLOGICAL FACILITY LOCATED 0.78 MILES ESE OF BROWNS FERRY NUCLEAR PLANT  
TEMPERATURE INSTRUMENTS 33 AND 150 FEET ABOVE GROUND  
RADWASTE BUILDING-GROUND LEVEL RELEASE 33 FEET WIND INFORMATION.

POOR ORIGINAL

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Table 1.3 (Continued)

JOINT PERCENTAGE FREQUENCIES OF WIND DIRECTION AND WIND SPEED  
FOR DIFFERENT STABILITY CLASSES \*

STABILITY CLASS E  
-0.5 < DELTA-T < 1.5 DEG. C/100M

BROWNS FERRY NUCLEAR PLANT METEOROLOGICAL FACILITY\*

JAN 1, 74 - DEC 31, 75

WIND DIRECTION	WIND SPEED (MPH)										TOTAL
	0.0-1.4	1.5-3.4	3.5-5.4	5.5-7.4	7.5-12.4	12.5-18.4	18.5-24.4	24.5-34.4	35-47.4		
N	0.06	0.55	0.52	0.37	0.26	0.01	0.0	0.0	0.0	1.77	
NNE	0.10	0.77	0.50	0.26	0.13	0.01	0.0	0.0	0.0	1.77	
NE	0.07	0.47	0.45	0.10	0.05	0.0	0.0	0.0	0.0	1.14	
ENE	0.10	0.58	0.15	0.02	0.0	0.0	0.0	0.0	0.0	0.85	
E	0.03	0.74	0.44	0.08	0.02	0.0	0.0	0.0	0.0	1.31	
ESE	0.04	0.97	1.09	0.48	0.17	0.0	0.0	0.0	0.0	2.75	
SE	0.23	2.31	1.87	1.01	0.53	0.0	0.0	0.0	0.0	5.95	
SSE	0.22	1.08	0.56	0.21	0.09	0.0	0.0	0.0	0.0	2.16	
S	0.14	0.94	0.84	0.63	0.23	0.0	0.0	0.0	0.0	2.78	
SSW	0.17	0.58	0.28	0.18	0.08	0.01	0.0	0.0	0.0	1.30	
SW	0.10	0.55	0.12	0.04	0.01	0.0	0.0	0.0	0.0	0.72	
WSW	0.04	0.56	0.34	0.12	0.11	0.02	0.0	0.0	0.0	1.19	
W	0.02	0.56	0.65	0.25	0.15	0.04	0.0	0.0	0.0	1.67	
WNW	0.04	0.15	0.16	0.13	0.13	0.06	0.0	0.0	0.0	0.67	
NW	0.05	0.15	0.21	0.09	0.26	0.09	0.0	0.0	0.0	0.85	
NNW	0.08	0.50	0.56	0.39	0.31	0.04	0.0	0.0	0.0	1.88	
SUBTOTAL	1.49	11.36	8.74	4.36	2.53	0.28	0.0	0.0	0.0	28.76	
CALM =	0.06										

4764 STABILITY CLASS E OCCURRENCES OUT OF TOTAL 16559 VALID TEMPERATURE DIFFERENCE READINGS

4700 VALID WIND DIRECTION - WIND SPEED READINGS OUT OF TOTAL 4764 STABILITY CLASS E OCCURRENCES

ALL COLUMNS AND CALM TOTAL 100 PERCENT OF NET VALID READINGS

\*METEOROLOGICAL FACILITY LOCATED 0.78 MILES ESE OF BROWNS FERRY NUCLEAR PLANT  
TEMPERATURE INSTRUMENTS 33 AND 150 FEET ABOVE GROUND  
RADWASTE BUILDING-GROUND LEVEL RELEASE 3 FEET WIND INFORMATION.

POOR ORIGINAL

302 024

Table 1.3 (Continued)

JOINT COMMERCIAL FREQUENCIES OF WIND DIRECTION AND WIND SPEED  
FOR DIFFERENT STABILITY CLASSES

STABILITY CLASS F  
1.5< UFLTA - 4.0 DEG. C/100M

BROWNS FERRY NUCLEAR PLANT METEOROLOGICAL FACILITY

JAN 1, 74 - DEC 31, 75

WIND DIRECTION	0.5-1.4	1.5-3.4	3.5-5.4	5.5-7.4	7.5-12.4	12.5-18.4	18.5-24.4	24.5	TOTAL
N	0.10	0.45	0.34	0.12	0.02	0.0	0.0	0.0	1.03
NNE	0.12	0.65	0.36	0.10	0.0	0.0	0.0	0.0	1.43
NE	0.10	0.51	0.15	0.02	0.0	0.0	0.0	0.0	0.78
ENE	0.09	0.60	0.06	0.0	0.0	0.0	0.0	0.0	0.75
E	0.06	0.93	0.36	0.0	0.0	0.0	0.0	0.0	1.35
ESE	0.07	0.72	0.28	0.04	0.0	0.0	0.0	0.0	1.11
SE	0.25	1.34	0.61	0.23	0.08	0.0	0.0	0.0	2.51
SSE	0.14	0.59	0.25	0.15	0.10	0.0	0.0	0.0	1.23
S	0.09	0.50	0.43	0.30	0.20	0.0	0.0	0.0	1.52
SSW	0.06	0.16	0.07	0.01	0.0	0.0	0.0	0.0	0.30
SW	0.04	0.15	0.01	0.0	0.0	0.0	0.0	0.0	0.20
WSW	0.05	0.10	0.0	0.01	0.01	0.0	0.0	0.0	0.17
W	0.04	0.09	0.02	0.01	0.0	0.0	0.0	0.0	0.16
WNW	0.02	0.13	0.03	0.01	0.0	0.0	0.0	0.0	0.19
NW	0.04	0.12	0.10	0.01	0.0	0.01	0.0	0.0	0.28
NNW	0.08	0.33	0.34	0.11	0.01	0.0	0.0	0.0	0.87
SUBTOTAL	1.35	7.57	3.41	1.12	0.42	0.01	0.0	0.0	13.88

CALM = 0.07

2286 STABILITY CLASS F OCCURRENCES OUT OF TOTAL 16559 VALID TEMPERATURE DIFFERENCE READINGS

2247 VALID WIND DIRECTION - WIND SPEED READINGS OUT OF TOTAL 2286 STABILITY CLASS F OCCURRENCES

ALL COLUMNS AND CALM TOTAL 100 PERCENT OF NET VALID READING

\*METEOROLOGICAL FACILITY LOCATED 0.78 MILES ESE OF BROWNS FERRY NUCLEAR PLANT  
TEMPERATURE INSTRUMENTS 33 AND 150 FEET ABOVE GROUND  
RADWASTE BUILDING-GROUND LEVEL RELEASE 33 FEET WIND INFORMATION.

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Table 1.3 (Continued)

JOINT PERCENTAGE OCCURRENCES OF WIND DIRECTION AND WIND SPEED  
FOR DIFFERENT STABILITY CLASSES

STABILITY CLASS G  
DELTA T > 4.0 DEG. C/100M

BROWNS FERRY NUCLEAR PLANT METEOROLOGICAL FACILITY

JAN 1, 74 - DEC 31, 75

WIND DIRECTION	WIND SPEED (MPH)							TOTAL
	0.0-1.4	1.5-3.4	3.5-5.4	5.5-7.4	7.5-12.4	12.5-18.4	18.5-24.4	
N	0.29	0.93	0.17	0.04	0.0	0.0	0.0	1.43
NNE	0.20	1.28	0.10	0.02	0.0	0.0	0.0	1.60
NE	0.14	0.44	0.02	0.0	0.0	0.0	0.0	0.60
NNE	0.09	0.52	0.02	0.0	0.0	0.0	0.0	0.63
E	0.07	0.66	0.15	0.0	0.0	0.0	0.0	0.88
ESE	0.04	0.35	0.01	0.0	0.0	0.0	0.0	0.40
SE	0.15	0.74	0.09	0.03	0.01	0.0	0.0	1.02
SSE	0.19	0.61	0.13	0.04	0.02	0.0	0.0	0.99
S	0.14	0.54	0.14	0.06	0.0	0.0	0.0	0.88
SSW	0.07	0.06	0.0	0.0	0.0	0.0	0.0	0.13
SW	0.06	0.05	0.0	0.0	0.0	0.0	0.0	0.11
WSW	0.04	0.04	0.0	0.0	0.0	0.0	0.0	0.08
W	0.01	0.04	0.01	0.0	0.0	0.0	0.0	0.06
WNW	0.07	0.06	0.01	0.0	0.0	0.0	0.0	0.14
NW	0.07	0.09	0.01	0.0	0.0	0.0	0.0	0.17
NNW	0.18	0.36	0.10	0.04	0.0	0.0	0.0	0.68
SUM TOTAL	1.81	6.77	9.96	9.23	9.03	9.0	9.0	9.80
CALM =	0.09							

1620 STABILITY CLASS G OCCURRENCES OUT OF TOTAL 16559 VALID TEMPERATURE DIFFERENCE READINGS

1612 VALID WIND DIRECTION - WIND SPEED READINGS OUT OF TOTAL 1620 STABILITY CLASS G OCCURRENCES

ALL COLUMNS AND CALM TOTAL 100 PERCENT OF NET VALID READINGS

METEOROLOGICAL FACILITY LOCATED 0.78 MILES ESE OF BROWNS FERRY NUCLEAR PLANT  
TEMPERATURE INSTRUMENTS 33 AND 150 FEET ABOVE GROUND  
RADWASTE BUILDING-GROUND LEVEL RELEASE 33 FEET WIND INFORMATION

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Table 1.3 (Cont Inued)

July 1969 Table 1.3 - Summary of Wind Frequency Data - 1600 SRE -  
For Stability Classes

STABILITY CLASS D  
-1.5< DELTA-T<-0.5 DEG. C/1000  
BROWNS FERRY NUCLEAR PLANT METEOROLOGICAL FACILITY\*

JAN 1, 74 - DEC 31, 75

WIND DIRECTION	0-6-1-6	1-5-3-6	3-5-5-6	5-5-7-6	7-5-12-6	12-5-18-6	18-5-26-6	26-5-36-6	IGI41
N	0.0	0.02	0.12	0.23	0.79	0.92	0.31	0.01	2.40
NNE	0.01	0.10	0.21	0.36	1.04	0.86	0.13	0.0	2.69
NE	0.01	0.04	0.15	0.20	0.72	0.32	0.01	0.6	1.45
ENE	0.01	0.03	0.07	0.16	0.36	0.07	0.0	0.0	0.66
E	0.0	0.04	0.11	0.17	0.19	0.01	0.0	0.0	0.52
ESE	0.0	0.13	0.17	0.18	0.62	0.10	0.07	0.02	1.09
SE	0.0	0.22	0.55	0.54	1.25	0.81	0.48	0.19	4.04
SSE	0.01	0.32	0.60	0.41	0.84	0.72	0.39	0.11	3.20
S	0.0	0.18	0.26	0.31	0.78	0.59	0.28	0.15	2.55
SSW	0.0	0.11	0.20	0.12	0.56	0.37	0.28	0.15	2.09
SW	0.01	0.24	0.33	0.20	0.58	0.53	0.18	0.04	2.11
WSW	0.0	0.17	0.47	0.28	0.36	0.41	0.16	0.13	1.91
W	0.01	0.10	0.39	0.40	0.56	0.48	0.28	0.21	2.41
WNW	0.0	0.09	0.22	0.40	0.75	0.55	0.30	0.21	2.52
NW	0.0	0.10	0.43	0.47	1.18	0.92	0.60	0.22	3.92
NNW	0.01	0.14	0.21	0.20	0.73	1.40	0.58	0.07	3.24
SURTOTAL	0.07	1.93	4.29	4.59	11.09	9.26	4.05	1.51	36.89

CALM = 0.01

6114 STABILITY CLASS D OCCURRENCES OUT OF TOTAL 16401 VALID TEMPERATURE DIFFERENCE READINGS

6038 VALID WIND DIRECTION - WIND SPEED READINGS OUT OF TOTAL 6114 STABILITY CLASS D OCCURRENCES

ALL COLUMNS AND CALM TOTAL 100 PERCENT OF NET VALID READINGS

\*METEOROLOGICAL FACILITY LOCATED 0.78 MILES ESE OF BROWNS FERRY NUCLEAR PLANT  
TEMPERATURE INSTRUMENTS 300 AND 150 FEET ABOVE GROUND  
WIND INSTRUMENTS AT 300 FEET ABOVE GROUND

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Table 1.3 (Continued)

BRUNSWICK COUNTY, NORTH CAROLINA  
EWE-ALL-DIRECTION

BROWNS FERRY NUCLEAR PLANT METEOROLOGICAL FACILITY

JAN 1, 74 - DEC 31, 75

WIND DIRECTION	WIND SPEED (MPH)										TOTAL
	0-5	5-10	10-15	15-20	20-25	25-30	30-35	35-40	40-45	45-50	
N	0.02	0.23	1.29	1.71	1.96	0.51	0.02				5.20
NNE	0.03	0.24	0.38	2.06	2.36	0.60	0.07				6.30
NNE	0.07	0.15	0.60	1.80	1.83	0.50	0.03				5.71
E	0.03	0.15	0.36	1.25	0.85	0.21	0.01				3.32
E	0.01	0.23	0.69	1.02	0.37	0.06	0.0				2.67
ESE	0.03	0.34	0.53	1.62	1.12	0.29	0.05				4.56
SE	0.04	0.56	1.19	3.63	2.76	1.39	0.56				11.66
SSE	0.08	0.66	0.99	3.11	3.66	1.29	0.07				10.61
S	0.03	0.68	0.83	2.76	2.69	1.08	0.74				9.63
SSW	0.03	0.60	0.63	2.17	2.71	1.62	0.50				8.42
SW	0.04	0.69	0.63	1.77	1.08	0.67	0.20				6.35
WSW	0.02	0.37	0.90	1.20	0.87	0.27	0.23				4.52
W	0.03	0.27	0.77	1.36	0.84	0.63	0.28				4.72
WNW	0.03	0.18	0.42	1.39	0.90	0.42	0.26				4.69
NW	0.02	0.31	0.70	2.08	1.50	0.85	0.27				6.57
NNW	0.03	0.23	0.67	1.56	2.27	0.71	0.09				5.87
TOTAL	0.48	5.27	9.98	30.45	27.55	10.63	3.98				99.88

ALM = 0.11

6850 VALID WIND DIRECTION - WIND SPEED READINGS OUT OF 37520 TOTAL HOURS = 96.18 PERCENT

ALL COLUMNS AND CALM TOTAL 100 PERCENT OF NET VALID READINGS

METEOROLOGICAL FACILITY LOCATED 0.78 MILES ESE OF BROWNS FERRY NUCLEAR PLANT  
WIND INSTRUMENTS AT 300 FEET ABOVE GROUND

POOR ORIGINAL

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TABLE 1.4

BROWNS FERRY NUCLEAR PLANT LAND SITE BOUNDARY DATA

<u>Sector</u>	<u>Distance (m)</u>	<u>Elevated <math>\chi/Q^1</math></u>	<u>Elevated <math>D/Q^2</math></u>	<u>Ground <math>\chi/Q^1</math></u>	<u>Ground <math>D/Q^2</math></u>
N	1,550	1.88(-10) <sup>3</sup>	9.55(-10)	2.26(-6)	5.66(-9)
NNE	1,400	4.06(-11)	7.71(-10)	1.02(-6)	2.05(-9)
NE	1,370	3.51(-11)	5.72(-10)	7.93(-7)	1.65(-9)
ENE	1,400	1.65(-11)	4.14(-10)	9.34(-7)	3.18(-9)
E	1,570	6.08(-11)	4.73(-10)	8.04(-7)	3.34(-9)
ESE	1,470	2.79(-11)	4.27(-10)	6.81(-7)	3.39(-9)
SE	5,460	9.33(-9)	3.18(-10)	1.11(-7)	3.83(-10)
SSE	2,740	1.82(-9)	5.99(-10)	7.03(-7)	1.90(-9)
S	2,380	8.43(-10)	5.47(-10)	1.19(-6)	2.51(-9)
SSW	2,410	1.08(-9)	6.61(-10)	1.32(-6)	2.40(-9)
SW	2,160	4.93(-10)	5.60(-10)	8.50(-7)	1.45(-9)
WSW	3,120	1.87(-9)	3.16(-10)	4.90(-7)	6.11(-10)
W	2,350	5.23(-10)	2.82(-10)	8.83(-7)	1.37(-9)
WNW	3,120	2.66(-9)	4.34(-10)	6.16(-7)	1.38(-9)
NW	3,440	7.97(-9)	9.76(-10)	1.29(-6)	2.84(-9)
NNW	1,620	1.73(-10)	1.09(-9)	2.20(-6)	4.84(-9)

1.  $s/m^3$

2.  $m^{-2}$

3.  $1.88(-10) = 1.88 \times 10^{-10}$

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TABLE 1.5

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## DOSE FACTORS FOR SUBMERSION IN NOBLE GASES

	<u>DFB<sup>1</sup></u>	<u>DFY<sup>2</sup></u>	<u>DFS<sup>1</sup></u>	<u>DFB<sup>2</sup></u>
Kr-85m	1.17(+3) <sup>3</sup>	1.21(+3)	1.46(+3)	3.86(+3)
Kr-85	1.61(+1)	1.69(+1)	1.34(+3)	3.83(+3)
Kr-87	5.92(+3)	6.05(+3)	9.73(+3)	2.01(+4)
Kr-88	1.47(+4)	1.50(+4)	2.37(+3)	5.72(+3)
Kr-89	1.66(+4)	1.59(+4)	1.01(+4)	1.88(+4)
Xe-131m	9.15(+1)	1.53(+2)	4.76(+2)	2.18(+3)
Xe-133m	2.51(+2)	3.17(+2)	9.94(+2)	2.90(+3)
Xe-133	2.94(+2)	3.46(+2)	3.06(+2)	2.06(+3)
Xe-135m	3.12(+3)	3.30(+3)	7.11(+2)	1.45(+3)
Xe-135	1.81(+3)	1.88(+3)	1.86(+3)	4.84(+3)
Xe-137	1.42(+3)	1.48(+3)	1.22(+4)	2.50(+4)
Xe-138	8.83(+3)	9.00(+3)	4.13(+3)	9.25(+3)
Ar-41	8.84(+3)	9.76(+3)	2.69(+3)	5.54(+3)

1. mrem/y per  $\mu\text{Ci}/\text{m}^3$ .
2. mrad/y per  $\mu\text{Ci}/\text{m}^3$ .
3.  $1.17(+3) = 1.17 \times 10^3$ .

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STABLE ELEMENT TRANSFER DATA

<u>Element</u>	<u>B<sub>fv</sub></u> <u>Vec/Soil</u>	<u>F<sub>m</sub> (Cow)</u> <u>Milk (d/L)</u>
H	4.8E-00	1.0E-02
C	5.2E-00	1.2E-02
Na	5.2E-02	4.0E-02
P	7.1E-00	2.5E-02
Cr	2.2E-03	2.2E-03
Mn	2.2E-02	2.5E-04
Fe	5.6E-01	1.2E-03
Co	9.2E-03	1.0E-03
Ni	1.0E-02	6.7E-03
Cu	1.2E-01	1.4E-02
Zn	4.0E-01	3.0E-02
Ed	1.2E-01	3.0E-02
Sr	1.7E-02	8.0E-04
Y	2.2E-03	1.2E-05
Zr	1.2E-04	5.1E-05
Nb	9.2E-03	2.5E-03
Mo	1.2E-01	7.5E-03
Tc	2.2E-01	2.5E-02
Ru	5.0E-02	1.0E-05
Rh	1.2E-01	1.0E-02
Ag	1.2E-01	5.0E-02
Cd	1.2E-00	1.0E-03
I	2.0E-02	6.0E-03
Cs	1.0E-02	1.2E-02
Ba	5.0E-03	4.0E-04
La	2.0E-03	5.0E-05
Ce	2.0E-03	1.0E-04
Pr	2.0E-03	5.0E-05
Ad	2.2E-03	5.0E-05
M	1.0E-02	5.0E-04
Kp	2.5E-03	5.0E-06

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6/21/79INTERNAL DOS. FACTORS - INFANT THYROID

<u>Radionuclide</u>	<u>Inhalation (mrem/pCi)</u>	<u>Ingestion (mrem/pCi)</u>
H-3	4.62(-7)	3.08(-7)
C-14	3.79(-6)	5.06(-6)
Cr-51	4.11(-8)	9.20(-9)
Te-132	1.99(-7)	1.52(-5)
I-131	1.06(-2)	1.39(-2)
I-132	1.21(-4)	1.58(-4)
I-133	2.54(-3)	3.31(-3)
I-134	3.18(-5)	4.15(-5)
I-135	4.97(-4)	6.49(-4)

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Table 1.8  
EXTERNAL DOSE FACTORS FOR STANDING ON CONTAMINATED GROUND  
(mrem/hr per pCi/m<sup>2</sup>)

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Element	Total Body	Skin
H-3	0.0	0.0
C-14	0.0	0.0
KA-24	2.50E-08	2.90E-08
P-32	0.0	0.0
Cr-51	2.20E-10	2.60E-10
Mn-54	5.80E-09	6.80E-09
Mn-56	1.10E-08	1.30E-08
Fe-55	0.0	0.0
Fe-59	8.30E-09	9.40E-09
Co-58	7.00E-09	8.20E-09
Co-60	1.70E-08	2.00E-08
Ni-63	0.0	0.0
Ni-65	3.70E-09	4.30E-09
Cu-64	1.50E-09	1.70E-09
Zn-65	4.00E-09	4.60E-09
Zn-69	0.0	0.0
Br-81	6.40E-11	9.30E-11
Br-84	1.20E-08	1.40E-08
Br-85	0.0	0.0
Rb-86	6.30E-10	7.20E-10
Rb-88	3.50E-09	4.00E-09
Rb-89	1.50E-08	1.80E-08
Sr-89	5.60E-13	6.50E-13
Sr-91	7.10E-09	8.30E-09
Sr-92	9.00E-09	1.00E-08
Y-90	2.20E-12	2.60E-12
Y-91M	3.80E-09	4.40E-09
Y-91	2.40E-11	2.70E-11
Y-92	1.60E-09	1.90E-09
Y-93	5.70E-10	7.80E-10
Zr-95	5.00E-09	5.80E-09
Zr-97	5.50E-09	6.40E-09
Nb-95	5.10E-09	6.00E-09
Mo-99	1.90E-09	2.20E-09
Tc-99M	9.60E-10	1.10E-09
Tc-101	2.70E-09	3.00E-09
Ru-103	3.60E-09	4.20E-09
Ru-105	4.50E-09	5.10E-09
Ru-106	1.50E-09	1.80E-09
Ag-110M	1.80E-08	2.10E-08
Te-125M	3.50E-11	4.60E-11
Te-127M	1.10E-12	1.30E-12
Te-127	1.00E-11	1.10E-11
Te-125M	7.70E-10	9.00E-10
Te-129	7.10E-10	8.40E-10
Te-131M	8.40E-09	9.90E-09
Te-131	2.20E-09	2.60E-09
Te-132	1.70E-09	2.00E-09
I-130	1.40E-08	1.70E-08
I-131	2.80E-09	3.40E-09
I-132	1.70E-08	2.00E-08
I-133	3.70E-09	4.50E-09
I-134	1.60E-08	1.90E-08
I-135	1.20E-08	1.40E-08
Cs-134	1.20E-08	1.40E-08
Cs-136	1.50E-08	1.70E-08
Cs-137	4.20E-09	4.90E-09
Cs-138	2.10E-08	2.40E-08
Ba-139	2.40E-09	2.70E-09
Ba-140	2.10E-09	2.40E-09
Ba-141	4.30E-09	4.90E-09
Ba-142	7.90E-09	9.00E-09
La-140	1.50E-08	1.70E-08
La-142	1.50E-08	1.80E-08
Ce-141	5.50E-10	6.20E-10
Ce-143	2.20E-09	2.50E-09
Ce-144	3.20E-10	3.70E-10
Pr-143	0.0	0.0
Pr-144	2.00E-10	2.30E-10
Nd-147	1.00E-09	1.20E-09
M-187	3.10E-09	3.60E-09
Np-239	9.50E-10	1.10E-09

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FIGURE 1.1

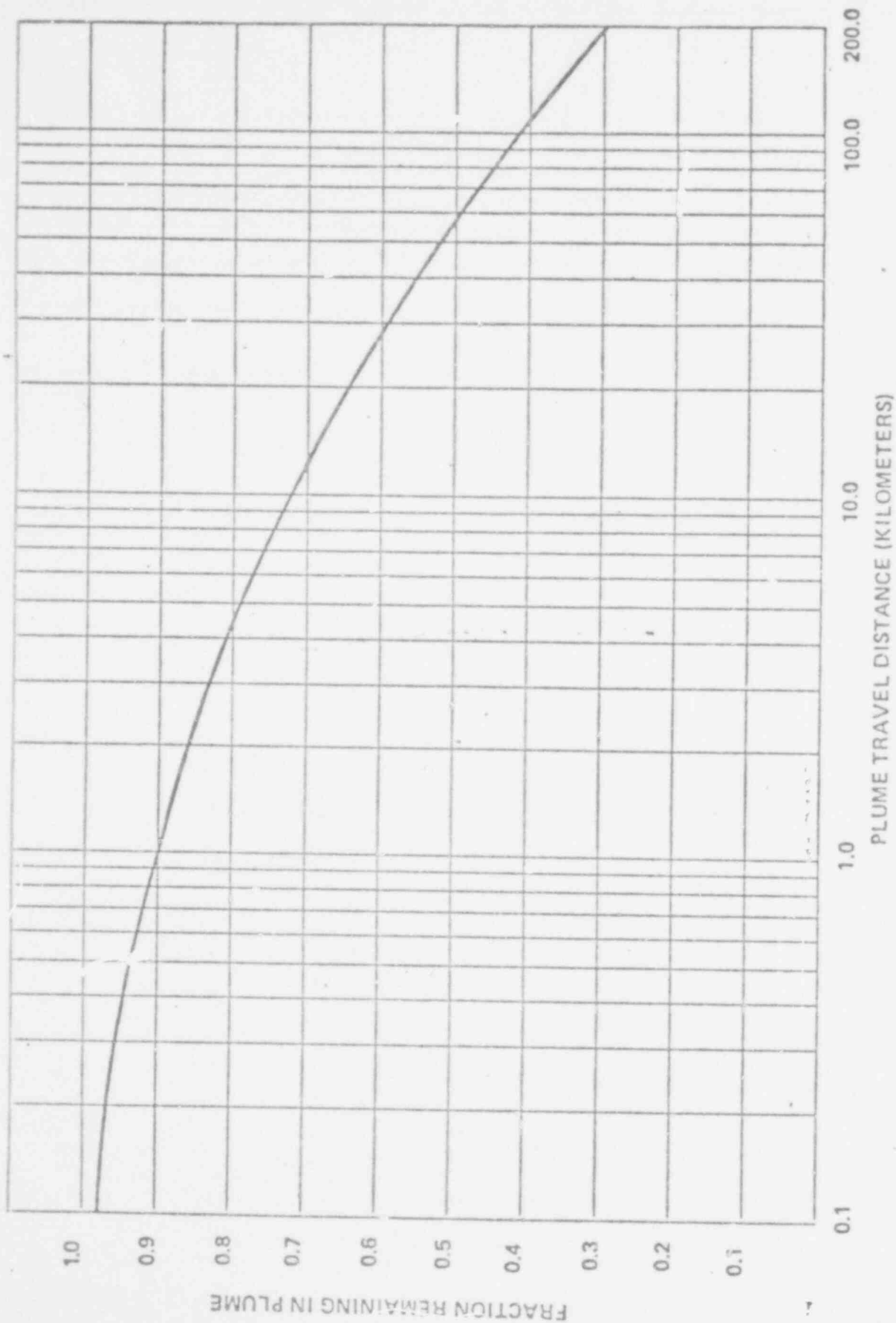
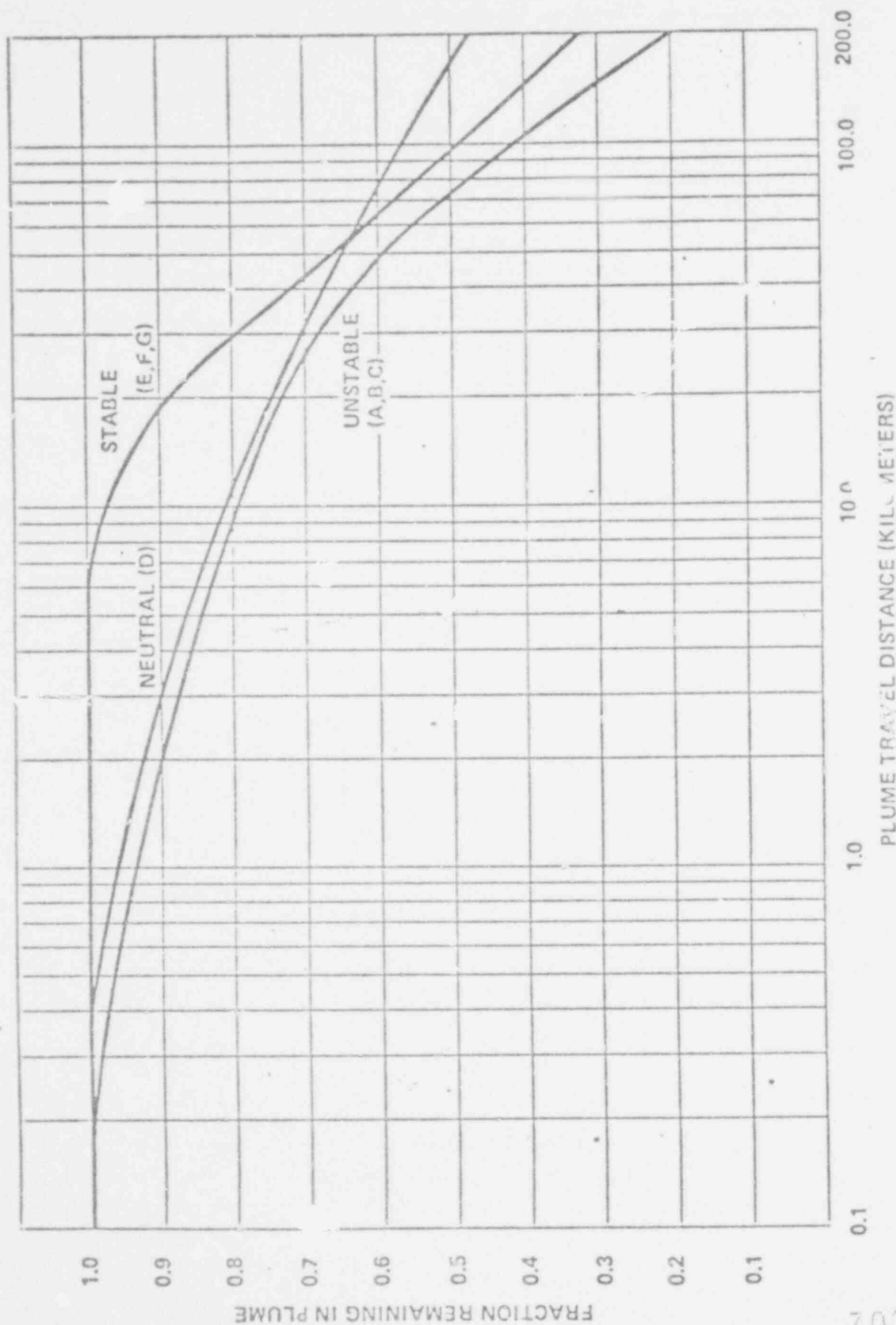


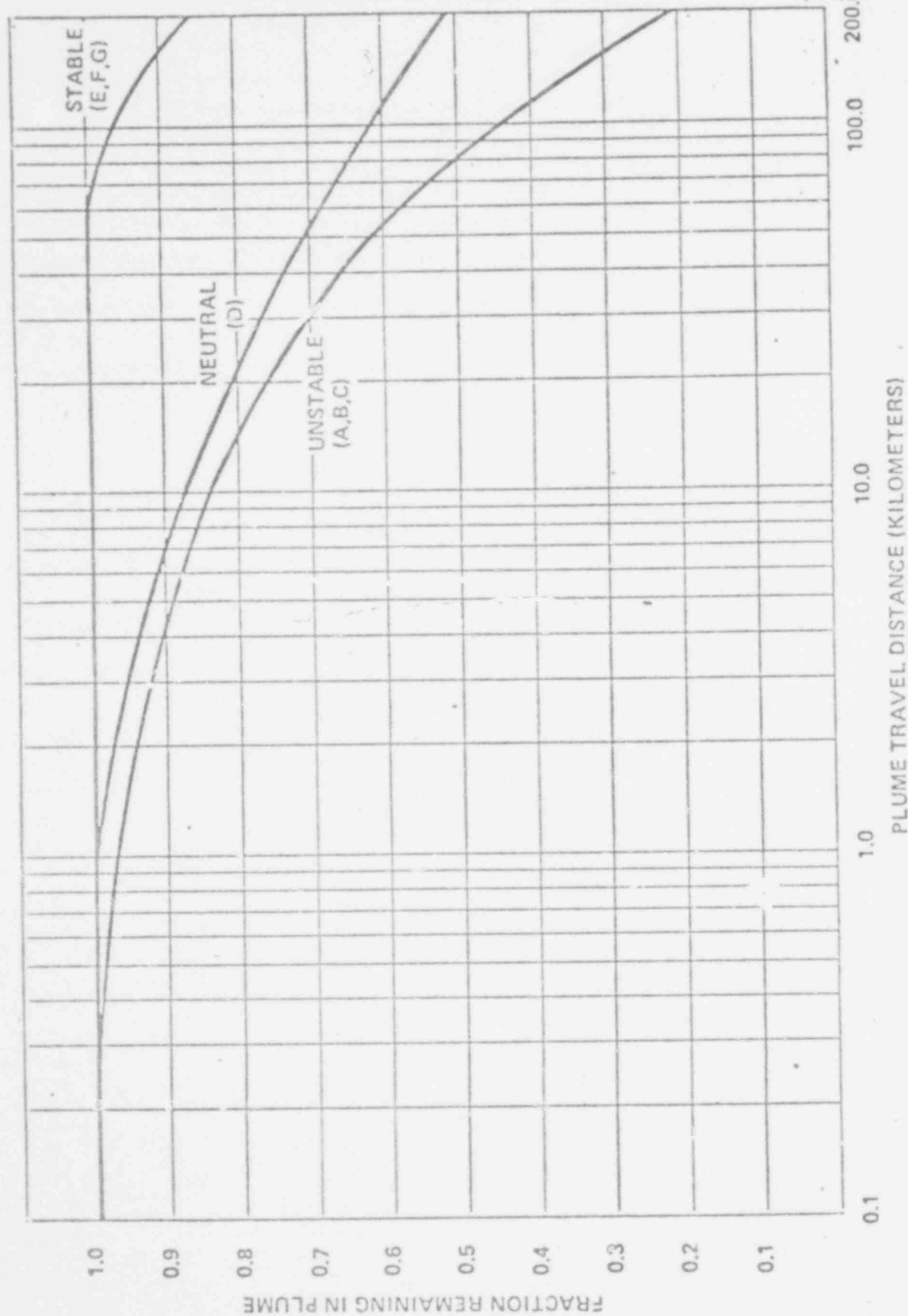
FIGURE 1.1 (CONTINUED)



Plume Depletion Effect for 30m Releases (Letters denote Pasquill Stability Class)

302 035

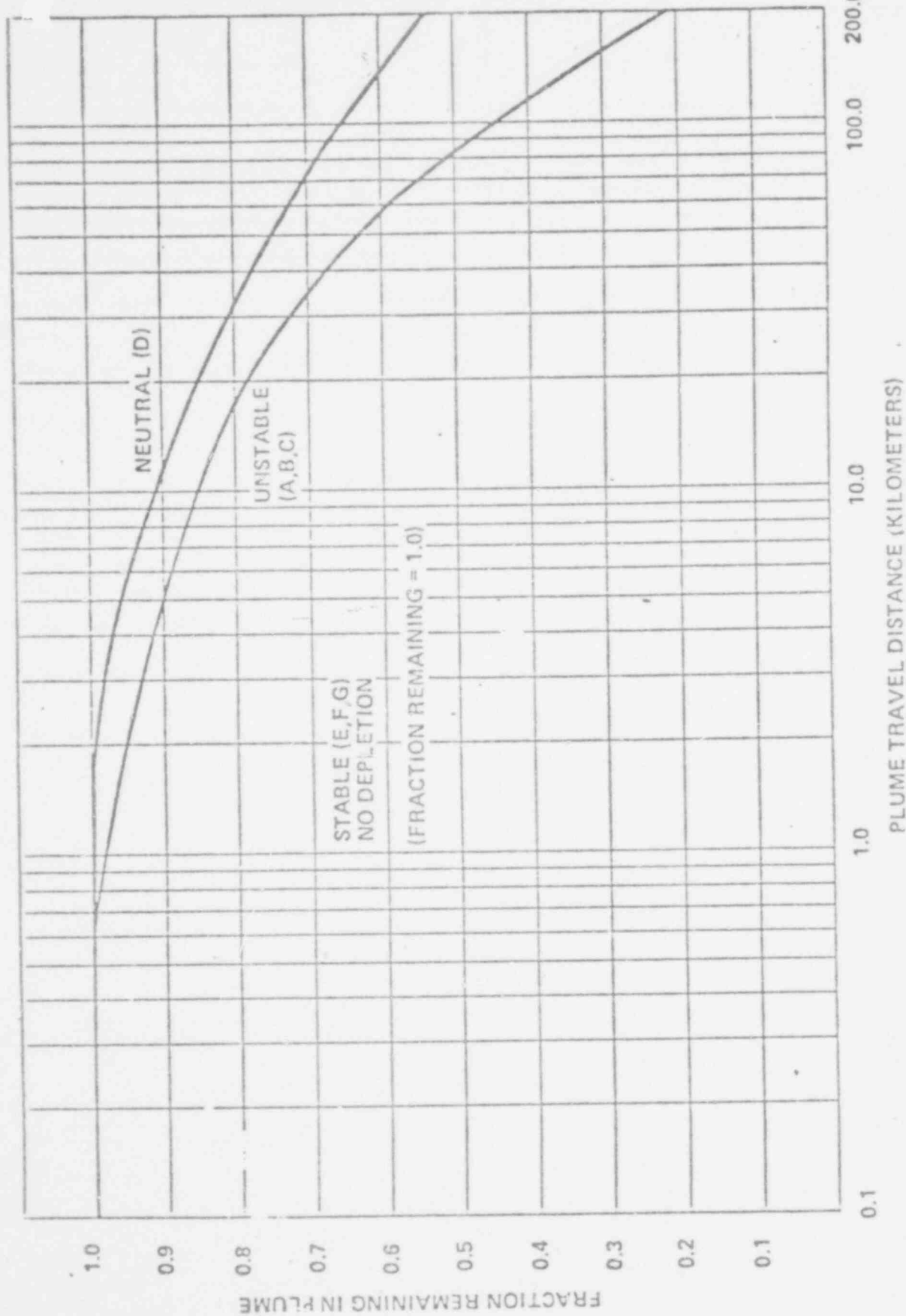
FIGURE 1.1 (CONTINUED)



Plume Depletion Effect for 60m Releases (Letters denote Pasquill Stability Class)

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FIGURE 1.1 (CONTINUED)

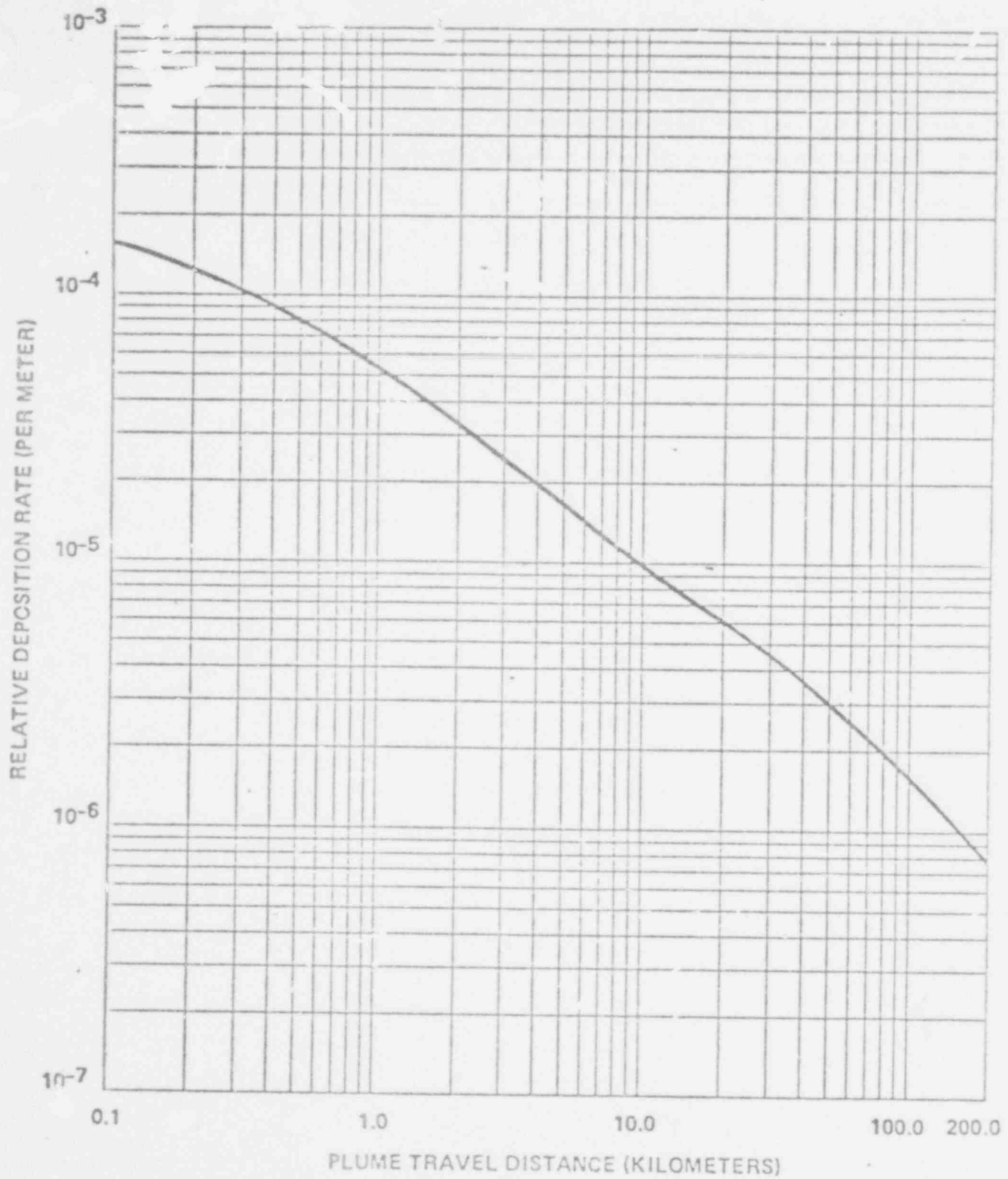


Plume Depletion Effect for 100m Releases (Letters denote Pasquill Stability Class)

302 037

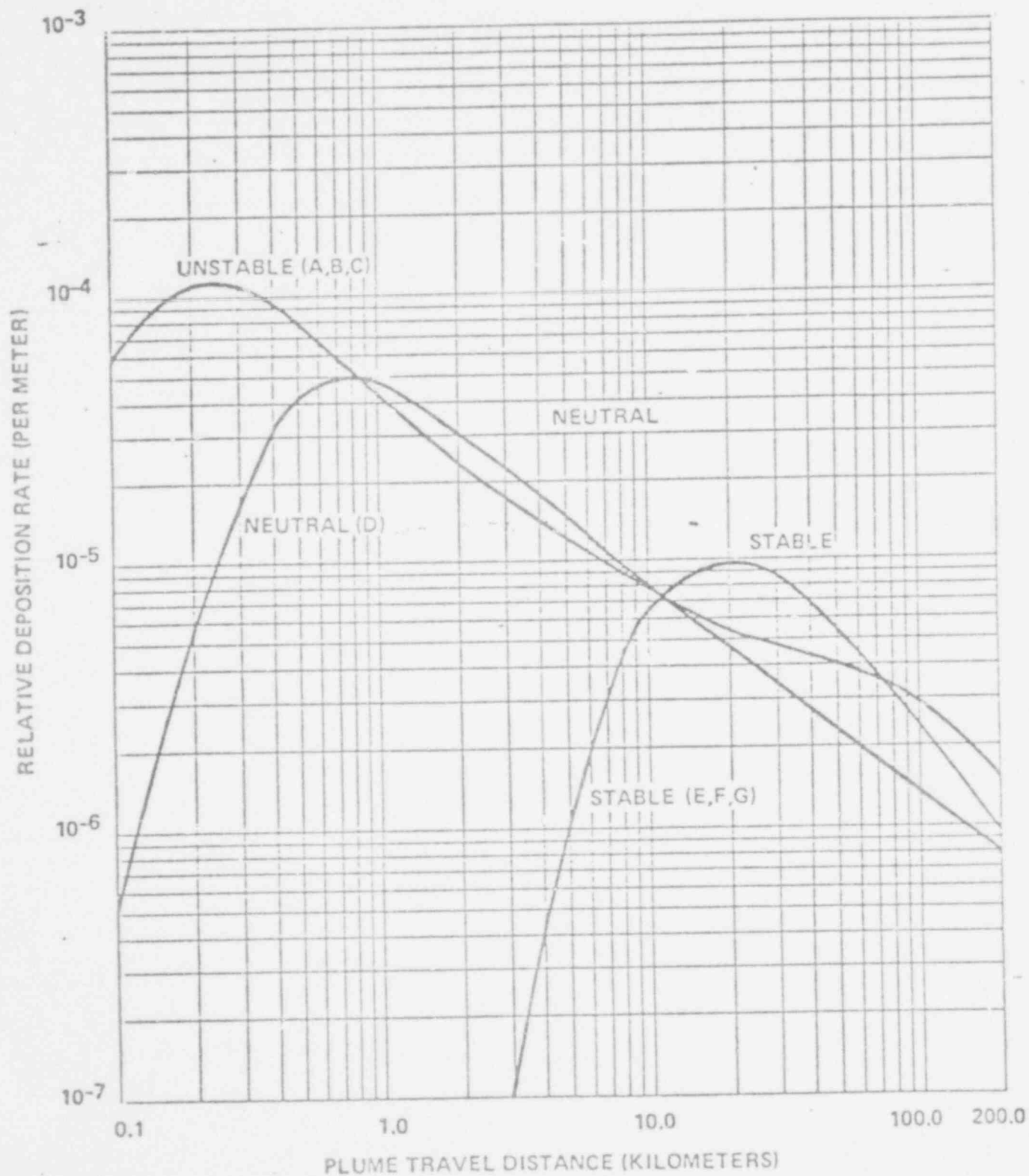
FIGURE 1.2

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Relative Deposition for Ground Level Releases (All Atmospheric Stability Classes)

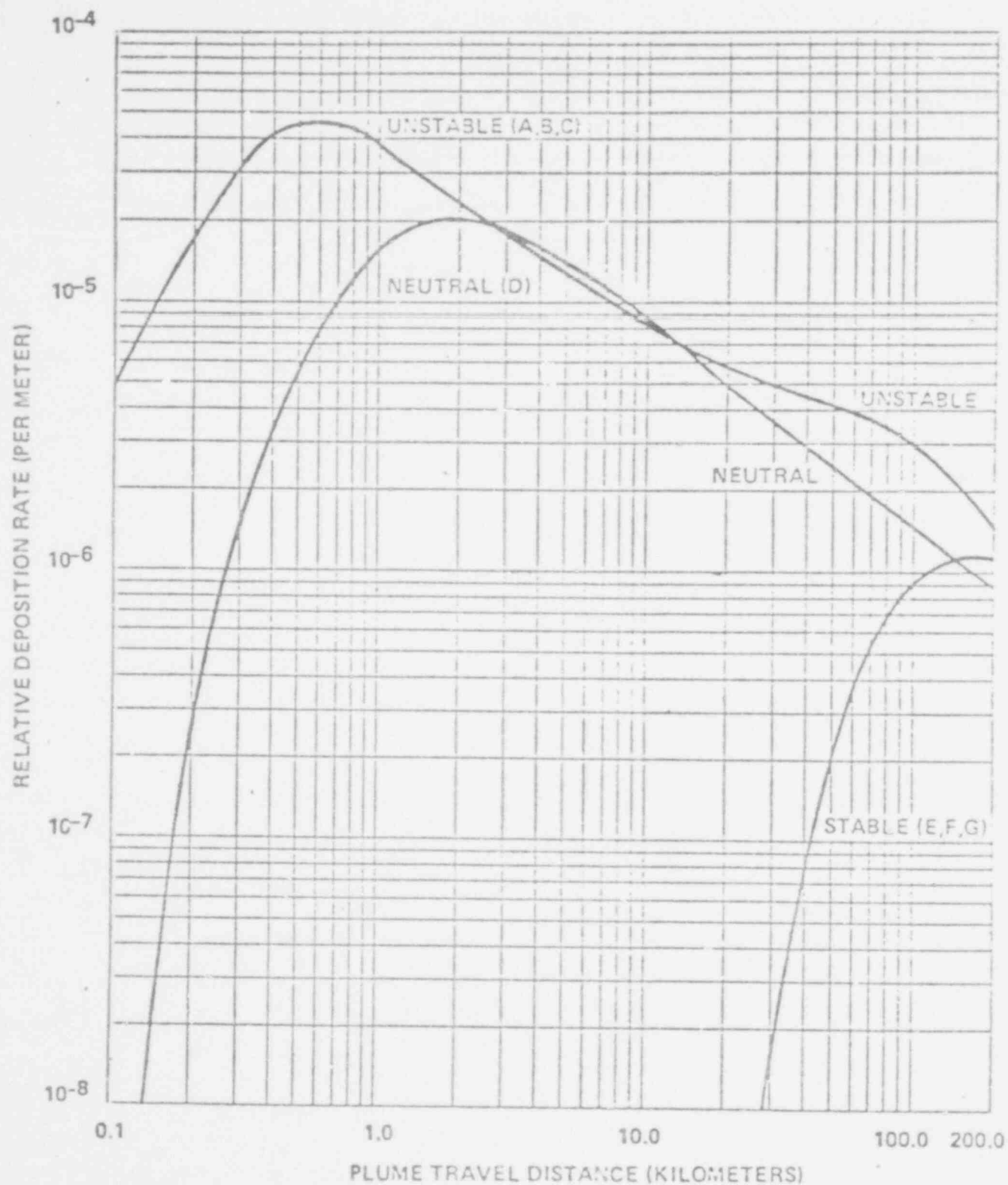
302 038



Relative Deposition for 30m Releases (Letters denote Pasquill Stability Class)

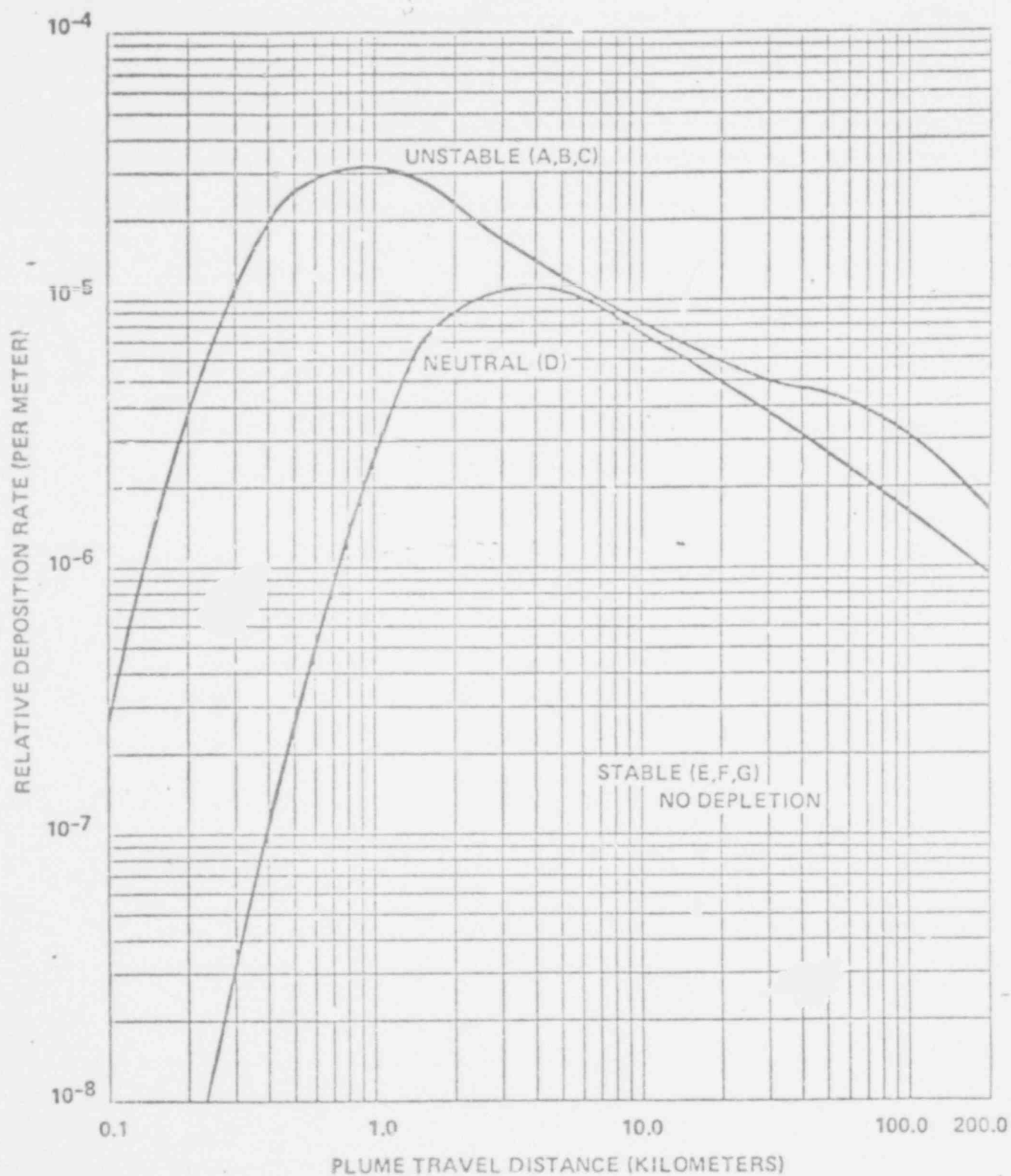
302 039





\* Relative Deposition for 60m Releases (Letters denote Pasquill Stability Class)

302 040

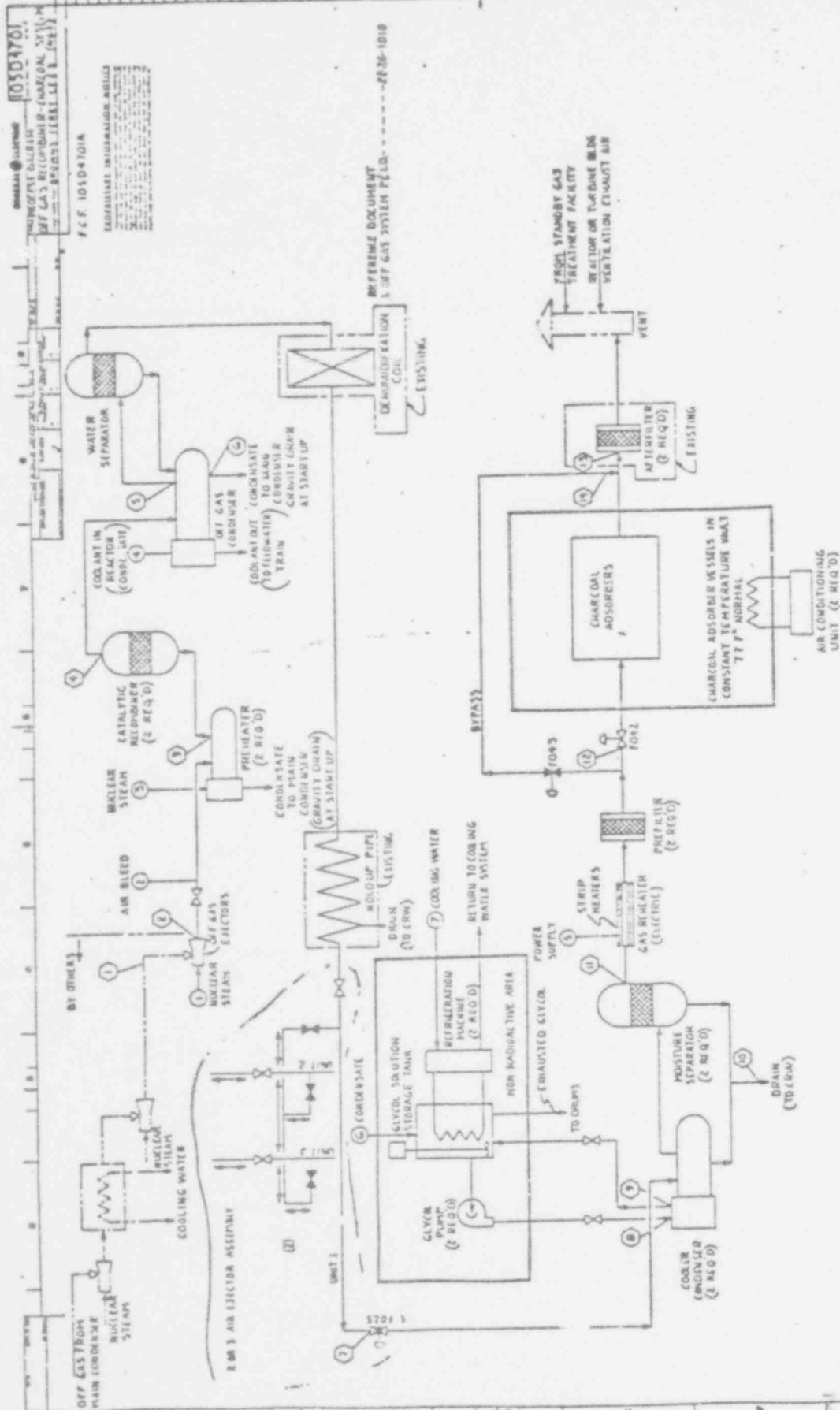


Relative Deposition for 100m Releases (Letters denote Pasquill Stability Class)

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FIGURE 1.3

### CASEOUS R.D.WASTE TREATMENT SYSTEM FLOW DIAGRAM



NOT UPDATED

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## 2. Liquid Effluents

### 2.1 Concentration

#### 2.1.1 RETS Requirement

Specification 3.8.A.1 of the Radiological Effluent Technical Specifications (RETS) requires that the concentration of radioactive material released at any time from the site to unrestricted areas (see Figure 2.1.) shall be limited to the Maximum Permissible Concentration (MPC, attached as Appendix I) specified in 10CFR20, Appendix B, Table II, Column 2 for nuclides other than dissolved or entrained noble gases. For dissolved or entrained noble gases, the concentration shall be limited to  $2 \times 10^{-4}$   $\mu\text{Ci/ml}$  total activity. To ensure compliance, the following approach will be used for each release.

#### 2.1.2 Prerelease Analysis

Prior to release a grab sample will be analyzed for the concentration of each radionuclide.

$$C = \sum_{i=1}^n C_i \quad (2.1)$$

where:

$C$  = total concentration in the liquid effluent,  $\mu\text{Ci/ml}$ .

$C_i$  = concentration of radionuclide  $i$ ,  $\mu\text{Ci/ml}$ .

#### 2.1.3 MPC-Sum of the Ratios

The sum of the ratios ( $R_j$ ) for the release will be calculated by the following relationship.

$$R = \frac{C_A}{MPC_A} + \frac{C_B}{MPC_B} + \dots + \frac{C_i}{MPC_i} + \dots + \frac{C_n}{MPC_n} \quad (2.2)$$

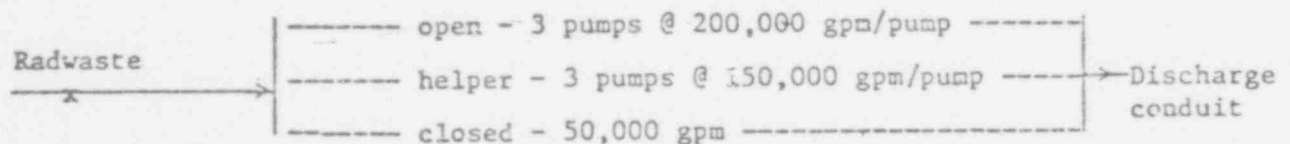
where:

$C_1$  = undiluted effluent concentration of radionuclide 1, as determined in Section 2.1.2,  $\mu\text{Ci/ml}$ .

$\text{MPC}_1$  = the MPC of radionuclide 1,  $\mu\text{Ci/ml}$ .

$R$  = the sum of the ratios for the release.

For prerelease and post-release analysis each  $C_1$  is first assumed to be unknown and the MPC is then  $1 \times 10^{-7}$   $\mu\text{Ci/ml}$  for each radionuclide 1. If the  $R$  calculated is too large for equation 2.3 then the appropriate  $\text{MPC}_1$  will be used for each  $C_1$ . There is one liquid release point into the discharge canal by one of 3 possible modes.



The following relationship will assure concentrations are within allowable limits.

$$f(R-1) \leq F \quad (2.3)$$

where:

$f$  = the radwaste flow rate (gallons/minute) before dilution.

$R$  = the sum of the ratios of the release as determined by Equation 2.2.

$F$  = minimum dilution flow rate for prerelease analysis.

## 2.2 Instrument Setpoints

### 2.2.1 Setpoint Determination

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The respective alarm/trip setpoints at each release point will be set such that Equation 2.3 is satisfied. The methodology describing the setpoint determination is contained in Technical Instruction 45.

### 2.2.2 Post-Release Analysis

A post-release analysis will be done using actual release data to ensure that the limits specified in Section 2.1.1 were not exceeded.

A composite list of concentrations ( $C_i$ ), by isotope, will be used with the actual liquid radwaste (f) and dilution (F) flow rates (or volumes) during the release. The data will be substituted into Equation 2.3 to demonstrate compliance with the limits in Section 2.1.1. This data and setpoints will be recorded in auditable records by plant personnel.

## 2.3 Dose

### 2.3.1 RETS Requirement

Specification 3.8.A.2 of the Radiological Effluent Technical Specification (RETS) requires that the dose or dose commitment to an individual from radioactive materials in liquid effluents released to unrestricted areas from each reactor (see Figure 2.1) shall be limited:

- a. During any calendar quarter to  $\leq 1.5$  mrem to the total body and to  $\leq 5$  mrem to any organ, and
- b. During any calendar year to  $\leq 3$  mrem to the total body and to  $\leq 10$  mrem to any organ.

To ensure compliance, cumulative dose calculations will be performed at least once per month according to the following methodology.

### 2.3.2 Monthly Analysis

Principal radionuclides will be used to conservatively estimate the monthly contribution to the cumulative dose. If the projected dose exceeds the above limits, the methodology in Section 2.3.2 will be implemented.

The following radionuclides contribute at least 98 percent of the total estimated dose based on four years of operational source terms.

	<u>Percent of Fish Dose</u>		<u>Percent of Ingestion Dose</u>	
	<u>Total Body</u>	<u>GI Tract</u>	<u>Total Body</u>	<u>Thyroid</u>
H-3	-	-	8.5	1.0
Na-24	-	-	2.5	.3
Co-60	-	.5	1.8	.2
Zn-65	5.0	3.9	3.7	.4
Sr-90	.9	-	32.2	3.8
Nb-95	-	67.4	-	-
I-131	-	.1	1.2	81.1
I-133	-	-	-	5.9
Cs-134	40.4	8.3	20.7	2.4
Cs-136	2.4	3.3	1.7	.2
Cs-137	<u>51.0</u> 99.7	<u>14.5</u> 98.0	<u>26.1</u> 98.4	<u>3.1</u> 98.4

A conservative calculation of the monthly dose will be done according to the following procedure. First, the monthly operating report containing the release data will be obtained and the activities released of each of the above 11 radionuclides will be noted. This information will then be used in the following calculations.

#### 2.3.2.1 Water Ingestion

The dose to an individual from ingestion of water is described by the following equation.

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$$D_j = \frac{1}{.95} \sum_{i=1}^{11} (DCF)_{ij} \times I_i \text{ rem} \quad (2.11)$$

where:

$D_j$  = dose for the  $j^{\text{th}}$  organ from 11 radionuclides, rem.

$j$  = the organ of interest (thyroid or total body).

..95 = conservative correction factor, considering only 11 radionuclides.

$DCF_{ij}$  = adult ingestion dose commitment factor for the  $j^{\text{th}}$  organ from the  $i^{\text{th}}$  radionuclide rem/ $\mu\text{Ci}$ , see attached Table 2.1.

$I_i$  = monthly activity ingested of the  $i^{\text{th}}$  radionuclide,  $\mu\text{Ci}$ .

$I_i$  is described by

$$I_i = \frac{365 A_i V}{12 U d}, \quad (2.12)$$

where:

365 = days per year

$A_i$  = activity released of  $i^{\text{th}}$  radionuclide during the month,  $\mu\text{Ci}$ .

$V$  = average rate of water consumption (730 ml/d ICRP 23, p. 358)

12 = months per year

$U$  = total cooling tower blowdown during releases, ml.

$d$  = minimum diffuser pipe dilution (5)

The dose equation then becomes

$$D_j = \frac{4.6 \times 10^6}{U} \sum_{i=1}^{11} (DCF)_{ij} \times A_i \text{ mrem} \quad (2.13)$$

#### 2.3.2.2 Fish Ingestion

The dose to an individual from the consumption of fish may be described by Equation 2.11 where  $i$  is described by

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$$I_1 = \frac{A_1 B_1 M}{U d}, \text{ } \mu\text{Ci} \quad (2.14)$$

where:

$A_1$  = activity released of  $i^{\text{th}}$  radionuclide during the month,  
 $\mu\text{Ci}$

$B_1$  = fish concentration factor of  $i^{\text{th}}$  radionuclide  $\frac{\mu\text{Ci/gm}}{\mu\text{Ci/ml}}$ , see  
attached Table 2.1.

$M$  = amount of fish eaten monthly ( $1.9 \times 10^3 \text{ gm}$ )

$U$  = total cooling tower blowdown during releases, ml.

$d$  = minimum diffuser pipe dilution (5)

The dose equation then becomes

$$Dg = \frac{4 \times 10^5}{U} \sum_{i=1}^{11} A_i \times B_i \times DCF_i \text{ mrem} \quad (2.15)$$

If these calculated monthly doses exceed limits specified in Section 2.3.1, then a more accurate and complete calculation will be done as described in Section 2.3.3. An annual check will be made to ensure that the monthly dose estimates account for at least 95 percent of the dose calculated by the method described in Section 2.3.3. If less than 95 percent of the dose has been estimated, a new list of principal isotopes will be prepared.

### 2.3.3 Annual Analysis

A complete analysis utilizing the total source release will be done at least annually (monthly if necessary). This analysis will replace previous estimates calculated in Section 2.3.2 and consists of the following approach. The dose to the  $j^{\text{th}}$  organ from  $n$  radionuclides,  $D_j$ , is described by

$$D_j = \sum_{i=1}^m D_{ij}, \text{ rem} \quad (2.16)$$

$$= \sum_{i=1}^m (DCF)_{ij} \times I_i, \text{ rem} \quad (2.17)$$

where:

$D_{ij}$  = dose to the  $j^{\text{th}}$  organ from the  $i^{\text{th}}$  radionuclide, rem.

$j$  = the organ of interest (bone, GI tract, thyroid, and total body).

$(DCF)_{ij}$  = adult ingestion dose commitment factor for the  $j^{\text{th}}$  organ from the  $i^{\text{th}}$  radionuclide, rem/ $\mu\text{Ci}$ , see attached Table 2.1.

$I_i$  for water ingestion is described by

$$I_i = \frac{A_i V n}{U d}, \mu\text{Ci} \quad (2.18)$$

and for fish ingestion  $I_i$  is described by

$$I_i = \frac{A_i B_i M}{U d}, \mu\text{Ci} \quad (2.19)$$

where:

$A_i$  = activity released of  $j^{\text{th}}$  radionuclide during the release period,  $\mu\text{Ci}$ .

$V$  = average rate of water consumption (730 ml/d).

$n$  = number of days during the release period (d).

$U$  = cooling tower blowdown during the release period, ml.

$B_i$  = fish concentration factor of the  $i^{\text{th}}$  radionuclide,  $\frac{\mu\text{Ci/gm}}{\mu\text{Ci/ml}}$

$M$  = amount of fish eaten monthly ( $1.9 \times 10^3$  gm).

$d$  = minimum diffuser pipe dilution (5).

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## 2.4 Operability of Liquid Radwaste Equipment

Specification 3.8.A.5 of the Radiological Effluent Technical Specifications requires that the liquid radwaste system shall be used to reduce the radioactive materials in liquid wastes prior to their discharge when the projected dose per unit due to liquid effluent releases to unrestricted areas (see Figure 2.1. ) when averaged over 31 days would exceed 0.06 mrem to the total body or 0.21 mrem to any organ. The following methodology will be implemented to assure compliance.

### 2.4.1 Release Limit

The liquid radwaste operability limit is an activity release limit based upon four years of operational releases excluding tritium. The curie limit is dependent upon the future operational mix being similar to past operational mix. The most restrictive pathway is to the GI tract by ingestion of fish. The individual dose from the operational source terms was calculated to be .04 mrem/mo. This dose is a factor of 5 below the operability limit of 0.21 mrem to any organ. The total activity released excluding tritium is 0.10 curies. The allowable release without exceeding 0.21 mrem/mo is 5 times 0.1 curies, or 0.50 curies/mo excluding tritium.

$$A_{\text{limit}} = 0.50 \text{ Ci/mo. excluding tritium}$$

The value of 0.50 Ci/mo will correspond to the limits specified in Section 2.4 if the mixture of isotopes is similar to the historical mixture.

POOR ORIGINAL

TABLE 2.1

DOSE CALCULATION DATA

NUCLIDE	RADIOL. HALF-LIFE (DAYS)	BIOLOGICAL HALF-LIFE (DAYS)	EFFECTIVE HALF-LIFE (DAYS)	HUMAN DOSE COMMITMENT FACTORS (HEP/UCI)				FISH CONCENTRATION FACT. STABLE		BIOLOG. HALF-LIFE (DAYS)
				BONE	GI TRACT	THYROID	TOTAL BODY	RAIOLLO.	RAIOLLO.	
H-3	4.44E-03	1.00E-01	9.90E-00	9.77E-05	9.77E-05	9.77E-05	9.77E-05	1.00E-00	1.00E-00	0.0
C-14	2.07E-04	1.00E-01	1.00E-01	2.85E-03	5.70E-04	5.70E-04	5.70E-04	4.55E-03	4.55E-03	0.0
HA-24	6.73E-01	1.10E-01	5.79E-01	1.73E-03	5.32E-02	1.73E-03	1.73E-03	1.00E-02	1.00E-02	0.0
P-32	1.43E-01	2.57E-02	1.35E-01	1.95E-01	1.24E-01	1.47E-03	1.47E-03	1.00E-03	1.00E-03	0.0
K-40	4.60E-11	5.80E-01	5.80E-01	3.45E-02	0.0	3.45E-02	3.45E-02	2.50E-03	2.50E-03	0.0
CR-51	2.70E-01	6.16E-02	2.66E-01	3.21E-06	1.71E-03	3.39E-06	3.21E-06	2.00E-02	2.00E-02	0.0
MN-54	3.03E-02	1.70E-01	1.61E-01	8.83E-04	2.43E-02	8.83E-04	8.83E-04	4.00E-02	4.00E-02	0.0
MN-56	1.07E-01	1.70E-01	1.05E-01	2.04E-05	4.68E-03	2.04E-05	2.04E-05	4.00E-02	4.00E-02	0.0
FE-55	9.57E-02	8.00E-02	4.74E-02	3.83E-04	1.13E-03	2.74E-04	2.74E-04	1.00E-02	1.00E-02	0.0
FE-57	4.58E-01	8.00E-02	4.51E-01	3.32E-03	5.54E-02	3.81E-03	3.81E-03	1.00E-02	1.00E-02	0.0
CO-58	7.13E-01	9.50E-00	8.38E-00	1.69E-03	3.29E-02	1.69E-03	1.69E-03	5.00E-01	4.75E-01	1.00E-02
CU-60	1.92E-03	9.50E-00	9.45E-00	4.73E-03	8.58E-02	4.73E-03	4.73E-03	5.00E-01	4.75E-01	1.00E-02
NI-65	1.07E-01	6.67E-02	1.07E-01	5.30E-04	3.16E-03	3.27E-05	3.27E-05	1.00E-02	1.00E-02	0.0
ZN-65	2.45E-02	9.33E-02	1.94E-02	3.01E-03	1.69E-02	7.13E-03	7.13E-03	2.00E-03	1.42E-03	1.00E-02
ZN-67M	5.75E-01	9.33E-02	5.75E-01	1.55E-04	2.91E-03	3.64E-05	3.64E-05	2.00E-03	1.14E-01	1.00E-02
ZN-67	3.46E-02	9.33E-02	3.96E-02	1.03E-05	9.97E-04	1.37E-06	1.37E-06	2.00E-03	7.42E-01	1.00E-02
BR-83	1.00E-01	8.00E-00	9.88E-02	3.55E-05	1.30E-03	3.55E-05	3.55E-05	4.20E-02	4.20E-02	0.0
BR-84	2.21E-02	8.00E-00	2.20E-02	6.04E-05	4.53E-03	6.04E-05	6.04E-05	4.20E-02	4.20E-02	0.0
BR-85	2.06E-03	8.00E-00	2.06E-03	5.17E-07	7.24E-05	5.17E-07	5.17E-07	4.20E-02	4.20E-02	0.0
KR-83M	7.75E-02	1.00E-00	7.19E-02	0.0	1.46E-04	0.0	0.0	1.00E-00	1.00E-00	0.0
KR-83M	1.83E-01	1.00E-00	1.55E-01	0.0	3.30E-03	0.0	0.0	1.00E-00	1.00E-00	0.0
KR-85	3.93E-03	1.00E-00	1.00E-00	0.0	4.62E-02	0.0	0.0	1.00E-00	1.00E-00	0.0
RB-88	1.24E-02	4.50E-01	1.24E-02	3.34E-05	3.09E-03	3.34E-05	3.34E-05	2.00E-03	2.00E-03	0.0
RB-89	1.07E-02	4.50E-01	1.07E-02	2.86E-05	1.76E-03	2.86E-05	2.86E-05	2.00E-03	2.00E-03	0.0
SR-89	5.27E-01	1.30E-04	5.25E-01	1.39E-01	1.04E-01	9.22E-03	9.22E-03	3.00E-01	1.04E-01	1.00E-02
SR-90	1.51E-04	1.30E-04	5.68E-03	1.17E-01	3.58E-02	1.76E-00	1.76E-00	3.00E-01	2.97E-01	1.00E-02
SI-91	4.03E-01	1.30E-04	4.03E-01	1.72E-03	2.06E-02	1.92E-04	1.92E-04	3.00E-01	1.25E-01	1.00E-02
SI-92	1.15E-01	1.30E-04	1.13E-01	9.17E-04	1.35E-03	6.89E-05	6.89E-05	3.00E-01	3.39E-02	1.00E-02
SR-94	5.56E-03	1.30E-04	5.56E-03	6.39E-05	1.89E-03	9.90E-06	8.90E-06	3.00E-01	1.67E-03	1.00E-02
Y-90	2.67E-01	1.40E-04	2.67E-01	9.62E-06	1.25E-01	2.57E-07	2.57E-07	2.50E-01	2.50E-01	0.0
Y-91M	3.47E-02	1.40E-04	3.47E-02	2.12E-08	5.06E-04	1.72E-09	1.72E-09	2.50E-01	2.50E-01	0.0
Y-91	5.85E-01	1.40E-04	5.86E-01	1.37E-04	1.10E-01	3.66E-06	3.66E-06	2.50E-01	2.50E-01	0.0
Y-92	1.47E-01	1.40E-04	1.47E-01	8.49E-07	1.27E-02	2.47E-08	2.47E-08	2.50E-01	2.50E-01	0.0
Y-93	4.29E-01	1.40E-04	4.29E-01	1.97E-06	3.51E-02	5.51E-08	5.51E-08	2.50E-01	2.50E-01	0.0
ZP-95	6.55E-01	4.50E-02	5.72E-01	2.54E-05	4.28E-02	6.38E-06	6.38E-06	3.33E-00	3.33E-00	0.0
ZR-97	7.03E-01	4.50E-02	7.07E-01	1.64E-06	4.79E-02	1.55E-07	1.55E-07	3.33E-00	3.33E-00	0.0
HB-95M	3.75E-00	7.60E-02	3.73E-00	5.40E-07	3.55E-02	2.88E-07	2.88E-07	3.00E-04	3.00E-04	0.0
HB-95	3.57E-01	7.60E-02	3.55E-01	5.12E-06	3.11E-02	1.83E-06	1.83E-06	3.00E-04	3.00E-04	0.0
HB-97	5.09E-02	7.60E-02	5.09E-02	4.90E-08	2.10E-03	4.60E-09	4.60E-09	3.00E-04	3.00E-04	0.0
PD-99	2.74E-00	5.30E-00	1.77E-00	8.47E-04	5.93E-02	8.47E-04	8.47E-04	1.00E-01	1.00E-01	0.0
TC-99M	2.52E-01	1.00E-00	2.01E-01	2.44E-07	6.09E-04	9.37E-06	9.37E-06	1.50E-01	1.50E-01	0.0
TC-99	7.74E-01	1.00E-00	1.00E-00	1.27E-04	1.89E-02	5.06E-05	5.06E-05	1.50E-01	1.50E-01	0.0
TC-101	9.93E-03	1.00E-00	9.83E-03	2.57E-07	7.94E-04	3.60E-06	3.60E-06	1.50E-01	1.50E-01	0.0
RC-103	3.96E-01	7.30E-00	6.16E-00	1.64E-04	2.55E-02	7.78E-05	7.78E-05	1.00E-01	1.00E-01	0.0
RIJ-106	3.60E-02	7.30E-00	7.16E-00	2.66E-03	2.67E-01	3.50E-04	3.50E-04	1.00E-01	1.00E-01	0.0

TABLE 2.1 (CONTINUED)

NUCLIDE	RADIOL, HALF-LIFE (DAYS)	BIOLOGICAL HALF-LIFE (DAYS)	EFFECTIVE HALF-LIFE (DAYS)	HUMAN DOSE COMMITMENT FACTORS (RHM/UCI)				FISH CONCENTRATION FACT, RADIOLO, (DAYS)		BIOLOG, HALF-LIFE (DAYS)
				BONE	GI TRACT	THYROID	TOTAL BUDY	STABLE	RADIOLO, (DAYS)	
RN-130	3.56E-02	7.30E-00	3.94E-02	1.67E-07	1.21E-04	4.79E-08	4.59E-08	1.00E-01	1.00E-01	0.0
AG-110H	2.53E-02	5.00E-00	4.90E-00	1.34E-04	9.27E-02	8.79E-05	8.73E-05	2.00E-00	2.00E-00	0.0
TE-125M	5.00E-01	1.50E-01	1.19E-01	2.52E-03	2.25E-02	8.15E-04	4.55E-04	4.00E-02	4.00E-02	0.0
TE-127M	1.02E-02	1.50E-01	1.32E-01	8.91E-03	1.56E-02	2.37E-03	1.12E-03	4.00E-02	4.00E-02	0.0
TE-127	3.92E-01	1.50E-01	3.82E-01	1.13E-04	6.76E-03	8.36E-05	2.44E-05	4.00E-02	4.00E-02	0.0
TE-129M	3.41E-01	1.50E-01	1.04E-01	1.14E-02	4.96E-02	3.96E-03	1.84E-03	4.00E-02	4.00E-02	0.0
TE-129	4.77E-02	1.50E-01	4.75E-02	3.00E-05	1.77E-03	2.32E-05	7.37E-06	4.00E-02	4.00E-02	0.0
TE-131M	1.25E-00	1.50E-01	1.15E-00	7.15E-04	3.61E-02	6.77E-04	4.89E-04	4.00E-02	4.00E-02	0.0
TE-131	1.74E-02	1.50E-01	1.72E-02	1.42E-05	1.79E-03	1.61E-05	6.44E-06	4.00E-02	4.00E-02	0.0
TE-132	3.24E-00	1.50E-01	2.66E-00	2.44E-03	2.21E-02	1.00E-03	1.50E-03	4.00E-02	4.00E-02	0.0
TE-134	2.22E-02	1.50E-01	2.91E-02	2.10E-05	8.93E-05	2.00E-05	1.57E-05	4.00E-02	4.00E-02	0.0
I-127	6.21E-09	1.30E-02	1.36E-02	3.10E-03	0.0	9.61E-00	1.24E-02	5.00E-01	3.00E-01	1.00E-00
I-131	8.05E-00	1.30E-02	7.61E-00	4.06E-03	4.44E-02	2.01E-00	3.52E-03	5.00E-01	4.5E-01	1.00E-00
I-132	9.62E-02	1.30E-02	9.41E-02	1.97E-04	4.25E-03	7.91E-02	1.57E-04	5.00E-01	4.30E-00	1.00E-00
I-133	6.60E-01	1.30E-02	8.41E-01	1.36E-03	3.70E-02	4.69E-01	7.51E-04	5.00E-01	2.29E-01	1.00E-00
I-134	3.61E-02	1.30E-02	3.61E-02	7.84E-05	3.40E-03	2.94E-02	7.47E-05	5.00E-01	1.74E-00	1.00E-00
I-135	2.78E-01	1.30E-02	2.77E-01	3.70E-04	1.17E-02	1.47E-01	3.98E-04	5.00E-01	1.09E-01	1.00E-00
XE-133H	2.26E-00	1.00E-00	6.23E-01	0.0	2.65E-02	0.0	0.0	1.00E-00	1.00E-00	0.0
XE-133	5.27E-00	1.00E-00	8.41E-01	0.0	2.58E-02	0.0	0.0	1.00E-00	1.00E-00	0.0
XE-135H	1.08E-02	1.00E-00	1.07E-02	0.0	3.29E-04	0.0	0.0	1.00E-00	1.00E-00	0.0
CS-137	3.83E-01	1.00E-00	2.77E-01	0.0	1.00E-02	0.0	0.0	1.00E-00	1.00E-00	0.0
CS-134	7.47E-02	7.00E-01	6.40E-01	5.49E-02	7.67E-02	1.20E-01	1.20E-01	2.00E-03	2.00E-03	1.00E-00
CS-135	1.15E-02	1.15E-02	1.15E-02	1.94E-02	0.0	0.0E-03	0.0E-03	2.00E-03	2.00E-03	1.00E-00
CS-137	1.17E-01	7.00E-01	1.15E-01	5.90E-03	8.77E-02	7.01E-02	2.03E-02	2.00E-03	1.86E-03	1.00E-00
CS-137	1.15E-04	7.00E-01	6.96E-01	7.47E-02	6.40E-02	7.24E-02	7.24E-02	2.00E-03	2.00E-03	1.00E-00
CS-138	2.24E-02	7.00E-01	2.24E-02	9.94E-06	2.61E-03	5.17E-05	5.72E-05	2.00E-03	4.30E-01	1.00E-00
PA-137	5.76E-02	6.50E-01	5.75E-02	1.05E-04	3.34E-03	3.07E-06	3.07E-06	4.00E-00	4.00E-00	0.0
PA-140	1.24E-01	6.50E-01	1.07E-01	1.61E-02	6.03E-02	1.23E-03	1.23E-03	4.00E-00	4.00E-00	0.0
LA-140	1.60E-00	5.00E-02	1.67E-00	1.90E-06	8.55E-02	3.09E-07	3.09E-07	2.50E-01	2.50E-01	0.0
LA-141	1.63E-01	5.00E-01	1.62E-01	3.90E-07	7.60E-03	2.01E-03	2.01E-03	2.50E-01	2.50E-01	0.0
CE-141	3.25E-01	5.63E-02	3.07E-01	9.32E-06	3.75E-02	7.12E-07	7.12E-07	2.50E-01	2.50E-01	0.0
CE-142	1.35E-01	5.63E-02	1.36E-01	5.53E-06	5.09E-02	3.56E-08	3.56E-08	2.50E-01	2.50E-01	0.0
CE-144	2.94E-02	5.63E-02	1.89E-02	4.90E-06	1.87E-02	2.84E-05	2.84E-05	2.50E-01	2.50E-01	0.0
PR-142	1.36E-01	7.50E-02	1.24E-01	9.23E-06	5.83E-02	4.60E-07	4.60E-07	2.50E-01	2.50E-01	0.0
PR-144	1.20E-02	7.50E-02	1.20E-02	3.04E-08	1.95E-03	1.54E-09	1.54E-09	2.50E-01	2.50E-01	0.0
ID-147	1.11E-01	6.56E-02	1.09E-01	6.37E-06	5.06E-02	4.25E-07	4.25E-07	2.50E-01	2.50E-01	0.0
PM-147	5.27E-02	6.56E-02	3.89E-02	7.60E-05	1.33E-02	2.89E-06	2.89E-06	2.50E-01	2.50E-01	0.0
PM-147	2.21E-00	6.56E-02	2.20E-00	1.54E-06	4.86E-02	8.87E-08	8.87E-08	2.50E-01	2.50E-01	0.0
PM-151	1.14E-00	6.56E-02	1.12E-00	6.74E-07	3.17E-02	5.91E-04	5.91E-04	2.50E-01	2.50E-01	0.0
SH-151	3.19E-04	6.56E-02	6.43E-02	6.07E-05	4.77E-03	1.56E-06	1.56E-06	2.50E-01	2.50E-01	0.0
SM-153	1.92E-00	6.56E-02	1.94E-00	1.01E-06	3.58E-02	6.66E-08	6.66E-08	2.50E-01	2.50E-01	0.0
SM-155	3.92E-01	6.56E-02	3.92E-01	6.63E-07	5.80E-03	5.33E-08	5.33E-08	2.50E-01	2.50E-01	0.0
EU-155	6.61E-02	6.56E-02	3.24E-02	5.72E-05	1.35E-02	3.35E-06	3.35E-06	2.50E-01	2.50E-01	0.0
EU-156	1.54E-01	6.56E-02	1.50E-01	1.31E-05	1.02E-01	1.65E-06	1.65E-06	2.50E-01	2.50E-01	0.0
W-157	9.96E-01	1.00E-00	4.99E-01	8.70E-05	2.54E-02	2.70E-05	2.70E-05	1.20E-03	1.20E-03	0.0
IP-232	2.35E-00	3.90E-04	2.35E-00	1.45E-06	3.10E-02	7.74E-08	7.74E-08	1.00E-01	1.00E-01	0.0

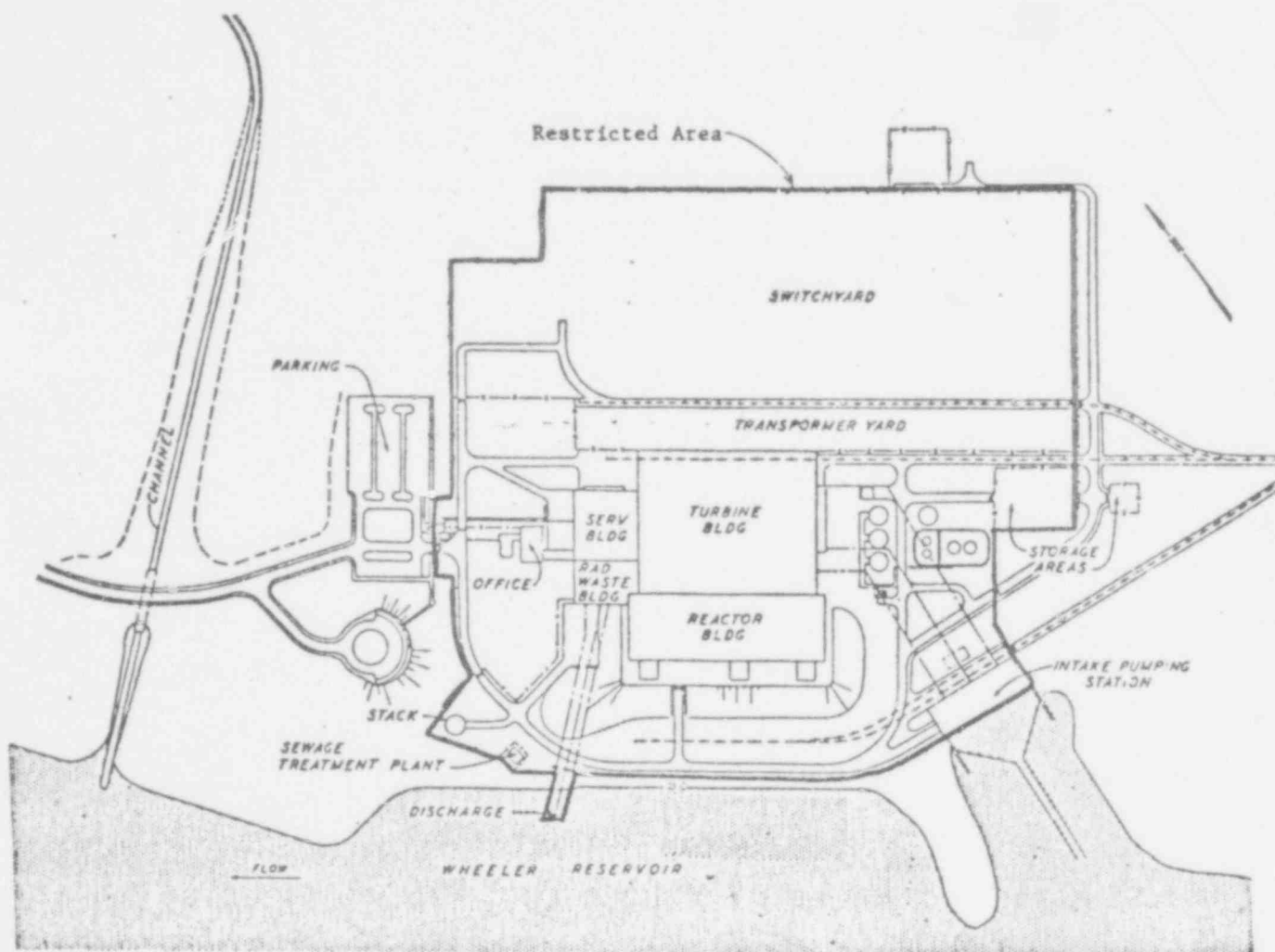


Figure 2.1--Assumed Liquid Effluent Restricted Area

POOR ORIGINAL

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3.0 Radiological Environmental Monitoring

3.1 Monitoring Program

An environmental radiological monitoring program shall be conducted

as described in Tables 3.1-1, 3.1-2 and 3.1-3, and in Figures 3.1-1, 3.1-2, 3.1-3, and 3.1-4. Results of this program shall be reported in accordance with Technical Specifications 6.7.1.d and 6.7.2.c.

The atmospheric environmental radiological monitoring program shall consist of 11 monitoring stations from which samples of air particulates, atmospheric radioiodine, rainwater, and heavy particle fallout shall be collected.

The terrestrial monitoring program shall consist of the collection of milk, soil, ground water, drinking water, and food crops. In addition, direct gamma radiation levels will be measured in the vicinity of the plant.

The reservoir sampling program shall consist of the collection of samples of surface water, sediment, and fish.

Deviations are permitted from the required sampling schedule if specimens are unobtainable due to hazardous conditions, sample unavailability, or to malfunction of sampling equipment. If the latter, every effort shall be made to complete corrective action prior to the end of the next sampling period.

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3.2

Detection Capabilities

Analytical techniques shall be such that the detection capabilities listed in Table 3.2-1 are achieved.

**POOR ORIGINAL** 302 055



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TABLE 3.1-1

ENVIRONMENTAL RADIOLOGICAL MONITORING

Exposure Pathway and/or Sample	Sample Locations*	Sampling and Collection Frequency	Type of Frequency of Analysis
AIRBORNE			
Particulates	4 samples from locations (in different sectors) at or near the site boundary (LM 1, 2, 3, & 5)	Continuous sampler operation with sample collection weekly	Gross beta following filter change composite (by location) monthly for gamma scan. Composite quarterly for $^{89}\text{Sr}$ , $^{90}\text{Sr}$ . If any filter indicates a gross beta concentration 1.0 pCi/m <sup>3</sup> greater than the average of the control stations, a gamma scan will be performed on the filter
Radioiodine	1 sample from the residence having the highest X/Q (LM-4)	Continuous sampler operation with filter collection weekly	$^{131}\text{I}$ weekly
Fallout	4 samples from communities approximately 10 miles distant from the plant (PM 1-4)	Heavy particle fallout collected continuously on gummed acetate paper with paper collection monthly	Gross beta monthly
Rainwater	2 samples from control locations greater than 10 miles from the plant (RM 1&2)	Rainwater collected continuously with composite sample analyzed monthly	Gamma scan, monthly
Soil	Samples from same locations as air particulates	Once per 3 years	Gamma scan, $^{89}\text{Sr}$ , $^{90}\text{Sr}$ once each 3 years

\*Sample locations are shown in Figures 3.1-1, 3.1-2, 3.1-3, and 3.1-4.

TABLE 3.1-1 (Continued)

Exposure Pathway and/or Sample	Sample Locations*	Quarterly	Sampling and Collection Frequency	Type and Frequency of Analysis
DIRECT	2 or more dosimeters placed at the air particulate sampling stations located greater than 5 miles from the plant (PM 1-4 and RM 1 & 2)			Gamma dose quarterly
	2 or more dosimeters placed at 8 locations (in different sectors) at or near the site boundary (Figure 3.1-2)			
WATERBORNE				
Surface (Figure 3.1-4)	TRM 305.0 TRM 293.5 TRM 285.2	Collected by automatic sequential-type sampler with composite sample taken monthly		Gamma scan monthly Composite for tritium, $^{90}\text{Sr}$ and $^{90}\text{Sr}$ quarterly
Ground (Figure 3.1-3)	1 sample adjacent to plant	Collected by automatic sequential-type sampler with composite sample taken monthly		Gamma scan monthly. Composite quarterly for tritium.
	1 sample from ground water source upgradient	Monthly grab sample		Gamma scan monthly. Composite quarterly for tritium
Drinking (Table 3.1-3) (Figure 3.1-4)	1 sample at the first potable surface water supply downstream from the plant (TRM 282.6)	Collected by automatic sequential-type sampler with composite sample taken monthly		Cross beta and gamma scan monthly. Composite quarterly for $^{90}\text{Sr}$ , $^{90}\text{Sr}$ , and tritium.

\*Sample locations are shown in Figures 3.1-1, 3.1-2, 3.1-3, and 3.1-4.

TABLE 3.1-1 (Continued)

<u>Exposure Pathway and/or Sample</u>	<u>Sample Location*</u>	<u>Sampling and Collection Frequency</u>	<u>Type and Frequency of Analysis</u>
	1 sample at the next 2 downstream potable surface water supplies (greater than 10 miles downstream) (TRM's 274.9 and 254.3)	Monthly grab sample	Gross beta and gamma scan monthly. Composite quarterly for tritium, $^{89}\text{Sr}$ , and $^{90}\text{Sr}$ .
	1 sample at a control location (TRM 306.0)	Monthly grab sample	
Sediment (Figure 3.1-4)	TRM 307.5 TRM 393.7 TRM 288.8 TRM 278.0	Semiannually	Gamma scan, $^{89}\text{Sr}$ , and $^{90}\text{Sr}$ analyses semiannually
INGESTION			
Milk (Figure 3.1-3)	1 sample from milk producing animals in each of 1-3 areas indicated by the cow census where doses are calculated to be highest. If samples are not available from an area, doses to that area will be estimated by projecting the doses from concentrations detected in milk from other sectors or by sampling vegeta- tion where milk is not avail- able	Semi-monthly when animals are on pasture. Monthly when animals are off pasture.	$^{131}\text{I}$ analysis semi-monthly or monthly on collection. Gamma scan, $^{89}\text{Sr}$ , and $^{90}\text{Sr}$ monthly.
	1 sample from a control location		

\*Sample locations are shown in Figures 3.1-1, 3.1-2, 3.1-3, and 3.1-4.

TABLE 3.1-1 (Continued)

Exposure Pathway  
and/or Sample

Fish	1 sample each of a commercial and a game species in Cuntersville Reservoir above the plant		
	1 sample each of a commercial and a game species in Wheeler Reservoir near the plant	Semiannually	Gamma scan semiannually.
	1 sample each of a commercial and a game species in Wilson Reservoir below the plant		
Food Products	1 sample each of principal food products grown at private gardens and/or farms in the immediate vicinity of the plant. Selection of locations to be based on the land use census.	Annually, at time of harvest. The types of foods available for sampling will vary. Following is a list of typical foods which may be available: cabbage and/or lettuce, corn, green beans, potatoes, and tomatoes.	Gamma scan on edible portion
	1 sample each of the same food products grown at control locations.		

\*Sample locations are shown in Figures 3.1-1, 3.1-2, 3.1-3, and 3.1-4.

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ATMOSPHERIC AND TERRESTRIAL MONITORING STATION LOCATIONSBROWNS FERRY NUCLEAR PLANT

	<u>Location and Approximate Distance and Direction from Plant</u>
LM-1 BF	1.0 mile N
LM-2 BF	0.9 miles NNE
LM-3 BF	1.0 miles NE
LM-4 BF	1.7 miles NNW
LM-5 BF	2.5 miles WSW
PM-1 BF (Rogersville, AL)	13.8 miles NW
PM-2 BF (Athens, AL)	10.9 miles NE
PM-3 BF (Decatur/Trinity, AL)	8.2 miles SSE
PM-4 BF (Courtland, AL)	10.5 miles WSW
RM-1 BF (Muscle Shoals, AL)	32.0 miles W
RM-2 BF (Lawrenceburg, TN)	40.5 miles NNW
Farm B	7.0 miles NNW
Farm S	4.8 miles N
Farm Bi	4.5 miles ENE
Farm L	5.8 miles ENE
Farm T	7.0 miles ENE
Farm N (control)	27 miles NW
Farm J (control)	40 miles NNW
Farm C (control)	32 miles N
Farm Ca (control)	32 miles W

TABLE 3.1-3

LISTING OF TENNESSEE RIVER SURFACE WATER SUPPLIES TO  
BE SAMPLED IN ENVIRONMENTAL MONITORING PROGRAM

<u>Supply</u>	<u>Source</u>	<u>Distance from Plant</u> <u>(miles)</u>
Courtland (Champion Paper Co.) <sup>a</sup>	Tennessee River (mile 282.6)	11.6
Decatur <sup>b</sup>	Tennessee River (mile 306.0)	12.0
Wheeler Hydro Plant	Tennessee River (mile 274.9)	19.1
Sheffield	Tennessee River (mile 254.3)	39.7

a. First potable water supply downstream of the plant. Sample collected automatically and analyzed monthly.

b. Decatur is upstream of the Browns Ferry Nuclear Plant.

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Table 3.2-1

DETECTION CAPABILITIES FOR ENVIRONMENTAL SAMPLE ANALYSIS

A. Specific Analyses

NOMINAL LOWER LIMIT OF DETECTION (LLD)\*

	Air Particulates pCi/m <sup>3</sup>	Charcoal pCi/m <sup>3</sup>	Fallout mCi/Km <sup>2</sup>	Water pCi/l	Vegetation and grain pCi/g, dry	Soil and Sediment pCi/g, dry	Fish, clam flesh, plankton, pCi/g, dry	Clam shells pCi/g, dry	Food, meat, poultry, pCi/Kgm, wet	Milk pCi/l
Total α					0.01				1.5	
Cross α	0.003		0.05	2.0	0.05	0.35	0.1	0.7		
Cross β	0.01			2.3	0.20	0.70	0.1	0.7	25	
<sup>3</sup> H				330						0.3
<sup>131</sup> I		0.01								10
<sup>90</sup> Sr	0.005			10	0.25	1.5	0.5	5.0	40	2
<sup>137</sup> Sr	0.001			2	0.05	0.3	0.1	1.0	8	

B. Gamma Analyses

NOMINAL LOWER LIMIT OF DETECTION (LLD)

	Air particulates		Water and milk		Vegetation and grain *		Soil and sediment		Fish		Clam flesh and plankton		Clam shells		Food, tomatoes potatoes, etc.)		Meat and poultry	
	pCi/m <sup>3</sup>		pCi/l		pCi/g, dry		pCi/g, dry		pCi/g, dry		pCi/g, dry		pCi/g, dry		pCi/Kgm, wet		pCi/Kgm, wet	
	NaI	Ge(Li)**	NaI	Ge(Li)	NaI	Ge(Li)	NaI	Ge(Li)	NaI	Ge(Li)	NaI	Ge(Li)	NaI	Ge(Li)	NaI	Ge(Li)	NaI	Ge(Li)
<sup>137</sup> Cs	0.03		8		0.55		0.35		0.35			0.35	0.35		38		90	
<sup>134</sup> Cs		0.02		33		0.22		0.06		0.06		0.35		0.06		33		40
<sup>51</sup> Cr	0.07	0.03	60	44	1.10	0.47	0.60	0.10	0.60	0.10	0.56	0.60	0.10	60	44	200	90	
<sup>131</sup> I	0.01	0.01	15	8	0.35	0.09	0.20	0.02	0.20	0.02	0.07	0.20	0.02	15	8	30	20	
<sup>106</sup> Ru	0.04		40		0.65		0.45		0.45			0.45		40		150		
<sup>106</sup> Ru		0.03		40		0.51		0.11		0.11		0.74		0.11		40	90	
<sup>132</sup> Cs	0.01	0.02	10	26	0.20	0.33	0.12	0.08	0.12	0.08	0.48	0.12	0.08	10	26	40	50	
<sup>137</sup> Cs	0.01	0.01	10	5	0.20	0.06	0.12	0.02	0.12	0.02	0.08	0.12	0.02	10	5	40	15	
<sup>90</sup> Zr-Nb	0.01		10		0.20		0.12		0.12			0.12		10		40		
<sup>90</sup> Zr		0.01		10		0.11		0.03		0.03		0.15		0.03		10	20	
<sup>90</sup> Nb		0.01		5		0.05		0.01		0.01		0.07		0.01		5	15	
<sup>56</sup> Co	0.02	0.01	15	5	0.23	0.05	0.20	0.01	0.20	0.01	0.07	0.20	0.01	15	5	55	15	
<sup>57</sup> Co	0.02	0.01	10	5	0.20	0.05	0.15	0.01	0.15	0.01	0.08	0.15	0.01	10	5	40	15	
<sup>65</sup> Zn	0.02	0.01	15	9	0.25	0.11	0.23	0.02	0.23	0.02	0.17	0.23	0.02	15	9	70	20	
<sup>60</sup> Co	0.01	0.01	10	5	0.17	0.06	0.11	0.01	0.11	0.01	0.08	0.11	0.01	10	5	30	15	
<sup>60</sup> Co	0.10		150		2.50		0.90		0.90			0.90		150		400		
<sup>137</sup> Ba-La	0.02		15		0.68		0.15		0.15			0.15		15		50		
<sup>137</sup> Ba		0.02		25		0.34		0.07		0.07		0.30		0.07		25	50	
<sup>137</sup> La		0.01		7		0.08		0.02		0.02		0.10		0.02		7	15	

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TABLE 3.2-1 (Continued)

TABLE NOTATIONS

- \* The NaI(Tl) LLD values are calculated by the method developed by Pasternak and Harley as described in HASL-300 and Nucl. Instr. Methods, 533-40 (1971). These LLD values are expected to vary depending on the activities of the components in the samples. These figures do not represent the LLD values achievable on a given sample. Water is counted in a 3.5-L Marinelli beaker. Vegetation, fish, soil, and sediment are counted in a 1-pint container as dry weight. The average dry weight is 120 grams for vegetation and 400-500 grams for soil sediment and fish. Meat and poultry are counted in a 1-pint container as dry weight, then corrected to wet weight using an average moisture content of 70%. Average dry weight is 250 grams. Air particulates are counted in a well crystal. The counting system consists of a multi-channel analyzer and either a 4" x 5" well NaI(Tl) crystal. The counting time is 4000 seconds. All calculations are performed by the least-squares computer program ALPHA-M. The assumption is made that the samples are analyzed within one week of the collection date.
- \*\* The Ge(Li) LLD values are calculated by the methods developed by Pasternak and Harley as described in HASL-300. These LLD values are expected to vary depending on the activities of the components in the samples. These figures do not represent the LLD values achievable on given samples. Water is counted in either a 0.5-L or 3.5-L Marinelli beaker. Solid samples such as soil, sediment, and clam shells are counted in a 0.5-L Marinelli beaker as dry weight. The average dry weight is 400-500 grams. Air filters and very small volume samples are counted in petrie dishes centered in the detector endcap. The counting system consists of a ND-4420 multichannel analyzer and either a 8%, 14%, or 18% Ge(Li) detector. The counting time is normally 8 hours. All spectral analysis is performed using the software provided with the ND-4420. The assumption is made that all samples are analyzed within one week of the collection date.
- a. All LLD values for isotopic separations are calculated by the method developed by Pasternak and Harley as described in HASL-300. Factors such as sample size, decay times, chemical yield, and counting efficiency may vary for a given sample; these variations may change the LLD value for the given sample. The assumption is made that all samples are analyzed within one week of the collection date.

The LLD is the smallest concentration of radioactive material in a sample that will be detected with 95% probability with 5% probability of falsely concluding that a blank observation represents a "real" signal.



TABLE 3.2-1 (Continued)

TABLE NOTATION

For a particular measurement system (which may include radiochemical separation):

$$LLD = \frac{4.66 s_b}{E \cdot V \cdot 2.22 \cdot y \cdot \exp(-\lambda \Delta t)}$$

where

LLD is the lower limit of detection as defined above (as pCi per unit mass or volume)

$s_b$  is the standard deviation of the background counting rate or of the counting rate of a blank sample as appropriate (as counts per minute)

E is the counting efficiency (as counts per transformation)

V is the sample size (in units of mass or volume)

2.22 is the number of transformation per minute per picocurie

Y is the fractional radiochemical yield (when applicable)

$\lambda$  is the radioactive decay constant for the particular radionuclide

$\Delta t$  is the elapsed time between sample collection (or end of the sample collection period) and time of counting

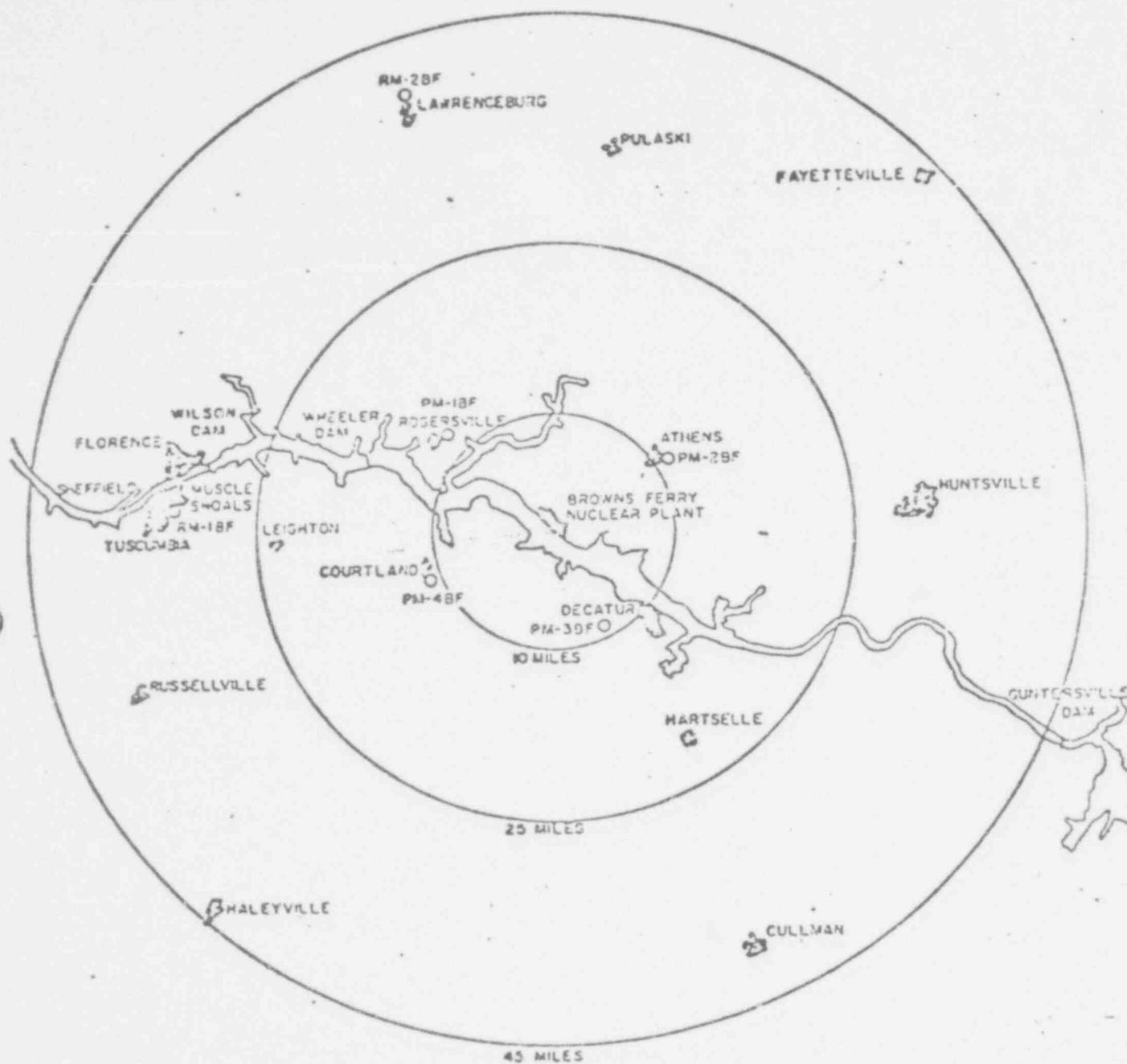
The value of  $s_b$  used in the calculation of the LLD for a detection system shall be based on the actual observed variance of the background counting rate or of the counting rate of the blank samples (as appropriate) rather than on an unverified theoretically predicted variance.

Figure 3.1-1

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Browns Ferry Nuclear Plant

ATMOSPHERIC AND TERRESTRIAL MONITORING NETWORK



○-ENVIRONMENTAL MONITORING STATION

NOTE THE FOLLOWING SAMPLES ARE COLLECTED FROM EACH STATION:

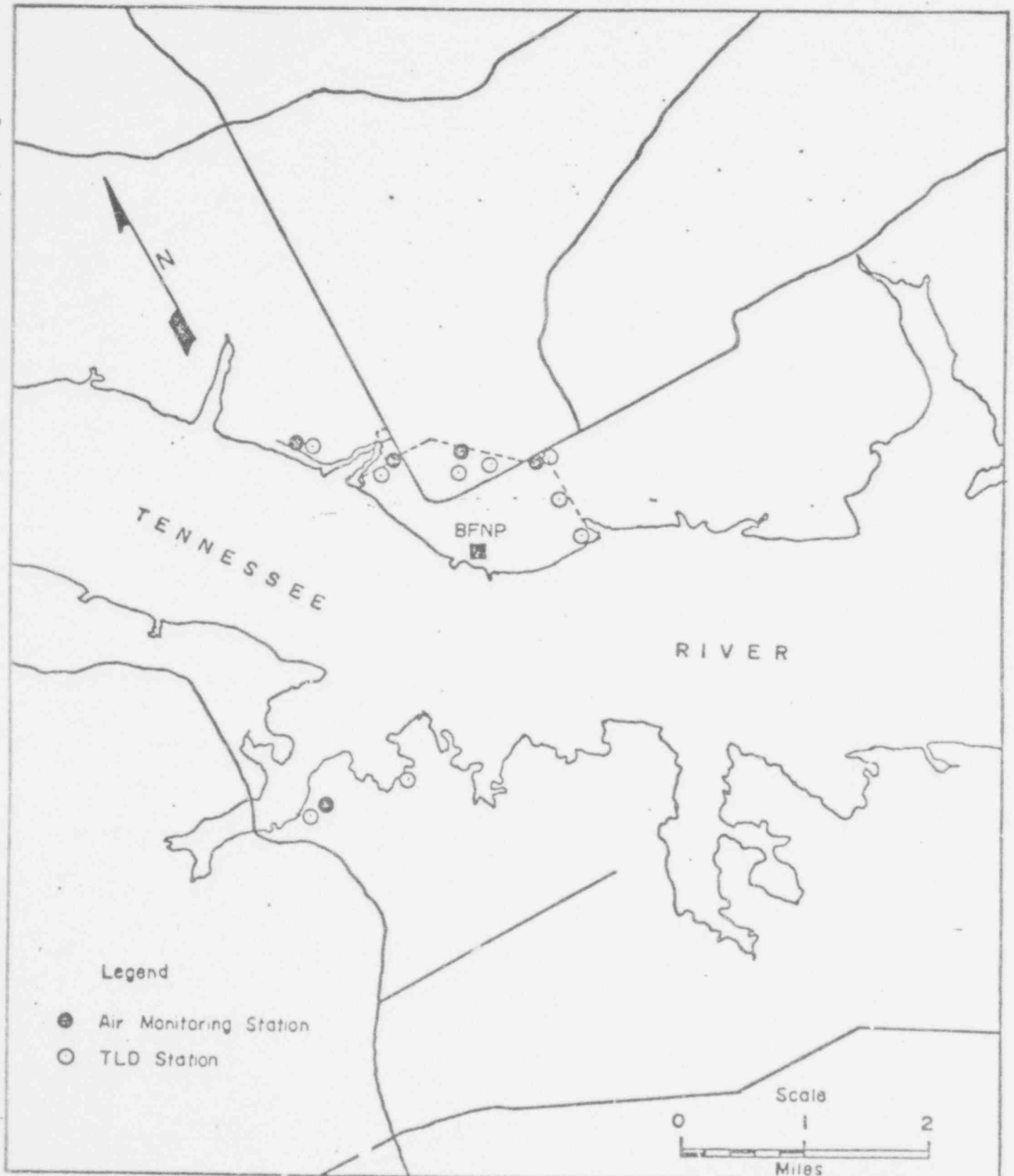
AIR PARTICULATES  
RADIOCINE  
HEAVY PARTICLE FALLOUT

RAINWATER  
SOIL  
VEGETATION

POOR ORIGINAL

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# LOCAL MONITORING STATIONS BROWNS FERRY NUCLEAR PLANT

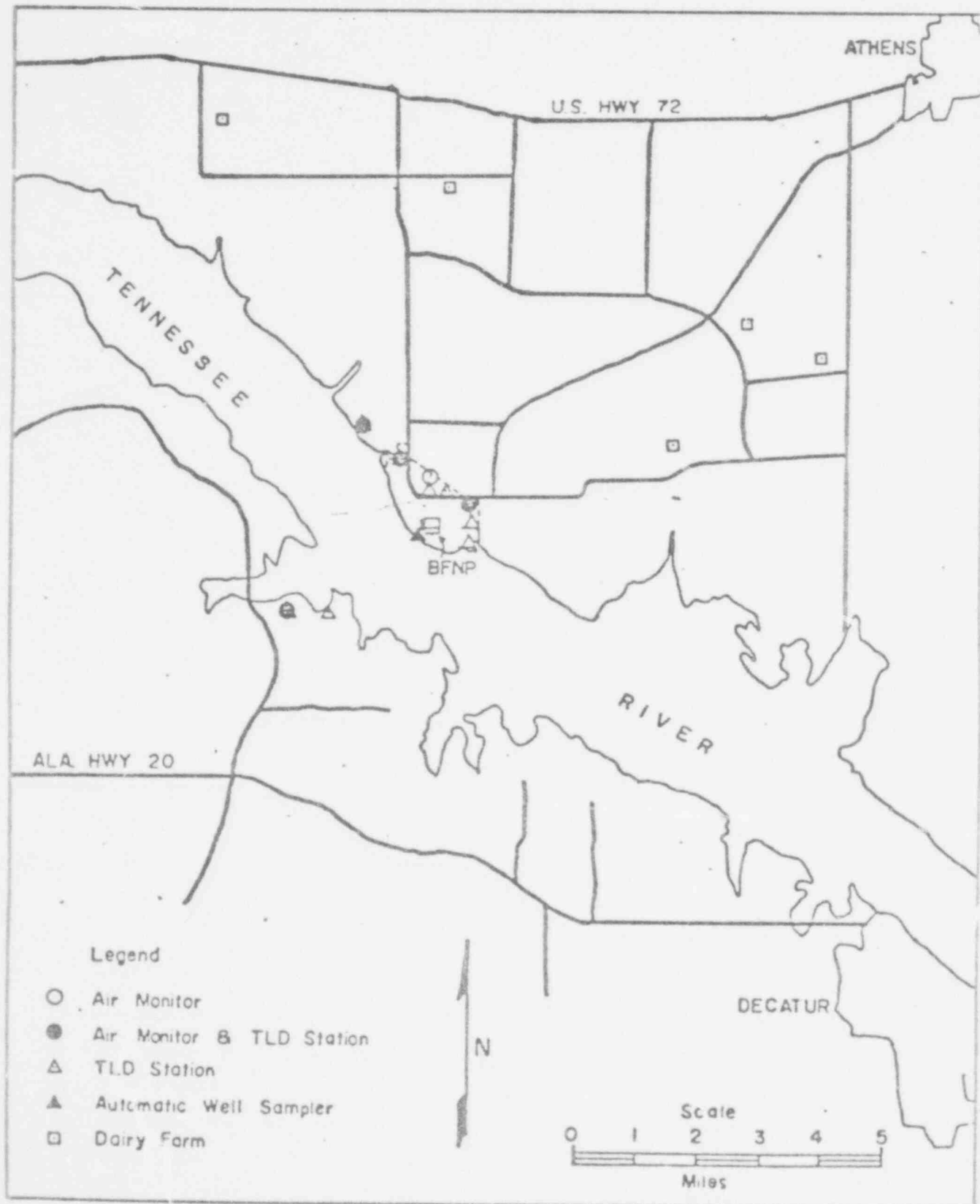


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POOR ORIGINAL

# LOCAL MONITORING STATIONS

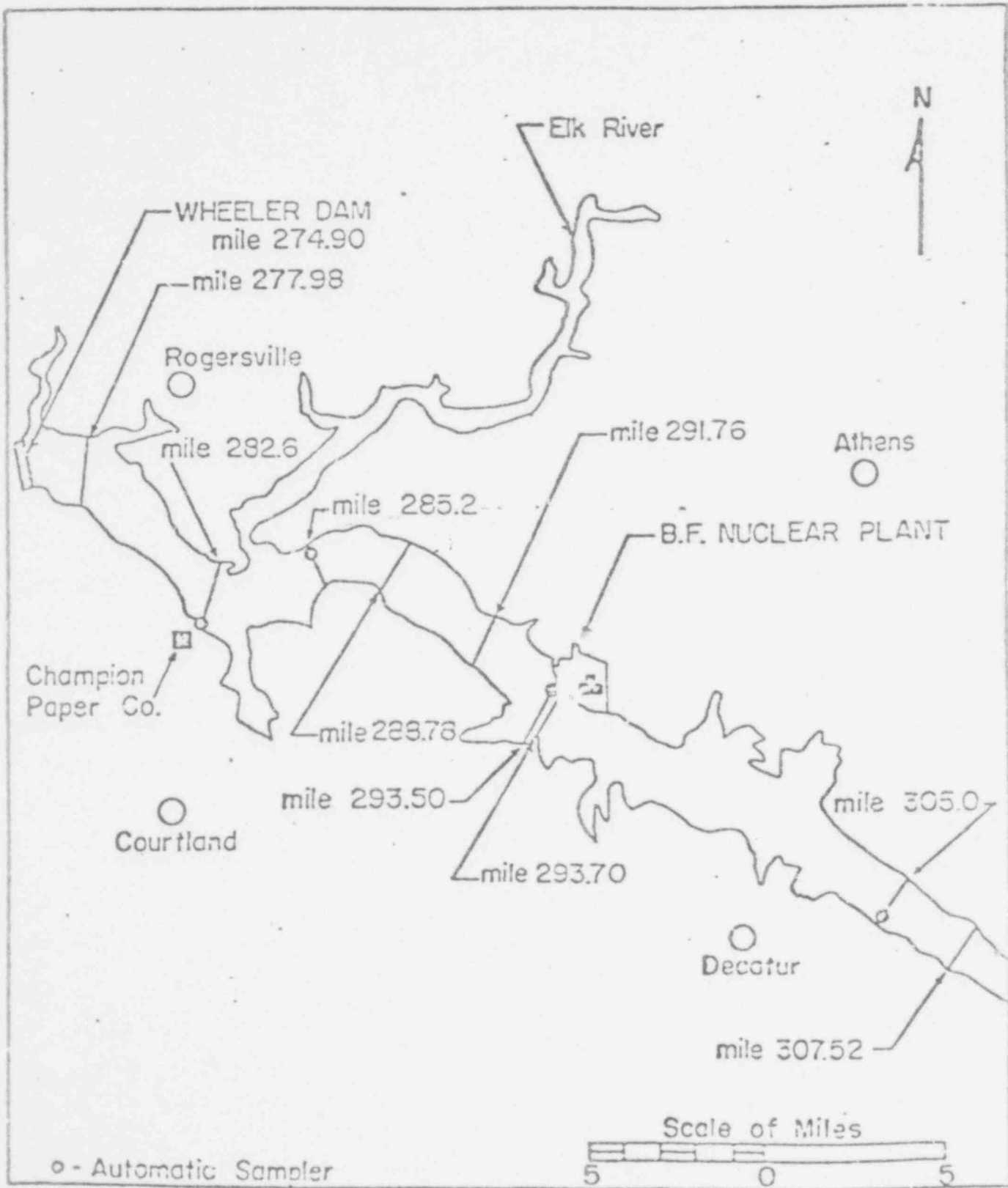
BROWNS FERRY NUCLEAR PLANT



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Browns Ferry Nuclear Plant

# RESERVOIR MONITORING NETWORK



## Appendix I

This appendix contains 10CFR20, Appendix B. The values in this appendix are the maximum permissible concentrations (MPC) in air and water above natural background.

POCA ORIGINAL

APPENDIX B

Concentrations in Air and Water Above Natural Background

(See notes at end of appendix)

Element (atomic number)	Isotope <sup>1</sup>	Table I		Table II	
		Column 1 Air ( $\mu\text{c}/\text{ml}$ )	Column 2 Water ( $\mu\text{c}/\text{ml}$ )	Column 1 Air ( $\mu\text{c}/\text{ml}$ )	Column 2 Water ( $\mu\text{c}/\text{ml}$ )
Actinium (89).....	Ac 227	$2 \times 10^{-11}$	$6 \times 10^{-12}$	$8 \times 10^{-11}$	$2 \times 10^{-11}$
	Ac 228	$3 \times 10^{-11}$	$9 \times 10^{-12}$	$9 \times 10^{-11}$	$2 \times 10^{-11}$
	Ac 228	$8 \times 10^{-11}$	$3 \times 10^{-11}$	$3 \times 10^{-11}$	$7 \times 10^{-12}$
Americium (95).....	Am 241	$2 \times 10^{-11}$	$3 \times 10^{-11}$	$6 \times 10^{-11}$	$9 \times 10^{-12}$
	Am 242m	$6 \times 10^{-11}$	$1 \times 10^{-11}$	$2 \times 10^{-11}$	$4 \times 10^{-12}$
	Am 242	$1 \times 10^{-11}$	$8 \times 10^{-12}$	$4 \times 10^{-11}$	$3 \times 10^{-12}$
Antimony (51).....	As 127	$3 \times 10^{-11}$	$3 \times 10^{-11}$	$9 \times 10^{-11}$	$9 \times 10^{-12}$
	As 128	$4 \times 10^{-11}$	$4 \times 10^{-11}$	$1 \times 10^{-11}$	$1 \times 10^{-11}$
	As 128	$5 \times 10^{-11}$	$4 \times 10^{-11}$	$2 \times 10^{-11}$	$4 \times 10^{-12}$
Argon (18).....	Ar 37	$6 \times 10^{-11}$	$1 \times 10^{-11}$	$2 \times 10^{-11}$	$1 \times 10^{-11}$
	Ar 41	$2 \times 10^{-11}$	$1 \times 10^{-11}$	$9 \times 10^{-11}$	$1 \times 10^{-11}$
	Ar 72	$3 \times 10^{-11}$	$3 \times 10^{-11}$	$1 \times 10^{-11}$	$1 \times 10^{-11}$
Arsenic (33).....	As 74	$3 \times 10^{-11}$	$3 \times 10^{-11}$	$4 \times 10^{-11}$	$2 \times 10^{-11}$
	As 76	$1 \times 10^{-11}$	$6 \times 10^{-12}$	$2 \times 10^{-11}$	$2 \times 10^{-11}$
	As 77	$1 \times 10^{-11}$	$6 \times 10^{-12}$	$2 \times 10^{-11}$	$2 \times 10^{-11}$
Astatine (85).....	At 211	$4 \times 10^{-11}$	$2 \times 10^{-11}$	$2 \times 10^{-11}$	$2 \times 10^{-11}$
	At 213	$3 \times 10^{-11}$	$3 \times 10^{-11}$	$4 \times 10^{-11}$	$2 \times 10^{-11}$
	At 215	$1 \times 10^{-11}$	$3 \times 10^{-11}$	$1 \times 10^{-11}$	$2 \times 10^{-11}$
Barium (56).....	Ba 131	$4 \times 10^{-11}$	$3 \times 10^{-11}$	$1 \times 10^{-11}$	$2 \times 10^{-11}$
	Ba 140	$1 \times 10^{-11}$	$8 \times 10^{-12}$	$4 \times 10^{-11}$	$3 \times 10^{-12}$
	Ba 140	$4 \times 10^{-11}$	$7 \times 10^{-12}$	$1 \times 10^{-11}$	$2 \times 10^{-12}$
Berkelium (97).....	Bk 249	$9 \times 10^{-11}$	$2 \times 10^{-11}$	$3 \times 10^{-11}$	$6 \times 10^{-12}$
	Bk 250	$1 \times 10^{-11}$	$2 \times 10^{-11}$	$4 \times 10^{-11}$	$2 \times 10^{-12}$
	Bk 250	$1 \times 10^{-11}$	$6 \times 10^{-12}$	$3 \times 10^{-11}$	$2 \times 10^{-12}$
Beryllium (4).....	Be 7	$6 \times 10^{-11}$	$3 \times 10^{-11}$	$2 \times 10^{-11}$	$2 \times 10^{-12}$
	Be 9	$1 \times 10^{-11}$	$3 \times 10^{-11}$	$4 \times 10^{-11}$	$2 \times 10^{-12}$
	Be 10	$2 \times 10^{-11}$	$1 \times 10^{-11}$	$3 \times 10^{-11}$	$3 \times 10^{-12}$
Bismuth (83).....	Bi 209	$2 \times 10^{-11}$	$2 \times 10^{-11}$	$6 \times 10^{-11}$	$6 \times 10^{-12}$
	Bi 210	$6 \times 10^{-11}$	$1 \times 10^{-11}$	$2 \times 10^{-11}$	$4 \times 10^{-12}$
	Bi 210	$6 \times 10^{-11}$	$1 \times 10^{-11}$	$2 \times 10^{-11}$	$4 \times 10^{-12}$

PART 20 • STANDARDS FOR PROTECTION AGAINST

APPENDIX B

Concentrations in Air and Water Above Natural Background—Continued

(See notes at end of appendix)

Element (atomic number)	Isotope <sup>1</sup>	Table I		Table II	
		Column 1 Air ( $\mu\text{c}/\text{ml}$ )	Column 2 Water ( $\mu\text{c}/\text{ml}$ )	Column 1 Air ( $\mu\text{c}/\text{ml}$ )	Column 2 Water ( $\mu\text{c}/\text{ml}$ )
Bromine (35).....	Br 82	$1 \times 10^{-11}$	$8 \times 10^{-12}$	$1 \times 10^{-11}$	$3 \times 10^{-12}$
	Br 82	$3 \times 10^{-11}$	$1 \times 10^{-11}$	$3 \times 10^{-11}$	$4 \times 10^{-12}$
	Br 82	$5 \times 10^{-11}$	$3 \times 10^{-11}$	$3 \times 10^{-11}$	$3 \times 10^{-12}$
Cadmium (48).....	Cd 109	$7 \times 10^{-11}$	$5 \times 10^{-11}$	$3 \times 10^{-11}$	$2 \times 10^{-12}$
	Cd 115m	$4 \times 10^{-11}$	$7 \times 10^{-12}$	$1 \times 10^{-11}$	$3 \times 10^{-12}$
	Cd 115	$4 \times 10^{-11}$	$7 \times 10^{-12}$	$1 \times 10^{-11}$	$3 \times 10^{-12}$
Cesium (55).....	Cs 132	$2 \times 10^{-11}$	$1 \times 10^{-11}$	$4 \times 10^{-11}$	$3 \times 10^{-12}$
	Cs 134	$3 \times 10^{-11}$	$3 \times 10^{-11}$	$4 \times 10^{-11}$	$3 \times 10^{-12}$
	Cs 134	$3 \times 10^{-11}$	$3 \times 10^{-11}$	$4 \times 10^{-11}$	$3 \times 10^{-12}$
Chlorine (17).....	Cl 35	$9 \times 10^{-11}$	$7 \times 10^{-12}$	$3 \times 10^{-11}$	$2 \times 10^{-12}$
	Cl 36	$4 \times 10^{-11}$	$2 \times 10^{-11}$	$1 \times 10^{-11}$	$9 \times 10^{-12}$
	Cl 38	$2 \times 10^{-11}$	$1 \times 10^{-11}$	$2 \times 10^{-11}$	$3 \times 10^{-12}$
Chromium (24).....	Cr 51	$1 \times 10^{-11}$	$3 \times 10^{-12}$	$1 \times 10^{-11}$	$3 \times 10^{-12}$
	Cr 51	$1 \times 10^{-11}$	$3 \times 10^{-12}$	$1 \times 10^{-11}$	$3 \times 10^{-12}$
	Cr 51	$1 \times 10^{-11}$	$3 \times 10^{-12}$	$1 \times 10^{-11}$	$3 \times 10^{-12}$







## APPENDIX B

**COPY**

(See notes at end of appendix.)

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## APPENDIX B

## APPENDIX B

Concentrations in Air and Water Above Natural Background—Continued

Conservation in Air and Water Above National Background - CanHabitat

(See notes at end of appendix)

(See notes at end of appendix)

Element (atomic number)	Isotope	Table I		Table II	
		Column 1 Air ( $\mu\text{e}/\text{ml}$ )	Column 2 Water ( $\mu\text{e}/\text{ml}$ )	Column 1 Air ( $\mu\text{e}/\text{ml}$ )	Column 2 Water ( $\mu\text{e}/\text{ml}$ )
Technetium (43).....	Tc 96m	$8 \times 10^{-3}$	$4 \times 10^{-1}$	$3 \times 10^{-4}$	$1 \times 10^{-3}$
	Tc 96	$2 \times 10^{-3}$	$3 \times 10^{-1}$	$1 \times 10^{-3}$	$1 \times 10^{-3}$
	Tc 97m	$6 \times 10^{-7}$	$3 \times 10^{-3}$	$2 \times 10^{-6}$	$1 \times 10^{-4}$
	Tc 97	$2 \times 10^{-7}$	$1 \times 10^{-3}$	$8 \times 10^{-8}$	$5 \times 10^{-4}$
	Tc 98m	$2 \times 10^{-6}$	$1 \times 10^{-3}$	$8 \times 10^{-6}$	$4 \times 10^{-4}$
	Tc 98	$2 \times 10^{-7}$	$5 \times 10^{-3}$	$5 \times 10^{-7}$	$2 \times 10^{-4}$
	Tc 99m	$1 \times 10^{-3}$	$5 \times 10^{-3}$	$4 \times 10^{-7}$	$2 \times 10^{-3}$
	Tc 99	$3 \times 10^{-7}$	$2 \times 10^{-3}$	$1 \times 10^{-6}$	$8 \times 10^{-4}$
	Tc 100m	$4 \times 10^{-3}$	$2 \times 10^{-3}$	$1 \times 10^{-4}$	$6 \times 10^{-3}$
	Tc 100	$1 \times 10^{-3}$	$8 \times 10^{-3}$	$5 \times 10^{-7}$	$3 \times 10^{-3}$
Technetium (52).....	Tc 123m	$6 \times 10^{-6}$	$5 \times 10^{-3}$	$2 \times 10^{-6}$	$2 \times 10^{-4}$
	Tc 127m	$1 \times 10^{-7}$	$3 \times 10^{-3}$	$1 \times 10^{-8}$	$2 \times 10^{-4}$
	Tc 127	$1 \times 10^{-7}$	$2 \times 10^{-3}$	$4 \times 10^{-8}$	$1 \times 10^{-4}$
	Tc 129m	$2 \times 10^{-6}$	$7 \times 10^{-3}$	$5 \times 10^{-6}$	$4 \times 10^{-3}$
	Tc 129	$2 \times 10^{-6}$	$8 \times 10^{-3}$	$1 \times 10^{-6}$	$3 \times 10^{-4}$
	Tc 129m	$9 \times 10^{-7}$	$5 \times 10^{-3}$	$3 \times 10^{-8}$	$2 \times 10^{-3}$
	Tc 129	$8 \times 10^{-8}$	$1 \times 10^{-3}$	$2 \times 10^{-8}$	$2 \times 10^{-3}$
	Tc 131m	$4 \times 10^{-6}$	$2 \times 10^{-3}$	$1 \times 10^{-7}$	$8 \times 10^{-4}$
	Tc 132	$2 \times 10^{-7}$	$1 \times 10^{-3}$	$1 \times 10^{-8}$	$6 \times 10^{-3}$
	Tc 132	$2 \times 10^{-7}$	$6 \times 10^{-3}$	$7 \times 10^{-8}$	$4 \times 10^{-3}$
Technetium (63).....	Tc 160	$1 \times 10^{-7}$	$1 \times 10^{-3}$	$3 \times 10^{-8}$	$4 \times 10^{-3}$
	Tc 160	$3 \times 10^{-6}$	$1 \times 10^{-3}$	$1 \times 10^{-6}$	$4 \times 10^{-3}$
	Tc 200	$2 \times 10^{-6}$	$1 \times 10^{-3}$	$9 \times 10^{-7}$	$4 \times 10^{-4}$
	Tc 201	$1 \times 10^{-6}$	$7 \times 10^{-3}$	$4 \times 10^{-6}$	$2 \times 10^{-4}$
	Tc 201	$2 \times 10^{-6}$	$9 \times 10^{-3}$	$7 \times 10^{-6}$	$3 \times 10^{-4}$
	Tc 202	$9 \times 10^{-7}$	$5 \times 10^{-3}$	$3 \times 10^{-6}$	$2 \times 10^{-4}$
	Tc 202	$8 \times 10^{-7}$	$4 \times 10^{-3}$	$3 \times 10^{-6}$	$1 \times 10^{-4}$
	Tc 204	$2 \times 10^{-7}$	$2 \times 10^{-3}$	$8 \times 10^{-7}$	$7 \times 10^{-4}$
	Tc 204	$4 \times 10^{-7}$	$2 \times 10^{-3}$	$5 \times 10^{-7}$	$1 \times 10^{-4}$
	Tc 204	$3 \times 10^{-6}$	$2 \times 10^{-3}$	$9 \times 10^{-6}$	$6 \times 10^{-4}$
Technetium (90).....	Tc 227	$3 \times 10^{-6}$	$2 \times 10^{-3}$	$1 \times 10^{-6}$	$2 \times 10^{-4}$
	Tc 227	$3 \times 10^{-10}$	$5 \times 10^{-4}$	$1 \times 10^{-11}$	$2 \times 10^{-8}$
	Tc 228	$2 \times 10^{-10}$	$5 \times 10^{-4}$	$6 \times 10^{-11}$	$2 \times 10^{-8}$
	Tc 228	$8 \times 10^{-11}$	$2 \times 10^{-4}$	$3 \times 10^{-11}$	$7 \times 10^{-8}$
	Tc 230	$6 \times 10^{-11}$	$4 \times 10^{-4}$	$2 \times 10^{-11}$	$1 \times 10^{-8}$
	Tc 230	$2 \times 10^{-11}$	$3 \times 10^{-4}$	$8 \times 10^{-11}$	$2 \times 10^{-8}$
	Tc 231	$1 \times 10^{-11}$	$5 \times 10^{-4}$	$3 \times 10^{-11}$	$2 \times 10^{-8}$
	Tc 231	$1 \times 10^{-11}$	$7 \times 10^{-4}$	$5 \times 10^{-11}$	$2 \times 10^{-8}$
	Tc 232	$1 \times 10^{-11}$	$3 \times 10^{-4}$	$4 \times 10^{-11}$	$2 \times 10^{-8}$
	Tc 232	$3 \times 10^{-11}$	$5 \times 10^{-4}$	$1 \times 10^{-11}$	$2 \times 10^{-8}$
Technetium (81).....	Tc natural	$3 \times 10^{-11}$	$3 \times 10^{-4}$	$1 \times 10^{-11}$	$1 \times 10^{-8}$
	Tc natural	$2 \times 10^{-11}$	$3 \times 10^{-4}$	$1 \times 10^{-11}$	$1 \times 10^{-8}$

Element (atomic number)	Isotope	Table I		Table II	
		Column 1 Air ( $\mu\text{e}/\text{ml}$ )	Column 2 Water ( $\mu\text{e}/\text{ml}$ )	Column 1 Air ( $\mu\text{e}/\text{ml}$ )	Column 2 Water ( $\mu\text{e}/\text{ml}$ )
Thorium (90).....	Th 234	$6 \times 10^{-8}$	$3 \times 10^{-6}$	$2 \times 10^{-7}$	$2 \times 10^{-5}$
	Th 230	$3 \times 10^{-8}$	$3 \times 10^{-6}$	$1 \times 10^{-7}$	$2 \times 10^{-5}$
	Th 232	$4 \times 10^{-8}$	$1 \times 10^{-6}$	$1 \times 10^{-9}$	$3 \times 10^{-8}$
	Th 234	$2 \times 10^{-6}$	$1 \times 10^{-8}$	$1 \times 10^{-9}$	$5 \times 10^{-8}$
Thallium (81).....	Tm 171	$1 \times 10^{-7}$	$1 \times 10^{-8}$	$4 \times 10^{-9}$	$3 \times 10^{-8}$
	Tm 173	$2 \times 10^{-7}$	$1 \times 10^{-8}$	$6 \times 10^{-9}$	$2 \times 10^{-8}$
	Tm 175	$4 \times 10^{-7}$	$2 \times 10^{-8}$	$1 \times 10^{-8}$	$9 \times 10^{-8}$
	Tm 177	$2 \times 10^{-7}$	$2 \times 10^{-8}$	$1 \times 10^{-8}$	$9 \times 10^{-8}$
Tin (50).....	Sn 113	$3 \times 10^{-7}$	$2 \times 10^{-8}$	$1 \times 10^{-8}$	$9 \times 10^{-8}$
	Sn 115	$3 \times 10^{-7}$	$2 \times 10^{-8}$	$2 \times 10^{-8}$	$8 \times 10^{-8}$
	Sn 117	$1 \times 10^{-7}$	$5 \times 10^{-8}$	$4 \times 10^{-8}$	$2 \times 10^{-8}$
	Sn 119	$8 \times 10^{-8}$	$3 \times 10^{-8}$	$3 \times 10^{-8}$	$2 \times 10^{-8}$
Tungsten (Wolfram) (74).....	W 181	$2 \times 10^{-7}$	$1 \times 10^{-8}$	$8 \times 10^{-8}$	$4 \times 10^{-8}$
	W 183	$1 \times 10^{-7}$	$1 \times 10^{-8}$	$4 \times 10^{-8}$	$1 \times 10^{-8}$
	W 185	$8 \times 10^{-7}$	$2 \times 10^{-8}$	$2 \times 10^{-8}$	$1 \times 10^{-8}$
	W 187	$4 \times 10^{-7}$	$2 \times 10^{-8}$	$2 \times 10^{-8}$	$7 \times 10^{-8}$
Uranium (92).....	U 230	$3 \times 10^{-10}$	$1 \times 10^{-6}$	$1 \times 10^{-11}$	$3 \times 10^{-8}$
	U 232	$1 \times 10^{-10}$	$8 \times 10^{-6}$	$4 \times 10^{-11}$	$3 \times 10^{-8}$
	U 233	$3 \times 10^{-11}$	$8 \times 10^{-6}$	$9 \times 10^{-11}$	$3 \times 10^{-8}$
	U 234	$1 \times 10^{-10}$	$9 \times 10^{-6}$	$2 \times 10^{-11}$	$3 \times 10^{-8}$
Vanadium (23).....	V 48	$2 \times 10^{-7}$	$8 \times 10^{-8}$	$2 \times 10^{-8}$	$3 \times 10^{-8}$
	V 50	$4 \times 10^{-7}$	$8 \times 10^{-8}$	$2 \times 10^{-8}$	$3 \times 10^{-8}$
	V 51	$2 \times 10^{-7}$	$8 \times 10^{-8}$	$2 \times 10^{-8}$	$3 \times 10^{-8}$
	V 52	$4 \times 10^{-7}$	$8 \times 10^{-8}$	$2 \times 10^{-8}$	$3 \times 10^{-8}$
Xenon (54).....	Xe 131m	$2 \times 10^{-11}$	Sub	$4 \times 10^{-11}$	$1 \times 10^{-11}$
	Xe 133	$1 \times 10^{-11}$	Sub	$3 \times 10^{-11}$	$1 \times 10^{-11}$
	Xe 133m	$1 \times 10^{-11}$	Sub	$3 \times 10^{-11}$	$2 \times 10^{-11}$
	Xe 135	$4 \times 10^{-11}$	Sub	$1 \times 10^{-11}$	$2 \times 10^{-11}$
Yttrium (39).....	Yb 175	$7 \times 10^{-11}$	$3 \times 10^{-11}$	$2 \times 10^{-11}$	$1 \times 10^{-11}$
	Y 89	$6 \times 10^{-11}$	$3 \times 10^{-11}$	$2 \times 10^{-11}$	$1 \times 10^{-11}$
	Y 90	$1 \times 10^{-11}$	$3 \times 10^{-11}$	$2 \times 10^{-11}$	$1 \times 10^{-11}$
	Y 91	$2 \times 10^{-11}$	$3 \times 10^{-11}$	$2 \times 10^{-11}$	$1 \times 10^{-11}$
Zinc (30).....	Zn 64	$4 \times 10^{-11}$	$3 \times 10^{-11}$	$2 \times 10^{-11}$	$1 \times 10^{-11}$
	Zn 66	$1 \times 10^{-11}$	$3 \times 10^{-11}$	$2 \times 10^{-11}$	$1 \times 10^{-11}$
	Zn 68	$2 \times 10^{-11}$	$3 \times 10^{-11}$	$2 \times 10^{-11}$	$1 \times 10^{-11}$
	Zn 70	$4 \times 10^{-11}$	$3 \times 10^{-11}$	$2 \times 10^{-11}$	$1 \times 10^{-11}$

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## APPENDIX B

## Concentrations in Air and Water Above Natural Background - Continued

(See notes at end of appendix)

Element (atomic number)	Isotope <sup>1</sup>	Table I		Table II	
		Column 1 Air ( $\mu\text{Ci}/\text{ml}$ )	Column 2 Water ( $\mu\text{Ci}/\text{ml}$ )	Column 1 Air ( $\mu\text{Ci}/\text{ml}$ )	Column 2 Water ( $\mu\text{Ci}/\text{ml}$ )
Zinc (30)	Zn 63	$1 \times 10^{-7}$	$3 \times 10^{-3}$	$4 \times 10^{-9}$	$1 \times 10^{-4}$
		$6 \times 10^{-8}$	$5 \times 10^{-3}$	$2 \times 10^{-9}$	$2 \times 10^{-4}$
	Zn 69m	$4 \times 10^{-7}$	$2 \times 10^{-3}$	$1 \times 10^{-8}$	$7 \times 10^{-3}$
		$3 \times 10^{-7}$	$2 \times 10^{-3}$	$1 \times 10^{-8}$	$6 \times 10^{-3}$
Zincium (40)	Zn 69	$7 \times 10^{-7}$	$5 \times 10^{-3}$	$2 \times 10^{-7}$	$2 \times 10^{-3}$
		$9 \times 10^{-8}$	$5 \times 10^{-3}$	$3 \times 10^{-7}$	$2 \times 10^{-3}$
	Zr 93	$1 \times 10^{-7}$	$2 \times 10^{-3}$	$4 \times 10^{-9}$	$8 \times 10^{-4}$
		$3 \times 10^{-7}$	$2 \times 10^{-3}$	$1 \times 10^{-8}$	$8 \times 10^{-4}$
	Zr 95	$1 \times 10^{-7}$	$2 \times 10^{-3}$	$4 \times 10^{-9}$	$6 \times 10^{-4}$
		$3 \times 10^{-8}$	$2 \times 10^{-3}$	$1 \times 10^{-8}$	$6 \times 10^{-4}$
Zr 97		$1 \times 10^{-7}$	$5 \times 10^{-4}$	$4 \times 10^{-9}$	$2 \times 10^{-3}$
		$9 \times 10^{-8}$	$5 \times 10^{-4}$	$3 \times 10^{-9}$	$2 \times 10^{-3}$
	Sub	$1 \times 10^{-9}$	.....	$3 \times 10^{-9}$	.....
Any single radionuclide not listed above with decay mode other than alpha emission or spontaneous fission and with radioactive half-life less than 2 hours		$3 \times 10^{-9}$	$9 \times 10^{-3}$	$1 \times 10^{-10}$	$3 \times 10^{-4}$
		.....	.....	.....	.....
Any single radionuclide not listed above with decay mode other than alpha emission or spontaneous fission and with radioactive half-life greater than 2 hours		$6 \times 10^{-10}$	$4 \times 10^{-7}$	$2 \times 10^{-11}$	$3 \times 10^{-5}$
		.....	.....	.....	.....
Any single radionuclide not listed above which decays by alpha emission or spontaneous fission		.....	.....	.....	.....
		.....	.....	.....	.....

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