

# Calculation Cover Sheet

## Cook Nuclear Plant

SECTION

SHEET 1 OF 20

APPROVED BY: Paul D. Hoyer 12/2/96  
DATE

METHOD OF VERIFICATION: ALTERNATE CALCULATION \_\_\_\_\_ DESIGN REVIEW *OK 11/27/86*

Date \_\_\_\_\_



## Design Inputs

Required pump flows and CCP NPSH obtained from the various pump curves are as follows:

Containment Spray Pump - 3200 gpm (SD-12-CTS-100, Rev 0, 6.2)  
Safety Injection Pump - 650 gpm (SD DCC-NEMH111 Rev 16, 3.4.2.b.12)  
Residual Heat Removal Pump - 4500 gpm (SD-12-RHR-100, Rev 0, 8.0)  
Centrifugal Charging Pump - 550 gpm (SD DCC-NEMH111, Rev 16, 3.4.1A)  
Centrifugal Charging Pump NPSH required - 22 ft abs @ 550 gpm

Calculation NEMP950501JEW approved 4/11/96 performed for severe accident setpoints. Note 100°F water temperature obtained from this calculation.

Suction piping configuration (length, dia, fittings, etc) obtain from the isometric drawings.

## References

Containment Spray Pump - Byron Jackson Pump curve T-32913-1  
Safety Injection Pump - Pacific Pump curve 34554D  
Residual Heat Removal Pump - Ingersoll-Rand Pump curve N-318  
Centrifugal Charging Pump - Pacific Pump curve 34617I

## Isometric Drawings

2-SI-53    2-SI-6    2-SI-43    2-CS-79    2-CS-80  
2-CS-81

Hydraulic friction loss program HFLC5 will be used to determine the frictional losses thru suction piping. HFLC5 is an inhouse developed program which was approved for use on Feb 28, 1988. This program was validated and approved in accordance with the requirements of GP 2.6 Software Quality assurance Standard in use in 1988.

## Description

### Purpose:

DBD action item DB-12-ECCS-24 "Centrifugal Charging Pump Available NPSH Calculation" indicated that an NPSH available calculation for the CCPs could not be found. The action item requested that a calculation be prepared which would determine the NPSH available to the CCPs during the Injection Phase.

This calculation will determine the NPSH available to the CCPs based on providing flow to two trains of safeguards pumps (containment spray, safety injection, residual heat removal, and centrifugal charging).

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### Method:

In order to obtain the frictional losses associated with the suction piping the isometric drawings were used to obtain the piping configuration. The sketch (pg 4 ) shows the flow path and branching flows to the other safeguard pumps. The data obtained from the isometric drawings was compiled on the attached "pipe Friction Calculation Data Sheets". The totals shown on these sheets is used as input to HFLC5.

HFLC5 calculates the segments frictional losses and is based on the Dracy-Weisbach formula

$$H = f \frac{L}{D} \frac{V^2}{2g}$$

where: H- frictional loss in feet  
f- friction factor, dimensionless  
L- pipe length in feet  
D- pipe diameter in feet  
V- pipe velocity in feet/sec  
g- gravitational constant, 32.174 feet/sec<sup>2</sup>

The NPSH available is then determined as follows:

$$NPSH_a = H_p - H_{VPA} + H_{st} - H_{fs}$$

where: NPSH<sub>a</sub> - net positive suction head available in ft abs  
H<sub>p</sub> - atmospheric pressure in ft  
H<sub>VPA</sub> - vapor pressure of water  
H<sub>st</sub> - static elevation difference in feet  
H<sub>fs</sub> - friction losses in feet

### Assumptions:

1 - RWST water level is at minimum elevation (bottom of pipe) and is determined as 611.25' (24" suction pipe center line) - 1' (radius of 24" pipe) results in 610.25'. This is conservative since in normal ECCS operation the CCPs are transferred to the recirculation sump/RHR before the RWST level reaches Lo-Lo or elevation 613.0'.

2 - RWST temperature is 100°F for conservatism. Vapor pressure at 100°F is .94925 psia or 2.21' based on multiplying by the conversion factor 2.323 ft for 100°F water.

3 - RWST is open to atmosphere

4 - For purposes of this calculation it is assumed that all safeguards pumps are operating. That is, 2 safety injection, 2 residual heat removal, 2 containment spray, and 2 centrifugal charging pumps.

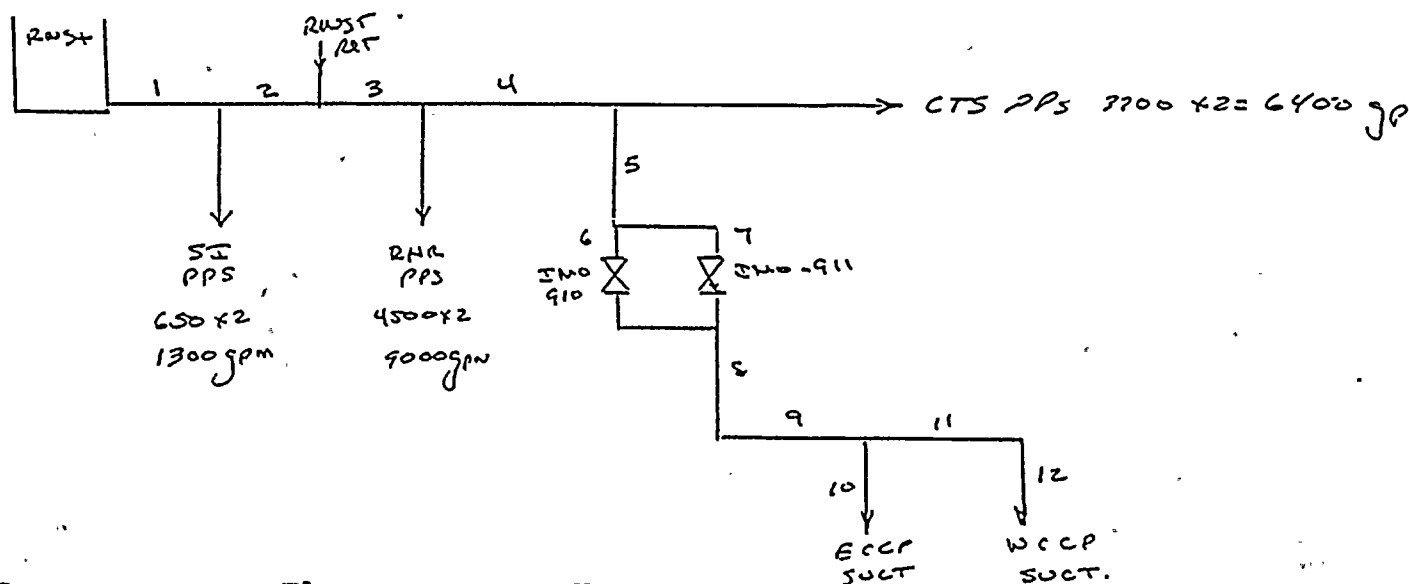
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## Conclusions:

This results of this calculation indicate that the NPSH available to the charging pumps exceeds the NPSH required by approximately 7' absolute (6.97' East pp and 6.55' West pp) at the CCP flow of 550 gpm.

## Calculation:



Segments	Flow	H <sub>f</sub>
1	17,800	11.71
2	16,500	.68
3	16,500	.7
4	7,500	.15
5	1,100	1.54
6	550	.21
7	550	.33
8	1,100	3.04
9	1,100	.74
10	550	1.64
11	550	.24
12	550	.56
13	550	1.26

$$NPSH_a = H_a - H_{vpa} + H_{st} - H_{fs}$$

$$H_a = 33.96 \text{ ft}$$

$$H_{vpa} = .95 \text{ psia or } 2.21 \text{ ft}$$

$$H_{st} = 610.25 - 592.5 = 17.75 \text{ ft}$$

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The friction loss for each pump is determined by adding the respective line segments to that pump. That is for the east CCP add segments 1 thru 5 and 7 thru 10 and for the west CCP add segments 1 thru 5 and 7 thru 9 and 11 thru 13.

$$\begin{aligned} H_f \text{ ECCP} &= 11.71 + .68 + .7 + .15 + 1.54 + .33 + 3.04 + .74 + 1.64 \\ &= 20.53 \text{ ft} \end{aligned}$$

$$\begin{aligned} H_f \text{ WCCP} &= 11.71 + .68 + .7 + .15 + 1.54 + .33 + 3.04 + .74 + .24 + \\ &\quad .56 + 1.26 \\ &= 20.95 \text{ ft} \end{aligned}$$

$$\begin{aligned} \text{NPSH}_a \text{ ECCP} &= 33.96 - 2.21 + 17.75 - 20.53 \\ &= 28.97 \text{ ft abs} \end{aligned}$$

$$\begin{aligned} \text{NPSH}_a \text{ WCCP} &= 33.96 - 2.21 + 17.75 - 20.95 \\ &= 28.55 \text{ ft abs} \end{aligned}$$

NPSH<sub>r</sub> at 550 gpm is 22 ft

Therefore, the NPSH<sub>a</sub> exceeds the NPSH<sub>r</sub> by 6.97 ft abs and 6.55 ft abs for the ECCP and WCCP respectively.

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## PIPE FRICTION CALC - INPUT FILE IS-c:\calc\ccpnpsh

INPUT DATA FOR THE HFLC5 SYS. RES. CALC.  
CONSISTS OF THE FOLLOWING DATA:

T - TEMPERATURE DEG F  
E - PIPE ABSOLUTE ROUGHNESS (FT.)  
N - FIRST PIPE SEGMENT NUMBER  
N1 - LAST PIPE SEGMENT NUMBER  
QDES - DESIGN FLOW THRU PIPE SEGMENT (GPM)  
QMIN - MINIMUM FLOW THRU PIPE SEGMENT (GPM)  
QMAX - MAXIMUM FLOW THRU PIPE SEGMENT (GPM)  
QDELT - FLOW INCREMENT THRU PIPE SEGMENT (GPM)  
D - PIPE SEGMENT INTERNAL DIA. (IN.)  
L - PIPE SEGMENT LENGTH (FT.)  
K - PIPE SEGMENT K FACTORS  
L/D - PIPE SEGMENT L/D FACTORS

FOLLOWING IS YOUR INPUT DATA

T	E	N	N1
100.00	.00015	1	13

QDES	QMIN	QMAX	QDELT	D	L	K	L/D
.00	17000.00	17800.00	200.00	23.250	221.33	1.00	148.00
.00	16000.00	16500.00	500.00	23.250	6.00	.00	20.00
.00	16000.00	16500.00	500.00	23.250	7.81	.00	20.00
.00	7000.00	7500.00	500.00	23.250	6.35	.00	20.00
.00	1000.00	1100.00	100.00	7.981	13.55	.44	80.00
.00	500.00	550.00	50.00	7.981	8.00	.00	53.00
.00	500.00	550.00	50.00	7.981	8.00	.00	93.00
.00	1000.00	1100.00	100.00	7.981	12.94	.00	235.00
.00	1000.00	1100.00	100.00	7.981	1.20	.00	60.00
.00	500.00	550.00	50.00	6.065	19.00	.00	133.00
.00	500.00	550.00	50.00	7.981	15.96	.00	52.00
.00	500.00	550.00	50.00	6.065	12.71	.22	20.00
.00	500.00	550.00	50.00	6.065	9.35	.00	113.00

FOLLOWING IS HFLC5 RESULTS

WATER TEMP. (F) = 100.00  
DENSITY (LBM/CUFT) = 62.00  
ABS VISCOSITY (LBM/SEC/FT) = .460533E-03  
PIPE ABS ROUGHNESS (FT) = .150000E-03

PIPE SEG NO	1	PIPE DIA (ID-IN) = 23.250				
FLOW-GPM	VEL (FPS)	LHD (FT)	KHD (FT)	LDHD (FT)	TOT	HD (FT)
17000.0	12.85	3.54	2.56	4.59	10.70	
17200.0	13.00	3.63	2.63	4.70	10.95	
17400.0	13.15	3.71	2.69	4.80	11.20	
17600.0	13.30	3.79	2.75	4.91	11.45	
17800.0	13.45	3.88	2.81	5.02	11.71	

PIPE SEG NO	2	PIPE DIA (ID-IN) = 23.250				
FLOW-GPM	VEL (FPS)	LHD (FT)	KHD (FT)	LDHD (FT)	TOT	HD (FT)
16000.0	12.09	.09	.00	.55	.64	
16500.0	12.47	.09	.00	.59	.68	

PIPE SEG NO	3	PIPE DIA (ID-IN) = 23.250				
FLOW-GPM	VEL (FPS)	LHD (FT)	KHD (FT)	LDHD (FT)	TOT	HD (FT)
16000.0	12.09	.11	.00	.55	.66	
16500.0	12.47	.12	.00	.59	.70	

PIPE SEG NO	4	PIPE DIA (ID-IN) = 23.250				
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PIPE SEG NO	PIPE DIA (ID-IN) =	7.981			
5	7.981				
FLOW-GPM	VEL (FPS)	LHD (FT)	KHD (FT)	LDHD (FT)	TOT HD (FT)
7000.0	5.29	.02	.00	.11	.13
7500.0	5.67	.02	.00	.13	.15
6	7.981				
FLOW-GPM	VEL (FPS)	LHD (FT)	KHD (FT)	LDHD (FT)	TOT HD (FT)
1000.0	6.41	.20	.28	.79	1.28
1100.0	7.05	.24	.34	.96	1.54
7	7.981				
FLOW-GPM	VEL (FPS)	LHD (FT)	KHD (FT)	LDHD (FT)	TOT HD (FT)
500.0	3.21	.03	.00	.14	.17
550.0	3.53	.04	.00	.17	.21
8	7.981				
FLOW-GPM	VEL (FPS)	LHD (FT)	KHD (FT)	LDHD (FT)	TOT HD (FT)
500.0	3.21	.03	.00	.25	.28
550.0	3.53	.04	.00	.30	.33
9	7.981				
FLOW-GPM	VEL (FPS)	LHD (FT)	KHD (FT)	LDHD (FT)	TOT HD (FT)
1000.0	6.41	.19	.00	2.34	2.53
1100.0	7.05	.23	.00	2.81	3.04
10	6.065				
FLOW-GPM	VEL (FPS)	LHD (FT)	KHD (FT)	LDHD (FT)	TOT HD (FT)
500.0	5.55	.30	.00	1.06	1.36
550.0	6.11	.36	.00	1.28	1.64
11	7.981				
FLOW-GPM	VEL (FPS)	LHD (FT)	KHD (FT)	LDHD (FT)	TOT HD (FT)
500.0	3.21	.06	.00	.14	.20
550.0	3.53	.08	.00	.17	.24
12	6.065				
FLOW-GPM	VEL (FPS)	LHD (FT)	KHD (FT)	LDHD (FT)	TOT HD (FT)
500.0	5.55	.20	.10	.16	.47
550.0	6.11	.24	.13	.19	.56
13	6.065				
FLOW-GPM	VEL (FPS)	LHD (FT)	KHD (FT)	LDHD (FT)	TOT HD (FT)
500.0	5.55	.15	.00	.90	1.05
550.0	6.11	.18	.00	1.09	1.26

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# PIPE FRICTION CALCULATION DATA SHEETS

 NESN 961021AF  
 SHEET 8 OF 20  
 PLANT Cook  
 BY AE DATE 10/20/96

 SYSTEM: 126 P = 1125 IN CALCULATION UNIT: 2

 PIPE SEGMENT TO & FROM: FROM RWIT TO SJ PP TARGE OFF

 DWG. REF.: 2-SI-53 1062 2-SI-6

 FLUID TEMP (°F): 100 PIPE ABS. ROUGHNESS (FT): \_\_\_\_\_ PIPE SEGMENT NUMBER: 1

 DESIGN FLOW: 1 MINIMUM FLOW: 1000 MAXIMUM FLOW: 13000 FLOW INCREMENT: 1000

 PIPE I.D. (IN): 24" Ø 13-14 23 25 PIPE EL: 611-3 TO EL: 585-1 7/16"

 STRAIGHT PIPE LENGTHS      FITTINGS      NUMBER      \*K OR L/D       $\Sigma K$        $\Sigma L/D$ 

2'-6"	GATE VALVE	13		
46'-6"	GLOBE VALVE	340		
4.95'	BUTTERFLY VALVE	40		
7'-7"	SWING CHECK	135		
31'-0"	90° STD. ELBOW	30		
64'-0"	90° S.R. ELBOW	50		
59'-3"	90° L.R. ELBOW 5	20		100
2'-3 9/16"	45° STD. ELBOW 3	16		40
3'-3"	45° S.R. ELBOW	26		
	180° CLOSE RETURN	50		
	STD. TEE RUN	20		
	STD. TEE BRANCH	60		
	* MITRE BENDS	1.2 (1-cos $\theta$ )		
	* LATERAL $\searrow$ OUTLET	1.0		
	* LATERAL $\swarrow$ INLET	0.5		
	* STRAIGHT RUN LATERAL	0.15		
	* PIPE ENTR PROJ. INWD.	0.78		
	* " " SHARP EDGE	0.50		
	* " " WELL ROUND	0.04		
	* PIPE EXIT SHARP EDGE 1	1.0		
	* ORIFICE ( $C_D = .61$ )	2.69 RF/B <sup>4</sup>		
	* SUDDEN CONTRACTION +	.5(1-B <sup>2</sup> )		
	* SUDDEN INCREASE +	(1-B <sup>2</sup> ) <sup>2</sup>		
	* VALVE, MISCELLANEOUS	891.4 d <sup>4</sup> /C <sub>v</sub> <sup>2</sup>		
	MISC.			
ALS (6) 221.33			(7)	(8) 148

\* ITEMS ARE "K" VALUES ONLY

+ BASED ON SMALLER PIPE DIAMETER

B = d/D

RF = RECOVERY FACTOR

# PIPE FRICTION CALCULATION DATA SHEETS

NBSW 961021AF  
SHEET 9 OF 20  
PLANT COOR  
BY MC DATE 10/24/96

SYSTEM: CCP KPS IN CALC. UNIT: 2

PIPE SEGMENT TO & FROM: GROW SEPT TANKAGE TO REST PIT

DWG. REF.: 2-S-6

FLUID TEMP (°F): \_\_\_\_\_ PIPE ABS. ROUGHNESS (FT): \_\_\_\_\_ PIPE SEGMENT NUMBER: 1

① DESIGN FLOW: \_\_\_\_\_ ② MINIMUM FLOW: 1000 ③ MAXIMUM FLOW: 17000 ④ FLOW INCREMENT: 1000

⑤ PIPE I.D. (IN): 24" A-S 23.25 PIPE EL.: 585-17/16 TO EL.: 525-17/16

STRAIGHT PIPE LENGTHS      FITTINGS      NUMBER      \*K OR L/D       $\Sigma K$        $\Sigma L/D$

6' 0"	GATE VALVE	13		
	GLOBE VALVE	340		
	BUTTERFLY VALVE	40		
	SWING CHECK	135		
	90° STD. ELBOW	30		
	90° S.R. ELBOW	50		
	90° L.R. ELBOW	20		
	45° STD. ELBOW	16		
	45° S.R. ELBOW	26		
	180° CLOSE RETURN	50		
	STD. TEE RUN	20		20
	STD. TEE BRANCH	60		
	* MITRE BENDS	1.2 (1-cos $\theta$ )		
	* LATERAL $\searrow$ OUTLET	1.0		
	* LATERAL $\swarrow$ INLET	0.5		
	* STRAIGHT RUN LATERAL	0.15		
	* PIPE ENTR PROJ. INWD.	0.78		
	* " " SHARP EDGE	0.50		
	* " " WELL ROUND	0.04		
	* PIPE EXIT SHARP EDGE	1.0		
	* ORIFICE ( $C_d = .61$ )	2.69 RF/B <sup>4</sup>		
	* SUDDEN CONTRACTION +	.5(1-B <sup>2</sup> )		
	* SUDDEN INCREASE +	(1-B <sup>2</sup> ) <sup>2</sup>		
	* VALVE, MISCELLANEOUS	891.4 d <sup>4</sup> /C <sub>v</sub> <sup>2</sup>		
	MISC.			
⑥ 6			⑦	⑧ 20

\* ITEMS ARE "K" VALUES ONLY

B = d/D

RF = RECOVERY FACTOR

+ BASED ON SMALLER PIPE DIAMETER



# PIPE FRICTION CALCULATION DATA SHEETS

 NESH 961021AF  
 SHEET 10 OF 20  
 PLANT COOK  
 BY ME DATE 10/30/96
SYSTEM: CCP NASH CASEUNIT: 2PIPE SEGMENT TO & FROM: FROM EAST RT TO NASH PDS TANKSDWG. REF.: 2-S2-1FLUID TEMP (°F): \_\_\_\_\_ PIPE ABS. ROUGHNESS (FT): \_\_\_\_\_ PIPE SEGMENT NUMBER: 3DESIGN FLOW: \_\_\_\_\_ MINIMUM FLOW: 1000 MAXIMUM FLOW: 17000 FLOW INCREMENT: 1000PIPE I.D. (IN): 240 1.14 23.25 PIPE EL.: 585-7 1/4 TO EL.: 585-7 1/4

## STRAIGHT PIPE LENGTHS

## FITTINGS

## NUMBER

## \*K OR L/D

## Σ K

## Σ L/D

7' - 9 3/4'	GATE VALVE	13		
	GLOBE VALVE	340		
	BUTTERFLY VALVE	40		
	SWING CHECK	135		
	90° STD. ELBOW	30		
	90° S.R. ELBOW	50		
	90° L.R. ELBOW	20		
	45° STD. ELBOW	16		
	45° S.R. ELBOW	26		
	180° CLOSE RETURN	50		
	STD. TEE RUN	20		20
	STD. TEE BRANCH	60		
	* MITRE BENDS	1.2 (1-cosθ)		
	* LATERAL OUTLET	1.0		
	* LATERAL INLET	0.5		
	* STRAIGHT RUN LATERAL	0.15		
	* PIPE ENTR PROJ. INWD.	0.78		
	* " " SHARP EDGE	0.50		
	* " " WELL ROUND	0.04		
	* PIPE EXIT SHARP EDGE	1.0		
	* ORIFICE (C <sub>D</sub> = .61)	2.69 RF/B <sup>4</sup>		
	* SUDDEN CONTRACTION +	.5(1-B <sup>2</sup> )		
	* SUDDEN INCREASE +	(1- B <sup>2</sup> ) <sup>2</sup>		
	* VALVE, MISCELLANEOUS	891.4 d <sup>4</sup> /C <sub>v</sub> <sup>2</sup>		
	MISC.			
TOTALS	(6) 7.81		(7)	(8) 20

\* ITEMS ARE "K" VALUES ONLY

+ BASED ON SMALLER PIPE DIAMETER

B = d/D

RF = RECOVERY FACTOR



# PIPE FRICTION CALCULATION DATA SHEETS

 HSW 961021 AF  
 SHEET 11 OF 20  
 PLANT CCP  
 BY DE DATE 02/28/96
SYSTEM: CCP - 2014UNIT: 2PIPE SEGMENT TO & FROM: FROM PWR TAIL OFF TO CCP TAIL OFFDWG. REF.: 2-SI-6FLUID TEMP (°F): \_\_\_\_\_ PIPE ABS. ROUGHNESS (FT): \_\_\_\_\_ PIPE SEGMENT NUMBER: 4DESIGN FLOW: \_\_\_\_\_ MINIMUM FLOW: 1000 MAXIMUM FLOW: 8000 FLOW INCREMENT: 1000PIPE I.D. (IN): 34" A-S 23.25 PIPE EL: 585-1 1/16 TO EL: 585-1 7/16

## STRAIGHT PIPE LENGTHS

## FITTINGS

## NUMBER

## \*K OR L/D

## Σ K

## Σ L/D

6' - 4 1/4"	GATE VALVE	13		
	GLOBE VALVE	340		
	BUTTERFLY VALVE	40		
	SWING CHECK	135		
	90° STD. ELBOW	30		
	90° S.R. ELBOW	50		
	90° L.R. ELBOW	20		
	45° STD. ELBOW	16		
	45° S.R. ELBOW	26		
	180° CLOSE RETURN	50		
	STD. TEE RUN	20		20
	STD. TEE BRANCH	60		
	* MITRE BENDS	1.2 (1-cosθ)		
	* LATERAL OUTLET	1.0		
	* LATERAL INLET	0.5		
	* STRAIGHT RUN LATERAL	0.15		
	* PIPE ENTR PROJ. INWD.	0.78		
	* " " SHARP EDGE	0.50		
	* " " WELL ROUND	0.04		
	* PIPE EXIT SHARP EDGE	1.0		
	* ORIFICE (C <sub>d</sub> = .61)	2.69 RF/β <sup>4</sup>		
	* SUDDEN CONTRACTION +	.5(1-β <sup>2</sup> )		
	* SUDDEN INCREASE +	(1-β <sup>2</sup> ) <sup>2</sup>		
	* VALVE, MISCELLANEOUS	891.4 d <sup>4</sup> /C <sub>v</sub> <sup>2</sup>		
	MISC.			
TOTALS	⑥ 6.35		⑦	⑧

\* ITEMS ARE "K" VALUES ONLY

+ BASED ON SMALLER PIPE DIAMETER

β = d/D

RF = RECOVERY FACTOR



# PIPE FRICTION CALCULATION DATA SHEETS

 DESN 961021AF  
 SHEET 12 OF 20  
 PLANT COOK  
 BY AR DATE 10/28/96
SYSTEM: CLP NPSUNIT: 2PIPE SEGMENT TO & FROM: COOK CLP TO THE FAS TO TPC (JNU-910 911)DWG. REF.: 2-52-6, 2-52-43FLUID TEMP (°F): \_\_\_\_\_ PIPE ABS. ROUGHNESS (FT): \_\_\_\_\_ PIPE SEGMENT NUMBER: 5① DESIGN FLOW: \_\_\_\_\_ ② MINIMUM FLOW: 100 ③ MAXIMUM FLOW: 1300 ④ FLOW INCREMENT: 100⑤ PIPE I.D. (IN): 80 A-3 7.961 PIPE EL.: 585-17/16 TO EL.: 583-6

## STRAIGHT PIPE LENGTHS

## FITTINGS

## NUMBER

## \*K OR L/D

## Σ K

## Σ L/D

16"	GATE VALVE	13		
2'-9 1/16"	GLOBE VALVE	340		
10'-2"	BUTTERFLY VALVE	40		
	SWING CHECK	135		
	90° STD. ELBOW	30		
	90° S.R. ELBOW	50		70
	90° L.R. ELBOW	20		
	45° STD. ELBOW	16		
	45° S.R. ELBOW	26		
	180° CLOSE RETURN	50		
	STD. TEE RUN	20		
	STD. TEE BRANCH	60		60
	* MITRE BENDS	1.2 (1-cosθ)		
	* LATERAL > OUTLET	1.0		
	* LATERAL > INLET	0.5		
	* STRAIGHT RUN LATERAL	0.15		
	* PIPE ENTR PROJ. INWD.	0.78		
	* " " SHARP EDGE	0.50		
	* " " WELL ROUND	0.04		
	* PIPE EXIT SHARP EDGE	1.0		
	* ORIFICE (C <sub>D</sub> = .61)	2.69 RF/B <sup>4</sup>		
	* SUDDEN CONTRACTION + 8x24	.5(1-β <sup>2</sup> )	.44	
	* SUDDEN INCREASE +	(1-β <sup>2</sup> ) <sup>2</sup>		
	* VALVE, MISCELLANEOUS	891.4 d <sup>4</sup> /C <sub>v</sub> <sup>2</sup>		
	MISC.			
TOTALS ①	13.55		① .44	① 80

\* ITEMS ARE "K" VALUES ONLY

+ BASED ON SMALLER PIPE DIAMETER

B = d/D

RF = RECOVERY FACTOR

# PIPE FRICTION CALCULATION DATA SHEETS

DESIGN 1021A  
SHEET 13 OF 20  
PLANT CORR  
BY AD DATE 12/24/96

SYSTEM: CCP NORTH UNIT: 2

PIPE SEGMENT TO & FROM: FROM TEE TO TEE TAP TWO-910

DWG. REF.: 2-S-413

FLUID TEMP (°F): \_\_\_\_\_ PIPE ABS. ROUGHNESS (FT): \_\_\_\_\_ PIPE SEGMENT NUMBER: 6

DESIGN FLOW: \_\_\_\_\_ MINIMUM FLOW: 100 MAXIMUM FLOW: 1300 FLOW INCREMENT: 100

PIPE I.D. (IN): 50 A-3 7.981 PIPE EL.: 588-6 TO EL.: 588-6

STRAIGHT PIPE LENGTHS      FITTINGS      NUMBER      \*K OR L/D      Σ K      Σ L/D

15"	GATE VALVE TWO-910	13			13
16"	GLOBE VALVE	340			
12"	BUTTERFLY VALVE	40			
4'-6"	SWING CHECK	135			
	90° STD. ELBOW	30			
	90° S.R. ELBOW	50			
	90° L.R. ELBOW	20			20
	45° STD. ELBOW	16			
	45° S.R. ELBOW	26			
	180° CLOSE RETURN	50			
	STD. TEE RUN	20			20
	STD. TEE BRANCH	60			
	* MITRE BENDS	1.2 (1-cosθ)			
	* LATERAL OUTLET	1.0			
	* LATERAL INLET	0.5			
	* STRAIGHT RUN LATERAL	0.15			
	* PIPE ENTR PROJ. INWD.	0.78			
	* " " SHARP EDGE	0.50			
	* " " WELL ROUND	0.04			
	* PIPE EXIT SHARP EDGE	1.0			
	* ORIFICE (C <sub>D</sub> = .61)	2.69 RF/B <sup>4</sup>			
	* SUDDEN CONTRACTION +	.5(1-B <sup>2</sup> )			
	* SUDDEN INCREASE +	(1-B <sup>2</sup> ) <sup>2</sup>			
	* VALVE, MISCELLANEOUS	891.4 d <sup>4</sup> /C <sub>v</sub> <sup>2</sup>			
	MISC.				
Σ				0	53

\* ITEMS ARE "K" VALUES ONLY      + BASED ON SMALLER PIPE DIAMETER  
B = d/D      RF = RECOVERY FACTOR



# PIPE FRICTION CALCULATION DATA SHEETS

 HSDN 9610 21AF  
 SHEET 14 OF 20  
 PLANT COOL  
 BY LR DATE 01/30/96

 SYSTEM: ECP NPS 12 COOL UNIT: Z

 PIPE SEGMENT TO & FROM: FROM TEE TO TEE THRU IM-911

 DWG. REF.: 2-SI-43

 FLUID TEMP (°F):          PIPE ABS. ROUGHNESS (FT):          PIPE SEGMENT NUMBER: 7

 ① DESIGN FLOW:          ② MINIMUM FLOW: 100 ③ MAXIMUM FLOW: 1300 ④ FLOW INCREMENT: 100

 ⑤ PIPE I.D. (IN): 20 A-3 7.981 PIPE EL.: 588-6 TO EL.: 588-6

 STRAIGHT PIPE LENGTHS      FITTINGS      NUMBER      \*K OR L/D       $\Sigma K$        $\Sigma L/D$ 

4-6	GATE VALVE IM-911	13		13
12"	GLOBE VALVE	340		
16"	BUTTERFLY VALVE	40		
12"	SWING CHECK	135		
	90° STD. ELBOW	30		
	90° S.R. ELBOW	50		
	90° L.R. ELBOW	/ 20		70
	45° STD. ELBOW	16		
	45° S.R. ELBOW	26		
	180° CLOSE RETURN	50		
	STD. TEE RUN	20		60
	STD. TEE BRANCH	/ 60		
	* MITRE BENDS	1.2 (1-cos $\theta$ )		
	* LATERAL $\searrow$ OUTLET	1.0		
	* LATERAL $\swarrow$ INLET	0.5		
	* STRAIGHT RUN LATERAL	0.15		
	* PIPE ENTR PROJ. INWD.	0.78		
	* " " SHARP EDGE	0.50		
	* " " WELL ROUND	0.04		
	* PIPE EXIT SHARP EDGE	1.0		
	* ORIFICE ( $C_D = .61$ )	2.69 RF/B <sup>3</sup>		
	* SUDDEN CONTRACTION +	.5(1-B <sup>2</sup> )		
	* SUDDEN INCREASE +	(1-B <sup>2</sup> ) <sup>2</sup>		
	* VALVE, MISCELLANEOUS	891.4 d <sup>4</sup> /C <sub>v</sub> <sup>2</sup>		
	MISC.			
TOTALS ⑥ 8			⑦ 0	⑧ 93

\* ITEMS ARE "K" VALUES ONLY

+ BASED ON SMALLER PIPE DIAMETER

B = d/D

RF = RECOVERY FACTOR



Rev. 5/94

# PIPE FRICTION CALCULATION DATA SHEETS

 DES 9610 2142  
 SHEET 15 OF 20  
 PLANT CORC  
 BY AP DATE 01/20/96

 SYSTEM : CCP UPS HX UNIT : 2

 PIPE SEGMENT TO & FROM : FROM TEE TO TEE




 DWG. REF. : 2-37-43 2-63-79

 FLUID TEMP (°F) : \_\_\_\_\_ PIPE ABS. ROUGHNESS (FT) : \_\_\_\_\_ PIPE SEGMENT NUMBER : 8

 DESIGN FLOW : \_\_\_\_\_ MINIMUM FLOW : 100 MAXIMUM FLOW : 1300 FLOW INCREMENT : 100

 PIPE I.D. (IN) : 8" A-3 7.981 PIPE EL. : 588-6 TO EL. : 596-4 5/16

 STRAIGHT PIPE LENGTHS      FITTINGS      NUMBER      \*K OR L/D       $\Sigma K$        $\Sigma L/D$ 

19"	GATE VALVE	13		
7' 10 5/16	GLOBE VALVE	340		
2'	BUTTERFLY VALVE	40		
18" 	SWING CHECK 15" C B O 8 C S	135		135
	90° STD. ELBOW	30		
	90° S.R. ELBOW	50		
	90° L.R. ELBOW	20		20
	45° STD. ELBOW	16		
	45° S.R. ELBOW	26		
	180° CLOSE RETURN	50		
	STD. TEE RUN	20		20
	STD. TEE BRANCH	60		20
	* MITRE BENDS	1.2 (1-cos $\theta$ )		
	* LATERAL  OUTLET	1.0		
	* LATERAL  INLET	0.5		
	* STRAIGHT RUN LATERAL	0.15		
	* PIPE ENTR PROJ. INWD.	0.78		
	* " " SHARP EDGE	0.50		
	* " " WELL ROUND	0.04		
	* PIPE EXIT SHARP EDGE	1.0		
	* ORIFICE (C <sub>D</sub> = .61)	2.69 RF/B <sup>4</sup>		
	* SUDDEN CONTRACTION +	.5(1-B <sup>2</sup> )		
	* SUDDEN INCREASE +	(1-B <sup>2</sup> ) <sup>2</sup>		
	* VALVE, MISCELLANEOUS	891.4 d <sup>4</sup> /Q <sub>v</sub> <sup>2</sup>		
	MISC.			
12.94				235

\* ITEMS ARE "K" VALUES ONLY

+ BASED ON SMALLER PIPE DIAMETER

B = d/D

RF = RECOVERY FACTOR

# PIPE FRICTION CALCULATION DATA SHEETS

 VBRM 961021AR  
 SHEET 16 OF 20  
 PLANT COOL  
 BY LC DATE 10/30/06
SYSTEM: CCP NDSHUNIT: 2PIPE SEGMENT TO & FROM: FROM TOP TO "E" CCP TAKEOFFDWG. REF.: 2-LS-79FLUID TEMP (°F): \_\_\_\_\_ PIPE ABS. ROUGHNESS (FT): \_\_\_\_\_ PIPE SEGMENT NUMBER: 9① DESIGN FLOW: \_\_\_\_\_ ② MINIMUM FLOW: 100 ③ MAXIMUM FLOW: 1300 ④ FLOW INCREMENT: 100⑤ PIPE I.D. (IN): 5" A-3 7.981 PIPE EL.: 596-4 5/16 TO EL.: 596-4 5/16

## STRAIGHT PIPE LENGTHS

## FITTINGS

## NUMBER

## \*K OR L/D

## Σ K

## Σ L/D

14"	GATE VALVE	13		
	GLOBE VALVE	340		
	BUTTERFLY VALVE	40		
	SWING CHECK	135		
	90° STD. ELBOW	30		
	90° S.R. ELBOW	50		
	90° L.R. ELBOW	20		
	45° STD. ELBOW	16		
	45° S.R. ELBOW	26		
	180° CLOSE RETURN	50		
	STD. TEE RUN	20		
	STD. TEE BRANCH	60		60
	* MITRE BENDS	1.2 (1-cosθ)		
	* LATERAL > OUTLET	1.0		
	* LATERAL > INLET	0.5		
	* STRAIGHT RUN LATERAL	0.15		
	* PIPE ENTR PROJ. INWD.	0.78		
	* " " SHARP EDGE	0.50		
	* " " WELL ROUND	0.04		
	* PIPE EXIT SHARP EDGE	1.0		
	* ORIFICE (C <sub>D</sub> = .61)	2.69 RF/β <sup>4</sup>		
	* SUDDEN CONTRACTION +	.5(1-β <sup>2</sup> )		
	* SUDDEN INCREASE +	(1-β <sup>2</sup> ) <sup>2</sup>		
	* VALVE, MISCELLANEOUS	891.4 d <sup>4</sup> /C <sub>v</sub> <sup>2</sup>		
	MISC.			
ALS ⑤ 1.2			⑦	⑧ 60

\* ITEMS ARE "K" VALUES ONLY

+ BASED ON SMALLER PIPE DIAMETER

B = d/D

RF = RECOVERY FACTOR



# PIPE FRICTION CALCULATION DATA SHEETS

 USS-961021AR  
 SHEET 17 OF 20  
 PLANT Con  
 BY br DATE 10/20/96
SYSTEM: CCP NPS-4UNIT: 2PIPE SEGMENT TO & FROM: FROM "E" CCP TAKEOFF TO "2" CCP SUCT. INDWG. REF.: 2-CS-79 2-CS-80FLUID TEMP (°F): \_\_\_\_\_ PIPE ABS. ROUGHNESS (FT): \_\_\_\_\_ PIPE SEGMENT NUMBER: 10① DESIGN FLOW: \_\_\_\_\_ ② MINIMUM FLOW: 100 ③ MAXIMUM FLOW: 700 ④ FLOW INCREMENT: 100⑤ PIPE I.D. (IN): 6" Ø 8-14 6.065 PIPE EL.: 596-4 1/16 TO EL.: 592-6

## STRAIGHT PIPE LENGTHS

## FITTINGS

## NUMBER

## \*K OR L/D

## Σ K

## Σ L/D

10.3"	GATE VALVE 156506SS	13		13
5' 10 3/4"	GLOBE VALVE	340		
6' 5"	BUTTERFLY VALVE	40		
4.8'	SWING CHECK	135		
12 5/8"	90° STD. ELBOW	30		
	90° S.R. ELBOW	50		
	90° L.R. ELBOW	20	3	60
	45° STD. ELBOW	16		
	45° S.R. ELBOW	26		
	180° CLOSE RETURN	50		
	STD. TEE RUN	20		
	STD. TEE BRANCH	60	1	60
	* MITRE BENDS	1.2 (1-cosθ)		
	* LATERAL > OUTLET	1.0		
	* LATERAL > INLET	0.5		
	* STRAIGHT RUN LATERAL	0.15		
	* PIPE ENTR PROJ. INWD.	0.78		
	* " " SHARP EDGE	0.50		
	* " " WELL ROUND	0.04		
	* PIPE EXIT SHARP EDGE	1.0		
	* ORIFICE (C <sub>D</sub> = .61)	2.69 RF/B <sup>4</sup>		
	* SUDDEN CONTRACTION +	.5(1-β <sup>2</sup> )		
	* SUDDEN INCREASE +	(1-β <sup>2</sup> ) <sup>2</sup>		
	* VALVE, MISCELLANEOUS	891.4 d <sup>4</sup> /C <sub>v</sub> <sup>2</sup>		
	MISC.			
⑥ 19			⑦ 0	⑧ 133

\* ITEMS ARE "K" VALUES ONLY

+ BASED ON SMALLER PIPE DIAMETER

B = d/D

RF = RECOVERY FACTOR

# PIPE FRICTION CALCULATION DATA SHEETS

NESU 961021AF  
 SHEET 18 OF 20  
 PLANT COOK  
 BY AE DATE 10/30/96

SYSTEM: CCP - DS -UNIT: 2PIPE SEGMENT TO & FROM: FROM "S" CCP TAKE OFF TO VAL - XTIEDWG. REF.: 2-C5-79FLUID TEMP (°F): \_\_\_\_\_ PIPE ABS. ROUGHNESS (FT): \_\_\_\_\_ PIPE SEGMENT NUMBER: 18DESIGN FLOW: \_\_\_\_\_ MINIMUM FLOW: 100 MAXIMUM FLOW: 700 FLOW INCREMENT: 100PIPE I.D. (IN): 8" A-3 7.981 PIPE EL: 596-4 5/16 TO EL: 596-4 5/16

## STRAIGHT PIPE LENGTHS

## FITTINGS

## NUMBER

## \*K OR L/D

## Σ K

## Σ L/D

<u>15'-11 1/2"</u>	GATE VALVE		13		
	GLOBE VALVE		340		
	BUTTERFLY VALVE		40		
	SWING CHECK		135		
	90° STD. ELBOW		30		
	90° S.R. ELBOW		50		
	90° L.R. ELBOW		20		
	45° STD. ELBOW	<u>2</u>	16		<u>72</u>
	45° S.R. ELBOW		26		
	180° CLOSE RETURN		50		
	STD. TEE RUN	<u>1</u>	20		<u>70</u>
	STD. TEE BRANCH		60		
	* MITRE BENDS		1.2 (1-cosθ)		
	* LATERAL OUTLET		1.0		
	* LATERAL INLET		0.5		
	* STRAIGHT RUN LATERAL		0.15		
	* PIPE ENTR PROJ. INWD.		0.78		
	* " " SHARP EDGE		0.50		
	* " " WELL ROUND		0.04		
	* PIPE EXIT SHARP EDGE		1.0		
	* ORIFICE (C <sub>D</sub> = .61)		2.69 RF/B <sup>4</sup>		
	* SUDDEN CONTRACTION +		.5(1-B <sup>2</sup> )		
	* SUDDEN INCREASE +		(1-B <sup>2</sup> ) <sup>2</sup>		
	* VALVE, MISCELLANEOUS		891.4 d <sup>4</sup> /C <sub>v</sub> <sup>2</sup>		
	MISC.				
Σ				<u>0</u>	<u>52</u>

\* ITEMS ARE "K" VALUES ONLY

+ BASED ON SMALLER PIPE DIAMETER

B = d/D

RF = RECOVERY FACTOR

# PIPE FRICTION CALCULATION DATA SHEETS

 N554-96021AF  
 SHEET 19 OF 20  
 PLANT CORSE  
 BY RF DATE 04/3/96
SYSTEM: CCP NPS 14UNIT: 2PIPE SEGMENT TO & FROM: FROM UNIT 11F TO WCCP TAP OFFDWG. REF.: 2-CC-79FLUID TEMP (°F): \_\_\_\_\_ PIPE ABS. ROUGHNESS (FT): \_\_\_\_\_ PIPE SEGMENT NUMBER: 12① DESIGN FLOW: \_\_\_\_\_ ② MINIMUM FLOW: 100 ③ MAXIMUM FLOW: 700 ④ FLOW INCREMENT: 100⑤ PIPE I.D. (IN): 6.065 PIPE EL.: 596-4 5/16 TO EL.: 597-5 1/16
 STRAIGHT PIPE LENGTHS      FITTINGS      NUMBER      \*K OR L/D       $\Sigma K$        $\Sigma L/D$ 

2' - 2 1/2"	GATE VALVE	13		
	GLOBE VALVE	340		
10' - 6"	BUTTERFLY VALVE	40		
	SWING CHECK	135		
	90° STD. ELBOW	30		
	90° S.R. ELBOW	50		
	90° L.R. ELBOW	20		
	45° STD. ELBOW	16		
	45° S.R. ELBOW	26		
	180° CLOSE RETURN	50		
	STD. TEE RUN	20		20
	STD. TEE BRANCH	60		
	* MITRE BENDS	1.2 (1-cos $\theta$ )		
	* LATERAL $\curvearrowright$ OUTLET	1.0		
	* LATERAL $\curvearrowright$ INLET	0.5		
	* STRAIGHT RUN LATERAL	0.15		
	* PIPE ENTR PROJ. INWD.	0.78		
	* " " SHARP EDGE	0.50		
	* " " WELL ROUND	0.04		
	* PIPE EXIT SHARP EDGE	1.0		
	* ORIFICE ( $C_D = .61$ )	2.69 RF/B <sup>4</sup>		
	* SUDDEN CONTRACTION + 6x8	.5(1-B <sup>2</sup> )	2188	
	* SUDDEN INCREASE +	(1-B <sup>2</sup> ) <sup>2</sup>		
	* VALVE, MISCELLANEOUS	891.4 d <sup>4</sup> /Q <sub>v</sub> <sup>2</sup>		
	MISC.			
⑤ 12.71			⑤ 2188	⑤ 20

\* ITEMS ARE "K" VALUES ONLY

B = d/D

RF = RECOVERY FACTOR

+ BASED ON SMALLER PIPE DIAMETER

# PIPE FRICTION CALCULATION DATA SHEETS

 DES 961021 AF  
 SHEET 20 OF 20  
 PLANT CCRG  
 BY PC DATE 12/2/96

 SYSTEM: CCP MPS 14 UNIT: 2

 PIPE SEGMENT TO & FROM: CR. T. N. CCP TOWER TO W CCP SUB. ST.

 DWG. REF.: 2-C3-79 2-C3-81

 FLUID TEMP (°F): \_\_\_\_\_ PIPE ABS. ROUGHNESS (FT): \_\_\_\_\_ PIPE SEGMENT NUMBER: 13

 ① DESIGN FLOW: \_\_\_\_\_ ② MINIMUM FLOW: 100 ③ MAXIMUM FLOW: 700 ④ FLOW INCREMENT: 100

 ⑤ PIPE I.D. (IN): 60 A.3 6.065 PIPE EL.: 597.5/16 TO EL.: 592-0

STRAIGHT PIPE LENGTHS      FITTINGS      NUMBER      \*K OR L/D      Σ K      Σ L/D

3'-6"	GATE VALVE 15" 6, 12, 16, 20	13			13
4'-0"	GLOBE VALVE	340			
12'-5/8"	BUTTERFLY VALVE	40			
	SWING CHECK	135			
	90° STD. ELBOW	30			
	90° S.R. ELBOW	50			
	90° L.R. ELBOW	20			40
	45° STD. ELBOW	16			
	45° S.R. ELBOW	26			
	180° CLOSE RETURN	50			
	STD. TEE RUN	20			
	STD. TEE BRANCH	60			60
	* MITRE BENDS	1.2 (1-cosθ)			
	* LATERAL OUTLET	1.0			
	* LATERAL INLET	0.5			
	* STRAIGHT RUN LATERAL	0.15			
	* PIPE ENTR PROJ. INWD.	0.78			
	* " " SHARP EDGE	0.50			
	* " " WELL ROUND	0.04			
	* PIPE EXIT SHARP EDGE	1.0			
	* ORIFICE (C <sub>D</sub> = .61)	2.69 RF/B <sup>4</sup>			
	* SUDDEN CONTRACTION +	.5(1-β <sup>2</sup> )			
	* SUDDEN INCREASE +	(1-β <sup>2</sup> ) <sup>2</sup>			
	* VALVE, MISCELLANEOUS	891.4 d <sup>4</sup> /C <sub>v</sub> <sup>2</sup>			
	MISC.				
ALS ⑥ 9.35				⑦	⑧ 113

\* ITEMS ARE "K" VALUES ONLY

+ BASED ON SMALLER PIPE DIAMETER

B = d/D

RF = RECOVERY FACTOR

DONALD C. COOK NUCLEAR PLANT

NESM \_\_\_\_\_ Section

DESIGN VERIFICATION CHECKLIST - CALCULATIONS

Calculation Number NESM961021AF

Rev. 0

John J. Ribak  
Signature of Verifier

11/27/96  
Date

1.0 Were the inputs correctly selected, incorporated and documented into the calculation? Yes ☒ N/A ☐

Basis: The inputs are consistent with the analysis used for this calculation

2.0 Are assumptions necessary to perform the calculation adequately described and reasonable? Yes ☒ N/A ☐

Basis: The assumptions are appropriate and their basis is well defined.

3.0 Are the applicable codes, standards and regulatory requirements identified and requirements for design met? Yes ☐ N/A ☒

Basis: There are no codes, standards or regulatory requirements applicable to this calculation

4.0 Was an appropriate design method used? Yes ☐ N/A ☒

Basis: This is not a design process

5.0 Is the output reasonable compared to input? Yes ☒ N/A ☐

Basis: The outputs are consistent w/ the inputs.

6.0 Are the results numerically correct? Yes ☒ N/A ☐

Basis: Arithmetic check of inputs and calc.