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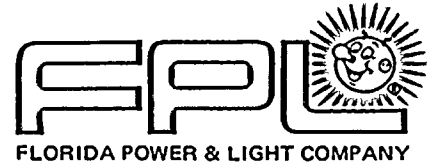
ACCESSION NBR: 8404050137 DOC. DATE: 84/04/02 NOTARIZED: NO DOCKET #
 FACIL: 50-250 Turkey Point Plant, Unit 3, Florida Power and Light C 05000250
 50-251 Turkey Point Plant, Unit 4, Florida Power and Light C 05000251
 AUTH. NAME AUTHOR AFFILIATION
 WILLIAMS, J.W. Florida Power & Light Co.
 RECIP. NAME RECIPIENT AFFILIATION
 VARGA, S.A. Operating Reactors Branch 1

SUBJECT: Forwards data re Cycle 9 core octant time averaged relative power density, time averaged peripheral assembly axial power & peripheral assembly radial pin power per 831117 request for info on pressurized thermal shock issue.

DISTRIBUTION CODE: A001S COPIES RECEIVED: LTR 1 ENCL 1 SIZE: 15
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NOTES:

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	NRC PDR 02		1	1	NSIC 05		1	1
	NTIS		1	1				



April 2, 1984
L-84-91

Office of Nuclear Reactor Regulation
Attention: Mr. Steven A. Varga, Chief
Operating Reactors Branch #1
Division of Licensing
U.S. Nuclear Regulatory Commission
Washington, D.C. 20555

RE: Turkey Point Units 3 & 4
Docket Nos. 50-250 & 50-251
Pressurized Thermal Shock -
Flux Reduction Program

Reference: "Turkey Point Unit 3 and 4 Neutron Source Data
Schedule", Letter from Mr. J. W. Williams to
Mr. S. A. Varga, December 21, 1983, L-83-597

Dear Mr. Varga:

Your letter dated November 17, 1983, requested integral neutron source data for the purpose of evaluating and verifying flux reduction. The data in Attachment A to this letter is submitted for Turkey Point Unit 3, Cycle 9 in accordance with our schedule in the Reference and consists of:

1. Cycle 9 core octant time averaged relative power density.
2. Time averaged peripheral assembly axial power.
3. Peripheral assembly radial pin power.

The time averaged core octant relative power densities provided are based on predicted assembly powers from the FPL PDQ-7 model, assuming an expected core average burnup of 12,700 MWD/MTU.

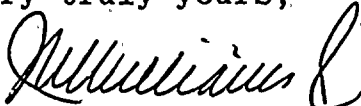
The peripheral assembly axial powers are based on predicted data from the FPL EPRI-NODE model. Comparisons of measured and predicted axial power data show good correlation and make the predicted value applicable for the purpose of the flux reduction evaluation.

8404050137 840402
PDR ADOCK 05000250
PDR

The peripheral assembly radial pin powers provided are based on predicted values from the FPL PDQ-7 model and are representative of the cycle average. These pin powers form the basis of the azimuthal flux variation to be used at the core periphery. The pin powers of all other assemblies are assumed to be flat.

Additional data, as requested by Mr. Lambros Lois of your office by telephone on March 20, 1984, has been provided in Attachment B. This data consists of the location of the critical weld for Turkey Point Units 3 and 4 and the time averaged peripheral assembly axial powers for Unit 4 Cycle 9. Should you have any questions, please contact Dr. Finis Southworth at 305-552-3468.

Very truly yours,



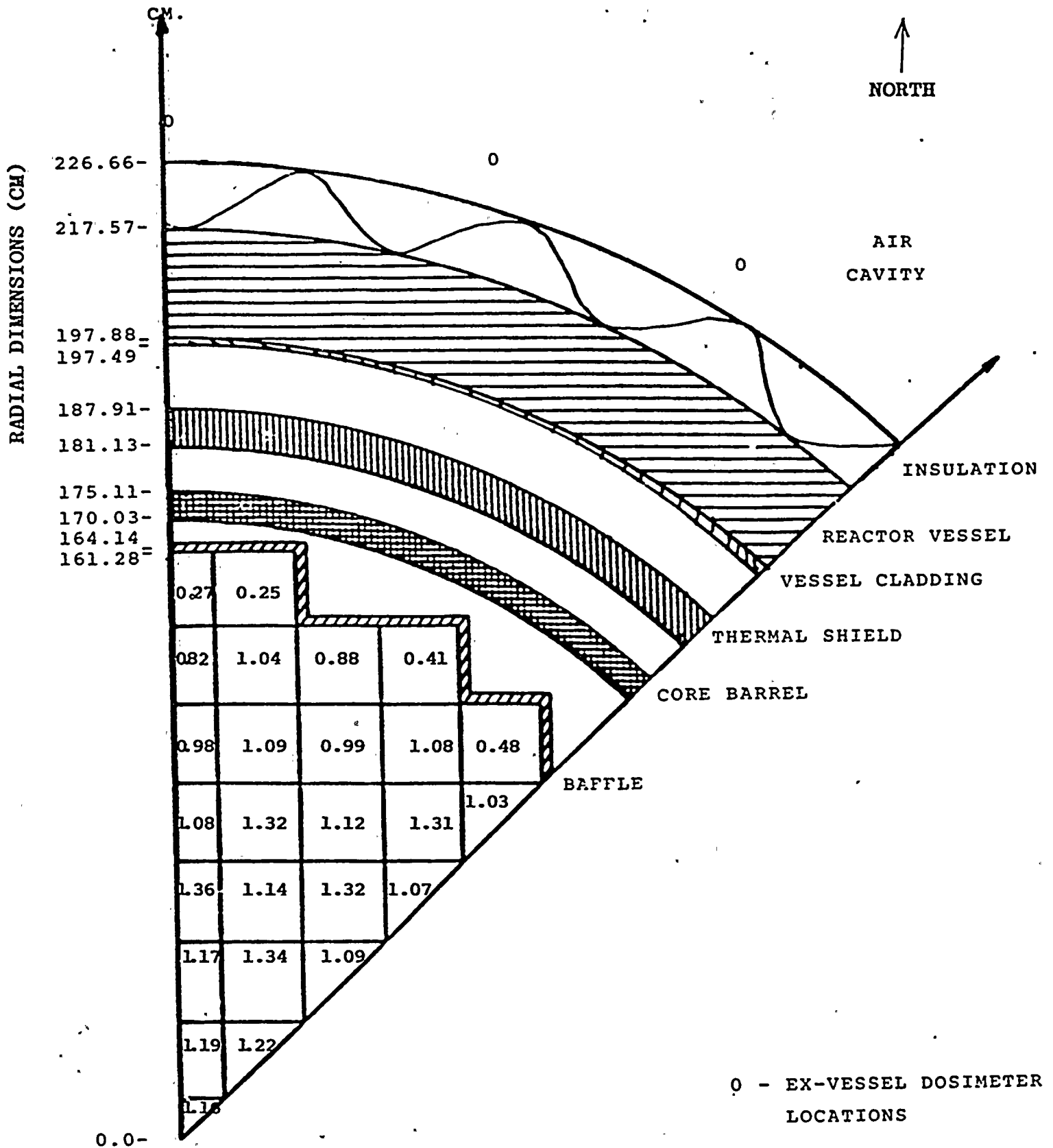
J. W. Williams, Jr.
Vice President
Nuclear Energy

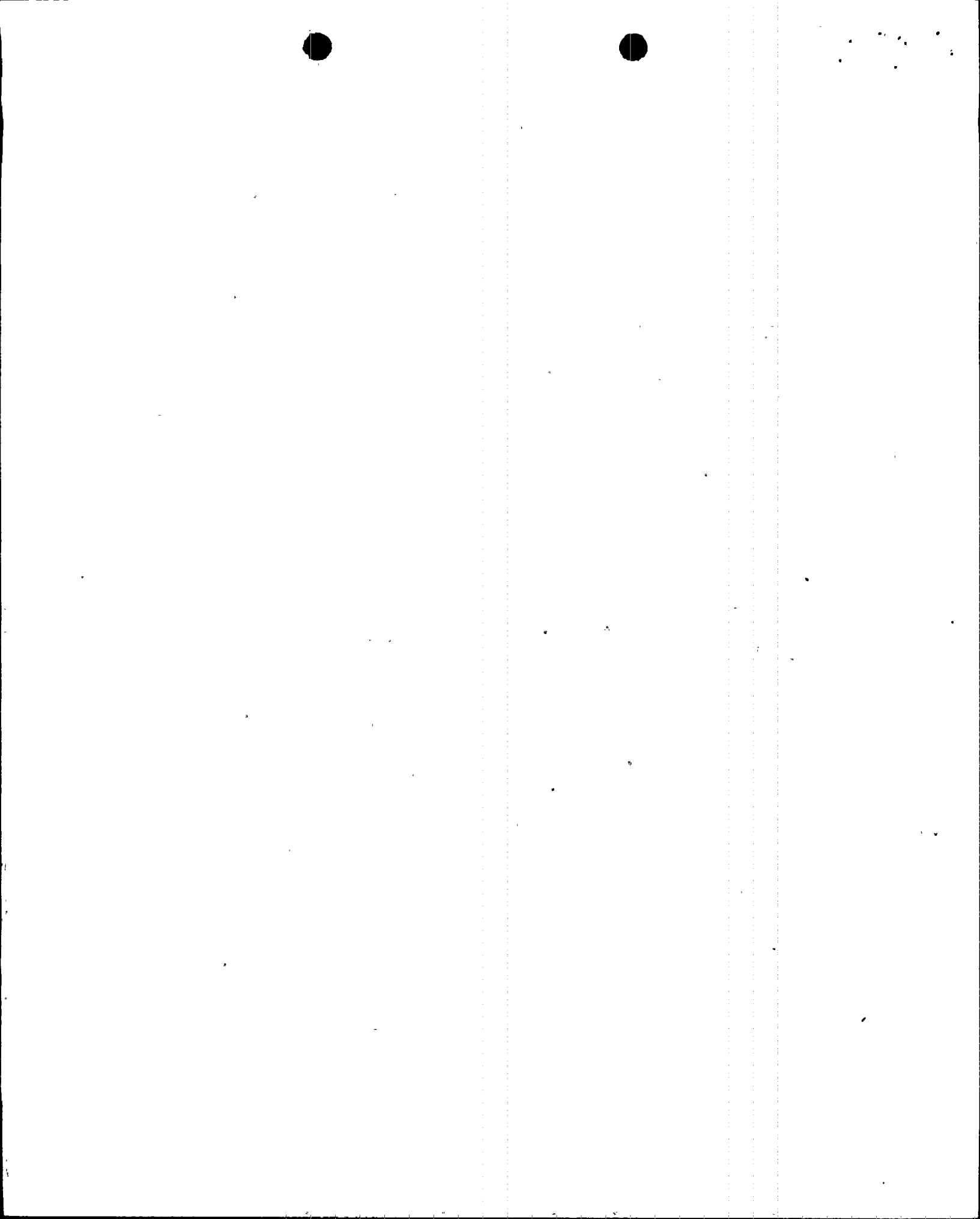
JWW/^{ERK}ERK/daj

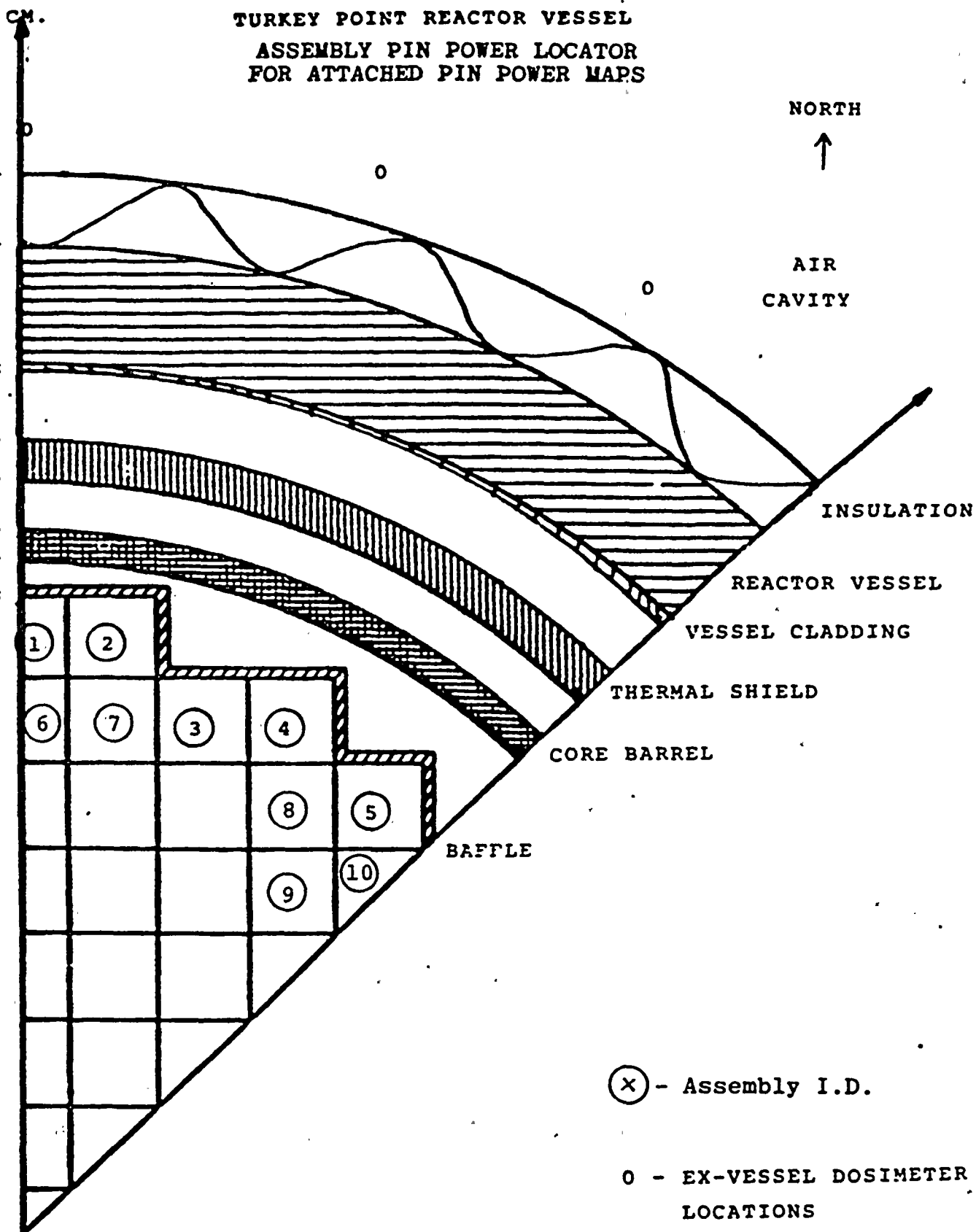
cc: J. P. O'Reilly, Region II
Harold F. Reis, Esquire

ATTACHMENT A

TURKEY POINT UNIT 3 CYCLE 9
CYCLE AVERAGE
RELATIVE POWER DENSITY







TURKEY POINT
UNIT 3 CYCLE 9

Normalized Assembly Axial Power Profiles
(Normalized to Unity)

Assembly No.	<u>1</u>	<u>2</u>	<u>3</u>	<u>4</u>	<u>5</u>	
	0.92	0.83	0.61	0.70	0.74	Top
	1.18	1.12	0.92	0.96	0.99	
	1.22	1.19	1.03	1.05	1.05	
	1.24	1.23	1.07	1.08	1.08	
	1.20	1.20	1.09	1.08	1.07	
	1.16	1.17	1.11	1.09	1.08	
	0.84	0.88	1.11	1.08	1.07	
	0.80	0.86	1.12	1.09	1.08	critical weld
	0.78	0.84	1.12	1.08	1.07	
	0.81	0.87	1.12	1.07	1.06	
	1.03	1.03	1.02	0.99	0.98	
	<u>0.82</u>	<u>0.78</u>	<u>0.69</u>	<u>0.71</u>	<u>0.73</u>	Bottom
	0.27	0.25	0.88	0.41	0.48	Assembly Average (RPD)

Assembly No.	<u>6</u>	<u>7</u>	<u>8</u>	<u>9</u>	<u>10</u>	
	0.73	0.63	0.63	0.63	0.66	Top
	1.00	0.93	0.91	0.90	0.93	
	1.06	1.03	1.01	1.01	1.02	
	1.10	1.08	1.06	1.05	1.06	
	1.09	1.09	1.07	1.07	1.07	
	1.09	1.10	1.10	1.09	1.09	
	1.05	1.09	1.10	1.10	1.09	
	1.06	1.10	1.13	1.12	1.11	critical weld
	1.04	1.11	1.13	1.13	1.11	
	1.05	1.10	1.12	1.12	1.10	
	1.00	1.03	1.03	1.04	1.02	
	<u>0.73</u>	<u>0.71</u>	<u>0.72</u>	<u>0.73</u>	<u>0.73</u>	Bottom
	0.82	1.04	1.08	1.31	1.03	Assembly Average (RPD)

Note: To obtain assembly axial relative power density (RPD), multiply normalized assembly axial power by assembly average relative power density.

BY S. R. Kneale DATE 3/2/84
CHKD. BY 748 DATE 3/22/84



SHEET NO. 1 OF 5
PROJECT NO. 4 Unit 3 Cycle 2

RELATIVE PIN POWERS (x100)
ASSEMBLY 1

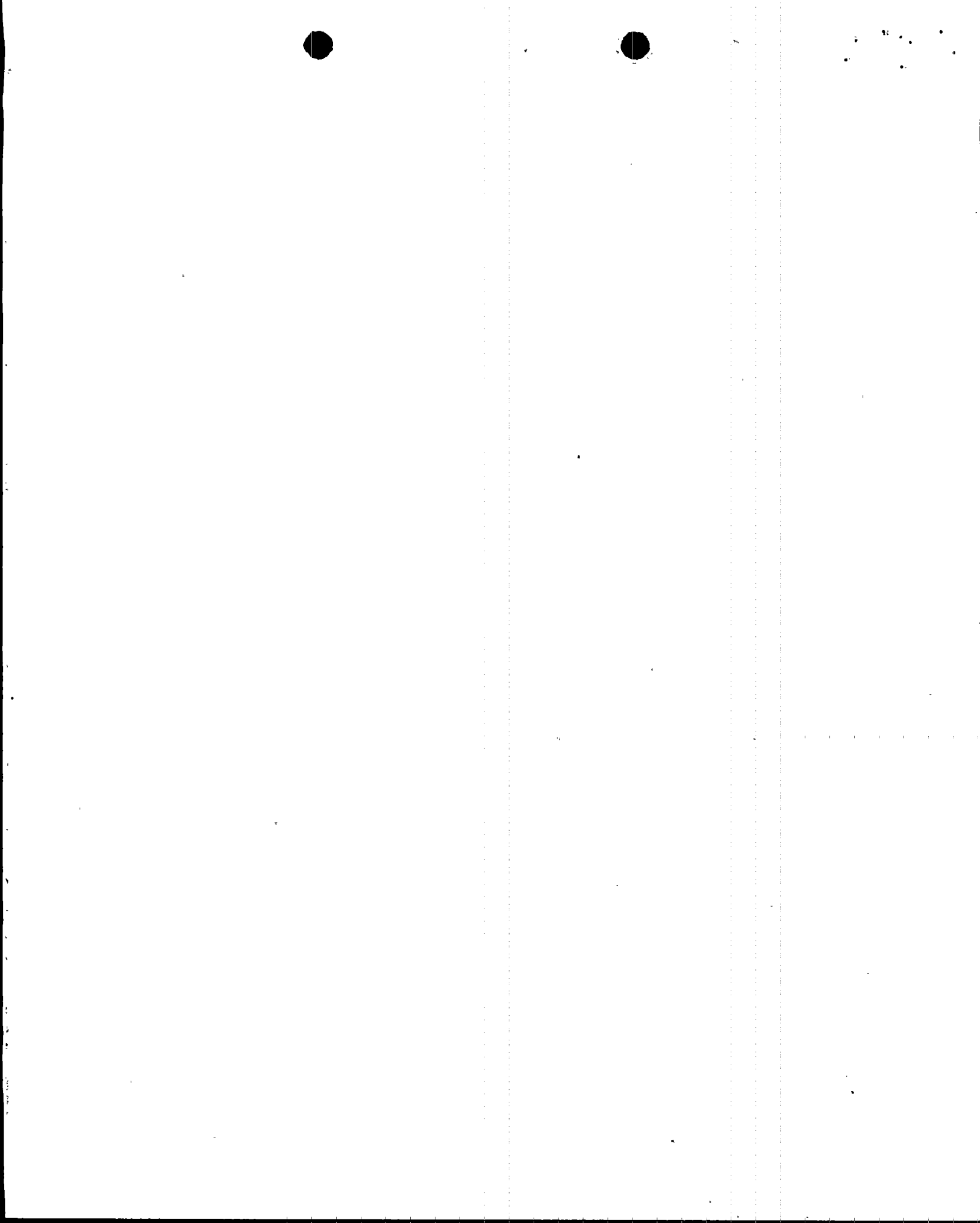
↑
NORTH

J	I														
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
1															
2															
3															
4															
5															
6															
7															
8	46	42	38	0	33	32	30	0	25	22	19	0	15	13	11
9	46	41	37	35	33	31	29	27	25	22	19	16	15	13	11
10	46	41	0	34	32	31	29	27	24	21	19	16	15	13	11
11	46	42	38	35	0	30	28	26	23	21	0	16	15	13	11
12	46	42	38	35	32	30	27	0	23	20	18	17	15	13	11
13	47	42	0	36	33	0	27	25	23	0	19	17	0	13	11
14	48	43	40	37	34	31	29	26	24	21	19	17	15	13	11
15	49	45	41	38	35	32	30	27	25	22	20	18	16	14	11



BY E. R. [Signature]DATE 3/22/84CHKD. BY [Signature]DATE 3/22/84SHEET NO. 2 OF 5PROJECT NO. Unit 3 Cycle 9RELATIVE PIN POWERS ($\times 100$)
ASSEMBLY 2↑
NORTH

J	I														
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
1	51	47	43	40	37	33	31	28	25	23	21	18	16	14	11
2	51	46	42	39	36	32	30	27	24	22	20	17	15	13	10
3	51	46	0	38	35	0	29	26	23	0	19	17	0	13	10
4	51	46	41	38	35	32	28	0	23	21	19	17	14	12	10
5	51	46	41	38	0	32	29	26	24	21	0	16	14	12	10
6	51	45	0	38	35	32	29	26	24	21	18	16	0	12	10
7	51	45	40	37	34	32	29	27	24	21	18	15	13	12	9
8	51	45	40	0	34	31	29	0	24	20	17	0	13	11	9
9	50	44	39	36	33	31	28	25	23	20	17	14	12	11	9
10	49	43	0	35	32	30	27	24	21	19	16	14	0	10	8
11	49	43	38	34	0	28	25	22	20	18	0	13	11	10	8
12	48	42	37	33	30	26	23	0	18	16	14	13	11	9	7
13	46	40	0	31	28	0	22	19	17	0	13	12	0	9	7
14	44	37	33	29	26	23	20	18	16	14	12	11	9	8	6
15	39	32	28	25	23	20	18	16	14	12	11	9	8	7	6



BY E. R. Kuntz DATE 3/2/84
CHKD. BY 778 DATE 3/22/84

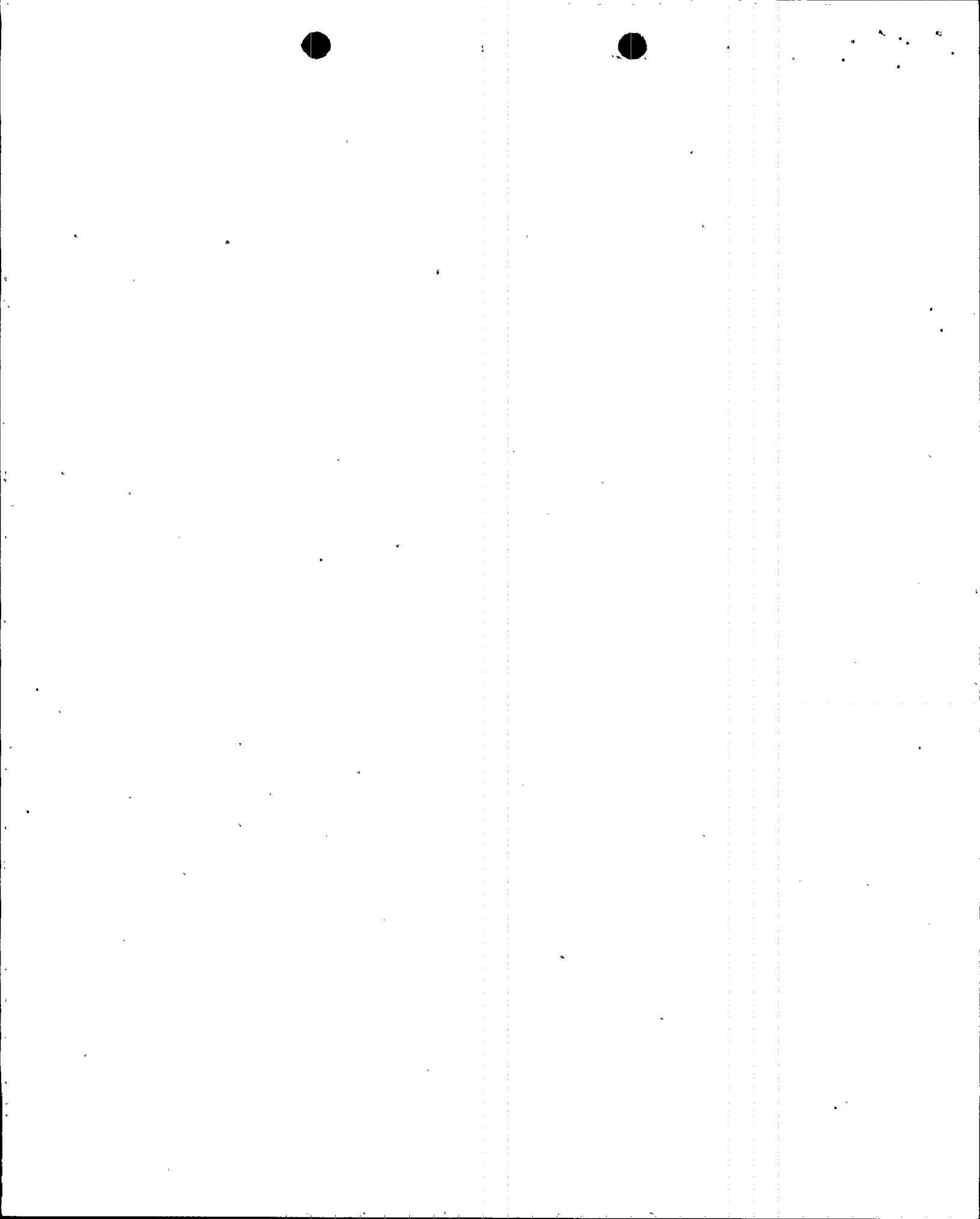


SHEET NO. 3 OF 5
PROJECT NO. Unit 3 Cycle 9

RELATIVE PIN POWERS (x100)
ASSEMBLY 3

↑
NORTH

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
1	110	111	111	110	108	106	103	99	95	91	86	81	74	66	54
2	111	114	116	113	112	111	106	101	98	95	89	83	76	66	51
3	112	116	0	118	116	0	112	106	103	0	92	85	0	66	50
4	111	115	118	118	118	116	112	0	103	99	93	85	77	64	49
5	111	114	118	119	0	111	105	102	97	94	0	85	75	63	48
6	110	115	0	118	113	106	100	96	92	89	87	83	0	63	48
7	108	111	112	116	108	101	94	96	11	85	83	80	73	60	46
8	107	108	114	0	107	100	98	0	90	83	81	0	70	57	45
9	106	109	113	112	105	98	95	93	87	81	79	76	69	57	43
10	105	109	0	111	105	98	92	88	84	81	78	75	0	56	42
11	103	105	108	109	0	100	93	90	85	82	0	73	64	53	40
12	101	103	105	105	103	100	95	0	86	82	76	69	61	51	39
13	99	102	0	100	98	0	92	86	83	0	72	65	0	49	37
14	97	97	97	94	91	89	84	78	75	72	65	60	54	45	35
15	94	92	91	88	85	82	78	73	69	65	60	55	49	42	33



BY E. J. Kunkle DATE 2/22/84
CHKD. BY FHS DATE 2/22/84



SHEET NO. 4 OF 5
PROJECT NO. Unit 3 Cycle

RELATIVE PIN POWERS (x100)
ASSEMBLY 4

↑
NORTH

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
1	73	71	70	67	64	62	59	55	52	49	45	41	37	32	25
2	72	71	69	67	64	61	58	54	51	48	44	40	36	31	24
3	71	70	0	66	64	0	57	53	50	0	43	39	0	30	23
4	69	68	67	66	64	60	55	0	49	46	43	38	33	28	22
5	68	67	66	65	0	58	53	50	46	44	0	37	32	27	21
6	66	65	0	62	59	54	49	46	43	41	38	35	0	26	20
7	64	62	61	59	55	50	47	44	40	37	35	32	28	24	19
8	62	60	58	0	52	48	45	0	38	35	33	0	27	22	17
9	60	58	56	54	50	46	42	39	36	33	31	28	25	21	16
10	57	56	0	52	49	44	40	37	34	32	30	27	0	20	15
11	55	53	51	50	0	43	38	35	32	31	0	26	22	18	14
12	52	50	48	46	44	40	36	0	30	28	26	23	20	17	13
13	49	46	0	41	39	0	33	30	27	0	23	20	0	15	12
14	44	41	39	36	33	31	28	26	24	22	19	17	15	13	10
15	37	33	31	29	27	25	23	21	19	17	15	14	12	10	8

BY E R Kunkle DATE 3/22/84
CHKD. BY FHJ DATE 3/23/84

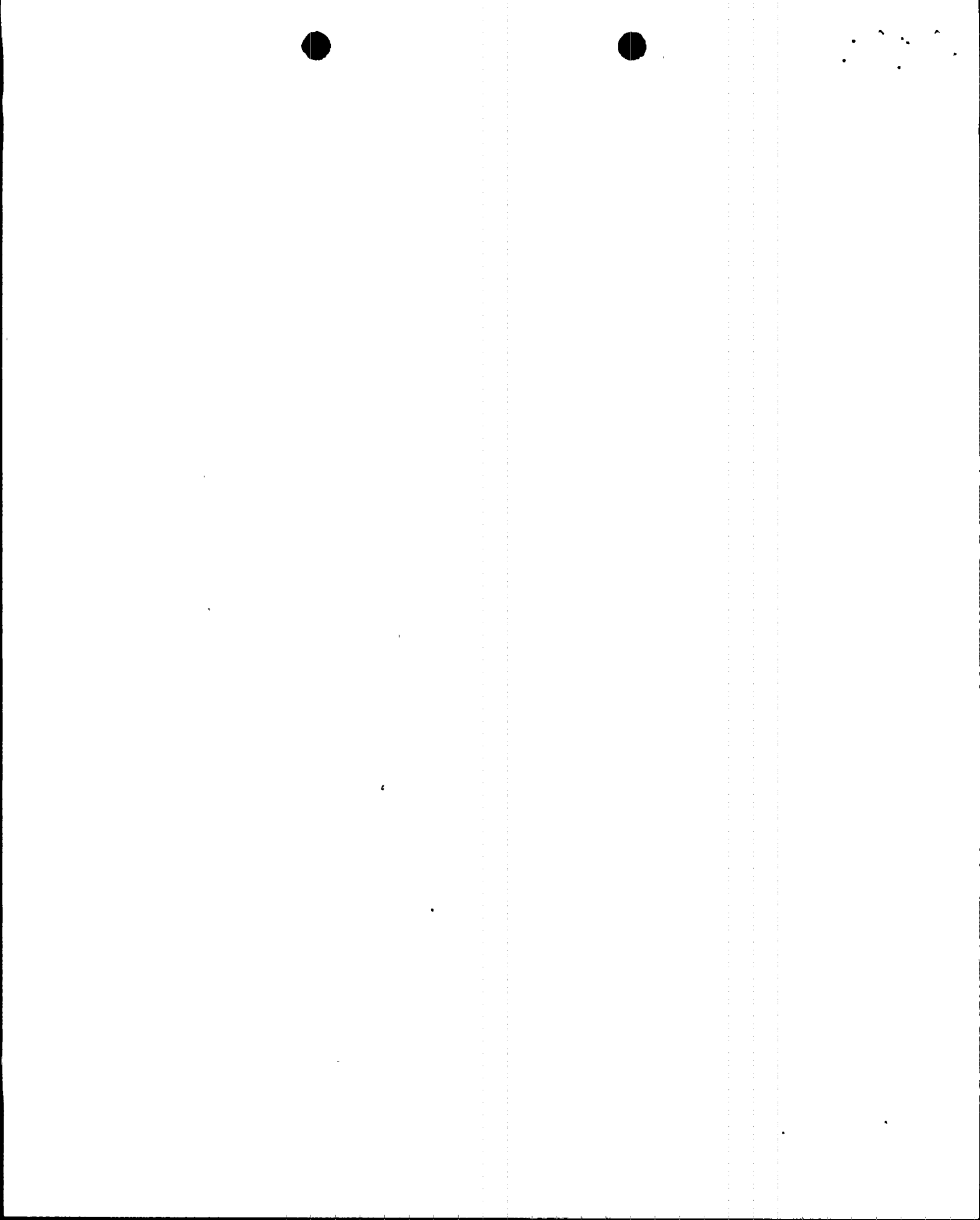


SHEET NO. 5 OF 5
PROJECT NO. Unit 3 Cycle 9

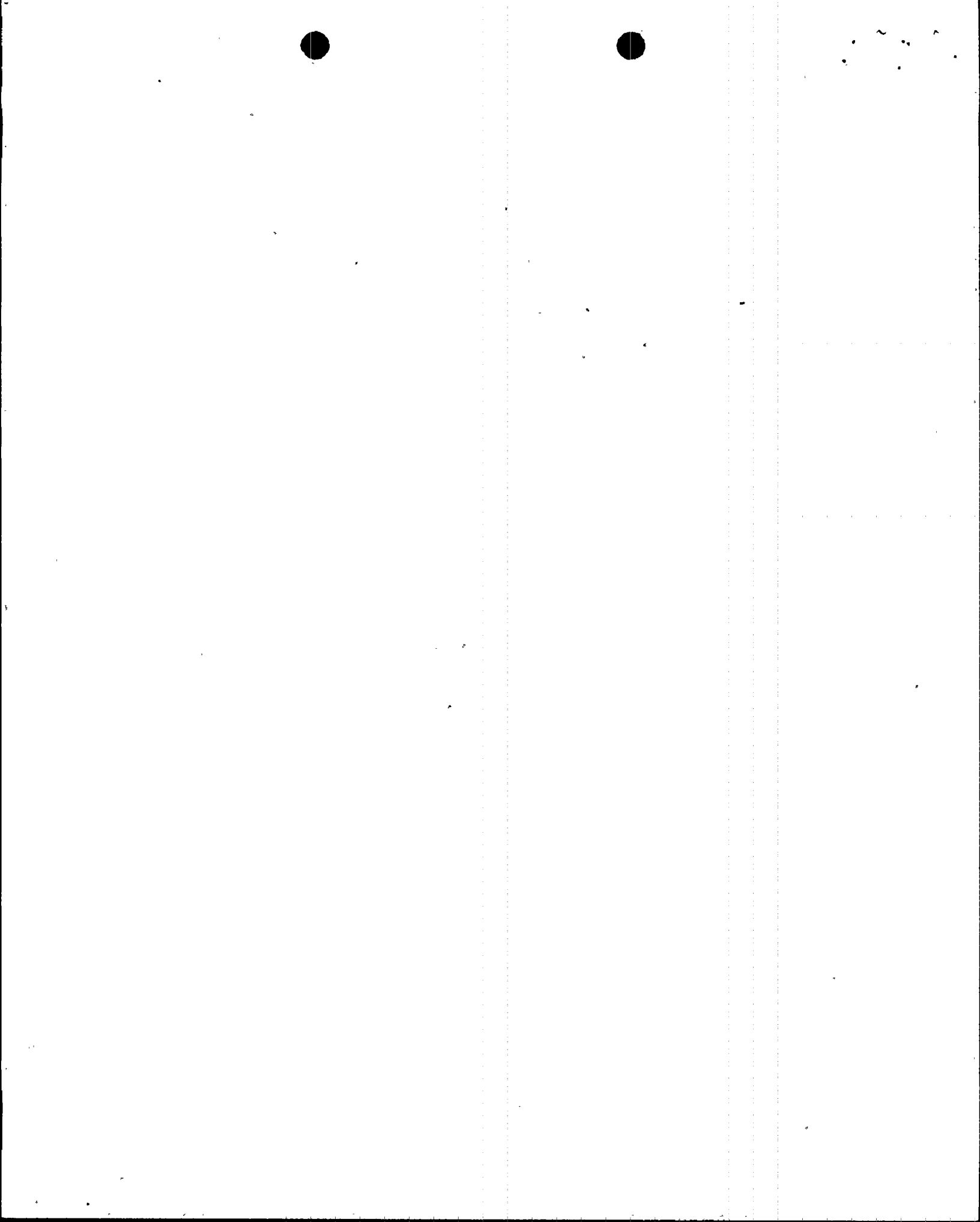
RELATIVE PIN POWERS ($\times 100$)
ASSEMBLY 5

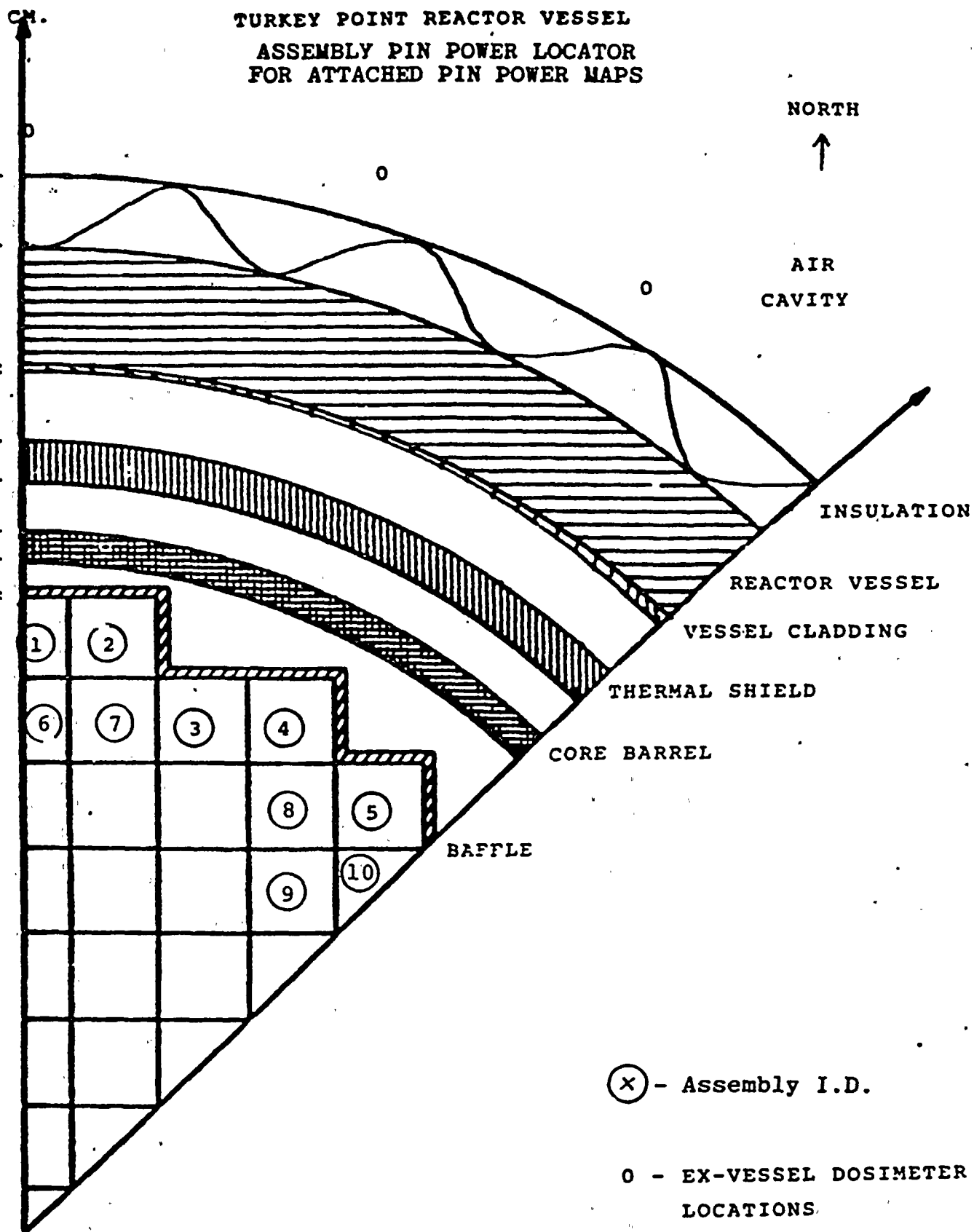
↑
NORTH

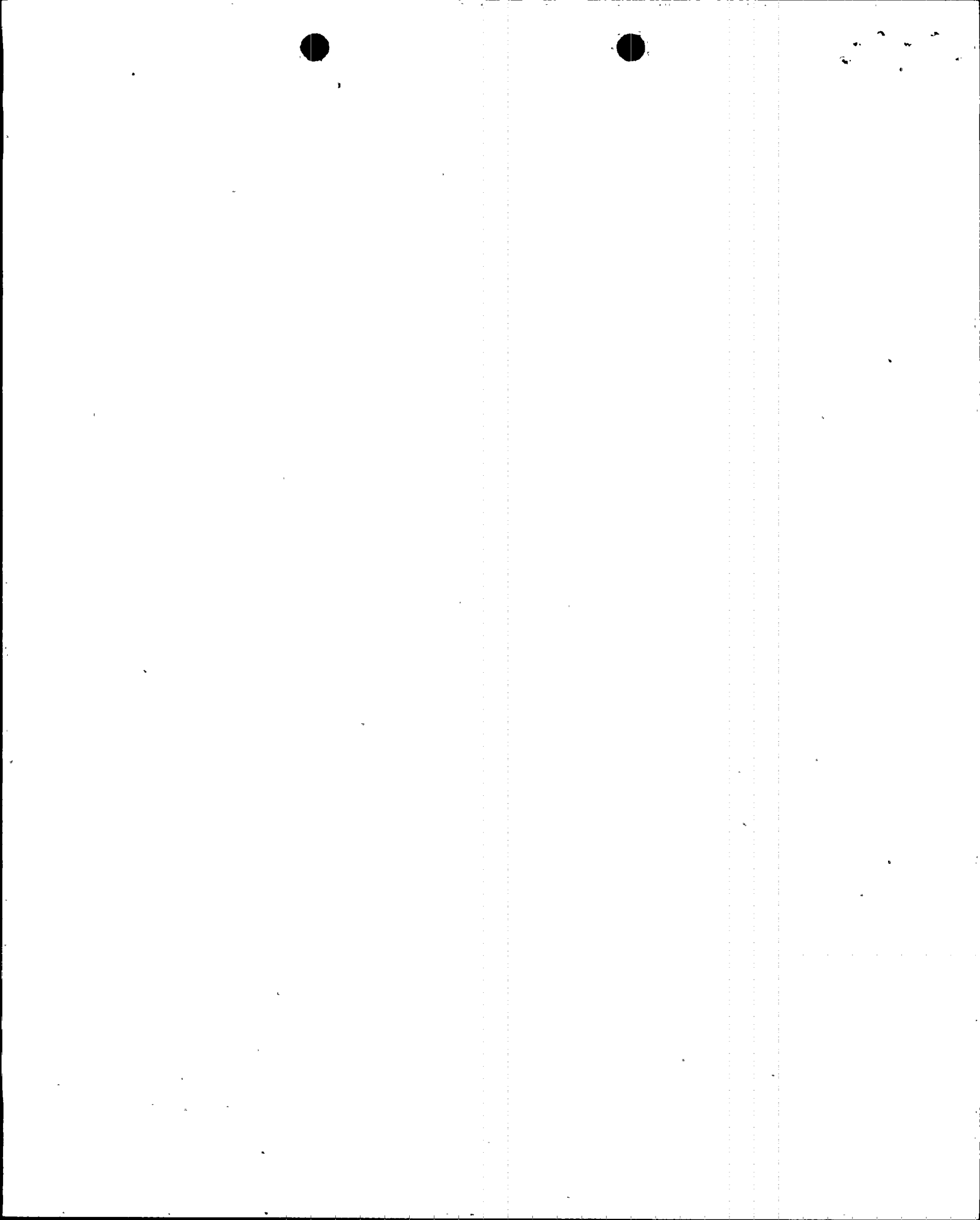
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
1	94	90	87	83	80	77	73	70	66	63	60	55	51	46	39
2	90	87	85	82	78	75	71	67	64	61	57	53	48	43	34
3	86	85	0	80	77	0	70	65	62	0	55	50	0	40	32
4	83	81	80	78	75	71	67	0	59	56	53	48	43	38	30
5	79	78	77	75	0	68	63	59	55	53	0	46	41	35	28
6	76	75	0	71	68	63	58	55	51	49	46	42	0	33	26
7	73	71	70	67	63	58	54	51	48	45	42	39	35	30	24
8	69	67	66	0	59	55	51	0	45	41	39	0	32	28	22
9	66	64	63	60	56	51	48	45	42	39	36	33	30	26	21
10	63	61	0	57	53	49	45	42	39	36	34	31	0	24	19
11	59	57	56	54	0	46	42	39	36	34	0	29	25	22	17
12	56	53	51	49	46	43	39	0	34	31	29	26	23	19	15
13	52	49	0	44	41	0	36	33	30	0	25	23	0	17	14
14	46	44	41	38	36	34	31	28	26	24	22	20	17	15	12
15	39	35	33	31	29	27	25	23	21	19	17	15	14	12	10



ATTACHMENT B







TURKEY POINT
UNIT 4 CYCLE 9

Normalized Assembly Axial Power Profiles
(Normalized to Unity)

Assembly No.	<u>1</u>	<u>2</u>	<u>3</u>	<u>4</u>	<u>5</u>	
	0.82	0.76	0.56	0.66	0.68	Top
	1.02	0.99	0.87	0.93	0.95	
	1.04	1.03	0.99	1.02	1.03	
	1.07	1.07	1.06	1.08	1.08	
	1.05	1.06	1.09	1.08	1.08	
	1.08	1.09	1.12	1.11	1.11	
	1.05	1.07	1.14	1.11	1.10	
	1.07	1.09	1.16	1.13	1.11	critical weld
	1.04	1.06	1.17	1.11	1.09	
	1.04	1.06	1.15	1.09	1.08	
	0.97	0.97	1.03	0.98	0.98	
	<u>0.77</u>	<u>0.73</u>	<u>0.66</u>	<u>0.69</u>	<u>0.70</u>	Bottom
	0.31	0.29	1.02	0.44	0.47	Assembly Average (RPD)
Assembly No.	<u>6</u>	<u>7</u>	<u>8</u>	<u>9</u>	<u>10</u>	
	0.72	0.58	0.57	0.64	0.59	Top
	0.96	0.88	0.87	0.91	0.89	
	1.02	0.99	1.00	1.01	1.01	
	1.06	1.05	1.06	1.06	1.06	
	1.06	1.08	1.09	1.08	1.09	
	1.09	1.11	1.12	1.10	1.11	
	1.08	1.13	1.13	1.10	1.13	
	1.10	1.15	1.16	1.13	1.15	critical weld
	1.08	1.16	1.16	1.12	1.15	
	1.08	1.15	1.14	1.11	1.13	
	1.00	1.04	1.03	1.02	1.02	
	<u>0.74</u>	<u>0.69</u>	<u>0.68</u>	<u>0.72</u>	<u>0.68</u>	Bottom
	0.73	1.12	1.16	1.19	1.13	Assembly Average (RPD)

Note: To obtain assembly axial relative power density (RPD), multiply normalized assembly axial power by assembly average relative power density.

