

# NY NIAGARA MOHAWK

NIAGARA MOHAWK POWER CORPORATION/300 ERIE BOULEVARD WEST, SYRACUSE, N.Y. 13202/TELEPHONE (315) 474-1511

December 13, 1978

Director of Nuclear Reactor Regulation  
Attention: Mr. Thomas Ippolito, Chief  
Operating Reactors Branch No. 3  
U. S. Regulatory Commission  
Washington, D. C. 20555

Re: Nine Mile Point Unit #1  
Docket No. 50-220 DPR-63  
Radwaste Reduction System

Gentlemen:

Niagara Mohawk Power Corporation plans to install a radwaste reduction system at Nine Mile Point Unit #1. This system was previously described in a letter to you dated September 1, 1978, with an attached report. A new radwaste building is being constructed to house improved equipment for normal waste solidification and handling operations. The construction of this building and installation of that equipment is not dependent upon installation of the radwaste reduction system. The solidification and handling system was described in a separate report dated November 30, 1978.

The advantage of the radwaste reduction system will be to decrease the amount of solid waste that is shipped to off-site burial grounds. This system is expected to reduce the volume by about ten to one. This will result in fewer shipments of radwaste, will extend the existing space at off-site burial grounds, and result in fewer radwaste containers. Increases in off-site doses during normal operation are expected to be insignificant.

This letter requests approval for the radwaste reduction system described in Attachment A pursuant to the requirements of 10CFR20.305.

An evaluation has been made by the Station Operation Review Committee and Safety Review and Audit Board relative to 10CFR50.59(a), and it was concluded that the radwaste reduction system does not involve an unreviewed safety question since:

- (1) The probability of occurrence or the consequences of an accident or malfunction of equipment important to safety previously evaluated in the Safety Analysis Report will not increase.

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- (2) The possibility for an accident or malfunction of a different type than any evaluated previously in the Safety Analysis Report will not be created.
- (3) The margin of safety as defined in the basis for any technical specification will not be reduced.

This modification does not affect any technical specifications.

Analyses have been performed assuming release, within the building, of the maximum amount of incinerated, but non-solidified radwaste on-hand. The results show that conservatively calculated doses to the public are well within regulatory requirements, such as outlined in 10CFR100. The building will be equal to or better than the existing radwaste building in terms of probability or consequences of failure. The building will be designed to the Class I seismic requirements described in the Final Safety Analysis Report.

The final product (incombustible residue) from the radwaste reduction system will be processed through a solidification and handling system into 55-gallon containers. The solidified product will be a solid cement matrix. In the event that the radwaste reduction system is not operating, any reason, the waste can go directly to solidification. The radwaste reduction and solidification and handling systems will be remotely operated.


Any spillage of liquid waste will be controlled by the floor drains in the building. There will be no increases in liquid waste effluents to the environment due to operation of the system. The equipment will be designed to the requirements outlined in Nuclear Regulatory Commission Branch Technical Position 11-1 (Revision 1).

Wastes processed by the radwaste reduction system will be no different from those previously described in the Final Safety Analysis Report. These wastes include:

- (1) Filter sludges
- (2) Deep bed and powdered demineralizer resins
- (3) Concentrated wastes
- (4) Filters, paper, wood, and other combustible materials which may have been radioactively contaminated.

Very truly yours,

NIAGARA MOHAWK POWER CORPORATION



Donald P. Dise  
Vice President - Engineering

LMM/kmb  
Attachment



ATTACHMENT A  
RADWASTE REDUCTION SYSTEM

I. Background

The radwaste reduction system for radwaste Volume reduction has been described in detail in the Licensing Topical Report.<sup>1</sup> The installation at Nine Mile Point Unit 1 will not vary significantly from the system described in the Licensing Topical Report.

As was stated in the Licensing Topical Report, the basic processes of liquid calcination and combustible waste incineration which are used in the radwaste reduction system have been used in industrial plants for decades. Fluidized bed calcination of radioactive waste was developed during the period 1952-1959 at the Idaho National Engineering Laboratory. Use of calcination for liquid radwaste reduction was first demonstrated in an engineering scale facility, the Waste Calcining Facility, at the Idaho Chemical Processing Plant in 1963. The successful operation of the waste calcining facility has demonstrated that liquid wastes can be routinely calcined into a granular free-flowing powder and can subsequently be handled in a simplified manner. Since 1963, the Waste Calcining Facility has handled over 2.5 million gallons of radioactive aqueous waste which have been calcined to approximately 42,500 cubic feet of solids.

Incineration of combustible radioactive wastes has been in use as a disposal technique since 1948 when a pilot plant incinerator and off-gas cleanup system were built at Mound Laboratory. Early systems were adaptations of standard refuse incinerators and did show that considerable volume reduction in waste handling was possible.

The radwaste reduction system is based on advanced fluidized bed technology using an inert bed medium to incinerate and calcine within a single-chamber process vessel. The purpose is to reduce the volume of the radwaste shipped offsite. Efficient volume reduction depends upon complete combustion and effective separation of gases and solids in the effluent gas stream. This separation takes place in the off-gas cleanup system. The high heat capacity of the fluidized bed gives high temperature stability and results in very efficient combustion. The air, which maintains the bed in its fluid state, provides an ample supply of oxygen for combustion.

Some wastes such as sludges and slurries do not have sufficient caloric content to maintain the bed at the desired temperature. In these cases, additional heat is provided by the combustion of supplemental fuel. The thermal inertia of the bed insures that the system is relatively insensitive to moderate variations and caloric content of the feed.

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1. Topical Report, Radwaste Volume Reduction System, EI/NNI-77-7-P, Newport News Industrial Corporation and Energy Incorporated, June 1977.



In the calcination mode, heat is used to drive off water as a vapor, leaving behind an incombustible residue. This incombustible residue is ground off the bed particles by the agitation of the bed. It exits from the process vessel to a dry cyclone. The calcination process is endothermic, and heat is supplied by the combustion of supplemental fuel. The use of special inert bed material means that the bed does not have to be changed when switching from incineration to calcination.

## II. System Description

The system consists of the process vessel, a dry cyclone, a product hopper, a wet scrubbing system and filtration system. Solids (ash or incombustible residue) are removed as the gas exits from the process vessel to the cyclone. Most of the solids are deposited in the dry cyclone; while the gases and remaining solids are scrubbed and treated by an offgas system. A product hopper collects the solids from the dry cyclone. Figure 1 shows the major components in a block flow diagram.

Process off-gas leaving the cyclone is cleaned by a wet scrubbing and filtration system. The wet scrubbing system is comprised of a spray quench tank, a high energy venturi scrubber followed by a wet cyclone, a condenser, and mist eliminator. Gaseous fission products (particulates and iodines) are removed by the scrub liquid and the filtration system. Particulate material is removed by the wet scrub system, and high efficiency particulate absolute filters. Cleaned off-gas is vented to the atmosphere (via the plant stack) while the product, a dry granular residue from the dry cyclone, is removed for solidification, storage and shipment. Scrub liquid will be processed through the liquid waste system. There are alternate routes for this liquid to be returned to the waste concentrator or to a day tank which feeds the radwaste reduction system.

The system is designed to operate at a negative pressure with respect to its surroundings, thereby providing further assurance that no leakage of radioactive material will occur. Continuous air monitors are intended to monitor the room air. Alarms will indicate locally high airborne activity in the unlikely event of leakage. In addition, ventilation air is routed to the main stack where all effluents are monitored prior to release.

The efficient treatment of the offgas cleanup system minimizes the release of gaseous effluents to the atmosphere. In case a portion of the offgas cleanup system should fail to clean adequately the radwaste reduction system has the capability of recirculating the offgas through the cleanup system instead of releasing it to the atmosphere. This action is initiated by the radiation monitor in the exhaust stream. There will be no liquid releases from the system directly to the environment. Scrub liquid returns to the liquid radwaste system as described above.

Appropriate instrumentation will be provided to detect conditions that may result in excessive radiation levels within the system. Controls designed to sense and activate an alarm upon the occurrence of





a wide variety of off-normal operating conditions will be included. A part of the controls will be an annunciator panel, which will provide identification of the causes of an alarm. Corrective action will be taken either automatically or manually, depending on the potential seriousness of the occurrence. Off-gas from the system is routed to the main stack. The stack monitoring system will monitor these releases. In addition a separate system radioactivity monitor will be located in the off-gas exhaust line to the plant stack. The incremental dose rates, as shown in Table 1 for normal operation, are well below the limits set in Appendix I to 10CFR50. The radioactive effluents produced by the system during normal operations will be so small that this addition to other effluents currently discharged from Nine Mile Point will have no significant environmental impact. Table 1 compares the maximum permissible concentrations from Table 2, column 1 of 10CFR20 Appendix B and the maximum average boundary concentrations resulting from radwaste reduction system operation. For all isotopes discharged, the maximum average concentration is well below the values of 10CFR20. The highest maximum nuclide (Cs-137) concentration is a factor of  $5 \times 10^6$  below its maximum permissible concentration.

The solid granular residue, or product, from the system will be packaged and transported to a licensed disposal site. In accordance with Regulatory Guide 1.21, provisions will be made to monitor the radiation from each package of solid waste. This will permit the operator to control radiation exposure to personnel and to meet the regulatory requirements of 10CFR71

### III. Analysis

The system as installed at Nine Mile Point Unit 1, will be in compliance with federal regulations concerning protection of personnel against radiation and other technical and legal licensing requirements. The system design results in very low radiation levels. The individual cubicles formed by the concrete shield walls, and the operation of the system at less than atmospheric pressure, will assure that the operational dose rate is below the levels required by 10CFR20 and are consistent with as low as reasonably achievable criterion. The emissions from normal operation of the system result in concentrations and dose rates at the site boundary, which are well below the limiting values of 10CFR20 for unrestricted areas. It may be noted that even if no credit is taken for any system cleanup (system decontamination factor is 40,000 from Table 1) the maximum permissible concentrations of 10CFR20 will not be exceeded. The highest isotopic concentration, that of Cs-137, would still be a factor of 130 below the 10CFR20 maximum permissible concentration for that isotope.

The normal release rates from this system have been computed, and are shown in Table 1, using the maximum activities and composition shown on Table 2 and the decontamination factors from Table 4-2 of the Licensing Topical Report. The dose factors are from Regulatory Guide 1.109; a breathing rate of 20 cubic meters/day has been used. The annual dose contributions are all less than 0.001 millirem.



Exposures from transient events and accidents have been discussed in Section 4.3 of the Licensing Topical Report. No additional coverage of transients will be presented here. None of the transient events have consequences which are more severe than the maximum credible accident. As in the Licensing Topical Report, the maximum credible accident for the Nine Mile Point Unit 1 radwaste reduction system is the gross failure of the product container.

The doses for this accident are presented in Table 3. These doses are conservative since it was assumed that only 90 percent of the activity was retained within the cubicle, the building and ventilation system combined. The building housing this system is a seismic Class I structure and the building ventilation discharges to the plant stack. In addition, the product container will also be located in a cubicle within the radwaste building. If the product container were to catastrophically fail, much of the material would be retained inside the cubicle. The amount escaping the cubicle would be drawn into the ventilation system. No credit is taken for ventilation system removal efficiency. However, the ventilation system will contain a high efficiency particulate filter having a design removal efficiency of 99.97 percent.

The capacity of the product container is equivalent to three 55-gallon drums (0.624 cubic meters), and it is conservatively calculated that 1,710 curies is the maximum credible activity that can be expected to accumulate in the product container. This is based on the maximum specific activity for filter sludge shipped and reported for any 6 months (68.5 curies/cubic meter). This occurred in the second half of 1975. The figure is felt to be conservative since specific activities were highest during this period. The specific activity of 68.5 curies/cubic meter has been multiplied by a factor of 2 to allow for variations within the 6 month period. Thus, it is assumed that enough feed is available at 137 curies/cubic meter to fill up the product container. The maximum volume reduction factor envisioned for waste other than dry, combustible solids is 20 to 1. The 1,710 curies is over two-thirds of the annual expected activity for resin/sludge. It is extremely unlikely that such a large portion of the activity in a year's waste would accumulate in such a small volume. The composition of the 1,710 curies is taken to be that given in the resin/sludge column of Table 2.

Despite the above, it is conservatively assumed that 10 percent of the granular ash (171 curies) in the product container escapes from the area containing this system and remains airborne long enough to reach the site boundary. The doses due to this release are shown in Table 3. The site boundary closest to Nine Mile Point Unit 1 is 1,500 meters in the southwest sector. The dilution factor,  $X/Q$ , is from Regulatory Guide 1.3 for an elevated (100 meter) release and fumigation conditions are assumed. The material was assumed to be released in the first four (4) hours. These assumptions are from the latest Regulatory Guides and are therefore different from the assumptions used in the Nine Mile Point Unit 1 Final Safety Analysis Report. The dose factors have been taken from Regulatory Guide 1.109, and the breathing rate was 20 cubic meters/day. The maximum dose was found to be 534 mrem to the lung. The maximum total body dose was found to be 141.5 mrem.



Effects due to construction of the radwaste volume reduction system will be minimal. The system will be placed in a building described in a separate report. Construction effects related to the building were considered in that report. Additional effects due to the installation of this system will be very minor. Some heavy equipment and a crane will be necessary for installation. Precautions will be taken in the movement of the equipment to prevent damage to safety related structures. Gaseous releases from the equipment will be kept below those allowable by state regulations.

#### IV. Conclusion

A report in accordance with the requirements of Section 102 C of the National Environmental Policy Act is not necessary. The releases from this system will not significantly effect the quality of the environment, as was stated in Sections II and III. Normal average releases will be a factor of  $5 \times 10^6$  below the amounts on Table II, Appendix B of 10CFR20 using conservative system decontamination factors. Taking no credit for any system decontamination factor would result in average releases that are a factor of 130 below Table II, Appendix B of 10CFR20. There are no other gaseous, liquid or other releases from this sytem that would constitute a significant effect on the quality of the environment.

Effects of construction will be minimal, as stated in Section III above. Precautions will be taken in the movement of heavy equipment or cranes to prevent damage to any safety related structures. Effects due to the construction of the building were considered in a separate report.



TABLE 1

ADDITIONAL EMISSION RATES, BOUNDARY CONCENTRATIONS, AND DOSE RATES  
DUE TO OPERATION OF THE RADWASTE REDUCTION SYSTEM

	Maximum Feed Rate (Ci/year)	Decontamination Factor	Release Rate (Ci/year)	Concentration(1) Limit (pCi/m <sup>3</sup> )	Maximum Boundary Concentration (pCi/m <sup>3</sup> )	Dose Rates		
						Thyroid	Lung (mrem/yr)	Total Body
NA-24	15	$4 \times 10^4$	$3.8 \times 10^{-4}$	5000	$6.7 \times 10^{-7}$	$8.3 \times 10^{-9}$	$8.3 \times 10^{-9}$	$8.3 \times 10^{-9}$
Mn-54	125	$4 \times 10^4$	$3.1 \times 10^{-3}$	1000	$5.5 \times 10^{-6}$	0.0	$7.0 \times 10^{-6}$	$3.2 \times 10^{-6}$
Co-60	915	$4 \times 10^4$	$2.3 \times 10^{-2}$	300	$4.0 \times 10^{-5}$	0.0	$2.2 \times 10^{-4}$	$5.5 \times 10^{-5}$
Sr-89	10	$4 \times 10^4$	$2.5 \times 10^{-4}$	300	$4.4 \times 10^{-7}$	0.0	$5.6 \times 10^{-7}$	$3.5 \times 10^{-7}$
I-131	50	$1 \times 10^4$	$5.0 \times 10^{-3}$	100	$8.8 \times 10^{-6}$	$9.6 \times 10^{-5}$	0.0	$1.7 \times 10^{-5}$
Cs-134	1225	$4 \times 10^4$	$3.06 \times 10^{-2}$	400	$5.4 \times 10^{-5}$	0.0	$4.8 \times 10^{-6}$	$3.6 \times 10^{-6}$
Cs-137	2160	$4 \times 10^4$	$5.4 \times 10^{-2}$	500	$9.5 \times 10^{-5}$	0.0	$6.6 \times 10^{-6}$	$3.7 \times 10^{-6}$
TOTAL	4500		$1.16 \times 10^{-1}$		$2.1 \times 10^{-4}$	$9.5 \times 10^{-5}$	$2.4 \times 10^{-4}$	$7.4 \times 10^{-5}$

(1) 10CFR20, Appendix B, Table II, Column 1.





TABLE 2

PROJECTED ACTIVITIES IN THE LIQUID AND RESIN/SLUDGE FEED  
TO THE RADWASTE REDUCTION SYSTEM FOR NINE MILE POINT UNIT ONE

	Liquid			Resin/Sludge		
	<u>(percent)</u>	<u>Expected (Ci/yr)</u>	<u>Maximum (Ci/yr)</u>	<u>(percent)</u>	<u>Expected (Ci/yr)</u>	<u>Maximum (Ci/yr)</u>
Na-24	1.5	9	15			
Mn-54	2	12	20	3	75	135
Co-60	11	66	110	23	575	805
Sr-89	1	6	10			
I-131	1.5	9	15	1	25	35
Cs-134	35	210	350	25	625	875
Cs-137	48	288	480	48	1200	1680
Total		600	1000		2500	3500



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TABLE 3

DOSES AT THE SITE BOUNDARY DUE TO THE MAXIMUM CREDIBLE ACCIDENT  
FOR THE NINE MILE POINT UNIT #1 RADWASTE REDUCTION SYSTEM

10% of the Ash Released

Organ Dose (mrem)

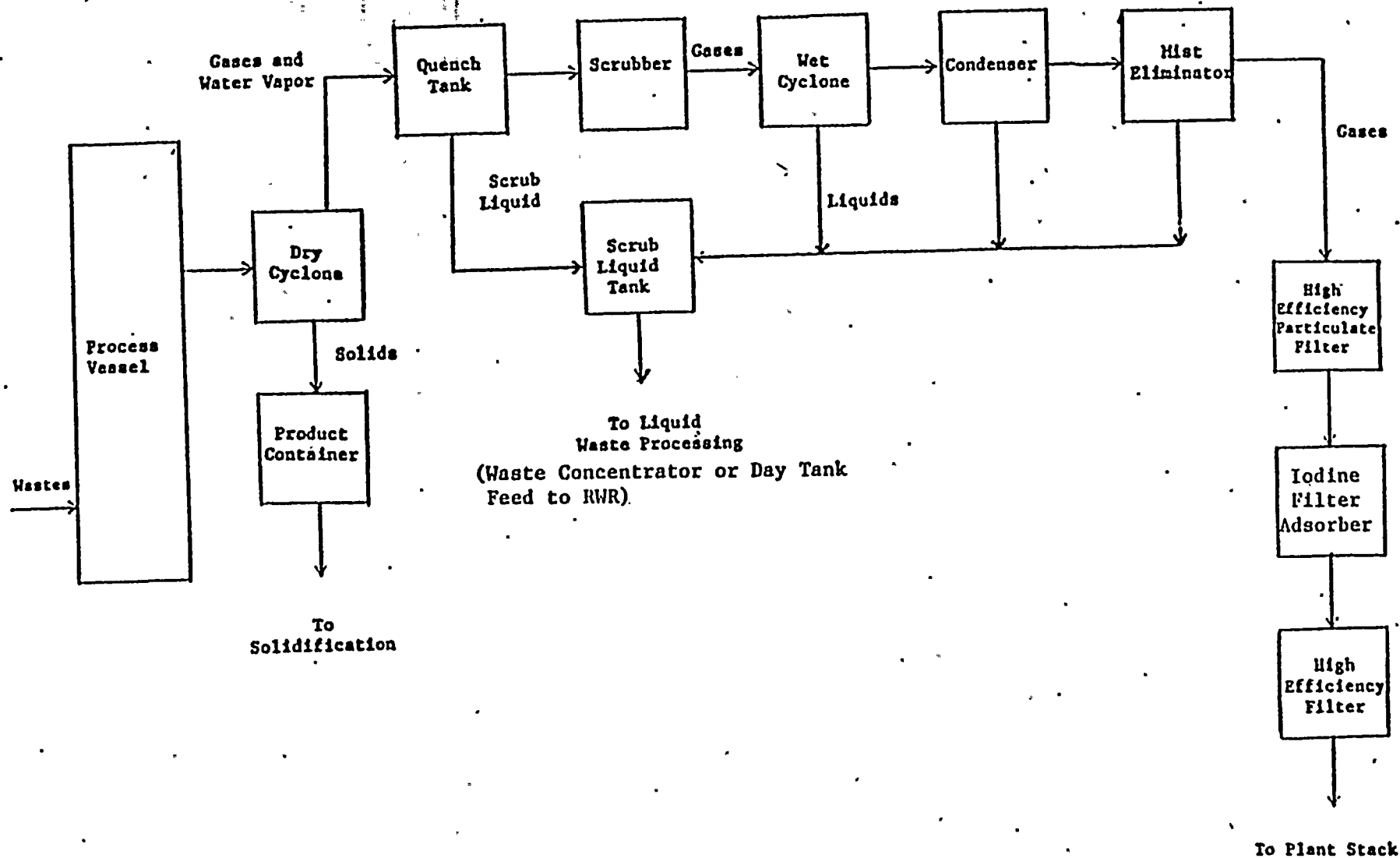
Nuclide	Bone	Liver	Thyroid	Kidney	Lung	Total Body
Mn- 54	0.0	0.4	0.0	0.1	15.3	0.1
Cr 59	0.0	1.0	0.0	0.0	496.5	1.2
	0.1	0.1	43.2	0.2	0.0	0.1
Cs-134	33.5	76.5	0.0	26.1	8.7	65.7
Cs-137	82.8	107.7	0.0	38.7	13.2	74.4
TOTAL	116.4	185.7	43.2	65.1	533.7	141.5



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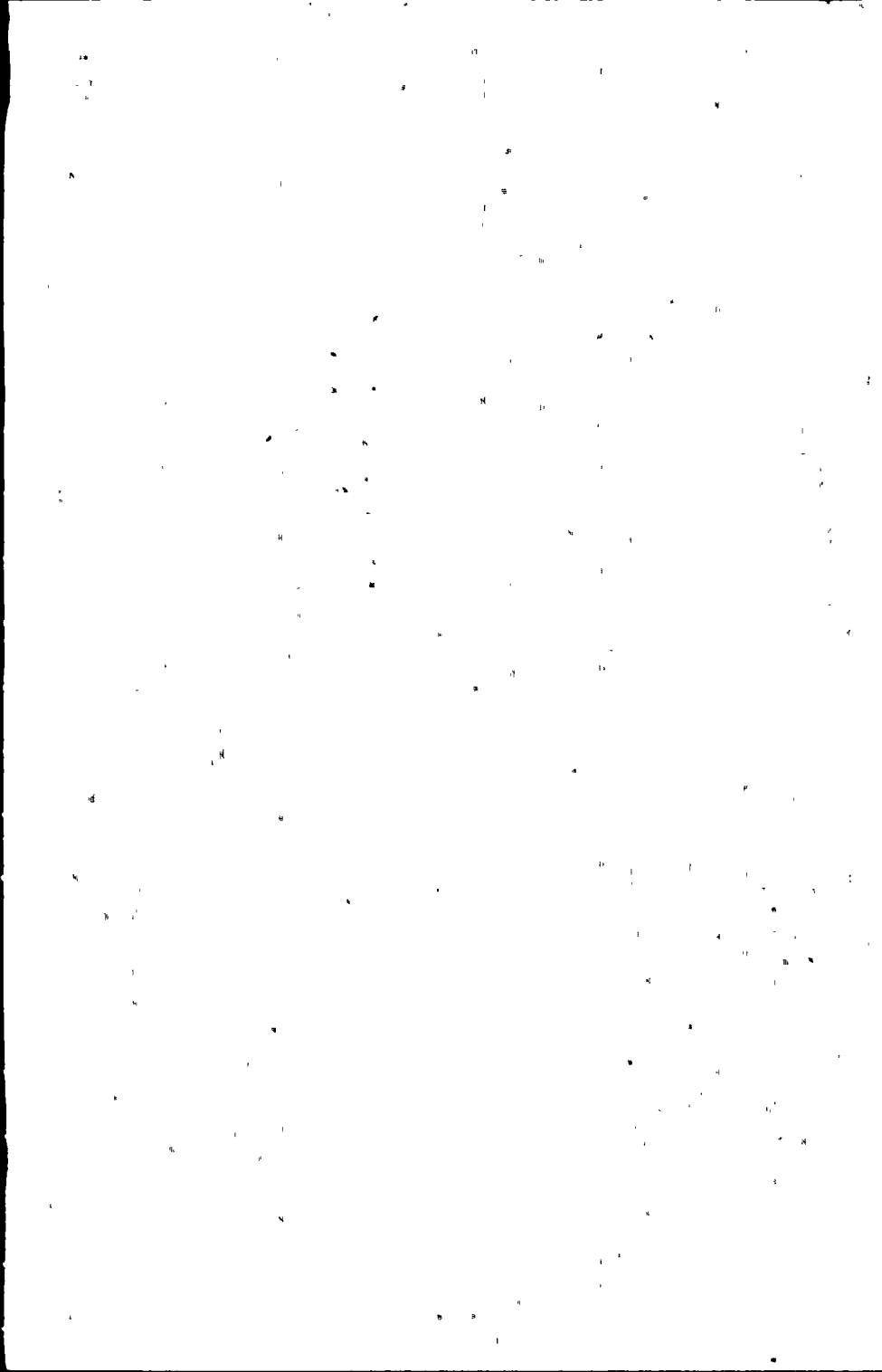
Radwaste Reduction Sys

Block Flow Diagram



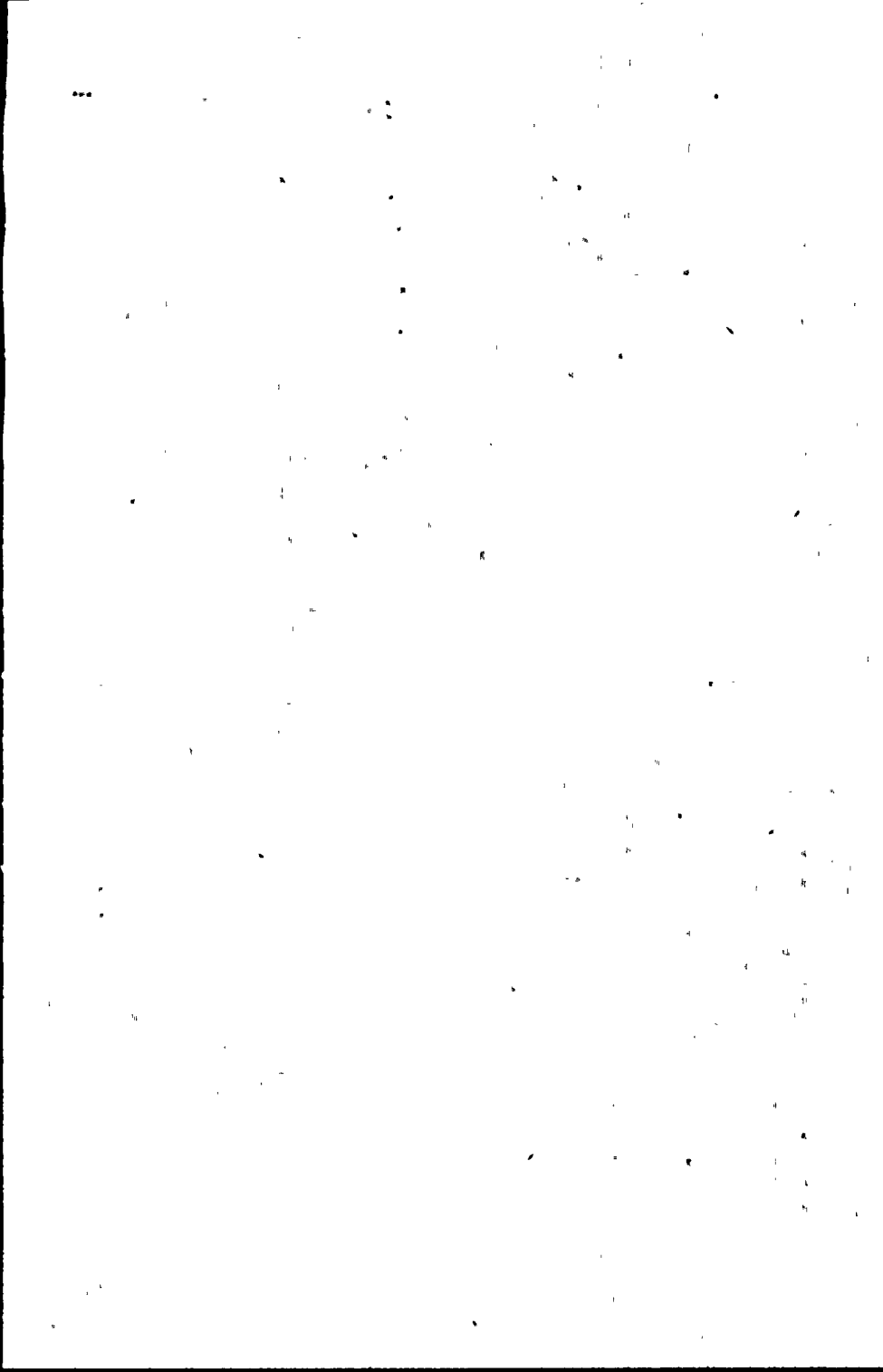


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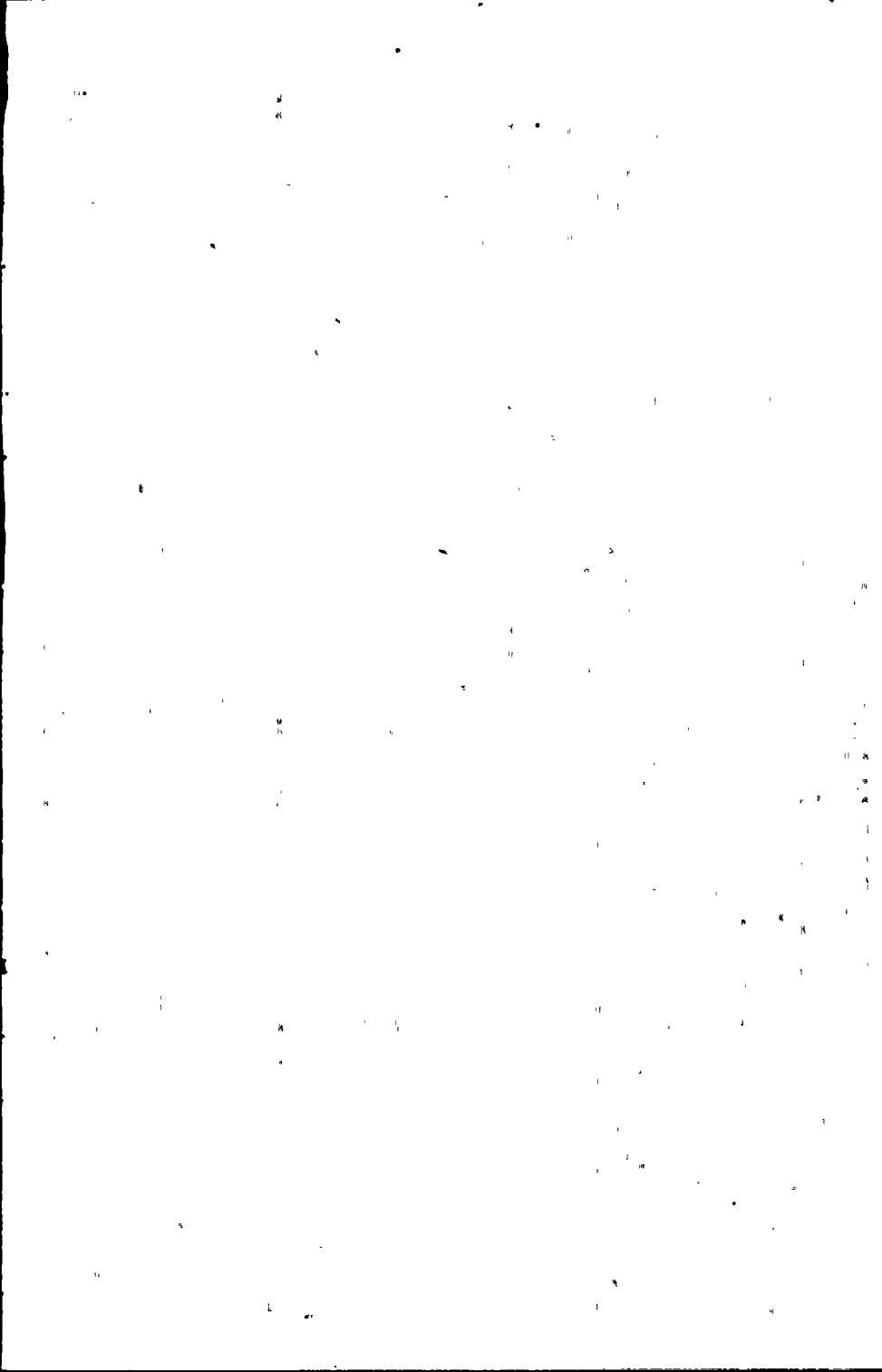




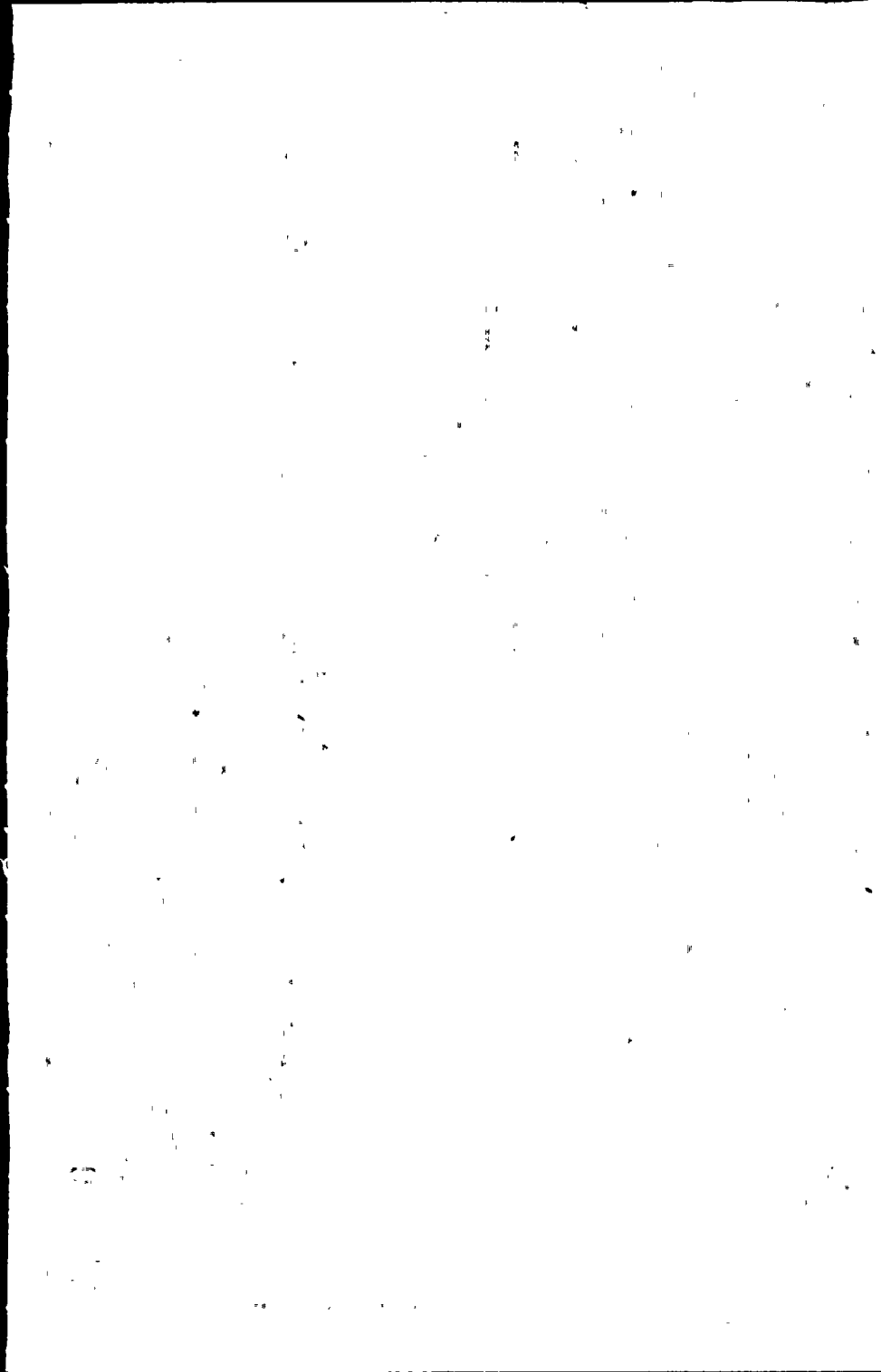
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				JCAE NOTIFICATION RECOMMENDED: <input type="checkbox"/> YES <input type="checkbox"/> NO			







No. ~~XXXXXXXXXXXX~~Logging Date 1/26/79

## NRC SECRETARIAT

TO: ☐ Commissioner \_\_\_\_\_ Date \_\_\_\_\_  
☒ Exec. Dir./Oper. \_\_\_\_\_ ☐ Gen. Counsel \_\_\_\_\_  
☐ Cong. Liaison \_\_\_\_\_ ☐ Solicitor \_\_\_\_\_  
☐ Public Affairs \_\_\_\_\_ ☐ Secretary \_\_\_\_\_  
☐ \_\_\_\_\_

Incoming: Richard Hermans, Chairperson  
 From: Safe Energy Coalition of New York  
State

To: Chairman Hendrie Date 1/22/79  
 Subject: Requests hearing and Env. Statement be  
prepared on proposed Nine-Mile Pt. low-level  
waste incinerator

☐ Prepare reply for signature of:

☐ Chairman

☐ Commissioner \_\_\_\_\_

☐ EDO, GC, CL, SOL, PA, SECY

☐ Signature block omitted

☐ \_\_\_\_\_

☐ Return original of incoming with response

Rec'd Off. EDO

Date 1/30/79  
 Time 10:30

~~XXXX~~ For direct reply ~~XXXXXXXXXXXX~~

☐ For appropriate action

Suspense; Feb. 5

☐ For information

☐ For recommendation

(See also SECY Tickets #~~XXX~~ 78-1587

78-1570

78-1801)

Remarks: Original to Docket.

For the Commission: Combs

\*Send three (3) copies of reply to Secy Mail Facility





No. 78-1801Logging Date 12/19/78

## NRC SECRETARIAT

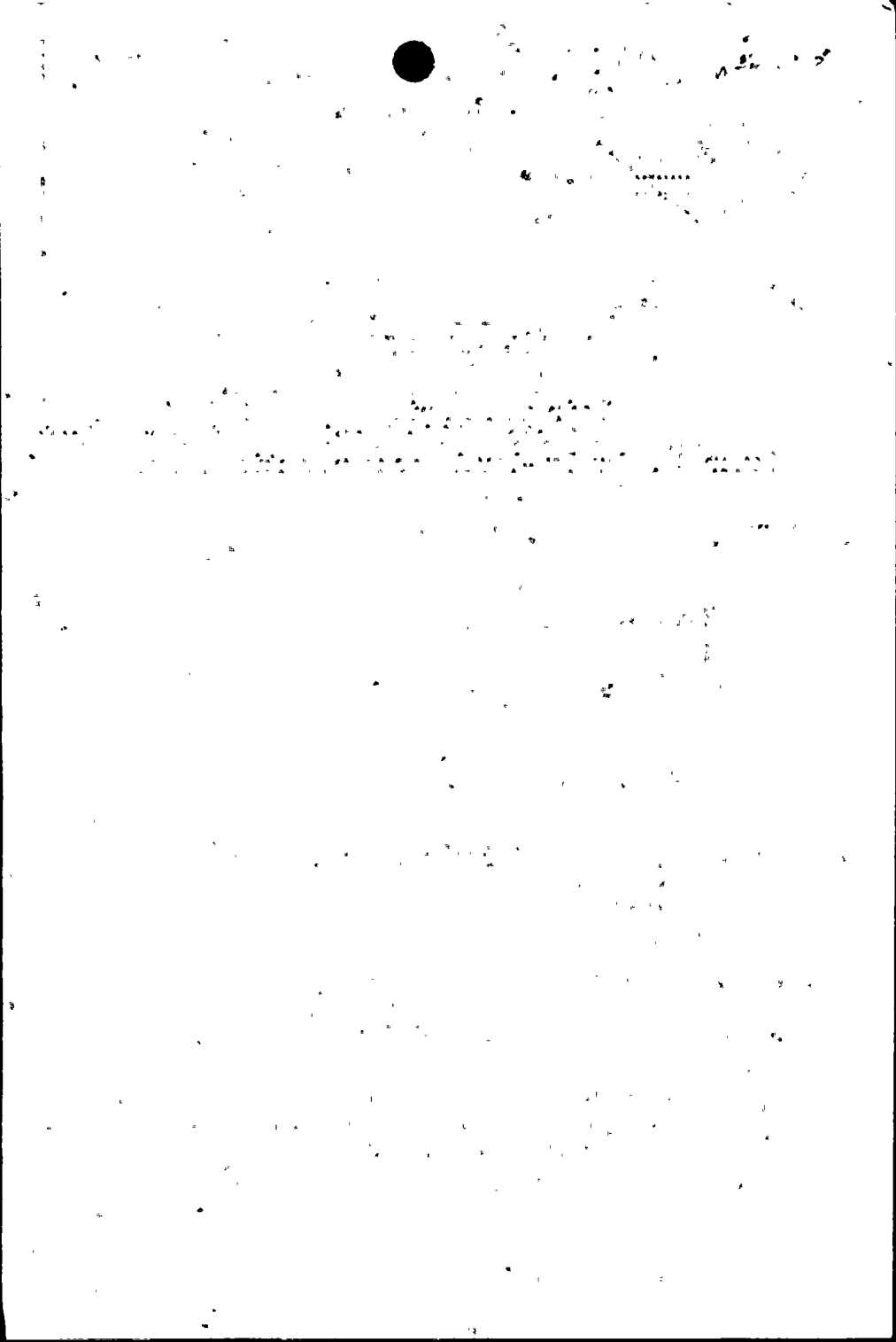
TO: ☐ Commissioner \_\_\_\_\_ Date \_\_\_\_\_  
☒ Exec. Dir./Oper. ☐ Gen. Counsel  
☐ Cong. Liaison ☐ Solicitor  
☐ Public Affairs ☐ Secretary  
☐ \_\_\_\_\_

Incoming: John R. Zagame, AssemblymanFrom: State of New YorkTo: Chairman Hendrie Date 12/12/78Subject: Requests public hearing on Niagara Mohawk  
Power Co. for low-level waste reduction system☒ Prepare reply for signature of:☐ Chairman☐ Commissioner \_\_\_\_\_☒ EDO, GC, CL, SOL, PA, SECY☐ Signature block omitted☐ \_\_\_\_\_☐ Return original of incoming with response☐ For direct reply\*

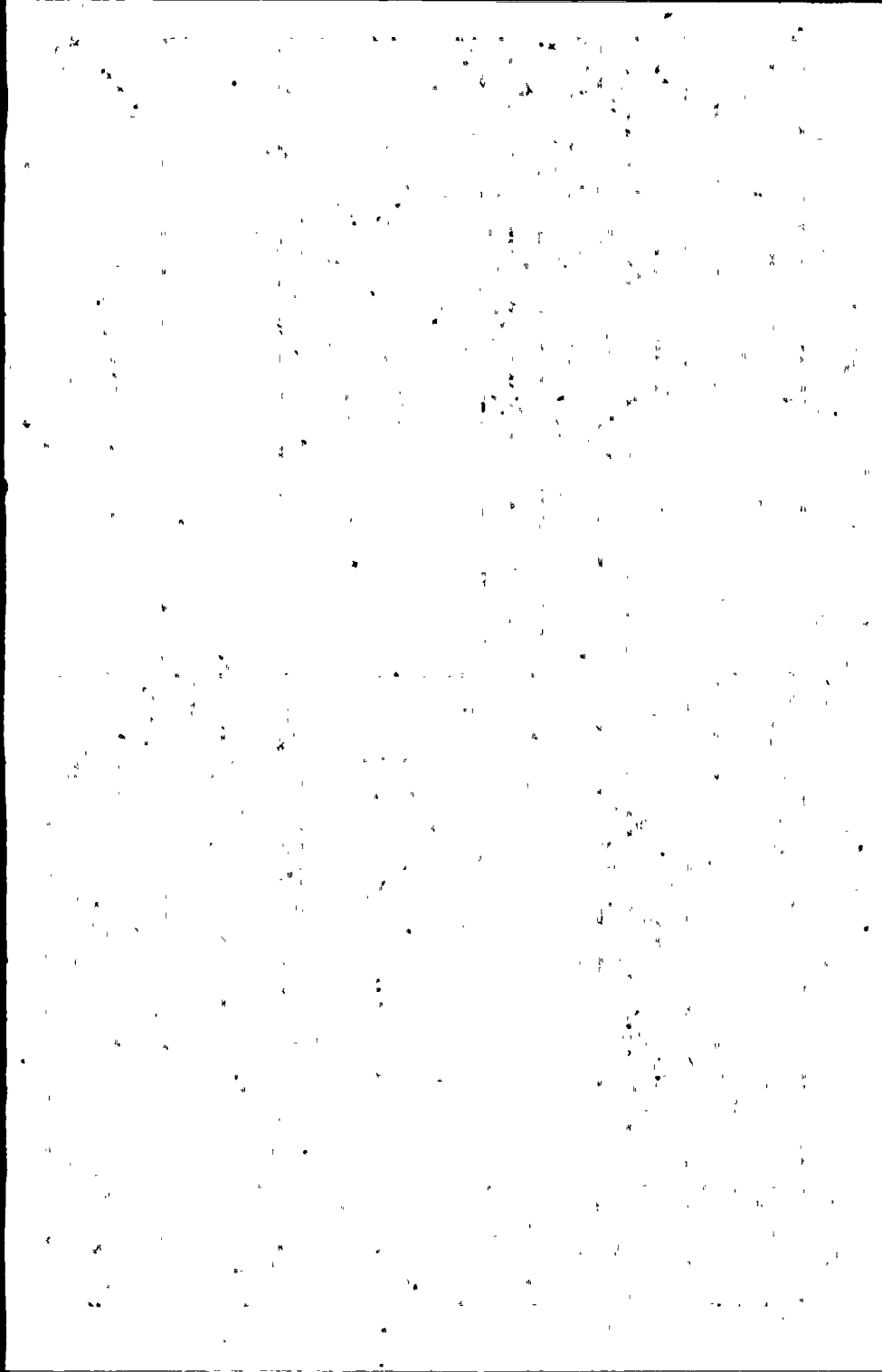
Suspense: Jan, 3

☐ For appropriate action☐ For information☐ For recommendationRemarks: Cpys to: RF. Original to DocketFor the Commission: Combs

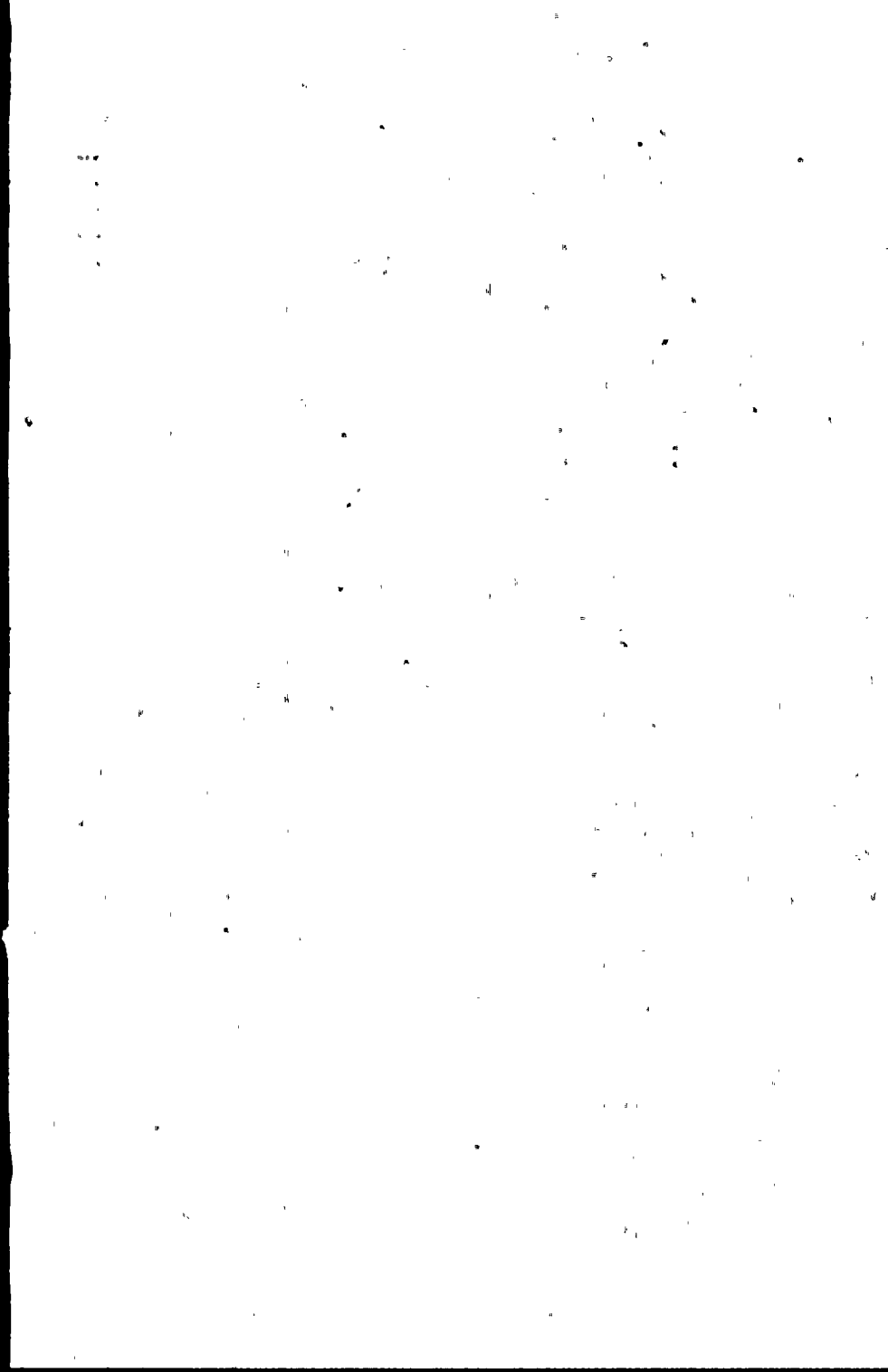
\*Send three (3) copies of reply to Secy Mail Facility







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Chairman Hendrie							
DESCRIPTION <input type="checkbox"/> LETTER <input type="checkbox"/> MEMO <input type="checkbox"/> REPORT <input type="checkbox"/> OTHER				SPECIAL INSTRUCTIONS OR REMARKS			
Supports the Oswego County Legislature request for full hearings on proposed construction of a low-level waste reduction system at Nine Mile 1				Incoming and reply to be put in PER simultaneously			
CLASSIFIED DATA							
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JCAE NOTIFICATION RECOMMENDED:				<input type="checkbox"/> YES <input type="checkbox"/> NO			

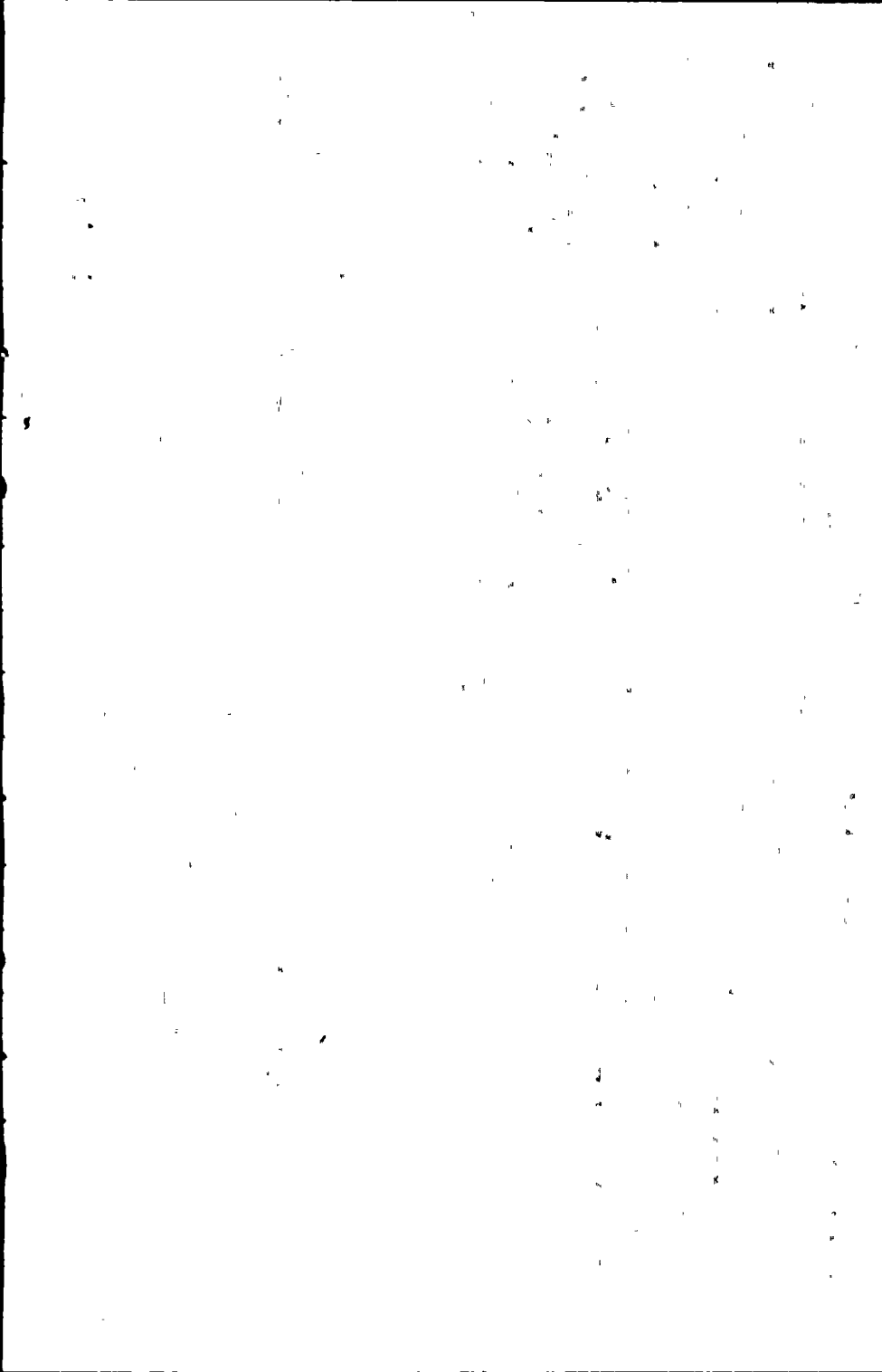




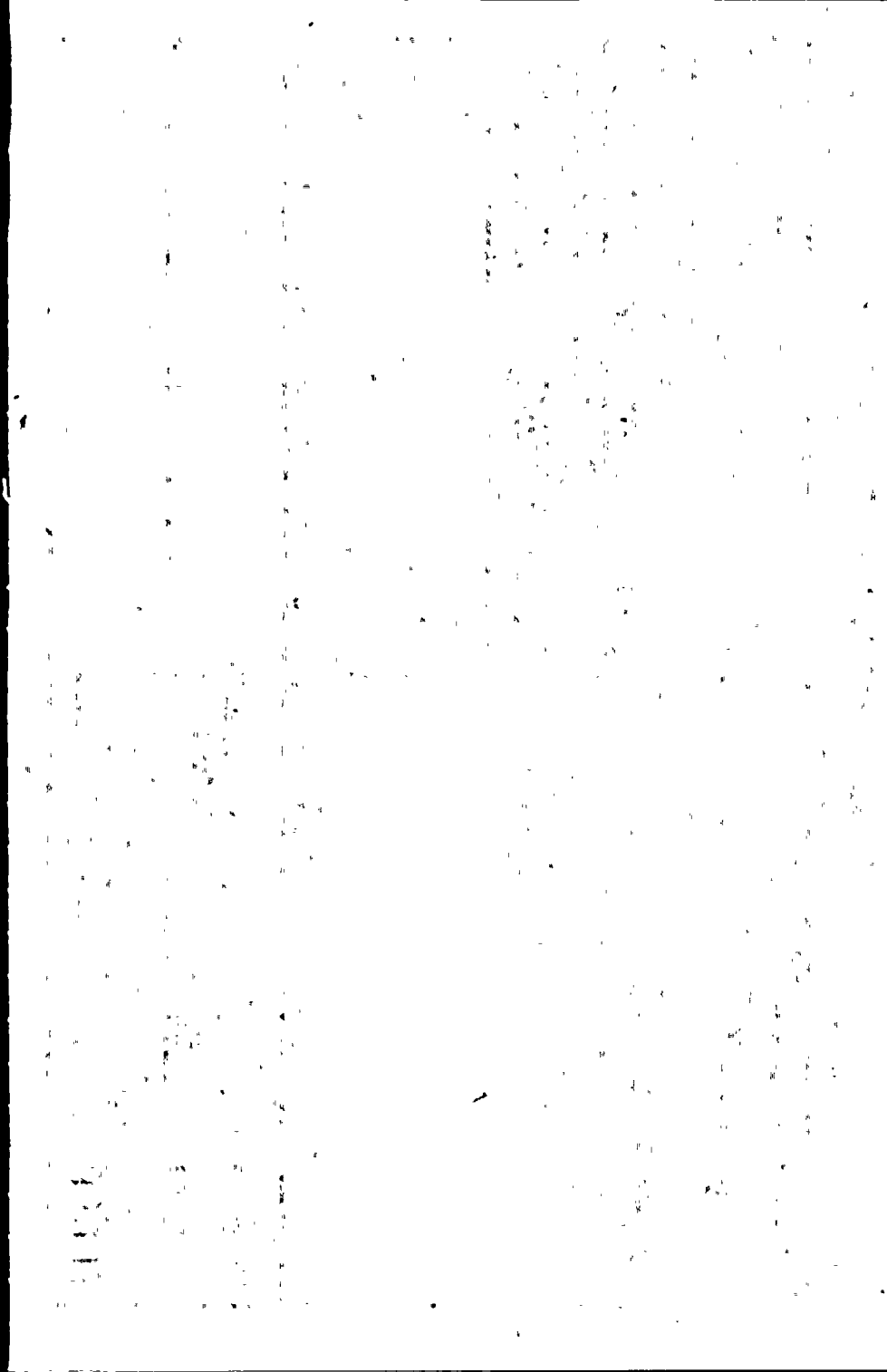




FROM:		ACTION CONTROL		DATES		CONTROL NO.	
John A. Zepeda, Assemblyman State of New York		COMPL DEADLINE		1/27/78		05091	
TO:		ACKNOWLEDGMENT				DATE OF DOCUMENT	
Executive Director		INTERIM REPLY				1/27/78	
		FINAL REPLY				PREPARE FOR SIGNATURE OF:	
		FILE LOCATION				<input type="checkbox"/> CHAIRMAN <input type="checkbox"/> EXECUTIVE DIRECTOR OTHER: <u>SECRET</u>	
DESCRIPTION <input type="checkbox"/> LETTER <input type="checkbox"/> MEMO <input type="checkbox"/> REPORT <input type="checkbox"/> OTHER				SPECIAL INSTRUCTIONS OR REMARKS			
Supports the Lewis County Legislature request for full hearings on proposed construction of a low-level waste reduction system at Elmira I.				Incoming and reply to be put to ECR simultaneously			
CLASSIFIED DATA							
DOCUMENT/COPY NO.				CLASSIFICATION			
NUMBER OF PAGES				CATEGORY			
POSTAL REGISTRY NO.				<input type="checkbox"/> NSI <input type="checkbox"/> RD <input type="checkbox"/> FRD		5637 72-1001	
ASSIGNED TO:		DATE		INFORMATION ROUTING		LEGAL REVIEW <input type="checkbox"/> FINAL <input type="checkbox"/> COPY	
5637-57		1/27/78		Deaton		ASSIGNED TO: DATE: NO LEGAL OBJECTIONS NOTIFY: <input type="checkbox"/> EDO ADMIN & CORRES BR EXT. COMMENTS, NOTIFY: EXT.	
JCAE NOTIFICATION RECOMMENDED:				<input type="checkbox"/> YES <input type="checkbox"/> NO			



<b>FROM:</b> John A. Zajano, Assemblyman State of New York		<b>ACTION CONTROL</b> COMPL DEADLINE <u>1/3/73</u> ACKNOWLEDGMENT INTERIM REPLY FINAL REPLY FILE LOCATION		<b>DATES</b> <b>CONTROL NO.</b> <span style="font-size: 1.5em;">05091</span> <b>DATE OF DOCUMENT</b> <span style="font-size: 1.2em;">12/12/72</span> <b>PREPARE FOR SIGNATURE OF:</b> <input type="checkbox"/> CHAIRMAN <input type="checkbox"/> EXECUTIVE DIRECTOR OTHER: <u>Singer</u>	
<b>TO:</b> Chairman Kerner					
<b>DESCRIPTION</b> <input type="checkbox"/> LETTER <input type="checkbox"/> MEMO <input type="checkbox"/> REPORT <input type="checkbox"/> OTHER Supports the Oswego County Legislature request for full hearings on proposed construction of a low-level waste reduction system at Mine Hill 1		<b>SPECIAL INSTRUCTIONS OR REMARKS</b> <div style="text-align: center; padding: 20px;">             Incoming and reply to be put in P.O. simultaneously           </div> <div style="text-align: center; padding: 20px;"> <b>SECY 72-1001</b> </div>			
<b>CLASSIFIED DATA</b>					
<b>DOCUMENT/COPY NO.</b> <b>NUMBER OF PAGES</b> <b>POSTAL REGISTRY NO.</b>		<b>CLASSIFICATION</b> <b>CATEGORY</b> <input type="checkbox"/> NSI <input type="checkbox"/> RD <input type="checkbox"/> FRD			
<b>ASSIGNED TO:</b> <u>Singer</u>		<b>DATE</b> <u>12/25/72</u>		<b>INFORMATION ROUTING</b> <u>Boston</u>	
_____ _____ _____ _____ _____		_____ _____ _____ _____ _____		<b>LEGAL REVIEW</b> <input type="checkbox"/> FINAL <input type="checkbox"/> COPY <b>ASSIGNED TO:</b> <b>DATE</b> _____ _____ _____ _____ _____	
				NO LEGAL OBJECTIONS NOTIFY: <input type="checkbox"/> EDO ADMIN & CORRES BR _____ EXT. _____ COMMENTS; NOTIFY: _____ EXT. _____	
<b>JCAE NOTIFICATION RECOMMENDED:</b>				<input type="checkbox"/> YES <input type="checkbox"/> NO	



USNRC

Sirs:

Please send me information on the request of Niagara Mohawk  
to install a low level radioactive waste incinerator at  
their Nine Mile point Nuclear Power plant.  
What is the Docket Number and may I send in a limited  
appearance statement?

Please send copies to Marvin I. Lewis.  
J. H. Johnsrud  
433 Orlando Av State College, PA

(814)

Marvin I. Lewis  
6504 Bradford Terrace  
Phila. PA 19149  
1-15-79.

~~(215) 377-7775~~  
~~(215) 375-0606~~

(215) CU 9 5968  
(215) 934 6685

Al and Eleanor Coleman  
d 35 K Dr Pennsville, N.J. 08070  
(609) 678-7125

