



February 15, 2018

Commission adjudicatory staff has received the attached email from the NRC Staff regarding the proposed exemption related to the maximum safety wet bulb (noncoincident) air temperature and its associated departure, PTN DEP 2.0-3, for the Turkey Point, Units 6 and 7, combined license application. This information is being served on the parties to the proceeding for their information.

From: [Weisman, Robert](#)
To: [Silvia, Andrea](#)
Cc: [Wright, Megan](#); [Vrahoretis, Susan](#); [Martin, Jody](#)
Subject: Exemption for safety wet bulb (non-coincident) air temperature
Date: Thursday, February 08, 2018 5:18:17 PM
Attachments: [image2018-02-07-174102.pdf](#)
[Turkey Point COLA Part 7 Departures.pdf](#)

Andrea,

We talk to Brooke yesterday, and informed her that this exemption was left out of the draft Turkey Point licenses. Please note this is the Tier 1 *safety* wet bulb air temp, and not the Tier 2 *normal* wet bulb air temp, which we discussed last week and does not need an exemption. The safety wet bulb temp is in the AP1000 DCD at Table 5.0-1 (Tier 1), and is also listed in Tier 2 at Table 2-1 (attached). The departure is discussed in the Application, Part 7, at 7-33 to 7-35 (attached), in SECY 16-0136 at 17-18, and SER section 2.0.4 at 2-9 to 2-11 and sec. 2.3.1.4.5. We had suggested to Brooke that the exemption belonged in Turkey Point license condition 2.F.(4).

We spoke to the staff, and they suggested that the exemption should be in condition 2.F.(2) rather than 2.F.(4). The staff suggestion would follow the Summer license, which grants an exemption from the rule requirement in 10 CFR Part 52. App. D, sec. IV.A.2.d, for the applicant to include information in the application to show the site parameters are met (with particular reference to safety wet bulb (non-coincident) air temp). This appears sufficient to me. Here are the ADAMS links to the staff markup for your information:

[View ADAMS Properties ML17088A295](#)

[Open ADAMS Document \(Turkey Point Unit 6 COL without Appendices\)](#)

[View ADAMS Properties ML17088A311](#)

[Open ADAMS Document \(Turkey Point Unit 7 COL without Appendices\)](#)

Turkey Point Condition 2.F.(4), which goes to “exemptions associated with departures from Tier 1 and generic [TS],” and is identical to the Levy Condition for Tier 1 departures, also appears to address this issue, since FPL is departing from Tier 1, Table 5.0-1, in regard to the value of the safety wet bulb (non-coincident) temp (the Summer license does not

have a condition like this one). It might look odd to omit the safety wet bulb temp from the Turkey Point list in condition 2.F.(4). Further, the essence of a departure from a site parameter is, to me, the different value used, rather than relief from the application information requirement. It seems that departures from site parameters should be covered in both sections. Whatever OCAA decides, we will consider how to structure the exemption condition in future licenses to account for that possibility and take this as a lesson-learned.

As an alternative, we could augment the staff approach by adding another bullet to Turkey Pt condition 2.F.(4) to address the App. D, sec. VIII.A.4 requirements and special circumstances for the safety wet bulb temp, and add condition 2.F.(4)(f) to list "PTN DEP 2.0-3 (exemption from Tier 1)." (It could also be condition 2.F.(4)(a) and renumber the rest of them to keep them in numerical order.) But this would look different from Levy.

Please call or e-mail me if you have any questions or need any further information,

Thanks,
Bob

Robert M. Weisman
Special Counsel for New Reactor Licensing, New Reactor Programs
Office of the General Counsel, USNRC
Mail Stop O 16 F-3
(301) 287.9177
(301) 415.3725 (FAX)

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Florida Power & Light Company
Turkey Point Plant, Units 6 & 7
COL Application

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The following departures are described and evaluated in Part A, STD and PTN Departures, of this report.

A.1 Departures That Can Be Implemented Without Prior NRC Approval

Departure Number	Description
STD DEP 1.1-1	Administrative departure for organization and numbering for the FSAR sections and subsections
PTN DEP 1.8-1	Correction of an inconsistency in regulatory citation in an interface description
PTN DEP 2.0-2	Maximum normal wet bulb (noncoincident) air temperature
PTN DEP 2.0-4	Population distribution exclusion area (site)
PTN DEP 2.5-1	DELETED
PTN DEP 3.11-1	Revision of “Envir. Zone” numbers for Spent Fuel Pool Level Instruments
PTN DEP 6.3-1	Quantification of the term “indefinitely” as used in the DCD for maintenance of safe shutdown conditions using the PRHR HX during non-LOCA accidents
STD DEP 8.3-1	Class 1E voltage regulating transformer current limiting features
PTN DEP 9.3-1	DELETED
PTN DEP 18.8-1	Operations support center location
PTN DEP 18.8-2	Technical support center location
PTN DEP 19.58-1	Severe winds and tornadoes

A.2 Departures That Require NRC Approval Prior to Implementation

Departure Number	Description
PTN DEP 2.0-1	Operating basis wind speed
PTN DEP 2.0-3	Maximum safety wet bulb (noncoincident) air temperature
PTN DEP 3.2-1	Addition of downspouts to the condensate return portion of the Passive Core Cooling System
PTN DEP 6.2-1	The ITAAC Acceptance Criteria for the in-containment PXS compartment vents are revised to reflect the current plant configuration
PTN DEP 6.4-1	Main Control Room Operator Dose
PTN DEP 6.4-2	Main Control Room Heatup
PTN DEP 7.3-1	Compliance with IEEE 603

The following exemptions are being requested in Part B, Turkey Point Units 6 & 7 Exemption Requests, of this report.

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B. Turkey Point Units 6 & 7 Exemption Requests

Exemption Number	Description
B.1	Combined License (COL) Application organization and numbering
B.2	Maximum safety wet bulb (noncoincident) air temperature
B.3	DELETED
B.4	Special Nuclear Material (SNM) Material Control and Accounting Program Description
B.5	Combustible Gas Control in Containment
B.6	Source Range Neutron Flux Doubling Block Permissive
B.7	Main Control Room Heatup
B.8	Containment Cooling Changes in regard to Passive Core Cooling System Condensate Return
B.9	Main Control Room Dose

Turkey Point Units 6 & 7
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A. STD and PTN Departures

This Departure Report includes deviations in the Turkey Point Units 6 & 7 COL Application FSAR from the information in the applicable DCD, pursuant to 10 CFR Part 52, Appendix D, Section VIII and Section X.B.1.

A.1 Departures That Can Be Implemented Without Prior NRC Approval

Departure Number	Description
STD DEP 1.1-1	Administrative departure for organization and numbering for the FSAR sections and subsections
PTN DEP 1.8-1	Correction of an inconsistency in regulatory citation in an interface description
PTN DEP 2.0-2	Maximum normal wet bulb (noncoincident) air temperature
PTN DEP 2.0-4	Population distribution exclusion area (site)
PTN DEP 2.5-1	DELETED
PTN DEP 3.11-1	Revision of "Envir. Zone" numbers for Spent Fuel Pool level Instruments
PTN DEP 6.3-1	Quantification of the term "indefinitely" as used in the DCD for maintenance of safe shutdown conditions using the PRHR HX during non-LOCA accidents
STD DEP 8.3-1	Class 1E voltage regulating transformer current limiting features
PTN DEP 9.3-1	DELETED
PTN DEP 18.8-1	Operations support center location
PTN DEP 18.8-2	Technical support center location
PTN DEP 19.58-1	Severe winds and tornadoes

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Departure Number: STD DEP 1.1-1

AFFECTED DCD/FSAR SECTIONS:

2.1.1; 2.1.4; 2.2.1; 2.2.4; 2.4.1; 2.4.15; 2.5; 2.5.6; 9.2.11; 9.2.12; 9.2.13; 9.2.14; 9.5.1.8; 9.5.1.9; 13.1; 13.1.4; 13.5; 13.5.3; 13.7; 17.5; 17.6; 17.7; 17.8 (Note the affected sections may vary in subsequent COL Applications, but the departure is standard).

SUMMARY OF DEPARTURE:

This FSAR generally follows the AP1000 DCD organization and numbering. Some organization and numbering differences are adopted where necessary to include additional material, such as additional content identified in Regulatory Guide 1.206.

SCOPE/EXTENT OF DEPARTURE:

The renumbered sections associated with this departure are identified in the FSAR (at the sections identified above).

DEPARTURE JUSTIFICATION:

An administrative departure is established to identify instances where the renumbering of FSAR sections is necessary to effectively include content consistent with Regulatory Guide 1.206, as well as NUREG-0800, Standard Review Plan.

DEPARTURE EVALUATION:

This departure is an administrative change that affects only section numbering of the indicated FSAR sections. Accordingly, it does not:

1. Result in more than a minimal increase in the frequency of occurrence of an accident previously evaluated in the plant-specific DCD.
2. Result in more than a minimal increase in the likelihood of occurrence of a malfunction of a structure, system, or component (SSC) important to safety and previously evaluated in the plant-specific DCD.
3. Result in more than a minimal increase in the consequences of an accident previously evaluated in the plant-specific DCD.

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Departure Number: STD DEP 1.1-1 (continued)

4. Result in more than a minimal increase in the consequences of a malfunction of an SSC important to safety previously evaluated in the plant-specific DCD.
5. Create a possibility for an accident of a different type than any evaluated previously in the plant-specific DCD.
6. Create a possibility for a malfunction of an SSC important to safety with a different result than any evaluated previously in the plant-specific DCD.
7. Result in a design basis limit for a fission product barrier as described in the plant-specific DCD being exceeded or altered.
8. Result in a departure from a method of evaluation described in the plant-specific DCD used in establishing the design bases or in the safety analyses.

This departure does not affect resolution of a severe accident issue identified in the plant-specific DCD. Therefore, this departure has no safety significance.

NRC APPROVAL REQUIREMENT:

This departure does not require NRC approval pursuant to 10 CFR Part 52, Appendix D, Section VIII.B.5.

This departure requires an exemption from 10 CFR Part 52, Appendix D, Section IV.A.2.a. Therefore, an exemption is requested in Part B of this COL Application part.

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Departure Number: PTN DEP 1.8-1

AFFECTED DCD/FSAR SECTIONS:

DCD Table 1.8-1 (Sheet 6 of 6); FSAR Table 1.8-203 (Sheet 6 of 6)

SUMMARY OF DEPARTURE:

DCD Tier 2 Table 1.8-1 (Sheet 6 of 6), Item 13.1, is changed to correct an inconsistency in the DCD. The DCD Item 13.1 references 10 CFR 50, Appendix O, for features that may affect plans for coping with emergencies as opposed to the Part 52 requirements contained in 10 CFR 52.137(a)(11).

SCOPE/EXTENT OF DEPARTURE:

This departure is identified in FSAR Table 1.8-203 (Sheet 6 of 6), Item 13.1. FSAR Table 1.8-203 replaced DCD Table 1.8-1.

The interface description in DCD Table 1.8-1 (Sheet 6 of 6), Item 13.1, is revised from “Features that may affect plans for coping with emergencies as specified in 10 CFR 50, Appendix O” to “The information pertaining to design features that affect plans for coping with emergencies in the operation of the reactor facility or a major portion thereof as specified in 10 CFR 52.137(a)(11)”.

DEPARTURE JUSTIFICATION:

Appendix O was transferred from Part 50 to Part 52, effective May of 1989, although the NRC neglected to physically remove the Appendix O text from Part 50. Appendix O text was not physically removed from Part 50 until the reorganization of the regulations was published in August of 2007. In the August 2007 reorganization the content of Appendix O in Part 52 was relocated to the new Subpart E of Part 52. This relocation of the regulation impacts DCD Tier 2 Table 1.8-1 (Sheet 6 of 6), Summary of AP1000 Plant Interfaces with Remainder of Plant, Item 13.1, Features that may affect plans for coping with emergencies as specified in 10 CFR 50, Appendix O, as referenced to DCD Section 13.3, is replaced with “The information pertaining to design features that affect plans for coping with emergencies in the operation of the reactor facility or a major portion thereof as specified in 10 CFR 52.137(a)(11)”. There is no change in requirements, only a relocation to another regulation. In conclusion, this is a departure from DCD Tier 2 Table 1.8-1, (Sheet 6 of 6), Item 13.1, which will be reflected in COLA Table 1.8-203, (Sheet 6 of 6), Item 13.1.

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Departure Number: PTN DEP 1.8-1 (continued)

DEPARTURE EVALUATION:

This Tier 2 departure revises DCD Table 1.8-1 (Sheet 6 of 6), Item 13.1. This departure does not result in any adverse affects to design features that affect plans for coping with emergencies in the operation of the reactor facility or a major portion thereof. Therefore, this departure does not:

1. Result in more than a minimal increase in the frequency of occurrence of an accident previously evaluated in the plant-specific DCD.
2. Result in more than a minimal increase in the likelihood of occurrence of a malfunction of an SSC important to safety and previously evaluated in the plant-specific DCD.
3. Result in more than a minimal increase in the consequences of an accident previously evaluated in the plant-specific DCD.
4. Result in more than a minimal increase in the consequences of a malfunction of an SSC important to safety previously evaluated in the plant-specific DCD.
5. Create a possibility for an accident of a different type than any evaluated previously in the plant-specific DCD.
6. Create a possibility for a malfunction of an SSC important to safety with a different result than any evaluated previously in the plant-specific DCD.
7. Result in a design basis limit for a fission product barrier as described in the plant-specific DCD being exceeded or altered.
8. Result in a departure from a method of evaluation described in the plant-specific DCD used in establishing the design bases or in the safety analyses.

This departure does not affect resolution of a severe accident issue identified in the plant-specific DCD. Therefore, this departure has no safety significance.

NRC APPROVAL REQUIREMENT:

This departure does not require NRC approval pursuant to 10 CFR Part 52, Appendix D, Section VIII.B.5.

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Departure Number: PTN DEP 2.0-2

AFFECTED DCD/FSAR SECTIONS:

2.0; 2.3.1.5; 9.2.1.2; 9.2.7.2

SUMMARY OF DEPARTURE:

The DCD site parameter value for the maximum normal air temperature wet bulb (noncoincident) in DCD Tier 2, Table 2-1 is 80.1°F. The corresponding site characteristic value is 81.5°F as reported in FSAR Subsection 2.3.1.5. This site characteristic exceeds the DCD site parameter by 1.4°F.

SCOPE/EXTENT OF DEPARTURE:

The section and subsection associated with this departure are identified in the FSAR (at the section and subsection identified above).

DEPARTURE JUSTIFICATION:

The maximum normal wet bulb (noncoincident) air temperature for Units 6 & 7 is 81.5°F. This is the 0.4 percent annual exceedance value as reported in FSAR Subsection 2.3.1.5. This value is approximately equivalent to the 1 percent seasonal exceedance value, as stated in note (b) of DCD Table 2-1. This temperature exceeds the DCD site parameter of 80.1°F by 1.4°F. Analysis of the maximum normal wet bulb (noncoincident) air temperature for Units 6 & 7 has been performed. The results of this analysis show that the higher site characteristic temperature will not adversely affect any SSCs, their functional capability, or analysis methods as presented in the DCD.

Specifically, the following evaluations were performed with the following results:

- Design Basis Heating Ventilation Air Conditioning Systems Operation

The increase in wet bulb temperature will impact the standard plant design of the chilled water system (VWS) high capacity subsystem. To accommodate the impact of the higher wet bulb temperature on HVAC margins, the size of the air-cooled chillers in the VWS high capacity subsystem will be increased. The current VWS high capacity subsystem has two 1700-ton water cooled chillers coupled with two 300-ton air-cooled chillers. Replacing the two 300-ton air-cooled chillers with 400-ton air cooled chillers will maintain adequate HVAC design margins and allow the VWS high capacity subsystem to meet the increased load due to higher wet bulb design basis. There is no impact on the performance of SSCs important to safety or to analysis methods as a result of the increase in maximum normal wet bulb temperature.

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Departure Number: PTN DEP 2.0-2 (continued)

- Maximum Spent Fuel Pool Temperatures

A SFS heat exchanger design will satisfy DCD Spent Fuel Pool temperature requirements taking into account elevated site wet bulb ambient temperatures and elevated CCS temperatures. All spent fuel pool temperature limit criteria are met with ambient wet bulb temperatures as specified for each case identified in the DCD.

- Service Water System (SWS) Maximum Cooling Water Temperature of 88.5°F at Design Peak SWS Heat Duty

At conservative, yet more realistic best estimate conditions, the SWS demonstrates a capability to deliver water to the CCS heat exchanger at less than 88.5°F and meets the plant cooldown commitments with a maximum normal wet bulb temperature. This meets the acceptance criteria established for this analysis. SWS cold water temperature rises to 89.8°F with peak CCS/SWS heat duty four hours after reactor shutdown (beginning of cooldown), with an ambient wet bulb temperature of 81.5°F.

- Maximum Reactor Coolant System Cooldown Times

Two cooldown cases have been analyzed:

Case 1: 1 percent exceedance wet bulb temperature and operation of the blowdown HX.

Case 2: 1 percent exceedance wet bulb temperature and no credit taken for the operation of the blowdown HX.

The cooldown capability to 125°F within 96 hours can be met at ambient wet bulb temperature of 81.5°F.

- Turbine Building Closed Cooling Water (TCS) Maximum Temperature Limit of 105°

The temperature of the TCS cooling water supplied to turbine and generator auxiliaries is lower than 105°F for the maximum ambient wet bulb temperature of 81.5°F. The plant can operate at full output at the maximum normal wet bulb condition without any restriction imposed by turbine or generator auxiliary cooling requirements.

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Departure Number: PTN DEP 2.0-2 (continued)

DEPARTURE EVALUATION:

The effect of the site-specific maximum normal wet bulb temperature of 81.5°F (noncoincident) versus the DCD value of 80.1°F on SSCs important to safety or analyses described in the DCD was evaluated. The change to maximum normal wet bulb temperature does not affect the function of any SSCs important to safety or analysis methods as presented in the DCD. The following summarizes the evaluation:

1. Increase VWS high capacity subsystem chiller refrigeration tonnage by 100 tons (total 2100 tons per train) by increasing the capacity of the air-cooled VWS high capacity subsystem chillers to 400 tons. No change to VWS low capacity subsystem chiller tonnage is required.
2. All spent fuel pool temperature limit criteria are met with ambient wet bulb temperatures as specified for each case identified in the DCD.
3. SWS cold water temperature increases to 89.8°F with peak CCS/SWS heat duty four hours after reactor shutdown (beginning of cooldown) with ambient wet bulb temperature of 81.5°F. With a conservative realistic design basis the SWS cold water temperature remains at or below 88.5°F with CCS/SWS heat duty at four hours after reactor shutdown (beginning of cooldown) and an ambient wet bulb temperature of 81.5°F.
4. The cooldown capability to 125°F within 96 hours can be met at ambient wet bulb temperature of 81.5°F.
5. TCS supply temperature remains below 105°F for all ambient wet bulb conditions, including the maximum normal value of 81.5°F.

Therefore, this departure does not:

1. Result in more than a minimal increase in the frequency of occurrence of an accident previously evaluated in the plant-specific DCD.
2. Result in more than a minimal increase in the likelihood of occurrence of a malfunction of an SSC important to safety and previously evaluated in the plant-specific DCD.
3. Result in more than a minimal increase in the consequences of an accident previously evaluated in the plant-specific DCD.
4. Result in more than a minimal increase in the consequences of a malfunction of an SSC important to safety previously evaluated in the plant-specific DCD.

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Departure Number: PTN DEP 2.0-2 (continued)

5. Create a possibility for an accident of a different type than any evaluated previously in the plant-specific DCD.
6. Create a possibility for a malfunction of an SSC important to safety with a different result than any evaluated previously in the plant-specific DCD.
7. Result in a design basis limit for a fission product barrier as described in the plant-specific DCD being exceeded or altered.
8. Result in a departure from a method of evaluation described in the plant-specific DCD used in establishing the design bases or in the safety analyses.

This departure does not affect resolution of a severe accident issue identified in the plant-specific DCD. Therefore, this departure has no safety significance.

NRC APPROVAL REQUIREMENT:

This departure does not require NRC approval pursuant to 10 CFR Part 52, Appendix D, Section VIII.B.5.

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Departure Number: PTN DEP 2.0-4

AFFECTED DCD/FSAR SECTIONS:

2.0; 2.1.2; 2.3.4.2

SUMMARY OF DEPARTURE:

DCD Table 2-1 lists a site parameter for the population distribution exclusion area (site) of 0.5 miles. The distance from the Units 6 & 7 source boundary to the exclusion area boundary (EAB) and the atmospheric dispersion value (X/Q) at the EAB are listed in the following table:

Sector	Distance to EAB (feet)	Distance to EAB (miles)	X/Q (sec/m ³) 0-2 Hours
S	2756	0.52	2.51E-04
SSW	2687	0.51	1.03E-04
SW	2375	0.45	1.25E-04
WSW	2559	0.49	1.17E-04
W	2566	0.49	1.38E-04
WNW	2589	0.49	1.33E-04
NW	2513	0.48	1.39E-04
NNW	2516	0.48	1.18E-04
N	2516	0.48	1.10E-04
NNE	2516	0.48	1.23E-04
NE	1427	0.27	3.54E-04
ENE	1503	0.29	3.26E-04
E	1572	0.30	3.92E-04
ESE	1932	0.37	3.51E-04
SE	1923	0.37	4.19E-04
SSE	2782	0.53	3.04E-04

All sector distances, except for S, SSW, and SSE sectors, are less than the 0.5 mile site parameter, with the minimum being 0.27 miles in the northeast sector.

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Departure Number: PTN DEP 2.0-4 (continued)

SCOPE/EXTENT OF DEPARTURE:

The section and subsection associated with this departure is identified in the FSAR (at the section and subsection identified above).

DEPARTURE JUSTIFICATION:

DCD Table 2-1 lists the site parameter for the X/Q at the site boundary (0 – 2 hr) to be $\leq 5.1\text{E-}04$ sec/m³. Note (e) to this table states that the terms “site boundary” and “exclusion area boundary” are used interchangeably in the DCD. Therefore, this X/Q site parameter applies to the exclusion area boundary and is the limiting parameter, not distance. As listed in the above table, all the X/Q values in all the sectors are below the $5.1\text{E-}04$ sec/m³ DCD site parameter limit for X/Q.

DEPARTURE EVALUATION:

This departure does not affect the design or function of any SSCs. Therefore, this departure does not:

1. Result in more than a minimal increase in the frequency of occurrence of an accident previously evaluated in the plant-specific DCD.
2. Result in more than a minimal increase in the likelihood of occurrence of a malfunction of an SSC important to safety and previously evaluated in the plant-specific DCD.
3. Result in more than a minimal increase in the consequences of an accident previously evaluated in the plant-specific DCD.
4. Result in more than a minimal increase in the consequences of a malfunction of an SSC important to safety previously evaluated in the plant-specific DCD.
5. Create a possibility for an accident of a different type than any evaluated previously in the plant-specific DCD.
6. Create a possibility for a malfunction of an SSC important to safety with a different result than any evaluated previously in the plant-specific DCD.
7. Result in a design basis limit for a fission product barrier as described in the plant-specific DCD being exceeded or altered.

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Departure Number: PTN DEP 2.0-4 (continued)

8. Result in a departure from a method of evaluation described in the plant-specific DCD used in establishing the design bases or in the safety analyses.

This departure does not affect resolution of a severe accident issue identified in the plant-specific DCD. Therefore, this departure has no safety significance.

NRC APPROVAL REQUIREMENT:

This departure does not require NRC approval pursuant to 10 CFR Part 52, Appendix D, Section VIII.B.5.

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Departure Number: PTN DEP 2.5-1

DELETED

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Departure Number: PTN DEP 3.11-1

AFFECTED DCD/FSAR SECTIONS:

DCD Table 3.11-1 (Sheet 14 of 51)

SUMMARY OF DEPARTURE:

DCD Table 3.11-1 (Sheet 14 of 51) "Envir. Zone" numbers for Spent Fuel Pool Level Instruments SFS-JE-LT019A, SFS-JE-LT019B, and SFS-JE-LT019C are changed to correct an inconsistency in the DCD. All 3 instruments currently have a Environmental Zone number of "11." SFS-JE-LT019A is changed to Envir. Zone 6, SFS-JE-LT019B is changed to Envir. Zone 7 and SFS-JE-LT019C is changed to Envir. Zone 6 in DCD Table 3.11-1 (Sheet 14 of 51).

SCOPE/EXTENT OF DEPARTURE:

SFS-JE-LT019A is revised to Envir. Zone 6, SFS-JE-LT019B is revised to Envir. Zone 7 and SFS-JE-LT019C is revised to Envir. Zone 6 in DCD Table 3.11-1 (Sheet 14 of 51).

DEPARTURE JUSTIFICATION:

The actual location of the Spent Fuel Pool Level instruments is not being changed from the designed location in this departure. The environmental zones the instruments are located in are being revised to be consistent with the designed instrument location. The AP1000 SFP level transmitters are located in rooms outside of the Fuel Handling Area in the Auxiliary Building. Per Westinghouse design documents, Spent Fuel Pool Level channels 019A and 019C are in room 12365 and channel 019B is in room 12341. Room 12365 is in Zone 6 on DCD Table 3.D.5-1 (Sheet 2 of 3). Room 12341 is in Zone 7 on DCD Table 3.D.5-1 (Sheet 2 of 3). Based on this information, SFS-JE-LT019A is being changed to Envir. Zone 6, SFS-JE-LT019B is being changed to Envir. Zone 7 and SFS-JE-LT019C is being changed to Envir. Zone 6 in DCD Table 3.11-1 (Sheet 14 of 51).

DCD Table 3.11-1 Environmental Zone numbers for Spent Fuel Pool Level provide a reference to environmental conditions in the associated instrument location correlated to an environmental zone in DCD Table 3D.5-1 for "Normal Operating Environments," DCD Table 3D.5-4 for "Abnormal Operating Environments Outside Containment" and DCD Table 3D.5-5 for "Accident Environments." The environmental qualification of the instrument is consistent with conditions identified for the associated environmental zone. Revising the Spent Fuel Pool Level instruments' environmental zone to accurately reflect their actual location will ensure they are environmentally qualified to function properly during normal, abnormal, and accident conditions.

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Departure Number: PTN DEP 3.11-1 (continued)

DEPARTURE EVALUATION:

This Tier 2 departure revises SFS-JE-LT019A Envir. Zone from 11 to 6, SFS-JE-LT019B Envir. Zone from 11 to 7, and SFS-JE-LT019C Envir. Zone from 11 to 6 in DCD Table 3.11-1 (Sheet 14 of 51). This departure does not result in any adverse affects to the SFP level indication design function and does not change the environmental qualification methodology. Therefore, this departure does not:

1. Result in more than a minimal increase in the frequency of occurrence of an accident previously evaluated in the plant-specific DCD.
2. Result in more than a minimal increase in the likelihood of occurrence of a malfunction of an SSC important to safety and previously evaluated in the plant-specific DCD.
3. Result in more than a minimal increase in the consequences of an accident previously evaluated in the plant-specific DCD.
4. Result in more than a minimal increase in the consequences of a malfunction of an SSC important to safety previously evaluated in the plant-specific DCD.
5. Create a possibility for an accident of a different type than any evaluated previously in the plant-specific DCD.
6. Create a possibility for a malfunction of an SSC important to safety with a different result than any evaluated previously in the plant-specific DCD.
7. Result in a design basis limit for a fission product barrier as described in the plant specific DCD being exceeded or altered.
8. Result in a departure from a method of evaluation described in the plant-specific DCD used in establishing the design bases or in the safety analyses.

This departure does not affect resolution of a severe accident issue identified in the plant specific DCD. Therefore, this departure has no safety significance.

NRC APPROVAL REQUIREMENT:

This departure does not require NRC approval pursuant to 10 CFR Part 52, Appendix D, Section VIII.B.5.

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Departure Number PTN DEP 6.3-1

AFFECTED DCD/FSAR SECTIONS:

Subsection 5.4.14.1, Subsections 6.3.1.1.1, 6.3.1.2, 6.3.1.3, 6.3.2.1.1, and 6.3.3.4.1, Subsection 7.4.1.1, Table 9.5.1-1 (Sheet 11), Subsection 15.2.6.1, Table 19.59-18 (Sheet 6), and Subsection 19E.4.10.2

SUMMARY OF DEPARTURE:

The Passive Residual Heat Removal Heat Exchanger (PRHR HX) has a functional requirement to be able to bring the AP1000 plant to a stable condition for events not involving a loss of coolant (i.e., non-LOCA event), DCD 6.3.1.1.4. The DCD in Subsection 6.3.1.1.1 further states “The PRHR HX in conjunction with the passive containment cooling system, is designed to remove decay heat for an indefinite time in a closed-loop mode of operation.” Additional evaluations have been subsequently performed that have identified that the use of the term “indefinite” does not describe the predicted PRHR HX long term operation properly. The word “indefinite” can be defined as an “unknown” or “unidentified” length of time; “indefinite” does not mean “infinite” which means having no boundaries or limits in time. The word “indefinite” in regards to PRHR HX long term operation needs to be changed with a definitive time period.

SCOPE/EXTENT OF DEPARTURE:

There are additional areas in the DCD that use the term “indefinite” in reference to long term PRHR HX operation that need to be changed in a departure to the DCD to more accurately reflect the PRHR HX long term operation during a non-LOCA event. The changes needed for the DCD departure PTN DEP 6.3-1 to incorporate this information include the following FSAR Sections or Tables:

Section 5.4.14.1
Section 6.3.1.1.1
Section 6.3.1.2
Section 6.3.1.3
Section 6.3.2.1.1
Section 6.3.3.4.1
Section 7.4.1.1
Table 9.5.1-1R
Section 15.2.6.1
Table 19.59-18R
Section 19E.4.10.2

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Departure Number: PTN DEP 6.3-1 (continued)

DEPARTURE JUSTIFICATION:

Recent PRHR HX evaluations performed under a variety of operating scenarios identified 14 days would be a conservative replacement time period for “indefinite”. The Westinghouse evaluation of the PRHR HX operation under non-bounding, conservative conditions demonstrates the ability to keep the average RCS temperature in safe shutdown conditions for greater than 14 days under passive conditions (no operator action). The evaluation does indicate that if no action is taken, the average RCS temperature will increase at some point after 15 days but the PRHR HX operation would still keep the average RCS temperature below 420°F for a longer period of time of approximately 20 days (420°F is identified as the RCS temperature objective for safe shutdown). If no action is able to be taken after this period of time and there is adverse trending of RCS conditions that might be indicative of leading to an unstable condition, the operators do still have the ability to initiate Automatic Depressurization System (ADS), go to open loop cooling and retain the plant in a stable condition.

DEPARTURE EVALUATION:

This Tier 2 departure is associated with defining the term “indefinite” as a conservative but specific duration (greater than 14 days). The departure results in a change to the DCD that does not impact the required design function (i.e., containment cooling condensate return). Accordingly, it does not:

1. Result in more than a minimal increase in the frequency of occurrence of an accident previously evaluated in the plant-specific DCD.
2. Result in more than a minimal increase in the likelihood of occurrence of a malfunction of an SSC important to safety and previously evaluated in the plant-specific DCD.
3. Result in more than a minimal increase in the consequences of an accident previously evaluated in the plant-specific DCD.
4. Result in more than a minimal increase in the consequences of a malfunction of an SSC important to safety previously evaluated in the plant-specific DCD.
5. Create a possibility for an accident of a different type than any evaluated previously in the plant-specific DCD.
6. Create a possibility for a malfunction of an SSC important to safety with a different result than any evaluated previously in the plant-specific DCD.
7. Result in a design basis limit for a fission product barrier as described in the plant-specific DCD being exceeded or altered.

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Departure Number: PTN DEP 6.3-1 (continued)

8. Result in a departure from a method of evaluation described in the plant-specific DCD used in establishing the design bases or in the safety analyses.

This departure does not affect resolution of a severe accident issue identified in the plant-specific DCD. Therefore, this departure has no safety significance.

NRC APPROVAL REQUIREMENT:

This departure does not require NRC approval pursuant to 10 CFR Part 52, Appendix D, Section VIII.B.5.

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Departure Number: STD DEP 8.3-1

AFFECTED DCD/FSAR SECTIONS:

8.3.2.2

SUMMARY OF DEPARTURE:

The DCD states that the Class 1E battery chargers and Class 1E voltage regulating transformers are designed to limit the input (ac) current to an acceptable value under faulted conditions on the output side. However, the AP1000 voltage regulating transformers do not have active components to limit current.

SCOPE/EXTENT OF DEPARTURE:

This departure is identified in FSAR Subsection 8.3.2.2.

DEPARTURE JUSTIFICATION:

DCD Subsection 8.3.2.2 states that the Class 1E voltage regulating transformers have built-in circuit breakers at the input and output sides for protection and isolation. The circuit breakers are coordinated and periodically tested to verify their designed coordination and isolation function. They are qualified as isolation devices between Class 1E and non-Class 1E circuits in accordance with IEEE 384 and Regulatory Guide 1.75. Since the isolation and protection function is provided by the breakers, there is no need for the voltage regulating transformers to have current limiting capability. This departure does not adversely affect any safety-related system, nor does it conflict with applicable regulatory guidance.

DEPARTURE EVALUATION:

This Tier 2 departure is associated with isolation between Class 1E loads and the non-Class 1E ac power source. The departure results in a change to the DCD that does not impact the required design function (i.e., isolation). Accordingly, it does not:

1. Result in more than a minimal increase in the frequency of occurrence of an accident previously evaluated in the plant-specific DCD.
2. Result in more than a minimal increase in the likelihood of occurrence of a malfunction of a structure, system, or component (SSC) important to safety and previously evaluated in the plant-specific DCD.
3. Result in more than a minimal increase in the consequences of an accident previously evaluated in the plant-specific DCD.

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Departure Number: STD DEP 8.3-1 (continued)

4. Result in more than a minimal increase in the consequences of a malfunction of an SSC important to safety previously evaluated in the plant-specific DCD.
5. Create a possibility for an accident of a different type than any evaluated previously in the plant-specific DCD.
6. Create a possibility for a malfunction of an SSC important to safety with a different result than any evaluated previously in the plant-specific DCD.
7. Result in a design basis limit for a fission product barrier as described in the plant-specific DCD being exceeded or altered.
8. Result in a departure from a method of evaluation described in the plant-specific DCD used in establishing the design bases or in the safety analyses.

This departure does not affect resolution of a severe accident issue identified in the plant-specific DCD. Therefore, this departure has no safety significance.

NRC APPROVAL REQUIREMENT:

This departure does not require NRC approval pursuant to 10 CFR Part 52, Appendix D, Section VIII.B.5.

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Departure Number: PTN DEP 9.3-1

DELETED

Turkey Point Units 6 & 7
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Part 7 — Departures and Exemption Requests

Departure Number: PTN DEP 18.8-1

AFFECTED DCD/FSAR SECTIONS:

1.2.3; 9.4.2.2; 9A; 12.3.1.2; 12.5.2.2; 12.5.3.2; 18.8.3.6

SUMMARY OF DEPARTURE:

The Operations Support Center (OSC) is being moved from the location identified in DCD Subsections 18.8.3.6, 12.5.2.2, and 12.5.3.2 and as identified on DCD figures in Subsections 1.2, 12.3, and Appendix 9A. There will be a single OSC for Units 6 & 7 located as described in the Emergency Plan.

SCOPE/EXTENT OF DEPARTURE:

The sections and subsections associated with this departure are identified in the FSAR (at the sections and subsections identified above).

DEPARTURE JUSTIFICATION:

The referenced DCD states, "The ALARA briefing and operations support center is located off the main corridor immediately beyond the main entry to the annex building," and indicates that the OSC location is identified on Figure 1.2-18. For Units 6 & 7, the OSC is being moved, as described in the Emergency Plan, and one OSC will serve both Units 6 & 7 to optimize use of space and operational resources.

DEPARTURE EVALUATION:

This departure is for a non-safety-related system, and the alternate location of the OSC meets applicable requirements. Relocating the OSC does not adversely affect its function and therefore this departure does not:

1. Result in more than a minimal increase in the frequency of occurrence of an accident previously evaluated in the plant-specific DCD.
2. Result in more than a minimal increase in the likelihood of occurrence of a malfunction of an SSC important to safety and previously evaluated in the plant-specific DCD.
3. Result in more than a minimal increase in the consequences of an accident previously evaluated in the plant-specific DCD.
4. Result in more than a minimal increase in the consequences of a malfunction of an SSC important to safety previously evaluated in the plant-specific DCD.

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Departure Number: PTN DEP 18.8-1 (continued)

5. Result in more than a minimal increase in the consequences of a malfunction of an SSC important to safety previously evaluated in the plant-specific DCD.
6. Create a possibility for an accident of a different type than any evaluated previously in the plant-specific DCD.
7. Create a possibility for a malfunction of an SSC important to safety with a different result than any evaluated previously in the plant-specific DCD.
8. Result in a design basis limit for a fission product barrier as described in the plant-specific DCD being exceeded or altered.
9. Result in a departure from a method of evaluation described in the plant-specific DCD used in establishing the design bases or in the safety analyses.

This departure does not affect resolution of a severe accident issue identified in the plant-specific DCD. Therefore, this departure has no safety significance.

NRC APPROVAL REQUIREMENT:

This departure does not require NRC approval pursuant to 10 CFR Part 52, Appendix D, Section VIII.B.5.

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Departure Number: PTN DEP 18.8-2

AFFECTED DCD/FSAR SECTIONS:

18.8.3.5

SUMMARY OF DEPARTURE:

The Technical Support Center (TSC) is not located in the control support area as identified in DCD Subsection 18.8.3.5. The TSC is common for Turkey Point Units 3, 4, 6, and 7 and is located as described in the Emergency Plan.

SCOPE/EXTENT OF DEPARTURE:

The subsection associated with this departure is identified in the FSAR (at the subsection identified above).

DEPARTURE JUSTIFICATION:

The referenced DCD states, "The TSC is located in the control support area (CSA)." This is not the case for Units 6 & 7. The TSC location is moved to a central location as identified in the Emergency Plan, such that a single TSC can serve Units 3, 4, 6, and 7 to optimize use of space and operational resources.

DEPARTURE EVALUATION:

This departure is for a non-safety-related system, and the alternate location of the TSC meets applicable requirements. Relocating the TSC does not adversely affect its function and therefore this departure does not:

1. Result in more than a minimal increase in the frequency of occurrence of an accident previously evaluated in the plant-specific DCD.
2. Result in more than a minimal increase in the likelihood of occurrence of a malfunction of an SSC important to safety and previously evaluated in the plant-specific DCD.
3. Result in more than a minimal increase in the consequences of an accident previously evaluated in the plant-specific DCD.
4. Result in more than a minimal increase in the consequences of a malfunction of an SSC important to safety previously evaluated in the plant-specific DCD.

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Departure Number: PTN DEP 18.8-2 (continued)

5. Create a possibility for an accident of a different type than any evaluated previously in the plant-specific DCD.
6. Create a possibility for a malfunction of an SSC important to safety with a different result than any evaluated previously in the plant-specific DCD.
7. Result in a design basis limit for a fission product barrier as described in the plant-specific DCD being exceeded or altered.
8. Result in a departure from a method of evaluation described in the plant-specific DCD used in establishing the design bases or in the safety analyses.

This departure does not affect resolution of a severe accident issue identified in the plant-specific DCD. Therefore, this departure has no safety significance.

NRC APPROVAL REQUIREMENT:

This departure does not require prior NRC approval pursuant to 10 CFR Part 52, Appendix D, Section VIII.B.5.

Turkey Point Units 6 & 7
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Departure Number: PTN DEP 19.58-1

AFFECTED DCD/FSAR SECTIONS:

19.58

SUMMARY OF DEPARTURE:

As shown in Table 19.58-201, the initiating event frequency for high winds at Units 6 & 7 are higher than those in the DCD. Therefore, a site-specific analysis of high winds and tornadoes was conducted to determine core damage frequency (CDF). The analysis determined the total CDF for Case 1 (loss of offsite power) is $3.3\text{E-}09$, the CDF for Case 2 (loss of offsite power with non-safety systems unavailable for select events) is $1.0\text{E-}08$, and for Case 3 (loss of offsite power with non-safety systems unavailable for all events) the CDF is $2.0\text{E-}08$ per year. These values are higher than the DCD CDF values listed in DCD Table 19.58-3.

SCOPE/EXTENT OF DEPARTURE:

The section associated with this departure is identified in the FSAR (at the section identified above).

DEPARTURE JUSTIFICATION:

The site-specific high winds and tornadoes analysis consists of three case studies, with Case 2 (loss of offsite power with non-safety systems unavailable for select events) considered to be the representative conservative model. Case 1 (loss of offsite power) and Case 3 (loss of offsite power with non-safety systems unavailable for all events) of the analysis are treated as sensitivity studies, with Case 3 being a very conservative scenario. The actual non-safety structures are designed to the Uniform Building Code and offer a degree of robustness such that the failure of all such systems in all events is considered extreme and conservative.

The site-specific CDF for Case 1 is $3.3\text{E-}09$ per year and Case 2 is $1.0\text{E-}08$ per year. These both meet the CDF screening criteria of $1.0\text{E-}08$ per year as described in Westinghouse Technical Report APP-GW-GLR-101, "AP1000 Probabilistic Risk Assessment Site-Specific Considerations," Revision 1, Section 3.0, High Winds Evaluation. Case 3 is slightly above the DCD value of $1.38\text{E-}08$, the result is considered very conservative for the reasons stated above. Therefore, a further detailed PRA for Units 6 & 7 high winds and tornadoes is not necessary. The complete discussion of the site-specific high winds and tornadoes analysis is provided in FSAR Section 19.58.

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Departure Number: PTN DEP 19.58-1 (continued)

DEPARTURE EVALUATION:

As reported in FSAR Section 19.58, the CDF for Case 2 of the high winds hazard evaluation is not greater than the $1.0\text{E-}08$ per year screening criteria. Consequently, further detailed PRA is not necessary for the Units 6 & 7 High Winds and Tornado analysis.

Therefore, this departure does not:

1. Result in more than a minimal increase in the frequency of occurrence of an accident previously evaluated in the plant-specific DCD.
2. Result in more than a minimal increase in the likelihood of occurrence of a malfunction of an SSC important to safety and previously evaluated in the plant-specific DCD.
3. Result in more than a minimal increase in the consequences of an accident previously evaluated in the plant-specific DCD.
4. Result in more than a minimal increase in the consequences of a malfunction of an SSC important to safety previously evaluated in the plant-specific DCD.
5. Create a possibility for an accident of a different type than any evaluated previously in the plant-specific DCD.
6. Create a possibility for a malfunction of an SSC important to safety with a different result than any evaluated previously in the plant-specific DCD.
7. Result in a design basis limit for a fission product barrier as described in the plant-specific DCD being exceeded or altered.
8. Result in a departure from a method of evaluation described in the plant-specific DCD used in establishing the design bases or in the safety analyses.

This departure does not affect resolution of a severe accident issue identified in the plant-specific DCD. Therefore, this departure has no safety significance.

NRC APPROVAL REQUIREMENT:

This departure does not require NRC approval pursuant to 10 CFR Part 52, Appendix D, Section VIII.B.5.

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A.2 Departures That Require NRC Approval Prior to Implementation

Departure Number	Description
PTN DEP 2.0-1	Operating basis wind speed
PTN DEP 2.0-3	Maximum safety wet bulb (noncoincident) air temperature
PTN DEP 3.2-1	Addition of downspouts to the condensate return portion of the Passive Core Cooling System
PTN DEP 6.2-1	The ITAAC Acceptance Criteria for the in-containment PXS compartment vents are revised to reflect the current plant configuration
PTN DEP 6.4-1	Main Control Room Operator Dose
PTN DEP 6.4-2	Main Control Room Heatup
PTN DEP 7.3-1	Compliance with IEEE 603

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Departure Number: PTN DEP 2.0-1

AFFECTED DCD/FSAR SECTIONS:

2.0; 2.3.1.3.1; 3.3.1.1; 3.3.3; 3H3.3

SUMMARY OF DEPARTURE:

The DCD site parameter value for operating basis wind speed in DCD Tier 2, Table 2-1 is 145 miles per hour. In DCD Appendix 3H, the operating basis wind speed is a Tier 2* value. The corresponding site characteristic is the 50-year return period, 3-second gust wind speed of 150 miles per hour as reported in FSAR Subsection 2.3.1.3.1. This site characteristic exceeds the DCD site parameter by 5 miles per hour.

SCOPE/EXTENT OF DEPARTURE:

The sections and subsections associated with this departure are identified in the FSAR (at the sections and subsections identified above).

DEPARTURE JUSTIFICATION:

The 50-year return, 3-second gust wind speed for Units 6 & 7 is 150 miles per hour. This wind speed exceeds the DCD site parameter of 145 miles per hour by 5 miles per hour. Analysis of the site characteristic wind speed has been performed and it has been concluded that the increase in wind design speed will not impact the AP1000 design. The safety related structures that are affected by the increase in wind speed are the Auxiliary Building and Shield Building of the Nuclear Island. There are no other safety related SSCs exposed to the wind speeds evaluated. The results of this analysis show that the higher wind speed will not adversely affect any safety-related SSCs.

DEPARTURE EVALUATION:

The wind load does not control the design for the Nuclear Island structures. The Auxiliary Building wall and roof structure design is controlled by tornado, seismic, and accident pressure/temperature. The Shield Building design is controlled by the seismic loads.

From this evaluation, it has been concluded:

1. The Auxiliary Building external walls and roof design is not controlled by the wind load, and an increase of wind speed from 145 mph to 150 mph will not require a redesign of the building.

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Departure Number: PTN DEP 2.0-1 (continued)

2. The Shield Building design is not controlled by the wind load, and an increase of wind speed from 145 mph to 150 mph will not require a redesign of the building.

Therefore, this departure does not:

1. Result in more than a minimal increase in the frequency of occurrence of an accident previously evaluated in the plant-specific DCD.
2. Result in more than a minimal increase in the likelihood of occurrence of a malfunction of an SSC important to safety and previously evaluated in the plant-specific DCD.
3. Result in more than a minimal increase in the consequences of an accident previously evaluated in the plant-specific DCD.
4. Result in more than a minimal increase in the consequences of a malfunction of an SSC important to safety previously evaluated in the plant-specific DCD.
5. Create a possibility for an accident of a different type than any evaluated previously in the plant-specific DCD.
6. Create a possibility for a malfunction of an SSC important to safety with a different result than any evaluated previously in the plant-specific DCD.
7. Result in a design basis limit for a fission product barrier as described in the plant-specific DCD being exceeded or altered.
8. Result in a departure from a method of evaluation described in the plant-specific DCD used in establishing the design bases or in the safety analyses.

This departure does not affect resolution of a severe accident issue identified in the plant-specific DCD. Therefore, this departure has no safety significance.

NRC APPROVAL REQUIREMENT:

This departure requires NRC approval pursuant to 10 CFR Part 52, Appendix D, Section VIII.B.6.

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Departure Number: PTN DEP 2.0-3

AFFECTED DCD/FSAR SECTIONS:

2.0; 2.3.1.5; 5.4.7.1; 6.2.1.1.3; 6.2.2.3; 6.4; 6.4.1.1; 9.1.3.1.3.1; 9.2.2.1; 9.2.7.2.4

SUMMARY OF DEPARTURE:

The site parameter value provided in DCD Tier 1, Table 5.0-1 for the air temperature maximum wet bulb (noncoincident) is 86.1°F. This site parameter value is listed as the maximum safety wet bulb (noncoincident) air temperature in DCD Tier 2, Table 2-1. The corresponding site characteristic value is 87.4°F as reported in FSAR Subsection 2.3.1.5. This site characteristic exceeds the DCD site parameter by 1.3°F.

SCOPE/EXTENT OF DEPARTURE:

The sections and subsections associated with this departure are identified in the FSAR (at the sections and subsections identified above).

DEPARTURE JUSTIFICATION:

The maximum safety wet bulb (noncoincident) air temperature is 87.4°F. This is the 100-year return estimate of 2-hour duration as reported in FSAR Subsection 2.3.1.5. This temperature exceeds the DCD site parameter of 86.1°F by 1.3°F. Analysis of the maximum safety wet bulb (noncoincident) air temperature has been performed. The results of this analysis show that the higher maximum safety wet bulb (noncoincident) air temperature will not adversely affect any safety-related SSCs, their functional capabilities or analysis methods as presented in the DCD.

Specifically, the following evaluations were performed with the following results:

- Containment Pressure Design Limit Evaluation

There is no change in maximum containment pressure value reported in the DCD as a result of increasing the maximum safety noncoincident wet bulb temperature to 87.4°F.

- IRWST Temperature Control with Normal Residual Heat Removal System (RNS)

The IRWST does not steam with RNS cooling initiated two hours after loss of high pressure heat removal and PRHR actuation, with the safety noncoincident wet bulb at or below 87.4°F.

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Departure Number: PTN DEP 2.0-3 (continued)

- Component Cooling Water System (CCS) Maximum Temperature <100°F During Power Operation

At the maximum safety noncoincident wet-bulb temperature, the Service Water System and CCS must maintain a CCS supply temperature of less than 100°F for all cooled loads at full power operating conditions. The CCS temperature remains below 100°F with the safety noncoincident wet bulb temperature at or below 87.4°F.

- Nuclear Island Nonradioactive Ventilation System (VBS) Capability

The evaluation shows that the increase in the safety noncoincident wet bulb temperature will not impact the standard plant design of the chilled water system (VWS) low capacity subsystem. With the increased heat loads resulting from the higher maximum safety wet bulb temperature, the VWS low capacity subsystem maintains the VBS's capability to maintain the main control room, and 1E electrical rooms below 75°F with a single train of VBS and the Chilled Water System in service. No change to VWS low capacity subsystem chiller capacity or the VBS capacity is required with the safety noncoincident wet bulb at or below 87.4°F.

DEPARTURE EVALUATION:

The effect of the site-specific maximum safety wet bulb (noncoincident) air temperature of 87.4°F was evaluated. The results of this evaluation determined that the Unit 6 & 7 site-specific value does not affect any SSC design function or analysis methods as presented in the DCD. The following summarizes the evaluation:

- There is no change in maximum containment pressure value reported in the DCD as a result of increasing the maximum safety noncoincident wet bulb temperature to 87.4°F.
- IRWST does not steam with RNS cooling initiated two hours after loss of high pressure heat removal and Passive Residual Heat Removal (PRHR) actuation, with maximum safety noncoincident wet bulb of 87.4°F.
- The CCS temperature remains below 100°F with a maximum safety noncoincident wet bulb temperature of 87.4°F.
- No change to VWS low capacity subsystem chiller capacity required due to the increase in the maximum safety wet bulb temperature.

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Therefore, this departure does not:

1. Result in more than a minimal increase in the frequency of occurrence of an accident previously evaluated in the plant-specific DCD.
2. Result in more than a minimal increase in the likelihood of occurrence of a malfunction of an SSC important to safety and previously evaluated in the plant-specific DCD.
3. Result in more than a minimal increase in the consequences of an accident previously evaluated in the plant-specific DCD.
4. Result in more than a minimal increase in the consequences of a malfunction of an SSC important to safety previously evaluated in the plant-specific DCD.
5. Create a possibility for an accident of a different type than any evaluated previously in the plant-specific DCD.
6. Create a possibility for a malfunction of an SSC important to safety with a different result than any evaluated previously in the plant-specific DCD.
7. Result in a design basis limit for a fission product barrier as described in the plant-specific DCD being exceeded or altered.
8. Result in a departure from a method of evaluation described in the plant-specific DCD used in establishing the design bases or in the safety analyses.

This departure does not affect resolution of a severe accident issue identified in the plant-specific DCD. Therefore, this departure has no safety significance.

NRC APPROVAL REQUIREMENT:

This departure requires an exemption from the requirements of 10 CFR Part 52, Appendix D, Section IV.A.2.d, which requires information demonstrating compliance with the site parameters and interface requirements. Therefore, an exemption is requested in Part B of this COL Application part.

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Departure Number PTN DEP 3.2-1

AFFECTED DCD/FSAR SECTIONS:

Tier 1 Table 2.2.3-1 and Table 2.2.3-2, Tier 2 Subsections 1.9.4.2.2 and 1.9.5.1.5, Table 3.2-3 (Sheet 16 of 75), Figure 3.8.2-1 (Sheet 3), Subsections 5.4.5.2.1, 5.4.11.2 and 5.4.14.1, Subsections 6.3.1.1.1, 6.3.1.1.4, 6.3.1.1.6, 6.3.1.2, 6.3.1.3, 6.3.2.1, 6.3.2.1.1, 6.3.2.2.5, 6.3.2.2.7, 6.3.2.8, 6.3.3, and 6.3.3.2.1.1, Chapter 6, Figure 6.3-1 (Sheets 1 through 3), Figure 6.3-2 (Not Used), Section 7.4, Subsection 7.4.1.1, Table 14.3-2 (Sheets 7 and 8 of 17), Subsections 15.0.13 and 15.2, Chapter 16 (TS Surveillance Requirement 3.5.4.7, TS Bases B 3.3.3 and B 3.5.4), Subsections 19E.2.3.2.6 and 19E.4.10.2, Table 19E.4.10-1, and Figures 19E.4.10-1 through 19E.4.10-4.

SUMMARY OF DEPARTURE:

Modifications to the Polar Crane Girder (PCG), Internal Stiffener, and Passive Core Cooling System (PXS) gutter were made. The fabrication holes at the top surface of the PCG and in the stiffener are blocked, drainage holes in the bottom of the PCG boxes are blocked, and flow communication holes between PCG boxes are added. A downspout piping network is added to collect and transport condensation from the top and interior of the PCG and the stiffener to the PXS Collection Boxes. Eight new PXS downspout screens are added at the entrance of each of the downspouts at the top of the PCG and the stiffener to prevent any larger debris from blocking the downspout piping. Visual inspection requirements to verify that the return flow to the IRWST will not be restricted by debris have been added to the Technical Specifications and Technical Specification Bases. In addition, clarification of long-term safe-shutdown conditions is provided.

SCOPE/EXTENT OF DEPARTURE:

Upon actuation of the Passive Residual Heat Removal Heat Exchanger (PRHR HX), a series of air-operated valves are actuated to isolate the normal gutter drain path to the Liquid Radwaste System, and divert condensation to the In-containment Refueling Water Storage Tank (IRWST). It is important that sufficient condensate return is achieved during non-loss of coolant accident (LOCA) PRHR HX operation, since reduction of IRWST level to below the top of the tubes will begin to degrade the heat exchanger performance to the point where safe shutdown (<420 deg F in <36 hours) may not be achieved.

As steaming in the containment begins, following initiation of PRHR HX operation and saturation of the IRWST, there are a number of mechanisms, both thermodynamic and geometric, that can prevent the condensed steam from returning to the IRWST. The mechanisms are as follows:

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- a. Steam to pressurize the containment
- b. Steam condensation on Passive Heat Sinks
- c. Raining from the containment roof, Containment ring misalignment
- d. Losses at the Polar Crane Girder and Stiffener
- e. Losses at support plates attached to the containment vessel
- f. Losses at the Equipment Hatch and Personnel Airlock
- g. Losses at entry to IRWST gutter

Losses due to pressurization and condensation on heat sinks are quantified with development of two new calculations. One additional existing calculation was revised based on the results of the new calculations in order to quantify the PRHR HX performance with the revised value of the condensate return and to ensure that the safe shutdown requirements are met. Additionally, analyses were performed which confirm the achievement of the PRHR performance requirements when heat losses are modeled.

A full scale section of the containment wall was constructed to test condensate losses. As a result of the condensate return testing, modifications to the Polar Crane Girder (PCG), Internal Stiffener, and Passive Core Cooling System (PXS) gutter designs are made. The fabrication holes at the top surface of the PCG and in the stiffener are blocked, drainage holes in the bottom of the PCG boxes are blocked, and flow communication holes between PCG boxes are added. A downspout piping network is added to collect and transport condensation from the top and interior of the PCG and the stiffener to the PXS Collection Boxes. Eight new PXS downspout screens are added at the entrance of each of the downspouts at the top of the PCG and the stiffener to prevent any larger debris from blocking the downspout piping. Visual inspection requirements to verify that the return flow to the IRWST will not be restricted by debris have been added to the Technical Specifications and Technical Specification Bases.

In addition to the condensate return changes, clarification of long-term safe shutdown conditions is provided. This clarification identifies the time frames in which the PRHR HX, ADS and passive injection/recirculation can be relied upon to ensure long-term safe shutdown requirements are met.

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DEPARTURE JUSTIFICATION:

The proposed change does not involve a significant reduction in the margin of safety. The proposed change does not reduce the redundancy or diversity of any safety-related SSCs. The proposed changes increase the amount of condensate available in the IRWST after the initiation of a design basis event compared to the design described in the AP1000 DCD Revision 19. Though the fraction of condensate returned is smaller than originally assumed, the proposed changes provide sufficient condensate return flow to maintain adequate IRWST water level for those events using the PRHR HX cooling function. While lower condensate return rates result in an earlier transition to PRHR HX uncover, the long-term shutdown temperature evaluation results show that the PRHR HX would continue to meet its acceptance criteria.

In conclusion, based on the considerations discussed above, (1) there is reasonable assurance that the health and safety of the public will not be endangered by operation in the proposed manner, (2) such activities will be conducted in compliance with the Commission's regulations, and (3) approval of the change will not be inimical to the common defense and security or to the health and safety of the public.

DEPARTURE EVALUATION:

This Tier 2 departure performs modifications to the PCG, Internal Stiffener, and PXS gutter designs. The fabrication holes at the top surface of the PCG and in the stiffener are blocked, drainage holes in the bottom of the PCG boxes are blocked, and flow communication holes between PCG boxes are added. A downspout piping network is added to collect and transport condensation from the top and interior of the PCG and the stiffener to the PXS Collection Boxes. Eight new PXS downspout screens are added at the entrance of each of the downspouts at the top of the PCG and the stiffener to prevent any larger debris from blocking the downspout piping. Visual inspection requirements to verify that the return flow to the IRWST will not be restricted by debris have been added to Technical Specifications and Technical Specification Bases. This departure also provides clarification of long-term safe shutdown conditions. The proposed change does not involve a significant reduction in the margin of safety. The proposed change does not reduce the redundancy or diversity of any safety-related SSCs. The proposed changes increase the amount of condensate available in the IRWST after the initiation of a design basis event compared to the original design. Though the fraction of condensate returned is less than assumed in the original design, the proposed design does not result in significantly degraded overall PXS performance, in that the ability to achieve safe shutdown within the required time frame is accomplished. Therefore, this departure does not:

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1. Result in more than a minimal increase in the frequency of occurrence of an accident previously evaluated in the plant-specific DCD.
2. Result in more than a minimal increase in the likelihood of occurrence of a malfunction of an SSC important to safety and previously evaluated in the plant-specific DCD.
3. Result in more than a minimal increase in the consequences of an accident previously evaluated in the plant-specific DCD.
4. Result in more than a minimal increase in the consequences of a malfunction of an SSC important to safety previously evaluated in the plant-specific DCD.
5. Create a possibility for an accident of a different type than any evaluated previously in the plant-specific DCD.
6. Create a possibility for a malfunction of an SSC important to safety with a different result than any evaluated previously in the plant-specific DCD.
7. Result in a design basis limit for a fission product barrier as described in the plant-specific DCD being exceeded or altered.
8. Result in a departure from a method of evaluation described in the plant-specific DCD used in establishing the design bases or in the safety analyses.

This departure does not affect resolution of a severe accident issue identified in the plant-specific DCD. Therefore, this departure has no safety significance.

NRC APPROVAL REQUIREMENT:

This departure requires an exemption from the requirements of 10 CFR Part 52, Appendix D, Section III.B, which requires compliance with Tier 1 requirements of the AP1000 DCD and the generic Technical Specifications. Therefore, an exemption is requested in Part B of this COL Application Part.

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Departure Number: PTN DEP 6.2-1

AFFECTED DCD/FSAR SECTIONS:

Tier 1 Table 2.3.9-3, Tier 2 Subsections 6.2.4.5.1 and 19.41.7

SUMMARY OF DEPARTURE:

The Containment Hydrogen Control System (VLS) has a function to limit the hydrogen concentration in containment following a severe accident so that it does not result in a failure of the containment shell (DCD Subsection 6.2.4). A severe accident (considered to be a beyond design basis event) involves a major core degradation or core melt that results in hydrogen production among other effects. A severe accident involving major core degradation/core melt is not a design basis accident; however, the VLS contains design features to address this scenario. The VLS promotes hydrogen burning soon after reaching the lower flammability limit. Burning off hydrogen at lower flammability limits is intended to prevent the hydrogen from reaching high concentration levels and potential adverse effects on containment integrity. There are hydrogen igniters positioned around various areas of containment to be able to burn off hydrogen in a controlled manner to help preserve containment integrity.

Openings in the ceilings of the Passive Core Cooling System (PXS) valve/accumulator rooms A and B (identified as Rooms 11206 and 11207, respectively) communicate with the room above where the CMTs are located (Room 11300). These openings allow access for hydrogen to vent. Igniters are placed in these areas to allow the hydrogen to ignite and burn. Evolution of the AP1000 configuration moved some equipment and room layouts such that the existing VLS ITAAC and Subsections 6.2.4.5.1 and 19.41.7 wording is no longer consistent with the revised plant design. The CMT-A opening in Room 11206 was moved closer to the containment shell while the equipment hatch opening in the same room was moved farther away, and a weir was added for flood protection (not related to hydrogen venting). The CMT-B opening in Room 11207 was moved farther away from the containment shell.

The changes proposed to the DCD by this departure reflect the current vent path configuration in Rooms 11206 and 11207, and provide clarification of “primary openings” in Rooms 11206 and 11207.

SCOPE/EXTENT OF DEPARTURE:

The changes to the DCD addressed by Departure 6.2-1 revise Tier 1 ITAAC Table 2.3.9-3, Item 3, Acceptance Criteria iii and Tier 2 Subsections 6.2.4.5.1 and 19.41.7 to reflect the actual vent path configuration, clarify the meaning of primary openings for Rooms 11206 and 11207, identify the vent path locations will be verified by pre-operational inspection, and hydrogen released from these vent paths will not challenge the integrity of the containment shell.

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DEPARTURE JUSTIFICATION:

The proposed changes correct information in the DCD regarding the plant layout of the primary openings in Containment Rooms 11206 and 11207 that will be used to vent hydrogen; specifically, changes involve the distance between the openings and the containment shell and clarifies what is designated as a primary opening for these rooms. An analysis demonstrates ignition of hydrogen venting through these openings will not result in failure of the containment shell.

The proposed changes will not increase the frequency of occurrence of an accident, nor result in a malfunction of a structure, system or component (SSC). The proposed changes regarding the primary openings layout information to be applied to pre-operational measurements and clarification of the primary openings will not result in an accident or malfunction of an SSC. The revised hydrogen vent locations will not result in containment shell failure and as such, will not impact a design basis limit for a fission product barrier. The updated DCD language for primary openings used for venting hydrogen is supported by analysis and does not affect resolution of an ex-vessel severe accident design feature.

DEPARTURE EVALUATION:

The proposed changes correct information in the DCD regarding the plant layout of the primary openings in Containment Rooms 11206 and 11207 that will be used to vent hydrogen during a beyond design basis event (severe accident). Pre-operational measurements will verify the location of these openings, and an analysis demonstrates postulated hydrogen releases through these openings do not result in a failure of the containment shell.

Therefore, this departure does not:

1. Result in more than a minimal increase in the frequency of occurrence of an accident previously evaluated in the plant-specific DCD.
2. Result in more than a minimal increase in the likelihood of occurrence of a malfunction of an SSC important to safety previously evaluated in the plant-specific DCD.
3. Result in more than a minimal increase in the consequences of an accident previously evaluated in the plant-specific DCD.
4. Result in more than a minimal increase in the consequences of a malfunction of an SSC important to safety previously evaluated in the plant-specific DCD.
5. Create a possibility for an accident of a different type than any evaluated previously in the plant-specific DCD.

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6. Create a possibility for a malfunction of an SSC important to safety with a different result than any evaluated previously in the plant-specific DCD.
7. Result in a design basis limit for a fission product barrier as described in the plant-specific DCD being exceeded or altered.
8. Result in a departure from a method of evaluation described in the plant-specific DCD used in establishing the design bases or in the safety analyses.
9. Affect resolution of an ex-vessel severe accident design feature identified in the plant-specific DCD.

Therefore, this departure has no safety significance.

NRC APPROVAL REQUIREMENT:

This departure requires an exemption from the requirements of 10 CFR Part 52, Appendix D, Section III.B, which requires compliance with Tier 1 requirements of the AP1000 DCD. Therefore, an exemption is requested in Part B of this COL Application Part.

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Departure Number PTN DEP 6.4-1

AFFECTED DCD/FSAR SECTIONS:

Tier 1 Subsection 2.2.5, Tier 1 Table 2.2.5-1, Tier 1 Table 2.2.5-5, Tier 1 Subsection 2.7.1, Tier 2 Table 1.6-1, Subsection 1.9.4.2.3, Appendix 1A, Subsection 3.1.2, Subsection 6.4, Subsection 6.4.2.6, Subsection 6.4.3.2, Subsection 6.4.4, Table 6.4-2, Subsection 7.3.1.2.17, Subsection 9.2.6.1.1, Subsection 9.4.1.1.1, Subsection 9.4.1.1.2, Subsection 9.4.1.2.1.1, Subsection 9.4.1.2.3.1, Figure 9.4.1-1 (Sheet 5 of 7), Table 11.1-4, Table 11.1-5, Table 11.1-6, Subsection 11.5.1.1, Subsection 11.5.2.3.1, Subsection 12.2.1.3.1, Subsection 12.2.1.3.2, Table 12.2-28, Table 12.2-29, Subsection 12.3.2.2.7, Figure 12.3-1 (Sheet 6 of 16), Table 14.3-7 (Sheet 2 of 3), Subsection 15.0.11.1, Subsection 15.0.11.6, Table 15.0-2, Subsection 15.1.5.4.1, Subsection 15.1.5.4.6, Table 15.1.5-1, Subsection 15.3.3.3.1, Table 15.3-3 (Sheet 1 of 2), Subsection 15.4.8.1.1.3, Subsection 15.4.8.1.2, Subsection 15.4.8.2, Subsection 15.4.8.2.1, Subsection 15.4.8.2.1.1, Subsection 15.4.8.2.1.2, Subsection 15.4.8.2.1.3, Subsection 15.4.8.2.1.4, Subsection 15.4.8.2.1.5, Subsection 15.4.8.2.1.7, Subsection 15.4.8.2.1.8, Subsection 15.4.8.2.1.9, Subsection 15.4.8.3, Subsection 15.4.8.3.1, Subsection 15.4.8.3.5, Subsection 15.4.8.3.6, Subsection 15.4.10, Table 15.4-1 (Sheets 2 and 3 of 3), Table 15.4-3 (Not Used), Table 15.4-4 (Sheets 1 and 2 of 2), Figure 15.4.8-1, Figure 15.4.8-2, Figure 15.4.8-3, Figure 15.4.8-4 (Not Used), Subsection 15.6.2.6, Subsection 15.6.3.3.1, Subsection 15.6.3.3.6, Subsection 15.6.5.3.2, Subsection 15.6.5.3.5, Subsection 15.6.5.3.8.1, Subsection 15.6.5.3.8.2, Subsection 15.6.6, Table 15.6.2-1, Table 15.6.3-3, Table 15.6.5-2 (Sheets 1-3 of 3), Table 15.6.5-3, Subsection 15.7.4.5, Table 15.7-1, Subsection 15A.3.1.2, Subsection 15B.1, Chapter 16 LCO 3.7.4, SR 3.7.4.1, Bases 3.4.10, Bases 3.7.4, Bases 3.7.6.

SUMMARY OF DEPARTURE:

If high levels of particulate or iodine radioactivity are detected in the main control room supply air duct that could lead to exceeding General Design Criterion (GDC) 19 operator dose limits (5 rem), the protection and safety monitoring system (PMS) automatically actuates the VES to ensure compliance. The VES design includes a passive filtration feature consisting of a HEPA filter in series with a charcoal adsorber and a postfilter which work to remove particulate and iodine from the air to reduce potential control room dose during VES operation.

During AP1000 design finalization, a number of issues were identified challenging the ability of the certified design to limit operator dose to less than 5 rem. In order to address these issues, site-specific revisions to the AP1000 design and associated dose consequence analyses presented in DCD Revision 19 are made to ensure that operator dose following a DBA is maintained below the 5 rem GDC limit for the duration of the event. Some design changes apply

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to all MCR design basis accidents and ventilation system alignments evaluated in DCD Section 6.4, while others are design basis accident specific.

A. Changes Impacting All MCR Design Basis Events

AP1000 generic changes impacting all MCR operator dose evaluations presented in DCD Section 6.4 and Chapter 15 required to address MCR dose analysis errors include:

1. Radiation contributions from HVAC filters were not considered in MCR dose calculation results reported in DCD Revision 19 Section 6.4. Regulatory Guide 1.183 indicates that these contributions should be considered in plant design. The radiological dose analyses are therefore revised to include direct radiation contributions from radioactive material postulated to accumulate on filters in the VES and VBS HVAC systems during design basis events.
2. In order to reduce the MCR operator direct radiation dose contribution from radioactive material postulated to accumulate on VES filter media during design basis events, shielding is added around the filters and is accounted for in the revised radiation analysis model. Consequence analyses considering filter contributions assume that control room occupants are located below these filters, using the defined occupancy factors (DCD Revision 19, Table 15.6.5-2, Sheet 2 of 3).
3. In order to partially offset increases in calculated MCR operator dose due to consideration of direct radiation from VES filter media and other corrections identified in this response, the VES filter efficiency for organic iodine is increased from 30% to 90% (DCD Revision 19 Table 15.6.5-2, Sheet 2 of 3). DCD Revision 19 post accident dose analyses applied an organic iodine filter efficiency of 30% to VES filtration units based on Regulatory Guide 1.52 Revision 2 and a conservative assumption that relative humidity within the MCR could exceed 95% following an accident. As part of AP1000 detailed design, environmental conditions have been evaluated to show that the humidity within the MCR is not expected to exceed 95%. Further, humidity is not expected to exceed 60% within the first 72 hours of an event, the time frame during which the filter would be operating, or exceed 95% at any time post accident. Thus, the higher filter efficiency can be credited in the MCR dose analyses consistent with Regulatory Guide 1.52 Revision 2. Additionally, it is noted that the analyses model an “overall” efficiency for each chemical form being filtered (elemental, organic, particulate). This overall efficiency accounts for filter media sizing (e.g. charcoal bed depth) and the potential for bypass around the filter.

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4. During AP1000 detailed design and re-evaluation of MCR doses to include consideration of HVAC filter contributions (Item A.1.), it was determined that the VBS radiation monitor setpoints applied in MCR dose calculations supporting DCD Revision 19 were not selected in a manner that a) ensures compliance with the GDC-19 for all postulated accident conditions including Design Basis Accidents (DBAs) evaluated in DCD Revision 19 Chapter 15, or b) fully supports the AP1000 design objective to use VBS supplemental filtration mode (SFM) when available rather than VES actuation to provide the MCR radiological protection function.

For postulated accident conditions involving a reduced source term or release rate other than evaluated for DBAs as part of the certified design, there may not be sufficient radioactivity within the MCR Envelope to prompt actuation of VES, and yet, enough radioactivity could exist that would lead to operator doses in excess of 5 rem without manual actuation. The radiation monitor setpoint values are therefore updated to ensure VBS or VES filtration mode actuation occurs for any radiological release event that could result in MCR operator doses in excess of GDC-19.

One of the fundamental objectives of VBS as described in DCD Revision 19 Section 9.4.1 is to "...minimize the potential for actuation of the main control room emergency habitability system...". This change uses a non-safety High-1 signal to actuate VBS SFM and the existing safety-related signal (High-2) to actuate VES in a manner that ensures High-2 would only be reached if VBS SFM was not functioning properly or is insufficient. This change also addresses release scenarios where high concentrations of particulates or iodine may exist with low levels of noble gas. If such a release occurred without this VBS setpoint logic change, direct VES actuation could be induced without the opportunity for VBS SFM to be actuated.

B. Large Break Loss of Coolant Accident (LOCA) Dose Consequence Changes

AP1000 generic changes impacting the LOCA MCR operator dose evaluations presented in DCD Sections 6.4 and 15.6.5 required to address MCR dose analysis errors include:

1. Dose contributions from adjacent structure direct and skyshine radiation included MCR operator dose results for LOCA as reported in DCD Revision 19 are based upon AP600 post-accident dose calculations and assume the presence of shielding that was not included in the AP1000 design. Post-accident radiological dose calculations are therefore changed to use updated AP1000 detailed design inputs and analyses for skyshine and direct radiation. The added dose incurred by this change is partially offset by other proposed changes.

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2. In order to partially offset increases in calculated MCR operator dose due to consideration of direct radiation from VES filter media and other corrections identified in this response, changes are made to the containment elemental iodine removal coefficient and re-suspension models supporting the DCD Revision 19 LOCA dose analysis.

Changes are made to the IRWST iodine re-evolution model. The changes involve a) the water/vapor partition factor modeled for elemental iodine and b) the timing associated with the conversion of elemental iodine to organic iodine and its availability for release. These refinements and modeling changes define the production of organic iodine based on re-evolved elemental iodine.

The iodine source term applied in the LOCA dose analysis supporting DCD Revision 19 is based upon the NUREG-1465 source term described in Regulatory Guide 1.183. The analysis models a staged release of core activity (i.e., gap release and early in-vessel) to the containment atmosphere over the first ~2 hours following the start of the event. The chemical form of iodine released is assumed to be 95% particulate, 4.85% elemental, and 0.15% organic, consistent with Regulatory Guide 1.183. Particulate removal via passive processes (i.e., diffusiophoresis, thermophoresis, and sedimentation) and elemental iodine removal via deposition are modeled. Organic iodine removal via processes other than decay or leakage from containment is not modeled.

Particulates removed to the containment shell are assumed to be washed off the shell by the flow of water resulting from condensing steam (i.e., condensate flow). The particulates may be either washed into the sump, which is controlled to a $\text{pH} \geq 7$ post-accident or into the IRWST, which is not pH controlled post-accident. Due to the assumed conditions in the IRWST, the particulate iodine washed into the IRWST may chemically convert to an elemental form and re-evolve, subject to partitioning, as airborne. A portion (3%) of that airborne elemental iodine is then assumed to convert to an organic form. This is consistent with elemental organic split assumed for the initial release from the core ($4.85/0.15 = 97/3$) and is consistent with the Regulatory Guide 1.183 guidance for other events.

The calculational approach to account for the iodine that is assumed to re-evolve from the IRWST post-LOCA is overly conservative in the certified design analysis. The certified design analysis applies a water-vapor partition factor of 5 for elemental iodine and neglects the time dependent formation of organic iodine from elemental iodine; the organic iodine that would be formed over time is assumed to be present at time zero.

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NUREG-1465 states that “It is unduly conservative to assume that organic iodine is not removed at all from containment atmosphere, once generated, since such an assumption can result in an overestimate of the long-term doses to the thyroid.” The revised analysis approach applies a conservative water/vapor elemental iodine partition factor of 10, selected to conservatively bound the time-dependent partition factors calculated using the NUREG/CR-5950 models and IRWST temperature and pH as a function of time. Additionally, the conversion of elemental iodine to organic iodine is modeled on a time-dependent basis in which 3% of the evolved elemental iodine is assumed to convert to an organic form upon its release to containment. It is noted that this does not impact the percentage of iodine assumed to convert to the organic form.

The passive containment elemental iodine deposition removal coefficient is also increased from the 1.7 hr^{-1} value applied in DCD Revision 19 LOCA dose calculations to 1.9 hr^{-1} . The larger elemental iodine removal rate constant is calculated based on a larger containment deposition surface area documented during the AP1000 detailed design. The DCD Revision 19 elemental iodine removal rate constant was based on an assumed 219,000 ft^2 deposition surface area. Updated detailed design calculations have documented a 251,000 ft^2 deposition surface area.

C. Main Steam Line Break (MSLB) Dose Consequence Changes

AP1000 generic changes impacting the MSLB MCR operator dose evaluations presented in DCD Sections 6.4 and 15.1.5 required to address MCR dose analysis errors include:

1. The AP1000 steam line break accident analysis described in DCD Revision 19 assumes a 10 minute faulted steam generator (SG) blowdown based on a Hot Zero Power (HZP) SG mass released at an average rate. This HZP case is conservative for offsite dose. It was determined, however, that a full power SG mass could lead to SG dry-out occurring at ~200 seconds. Earlier dry-out is more limiting for the purposes of operator post-accident dose calculations. To ensure a conservative dose for both offsite and MCR, the HZP initial mass was retained, a bounding release rate was modeled until 300 seconds, and any remaining activity was released thereafter.
2. In order to offset increases in calculated MCR operator dose for MSLB due to consideration of a bounding release rate and other corrections identified in this response, the Technical Specification limit for secondary iodine activity is reduced from 0.1 to 0.01 microcurie/gram dose equivalent (DE) I-131 (Limiting Condition for Operation (LCO) 3.7.4).

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The current Technical Specification (TS) limit for secondary iodine activity is 0.1 $\mu\text{Ci/g}$ dose equivalent (DE) I-131 (LCO 3.7.4). This is a standard value, however the TS Bases refer to the steam line break analysis; in other words, the steam line break analysis defines the level of secondary activity that is acceptable. The maximum secondary activity is also limited by other TS limits. Specifically, the primary coolant specific activity concentration limit of 1 $\mu\text{Ci/g}$ DE I-131 (based on the design basis fuel defect of 0.25%) and the TS primary to secondary leakage limit of 300 gallons per day.

Using these values, the secondary side coolant activity is calculated to be $8.3\text{E-}4$ $\mu\text{Ci/g}$ DE I-131, which is orders of magnitude below the current TS limit. The TS limit for secondary iodine activity is therefore revised from 0.1 $\mu\text{Ci/g}$ DE I-131 to 0.01 $\mu\text{Ci/g}$ DE I-131. The change does not impact the operational margin, as the secondary side specific activity is limited to values lower than the new proposed TS limit by the TS primary to secondary leakage limit and the design basis fuel defect. The revised value of 0.01 $\mu\text{Ci/g}$ DE I-131 is within the detection capability of existing instrumentation and is significantly above the typical secondary coolant activities observed at operating plants. No additional sampling or modifications to the frequency of LCO 3.7.4 are needed.

D. Rod Ejection Accident (REA) Dose Consequence Changes

AP1000 generic changes impacting the REA MCR operator dose evaluations presented in DCD Sections 6.4 and 15.4.8 required to address MCR dose analysis errors include:

1. The method for performing the REA dose analysis has changed from that applied in DCD Revision 19. As stated in NUREG-1793, the NRC accepted the use of NUREG-0800 Section 4.2 Revision 2 for design certification of the AP1000 plant. However, in NUREG-1793 Supplement 2 it is stated that:

“For COL applicants or licensees who reference the AP1000 or AP600 certified designs, the staff will review any change or departure from the certified design that requires prior NRC approval as specified in Section VIII of Appendices C and D to 10 CFR Part 52, respectively.

The staff will evaluate the reactivity-initiated accidents such as rod ejection accidents based on the acceptance criteria in effect 6 months before docketing the amendment request, such as the interim acceptance criteria specified in Appendix B to NUREG-0800 Section 4.2, Revision 3, if a change or departure in fuel design or other aspects is proposed that requires a reevaluation of final safety evaluation report Chapter 4, “Reactor,” or Chapter 15, “Transient and Accident Analysis.”

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Due to the need to incorporate other design changes in the REA MCR operator dose calculations, NUREG-0800 Section 4.2 Revision 3 is used for recalculation of the rod ejection dose analysis, which results in a significant impact to the rod ejection dose analysis. NUREG-0800 Section 4.2 Revision 3 precludes fuel melt, providing a dose benefit, but also connects the source term to the fuel enthalpy increase, which is a significant dose penalty. The dominant contributor to the increased dose is the increase by a factor of more than 5 in alkali metal releases.

2. The full-power moisture carryover from the steam generators used in the AP1000 REA dose analysis was increased from 0.1% to 0.35%. This input is used to calculate alkali metal releases from the SGs in the AP1000 REA dose analysis. This input was updated to be consistent with the updated AP1000 plant design.
3. The REA dose analysis results are updated to account for a reduction in the Technical Specification limit for secondary iodine activity from 0.1 to 0.01 microcurie/gram dose equivalent (DE) I-131 as described for the updated MSLB analysis in Item C.2., above.
4. The radial peaking factor has been adjusted to a value of 1.75. This provides a more conservative input than the DCD Revision 19 value and provides additional future core design margin.
5. The passive containment elemental iodine deposition removal coefficient is also increased from the 1.7 hr^{-1} value applied in DCD Revision 19 LOCA dose calculations to 1.9 hr^{-1} . The larger elemental iodine removal rate constant is calculated based on a larger containment deposition surface area documented during the AP1000 detailed design. The DCD Revision 19 elemental iodine removal rate constant was based on an assumed 219,000 ft² deposition surface area. Update detailed design calculations have documented a 251,000 ft² deposition surface area.

E. Steam Generator Tube Rupture (SGTR) Dose Consequence Changes

AP1000 generic changes impacting the SGTR MCR operator dose evaluations presented in DCD Sections 6.4 and 15.6.3 required to address MCR dose analysis errors include:

1. The full-power moisture carryover from the intact steam generator used in the AP1000 SGTR dose analysis was increased from 0.1% to 0.35%. This input is used to calculate alkali metal releases from non-faulted SG in the AP1000 SGTR dose analysis. This input was updated to be consistent with the updated AP1000 plant design.

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2. The full-power moisture carryover from the ruptured loop steam generator used in the AP1000 SGTR dose analysis was increased from 0.1% to 0.35%. This input is used to calculate alkali metal releases from the faulted SG in the AP1000 SGTR dose analysis. This input was updated to be consistent with the updated AP1000 plant design.
3. The SGTR results are updated to account for a reduction in the Technical Specification limit for secondary iodine activity from 0.1 to 0.01 microcurie/gram dose equivalent (DE) I-131 as described for the updated MSLB analysis in Item C.2., above.

F. Locked Rotor Accident Dose Consequence Changes

AP1000 generic changes impacting the locked rotor MCR operator dose evaluations presented in DCD Sections 6.4 and 15.3.3 required to address MCR dose analysis errors include:

1. The full-power moisture carryover from the steam generators used in the AP1000 locked rotor dose analysis was increased from 0.1% to 0.35%. This input was updated to be consistent with the updated AP1000 plant design.
2. The locked rotor results are updated to account for a reduction in the Technical Specification limit for secondary iodine activity from 0.1 to 0.01 microcurie/gram dose equivalent (DE) I-131 as described for the updated MSLB analysis in Item C.2., above.
3. The radial peaking factor has been adjusted to a value of 1.75. This provides a more conservative input than the DCD Revision 19 value and provides additional future core design margin.

G. Small Line Break Outside Containment Dose Consequence Changes

AP1000 generic changes impacting the small line break outside containment MCR operator dose evaluations presented in DCD Sections 6.4 and 15.6.2 required to address MCR dose analysis errors include:

1. The fraction of reactor coolant flashed was increased from the value used in DCD Revision 19 supporting calculations of 0.41 to 0.47 based on the updated detailed design. The certified design analysis used vessel average temperature (T_{avg}) as the basis for the flashing fraction. It was determined that the sample lines draw from the hot leg, thus, a hot leg temperature (which is greater than T_{avg}) was used.

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H. Fuel Handling Accident (FHA) Dose Consequence Changes

AP1000 generic changes impacting the FHA MCR operator dose evaluations presented in DCD Sections 6.4 and 15.7.4 required to address MCR dose analysis errors include:

1. The radial peaking factor has been adjusted to a value of 1.75. This provides a more conservative input than the DCD Revision 19 value and provides additional future core design margin.
2. No unique accident specific changes.

In addition to the required changes summarized above, other generic changes associated with AP1000 detailed design are incorporated in revised MCR dose calculations. These include:

- a) The MCR pressure boundary consists of the main control area, operator work area, mezzanine, operator break room, shift manager's office, kitchen area, and restrooms. The vestibule to enter the MCR and stairwell to the remote shutdown room is outside of the MCR pressure boundary. The MCR and MCR HVAC volumes are recalculated based on updated detailed design data, and are used as input to revised post-accident operator dose analyses.
- b) The VBS normal operation to VBS SFM switchover time and the response time to actuate VES used in DCD Revision 19 supporting analyses have been determined to be non-bounding. The certified design analyses used assumed/expected values that were ultimately not supportable by the updated detailed design. System-level requirements are developed for switch over and response times; these system-level requirements account for sample transport time, radiation detector response time, I&C response times, and VBS/VES equipment actuations (e.g., valves, dampers, etc.). The dose analyses for cases considering VBS SFM are revised to include a longer delay time between the point when airborne radioactivity in the control room reaches the High-1 setpoint concentration and when the VBS SFM is operational. The dose analyses for cases considering VES are revised to include a longer response time between the point when the High-2 setpoint is reached and when the VES is operational.

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- c) DCD Revision 19 post accident dose calculations model a normal VBS inflow rate of 1925 cfm until MCR isolation. This is the path for the released activity to enter the MCR. This value is based on an assumed preliminary design value of 1750 cfm and adding a 10% penalty to account for instrumentation uncertainty. A VBS outside air intake flow rate calculated as part of detailed design indicates a nominal outside air flow rate of 1320 cfm. The normal VBS outside air flow rate assumption used in the accident operator dose calculations is therefore decreased accordingly. It is noted that during plant start-up, the HVAC system is balanced and dampers that have specific criteria under certain modes of operation are adjusted to have a preset position which can then be controlled from the MCR. To address a potential inaccuracy of the damper positioning, a nominal value of 1500 cfm is established for the normal VBS outside air flow rate. For dose analyses, the assumed normal VBS outside air flow rate will therefore be 1650 cfm, which corresponds to 1500 cfm +10%.
- d) The VBS ancillary fan MCR air intake flow rate is also increased to 1900 cfm. The previous assumption of 1700 cfm had been specified as a minimum as part of the detailed design. For conservatism, the 1700 cfm was increased by 10% and rounded up to 1900 cfm.

Although these changes are considered as part of the updated MCR dose calculations, they are being implemented as general detailed design updates and are not specifically implemented to offset impacts of errors otherwise being addressed as part of this RAI response.

DEPARTURE JUSTIFICATION:

The proposed changes do not involve a significant reduction in the margin of safety. The proposed changes do not reduce the redundancy or diversity of any safety-related SSCs. The proposed changes improve the mitigating capabilities of the MCR Habitability System and address the MCR dose analysis errors. The MCR dose to the operators slightly decreases for the limiting DBA (LBLOCA) and the analysis shows that the results do not exceed the GDC-19 requirements of 5 rem.

In conclusion, based on the considerations discussed above, (1) there is reasonable assurance that the health and safety of the public will not be endangered by operation in the proposed manner, (2) such activities will be conducted in compliance with the Commission's regulations, and (3) approval of the change will not be inimical to the health and safety of the public or to the common defense and security.

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DEPARTURE EVALUATION:

This Tier 2 departure makes the changes stated above. The departure does not involve a significant reduction in the margin of safety and does not reduce the redundancy or diversity of any safety-related SSCs. Analysis results show that the MCR dose does not exceed GDC requirements of 5 rem. Therefore:

1. This proposed departure does not impact the frequency of occurrence of an accident previously evaluated in the plant-specific DCD. Therefore there is not more than a minimal increase in the frequency of occurrence.
2. This proposed departure does not impact the likelihood of a malfunction of an SSC. Shielding is a passive function that does not impact HVAC function and is designed to remain in place under seismic conditions. The switchover times from normal HVAC in the control room (VBS) to either the VBS supplemental filtration mode or to the emergency habitability system (VES) are analyzed to determine conservative setpoints to establish bounding system-level requirements for each system participating in the switchover.
3. New analyses determined that the radiation dose to the operator during the limiting DBA (LBLOCA) decreased from 4.41 rem to 4.33 rem and continues to meet the GDC limit of 5 rem. However, the radiation dose to the operator during the rod ejection accident increased from 1.8 to 3.6 rem. Therefore, this departure does result in more than a minimal increase in the consequences of an accident previously evaluated in the plant-specific DCD.
4. Potential malfunctions of the HVAC system operation and switchover modes were analyzed and evaluated, and there were no design changes affecting or increasing source terms. Therefore, this departure will not result in more than a minimal increase in the consequences of a malfunction of an SSC important to safety previously evaluated in the plant-specific DCD.
5. This departure does not impact the possibility of accidents, and therefore does not create a possibility for an accident of a different type than previously evaluated in the plant-specific DCD.
6. The operability of the HVAC system with the different modes of operation (VBS w/SFM vs. VES) along with the interface of the RMS was analyzed and evaluated for adverse effects. It was determined that this departure would not create a possibility for a malfunction of an SSC important to safety with a different result than any evaluated previously in the plant-specific DCD.

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7. This departure does not result in a design basis limit for a fission product barrier as described in the plant-specific DCD being exceeded or altered.
8. This departure proposes a refinement of the iodine evolution/re-evolution model, and a new computer code is used for recalculation of the rod ejection dose analysis. The use of the new iodine model and new rod ejection computer code is therefore considered to be a departure from a method of evaluation described in the plant-specific DCD used in establishing the design bases or in the safety analyses.

This departure does not affect resolution of a severe accident issue identified in the plant-specific DCD. Therefore, this departure has no safety significance.

NRC APPROVAL REQUIREMENT:

This departure requires an exemption from the requirements of 10 CFR Part 52, Appendix D, Section III.B, which requires compliance with Tier 1 requirements of the AP1000 DCD and the generic Technical Specifications. Therefore, an exemption is requested in Part B of this COL Application Part. This departure also requires NRC approval pursuant to 10 CFR Part 52, Appendix D, Section VIII.B.5.

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Departure Number PTN DEP 6.4-2:

AFFECTED DCD/FSAR SECTIONS:

Tier 1 Tables 2.2.5-1, 2.2.5-4, 2.5.2-3, 2.5.2-4, Tier 2 Table 3.7.3-1 (Sheets 1 and 2 of 3), Table 3.9-12 (Sheet 6 of 7), Table 3.9-16 (Sheet 23 of 26), Table 3.9-17, Table 3.11-1 (Sheets 17, 30 and 47 of 51), Figure 3D.5-1 (Sheet 1 of 3), Table 3I.6-2 (Sheet 11 of 28), Table 3I.6-3 (Sheets 10 and 28 of 32), Subsections 6.4.2.2, 6.4.2.3, 6.4.3.2, 6.4.4, 6.4.5.1, 6.4.5.3 and 6.4.8, Table 6.4-3, Figure 7.2-1 (Sheet 13 of 21), Subsection 7.3.1.2.17, Table 7.3-1 (Sheet 7 of 9), Table 7.3-3 (Sheet 2 of 2), Table 7.5-1 (Sheet 11 of 12), Table 7.5-7 (Sheet 4 of 4), Subsections 9.3.1.1.2, 9.4.1.1.2, 9.4.1.2.3.1 and 14.2.9.1.6, Table 14.3-7 (Sheet 1 of 3), TS 3.3.2, TS 3.7.6, TS B 3.3.2, TS B 3.7.6, TS Figure B 3.7.6-2.

SUMMARY OF DEPARTURE:

The AP1000 Design Control Document (DCD), Revision 19 describes a Main Control Room (MCR) Emergency Habitability System (VES) design objective of maintaining a habitable environment in the main control room envelope (MCRE) for 72 hours after VES actuation. The MCRE temperature modeling was based on a scenario with normal ac power not available and therefore, no heat contribution from normal ac powered loads. However, a more limiting event has been identified where the VES actuates, resulting in the isolation of the MCRE, without a loss of normal ac power. With normal ac power available, all equipment in the MCRE continues to generate heat, potentially raising the temperature above the human engineering design and equipment qualification guidelines for temperature that are referenced in the DCD. Also, the original MCRE temperature modeling was based on the AP600 configuration. AP1000 design evolution and finalization, which included the addition of sixteen new wall panel displays, has increased the heat load in the MCRE.

In order to address these issues, a departure from information presented in the generic DCD is necessary. This departure makes several changes to ensure that the VES can perform its design functions. These changes consist of adding load shedding devices, raising equipment qualification (EQ) temperature requirements, revising Technical Specifications (TS) and reclassifying VES components. These changes will make the VES system more robust and will ensure that habitability and EQ requirements are met in the most limiting event scenario.

SCOPE/EXTENT OF DEPARTURE:

There are 4 basic changes proposed by this departure:

1. Non-essential equipment in the MCRE will be automatically de-energized by new load shedding devices.

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2. TS will be modified to ensure that MCRE exterior temperatures do not exceed values assumed in supporting calculations, to ensure the quality of the air in the VES storage tanks and to ensure availability of the new VES load shedding function.
3. The EQ temperature requirement for safety related equipment in the MCRE will be increased.
4. Two valves in the VES system will be re-classified to "active" valves to facilitate offsite support following the depletion of compressed air in the VES.

Change 1 - Load Shedding:

To compensate for the increased heat loads, new load shedding equipment will be added to automatically shed non-essential, non-safety related loads, beginning upon actuation of VES. The new load shedding equipment is safety related and designed with the requisite redundancy, separation, isolation, and equipment qualification requirements. With these non-essential, non-safety related loads shed as described, the temperature modeling concludes that the 72 hour VES design objective for habitability will be met. However, even with the load shedding, the heat generation rate for the AP1000 design is greater than originally assumed, so values included in AP1000 DCD Tier 1 and Tier 2 tables will be revised.

Change 2 - TS Changes:

Ongoing construction of the AP1000 has revealed that insulating materials on some of the exterior walls of the MCRE cannot be installed as indicated in the DCD. To compensate for the loss of insulating materials, assumptions were made in the revised MCRE heat up calculations concerning maximum initial room temperatures outside the MCRE prior to a VES actuation.

These assumptions were determined to require new TS actions and surveillances addressing room temperature, the new electrical load shed function and air quality in the VES storage tanks.

Change 3 - Equipment Qualification Temperature Requirement:

Utilizing the load shedding scheme described in Change 1, the MCRE will remain below the MCRE's maximum habitability temperature limit for the 72 hour design basis of VES. After 72 hours, the Nuclear Island Non-Radioactive Ventilation System (VBS) can be aligned to circulate air into the MCRE from outside the plant. Based on maximum anticipated outdoor temperature, the calculated temperature in the MCRE could reach a maximum of 110°F. Therefore, a new temperature requirement of 110°F is established for EQ of safety related equipment located in the MCRE. This will ensure that equipment will operate as required.

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Change 4 - Two Valves Reclassified:

The capability of offsite support is expanded by reclassifying two VES manual valves. These valves are to be changed from “non-active” valves to “active” valves in order to maintain open and close capabilities following design basis accidents. With this re-classification, these manually operated valves provide a connection for offsite support during the post 72 hour operation of VES. Changing the classification impacts a Tier 1 table in the DCD.

DEPARTURE JUSTIFICATION:

The proposed changes do not involve a significant reduction in the margin of safety. The proposed changes do not reduce the redundancy or diversity of any safety-related structures, systems or components (SSCs). The proposed changes ensure that the VES system can perform its design functions including maintaining an environment suitable for MCRE habitability and EQ.

Based on these considerations: (1) there is reasonable assurance that the health and safety of the public will not be endangered by operation in the proposed manner, (2) such activities will be conducted in compliance with the Commission's regulations, and (3) approval of the change will not be inimical to the common defense and security or to the health and safety of the public.

DEPARTURE EVALUATION:

This departure adds safety related equipment to shed non-essential, non-safety related loads, increases the EQ temperature requirements for safety related equipment in the MCRE, and provides for a connection for offsite support following depleting of VES compressed air. This departure also adds TS actions and surveillances to ensure temperature limits are not exceeded and that equipment operates as designed. These changes will ensure that the MCRE habitability and EQ requirement are met in the most limiting event scenario. The departure does not involve a significant reduction in the margin of safety and does not reduce the redundancy or diversity of any safety-related SSCs. Therefore, this departure does not:

1. Result in more than a minimal increase in the frequency of occurrence of an accident previously evaluated in the plant-specific DCD.
2. Result in more than a minimal increase in the likelihood of occurrence of a malfunction of an SSC important to safety and previously evaluated in the plant-specific DCD.
3. Result in more than a minimal increase in the consequences of an accident previously evaluated in the plant-specific DCD.

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4. Result in more than a minimal increase in the consequences of a malfunction of an SSC important to safety previously evaluated in the plant-specific DCD.
5. Create a possibility for an accident of a different type than any evaluated previously in the plant-specific DCD.
6. Create a possibility for a malfunction of an SSC important to safety with a different result than any evaluated previously in the plant-specific DCD.
7. Result in a design basis limit for a fission product barrier as described in the plant-specific DCD being exceeded or altered.
8. Result in a departure from a method of evaluation described in the plant-specific DCD used in establishing the design bases or in the safety analyses.

This departure does not affect resolution of a severe accident issue identified in the plant-specific DCD. Therefore, this departure has no safety significance.

NRC APPROVAL REQUIREMENT:

This departure requires an exemption from the requirements of 10 CFR Part 52, Appendix D, Section III.B, which requires compliance with Tier 1 requirements of the AP1000 DCD and the generic Technical Specifications. Therefore, an exemption is requested in Part B of this COL Application Part.

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Departure Number: PTN DEP 7.3-1

AFFECTED DCD/FSAR SECTIONS:

DCD Figure 7.2-1 (Sheet 3 of 21), Table 7.3-1 (Sheets 6 and 7 of 9), Table 7.3-2 (Sheet 1 of 4), Subsections 7.3.1.2.14, 9.3.6.3.7, 9.3.6.4.5.1, 9.3.6.7, Table 14.3-2 (Sheets 9 and 12 of 17), Chapter 16 (TS Table 3.3.2-1 (Pages 9 and 10 of 13), TS Bases B 3.3.1 and B 3.3.2), and Subsection 19E.2.7.2.

Discussion and justification for each of these requests is provided in the following pages.

SUMMARY OF DEPARTURE:

IEEE 603 is a standard for safety systems imposed directly by 10 CFR part 50.55a(h). Clause 6.6 of this standard establishes three requirements for “Operating Bypasses”. This logic is included for many PMS functions to permit them to be blocked, so normal plant operations can occur without the unnecessary and onerous actuation of safety systems. Portions of the block/reset associated with the flux doubling logic does not comply with IEEE 603 Section 6.6. A permissive is required for bypasses in safety systems. The flux doubling actuation bypass does not have a permissive to prevent operating the bypass for the function.

With regard to IEEE 603 - 1991, the source range nuclear instrumentation includes a flux doubling function, the P-6 permissive instates this actuation. This actuation, when blocked, automatically reinstates the function when reset by P-6, which satisfies a part of IEEE 603 for automatic removal of the block. However, this function does not employ an operating bypass permissive to prevent blocking the function; or actuating the function when the conditions are not met.

SCOPE/EXTENT OF DEPARTURE:

Changes are made to ensure compliance with IEEE 603 and to support normal plant operation needs, as follows:

1. Add a new permissive, P-8, to permit blocking the flux logic during reactor startup. (Prevents blocking of flux doubling below 551°F RCS temperature for reactor startup, 510°F is the minimum temperature for criticality)
2. Add logic that will cause the PMS to force CVS valves 136A and 136B closed if the flux doubling logic is blocked during shutdown conditions (< 551°F). (Actuation if flux doubling is bypassed below 551°F RCS temperature, which is one option from IEEE 603, the other is to prevent the blocking, and this design change actuates the function)

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3. Include new permissive and actuation in Tech Specs, and describe the changes in Tier 2 information.

DEPARTURE JUSTIFICATION:

Preventing criticality from an inadvertent RCS dilution is the design function and the Source Range Neutron Flux doubling function is an input to it. Adding a permissive, as required by IEEE 603 -1991, for blocking this function when plant conditions require it to be active, prevents dilution water being added to the RCS. When blocked with an RCS temperature less than 551°F (Tech Spec minimum temperature for criticality), the demineralized water dilution valves are closed. This change satisfies IEEE 603 - 1991, Clause 6.6, and is consistent with accident analyses, as described in Chapter 19 and maintains reactor protection as required. This change provides protection from blocking the source range flux doubling signal when required for plant operation. Therefore, there are not any adverse effects on the design function.

Procedures currently provide guidance for operation of the flux doubling feature during plant operations and will continue to do so. Therefore, this is not an adverse change to procedures which control the Chemical and Volume Control System (CVS) during plant startup. This departure does not involve revising or replacing a described evaluation of methodology used for RCS inadvertent dilution. This change is consistent with the DCD analysis for inadvertent RCS dilution and does not affect any evaluation methodology. This activity does not involve a test or experiment not described in the plant-specific DCD, and is within the reference bounds of the design bases for preventing inadvertent dilution.

DEPARTURE EVALUATION:

This departure makes the changes stated above. The departure does not involve a significant reduction in the margin of safety and does not reduce the redundancy or diversity of any safety-related SSCs. Therefore, this departure does not:

1. Result in more than a minimal increase in the frequency of occurrence of an accident previously evaluated in the plant-specific DCD.
2. Result in more than a minimal increase in the likelihood of occurrence of a malfunction of an SSC important to safety and previously evaluated in the plant-specific DCD.
3. Result in more than a minimal increase in the consequences of an accident previously evaluated in the plant-specific DCD.
4. Result in more than a minimal increase in the consequences of a malfunction of an SSC important to safety previously evaluated in the plant-specific DCD.

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5. Create a possibility for an accident of a different type than any evaluated previously in the plant-specific DCD.
6. Create a possibility for a malfunction of an SSC important to safety with a different result than any evaluated previously in the plant-specific DCD.
7. Result in a design basis limit for a fission product barrier as described in the plant-specific DCD being exceeded or altered.
8. Result in a departure from a method of evaluation described in the plant-specific DCD used in establishing the design bases or in the safety analyses.

This departure does not affect resolution of a severe accident issue identified in the plant-specific DCD. Therefore, this departure has no safety significance.

NRC APPROVAL REQUIREMENT:

This departure requires an exemption from the requirements of 10 CFR Part 52, Appendix D, Section III.B, which requires compliance with generic Technical Specifications of the AP1000 DCD. Therefore, an exemption is requested in Part B of this COL Application Part.

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B. Turkey Point Units 6 & 7 Exemption Requests

FPL requests the following exemptions:

Exemption Number	Description
B.1	Combined License (COL) Application organization and numbering
B.2	Maximum safety wet bulb (noncoincident) air temperature
B.3	DELETED
B.4	Special Nuclear Material (SNM) Material Control and Accounting Program Description
B.5	Combustible Gas Control in Containment
B.6	Source Range Neutron Flux Doubling Block Permissive
B.7	Main Control Room Heatup
B.8	Containment Cooling Changes in regard to Passive Core Cooling System Condensate Return
B.9	Main Control Room Dose

Discussion and justification for each of these requests is provided in the following pages.

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B.1) COMBINED LICENSE (COL) APPLICATION ORGANIZATION AND NUMBERING (PART 52, APPENDIX D)

Applicable Regulation(s): 10 CFR Part 52, Appendix D, Section IV.A.2.a

Specific wording from which exemption is requested:

"IV. Additional Requirements and Restrictions

A. An applicant for a combined license that wishes to reference this appendix shall, in addition to complying with the requirements of 10 CFR 52.77, 52.79, and 52.80, comply with the following requirements:

1. Incorporate by reference, as part of its application, this appendix.
2. Include, as part of its application:
 - a. A plant-specific DCD containing the same type of information and using the same organization and numbering as the generic DCD for the AP1000 design, as modified and supplemented by the applicant's exemptions and departures;"

Pursuant to 10 CFR 52.7 and 52.93, FPL requests an exemption from the requirement of 10 CFR 52, Appendix D, Section IV.A.2.a, to include a plant-specific DCD "containing the same type of information and using the same organization and numbering as the generic DCD for the AP1000 design..." While the Turkey Point Units 6 & 7 plant specific DCD does contain the same type of information and generally follows the same organization and numbering as the generic DCD for the AP1000 design, some limited sections and subsections of the FSAR (as identified in the departures report as item STD DEP 1.1-1) do not follow the "same organization and numbering as the generic DCD for the AP1000 design." FPL proposes to provide the plant-specific DCD (i.e., FSAR) with some administrative revisions to the organization and numbering of the AP1000 DCD.

Discussion:

The AP1000 DCD generally has an organization and numbering format that provides text by subject in general conformance with the Standard Review Plans (SRPs) in effect at the time the DCD was written. Generally, COL information items are included at the end of a chapter, section, or subsection. In some cases, such as DCD Sections 2.1 and 2.2, the section may consist solely of a short description of topic and the COL information item subsection. This organization and numbering does not allow for the detailed discussion of these topics that is to be included in a complete FSAR section. As such, it is necessary to include numerous additional sections and subsections to fully address the topic as identified in the guidance of RG 1.206 and the applicable SRP. In other cases, the organization and numbering must be modified slightly to allow for

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inclusion of plant-specific discussions within the appropriate section of the FSAR, such as including an additional water system description in Section 9.2. In these cases, the COL information item discussions are retained at the end of the DCD corresponding chapter, section, or subsection (to maintain the organization), but the numbering may be different.

These differences are well identified in the FSAR as STD DEP 1.1-1 at each location where the departure is taken and are considered to be purely administrative to support a logical construction of the document. Where the departure from the DCD organization and numbering is taken, the revised organization and numbering generally follows the guidance provided in RG 1.206 and the applicable SRP. As such, there are no significant departures from the expected organization and numbering of a typical FSAR, and the information is readily identifiable to facilitate NRC review.

In view of the above, we believe that it would be inconsistent with the purpose of the rule for both FPL and the NRC to fully comply with the regulation of 10 CFR Part 52, Appendix D, Section IV.A.2.a, which requires strict adherence to the "same organization and numbering as the generic DCD for the AP1000 design." Accordingly, FPL hereby submits a request for an exemption from the regulations of 10 CFR 52, Appendix D, Section IV.A.2.a, pursuant to 10 CFR 52.7, "Specific Exemptions," and 10 CFR 52.93, "Exemptions and Variances."

Granting this request, which is authorized by law, would facilitate the NRC review of the Units 6 & 7 COL Application. For this and other reasons, granting this exemption request will not present an undue risk to the public health and safety, and is consistent with the common defense and security.

Moreover, compliance with the current rule would cause undue hardship for FPL and would also be inefficient and burdensome for the NRC staff. That approach would require FPL to prepare, and NRC to review, information with an organization and numbering that is unfamiliar and inconsistent with the current guidance for format and content of a COL Application.

Additionally, compliance with Appendix D, Section IV.A.2.a, is not necessary to achieve its underlying purpose. Most of the FSAR conforms to the organization and numbering of the referenced DCD. The exceptions are limited and do not lead to confusion regarding the incorporation of the DCD into the FSAR.

For these reasons, FPL requests approval of the requested exemption from current regulations of 10 CFR 52, Appendix D, Section IV.A.2.a, as identified herein and in the application departures report.

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B.2) MAXIMUM SAFETY WET BULB (NONCOINCIDENT) AIR TEMPERATURE (PART 52, APPENDIX D)

Applicable Regulation(s): 10 CFR Part 52, Appendix D, Section IV.A.2.d

Specific wording from which exemption is requested:

"IV. Additional Requirements and Restrictions

A. An applicant for a combined license that wishes to reference this appendix shall, in addition to complying with the requirements of 10 CFR 52.77, 52.79, and 52.80, comply with the following requirements:

1. Incorporate by reference, as part of its application, this appendix.
2. Include, as part of its application:
 - a. A plant-specific DCD containing the same type of information and using the same organization and numbering as the generic DCD for the AP1000 design, as modified and supplemented by the applicant's exemptions and departures;
 - b. The reports on departures from and updates to the plant-specific DCD required by paragraph X.B of this appendix;
 - c. Plant-specific TS, consisting of the generic and site-specific TS that are required by 10 CFR 50.36 and 50.36a;
 - d. Information demonstrating compliance with the site parameters and interface requirements;"

Pursuant to 10 CFR 52.7 and 52.93, FPL requests an exemption from the requirement of 10 CFR 52, Appendix D, Section IV.A.2.d, to include "information demonstrating compliance with the site parameters and interface requirements."

Discussion:

The site parameter value provided in DCD Tier 1, Table 5.0-1 for the air temperature maximum wet bulb (noncoincident) is 86.1°F. This site parameter value is listed as the maximum safety wet bulb (noncoincident) air temperature in DCD Tier 2, Table 2-1. The site characteristic for the maximum safety wet bulb (noncoincident) air temperature for Units 6 & 7 is 87.4°F. This is the 100-year return estimate of 2-hour duration as reported in FSAR Subsection 2.3.1.5. This temperature exceeds the DCD site parameter of 86.1°F by 1.3°F.

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Analysis of the maximum safety wet bulb (noncoincident) air temperature of 87.4°F for Units 6 & 7 has been performed. The results of this analysis show that the higher maximum safety wet bulb (noncoincident) air temperature will not adversely affect any safety-related structures, systems or components.

Conclusion:

This exemption request was evaluated in accordance with Section VIII.A.4 of the design certification rule which requires that 1) the change will not result in a significant decrease in the level of safety otherwise provided by the design; 2) the exemption is authorized by law, will not present an undue risk to the public health and safety, and is consistent with the common defense and security; 3) special circumstances are present as specified in 10 CFR 50.12(a)(2); and 4) the special circumstances outweigh any decrease in safety that may result from the reduction in standardization caused by the exemption. As shown below, each of these four criteria are satisfied.

(1) As described above, the exemption does not have an adverse impact on the AP1000 Standard Plant design and therefore will not result in a significant decrease in the level of safety otherwise provided by the design.

(2) The exemption is not inconsistent with the Atomic Energy Act or any other statute and therefore is authorized by law. As discussed above, the exemption does not have an adverse impact on the AP1000 Standard Plant design and therefore will not present an undue risk to the public health and safety. The exemption does not relate to security and does not otherwise pertain to the common defense and security.

(3) Special circumstances are present as specified in 10 CFR 50.12(a)(2). Specifically, application of 10 CFR 52, Appendix D, Section IV.A.2.d and the site parameters in Tier 1 of the DCD are not necessary to achieve the underlying purpose of the rules. The analysis described above shows that the increase in the maximum safety temperature does not affect the AP1000 Standard Plant design. Consequently, granting relief from the maximum safety air temperature in the DCD would maintain the level of safety in the design, which is the underlying purpose of the rule.

(4) The special circumstances outweigh any decrease in safety that may result from the reduction in standardization (due to the increase in the maximum safety temperature) caused by the exemption. Specifically, the exemption does not change the AP1000 Standard Plant design and does not affect the configuration of the plant or the manner in which the plant is operated.

As demonstrated above, this exemption request complies with the requirements in Section VIII.A.4 of the design certification rule for the AP1000. Therefore, the exemption also satisfies the requirements in 10 CFR 52.7 for an exemption from 10 CFR 52, Appendix D, Section IV.A.2.d,

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since the criteria in 10 CFR 52.7 are a subset of the criteria in Section VIII.A.4 of the design certification rule for the AP1000.

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B.3) DELETED

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B.4) SPECIAL NUCLEAR MATERIAL (SNM) MATERIAL CONTROL AND ACCOUNTING (MC&A) PROGRAM DESCRIPTION [PART 70, SUBPART D AND PART 74, SUBPARTS C, D, AND E]

Applicable Regulation(s): 10 CFR §§ 70.22(b), 70.32(c), 74.31, 74.41, and 74.51

Specific wording from which exemption is requested:

10 CFR 70.22(b), Contents of applications:

- (b) Each application for a license to possess special nuclear material, to possess equipment capable of enriching uranium, to operate an uranium enrichment facility, to possess and use at any one time and location special nuclear material in a quantity exceeding one effective kilogram, except for applications for use as sealed sources and for those uses involved in the operation of a nuclear reactor licensed pursuant to Part 50 of this chapter and those involved in a waste disposal operation, must contain a full description of the applicant's program for control and accounting of such special nuclear material or enrichment equipment that will be in the applicant's possession under license to show how compliance with the requirements of §§ 74.31, 74.33, 74.41, or 74.51 of this chapter, as applicable, will be accomplished.

10 CFR 70.32, Conditions of licenses:

- (c) (1) Each license authorizing the possession and use at any one time and location of uranium source material at an uranium enrichment facility or special nuclear material in a quantity exceeding one effective kilogram, except for use as sealed sources and those uses involved in the operation of a nuclear reactor licensed pursuant to Part 50 of this chapter and those involved in a waste disposal operation, shall contain and be subject to a condition requiring the licensee to maintain and follow:
 - (i) The program for control and accounting of uranium source material at an uranium enrichment facility and special nuclear material at all applicable facilities as implemented pursuant to § 70.22(b), or §§ 74.31(b), 74.33(b), 74.41(b), or 74.51(c) of this chapter, as appropriate;
 - (ii) The measurement control program for uranium source material at an uranium enrichment facility and for special nuclear material at all applicable facilities as implemented pursuant to §§ 74.31(b), 74.33(b), 74.45(c), or 74.59(e) of this chapter, as appropriate; and
 - (iii) Other material control procedures as the Commission determines to be essential for the safeguarding of uranium source material at an uranium enrichment facility

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or of special nuclear material and providing that the licensee shall make no change that would decrease the effectiveness of the material control and accounting program implemented pursuant to § 70.22(b), or §§ 74.31(b), 74.33(b), 74.41(b), or 74.51(c) of this chapter, and the measurement control program implemented pursuant to §§ 74.31(b), 74.33(b), 74.41(b), or 74.59(e) of this chapter without the prior approval of the Commission. A licensee desiring to make changes that would decrease the effectiveness of its material control and accounting program or its measurement control program shall submit an application for amendment to its license pursuant to § 70.34.

10 CFR 74.31, Nuclear material control and accounting for special nuclear material of low strategic significance:

- (a) General performance objectives. Each licensee who is authorized to possess and use more than one effective kilogram of special nuclear material of low strategic significance, excluding sealed sources, at any site or contiguous sites subject to control by the licensee, other than a production or utilization facility licensed pursuant to Part 50 or 70 of this chapter, or operations involved in waste disposal, shall implement and maintain a Commission approved material control and accounting system that will achieve the following objectives:

10 CFR 74.41, Nuclear material control and accounting for special nuclear material of moderate strategic significance:

- (a) General performance objectives. Each licensee who is authorized to possess special nuclear material (SNM) of moderate strategic significance or SNM in a quantity exceeding one effective kilogram of strategic special nuclear material in irradiated fuel reprocessing operations other than as sealed sources and to use this material at any site other than a nuclear reactor licensed pursuant to Part 50 of this chapter; or as reactor irradiated fuels involved in research, development, and evaluation programs in facilities other than irradiated fuel reprocessing plants; or an operation involved with waste disposal, shall establish, implement, and maintain a Commission-approved material control and accounting (MC&A) system that will achieve the following performance objectives:

10 CFR 74.51, Nuclear material control and accounting for strategic special nuclear material:

- (a) General performance objectives. Each licensee who is authorized to possess five or more formula kilograms of strategic special nuclear material (SSNM) and to use such material at any site, other than a nuclear reactor licensed pursuant to Part 50 of this chapter, an irradiated fuel reprocessing plant, an operation involved with waste disposal, or an independent spent fuel storage facility licensed pursuant to Part 72 of

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this chapter shall establish, implement, and maintain a Commission-approved material control and accounting (MC&A) system that will achieve the following objectives:

Discussion:

Florida Power & Light Company (FPL) requests an exemption from the requirements of 10 CFR § 70.22(b) and, in turn, §§ 70.32(c), 74.31, 74.41, and 74.51. Section 70.22(b) requires an application for a license for special nuclear material to contain a full description of the applicant's program for material control and accounting (MC&A) of special nuclear material under §§ 74.31, 74.33, 74.41, and 74.51¹. Section 70.32(c) requires a license authorizing the use of special nuclear material to contain and be subject to a condition requiring the licensee to maintain and follow a special nuclear material control and accounting program, measurement control program, and other material control procedures, including the corresponding records management requirements. However, §§ 70.22(b), 70.32(c), 74.31, 74.41, and 74.51 contain exceptions for nuclear reactors licensed under 10 CFR Part 50. The regulations applicable to the MC&A of special nuclear material for nuclear reactors licensed under 10 CFR Part 50 are provided in 10 CFR Part 74, Subpart B, §§ 74.11 through 74.19, excluding § 74.17. The purpose of this exemption request is to seek a similar exception for this combined license (COL) under 10 CFR Part 52, such that the same regulations will be applied to the special nuclear material MC&A program as nuclear reactors licensed under 10 CFR Part 50.

Nuclear reactors licensed under Part 50 are explicitly excepted from the requirements of §§ 70.22(b), 70.32(c), 74.31, 74.41, and 74.51. There is no technical or regulatory reason to treat nuclear reactors licensed under Part 52 differently than reactors licensed under Part 50 with respect to the MC&A provisions in 10 CFR Part 74. As indicated in the Statement of Considerations for 10 CFR § 52.0(b) (72 Fed. Reg. 49352, 49372, 49436 (Aug. 28, 2007)), applicants and licensees under Part 52 are subject to all of the applicable requirements in 10 CFR Chapter I, whether or not those provisions explicitly mention a COL under Part 52. This regulation clearly indicates that plants licensed under Part 52 are to be treated no differently than plants licensed under Part 50 with respect to the substantive provisions in 10 CFR Chapter I (which includes Parts 70 and 74). In particular, the exception for nuclear reactors licensed under Part 50, as contained in §§ 70.22(b), 70.32(c), 74.31, 74.41, or 74.51, should also be applied to reactors licensed under Part 52.

An exemption from the requirements of §§ 70.22(b), 70.32(c), 74.31, 74.41, and 74.51 would not mean that a MC&A program would be unnecessary or that the COL application would be silent regarding MC&A. To the contrary, the MC&A requirements in Subpart B to Part 74 would still be

¹ While not containing an explicit exception for Part 50 reactors, § 74.33 applies only to uranium enrichment facilities and thus is not directly implicated in this exemption request.

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applicable to the COL just as they are to licenses issued under Part 50. Additionally, the COL application will describe the MC&A program for satisfying Subpart B to Part 74.

This exemption request is evaluated under 10 CFR § 52.7, which incorporates the requirements of § 50.12. That section allows the Commission to grant an exemption if 1) the exemption is authorized by law, 2) will not present an undue risk to the public health and safety, 3) is consistent with the common defense and security, and 4) special circumstances are present as specified in 10 CFR § 50.12(a)(2). The criteria in § 50.12 encompass the criteria for an exemption in 10 CFR §§ 70.17(a) and 74.7, the specific exemption requirements for Parts 70 and 74, respectively. Therefore, by demonstrating that the exemption criteria in § 50.12 are satisfied, this request also demonstrates that the exemption criteria in §§ 52.7, 70.17(a) and 74.7 are satisfied.

Evaluation Against Exemption Criteria

- 1) This exemption is not inconsistent with the Atomic Energy Act or any other statute and is therefore authorized by law.
- 2) An exemption from the requirements of 10 CFR §§ 70.22(b), 70.32(c), 74.31, 74.41, and 74.51 would not present an undue risk to public health and safety. The exemption would treat the COL applicant similarly to Part 50 license applicants, who are excepted from the regulations in question. Furthermore, the COL application will contain a description of the applicant's MC&A program under Subpart B to Part 74. Therefore, the exemption from 10 CFR §§ 70.22(b), 70.32(c), 74.31, 74.41, and 74.51 would not present an undue risk to public health and safety.
- 3) An exemption from the requirements of 10 CFR §§ 70.22(b), 70.32(c), 74.31, 74.41, and 74.51 would not be inconsistent with the common defense and security. The exemption would treat the COL applicant similarly to Part 50 license applicants, who are excepted from the regulations in question. Furthermore, the COL application will contain a description of the applicant's MC&A program under Subpart B to Part 74. Therefore, the exemption from §§ 70.22(b), 70.32(c), 74.31, 74.41, and 74.51 is consistent with the common defense and security.
- 4) The exemption request involves special circumstances under 10 CFR § 50.12(a)(2)(ii). That subsection defines special circumstances as when "[a]pplication of the regulation in the particular circumstances would not serve the underlying purpose of the rule or is not necessary to achieve the underlying purpose of the rule." Since the Commission determined that the requirements in 10 CFR §§ 70.22(b), 70.32(c), 74.31, 74.41, and 74.51 are unnecessary for Part 50 applicants, those requirements are also unnecessary for Part 52 applicants.

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As demonstrated above, the exemption complies with the requirements of 10 CFR §§ 50.12, 52.7, 70.17, and 74.7. For these reasons, approval of the requested exemption is requested from the regulations of 10 CFR §§ 70.22(b), 70.32(c), 74.31, 74.41, and 74.51, as described herein.

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B.5) COMBUSTIBLE GAS CONTROL IN CONTAINMENT

Applicable Regulation(s): 10 CFR Part 52, Appendix D, Section III.B

Specific wording from which exemption is requested:

“III. Scope and Contents

- B. An applicant or licensee referencing this appendix, in accordance with Section IV of this appendix, shall incorporate by reference and comply with the requirements of this appendix, including Tier 1, Tier 2 (including the investment protection short-term availability controls in Section 16.3 of the DCD), and the generic TS except as otherwise provided in this appendix. Conceptual design information in the generic DCD and the evaluation of severe accident mitigation design alternatives in appendix 1B of the generic DCD are not part of this appendix.”

Pursuant to 10 CFR § 52.63(b)(1), an exemption from elements of the design as certified in the 10 CFR Part 52, Appendix D, design certification rule is requested for a plant-specific Tier 1 non-material departure from the AP1000 DCD for Tier 1 information. This exemption request is in accordance with the provisions of 10 CFR § 50.12, 10 CFR § 52.7, and 10 CFR Part 52, Appendix D.

Discussion:

The changes requested to Tier 1 Table 2.3.9-3 and associated Tier 2 changes to Subsections 6.2.4.5.1 and 19.41.7 provide a revised acceptance criteria for hydrogen venting inside containment, provide reasonable assurance that the facility has been constructed and will be operated in conformity with the applicable design criteria, codes and standards, and demonstrate acceptable Containment Hydrogen Control System performance during design basis scenarios.

Conclusion:

FPL evaluated this exemption request in accordance with 10 CFR Part 52, Appendix D, Section VIII.A.4, 10 CFR § 50.12, 10 CFR § 52.7 and 10 CFR § 52.63, which state that the NRC may grant exemptions from the requirements of the regulations provided the following six conditions are met: 1) the exemption is authorized by law [§ 50.12(a)(1)]; 2) the exemption will not present an undue risk to the health and safety of the public [§ 50.12(a)(1)]; 3) the exemption is consistent with the common defense and security [§ 50.12(a)(1)]; 4) special circumstances are present [§ 50.12(a)(2)]; 5) the special circumstances outweigh any decrease in safety that may result from the reduction in standardization caused by the exemption [§ 52.63(b)(1)]; and 6) the design change will not result in a significant decrease in the level of safety [Part 52, Appendix D,

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VIII.A.4]. The requested exemption satisfies the criteria for granting specific exemptions, as described below.

1. This exemption is authorized by law

The NRC has authority under 10 CFR §§ 50.12, 52.7, and 52.63 to grant exemptions from the requirements of NRC regulations. Specifically, 10 CFR §§ 50.12 and 52.7 state that the NRC may grant exemptions from the requirements of 10 CFR Part 52 upon a proper showing. No law exists that would preclude the changes covered by this exemption request. Additionally, granting of the proposed exemption does not result in a violation of the Atomic Energy Act of 1954, as amended, or the Commission's regulations.

Accordingly, this requested exemption is “authorized by law,” as required by 10 CFR § 50.12(a)(1).

2. This exemption will not present an undue risk to the health and safety of the public

The proposed exemption from the requirements of 10 CFR 52, Appendix D, Section III.B would allow changes to elements of the plant-specific Tier 1 DCD to depart from the AP1000 certified (Tier 1) design information. The plant-specific Tier 1 DCD will continue to reflect the approved licensing basis for the applicant, and will maintain a consistent level of detail with that which is currently provided elsewhere in Tier 1 of the plant-specific DCD. Because the change to the ITAAC acceptance criteria in Tier 1 Table 2.3.9-3 maintains the design margins of the Containment Hydrogen Control System, the changed acceptance criteria will ensure the protection of the health and safety of the public. Therefore, no adverse safety impact which would present any additional risk to the health and safety of the public is present. The affected Design Description in the plant-specific Tier 1 DCD will continue to provide the detail necessary to support the performance of the associated ITAAC.

Therefore, the requested exemption from 10 CFR 52, Appendix D, Section III.B would not present an undue risk to the health and safety of the public.

3. The exemption is consistent with the common defense and security

The exemption from the requirements of 10 CFR 52, Appendix D, Section III.B would change elements of the plant-specific Tier 1 DCD by departing from the AP1000 certified (Tier 1) design information relating to the control of combustible gas inside containment. The exemption does not alter the design, function, or operation of any structures or plant equipment that are necessary to maintain a secure status of the plant. The proposed exemption has no impact on plant security or safeguards procedures.

Therefore, the requested exemption is consistent with the common defense and security.

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4. Special circumstances are present

10 CFR § 50.12(a)(2) lists six “special circumstances” for which an exemption may be granted. Pursuant to the regulation, one of these special circumstances must be present in order for the NRC to consider granting an exemption request. The requested exemption meets the special circumstances of 10 CFR § 50.12(a)(2)(ii). That subsection defines special circumstances as when “Application of the regulation in the particular circumstances would not serve the underlying purpose of the rule or is not necessary to achieve the underlying purpose of the rule.”

The rule under consideration in this request for exemption from Tier 1 Table 2.3.9-3 is 10 CFR 52, Appendix D, Section III.B, which requires that an applicant referencing the AP1000 Design Certification Rule (10 CFR Part 52, Appendix D) shall incorporate by reference and comply with the requirements of Appendix D, including Tier 1 information. The Turkey Point Units 6 and 7 COLA references the AP1000 Design Certification Rule and incorporates by reference the requirements of 10 CFR Part 52, Appendix D, including Tier 1 information. The underlying purpose of Appendix D, Section III.B is to describe and define the scope and contents of the AP1000 design certification, and to require compliance with the design certification information in Appendix D to maintain the level of safety in the design.

The proposed change to the ITAAC acceptance criteria for combustible gas control maintains the design margins of the Containment Hydrogen Control System. This change does not impact the ability of any structures, systems, or components to perform their functions or negatively impact safety. Accordingly, this exemption from the certification information in Tier 1 Subsection Table 2.3.9-3 will enable the applicant to safely construct and operate the AP1000 facility consistent with the design certified by the NRC in 10 CFR 52, Appendix D.

Therefore, special circumstances are present, because application of the current generic certified design information in Tier 1 as required by 10 CFR Part 52, Appendix D, Section III.B, in the particular circumstances discussed in this request is not necessary to achieve the underlying purpose of the rule.

5. The special circumstances outweigh any decrease in safety that may result from the reduction in standardization caused by the exemption

Based on the nature of the changes to the plant-specific Tier 1 information and the understanding that these changes support the design function of the Containment Hydrogen Control System, other AP1000 applicants and licensees will likely request this exemption. However, if this is not the case, the special circumstances continue to outweigh any decrease in safety from the reduction in standardization because the key design functions of the Containment Hydrogen Control System associated with this request will continue to be

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maintained. This exemption request and the associated marked-up Tier 1 Table 2.3.9-3 demonstrates that the Containment Hydrogen Control System function continues to be maintained following implementation of the change from the generic AP1000 DCD, thereby minimizing the safety impact resulting from any reduction in standardization.

Therefore, the special circumstances associated with the requested exemption outweigh any decrease in safety that may result from the reduction in standardization caused by the exemption. In fact, as described in Condition 6 below, the exemption will result in no reduction in the level of safety.

6. The design change will not result in a significant decrease in the level of safety

The exemption revises the plant-specific DCD Tier 1 information by revising the acceptance criteria for an ITAAC in Table 2.3.9-3. There is no physical change to the plant associated with the change to the ITAAC acceptance criteria. Because the Containment Hydrogen Control System function is met, there is no reduction in the level of safety. Therefore, the change will not result in a significant decrease in the level of safety.

As demonstrated above, this exemption request satisfies NRC requirements for an exemption to the design certification rule for the AP1000 plant.

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B.6) SOURCE RANGE NEUTRON FLUX DOUBLING BLOCK PERMISSIVE

Applicable Regulation(s): 10 CFR Part 52 Appendix D, Section III.B

Specific wording from which exemption is requested:

“III. Scope and Contents

- B. An applicant or licensee referencing this appendix, in accordance with Section IV of this appendix, shall incorporate by reference and comply with the requirements of this appendix, including Tier 1, Tier 2 (including the investment protection short-term availability controls in Section 16.3 of the DCD), and the generic TS except as otherwise provided in this appendix. Conceptual design information in the generic DCD and the evaluation of severe accident mitigation design alternatives in appendix 1B of the generic DCD are not part of this appendix.”

Pursuant to 10 CFR § 52.63(b)(1), an exemption from elements of the design as certified in the 10 CFR Part 52, Appendix D, design certification rule is requested from the AP1000 DCD for a departure from the generic TS. These material departures involve the addition of a permissive to the source range flux doubling function to prevent bypassing the CVS makeup isolation actuation upon a source range flux doubling to more effectively perform its design function and provide reactor protection as analyzed. The departures include a change to TS Table 3.3.2-1 which involves adding the P-8 permissive to the instrument Table. This exemption request is in accordance with the provisions of 10 CFR § 50.12, 10 CFR § 52.7, and 10 CFR Part 52, Appendix D.

Discussion:

The changes requested to Tier 2, to Figure 7.2-1 (Sheet 3 of 21), Subsection 7.3.1.2.14, Table 7.3-1 (Sheet 6 of 9), Table 7.3-1 (Sheet 7 of 9), Table 7.3.2 (Sheet 1 of 4), Subsection 9.3.6.3.7, Subsection 9.3.6.4.5.1, Subsection 9.3.6.7, Table 14.3-2 (Sheet 9 of 17), Table 14.3-2 (Sheet 12 of 17), Subsection 19E.2.7.2, Technical Specifications Table 3.3.2-1 (Page 9, 10 of 13), and Tech Spec Bases Sections B 3.3.1 and B 3.3.2, provide additional equipment and TS requirements, provide reasonable assurance that the facility has been constructed and will be operated in conformity with the applicable design criteria, codes and standards, and demonstrate acceptable performance during design basis scenarios and reactor startup.

Conclusion:

This exemption request is evaluated in accordance with 10 CFR Part 52, Appendix D, Section VIII.A.4, 10 CFR § 50.12, 10 CFR § 52.7 and 10 CFR § 52.63, which state that the NRC

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may grant exemptions from the requirements of the regulations provided the following six conditions are met: 1) the exemption is authorized by law [§ 50.12(a)(1)]; 2) the exemption will not present an undue risk to the health and safety of the public [§ 50.12(a)(1)]; 3) the exemption is consistent with the common defense and security [§ 50.12(a)(1)]; 4) special circumstances are present [§ 50.12(a)(2)]; 5) the special circumstances outweigh any decrease in safety that may result from the reduction in standardization caused by the exemption [§ 52.63(b)(1)]; and 6) the design change will not result in a significant decrease in the level of safety [Part 52, Appendix D, VIII.A.1]. The requested exemption satisfies the criteria for granting specific exemptions, as described below.

1. This exemption is authorized by law

The NRC has authority under 10 CFR §§ 50.12, 52.7, and 52.63 to grant exemptions from the requirements of NRC regulations. Specifically, 10 CFR §§ 50.12 and 52.7 state that the NRC may grant exemptions from the requirements of 10 CFR Part 52 upon a proper showing. No law exists that would preclude the changes covered by this exemption request. Additionally, granting of the proposed exemption does not result in a violation of the Atomic Energy Act of 1954, as amended, or the Commission's regulations.

Accordingly, this requested exemption is “authorized by law,” as required by 10 CFR § 50.12(a)(1).

2. This exemption will not present an undue risk to the health and safety of the public

The proposed exemption from the requirements of 10 CFR 52, Appendix D, Section III.B would allow changes to elements of the generic Technical Specifications to depart from the AP1000 certified (Tier 2) information. The plant-specific Tier 1 DCD will continue to reflect the approved licensing basis for the applicant, and will maintain a consistent level of detail with that which is currently provided elsewhere in Tier 1 of the plant-specific DCD. Because the change to the source range flux doubling function description maintains its design functions, the changed design will ensure the protection of the health and safety of the public.

Therefore, no adverse safety impact which would present any additional risk to the health and safety of the public is present. The affected Design Description in the generic Technical Specifications will continue to provide the detail necessary to support the performance of the function requirements.

Therefore, the requested exemption from 10 CFR 52, Appendix D, Section III.B would not present an undue risk to the health and safety of the public.

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3. The exemption is consistent with the common defense and security

The exemption from the requirements of 10 CFR 52, Appendix D, Section III.B would change elements of the generic Technical Specifications by departing from the AP1000 certified design information relating to the flux doubling portion of the source ranges neutron flux and departing from the Tier 2 generic TS to include operability requirements of added plant equipment (P-8 permissive). The exemption does not alter the design, function, or operation of any structures or plant equipment that are necessary to maintain a safe and secure status of the plant. The proposed exemption has no impact on plant security or safeguards procedures. Therefore, the requested exemption is consistent with the common defense and security.

4. Special circumstances are present

10 CFR § 50.12(a)(2) lists six “special circumstances” for which an exemption may be granted. Pursuant to the regulation, it is necessary for one of these special circumstances to be present in order for the NRC to consider granting an exemption request. The requested exemption meets the special circumstances of 10 CFR § 50.12(a)(2)(ii). That subsection defines special circumstances as when “Application of the regulation in the particular circumstances would not serve the underlying purpose of the rule or is not necessary to achieve the underlying purpose of the rule.”

The rule under consideration in this request for exemption from Tier 2 generic TS is 10 CFR 52, Appendix D, Section III.B, which requires an applicant referencing the AP1000 Design Certification Rule (10 CFR Part 52, Appendix D) shall incorporate by reference and comply with the requirements of Appendix D, including Tier 1 information and generic TS. The Turkey Point Units 6 & 7 COLA references the AP1000 Design Certification Rule and incorporates by reference the requirements of 10 CFR Part 52, Appendix D, including Tier 1 information and generic TS. The underlying purpose of Appendix D, Section III.B, is to describe and define the scope and contents of the AP1000 design certification, and to require compliance with the design certification information in Appendix D to maintain the level of safety in the design.

The proposed changes to the source range neutron flux doubling function maintain the design margins. This change does not impact the ability of any structures, systems, or components to perform their functions or negatively impact safety. Accordingly, this exemption from the certification information in Tier 2 TS Table 3.3.2-1 will enable the applicant to safely construct and operate the AP1000 facility consistent with the design certified by the NRC in 10 CFR 52, Appendix D.

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Therefore, special circumstances are present, because application of the generic TS as required by 10 CFR Part 52, Appendix D, Section III.B in the particular circumstances discussed in this request is not necessary to achieve the underlying purpose of the rule.

5. The special circumstances outweigh any decrease in safety that may result from the reduction in standardization caused by the exemption

Based on the nature of the changes to the plant-specific Tier 2 and the generic TS and the understanding that these changes support the design function of the source range neutron flux doubling, it is likely that other AP1000 applicants and licensees will request this exemption. However, if this is not the case, the special circumstances continue to outweigh any decrease in safety from the reduction in standardization because the key design functions of the source range neutron flux doubling associated with this request will continue to be maintained. This exemption request and the associated TS marked-up tables demonstrate the source range neutron flux doubling function continues to be maintained following implementation of the change from the generic AP1000 DCD, thereby minimizing the safety impact resulting from any reduction in standardization.

Therefore, the special circumstances associated with the requested exemption outweigh any decrease in safety that may result from the reduction in standardization caused by the exemption. In fact, as described in Condition 6, below, the exemption will result in no reduction in the level of safety.

6. The design change will not result in a significant decrease in the level of safety

The exemption revises the generic Technical Specifications by adding components to TS Table 3.3.2-1. Because the Source Range neutron flux doubling design function is met, there is no reduction in the level of safety.

Therefore, the design change and associated change to the TS will not result in a significant decrease in the level of safety. As demonstrated above, this exemption request satisfies NRC requirements for an exemption to the design certification rule for the AP1000.

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B.7) MAIN CONTROL ROOM HEATUP

Applicable Regulation(s): 10 CFR Part 52, Appendix D, Section III.B

Specific wording from which exemption is requested:

"III. Scope and Contents

- B. An applicant or licensee referencing this appendix, in accordance with Section IV of this appendix, shall incorporate by reference and comply with the requirements of this appendix, including Tier 1, Tier 2 (including the investment protection short-term availability controls in Section 16.3 of the DCD), and the generic TS except as otherwise provided in this appendix. Conceptual design information in the generic DCD and the evaluation of severe accident mitigation design alternatives in appendix 1B of the generic DCD are not part of this appendix."

Pursuant to 10 CFR § 52.63(b)(1), an exemption from elements of the design as certified in the 10 CFR Part 52, Appendix D, design certification rule is requested for plant-specific Tier 1 departures from the AP1000 DCD for Tier 1 information and for material departures from the generic Technical Specification (TS).

Discussion:

The proposed changes are to Tier 1 Tables 2.2.5-1, 2.2.5-4, 2.5.2-3 and 2.5.2-4, and TS 3.3.2 and 3.7.6. These changes ensure the Main Control Room Emergency Habitability System (VES) design functions to: 1) maintain heat loads within the main control room envelope (MCRE) within design basis assumptions to limit the heat-up of the room, 2) ensure a 72-hour supply of breathable quality air for the occupants of the MCRE, 3) maintain the MCRE pressure boundary at a positive pressure with respect to the surrounding areas with a discharge of air through the main control room (MCR) vestibule, and 4) provide a passive recirculation flow of MCRE air to maintain MCR dose rates below an acceptable level during VES operation.

Conclusion:

FPL evaluated this exemption request in accordance with 10 CFR Part 52, Appendix D, Section VIII.A.4, 10 CFR § 50.12, 10 CFR § 52.7 and 10 CFR § 52.63, which state that the NRC may grant exemptions from the requirements of the regulations provided the following six conditions are met: 1) the exemption is authorized by law [§ 50.12(a)(1)]; 2) the exemption will not present an undue risk to the health and safety of the public [§ 50.12(a)(1)]; 3) the exemption is consistent with the common defense and security [§ 50.12(a)(1)]; 4) special circumstances are present [§ 50.12(a)(2)]; 5) the special circumstances outweigh any decrease in safety that may result from the reduction in standardization caused by the exemption [§ 52.63(b)(1)]; and 6) the

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design change will not result in a significant decrease in the level of safety [Part 52, Appendix D, VIII.A.4]. The requested exemption satisfies the criteria for granting specific exemptions, as described below.

1. This exemption is authorized by law

The NRC has authority under 10 CFR §§ 50.12, 52.7, and 52.63 to grant exemptions from the requirements of NRC regulations. Specifically, 10 CFR §§ 50.12 and 52.7 state that the NRC may grant exemptions from the requirements of 10 CFR Part 52 upon a proper showing. No law exists that would preclude the changes covered by this exemption request. Additionally, granting of the proposed exemption does not result in a violation of the Atomic Energy Act of 1954, as amended, or the Commission's regulations. Accordingly, this requested exemption is "authorized by law," as required by 10 CFR § 50.12(a)(1).

2. This exemption will not present an undue risk to the health and safety of the public

The proposed exemption from the requirements of 10 CFR 52, Appendix D, Section III.B would allow changes to elements of the plant-specific DCD Tier 1 design information and generic TS. The plant-specific Tier 1 DCD will continue to reflect the approved licensing basis for the applicant, and will maintain a consistent level of detail with that which is currently provided elsewhere in Tier 1 of the plant-specific DCD. Because the change to the VES system description and associated TS changes maintain VES design functions, the changed design will ensure the protection of the health and safety of the public.

Therefore, no adverse safety impact which would present any additional risk to the health and safety of the public is present. The affected Design Description in the plant-specific Tier 1 DCD will continue to provide the detail necessary to support the performance of the associated ITAAC. Therefore, the requested exemption from 10 CFR 52, Appendix D, Section III.B would not present an undue risk to the health and safety of the public.

3. The exemption is consistent with the common defense and security

The exemption from the requirements of 10 CFR 52, Appendix D, Section III.B would change elements of the plant-specific DCD Tier 1 design information relating to the operation of the VES and generic TS. The exemption does not alter the design, function, or operation of any structures or plant equipment that are necessary to maintain a secure status of the plant. The proposed exemption has no impact on plant security or safeguards procedures. Therefore, the requested exemption is consistent with the common defense and security.

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4. Special circumstances are present

10 CFR § 50.12(a)(2) lists six “special circumstances” for which an exemption may be granted. Pursuant to the regulation, it is necessary for one of these special circumstances to be present in order for the NRC to consider granting an exemption request. The requested exemption meets the special circumstances of 10 CFR § 50.12(a)(2)(ii). That subsection defines special circumstances as when “Application of the regulation in the particular circumstances would not serve the underlying purpose of the rule or is not necessary to achieve the underlying purpose of the rule.”

The rule under consideration in this request for exemption from Tier 1 subsections 2.2.5 and 2.5.2, and the generic TS is 10 CFR 52, Appendix D, Section III.B, which requires that an applicant referencing the AP1000 Design Certification Rule (10 CFR Part 52, Appendix D) shall incorporate by reference and comply with the requirements of Appendix D, including Tier 1 information and generic TS. The Turkey Point Units 6 and 7 COLA references the AP1000 Design Certification Rule and incorporates by reference the requirements of 10 CFR Part 52, Appendix D, including Tier 1 information and generic TS. The underlying purpose of Appendix D, Section III.B is to describe and define the scope and contents of the AP1000 design certification, and to require compliance with the design certification information in Appendix D to maintain the level of safety in the design.

The proposed changes maintain the design functions of the VES. This change does not impact the ability of any structures, systems, or components to perform their functions or negatively impact safety. Accordingly, this exemption from the certification information in Tier 1 subsections 2.2.5 and 2.5.2 and from generic TS will enable the applicant to safely construct and operate the AP1000 facility consistent with the design certified by the NRC in 10 CFR 52, Appendix D.

Therefore, special circumstances are present, because application of the current generic certified design information in Tier 1 and the generic TS as required by 10 CFR Part 52, Appendix D, Section III.B, in the particular circumstances discussed in this request is not necessary to achieve the underlying purpose of the rule.

5. The special circumstances outweigh any decrease in safety that may result from the reduction in standardization caused by the exemption

Based on the nature of the changes to the plant-specific Tier 1 information and generic TS and the understanding that these changes support the design function of the VES, it is likely that other AP1000 applicants and licensees will request this exemption. However, if this is not the case, the special circumstances continue to outweigh any decrease in safety from the reduction in standardization because the key design functions of the VES associated with this

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request will continue to be maintained. This exemption request and the associated DCD and TS changes demonstrate that the VES function continues to be maintained following implementation of the change from the generic AP1000 DCD, thereby minimizing the safety impact resulting from any reduction in standardization.

Therefore, the special circumstances associated with the requested exemption outweigh any decrease in safety that may result from the reduction in standardization caused by the exemption. In fact, as described in Condition 6 below, the exemption will not result in a reduction in the level of safety.

6. The design change will not result in a significant decrease in the level of safety

The exemption revises the plant-specific DCD Tier 1 information by enabling the VES to more effectively perform its design functions. This exemption also revises the generic TS to ensure equipment operability and temperature conditions are maintained. Because the VES design functions are met, there is no reduction in the level of safety.

Therefore, the design change and change to the TS will not result in a significant decrease in the level of safety.

As demonstrated above, this exemption request satisfies NRC requirements for an exemption to the design certification rule for the AP1000.

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B.8) CONTAINMENT COOLING CHANGES IN REGARD TO PASSIVE CORE COOLING
SYSTEM CONDENSATE RETURN

Applicable Regulation(s): 10 CFR Part 52 Appendix D, Section III.B

Specific wording from which exemption is requested:

“III. Scope and Contents

- B. An applicant or licensee referencing this appendix, in accordance with Section IV of this appendix, shall incorporate by reference and comply with the requirements of this appendix, including Tier 1, Tier 2 (including the investment protection short-term availability controls in Section 16.3 of the DCD), and the generic TS except as otherwise provided in this appendix. Conceptual design information in the generic DCD and the evaluation of severe accident mitigation design alternatives in appendix 1B of the generic DCD are not part of this appendix.”

Pursuant to 10 CFR § 52.63(b)(1), an exemption from elements of the design as certified in the 10 CFR Part 52, Appendix D, design certification rule is requested for plant-specific Tier 1 material departures from the AP1000 DCD for Tier 1 information and for a material departure from the generic Technical Specifications. These material departures are contained in Tier 1 Subsection 2.2.3, Tables 2.2.3-1 and 2.2.3-2, and involve the addition of components to the condensate return design to enable the Passive Core Cooling System to more effectively perform its design functions. The material departures also include a change to Technical Specifications Surveillance Requirement 3.5.4.7 which involves adding the downspout screens. This exemption request is in accordance with the provisions of 10 CFR § 50.12, 10 CFR § 52.7, and 10 CFR Part 52, Appendix D.

Discussion:

The changes requested to Tier 1 Table 2.2.3-1 and Table 2.2.3-2 and associated Tier 2 changes to Subsections 1.9.4.2.2 and 1.9.5.1.5, Table 3.2-3, Figure 3.8.2-1, Subsections 5.4.5.2.1, 5.4.11.2 and 5.4.14.1, Subsections 6.3.1.1.1, 6.3.1.1.4, 6.3.1.1.6, 6.3.1.2, 6.3.1.3, 6.3.2.1, 6.3.2.1.1, 6.3.2.2.5, 6.3.2.2.7, 6.3.2.8, 6.3.3, and 6.3.3.2.1.1 and Figures 6.3-1 and 6.3-2, Section 7.4, Subsection 7.4.1.1, Table 14.3-2, Subsections 15.0.3 and 15.2, Technical Specifications Surveillance Requirement 3.5.4.7, Technical Specifications Bases B 3.3.3 and B 3.5.4, Subsections 19E.2.3.2.6 and 19E.4.10.2, Table 19E.4.10-1, and Figures 19E.4.10-1 through 19E.4.10-4 provide additional equipment and surveillance requirements, provide reasonable assurance that the facility has been constructed and will be operated in conformity with the applicable design criteria, codes and standards, and demonstrate acceptable Passive Core Cooling System (PXS) system performance during design basis scenarios.

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Conclusion:

This exemption request is evaluated in accordance with 10 CFR Part 52, Appendix D, Section VIII.A.4, 10 CFR § 50.12, 10 CFR § 52.7 and 10 CFR § 52.63, which state that the NRC may grant exemptions from the requirements of the regulations provided the following six conditions are met: 1) the exemption is authorized by law [§ 50.12(a)(1)]; 2) the exemption will not present an undue risk to the health and safety of the public [§ 50.12(a)(1)]; 3) the exemption is consistent with the common defense and security [§ 50.12(a)(1)]; 4) special circumstances are present [§ 50.12(a)(2)]; 5) the special circumstances outweigh any decrease in safety that may result from the reduction in standardization caused by the exemption [§ 52.63(b)(1)]; and 6) the design change will not result in a significant decrease in the level of safety [Part 52, Appendix D, VIII.A.1]. The requested exemption satisfies the criteria for granting specific exemptions, as described below.

1. This exemption is authorized by law

The NRC has authority under 10 CFR §§ 50.12, 52.7, and 52.63 to grant exemptions from the requirements of NRC regulations. Specifically, 10 CFR §§ 50.12 and 52.7 state that the NRC may grant exemptions from the requirements of 10 CFR Part 52 with proper justification. No law exists that would preclude the changes covered by this exemption request. Additionally, granting of the proposed exemption does not result in a violation of the Atomic Energy Act of 1954, as amended, or the Commission's regulations.

Accordingly, this requested exemption is "authorized by law," as required by 10 CFR § 50.12(a)(1).

2. This exemption will not present an undue risk to the health and safety of the public

The proposed exemption from the requirements of 10 CFR 52, Appendix D, Section III.B would allow changes to elements of the plant-specific Tier 1 DCD to depart from the AP1000 certified (Tier 1) design information and a change to a Technical Specifications Surveillance Requirement to depart from the AP1000 certified (Tier 2) information. The plant-specific Tier 1 DCD will continue to reflect the approved licensing basis for the applicant, and will maintain a consistent level of detail with that which is currently provided elsewhere in Tier 1 of the plant-specific DCD. Because the change to the condensate return portion of the passive core cooling system description maintains its design functions, the changed design will ensure the protection of the health and safety of the public. Therefore, no adverse safety impact which would present any additional risk to the health and safety is present. The affected Design Description in the plant-specific Tier 1 DCD will continue to provide the detail necessary to support the performance of the associated ITAAC.

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Therefore, the requested exemption from 10 CFR 52, Appendix D, Section III.B would not present an undue risk to the health and safety of the public.

3. The exemption is consistent with the common defense and security

The exemption from the requirements of 10 CFR 52, Appendix D, Section III.B would change elements of the plant-specific Tier 1 DCD by departing from the AP1000 certified (Tier 1) design information relating to the condensate return portion of the passive core cooling system and departing from the Tier 2 generic Technical Specifications to include surveillance of added plant equipment. The exemption does not alter the design, function, or operation of any structures or plant equipment that are necessary to maintain a safe and secure status of the plant. The proposed exemption has no impact on plant security or safeguards procedures.

Therefore, the requested exemption is consistent with the common defense and security.

4. Special circumstances are present

10 CFR § 50.12(a)(2) lists six “special circumstances” for which an exemption may be granted. Pursuant to the regulation, it is necessary for one of these special circumstances to be present in order for the NRC to consider granting an exemption request. The requested exemption meets the special circumstances of 10 CFR § 50.12(a)(2)(ii). That Subsection defines special circumstances as when “Application of the regulation in the particular circumstances would not serve the underlying purpose of the rule or is not necessary to achieve the underlying purpose of the rule.”

The rule under consideration in this request for exemption from Tier 1 Subsection 2.2.3, Tables 2.2.3-1 and 2.2.3-2, and the Tier 2 generic Technical Specifications is 10 CFR 52, Appendix D, Section III.B, which requires that an applicant referencing the AP1000 Design Certification Rule (10 CFR Part 52, Appendix D) shall incorporate by reference and comply with the requirements of Appendix D, including Tier 1 information and generic Technical Specifications. The Turkey Point Units 6 and 7 COLA references the AP1000 Design Certification Rule and incorporates by reference the requirements of 10 CFR Part 52, Appendix D, including Tier 1 information and generic Technical Specifications. The underlying purpose of Appendix D, Section III.B is to describe and define the scope and contents of the AP1000 design certification, and to require compliance with the design certification information in Appendix D to maintain the level of safety in the design.

The proposed changes to the condensate return portion of the passive core cooling system maintain the design margins of the Passive Core Cooling System. This change does not impact the ability of any structures, systems, or components to perform their functions or

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negatively impact safety. Accordingly, this exemption from the certification information in Tier 1 Subsection 2.2.3, Tables 2.2.3-1 and 2.2.3-2, and Technical Specifications Surveillance Requirement 3.5.4.7 will enable the applicant to safely construct and operate the AP1000 facility consistent with the design certified by the NRC in 10 CFR 52, Appendix D.

Therefore, special circumstances are present, because application of the current generic certified design information in Tier 1 and the generic Technical Specification as required by 10 CFR Part 52, Appendix D, Section III.B, in the particular circumstances discussed in this request is not necessary to achieve the underlying purpose of the rule.

5. The special circumstances outweigh any decrease in safety that may result from the reduction in standardization caused by the exemption

Based on the nature of the changes to the plant-specific Tier 1 information and Tier 2 generic Technical Specifications and the understanding that these changes support the design function of the Passive Core Cooling System, it is likely that other AP1000 applicants and licensees will request this exemption. However, if this is not the case, the special circumstances continue to outweigh any decrease in safety from the reduction in standardization because the key design functions of the Passive Core Cooling System associated with this request will continue to be maintained. This exemption request and the associated marked-up tables and Technical Specifications Surveillance Requirements demonstrate that the Passive Core Cooling System function continues to be maintained following implementation of the change from the generic AP1000 DCD, thereby minimizing the safety impact resulting from any reduction in standardization.

Therefore, the special circumstances associated with the requested exemption outweigh any decrease in safety that may result from the reduction in standardization caused by the exemption. In fact, as described in Condition 6 below, the exemption will result in no reduction in the level of safety.

6. The design change will not result in a significant decrease in the level of safety

The exemption revises the plant-specific DCD Tier 1 information by adding components to Subsection 2.2.3, Tables 2.2.3-1 and 2.2.3-2, which were added to the condensate return design to enable the Passive Core Cooling System to more effectively perform its design functions. This exemption also revises the generic Technical Specifications Surveillance Requirement 3.5.4.7 to add the downspout screens to the surveillance. Because the Passive Core Cooling System design functions are met, there is no reduction in the level of safety.

Therefore, the design change and associated change to the Technical Specifications will not result in a significant decrease in the level of safety.

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As demonstrated above, this exemption request satisfies NRC requirements for an exemption to the design certification rule for the AP1000.

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B.9) MAIN CONTROL ROOM DOSE

Applicable Regulation(s): 10 CFR Part 52, Appendix D, Section III.B

Specific wording from which exemption is requested:

“III. Scope and Contents

- B. An applicant or licensee referencing this appendix, in accordance with Section IV of this appendix, shall incorporate by reference and comply with the requirements of this appendix, including Tier 1, Tier 2 (including the investment protection short-term availability controls in Section 16.3 of the DCD), and the generic TS except as otherwise provided in this appendix. Conceptual design information in the generic DCD and the evaluation of severe accident mitigation design alternatives in appendix 1B of the generic DCD are not part of this appendix.”

Pursuant to 10 CFR § 52.63(b)(1), an exemption from elements of the design as certified in the 10 CFR Part 52, Appendix D, design certification rule is requested for plant-specific Tier 1 departures from the AP1000 DCD for Tier 1 information and for a material departure from the generic TS. The Tier 1 departures are contained in Tier 1 Subsection 2.7.1 involving the revision of main control room emergency habitability system (VES) actuation signal name, and Tier 1 Subsection 2.2.5, Tier 1 Tables 2.2.5-1 and 2.2.5-5 involving the addition of VES filter shielding. The departures also include a change to TS LCO 3.7.4 and TS SR 3.7.4.1 which involves lowering allowable secondary iodine activity. This exemption request is in accordance with the provisions of 10 CFR § 50.12, 10 CFR § 52.7, and 10 CFR Part 52, Appendix D.

Discussion:

The changes requested to Tier 1 Subsections 2.7.1 and 2.2.5, Tier 1 Tables 2.2.5-1 and 2.2.5-5, TS LCO 3.7.4 and TS SR 3.7.4.1 provide reasonable assurance that the facility has been constructed and will be operated in conformity with the applicable design criteria, codes and standards, and demonstrate acceptable main control room operator dose during design basis scenarios.

Conclusion:

This exemption request is evaluated in accordance with 10 CFR Part 52, Appendix D, Section VIII.A.4, 10 CFR § 50.12, 10 CFR § 52.7 and 10 CFR § 52.63, which state that the NRC may grant exemptions from the requirements of the regulations provided the following six conditions are met: 1) the exemption is authorized by law [§ 50.12(a)(1)]; 2) the exemption will not present an undue risk to the health and safety of the public [§ 50.12(a)(1)]; 3) the exemption is consistent with the common defense and security [§ 50.12(a)(1)]; 4) special circumstances are

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present [§ 50.12(a)(2)]; 5) the special circumstances outweigh any decrease in safety that may result from the reduction in standardization caused by the exemption [§ 52.63(b)(1)]; and 6) the design change will not result in a significant decrease in the level of safety [Part 52, Appendix D, VIII.A.1]. The requested exemption satisfies the criteria for granting specific exemptions, as described below.

1. This exemption is authorized by law

The NRC has authority under 10 CFR §§ 50.12, 52.7, and 52.63 to grant exemptions from the requirements of NRC regulations. Specifically, 10 CFR §§ 50.12 and 52.7 state that the NRC may grant exemptions from the requirements of 10 CFR Part 52 upon a proper showing. No law exists that would preclude the changes covered by this exemption request. Additionally, granting of the proposed exemption does not result in a violation of the Atomic Energy Act of 1954, as amended, or the Commission's regulations.

Accordingly, this requested exemption is “authorized by law,” as required by 10 CFR § 50.12(a)(1).

2. This exemption will not present an undue risk to the health and safety of the public

The proposed exemption from the requirements of 10 CFR 52, Appendix D, Section III.B would allow changes to elements of the plant-specific Tier 1 DCD to depart from the AP1000 certified (Tier 1) design information and a change to a TS LCO and SR to depart from the AP1000 certified (Tier 2) information. The plant-specific Tier 1 DCD will continue to reflect the approved licensing basis for the applicant, and will maintain a consistent level of detail with that which is currently provided elsewhere in Tier 1 of the plant-specific DCD. Because the change maintains the capability of the Main Control Room Emergency Habitability System and Nuclear Island Nonradioactive Ventilation System to perform their design functions, the changed design will ensure the protection of the health and safety of the public. Therefore, no adverse safety impact which would present any additional risk to the health and safety is present.

Therefore, the requested exemption from 10 CFR 52, Appendix D, Section III.B would not present an undue risk to the health and safety of the public.

3. The exemption is consistent with the common defense and security

The exemption from the requirements of 10 CFR 52, Appendix D, Section III.B would change elements of the plant-specific Tier 1 DCD by departing from the AP1000 certified (Tier 1) design information relating to the Nuclear Island Nonradioactive Ventilation System and VES shielding and by departing from the generic TS to lower the allowable secondary iodine

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activity. The exemption does not alter the design, function, or operation of any structures or plant equipment that are necessary to maintain a safe and secure status of the plant. The proposed exemption has no impact on plant security or safeguards procedures.

Therefore, the requested exemption is consistent with the common defense and security.

4. Special circumstances are present

10 CFR § 50.12(a)(2) lists six “special circumstances” for which an exemption may be granted. Pursuant to the regulation, it is necessary for one of these special circumstances to be present in order for the NRC to consider granting an exemption request. The requested exemption meets the special circumstances of 10 CFR § 50.12(a)(2)(ii). That subsection defines special circumstances as when “Application of the regulation in the particular circumstances would not serve the underlying purpose of the rule or is not necessary to achieve the underlying purpose of the rule.”

The rule under consideration in this request for exemption from Tier 1 Subsections 2.7.1 and 2.2.5, Tier 1 Tables 2.2.5-1 and 2.2.5-5 and the generic TS is 10 CFR 52, Appendix D, Section III.B, which requires that an applicant referencing the AP1000 Design Certification Rule (10 CFR Part 52, Appendix D) shall incorporate by reference and comply with the requirements of Appendix D, including Tier 1 information and generic TS. The Turkey Point Units 6 & 7 COLA references the AP1000 Design Certification Rule and incorporates by reference the requirements of 10 CFR Part 52, Appendix D, including Tier 1 information and generic TS. The underlying purpose of Appendix D, Section III.B is to describe and define the scope and contents of the AP1000 design certification, and to require compliance with the design certification information in Appendix D to maintain the level of safety in the design.

The proposed change to the name of the actuation signal does not impact the design functions of the Nuclear Island Nonradioactive Ventilation System. The proposed change to add the VES shielding to the Tier 1 VES design description maintains the design functions of the VES. These changes do not impact the ability of any structures, systems, or components to perform their functions or negatively impact safety. Accordingly, this exemption from the certification information in Tier 1 Subsections 2.7.1 and 2.2.5, Tier 1 Tables 2.2.5-1 and 2.2.5-5, TS LCO 3.7.4 and TS SR 3.7.4.1 will enable the applicant to safely construct and operate the AP1000 facility consistent with the design certified by the NRC in 10 CFR 52, Appendix D.

Therefore, special circumstances are present, because application of the current generic certified design information in Tier 1 and the generic TS as required by 10 CFR Part 52, Appendix D, Section III.B, in the particular circumstances discussed in this request is not necessary to achieve the underlying purpose of the rule.

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5. The special circumstances outweigh any decrease in safety that may result from the reduction in standardization caused by the exemption

Based on the nature of the changes to the plant-specific Tier 1 information and generic TS and the understanding that these changes support the design function of the Main Control Room Emergency Habitability System and Nuclear Island Nonradioactive Ventilation System and establish limits for the specific activity in the secondary system, it is likely that other AP1000 applicants and licensees will request this exemption. However, if this is not the case, the special circumstances continue to outweigh any decrease in safety from the reduction in standardization because the key design functions of the Main Control Room Emergency Habitability System and Nuclear Island Nonradioactive Ventilation System associated with this request will be maintained with the implementation of these changes. This exemption request and the associated TS LCO and TS SR changes demonstrate that the Main Control Room Emergency Habitability System and Nuclear Island Nonradioactive Ventilation System functions continue to be maintained following implementation of the change from the generic AP1000 DCD, thereby minimizing the safety impact resulting from any reduction in standardization.

Therefore, the special circumstances associated with the requested exemption outweigh any decrease in safety that may result from the reduction in standardization caused by the exemption. In fact, as described in condition 6 below, the exemption will result in no reduction in the level of safety.

6. The design change will not result in a significant decrease in the level of safety

The exemption revises the plant-specific DCD Tier 1 information by adding a shielding design function to Subsection 2.2.5 and by changing the name of the actuation signal (High-2) for isolating the main control room penetrations in Subsection 2.7.1. This change does not alter the ability of the Main Control Room Emergency Habitability System or Nuclear Island Nonradioactive Ventilation System to maintain their design functions. This exemption also revises the generic TS LCO 3.7.4 and TS SR 3.7.4.1 to lower the allowable secondary iodine activity. Because these functions are met, there is no reduction in the level of safety.

Therefore, the design and TS changes will not result in a significant decrease in the level of safety.

As demonstrated above, this exemption request satisfies NRC requirements for an exemption to the design certification rule for the AP1000 design.

Table 5.0-1 Site Parameters	
Maximum Ground Water Level	Plant elevation 98 ft
Maximum Flood Level	Plant elevation 100 ft (design grade elevation)
Precipitation	
Rain	20.7 in/hr [1-hr 1-mi ² PMP]
Snow/Ice	Ground snow load of 75 lb/ft ² with exposure factor of 1.0 and importance factor of 1.2
Air Temperature	Limits based on historical data excluding peaks of less than 2 hours duration Maximum temperature of 115° dry bulb/86.1°F coincident wet bulb Maximum wet bulb 86.1°F (noncoincident) Minimum temperature of -40°F
Tornado	
Wind Speed	Maximum wind speed of 300 mph
Maximum Pressure Differential	Maximum pressure differential of 2.0 lb/in ²
Tornado Missile Spectra	4000-lb automobile at 105 mph horizontal, 74 mph vertical 275-lb, 8-in. shell at 105 mph horizontal, 74 mph vertical 1-in.-diameter steel ball at 105 mph in the most damaging direction
Soil	
Average Allowable Static Soil Bearing Capacity	The allowable bearing capacity, including a factor of safety appropriate for the design load combination, shall be greater than or equal to the average bearing demand of 8,900 lb/ft ² over the footprint of the nuclear island at its excavation depth.
Minimum Soil Angle of Internal Friction	The minimum soil angle of internal friction is greater than or equal to 35 degrees below the footprint of the nuclear island at its excavation depth. If the minimum soil angle of internal friction is below 35 degrees, a site-specific analysis shall be performed using the site-specific soil properties to demonstrate stability.
Dynamic Bearing Capacity for Normal Plus Safe Shutdown Earthquake (SSE)	The allowable bearing capacity, including a factor of safety appropriate for the design load combination, shall be greater than or equal to the maximum bearing demand of 35,000 lb/ft ² at the edge of the nuclear island at its excavation depth, or site-specific analyses demonstrate factor of safety appropriate for normal plus safe shutdown earthquake loads.

Table 2-1 (Sheet 1 of 4)	
SITE PARAMETERS	
Air Temperature	
Maximum Safety ^(a)	115°F dry bulb/86.1°F coincident wet bulb ^(g) 86.1°F wet bulb (noncoincident)
Minimum Safety ^(a)	-40°F
Maximum Normal ^(b)	101°F dry bulb/80.1°F coincident wet bulb 80.1°F wet bulb (noncoincident) ^(d)
Minimum Normal ^(b)	-10°F
Wind Speed	
Operating Basis	145 mph (3 second gust); importance factor 1.15 (safety), 1.0 (nonsafety); exposure C; topographic factor 1.0
Tornado	300 mph
Seismic	
CSDRS	0.30g peak ground acceleration ^{(c)(f)}
Fault Displacement Potential	No potential fault displacement considered beneath the seismic Category I and seismic Category II structures and immediate surrounding area. The immediate surrounding area includes the effective soil supporting media associated with the seismic Category I and seismic Category II structures.
Soil	
Average Allowable Static Bearing Capacity	The allowable bearing capacity, including a factor of safety appropriate for the design load combination, shall be greater than or equal to the average bearing demand of 8,900 lb/ft ² over the footprint of the nuclear island at its excavation depth.
Dynamic Bearing Capacity for Normal Plus SSE	The allowable bearing capacity, including a factor of safety appropriate for the design load combination, shall be greater than or equal to the maximum bearing demand of 35,000 lb/ft ² at the edge of the nuclear island at its excavation depth, or Site-specific analyses demonstrate factor of safety appropriate for normal plus safe shutdown earthquake loads.
Shear Wave Velocity	Greater than or equal to 1,000 ft/sec based on minimum low-strain soil properties over the footprint of the nuclear island at its excavation depth

UNITED STATES OF AMERICA
NUCLEAR REGULATORY COMMISSION

In the Matter of)
)
FLORIDA POWER & LIGHT COMPANY) Docket Nos. M-52-040 and 52-041-COL
(Juno Beach, Florida))
)
(Turkey Point, Units 6 & 7))

CERTIFICATE OF SERVICE

I hereby certify that copies of the foregoing **NOTICE TO THE PARTIES (Regarding Receipt of Communication)** have been served upon the following persons by Electronic Information Exchange.

U.S. Nuclear Regulatory Commission
Office of Commission Appellate Adjudication
Mail Stop: O-16B33
Washington, DC 20555-0001
ocaamail@nrc.gov

Florida Power & Light Company
700 Universe Blvd.
Juno Beach, Florida 33408
Nextera Energy Resources
William Blair, Esq.
william.blair@fpl.com

U.S. Nuclear Regulatory Commission
Office of the Secretary of the Commission
Mail Stop: O-16B33
Washington, DC 20555-0001
hearingdocket@nrc.gov

Florida Power & Light Company
801 Pennsylvania Ave. NW Suite 220
Washington, DC 20004
Steven C. Hamrick, Esq.
steven.hamrick@fpl.com

U.S. Nuclear Regulatory Commission
Office of the General Counsel
Mail Stop: O-15 D21
Washington, DC 20555-0001

Pillsbury, Winthrop, Shaw, Pittman, LLP
1200 Seventeenth Street, N.W.
Washington, DC 20036-3006

Patrick Moulding, Esq.
patrick.moulding@nrc.gov
Maxine R. Segamick, Esq.
Maxine.Segamick@nrc.gov
Robert Weisman, Esq.
robert.weisman@nrc.gov
Anthony C. Wilson, Esq.
anthony.wilson@nrc.gov
Megan Wright, Esq.
Megan.wright@nrc.gov
Susan Vrahoretis, Esq.
susan.vrahoretis@nrc.gov

Anne Leidich, Esq.
ann.leidich@pillsburylaw.com
David R. Lewis, Esq.
david.lewis@pillsburylaw.com
Michael G. Lepre, Esq.
michael.lepre@pillsburylaw.com
Timothy J. V. Walsh, Esq.
timothy.walsh@pillsburylaw.com

[Original signed by Clara Sola _____]
Office of the Secretary of the Commission

Dated at Rockville, Maryland,
this 15th day of February, 2018.