

Attachment to AEP:NRC:1018A

Proposed Revised Technical Specification Changes

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POWER DISTRIBUTION LIMITS

SURVEILLANCE REQUIREMENTS (Continued)

where

$$F_Q^M(Z) - F_Q(Z, \ell) \quad \text{at } \ell \text{ for which}$$

$$\frac{F_Q(Z, \ell)}{T(E_\ell)} \quad \text{is a maximum}$$

$$F_Q^L(Z) - F_Q^L(E_\ell) \quad \text{at } \ell, \text{ for which}$$

$$\frac{F_Q(Z, \ell)}{T(E_\ell)} \quad \text{is a maximum}$$

$F_Q^M(Z)$ and $F_Q^L(Z)$ are functions of core height, Z , and correspond at each $\frac{F_Q(Z, \ell)}{T(E_\ell)}$

Z to the rod ℓ for which $T(E_\ell)$ is a maximum at that Z

$V(Z)$ is a cycle dependent function and is provided in the Peaking Factor Limit Report. $K(Z)$ is defined in Figure 3.2-2 for Exxon Nuclear Company fuel and in Figure 3.2-3 for Westinghouse fuel. $T(E_\ell)$ is defined in Figures 3.2-4 and 3.2-5. $E_p(Z)$ is an uncertainty factor to account for the reduction in the $F_Q^L(E_\ell)$ curve due to accumulation of exposure prior to the next flux map.

Westinghouse Fuel

Exxon Nuclear Co. Fuel

$$E_p(Z) = 1.0$$

$$E_p(Z) = 1.0$$

$$0.0 \leq E_\ell \leq 17.62$$

$$E_p(Z) = 1.0$$

$$E_p(Z) = 1.0 + [.0040 \times F_Q^M(Z)]$$

$$17.62 < E_\ell \leq 34.5$$

$$E_p(Z) = 1.0$$

$$E_p(Z) = 1.0 + [.0093 \times F_Q^M(Z)]$$

$$34.5 < E_\ell \leq 42.2$$

$$E_p(Z) = 1.0 + [.0060 \times F_Q^M(Z)]$$

$$42.2 < E_\ell \leq 48.0$$

$$E_p(Z) = 1.0$$

$$48.0 < E_\ell \leq 48.7$$

POWER DISTRIBUTION LIMITS

LIMITING CONDITION FOR OPERATION (Continued)

<u>Westinghouse Fuel</u>	<u>ENC Fuel</u>	
$F_P = 1.0$	$F_P = 1.0$	$0.0 \leq E_\ell \leq 17.62$
$F_P = 1.0$	$F_P = 1.0 + [.0015 \times W]$	$17.62 < E_\ell \leq 34.5$
$F_P = 1.0$	$F_P = 1.0 + [.0033 \times W]$	$34.5 < E_\ell \leq 42.2$
	$F_P = 1.0 + [.0020 \times W]$	$42.2 < E_\ell \leq 48.0$
	$F_P = 1.0$	$48.0 < E_\ell \leq 48.7$

where W is the number of effective full power weeks (rounded up to the next highest integer) since the last full core flux map.

APPLICABILITY: MODE 1 above the minimum percent of RATED THERMAL POWER indicated by the relationships.*

$$\text{APL} = \min \text{ over } Z \text{ of } \frac{2.10 \times K(Z)}{F_Q(Z, \ell) \times V(Z)} \times 100\% \quad \text{Westinghouse Fuel}$$

$$\text{APL} = \min \text{ over } Z \text{ of } \frac{F_Q^L(E_\ell) \times K(Z)}{F_Q(Z, \ell) \times V(Z) \times E_P(Z)} \times 100\% \quad \text{Exxon Nuclear Co. Fuel}$$

where $F_Q(Z, \ell)$ is the measured $F_Q(Z, \ell)$, including a 3% manufacturing tolerance uncertainty and a 5% measurement uncertainty, at the time of target flux determination from a power distribution map using the movable incore detectors. $V(Z)$ is the function given in the Peaking Factor Limit Report. The above limit is not applicable in the following core plane regions.

1. Lower core region 0% to 10% inclusive.
2. Upper core region 90% to 100% inclusive.

* The APDMS may be out of service when surveillance for determining power distribution maps is being performed.

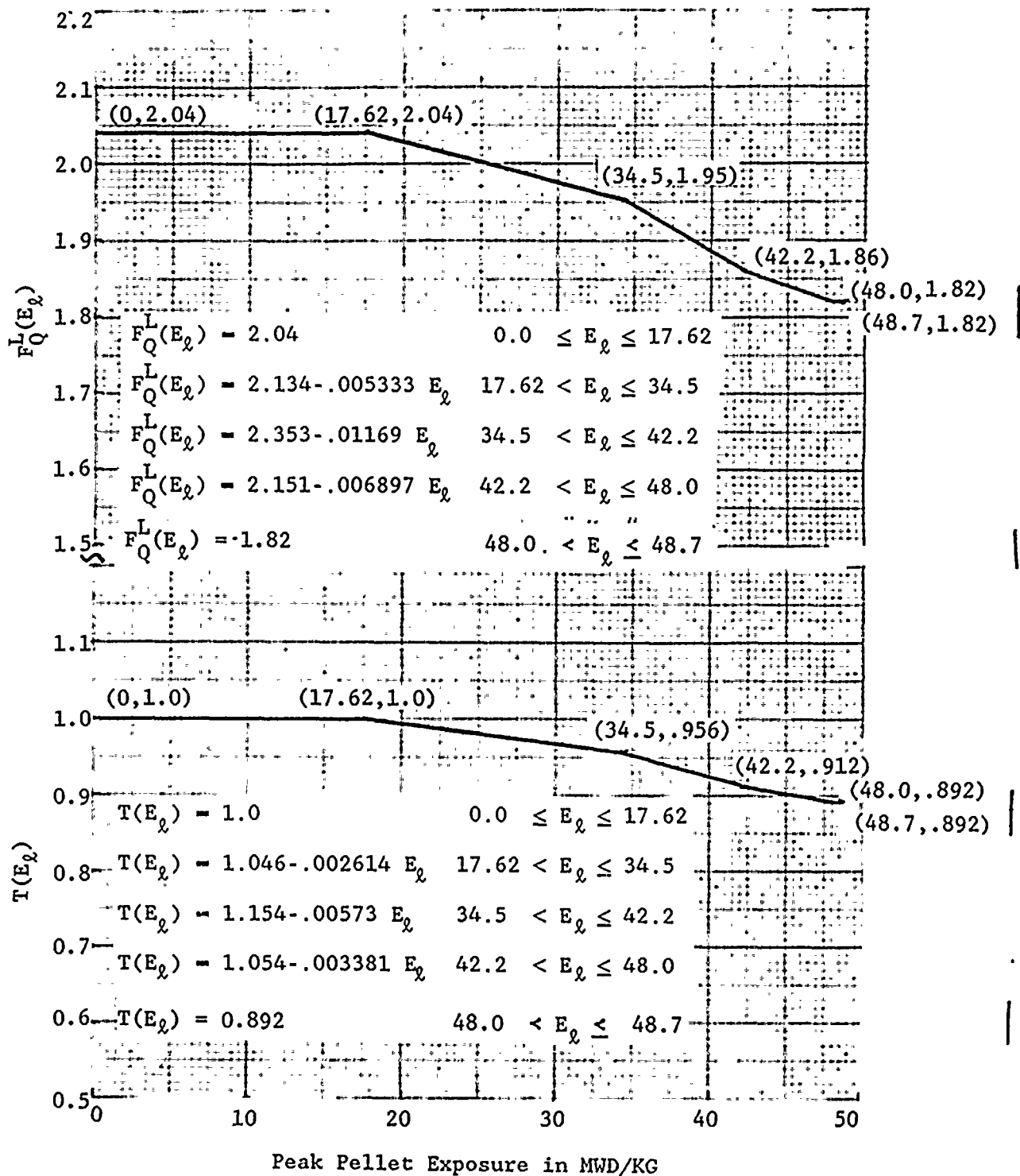


FIGURE 3.2-4
Exposure Dependent F_Q^L Limit, $F_Q^L(E_L)$, and Normalized Limit $T(E_L)$ as a function of Peak Pellet Burnup for Exxon Nuclear Company Fuel