

LICENSEE EVENT REPORT (LER)

(See reverse for required number of
digits/characters for each block)

Estimated burden per response to comply with this mandatory information collection request: 50 hrs. Reported lessons learned are incorporated into the licensing process and fed back to industry. Forward comments regarding burden estimate to the Records Management Branch (T-6 F33), U.S. Nuclear Regulatory Commission, Washington, DC 20555-0001, and to the Paperwork Reduction Project (3150-0104), Office of Management and Budget, Washington, DC 20503. If an information collection does not display a currently valid OMB control number, the NRC may not conduct or sponsor, and a person is not required to respond to, the information collection.

FACILITY NAME (1)

TURKEY POINT UNIT 3

DOCKET NUMBER (2)

05000250

PAGE (3)

1 OF 6

TITLE (4)

Auxiliary Feedwater System Inoperable due to Inadequate Inservice Testing of Check Valves

EVENT DATE (5)			LER NUMBER (6)			REPORT DATE (7)			OTHER FACILITIES INVOLVED (8)	
MONTH	DAY	YEAR	YEAR	SEQUENTIAL NUMBER	REVISION NUMBER	MONTH	DAY	YEAR	FACILITY NAME	DOCKET NUMBER
6	19	1998	1998	003	00	07	15	1998	TURKEY POINT UNIT 4	05000251
OPERATING MODE (9)			THIS REPORT IS SUBMITTED PURSUANT TO THE REQUIREMENTS OF 10 CFR §: (Check one or more) (11)							
1			20.2201(b)		20.2203(a)(2)(v)		X		50.73(a)(2)(i)	50.73(a)(2)(viii)
POWER LEVEL (10)			20.2203(a)(1)		20.2203(a)(3)(i)				50.73(a)(2)(ii)	50.73(a)(2)(x)
100			20.2203(a)(2)(i)		20.2203(a)(3)(ii)				50.73(a)(2)(iii)	73.71
			20.2203(a)(2)(ii)		20.2203(a)(4)				50.73(a)(2)(iv)	OTHER
			20.2203(a)(2)(iii)		50.36(c)(1)				50.73(a)(2)(v)	Specify in Abstract below or in NRC Form 366A
			20.2203(a)(2)(iv)		50.36(c)(2)				50.73(a)(2)(vii)	

LICENSEE CONTACT FOR THIS LER (12)

NAME

CRAIG MOWREY - COMPLIANCE SPECIALIST

TELEPHONE NUMBER (Include Area Code)

305-246-6204

COMPLETE ONE LINE FOR EACH COMPONENT FAILURE DESCRIBED IN THIS REPORT (13)

CAUSE	SYSTEM	COMPONENT	MANUFACTURER	REPORTABLE TO EPX	CAUSE	SYSTEM	COMPONENT	MANUFACTURER	REPORTABLE TO EPX

SUPPLEMENTAL REPORT EXPECTED (14)

YES
(If yes, complete EXPECTED SUBMISSION DATE).

X NO

EXPECTED
SUBMISSION
DATE (15)

MONTH DAY YEAR

ABSTRACT (Limit to 1400 spaces, i.e., approximately 15 single-spaced typewritten lines) (16)

During a design review of the Auxiliary Feedwater (AFW) System, Florida Power and Light (FPL) determined that surveillance procedures did not require several check valves in the AFW system to pass the maximum required accident flow rate. The Turkey Point Design Basis Document stipulates a maximum required accident flow rate of 466.8 gpm, based on the required flow for a Loss of Offsite Power to both units. Since one AFW pump may be required to supply water to both units, each pump discharge check valve and each pump suction check valve from the Condensate Storage Tank must pass 466.8 gpm. The Train 2 AFW steam supply check valves must pass enough steam for the pumps to produce 466.8 gpm.

The cause of this condition was a misunderstanding in the AFW testing criteria of one unit demand (Technical Specification surveillance criteria) versus two unit demand (Inservice Test [IST] criteria for check valves). This misunderstanding led to inadequate IST surveillances beginning in October 1989.

FPL verified that all affected check valves are capable of passing 467 gpm. Procedures will be revised to increase the IST flow rate for the affected check valves to 467 gpm. FPL is reviewing check valves in the IST program for shared systems needed during postulated two unit events, to verify that the specified surveillance criteria bounds the maximum accident flow rate requirement.

9807210013 980715
PDR ADOCK 05000250
S PDR

12

LICENSEE EVENT REPORT (LER) TEXT CONTINUATION

FACILITY NAME	DOCKET NUMBER	LER NUMBER	PAGE NO.
TURKEY POINT UNIT 3	05000250	98-003-00	2 OF 6

I. DESCRIPTION OF THE EVENT

During a design review of the Auxiliary Feedwater (AFW) System [BA], Florida Power and Light (FPL) determined that the delivered flow requirement for one AFW pump [BA:p] is 466.8 gallons per minute (gpm), in accordance with the Turkey Point Design Basis Documents (DBDs). Contrary to this requirement, however, the surveillance procedures for the AFW pumps' discharge check valves (20-143, 20-243 and 23-343) [BA:v] require only 390 gpm to satisfy the ASME Section XI (OM-10) full-stroke requirement. If passing flow is the method used to verify full-stroke, the check valve must pass the maximum required accident flow rate, in accordance with the guidance in NRC Generic Letter 89-04 and in NUREG-1482, "Guidelines for Inservice Testing at Nuclear Power Plants."

System Description

Three steam turbine driven AFW pumps are provided for Turkey Point Units 3 and 4. The three pumps are installed such that each supplies auxiliary feedwater to either Unit 3 or 4, with any single pump supplying the total feedwater requirement of either unit. The A pump is aligned to AFW Train 1, the B pump is aligned to Train 2, and the C pump can be aligned to either train. The AFW pumps are supplied with steam from the unit which has lost its normal feedwater supply. The steam supply valves [BA:isv] will automatically open on any of several signals, e.g., Safety Injection, Low-Low Level in any of the three steam generators [SB:sg], loss of both feedwater pumps [SJ:p] under normal operating conditions, and bus stripping [EC:bu].

The AFW system is currently configured to respond to any automatic actuation signal as follows:

1. The steam supply valves to all available pumps begin to open on the signal
2. All available pumps start and all Flow Control Valves fully open, within 95 seconds of the signal
3. The Flow Control Valves [BA:fcv] throttle back to 130 gpm per steam generator within one to two minutes of the pump start

Reportable Condition

Present surveillance procedures ensure that system response is as described above. Steam generator flow is verified to be 130 ± 5 gpm after the AFW system stabilizes. FPL determined that surveillance procedures did not require the AFW pumps' discharge check valves to pass the maximum required accident flow rate. The Turkey Point Design Basis Document stipulates a maximum required accident flow rate of 466.8 gpm, based on the required flow for a Loss of Offsite Power to both units. Since one AFW pump may be required to supply water to both units, each pump's discharge check valve must be shown to pass at least 466.8 gpm to satisfy the ASME Section XI (OM-10) full-stroke requirement for Inservice Testing (IST). The maximum flow rate, which occurs prior to stabilization, has typically not been documented. Therefore, adequate documentation cannot be found to prove that IST acceptance criteria has been met. As a result, based on this inadequate IST surveillance, the AFW system was technically inoperable, dating from July 1990, when FPL committed to test these check valves using full flow testing, in response to Generic Letter 89-04. This condition is prohibited by Technical Specifications, and is therefore reportable under 10 CFR 50.73(a)(2)(i)(B).

Pump flow rate is used as the positive means to verify that the steam supply check valves are passing design steam flow. Therefore, the Train 2 steam supply check valves (AFSS-003B and AFSS-003C) for the B and C AFW pump turbines also require a pump flow rate of 467 gpm to verify full-stroke opening. Train 2 steam to the A AFW

LICENSEE EVENT REPORT (LER) TEXT CONTINUATION

FACILITY NAME	DOCKET NUMBER	LER NUMBER	PAGE NO.
TURKEY POINT UNIT 3	05000250	98-003-00	3 OF 6

pump is not an allowed configuration per the Technical Specifications, so AFSS-003A is not required to be tested. The Train 1 steam supply has two check valves in parallel, one from each unit. There are no Train 1 steam supply check valves that are common to both units. Therefore no Train 1 check valves need to be tested to the 467 gpm criterion.

During recent testing (5/4/98 to 6/16/98), plant personnel verified that each pump produced in excess of 480 gpm during testing, thus satisfying the maximum accident flow rate IST requirement for the pump discharge check valves and for the AFW steam supply check valves.

No documentation could be located to indicate that the AFW pump suction valves from the Condensate Storage Tank [KA:tk] (3-20-401 and 4-20-401) were tested to 467 gpm. Therefore on July 6, 1998, both trains of the AFW system were declared inoperable. Testing of these two valves was completed satisfactorily within the 24 hours allowed for a missed surveillance by Technical Specification 4.0.3, and the AFW trains were declared operable. The existing condition was prohibited by Technical Specifications, and is therefore reportable under 10 CFR 50.73(a)(2)(i)(B).

II. CAUSE OF THE EVENT

The root cause for this procedural difference in the surveillance versus required flow rates was cognitive personnel error by utility non-licensed personnel in 1990, specifically a misunderstanding in the AFW testing criteria of one unit demand (Technical Specification required flow rate) versus two unit demand (IST criteria for check valves). That is, AFW testing is performed by delivering flow to only one unit, however, for certain check valves in the AFW system this does not represent the maximum required accident flow rate, which corresponds to a two unit event. The flow control valve setting(s) must be adjusted from its preset flow demand for single unit response (125 gpm minimum per steam generator) to produce and document flow testing for a two unit flow requirement.

The auxiliary feedwater system flow requirements have been reevaluated several times at Turkey Point. In the early 1980s, AFW requirements were reevaluated as part of the Steam Generator Replacement project. These analyses established the limiting AFW flow for a single unit event to be 373 gpm for the Loss of Normal Feedwater transient (LONF). AFW flow for this single unit event was based on a three minute time delay for AFW flow initiation and on no loss of offsite power. This 373 gpm flow requirement was incorporated into the Technical Specification Surveillance in Technical Specification Amendment 90/84 in December 1982.

Additional analyses were subsequently performed for the non-LOCA accidents and submitted in 1987 to permit changing the AFW Technical Specifications to allow a 30 day allowed outage time on the third AFW pump. These analyses demonstrated that the for a single unit event the minimum required flow for a loss of main feedwater event (no loss of offsite power) is 315 gpm in three minutes. For a two unit event, it was assumed 125 gpm would be provided to the farthest unit hydraulically for ten minutes followed by balancing flow to the two units at 230 gpm per unit (460 gpm total flow for two units). While this change to the Technical Specifications was accepted by the NRC, no change to the surveillance requirement of 373 gpm for 15 minutes was made.

The AFW Technical Specifications were further revised in 1990 as part of the Technical Specification upgrade program to change from custom Technical Specifications to Standard Technical Specifications modeled after the Westinghouse Standard Technical Specifications (NUREG-0452, Revision 5 Draft). The 373 gpm flow

LICENSEE EVENT REPORT (LER) TEXT CONTINUATION

FACILITY NAME	DOCKET NUMBER	LER NUMBER	PAGE NO.
TURKEY POINT UNIT 3	05000250	98-003-00	4 OF 6

requirement was retained in the revised Technical Specifications, and is considered a general performance test requirement for the AFW system.

III. SAFETY CONSEQUENCES OF THE EVENT

DESCRIPTION OF TRANSIENTS REQUIRING AFW

Loss of Normal Feedwater (LONF)

Loss of main feedwater transients are only postulated to occur in a single unit whether in single or dual unit operation. They are characterized by a rapid reduction in steam generator water levels which results in a reactor trip, a turbine trip, and auxiliary feedwater actuation by the protection system logic [JC]. Following reactor trip from high power, the power quickly falls to decay heat levels. The water levels continue to decrease, progressively uncovering the steam generator tubes as decay heat is transferred and discharged in the form of steam either through the steam dump valves to the condenser, or through the steam generator safeties or atmospheric steam dump valves. The reactor coolant [AB] temperature increases as the residual heat in excess of that dissipated through the steam generators is absorbed. With increased temperature the volume of reactor coolant expands, filling the pressurizer and increasing reactor coolant system pressure.

Hence, the timely introduction of sufficient auxiliary feedwater is necessary to arrest the decrease in the steam generator water levels, to reverse the rise in reactor coolant temperature, to prevent the pressurizer [AB:pzr] from filling to a water solid condition, and eventually to establish stable hot standby conditions. Subsequently, a decision may be made to proceed with plant cooldown.

Loss of Offsite Power (LOOP)

This transient differs from a simple LONF in that both units will trip causing a dual unit demand for AFW. Emergency power sources [EK] must be relied upon to operate vital equipment. The loss of power to the electric driven condenser circulating water pumps [SG:p] results in loss of condenser vacuum and condenser steam dump capability. Hence, steam is relieved through the steam generator safety valves [SB:rv] or the atmospheric dump valves [SB:pcv]. The calculated transients for each unit are similar for both LONF and LOOP except that reactor coolant pump [AB:p] heat input to the Reactor Coolant System (RCS) is not a consideration for LOOP following loss of power to the reactor coolant pump bus. The limiting criterion for both is preventing the pressurizer from filling with water.

Small Break Loss of Coolant Accident (LOCA)

Small LOCAs are characterized by relatively slow rates of decrease in reactor coolant system pressure and liquid volume. The principal contribution from the AFW System following small LOCAs is to remove the decay heat and RCS sensible energy which is not removed by the break flow. This also augments the depressurization of the RCS and eventually allows cooldown to achieve hot shutdown.

GENERIC IMPLICATIONS

AFW check valves in the IST Program were reviewed for applicability. Only the seven valves discussed were determined to be impacted: the pumps' discharge check valves (20-143, -243, and -343), the AFW suction valves from the Condensate Storage Tank (3-0-401 and 4-20-401), and the Train 2 AFW pump steam supply valves (AFSS-003B and AFSS-003C). Per NUREG-1482, flow measurements of full-stroke check valve testing are not subject to instrument range and accuracy requirements.

LICENSEE EVENT REPORT (LER) TEXT CONTINUATION

FACILITY NAME	DOCKET NUMBER	LER NUMBER	PAGE NO.
TURKEY POINT UNIT 3	05000250	98-003-00	5 OF 6

Based on the root cause of the discrepancy (Maximum accident flow requirement is based on a two unit event, and testing is performed based on a one unit event.), there do not appear to be any other safety related fluid systems which are shared between the units and are required simultaneously by both units at Turkey Point. However, FPL will perform a general review of the IST program check valves for shared systems needed during postulated two unit events, to verify that the specified surveillance criteria bounds the maximum accident flow rate requirement.

SUMMARY

Updated Final Safety Analysis Report Section 14.1.12 Loss of Non-Emergency A-C Power to the Plant Auxiliaries, represents the limiting event for AFW. The worst single failure in the AFW system could result in the availability of only AFW pump supplying 233.4 gpm to one of the units (466.8 gpm total to both units) 95 seconds following a start signal on low-low steam generator level. This AFW flow is less (per unit) than that assumed for a loss of normal feedwater, because Turkey Point Units 3 and 4 have a shared AFW system and a LOOP may occur simultaneously on both units.

Technical Specifications 3.7.1.2 and 4.0.5 provide the operational and surveillance requirements for AFW. Two independent AFW trains including three AFW pumps and associated flow paths are required to be operable during Modes 1, 2, or 3. The AFW pumps and associated valves are demonstrated operable at least once per 31 days by verifying each steam turbine driven pump operates for at least 15 minutes and develops at least 373 gpm to the steam generators. The IST program tests the valves and pumps in the program in accordance with Technical Specification 4.0.5 and ASME Section XI requirements.

The AFW Design Basis Document (DBD) specifies an (original) design flow capability of 600 gpm for the pump discharge check valves (20-143, -243, -343). However, the DBD identifies that the maximum accident flow rate to the steam generators required by one AFW pump as 466.8 gpm (LOOP on two units).

Recent testing of the AFW pump discharge check valves confirms that greater than 390 gpm of flow passes through the check valve. The intent of the ASME Code and the Technical Specifications is that an AFW pump discharge check valve should be capable of passing sufficient flow to support a dual unit transient (466.8 gpm per AFW DBD's Section 4.3.1, for Loss of Offsite Power for Units 3 and 4). Documentation could not be found for all pumps that explicitly verified that greater than 467 gpm would be passed.

While explicit documentation could not be found, testing data shows that the system behavior is such that when AFW is started for testing, a single pump will provide flow to the flow control valves associated with that train and unit (one flow control valve/steam generator/train). The design of the system is such that each AFW flow control valve will go to its wide open position, and then will control flow to its set point of 130 gpm (390 gpm total). Recent test results reviewed have shown that flow initially overshoots the 130 gpm set point on each FCV by a wide margin (flow peaks are typically greater than 200 gpm), with flow then being controlled to the set point in the next one to two minutes. Based on the results reviewed, there is reasonable evidence to indicate that greater than 467 gpm has been achieved through each AFW pump and discharge check valve, and that the steam supply check valves have passed adequate steam to achieve 467 gpm pump flow rate, during past monthly system tests.

As described in Section I, although no historical documentation of adequate testing could be located for the AFW pump suction valves 3-20-401 and 4-20-401, the valves were satisfactorily tested on July 6, 1998, to greater than 467 gpm.

LICENSEE EVENT REPORT (LER) TEXT CONTINUATION

FACILITY NAME	DOCKET NUMBER	LER NUMBER	PAGE NO.
TURKEY POINT UNIT 3	05000250	98-003-00	6 OF 6

All seven of the affected AFW check valves were capable of performing their intended design function. Accordingly, the failure to properly specify the valves to their maximum anticipated accident required flow in the surveillance procedures is judged to have little safety significance, and has had negligible impact on the health and safety of the public.

IV. CORRECTIVE ACTIONS

- 1) The pump discharge check valves and the CST outlet valves were verified capable of passing at least 467 gpm. The steam supply check valves were verified capable of supplying the steam flow required for the pumps to supply 467 gpm.
- 2) FPL reviewed all other AFW check valves in the IST program to ensure that the correct maximum required accident flow rate was specified.
- 3) Procedures will be revised to increase the flow rate requirement to 467 gpm for the quarterly Inservice Test on check valves 20-143, 20-243, 20-343, AFSS-003B, and AFSS-003C, and 3-20-401 and 4-20-401.
- 4) FPL is performing a general review of check valves in the IST program for shared systems needed during postulated two unit events, to verify that the specified surveillance criteria bounds the maximum accident flow rate requirement.

V. ADDITIONAL INFORMATION

- A. Similar events: LER 250/96-04 reported other surveillances which were determined to be inadequate, found as a result of reviews conducted in accordance with Generic Letter 96-01, Testing of Safety-related Logic Circuits. The condition reported herein involved a misunderstanding of acceptance criteria, rather than testing of circuits.
- B. EIIS Codes are shown in the format [EIIS SYSTEM: IEEE component function identifier, second component identifier (if appropriate)].