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November 20, 1979

Mr. William Kane  
Bulletins & Orders Task Force  
U.S. Nuclear Regulatory Commission  
Washington, D. C. 20555

Dear Mr. Kane:

Subject: Bulletins and Orders Task Force  
Long Term Systems Information

- Reference:
- (a) Division of Operating Reactors Letter dated 7/17/79, Additional Information Required for NRC Staff Generic Report on Boiling Water Reactors.
  - (b) USNRC Letter to General Electric "Summary of July 12, 1979 Meeting to Discuss BWR Loss of Feedwater and Small Break LOCA" dated 7/26/79.
  - (c) Letter from T. D. Keenan, Chairman, General Electric Operating Plant Owners' Group, to Mr. D. F. Ross, Jr. of the NRC dated 8/17/79, General Electric Report "NEDO-24708, Additional Information Required for NRC Staff Generic Report on Boiling Water Reactors".

Enclosure: (1) Bulletins & Orders Task Force - Long Term Systems Information

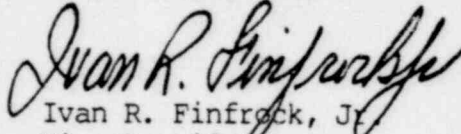
By letter dated July 17, 1979 (reference a), the NRC had requested that Jersey Central Power & Light Company provide additional information which was deemed necessary to enable the NRC staff to issue a generic report on BWRs. This information request was later modified by reference (b). Part of the information requested was sent to the NRC on August 17, 1979 (Reference c). Enclosure (1) to this letter provides the remainder of the requested information in accordance with the schedule provided in reference (b) except for the following: the containment isolation information requested by Item I of Attachment 2 to Enclosure 1 of reference (a) is still being compiled, and has not been included in this package; it will be forwarded to you as soon as

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possible, but no later than December 1, 1979.

If you need any clarification of our responses during your review of the information provided, please contact Mr. Jim Knubel, Supervisor, Nuclear Safety & Licensing, (201-455-8753) of my staff.

Very truly yours,

  
Ivan R. Finfrock, Jr.  
Vice President

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ENCLOSURE 1.

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PLANT Oyster Creek UNIT(S) 1

BYPASS CAPACITY

Plant Steam Bypass Capacity, % Rated 40

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PLANT Oyster Creek

SYSTEMS AND COMPONENTS SHARED BETWEEN UNITS

PAGE \_\_\_\_\_ CONTINUED PAGE \_\_\_\_\_

Single-unit plant check here ☒ and do not complete

System or Component

Shared Between  
Units Numbers

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PLANT Oyster Creek UNIT(S) 1

PLANT-SPECIFIC SYSTEM INFORMATION

Page 1, continued on page 2.

System	General		Water Sources		Instrumentation and Control		Frequency of * System and Component Tests
	Safety Classification	Seismic Category	Safety Classification	Seismic Category	Safety Classif.	Seismic Category	
1. RCIC	NA**	NA	NA	NA	NA	NA	NA
2. Isolation Condenser	Note 1	I	Note 1	I	Note 1	Note 2	EVERY REFUELING OUTAGE
3. HPCI	NA	NA	NA	NA	NA	NA	NA
4. HPCI	NA	NA	NA	NA	NA	NA	NA
5. LPCS	Note 1	I	Note 1	I	Note 1	Note 2	EVERY 3 MONTHS
6. LPCI	NA	NA	NA	NA	NA	NA	NA
7. ADS	Note 1	I	NA	NA	Note 1	Note 2	EVERY REFUELING OUTAGE
8. SRV	"	I	NA	NA	Note 1	"	ONCE EVERY THREE REFUELING OUTAGES
9. RHR (including shutdown cooling, steam condensing, suppression pool cooling, containment spray modes)	Note 1	II	Note 1	I	Note 1	Unknown	NOT TESTED
	"	I	"	I	"	Note 2	EVERY 3 MONTHS
	"	II	"	II	"	Unknown	EVERY 3 MONTHS
	"	I	"	I	"	Note 2	EVERY 3 MONTHS
10. SSW (Service Water System)	"	I	"	II	"	Unknown	NA
11. RBCCW	"	I	CLOSED LOOP	NA	"	"	NA
12. CRDS	"	I	Note 1	II	"	Note 2	ONCE PER MONTH
13. CST	"	II	NA	NA	"	Unknown	NA
14. Main Feedwater	"	I	Note 1	II	"	II	NA
15. Recirculation Pump/Motor Cooling	"	I	CLOSED LOOP	NA	"	Unknown	NA

Note 2: Original Burns & Roe design specifications calls for Category I design criteria, actual conditions in field indicate a probable non-seismic I installation.

Note 1: Safety classification did not exist when Oyster Creek was built, see next seven pages for design code specifications, information provided may be incomplete.

\* Some components of these systems are tested more frequently than indicated.

\*\* An entry of "NA" is provided when the question does not apply to a particular system or when the system does not exist at the plant.

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OYSTER CREEK  
COMPONENT/SUBSYSTEM

PLANT-SPECIFIC SYSTEM INFORMATION  
Page 2, continued on page 3.  
QUALITY GROUP

Sheet 1

REMARKS

NOTE  
1

STRUCTURES

1. REACTOR BLDG

2. DRYWELL, TORUS, VENTS

3. CONTROL ROOM PANELS

4. SPENT FUEL POOL

5. VENT STACK

6. TURBINE BLDG.

7. RADWASTE BLDG.

2,3

9. INTAKE & DISCHARGE

10. SCREEN HOUSE

EQUIPMENT  
NSSS

1,2,3

1. REACTOR VESSEL

1,2

2. CRDS Housing

1,2

Supports

1,2,3

3. RV SUPPORTS

1,2,3

4. FUEL ELEMENTS

1,2,3

5. CORE SHROUD

1,2,3

6. CORE SUPPORTS

1,2,3

7. STEAM SEPARATOR

PLANT  
DESIGN

R.G. 1.26  
SRP 3.2.2

PLANT  
DESIGN

R.G. 1.29  
SRP 3.2.1

ASME SEC. VIII  
1962 Edition & IV  
1270N-5  
1272N-5  
1271N  
SEC. VIII  
ASA, IBEE, ASTM,  
AWS, NBP & FED  
STATE & LOCAL

N/A

CLASS I

CLASS I

CLASS I

CLASS I

CLASS I

CLASS II

CLASS II

CLASS II

CLASS II

CLASS I

CLASS I

CLASS I

CLASS I

CLASS I

CLASS I

CLASS I

SEISMIC  
CATEGORY I  
(SEE)

I

I

NSI (OBE)

NONSEISMIC  
CATEGORY I  
(OBE)

SEISMIC I

SEISMIC I

SEISMIC

SEISMIC I

SEISMIC I

SEISMIC I

SEISMIC I

SEISMIC I

R.G. 1.29 C.1.0/(V.3.5)

R.G. 1.29 C.1.0/(V.3.5)

R.G. 1.29 C.1.n/(V.3.5)

R.G. 1.29 C.1.1/(V.3.5)

SEE SRP 11.3

IF THIS IS ULTIMATE HEAT  
SINK IT SHOULD BE SI  
R.G. 1.29(1g).

Pg. IV-1-1/R.G. 1.29  
C.1.a/(V.3.5)

R.G. 1.29 (C.2/(V.3.5))

R.G. 1.29 C.2/(V.3.5)

R.G. 1.29 C.2/(V.3.5)

R.G. 1.29 C.1.b/(V.3.5)

R.G. 1.29 C.1.b/(V.3.5)

R.G. 1.29 C.1.b/(V.3.5)

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OYSTER CREEK COMPONENT/SUBSYSTEM		PLANT-SPECIFIC SYSTEM INFORMATION		Page 3, continued on page 4.	
		QUALITY GROUP		SEISMIC	REMARKS
NOTE		PLANT DESIGN	R.G. 1.26 SRP 3.2.2	PLANT DESIGN	R.G. 1.29 SRP 3.2.1
1,2,3	8. STEAM DRYER	ASME 8 IX	N/A	CLASS I	SEISMIC I R.G. 1.29 C.1.b/V.3.5
3	9. PIPING FROM REACTOR VESSEL TO 1st ISOLATION VALVE EXTERNAL TO DRYWELL	ASME SI 1965 to first ISO VALVE OUTSIDE DRYWELL then ANSI B31.1-1965 & NUC Code Cases to 2nd ISO valve.	ASME BPV SIII C1 A	CLASS I	SEISMIC I R.G. 1.29 C.1.a
	RECIRCULATION SYSTEM				
1	1. PUMPS	ASA B31.1	ASME BPV SIII C1 A	CLASS I	SEISMIC I VI-1-1/R.G. 1.29 C.1.a
1	2. VALVES	ASME BPV I	" A	CLASS I	SEISMIC I IV-1-1/R.G. 1.29 C.1.a
1	3. PIPING	ASME BPV I ASA B31.1	" A	CLASS I	SEISMIC I IV-1-2/R.G. 1.29 C.1.A
	EMERGENCY SYSTEMS				
2,3	1. ISOLATION CONDENSER SHELL	ASME BPV SECT. VIII	C	CLASS I	SEISMIC I IV-1-2 R.G. 1.29 C.2
1,2,3	TUBE	ASME BPV S.III C1.A	ASME BPV SIII C2 B	CLASS I SIII CLASS 2	SEISMIC I R.G. 1.29 C.1.b
1,2,3	PIPING	ASME Sec. 1 1965	ASME BPV SIII CLASS 2 B	CLASS I	SEISMIC I R.G. 1.29 C.1.b
3*2	2. LIQUID POISON SYS. * Only if CRDS fails to operate	ASME 31-1965 ANSI B-31.1-1965 & NCC	ASME BPV SIII CLASS 2 B	CLASS I	SEISMIC I R.G. 1.29 C.1.b
	PUMP TANK	ASME SIII C1C API	B B		
1,3	3. CORE SPRAY SYS. PIPING	ASA B31.1	ASME BPV SIII C2 A/B	CLASS I "	SEISMIC I R.G. 1.29 C.1.c/VI.6.2 CLASS I
2	4. REACTOR BLDG CLOSED LOOP COOLING	ANSI-B31.1-1965 & Nuclear Code Cases	ASME BPV SIII CL 3 C	CLASS I	SEISMIC I V.3.5/R.G. 1.29 C.1.g
3	5. AUTOMATIC DEPRESSUR-		A		Part of ECOS; should be Seismic I, Class 2

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NOTE	OYSTER CREEK COMPONENT/SUBSYSTEM	QUALITY GROUP		SEISMIC		REMARKS
		PLANT DESIGN	R.G. 1.26 SRP 3.2.2	PLANT DESIGN	R.G. 1.29 SRP 3.2.1	
1	REACTOR EMERGENCY SYS.					
3	SERVICE WATER SYSTEM	ASME BPV SI & IX TO 1st ISO- LATION VALVE REST ASA 1331.1-1955* CHANGES TO 1966	ASME BPV SIII CLASS 3 C	CLASS I	SEISMIC I	R.G. 1.29 C.1.g/X-3-2
3	CONTAINMENT SPRAY SYSTEM	ASA 531.1 ASME S VIII TO 1st VALVE OUTSIDE CONTAINMENT	ASME BPV SIII CLASS 2 B	CLASS I	SEISMIC I	R.G. 1.29 C.1.c/VI-7-1
X	STANDBY GAS TREAT. SYS	GE	B**	CLASS I	SEISMIC I*	No description of system *if system removes H <sub>2</sub> **no req't if post accid fission product removal is not basis. O.C. uses H <sub>2</sub> inerting system
X	SPENT FUEL AND NEW FUEL STORAGE FACILITIES	ASTM, A373, A245, 6VA, B&C ASTM, A240 C1 304L		CLASS I	SEISMIC	Fuel Handling Not Covered by R. G. 1.26; R.G. 129 C.1.L requires seismic I
1,3	EMERGENCY ELEC. SYS. BATTERIES	ASA, ASTM, ASTM, IEEE NEMA, NFBJ NEMA, LOCAL	N/A	CLASS I	SEISMIC I	R.G. 1.29 (C.1.q) CLASS IE ONSITE POWER SUPPLIES IEEE 344. SRP 8.3.2
2,3	DIESEL GENERATOR	ASME, ASA, ASTM, IEEE, NEMA, NFBJ DEMI, LOCAL				R.G. 1.29 C.1.q Class IE Onsite Power
2,3	EMERGENCY BUSES, ETC.	ASA, IEEE, ASTM, NEMA				R.G. 1.29 C.1.8 Class IE Onsite Power Supplies IEEE 344. SRP 8.3.1

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PLANT-SPECIFIC SYSTEM INFORMATION  
Page 5, continued on page 6

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OYSTER CREEK COMPONENT/SUBSYSTEM	QUALITY GROUP		SEISMIC		REMARKS
	PLANT DESIGN	R.G. 1.26 SRP 3.2.2	PLANT DESIGN	R.G. 1.29 SRP 3.2.1	
NOTE 1					
STEAM SYSTEM					
1 1. Piping to Ist.I.V.	ASME BPV SECT. I	ASME BPV A III CLASS I A	CLASS I	SEISMIC I	R.G. 1.29 C.1.a/IV-1-2
2. Piping to Turb SV	ASA B31.1	ASME BPV VIII CLASS 2 B		SEISMIC I	R.G. 1.29 C.1.e
1 3. MSIV VALVE	ASME BPV SECT. I ASA B31.1 GB SPECS	ASME BPV VIII CLASS 1 A	CLASS I	SEISMIC I	R.G. 1.29 C.1.a/IV-1-2
4. TURBINE STOP VALVE		ANSI B31.1.1.0 D		NON SEISMIC I	SRP 3.2.1
1 5. SAFETY VALVE	ASME BPV SECT. I XNCC-1271N	ASME BPV VIII CLASS 1 A	CLASS I	SEISMIC I	R.G. 1.29 C.1.a/IV-1-2
1 6. RELIEF VALVE	ASME BPV SECT I	ASME BPV VIII CLASS 1 A	CLASS I	SEISMIC I	R.G. 1.29 C.1.a/IV-1-2
2 SHUTDOWN COOLING SYSTEMS PUMPS	----- ASME BPV SECT.III	----- ASME BPV VIII CLASS 2 C	CLASS II CLASS II	----- SEISMIC I	X-2-2 R.G. 1.29-C.1.d
2 SHUTDOWN COOLING TUBE	ASME BPV SECT CLASS C	ASME BPV VIII CLASS 2 C	CLASS II	SEISMIC I	R.G. 1.29 C.1.d

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PLANT-SPECIFIC SYSTEM INFORMATION  
Page 6, continued on page 7

Sheet 5

OYSTER CREEK COMPONENT/SUBSYSTEM	QUALITY GROUP		SEISMIC		REMARKS
	PLANT DESIGN	R.G. 1.26 SRP 3.2.2	PLANT DESIGN	R.G. 1.29 SRP 3.2.1	
NOTE 1					
2 x SHELL	ASME BPV SECT. VIII	ASME BPV SIII CLASS 2 C	CLASS II SIII CLASS 2	SEISMIC I	R.G. 1.29 C.1.g
CONDENSATE STORAGE TANKS & PUMPS			CLASS II Analysed for 0.11g seismic event - O.K.	SEISMIC II	CONDENSATE STORAGE SYSTEM IS RELATED TO SAFETY; ECCS SHALL BREAKS USE CRD WHICH HAS NORMAL SUCTION FROM CST ISOLATION CONDENSER CAN ALSO TAKE SUCTION FROM CST.
X LIQUID WASTE SYSTEM	API 650 STANDARD	ASME BPV SIII CLASS 3 D	CLASS II		WASTE MANAGEMENT SYSTEMS IS UNDER DEVELOPMENT SRP 5.4.8 REQUIRES THAT PIPING FROM THE RECIRCULATION LOOP TO THE OUTERMOST ISOLATION VALVE BE CLASS A, SEISMIC I
X REACTOR CLEANUP SYS.	ASME BPV SIII CLASS C	ASME BPV SIII CLASS 3 C	CLASS II	NON-SEISMIC	X-2-1
X AIR COMPRESSOR & RECEIVERS		NOT COVERED BY R.G. 1.26	CLASS II	NON-SEISMIC	AIR OPERATED VALVES IMPORTANT TO SAFETY ARE REQUIRED TO HAVE SEISMIC ACCUMULATORS
2,3 STATION AUXILIARY BUSES		N/A	CLASS II		
X MOISTURE SEPARATORS AND REHEATERS	ASME SEC. VIII	N/A	CLASS II		

NOTE 1 - #1 denotes equipment required to hold together to prevent a LOCA due to the seismic event  
#2 denotes equipment required to shutdown & hold in safe shutdown condition following seismic event  
#3 denotes equipment required if plant experiences a LOCA  
X denotes equipment not needed for safety during seismic event

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OYSTER CREEK  
COMPONENT/SUBSYSTEM

PLANT-SPECIFIC SYSTEM INFORMATION

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Sheet 6

NOTE		QUALITY GROUP		SEISMIC		REMARKS
		PLANT DESIGN	R.G. 1.26 SRP 3.2.2	PLANT DESIGN	R.G. 1.29 SRP 3.2.1	
1	INSTRUMENT AND CONTROL					
2, 3	REACTOR LEVEL INSTR.	B31.1 SI & VI ASA, IEEE, ASME, ASTM, ANSI, NBPV, & STATE & LOCAL		CLASS I	SEISMIC I	R.G. 1.29 C.1.k/V.3.6
2, 3	FEED WATER CONTROL VALVES			"	"	"
2*	LIQUID POISON SYS. INSTR.			"	"	"
	ANNUAL REACTOR CONTROL			"	"	"
2, 3	CONTROL ROD INST	ASA & IEEE	N/A	"	"	"
2, 3	CONT. ROD POSITION INDICATING SYST.			"	"	"
2, 3	REACTOR PROTECTION SYSTEM			"	"	"
2, 3	NEUTRON MONITOR SYSTEM			"	"	"
	FUEL RUPTURE DETECTION SYST. AREA MONITORS	ASME III C1.A Pressure Parts		"	"	"
				CLASS I		
X	TURBINE GENERATOR	ASME, ASA, ASTM, IEEE, NEMA, NBPV STDS OF TUBULAR EXCHANGER MANU- FACTURE ASSO- CIATION CLASS R. NJ & LOCAL CODES	N/A	Class II		No Seismic Req't/V-3-6
						No Seismic Req't/V-3-6
X	CONDENSER	HEAT EXCHANGER INSTITUTE	N/A	Class II	Dynamic analysis for 0.1g seismic event	
	FEEDWATER SYSTEM HEATERS PUMPS	ASME S1-1965 RV TO 1st VALVE OUTSIDE CONTAIN- MENT ASME SECT. VIII & TFMA STDS.		CLASS II	* *-The FWS is used as re- dundant ECCS to the ADS for Small Brks and single failure requirements. This would require that the FWS seismic I, Amend. 38 presents results of seismic analysis to show that the feedwater in- jection system meets Class I standards.	

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PLANT-SPECIFIC SYSTEM INFORMATION  
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Sheet 7

QUALITY STANDARDS

<u>NRC QUALITY GROUP A</u>	<u>NRC QUALITY GROUP B</u>	<u>NRC QUALITY GROUP C</u>	<u>NRC QUALITY GROUP D</u>
ASME Boiler and Pressure Vessel Code, Section III			ASME, Sec. VIII (pressure vessels) ANSI B31.1.0 (piping and valves) Mfg. Stds. (pumps)
Class 1	Class 2	Class 3	
or	or		
ASME Boiler and Pressure Vessel Code, Section III			
Class A	Class C	--	--
(pressure vessels)	(pressure vessels)		

NRC Quality Group A equivalent to Licensee Safety Class 1

NRC Quality Group B equivalent to Licensee Safety Class 2

NRC Quality Group C equivalent to Licensee Safety Class 3

NRC Quality Group D equivalent to Licensee Safety Class 4 or NNS

) Also seismic Category I

) Not always seismic Category I

) Non-seismic Category I

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PLANT: OYSTER CREEK NUCLEAR STATION UNIT 1

DESIGN REQUIREMENTS FOR CONTAINMENT ISOLATION BARRIERS

Page 1, continued  
on page 2

Question: Discuss the extent to which the quality standards and seismic design classification of the containment isolation provisions follow the recommendations of Regulatory Guides 1.26, "Quality Group Classifications and Standards for Water-, Steam-, and Radioactive-Water-Containing Components of Nuclear Power Plants", and 1.29, "Seismic Design Classification".

Response: The table shown below lists quality standards and seismic design classification used for the containment isolation provisions for Oyster Creek Nuclear Station. Also listed in the table are the standards and classifications recommended by Regulatory Guide 1.26 and 1.29.

SYSTEM	QUALITY GROUP		SEISMIC DESIGN	
	PLANT DESIGN	R.G. 1.26	PLANT DESIGN	R.G. 1.29
Piping From Reactor Vessel to 1st Isolation Valve external to Drywell	ASME BPV Section I (1965)	ASME BPV Section III C 1, A	Class I	Category I
Recirculation line	ASME BPV Section I ASA B31.1	ASME BPV Section III C1, A	Class I	Category I
Isolation Condenser	ASME BPV Section I (1965)	ASME BPV Section III C2, B	Class I	Category I
Core Spray	ASME BPV Section I ASA B31.1	ASME BPV Section III C2, A/B	Class I	Category I
Containment Spray	ASME BPV Section VIII	ASME BPV Section III C2, B	Class I	Category I
Steam Line	ASME BPV Section I ASA B31.1 GE Spec.	ASME BPV Section III C1, A	Class I	Category I
Reactor Clean Up	ASME BPV Section III Class C	ASME BPV Section III C3, C	Class II	Non-Seismic

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DESIGN REQUIREMENTS FOR CONTAINMENT ISOLATION BARRIERS

Page 2, FINAL

SYSTEM	QUALITY GROUP		SEISMIC DESIGN	
	PLANT DESIGN	R.G. 1.26	PLANT DESIGN	R.G. 1.29
Feedwater System	ASME BPV Section I (1965)	D	Class II  Amendment 38 to the Oyster Creek FSAR provides results of seismic anal- ysis to show that the feedwater in- jection system meets Class I standards.	Category II  If the FWS is used as redundant ECCS to the ADS for small breaks and single failure requirements, it would require that the FWS be Category I.

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## PROVISIONS FOR TESTING

Question: Discuss the design provisions for testing the operability of the isolation valves.

Response: The operability of primary containment isolation and reactor coolant isolation valves is tested during every refueling outage. Testing of primary containment isolation valve operability is performed in two ways: (1) by introducing a high drywell pressure signal to the drywell high pressure sensor and (2) by introducing a Lo Lo water level signal to the Yarway level sensors. Testing of reactor coolant isolation valve operability is performed by introducing a Lo Lo Water level signal to the Yarway level sensors.

Testing is performed by the following steps:

- (1) Isolate the pressure sensor or the Yarway level sensor to be tested.
- (2) Introduce an appropriate signal (either a high pressure signal or a level d/p signal) to the pressure sensor or level sensor until the appropriate relays trip.
- (3) Verify that all relays function as specified.
- (4) Restore the pressure sensor or level sensor back to service.
- (5) Repeat steps (1) through (4) until all sensors are tested, step (4) is omitted for the last sensor tested in order to obtain a 2 out of 4 coincidence trip when step (6) is performed.
- (6) Introduce an appropriate trip signal to one of the other sensors previously tested to obtain a 2 out of 4 coincidence trip.
- (7) Verify that all isolation valves are closed in accordance with procedure requirements.
- (8) Restore all sensors and other system components back to service.
- (9) Individually close and record closing times of the reactor coolant isolation valves.

These tests are considered acceptable if all requirements specified in the appropriate procedures are met.

PLANT Oyster Creek UNIT(S) 1

CODES, STANDARDS, AND GUIDES

Question: Identify the codes, standards, and guides applied in the design of the containment isolation system and system components.

Response: 1) Piping

A) From vessel to first - ASME Sec. I - 1965  
Isolation Valve

B) After first ISO valve - ANSI B31.1 - 1965  
to outside ISO valve

2) Valves and Operators - Revisions to 1965

American Standards Association  
American Society for Testing Materials  
ASME - Section I and VIII  
Pipe Fabrication Institute  
American Institute of Electrical Engineers  
National Electrical Manufacturers Association

3) Instrumentation

Except for material used in fabrication of  
instrumentation, manufacturer's standards  
apply.

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NORMAL OPERATING MODES AND ISOLATION MODES

Question: Discuss the normal operating modes and containment isolation provision and procedures for lines that transfer potentially radioactive fluids out of the containment.

Response:

Main Steam Isolation Valves

Each main steam line is provided with two isolation valves, one inside containment and one outside, which are open during normal operation. A test circuit is provided to permit slow speed exercising of each valve.

Automatic closure of the valves is initiated by the following signals:

- a. High flow in the main steam line.
- b. Rx Lo-Lo water level.
- c. Steam line high radiation.
- d. High temperature in steam tunnel.
- e. Low pressure in main steam line (825psig).

Main Steam line drains are closed in normal operation. These valves are (automatically) closed by the same signals associated with Main Steam isolation valves.

Energy Condenser Valves

The system is operable and ready for service at all times during power operation. Conditions requiring use of the system are considered abnormal. The two series valves in the steam inlet lines are open and one of two series valves in the condensate return line is open during normal operation. The vent isolation valves are normally open.

Automatic opening of the condensate return line is initiated by the following signals:

- a. Rx Lo-Lo water level.
- b. Rx high pressure.

Isolation of the steam inlet line and condensate return line is initiated by excess flow in either line.

Response: (Continued)

Feedwater System

Feedwater lines connected to the reactor vessel do not utilize automatic isolation valves, since operation of this system is essential following a loss of coolant accident. Check valves located in these lines inside the drywell and outside the drywell provide isolation when necessary.

Liquid Poison System

The liquid poison system is a stand-by system for use in the event that the control rod system is inoperable. The system is activated only by remote manual action from the control room; that is the squib valves are fired and pump started. Isolation is provided by two check valves.

Shutdown Cooling System

The shutdown cooling system removes fission product decay heat during shutdown with reactor pressure less than 150 psi. The isolation valves inside the drywell are interlocked to prevent system operation above 350°F.

Isolation valves in the suction and discharge headers are automatically closed by the following initialing signals:

- a. Rx Lo-Lo water level.
- b. High inlet temperature (350°F).

Clean Up System

The clean up demineralizer system is a filtration and ion exchange system for maintaining the purity of the water in the reactor vessel and is normally in service with isolation valves open. The influent piping has isolation valves inside and outside the drywell. The return pipe has an isolation valve outside drywell and a check valve inside the drywell.

Automatic isolation valve closure is initiated by any of the following conditions:

- a. Rx Lo-Lo water level.
- b. Low flow through the clean up filter.
- c. High temperature Rx water from non-regenerative heat exchanger.

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Response: (Continued)

Clean Up System (Continued)

- d. High pressure from the pressure reducing station.
- e. High temperature cooling water from the auxiliary clean-up pump.
- f. Liquid poison system flow to vessel.

An exception to the above is the return valve V-16-61 which closes on lo-lo reactor water level only.

Core Spray System

The core spray system is a low pressure stand-by core cooling system which provides an alternate supply of reactor cooling water in the event of a pipe break accident in the primary system. The isolation parallel valves are normally closed and do not open until after the system initiates from Rx lo-lo water level or high drywell pressure and reactor pressure is less than 285 psi.

Check valves are provided in each header inside drywell which provide isolation. The manual isolation valves inside the drywell are locked open and all other system valves in the flow path are open. The valves which recirculate water to the torus are closed except during testing.

Control-Rod Drive System

The control rod hydraulic system has two isolation valves. The first is a ball check which is part of the control drive mechanism and a normally closed hydraulic system control valve. The exhaust header takes water discharged by the drives during operation and returns this water to the reactor check valves and effectively isolates this line.

Instrument Air/Nitrogen

Control air and nitrogen valves are open for control instrument use during power operation. No automatic isolation is presently provided.

Drywell & Torus O<sub>2</sub> Sample System

The isolation valves in this system are open during power operation.

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Response: (Continued)

Drywell & Torus O<sub>2</sub> Sample System (Continued)

Isolation is provided automatically from the following signals:

- a. Rx Lo-Lo water level.
- b. Drywell high pressure.

Rx Building Closed Cooling Water System

The closed cooling water lines do not connect to the reactor primary system and are not open to the containment atmosphere. They are provided with isolation valves in the supply and return headers. No automatic isolation provided.

Reactor Primary-System Instrument Lines

Reactor primary-system instrumentation piping which leaves the primary containment are dead-ended at devices' location in the reactor building. These lines are provided with manual isolation valves outside drywell and excess flow checks in each line which close automatically with leakage flow.

Containment Spray System

The containment spray system is not provided with automatic isolation valves, but does have motor operated isolation valve that can be operated from the Control Room.

Reactor Head Cooling System

The head cooling system is used in conjunction with reactor vessel flooding and shutdown cooling system for vessel cool down. Manual and motor operated isolation valves are closed during power operation. No automatic isolation is required.

Drywell Equipment Drain Tank (DEDT) & Sump Drain

Floor and equipment drains are segregated in the drywell with the floor drains collected in a sump and the equipment drains collected in a drain tank. The contents of each are transferred to Radwaste Building. The DEDT tank is provided with overflow and vent lines to the sump.

Each discharger has dual isolation valves that are closed automatically by the following signals:

- a. Rx Lo-Lo water level.
- b. High drywell pressure.

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Response: (Continued)

Drywell Purge & Exhaust System

During reactor operation, the nitrogen atmosphere is isolated within the drywell and recirculated by the drywell cooler blowers. The make up is automatic on pressure control to the drywell only. In each supply line, drywell and torus series isolation valves are closed during reactor operation to isolate the containment vessel from the make up line, except when make up is required. All isolation valves are automatically closed by the following signals:

- a. Rx Lo-Lo water level.
- b. High drywell pressure.

A keylock bypass switch is installed which bypasses any drywell isolation signal allowing the operator to open any of the drywell purge as vent valves. The exhaust is vented normally to the stack with isolation valve normally closed and interlocked to close automatically by the following signals:

- a. Rx Lo-Lo water level.
- b. High drywell pressure.

All operable isolation valves in the containment inerting system are automatically closed. A keylock bypass switch is provided in the exhaust line to the gas treatment system to reduce pressure in the torus and drywell in the post accident phase.

Vacuum Relief System

Automatic vacuum-relief devices are used to prevent the primary containment from exceeding the external design pressure. The drywell vacuum-relief device draws atmosphere from the pressure absorption chamber and the pressure absorption chamber vacuum-relief device draws air from the reactor building. Two vacuum breakers in series are used in each of the two lines to atmosphere. One valve is activated by a differential pressure signal while the second valve is a check valve.

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