



830 Power Building
TENNESSEE VALLEY AUTHORITY
CHATTANOOGA, TENNESSEE 37401

Revised 1/2/76

MAY 17 1976

Mr. Norman C. Moseley, Director
Office of Inspection and Enforcement
U.S. Nuclear Regulatory Commission
Region II - Suite 818
230 Peachtree Street, NW.
Atlanta, Georgia 30303

Dear Mr. Moseley:

BROWNS FERRY NUCLEAR PLANT UNIT 3 - REPORTABLE DEFICIENCY -
POSSIBILITY OF marginally ADEQUATE SUPPORT STRUCTURE ON
MAIN STRAM AND RELIEF VALVE DISCHARGE PIPING - IR CONTROL
NO. H01127F2

Initial report of the subject reportable deficiency was made
to G. R. Klingler, NRC-IE, Region II, on December 23, 1975,
and was followed by our January 20, 1976, letter, J. E. Gilleland
to Donald F. Knuth. A second interim report was submitted to
NRC by our April 29, 1976, letter, J. E. Gilleland to Norman C.
Moseley. Enclosed is our final report concerning this deficiency
(Enclosure 1) and a copy of the Teledyne analysis (Enclosure 2)
relating to this deficiency.

Very truly yours,

J. E. Gilleland
Assistant Manager of Power

Enclosures

CC: ✓ Dr. E. Volgenau, Director
Office of Inspection and Enforcement
U.S. Nuclear Regulatory Commission
Washington, DC 20555

James

1. $\frac{1}{2} \times \frac{1}{2} = \frac{1}{4}$
 2. $\frac{1}{2} \times \frac{1}{4} = \frac{1}{8}$
 3. $\frac{1}{4} \times \frac{1}{4} = \frac{1}{16}$
 4. $\frac{1}{2} \times \frac{1}{8} = \frac{1}{16}$
 5. $\frac{1}{4} \times \frac{1}{8} = \frac{1}{32}$
 6. $\frac{1}{2} \times \frac{1}{16} = \frac{1}{32}$
 7. $\frac{1}{4} \times \frac{1}{16} = \frac{1}{64}$
 8. $\frac{1}{2} \times \frac{1}{32} = \frac{1}{64}$
 9. $\frac{1}{4} \times \frac{1}{32} = \frac{1}{128}$
 10. $\frac{1}{2} \times \frac{1}{64} = \frac{1}{128}$
 11. $\frac{1}{4} \times \frac{1}{128} = \frac{1}{256}$
 12. $\frac{1}{2} \times \frac{1}{256} = \frac{1}{256}$
 13. $\frac{1}{4} \times \frac{1}{256} = \frac{1}{512}$
 14. $\frac{1}{2} \times \frac{1}{512} = \frac{1}{512}$
 15. $\frac{1}{4} \times \frac{1}{512} = \frac{1}{1024}$
 16. $\frac{1}{2} \times \frac{1}{1024} = \frac{1}{1024}$
 17. $\frac{1}{4} \times \frac{1}{1024} = \frac{1}{2048}$
 18. $\frac{1}{2} \times \frac{1}{2048} = \frac{1}{2048}$
 19. $\frac{1}{4} \times \frac{1}{2048} = \frac{1}{4096}$
 20. $\frac{1}{2} \times \frac{1}{4096} = \frac{1}{4096}$
 21. $\frac{1}{4} \times \frac{1}{4096} = \frac{1}{8192}$
 22. $\frac{1}{2} \times \frac{1}{8192} = \frac{1}{8192}$
 23. $\frac{1}{4} \times \frac{1}{8192} = \frac{1}{16384}$
 24. $\frac{1}{2} \times \frac{1}{16384} = \frac{1}{16384}$
 25. $\frac{1}{4} \times \frac{1}{16384} = \frac{1}{32768}$
 26. $\frac{1}{2} \times \frac{1}{32768} = \frac{1}{32768}$
 27. $\frac{1}{4} \times \frac{1}{32768} = \frac{1}{65536}$
 28. $\frac{1}{2} \times \frac{1}{65536} = \frac{1}{65536}$
 29. $\frac{1}{4} \times \frac{1}{65536} = \frac{1}{131072}$
 30. $\frac{1}{2} \times \frac{1}{131072} = \frac{1}{131072}$
 31. $\frac{1}{4} \times \frac{1}{131072} = \frac{1}{262144}$
 32. $\frac{1}{2} \times \frac{1}{262144} = \frac{1}{262144}$
 33. $\frac{1}{4} \times \frac{1}{262144} = \frac{1}{524288}$
 34. $\frac{1}{2} \times \frac{1}{524288} = \frac{1}{524288}$
 35. $\frac{1}{4} \times \frac{1}{524288} = \frac{1}{1048576}$
 36. $\frac{1}{2} \times \frac{1}{1048576} = \frac{1}{1048576}$
 37. $\frac{1}{4} \times \frac{1}{1048576} = \frac{1}{2097152}$
 38. $\frac{1}{2} \times \frac{1}{2097152} = \frac{1}{2097152}$
 39. $\frac{1}{4} \times \frac{1}{2097152} = \frac{1}{4194304}$
 40. $\frac{1}{2} \times \frac{1}{4194304} = \frac{1}{4194304}$
 41. $\frac{1}{4} \times \frac{1}{4194304} = \frac{1}{8388608}$
 42. $\frac{1}{2} \times \frac{1}{8388608} = \frac{1}{8388608}$
 43. $\frac{1}{4} \times \frac{1}{8388608} = \frac{1}{16777216}$
 44. $\frac{1}{2} \times \frac{1}{16777216} = \frac{1}{16777216}$
 45. $\frac{1}{4} \times \frac{1}{16777216} = \frac{1}{33554432}$
 46. $\frac{1}{2} \times \frac{1}{33554432} = \frac{1}{33554432}$
 47. $\frac{1}{4} \times \frac{1}{33554432} = \frac{1}{67108864}$
 48. $\frac{1}{2} \times \frac{1}{67108864} = \frac{1}{67108864}$
 49. $\frac{1}{4} \times \frac{1}{67108864} = \frac{1}{134217728}$
 50. $\frac{1}{2} \times \frac{1}{134217728} = \frac{1}{134217728}$
 51. $\frac{1}{4} \times \frac{1}{134217728} = \frac{1}{268435456}$
 52. $\frac{1}{2} \times \frac{1}{268435456} = \frac{1}{268435456}$
 53. $\frac{1}{4} \times \frac{1}{268435456} = \frac{1}{536870912}$
 54. $\frac{1}{2} \times \frac{1}{536870912} = \frac{1}{536870912}$
 55. $\frac{1}{4} \times \frac{1}{536870912} = \frac{1}{1073741824}$
 56. $\frac{1}{2} \times \frac{1}{1073741824} = \frac{1}{1073741824}$
 57. $\frac{1}{4} \times \frac{1}{1073741824} = \frac{1}{2147483648}$
 58. $\frac{1}{2} \times \frac{1}{2147483648} = \frac{1}{2147483648}$
 59. $\frac{1}{4} \times \frac{1}{2147483648} = \frac{1}{4294967296}$
 60. $\frac{1}{2} \times \frac{1}{4294967296} = \frac{1}{4294967296}$
 61. $\frac{1}{4} \times \frac{1}{4294967296} = \frac{1}{8589934592}$
 62. $\frac{1}{2} \times \frac{1}{8589934592} = \frac{1}{8589934592}$
 63. $\frac{1}{4} \times \frac{1}{8589934592} = \frac{1}{17179869184}$
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 65. $\frac{1}{4} \times \frac{1}{17179869184} = \frac{1}{34359738368}$
 66. $\frac{1}{2} \times \frac{1}{34359738368} = \frac{1}{34359738368}$
 67. $\frac{1}{4} \times \frac{1}{34359738368} = \frac{1}{68719476736}$
 68. $\frac{1}{2} \times \frac{1}{68719476736} = \frac{1}{68719476736}$
 69. $\frac{1}{4} \times \frac{1}{68719476736} = \frac{1}{137438953472}$
 70. $\frac{1}{2} \times \frac{1}{137438953472} = \frac{1}{137438953472}$
 71. $\frac{1}{4} \times \frac{1}{137438953472} = \frac{1}{274877906944}$
 72. $\frac{1}{2} \times \frac{1}{274877906944} = \frac{1}{274877906944}$
 73. $\frac{1}{4} \times \frac{1}{274877906944} = \frac{1}{549755813888}$
 74. $\frac{1}{2} \times \frac{1}{549755813888} = \frac{1}{549755813888}$
 75. $\frac{1}{4} \times \frac{1}{549755813888} = \frac{1}{1099511627776}$
 76. $\frac{1}{2} \times \frac{1}{1099511627776} = \frac{1}{1099511627776}$
 77. $\frac{1}{4} \times \frac{1}{1099511627776} = \frac{1}{2199023255552}$
 78. $\frac{1}{2} \times \frac{1}{2199023255552} = \frac{1}{2199023255552}$
 79. $\frac{1}{4} \times \frac{1}{2199023255552} = \frac{1}{4398046511104}$
 80. $\frac{1}{2} \times \frac{1}{4398046511104} = \frac{1}{4398046511104}$
 81. $\frac{1}{4} \times \frac{1}{4398046511104} = \frac{1}{8796093022208}$
 82. $\frac{1}{2} \times \frac{1}{8796093022208} = \frac{1}{8796093022208}$
 83. $\frac{1}{4} \times \frac{1}{8796093022208} = \frac{1}{17592186044416}$
 84. $\frac{1}{2} \times \frac{1}{17592186044416} = \frac{1}{175921$



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THE UNIVERSITY OF CHICAGO
CHICAGO, ILLINOIS

[illegible]

1. The first group of people who are interested in the results of the study are the researchers themselves. They want to know if the study was successful in achieving its objectives and if the results are consistent with their expectations.

$$A_{\alpha} = \begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix}, \quad A_{\beta} = \begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix}, \quad A_{\gamma} = \begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

ENCLOSURE 1

BROWNS FERRY NUCLEAR PLANT UNIT 3 ADEQUATE SUPPORT STRUCTURE ON MAIN STEAM AND RELIEF VALVE DISCHARGE PIPING DDR.223 - FINAL REPORT

On December 23, 1975, an initial report was made to NRC-OIE Region II Inspector, G. R. Klingler by T. V. Abbatiello, T. W. Barkalow, M. A. Linn, and S. H. Mindel. The report was made in compliance with 10CFR50.55(e). This is the final report for this occurrence.

Description of Occurrence

An analysis of the Browns Ferry main steam lines and relief valve discharge piping, which was done in conjunction with the proposed substitution of two Crosby relief valves for two Target Rock relief valves on unit 3, revealed that the existing piping support of these lines was not adequate to prevent stresses from exceeding those reported in the FSAR.

Cause of Deficiency

The Browns Ferry plant was originally designed using the criteria set forth in the 1967 issue of ANSI B31.1. Since this code did not address the transient relief valve discharge loading condition and a mathematical model of these forces was not available, engineering judgment and conservatism were used in designing for this condition. Experience in fossil plant design had shown that while lines of this type do vibrate, e.g., start up systems with high pressure critical systems blowing down to the condenser, they stabilize within a short period of time and stresses are within the endurance stress limit of the piping. Present day modeling and computer solution of the transient loading phenomenon, when considered in conjunction with the other loading conditions and existing piping support, show stresses in the piping to be above the stated FSAR values.

Safety Implications

The analysis of the main steam lines and relief valve discharge piping show the maximum stress to occur in the 26"x6" sweepolet connecting the lines. Upon considering pressure, deadweight and other sustained mechanical loads, seismic, and relief valve operation, stresses are above the stated FSAR values and near the yield stress of the material at design temperature. Assuming all these loads occurring simultaneously and of sufficient magnitude to cause a failure at the sweepolet, a small diameter pipe loss of coolant accident could occur. The emergency core cooling system is sized to readily mitigate such an accident. However, the possibility that such a failure could have occurred is very remote since the highest calculated stress was still below that necessary to cause such a failure.

Description of Corrective Action

Teledyne Materials Research has conducted a new stress analysis for each main steam and relief valve discharge line in all units at Browns Ferry. The criteria of ANSI B31.1, 1973 edition, including all addenda up to summer 1975, have been used for this analysis. Additional mechanical shock arrestors and restraints have been added to the lines for satisfaction of the criteria.

Means Taken to Prevent a Recurrence

All TVA nuclear plants will be analyzed considering all loading conditions as required by the applicable codes and SAR commitments.

