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 RECIP. NAME RECIPIENT AFFILIATION
 KNIGHTON, G. Licensing Branch 3

SUBJECT: Forwards responds to Questions 640.01, 640.02 & 640.03 re procedure generation package.

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Arizona Public Service Company

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PDR ADDCK 05000528
A PDR

January 10, 1984
ANPP 28584-WFQ/TFQ

Director of Nuclear Reactor Regulation
Attention: Mr. George Knighton, Chief
Licensing Branch No. 3
Division of Licensing
U.S. Nuclear Regulatory Commission
Washington, D.C. 20555

Subject: Palo Verde Nuclear Generating Station (PVNGS)
Units 1, 2 and 3
Docket Nos. STN-50-528/529/530
File: 84-056-026; G.1.01.10

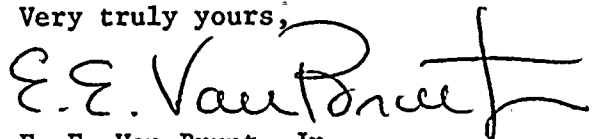
Reference: Letter from G. W. Knighton, NRC, to E. E. Van Brunt, Jr.,
APS, dated November 8, 1983.

Dear Mr. Knighton:

Attached for your review are APS' responses to questions transmitted by
the referenced letter. These questions, 640.01 640.02 and 640.03, are in
regard and to the PVNGS Procedure Generation Package.

Please contact me if you have any further questions on this matter.

Very truly yours,



E. E. Van Brunt, Jr.
APS Vice President
Nuclear Projects Management
ANPP Project Director

EEVB/TFQ/sp
Attachment

cc: E. A. Licitra (w/a)
A. C. Gehr "

Boo1
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11-11-61

1

1. The first part of the report
describes the general situation
of the country and the
state of the economy.

2. The second part of the report

describes the situation in the
different regions of the country.

3. The third part of the report
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different sectors of the economy.

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describes the situation in the
different sectors of the economy.

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describes the situation in the
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describes the situation in the
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STATE OF ARIZONA)
) ss.
COUNTY OF MARICOPA)

I, Edwin E. Van Brunt, Jr., represent that I am Vice President, Nuclear Projects of Arizona Public Service Company, that the foregoing document has been signed by me on behalf of Arizona Public Service Company with full authority to do so, that I have read such document and know its contents, and that to the best of my knowledge and belief, the statements made therein are true.

Edwin E. Van Brunt, Jr.
Edwin E. Van Brunt, Jr.

Sworn to before me this 9th day of January, 1984.

Nora E. Meador
Notary Public

My Commission Expires:

My Commission Expires April 6, 1987



640.01

On page 12 of Section III of PVNGS PGP, it states that CEN-152 LOCA Guidelines were broken down into two PVNGS documents, one for small LOCA and one for large LOCA. The reason given by PVNGS for developing specific guidelines for a small LOCA and a large LOCA is that the actions for the two are significantly different. A large LOCA is defined as a LOCA which raises the containment pressure to 5 psig or greater. A LOCA which does not raise the containment pressure above 5 psig is designated as a small LOCA.

Our concern is that the operator could be directed to the incorrect procedure if the 5 psig criterion is not valid. We request that you provide (1) or (2) below:

- (1) A discussion that justifies the adequacy of using the PVNGS large LOCA guideline for a small LOCA, and vice versa, in terms of the effect of omitting steps required in one guideline and not the other.
- (2) An analysis that supports using the large LOCA guidelines for containment pressure 5 psig and greater, and using the small LOCA guidelines for containment pressure less than 5 psig. Also, provide a detailed discussion of the model and assumptions used in the analysis for the primary systems, secondary system and containment.

640.01 Response

If the operator uses the small break LOCA procedure in a large LOCA situation, sufficient second checks are incorporated into the procedure to direct the operator to the proper (large LOCA) procedure. This ensures the actions required during a large LOCA are performed. These checks include the following:

- Step 3.0 - If 800 psia primary pressure is encountered within 15 minutes of SI proceed to large LOCA procedure.
- Step 9.0 - If a RAS signal is generated proceed to large LOCA procedure.
- Step 22.3- If the plant is incapable of supporting 538 psia, SDC criteria, proceed to large LOCA procedure.

The checks are based on FSAR Analysis and indicated that an inadequate RCS inventory is available to provide core cooling. The steps from CEN-152 that are identified in the Technical Guidelines as not incorporated (section III, page 199), affect this procedure as follows:

- Step 30 & 31 - These steps describe actions to be taken upon receipt of a RAS signal. They are omitted from the small LOCA procedure because a RAS signal is not anticipated in a small LOCA condition. If a RAS is received, step 7.0 of the small LOCA procedure will direct the operator to the procedure for a large LOCA that includes instructions for a RAS. This insures proper operation for plant conditions.
- Step 23 & 35 - These describe actions to reset and bypass the MSIS setpoint during cooldown. These are omitted from the small LOCA procedure because they are provided in the plant cooldown procedure and this referenced in the small LOCA procedure.
- Step 37 - 44 - These steps concern shutdown cooling, SIT operations and LTOP. These direct plant cooldown and address shutdown cooling, SIT isolation and LTOP protection as plant conditions warrant alterations in these systems. The small LOCA procedure provides guidance to the operator with special consideration for plant cooldown with a LOCA situation.

If, the operator implemented the large break LOCA procedure in a small LOCA situation, the large LOCA procedure provides the operator with sufficient guidance in both procedures for maintaining adequate core

640.02

In the PVNGS guidelines for the LOCA, step.22. on page 169 isolates the safety injection tanks (SIT) regardless of the pressure in the RCS. The CE guideline, CEN-152, requires that the SIT be isolated at a specific RCS pressure. The typical RCS pressure given in CEN-152 is 250 psia. To justify the removal of the pressure restrictions on the SIT isolation, provide the following:

- (1) Demonstrate over a spectrum of large breaks that the effect of injecting a noncondensable gas (nitrogen) into the primary system is negligible.
- (2) Show that premature SIT isolation is not likely, or provide an analysis (considering a range of large breaks) that shows that the effect of prematurely isolating the SIT is not a safety concern.

640.02 Response:

The original DRAFT of CEN-152 did not identify any criteria for SIT Isolation other than time. Rev-1 of CEN-152 identifies RCS/SIT pressure as the criteria for isolating SIT. PVNGS will establish SIT isolation criteria to prevent premature SIT isolation. This criteria will then be incorporated into the Technical Guidelines and Recovery Procedures by the time the procedures are issued.

640.03

In the PVNGS Plant Specific Guideline, the safety functions as defined by PVNGS differ from CEN-152 in that RCS inventory and RCS pressure control have been combined and all safety functions dealing with containment have been combined. This change affects the safety function status check, Figure 10-3 in CEN-152, the resource assessment trees, and the specific function recovery guidelines for RCS inventory control, RCS pressure control, containment isolation, containment temperature and pressure, and containment combustible gas control. Provide sufficient information to show that the function recovery guidelines have been combined in such a manner that they reflect CEN-152 generic guidelines, or provide the technical basis, including supporting analysis, for the differences from the generic guidelines.

Upon event initiation the operators are directed to maintain safety functions. These actions are outlined in the form of primary and secondary operator flow charts Figures 1 and 2, which defines the criteria to be met to insure functions are maintained. The criteria outlined in CEN-152 Figure 10-3 is the same criteria utilized during performance of the steps of the flow charts, with the following exceptions:

- Due to plant specific design T_c is used vice T_{AVE} ; CET readings are addressed, first by maintaining subcooling, then specific readings are taken in all Recovery Procedures.
- CET readings are one of the criteria used to maintain adequate core cooling. CET readings are taken during plant statusing at various points in the Recovery Procedures.
- H_2 control is addressed in the LOCA and Functional Recovery Procedures as plant conditions warrant.

These flow charts, do not identify or name the Safety Function to be monitored, but prescribe the criteria to be verified or established, as the preferred method of stabilizing plant parameters. This method is also used as a second check of parameters and criteria by the Supervisor while performing the steps of the diagnostic flow charts. These flow charts are not dependent on how the safety functions are defined but directly address the basic criteria which will indicate the status of the safety functions. This method allows for a symptomatic approach to accident mitigation. If diagnosis is not possible the Functional Recovery Procedure will be implemented. The criteria for evaluating plan response in the Functional Recovery Procedure is identical to the criteria listed in CEN-152, Figure 10-3. When any of these criteria cannot be met the appropriate actions will be directed. This method does define which safety function is to be monitored. However, where the safety functions, as defined by CE, have been combined the criteria for verifying those safety functions have also been combined. Operator actions are then directed based on this criteria.

FIGURE 10-3 SAFETY FUNCTION STATUS CHECK

THE SAFETY FUNCTIONS LISTED BELOW AND THEIR RESPECTIVE CRITERIA ARE THOSE USED TO CONFIRM THE ADEQUACY OF THE EVENTS' MITIGATION. ADDITIONAL SAFETY FUNCTIONS SHOULD BE MONITORED AS APPROPRIATE TO EVALUATE OVERALL PLANT STATUS

SAFETY FUNCTION	SUCCESS PATH CURRENTLY IN USE	CRITERIA	IF CRITERIA NOT MET IMPLIES PLANT CONDITIONS	RESOURCE TREE
1. REACTIVITY CONTROL	1A CEA TRIP	1a NO MORE THAN 3 CEA BOTTOM LIGHT NOT LIT AND RX POWER DECREASING	RX NOT SHUTDOWN AND EXCESSIVE HEAT PRODUCTION	TREE A
	1B BORATION USING CHARGING PUMPS	1b RX POWER < 10% AND CONSTANT OR DECREASING		
	1C BORATION USING ECCS PUMPS	1c BORON ADDITION RATE > (40) GPM AND CORE POWER DECREASING		
	1D CEA DRIVE DOWN	1d RX POWER < 10% AND CONSTANT OR DECREASING		
2. RCS INVENTORY CONTROL	2A CHARGING PUMPS	2a PRESSURIZER LEVEL > (36") AND CONSTANT OR INCREASING	PLCS MALFUNCTIONING OR RCS BOUNDARY BREACH OR EXCESSIVE RCS COOLING	TREE B
	2B ECCS PUMPS	2b SUBCOOLING > (201)"F (BY CET)		
	2C MANUAL CONTROL OF LETDOWN	2c ECCS DELIVERY CONSISTENT WITH FIGURE 10-11		
	2D	2d (36") < PRESSURIZER LEVEL < (244")		
3. RCS PRESSURE CONTROL	3A PRESSURIZER HEATERS	3a (201)"F < RCS SUBCOOLING < (200)"F	PPCS MALFUNCTIONING OR RCS BOUNDARY BREACH OR EXCESSIVE RCS COOLING	TREE C
	3B CVCS CHARGING, NO ECCS	3b RCS SUBCOOLED > (201)"F (BY CET)		
	3C ECCS PUMPS	3c RCS PRESSURE WITHIN LIMITS P-T CURVE (FIGURE 10-10)		
	3D MANUAL CONTROL OF PRESSURIZER SPRAY	3d ECCS DELIVERY CONSISTENT WITH FIGURE 10-11		
	3E RCS RUNNING WITH STEAM DISCHARGE THROUGH ADV'S OR TSS	3e RCS PRESSURE < (2340) PSIA AND CONSTANT OR DECREASING WITHIN P-T CURVE LIMITS (FIGURE 10-10)		
	3F NATURAL CIRC. STEAM DISCHARGE THROUGH ADV'S OR TSS	3f		
	3G PORV'S WITH ECCS OPERATING	3g		
4. RCS AND CORE HEAT REMOVAL	4A	4a AT LEAST ONE S/G LEVEL IS EITHER A) WITHIN THE ZERO POWER LEVEL BAND WITH FEEDWATER AVAILABLE TO MAINTAIN THE LEVEL OR B) BEING RESTORED BY A FEEDWATER FLOW > (150) GPM	LOSS OF FORCED CIRCULATION OR INADEQUATE NATURAL CIRC OR COOLANT SATURATED OR VOIDS OR INADEQUATE S/G HEAT SINK	TREE D
	4B	4b $T_{HT} - T_{CT} < (101)"F$		
	4C	4c $T_{AVE} < (545)"F$		
	4D	4d ECCS DELIVERY CONSISTENT WITH FIGURE 10-11		
	4E	4e CET < (800)"F OR DECREASING		
	4F	4f AT LEAST ONE S/G LEVEL IS EITHER A) WITHIN THE ZERO POWER LEVEL BAND WITH FEEDWATER AVAILABLE TO MAINTAIN THE LEVEL OR B) BEING RESTORED BY A FEEDWATER FLOW > (150) GPM		
	4G	4g		
	4H	4h		
	4I	4i		
	4J	4j		
5. CONTAINMENT ISOLATION	5A	5a NO STEAM PLANT ACTIVITY ALARMS	LARGE STEAM BREAK IN CONTNMT OR LARGE RCS BREAK IN CONTNMT	TREE E
	5B	5b NO CONTAINMENT RADIATION ALARMS		
	5C	5c CONTAINMENT PRESSURE < (4) PSIG		
6. CONTAINMENT TEMPERATURE & PRESSURE	6A	6a AT LEAST ONE CONTAINMENT ISOLATION VALVE FOR EACH CONTAINMENT PENETRATION (NOT REQUIRED IS CLOSED)	LARGE STEAM BREAK IN CONTNMT OR LARGE RCS BREAK IN CONTNMT	TREE F
	6B	6b CONTAINMENT PRESSURE < (1.5) PSIG		
	6C	6c CONTAINMENT TEMPERATURE < (215)"F		
7. CONTAINMENT COMBUSTIBLE GAS CONTROL	7A	7a CONTAINMENT SPRAY FLOW > (1500) GPM AND CONTAINMENT TEMPERATURE & PRESSURE CONSTANT OR DECREASING	RCS BOUNDARY BREACH	TREE G
	7B	7b		

FIGURE 10-3 SAFETY FUNCTION STATUS CHECK

* These Success Paths are addressed in the Functional Recovery Operating Procedure as alternates as appropriate.
 7a H₂ is addressed in every Recovery Procedure as a check of containment parameters
 10-104 CEN-152 Rev. 01



1. **Identify the main idea of the passage.**

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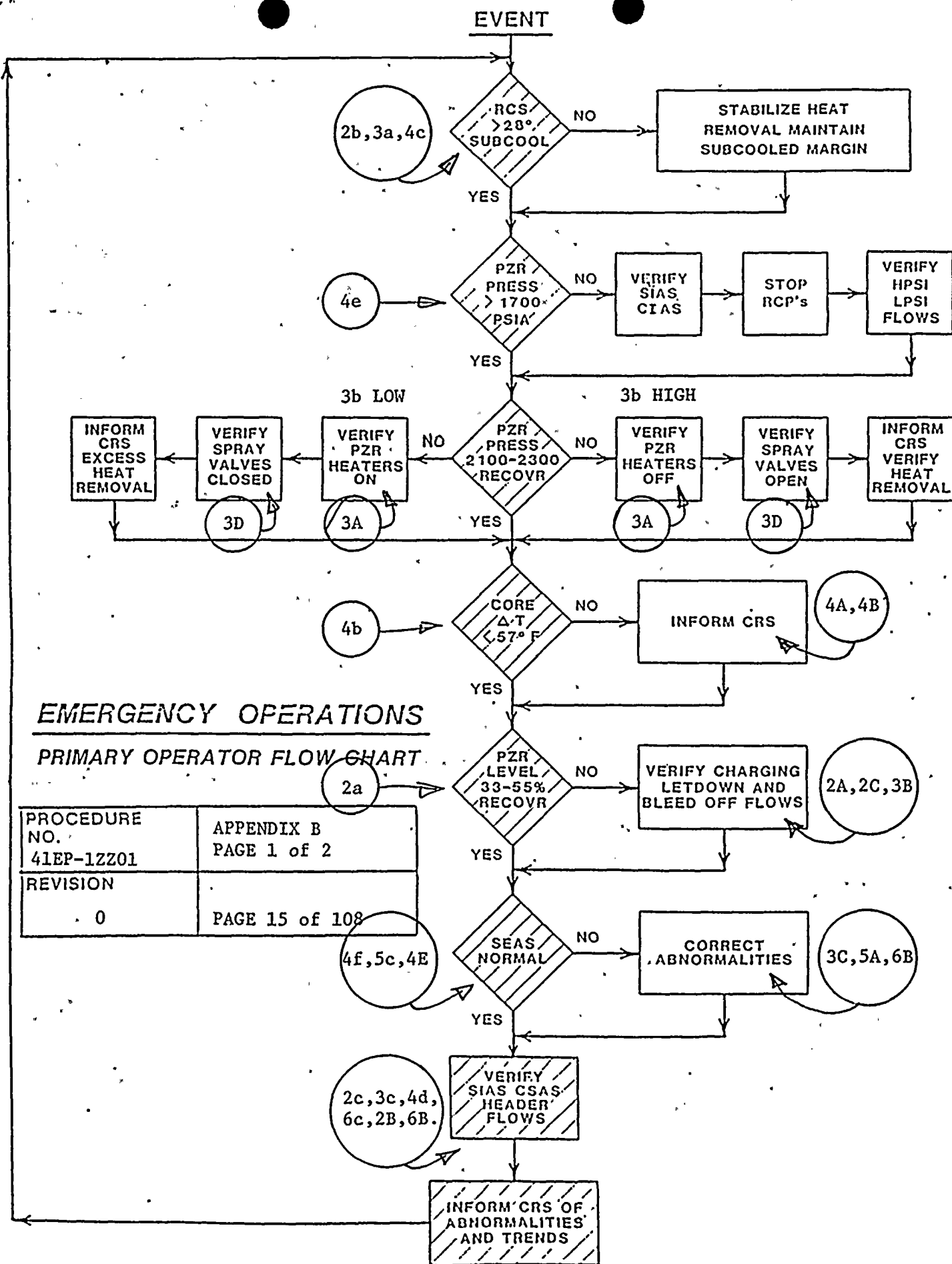


FIGURE 1

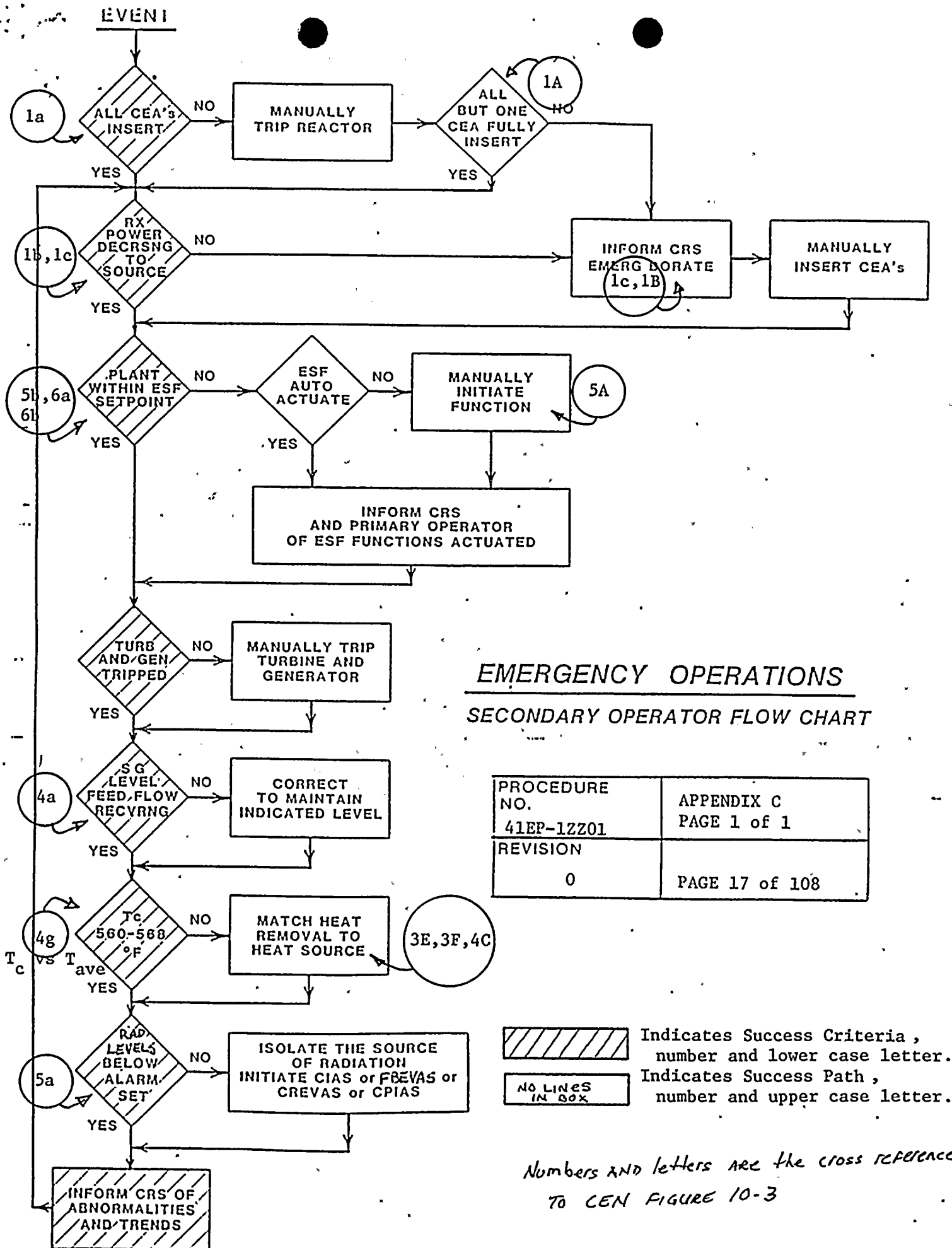


FIGURE 2

cooling and stabilizing plant parameters. The steps from CEN-152 identified in the Technical Guidelines as not incorporated (section III, page 174) are as follows:

- Step 20 - Refers to restoring automatic pressure control.
- Step 21 - Refers to restoring automatic level control.
- Step 29 - Involves restoring pressurizer level and maintaining level in the indicated range.
- Step 23 - Involves bypassing automatic initiated safety & 35 signals.

These steps affect the large break LOCA procedures's ability to mitigate a small LOCA as follows:

- Step 20 - These parameters are not expected to be controlled
21 & 29 due to loss of coolant inventory. However, included in the procedure are plant status points that insures plant awareness by the operators and directs maintenance of safety function. Each identified parameter is checked in each status point and checked in relation to maintaining the safety function. If action can be taken to restore the systems to automatic, the action would be performed as a result of safety function maintenance.
- Step 23 - The safety signal bypass steps are not
& 35 incorporated because MSIS and SIAS are generated as a result of 5 psig containment pressure. If this pressure has not occurred, the operator should be using the small LOCA procedure, If the large LOCA procedure is implemented, due to misdiagnosis, not resetting these signals would not adversely affect the procedure or plant response. However, additional operator actions to control pressurizer level with SI pumps and conduct the cooldown would be necessary. These extra actions and guidance are incorporated into the large LOCA procedure.

The diagnostic is expected to be performed within 20 minutes of the initiating event. Five pounds in containment within the time of performing the diagnostics is indicative of significant coolant inventory loss or a large break LOCA. Therefore, when performing the diagnostics 5 psig containment pressure is used for operator guidance in the determination of which Recovery Procedure to implement, the large or small LOCA. There is sufficient guidance in both procedures to either implement a more appropriate procedure or incorporate the appropriate operations to mitigate the full scale of LOCA casualties, regardless of containment pressure.

