

NUCLEAR ENERGY
BUSINESS OPERATIONS

GENERAL  ELECTRIC

23A1877AA SH NO. 1
REV 2

ORIGINAL

REVISION STATUS SHEET

SYS. 16,17

DOCUMENT TITLE REACTOR PROTECTION SYSTEM

LEGEND OR DESCRIPTION OF GROUPS

TYPE DESIGN SPECIFICATION DATA SHEET

THE SUPPLY SYSTEM IS RESPONSIBLE FOR
DESIGN CHANGE CONTROL OF THIS DOCUMENT

PAGE HANEORD 2

MPL ITEM NO. C72-4010

-Denotes Change

REVISIONS		C																																																																																							
0	Document Control Transfer per PWA 3608KK DMC-2414																																																																																								
2	<i>Approved 4-1-86</i> <i>4/26/86</i> <i>7/20/86</i> <i>Revised Per: 84-1281-0A-011</i> <i>Chkd By: Law 4/1/86</i>																																																																																								
<div style="text-align: center;">(F)</div>		<table border="1"><tr><td>1</td><td>Dwg. Transferred To Supply System Control As Per Work Order 4300 EMR-83-1808</td><td>12/2/83</td><td>T.L. H</td><td>DB</td><td>12/1/83</td></tr><tr><td>Rev. No.</td><td>Revision</td><td>Date</td><td>Drawn</td><td>Chkd</td><td>Appd. S.S. Engr.</td></tr><tr><td colspan="6">BURNS AND ROE Burns & Roe is Responsible Only For That Information It Has Added To This Drawing In Accordance With Supply System Direction By The Above Revisions.</td></tr><tr><td colspan="6">BURNS & ROE FILE NO. <u>2-14-1700</u></td></tr><tr><td>SUPPLY SYSTEM</td><td>02-02C72-03,</td><td>3</td><td>2.</td><td colspan="2">-</td></tr><tr><td></td><td>CVI Number</td><td>CVI Sheet</td><td>Rev.</td><td colspan="2">Dwg. Sheet</td></tr><tr><td>DR</td><td></td><td></td><td></td><td colspan="2"></td></tr><tr><td>366A</td><td></td><td></td><td></td><td colspan="2"></td></tr><tr><td>740RS</td><td></td><td></td><td></td><td colspan="2"></td></tr><tr><td>754MR</td><td></td><td></td><td></td><td colspan="2"></td></tr><tr><td>432QM</td><td></td><td></td><td></td><td colspan="2"></td></tr><tr><td>722D</td><td></td><td></td><td></td><td colspan="2"></td></tr><tr><td colspan="2">PRINTS TO</td><td></td></tr><tr><td>MADE BY <i>M HATA</i></td><td>APPROVALS <i>RA SIEMER</i></td><td>DEPT <u>NED</u></td><td colspan="3">LOCATION <u>SAN JOSE</u></td></tr><tr><td>CHKD BY <i>AB ROGUE</i></td><td>ISSUED <i>FM IKEMOTO</i></td><td colspan="4">CONT ON SHEET 2 SH NO. 1</td></tr></table>	1	Dwg. Transferred To Supply System Control As Per Work Order 4300 EMR-83-1808	12/2/83	T.L. H	DB	12/1/83	Rev. No.	Revision	Date	Drawn	Chkd	Appd. S.S. Engr.	BURNS AND ROE Burns & Roe is Responsible Only For That Information It Has Added To This Drawing In Accordance With Supply System Direction By The Above Revisions.						BURNS & ROE FILE NO. <u>2-14-1700</u>						SUPPLY SYSTEM	02-02C72-03,	3	2.	-			CVI Number	CVI Sheet	Rev.	Dwg. Sheet		DR						366A						740RS						754MR						432QM						722D						PRINTS TO			MADE BY <i>M HATA</i>	APPROVALS <i>RA SIEMER</i>	DEPT <u>NED</u>	LOCATION <u>SAN JOSE</u>			CHKD BY <i>AB ROGUE</i>	ISSUED <i>FM IKEMOTO</i>	CONT ON SHEET 2 SH NO. 1			
		1	Dwg. Transferred To Supply System Control As Per Work Order 4300 EMR-83-1808	12/2/83	T.L. H	DB	12/1/83																																																																																		
		Rev. No.	Revision	Date	Drawn	Chkd	Appd. S.S. Engr.																																																																																		
		BURNS AND ROE Burns & Roe is Responsible Only For That Information It Has Added To This Drawing In Accordance With Supply System Direction By The Above Revisions.																																																																																							
		BURNS & ROE FILE NO. <u>2-14-1700</u>																																																																																							
		SUPPLY SYSTEM	02-02C72-03,	3	2.	-																																																																																			
			CVI Number	CVI Sheet	Rev.	Dwg. Sheet																																																																																			
		DR																																																																																							
		366A																																																																																							
		740RS																																																																																							
754MR																																																																																									
432QM																																																																																									
722D																																																																																									
PRINTS TO																																																																																									
MADE BY <i>M HATA</i>	APPROVALS <i>RA SIEMER</i>	DEPT <u>NED</u>	LOCATION <u>SAN JOSE</u>																																																																																						
CHKD BY <i>AB ROGUE</i>	ISSUED <i>FM IKEMOTO</i>	CONT ON SHEET 2 SH NO. 1																																																																																							

NEO 807A (REV. 10/81)

9704220009 970415
PDR ADOCK 05000397
P PDR

T-5223

4.1.12 Reactor Protection System Trip - Reactor Vessel High Pressure

4.1.12.1 Function - Limit positive pressure effect on reactor power.
(Note 11) (See Paragraph 4.1.18 for Notes and Definitions)

4.1.12.2 Trip Channel Sensor	A1 B22-N023A
Identities	A2 B22-N023C
(Note 11)	B1 B22-N023B
	B2 B22-N023D

4.1.12.3 Normal Range 920-1005 psig

4.1.12.4 Channel Instrument Accuracy *

4.1.12.5 Channel Calibration Accuracy *

4.1.12.6 Channel Instrument Drift (Design) *

4.1.12.7 Analytical Limit *

4.1.12.8 Technical Specification Limit *

4.1.12.9 Nominal Trip Setpoint *

4.1.12.10 Alarm Setting **

4.1.12.11 Transient 140 psi/second

4.1.12.12 Trip Channel Sensor Response 0.5 seconds
Time

4.1.12.13 Trip System Trip Logic 1:2

* See Reference 2.1.2.g for these requirements.

** See Reference 2.1.2.r for this requirement.

240

240



DDS

NUCLEAR ENERGY
BUSINESS OPERATIONS

GENERAL  ELECTRIC

23A1877AA SH NO. 9
REV 2

4.1.5 Reactor Protection System Trip - Reactor Vessel Low Water Level

4.1.5.1 Function - Reduce possibility of uncovering reactor core
(Note 11) (See Paragraph 4.1.18 for Notes and Definitions)

4.1.5.2 Trip Channel Sensor	A1 B22-N024A
Identities	A2 B22-N024C
(Note 11)	B1 B22-N024B
	B2 B22-N024D

4.1.5.3 Normal Range	559 to 568 inches above vessel zero
----------------------	----------------------------------------

4.1.5.4 Channel Instrument Accuracy	*
-------------------------------------	---

4.1.5.5 Channel Calibration Accuracy	*
--------------------------------------	---

4.1.5.6 Channel Instrument Drift (Design)	*
-------------------------------------------	---

4.1.5.7 Analytical Limit	*
--------------------------	---

4.1.5.8 Technical Specification Limit	*
---------------------------------------	---

4.1.5.9 Nominal Trip Setpoint	*
-------------------------------	---

4.1.5.10 Alarm Setting	**
------------------------	----

4.1.5.11 Transient	- 7 inches/second
--------------------	-------------------

4.1.5.12 Trip Channel Sensor Response Time	1 second
-----------------------------------------------	----------

4.1.5.13 Trip System Trip Logic	1:2
---------------------------------	-----

* See Reference 2.1.2.g for these requirements.

** See Reference 2.1.2.r for these requirements.

DD2

TABLE 7.2-5
RPS RESPONSE TIME (DESIGN)

<u>FUNCTION</u>	<u>SENSOR RESPONSE TIME</u>	<u>CHANNEL, ACTUATOR, AND LOGIC RESPONSE TIME</u>	<u>MAXIMUM OVERALL RESPONSE TIME</u>
APRM*			
Flow Biased Simulated Thermal Power-Upscale	0.06 Seconds	0.05 Seconds**	0.09 Seconds**
Fixed Neutron Flux- Upscale	0.06 Seconds	0.05 Seconds	0.09 Seconds
Reactor Vessel High Pressure	0.5 Seconds	0.05 Seconds	0.55 Seconds
Reactor Vessel Low Water Level	1.0 Seconds	0.05 Seconds	1.05 Seconds
MSLIV Closure	0.01 Seconds	0.05 Seconds	0.06 Seconds
Turbine Stop Valve Closure	0.01 Seconds	0.05 Seconds	0.06 Seconds
Turbine Control Valve Fast Closure	0.03 Seconds	0.05 Seconds	0.08 Seconds#

* Neutron detectors are exempt from response time testing. Response time shall be measured from the detector output or from the input of the first electronic component in the channel.

** Total response time of 6 ± 1 seconds including simulated thermal power time constant.

Measured from start of turbine control valve fast closure.

9:30 Am.

RAW BENCH TEST R/T DATA
(SENSORS)

4785

Bill 4679

Terry Moore. 582 7735

MS-PS-23 B.

68-11-1770 RA

1079 psip

slow (.04 sec)

1 fast (.04 sec)

MS-PS-23 A1

68-11-1769 RA

1079 psip

slow (.02 sec)

↑ fast (.06 sec)

MS-PS-23 C

68-11-1771 RA

1078

slow (.23 sec)

fast (.07 sec)

PO 96811 item 1

88-7-1940

1077

slow (.20 sec)

fast (.08 sec)

PO 225541 item 1

92-7-7123

135

(MS-LS-61A)

SW #1 (.613 sec)

SW #2 (.50 sec)

slow

SW #1 (.465 sec)

SW #2 (.39 sec)

fast

PO 225541 item 1

92-7-7124

135

slow SW #1 (.80 sec)
SW #2 (.27 sec)SW #1 (.44 sec)
FAST SW #2 (.43 sec)

WHICH 11/11/11 STORES

7AS

By: WLL Date: 4/14/97
 CHECKED PAS 4/15/97

MS-LIS-61A, B, C, D Sensor
One sided upper tolerance bounds
 (Data is in seconds)

$$D_1 := \begin{bmatrix} .685 \\ .78 \\ .5 \\ .432 \\ .675 \\ .605 \\ .53 \\ .554 \end{bmatrix} \quad D_2 := \begin{pmatrix} .465 \\ .44 \end{pmatrix} \quad \text{Data} := \text{stack}(D_1, D_2)$$

Establish mean and standard deviation using standard Mathcad functions:

Notation as follows:

n = number of data points
 Mean = mean of the data
 s = standard deviation

$$n := \text{rows}(\text{Data}) \quad n = 10$$

$$\text{Mean} := \text{mean}(\text{Data}) \quad \text{Mean} = 0.5666 \quad s := \text{stdev}(\text{Data}) \cdot \sqrt{\frac{n}{n-1}} \quad s = 0.117$$

The following analysis establishes the 95%/ 95% one sided upper tolerance interval. The tolerance interval is obtained from the matrix Tol₉₅ using MathCad's linterp function.

$$\text{Tol}_{95} := \begin{bmatrix} 4 & 5.14 \\ 5 & 4.2 \\ 6 & 3.71 \\ 7 & 3.4 \\ 8 & 3.19 \\ 9 & 3.03 \\ 10 & 2.91 \\ 12 & 2.74 \\ 15 & 2.57 \\ 20 & 2.4 \\ 25 & 2.29 \\ 30 & 2.22 \\ 40 & 2.13 \\ 60 & 2.02 \end{bmatrix} \quad \text{TF} := \text{linterp}(\text{Tol}_{95}^{<1>}, \text{Tol}_{95}^{<2>}, n) \quad \text{TF} = 2.91$$



TAS 9/15/97

One-sided upper tolerance bound

$$T_{\text{upper}} := \text{Mean} + s \cdot TF$$

$$T_{\text{upper}} = 0.907$$

Establish normality plot:

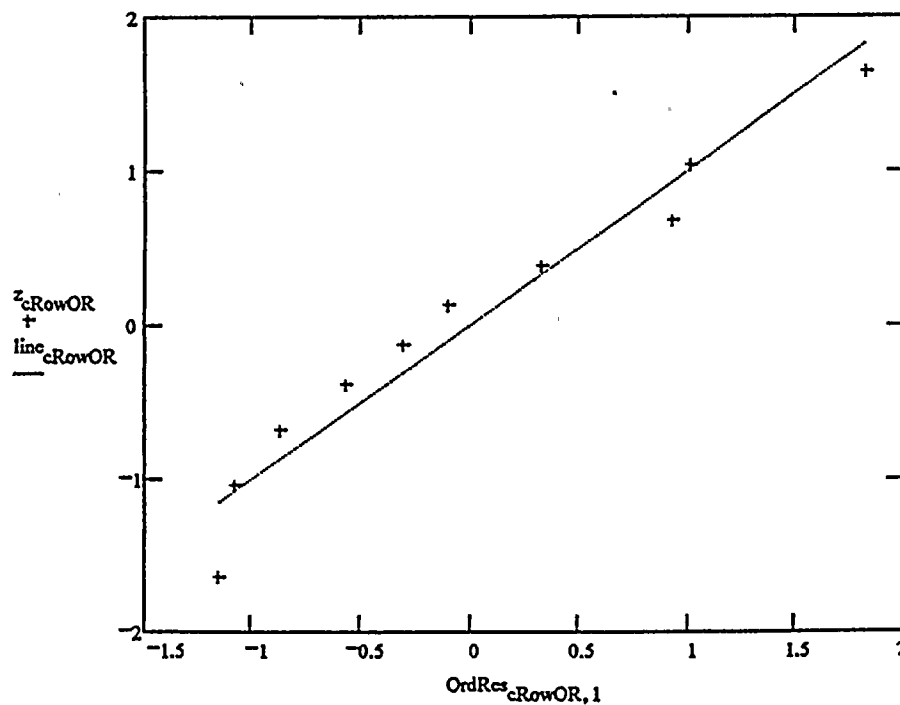
$$\text{Residuals} := \text{Data} - \text{Mean} \quad \text{Standard Residuals} := \frac{\text{Residuals}}{s}$$

$$\text{OrdRes} := \text{csort}(\text{Standard Residuals}, 1) \quad \text{cRowOR} := 1 \dots \text{rows}(\text{OrdRes})$$

$$\text{Prob}_{\text{cRowOR}} := \frac{\text{cRowOR} - \frac{1}{2}}{\text{rows}(\text{OrdRes})} \quad \text{OrdRes} := \text{augment}(\text{OrdRes}, \text{Prob})$$

$$x := 0 \quad z_{\text{cRowOR}} := \text{root}(\text{normal}(0, 1, x) - \text{Prob}_{\text{cRowOR}}, x)$$

$$m := 1 \quad \text{intercept} := 0 \quad \text{line}_{\text{cRowOR}} := m \cdot \text{OrdRes}_{\text{cRowOR}, 1} + \text{intercept}$$



MS-PS-23A,B,C,D SensorOne sided upper tolerance bounds

$$D_1 := \begin{bmatrix} .072 \\ .22 \\ .04 \\ .063 \\ .04 \\ .181 \\ .05 \end{bmatrix}$$

$$D_2 := \begin{bmatrix} .04 \\ .06 \\ .07 \\ .08 \end{bmatrix}$$

$$\text{Data} := \text{stack}(D_1, D_2)$$

(Data in sec)

Evaluate 0.22 and .181 as outliers:

$$S^2 = 0.0362$$

$$S_{1,2}^2 = 0.0019$$

$$\frac{S_{1,2}^2}{S^2} = \frac{.0019}{.0362} = 0.05$$

Establish mean and standard deviation using standard Mathcad functions:

Notation as follows:

n = number of data points

Mean = mean of the data

s = standard deviation

$$n := \text{rows}(\text{Data}) \quad n = 11 \quad \text{Mean} := \text{mean}(\text{Data}) \quad \text{Mean} = 0.0833$$

$$s := \text{stdev}(\text{Data}) \cdot \sqrt{\frac{n}{n-1}} \quad s = 0.0602 \quad S := \sum_{i=1}^n (\text{Data}_i - \text{Mean})^2 \quad S = 0.0362$$

$$n = 10$$

Per table S of ASTM:
E 178-94, Those points
are outliers at the 0.1%
level of significance.

The following analysis establishes the 95%/ 95% one sided upper tolerance interval. The tolerance interval is obtained from the matrix Tol₉₅ using MathCad's linterp function.

$$\text{Tol}_{95} := \begin{bmatrix} 4 & 5.14 \\ 5 & 4.2 \\ 6 & 3.71 \\ 7 & 3.4 \\ 8 & 3.19 \\ 9 & 3.03 \\ 10 & 2.91 \\ 12 & 2.74 \\ 15 & 2.57 \\ 20 & 2.4 \\ 25 & 2.29 \\ 30 & 2.22 \\ 40 & 2.13 \\ 60 & 2.02 \end{bmatrix}$$

$$\text{TF} := \text{linterp}(\text{Tol}_{95}^{<1>}, \text{Tol}_{95}^{<2>}, n) \quad \text{TF} = 2.825$$

By: WLL Date: 4/14/97
 PAS 4/15/97

One-sided upper tolerance bound

$$T_{\text{upper}} := \text{Mean} + s \cdot TF \quad T_{\text{upper}} = 0.2533$$

Establish normality plot:

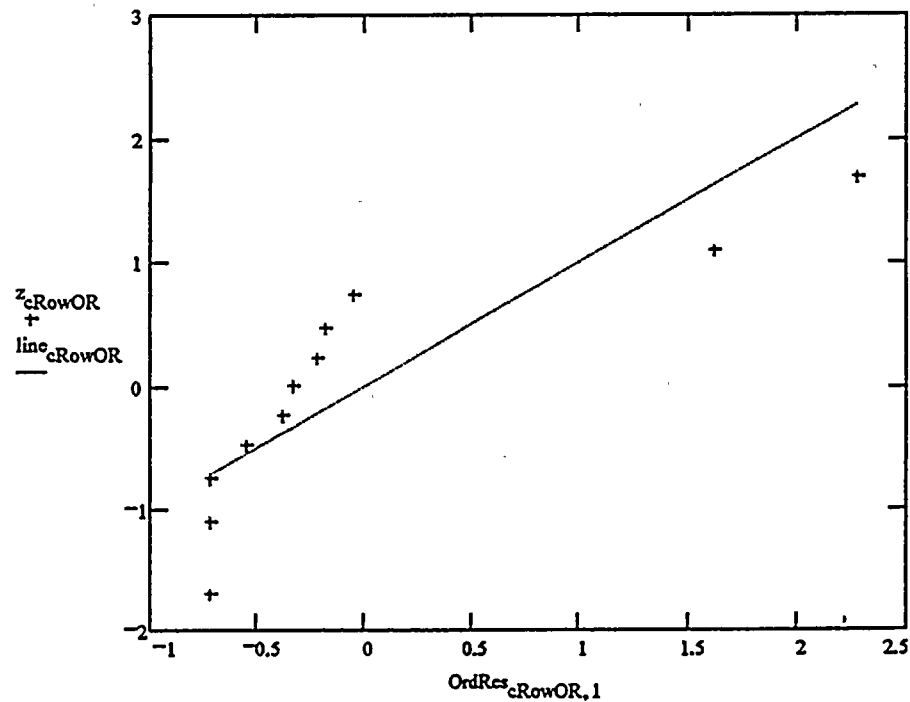
$$\text{Residuals} := \text{Data} - \text{Mean} \quad \text{Standard Residuals} := \frac{\text{Residuals}}{s}$$

$$\text{OrdRes} := \text{csort}(\text{Standard Residuals}, 1) \quad \text{cRowOR} := 1 \dots \text{rows}(\text{OrdRes})$$

$$\text{Prob}_{\text{cRowOR}} := \frac{\text{cRowOR} - \frac{1}{2}}{\text{rows}(\text{OrdRes})} \quad \text{OrdRes} := \text{augment}(\text{OrdRes}, \text{Prob})$$

$$x := 0 \quad z_{\text{cRowOR}} := \text{root}(\text{normal}(0, 1, x) - \text{Prob}_{\text{cRowOR}}, x)$$

$$m := 1 \quad \text{intercept} := 0 \quad \text{line}_{\text{cRowOR}} := m \cdot \text{OrdRes}_{\text{cRowOR}, 1} + \text{intercept}$$



By: WLL Date: 4/14/97

PA5 4/15/97

MS-PS-23A,B,C,D Sensor
One sided upper tolerance bounds

$$D_1 := \begin{bmatrix} .072 \\ .04 \\ .063 \\ .04 \\ .05 \end{bmatrix} \quad D_2 := \begin{bmatrix} .04 \\ .06 \\ .07 \\ .08 \end{bmatrix} \quad \text{Data} := \text{stack}(D_1, D_2)$$

Establish mean and standard deviation using standard Mathcad functions:

Notation as follows:

n = number of data points

Mean = mean of the data

s = standard deviation

$$n := \text{rows}(\text{Data}) \quad n = 9 \quad \text{Mean} := \text{mean}(\text{Data}) \quad \text{Mean} = 0.0572$$

$$s := \text{stdev}(\text{Data}) \cdot \sqrt{\frac{n}{n-1}} \quad s = 0.0153 \quad S := \sum_{i=1}^n (\text{Data}_i - \text{Mean})^2 \quad S = 0.0019$$

The following analysis establishes the 95%/ 95% one sided upper tolerance interval. The tolerance interval is obtained from the matrix Tol₉₅ using MathCad's linterp function.

$$\text{Tol}_{95} := \begin{bmatrix} 4 & 5.14 \\ 5 & 4.2 \\ 6 & 3.71 \\ 7 & 3.4 \\ 8 & 3.19 \\ 9 & 3.03 \\ 10 & 2.91 \\ 12 & 2.74 \\ 15 & 2.57 \\ 20 & 2.4 \\ 25 & 2.29 \\ 30 & 2.22 \\ 40 & 2.13 \\ 60 & 2.02 \end{bmatrix} \quad \text{TF} := \text{linterp}(\text{Tol}_{95}^{<1>}, \text{Tol}_{95}^{<2>}, n) \quad \text{TF} = 3.03$$

PAS 9/15/97

One-sided upper tolerance bound

$$T_{\text{upper}} := \text{Mean} + s \cdot TF$$

$$T_{\text{upper}} = 0.1037$$

Establish normality plot:

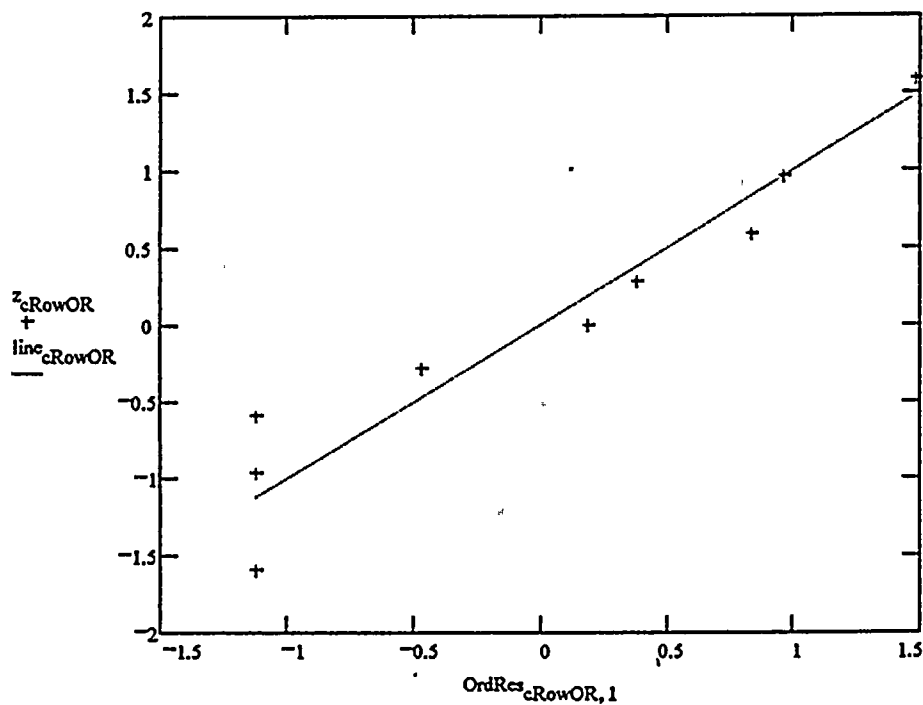
$$\text{Residuals} := \text{Data} - \text{Mean} \quad \text{Standard Residuals} := \frac{\text{Residuals}}{s}$$

$$\text{OrdRes} := \text{csort}(\text{Standard Residuals}, 1) \quad \text{cRowOR} := 1 \dots \text{rows}(\text{OrdRes})$$

$$\text{Prob}_{\text{cRowOR}} := \frac{\text{cRowOR} - \frac{1}{2}}{\text{rows}(\text{OrdRes})} \quad \text{OrdRes} := \text{augment}(\text{OrdRes}, \text{Prob})$$

$$x := 0 \quad z_{\text{cRowOR}} := \text{root}(\text{normal}(0, 1, x) - \text{Prob}_{\text{cRowOR}}, x)$$

$$m := 1 \quad \text{intercept} := 0 \quad \text{line}_{\text{cRowOR}} := m \cdot \text{OrdRes}_{\text{cRowOR}, 1} + \text{intercept}$$



7/15/97

By: WLL Date: 4/14/97
CHECKED FAS 4/15/97

RPS Low Level
One sided upper tolerance bounds

Barton 288A
(Data in msec)

D1 :=	520		
	523		
	485		
	420		
	320		
	465	468	
	460	400	
	400	559	
	455	495	Data := stack(D1,D2)
	430	381	
	357	476	
	542	470	
	542	377	
	540		
	470		
	497		
	358		

By: WLL Date: 4/14/97

PHS 4/15/97

Establish mean and standard deviation using standard Mathcad functions:

Notation as follows:

n = number of data points

Mean = mean of the data

s = standard deviation

n := rows(Data) n = 25

Mean := mean(Data) Mean = 456.4 s := stdev(Data) · $\sqrt{\frac{n}{n-1}}$ s = 65.8679

The following analysis establishes the 95%/ 95% one sided upper tolerance interval. The tolerance interval is obtained from the matrix Tol₉₅ using MathCad's linterp function.

Tol ₉₅ :=	4	5.14	TF := linterp(Tol ₉₅ ^{<1>} , Tol ₉₅ ^{<2>} , n)	TF = 2.29
	5	4.2		
	6	3.71		
	7	3.4		
	8	3.19		
	9	3.03		
	10	2.91		
	12	2.74		
	15	2.57		
	20	2.4		
	25	2.29		
30	2.22			
40	2.13			
60	2.02			

One-sided upper tolerance bound

T_{upper} := Mean + s · TF T_{upper} = 607.2375

TAS 4/15/97

Establish normality plot:

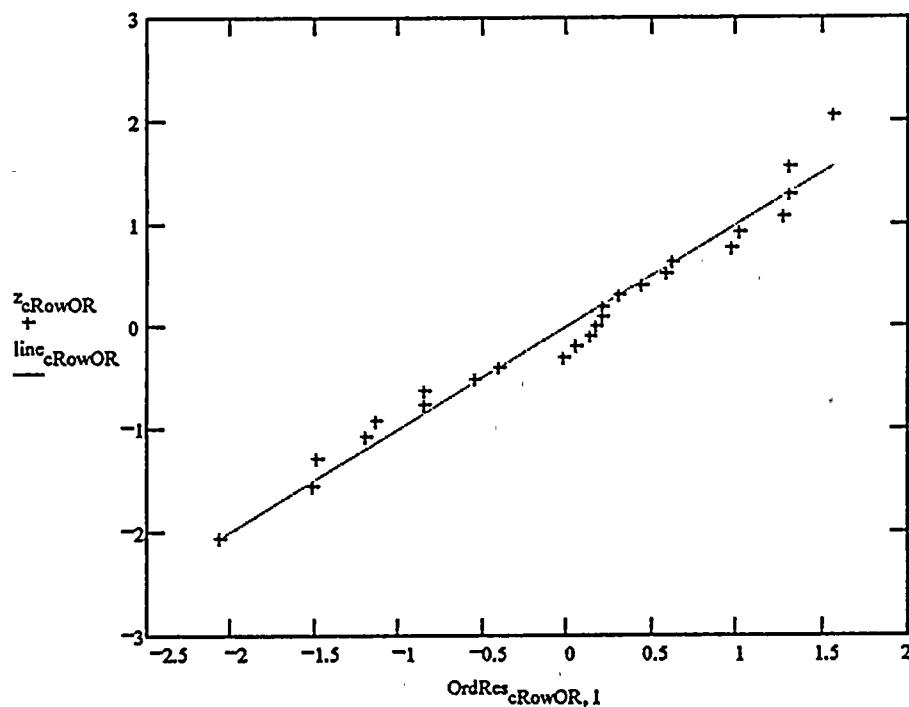
$$\text{Residuals} := \text{Data} - \text{Mean} \quad \text{Standard Residuals} := \frac{\text{Residuals}}{s}$$

$$\text{OrdRes} := \text{csort}(\text{Standard Residuals}, 1) \quad \text{cRowOR} := 1 \dots \text{rows}(\text{OrdRes})$$

$$\text{Prob}_{\text{cRowOR}} := \frac{\text{cRowOR} - \frac{1}{2}}{\text{rows}(\text{OrdRes})} \quad \text{OrdRes} := \text{augment}(\text{OrdRes}, \text{Prob})$$

$$x := 0 \quad z_{\text{cRowOR}} := \text{root}(\text{normal}(0, 1, x) - \text{Prob}_{\text{cRowOR}}, x)$$

$$m := 1 \quad \text{intercept} := 0 \quad \text{line}_{\text{cRowOR}} := m \cdot \text{OrdRes}_{\text{cRowOR}, 1} + \text{intercept}$$





By: WLL Date: 4/14/97
 CHECKED FRS 4/15/99

MS-LIS-61A,B,C,D and MS-DPIS-8A,B,C,D Logic

One sided upper tolerance bounds

(Data in msec)

$$D_1 := \begin{bmatrix} 30 \\ 20 \\ 30 \\ 25 \\ 25 \\ 10 \\ 20 \\ 20 \end{bmatrix} \quad D_2 := \begin{bmatrix} 17 \\ 14 \\ 30 \\ 20 \\ 26 \\ 24 \\ 12 \end{bmatrix} \quad Data := \text{stack}(D_1, D_2)$$

Establish mean and standard deviation using standard Mathcad functions:

Notation as follows:

n = number of data points

Mean = mean of the data

s = standard deviation

$n := \text{rows}(Data) \quad n = 15$

$Mean := \text{mean}(Data) \quad Mean = 21.5333 \quad s := \text{stdev}(Data) \cdot \sqrt{\frac{n}{n-1}} \quad s = 6.4128$

The following analysis establishes the 95%/ 95% one sided upper tolerance interval. The tolerance interval is obtained from the matrix Tol₉₅ using MatCad's linterp function.

$$Tol_{95} := \begin{bmatrix} 4 & 5.14 \\ 5 & 4.2 \\ 6 & 3.71 \\ 7 & 3.4 \\ 8 & 3.19 \\ 9 & 3.03 \\ 10 & 2.91 \\ 12 & 2.74 \\ 15 & 2.57 \\ 20 & 2.4 \\ 25 & 2.29 \end{bmatrix} \quad TF := \text{linterp}(Tol_{95}^{<1>}, Tol_{95}^{<2>}, n) \quad TF = 2.57$$

By: WLL Date: 4/14/97

AS 9/15/97

One-sided upper tolerance bound

$$T_{upper} := \text{Mean} + s \cdot TF$$

$$T_{upper} = 38.0142$$

Establish normality plot:

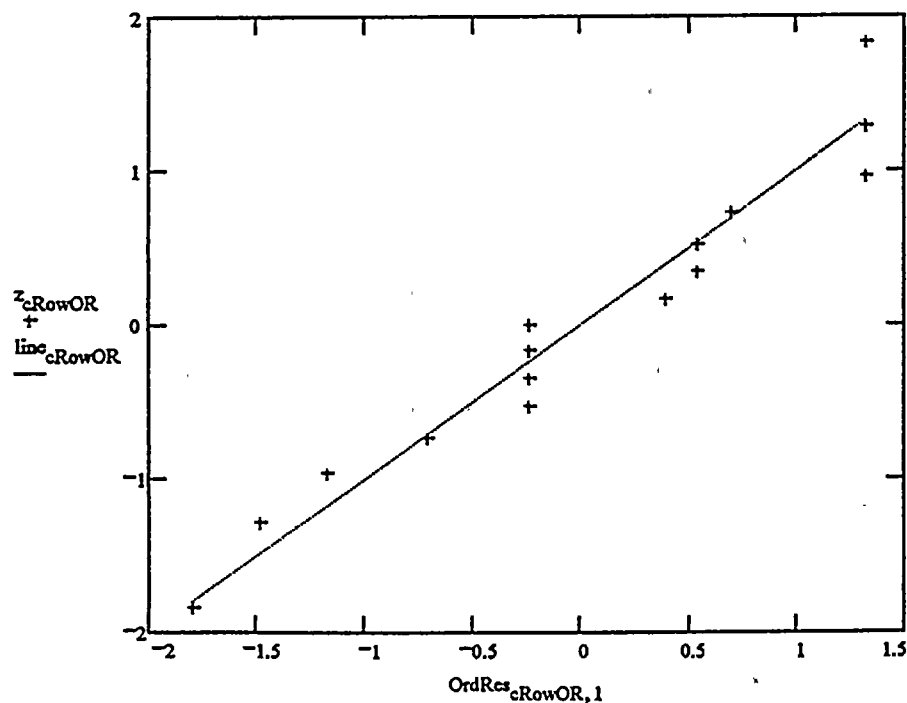
$$\text{Residuals} := \text{Data} - \text{Mean} \quad \text{Standard Residuals} := \frac{\text{Residuals}}{s}$$

$$\text{OrdRes} := \text{csort}(\text{Standard Residuals}, 1) \quad \text{cRowOR} := 1.. \text{rows}(\text{OrdRes})$$

$$\text{Prob}_{\text{cRowOR}} := \frac{\text{cRowOR} - \frac{1}{2}}{\text{rows}(\text{OrdRes})} \quad \text{OrdRes} := \text{augment}(\text{OrdRes}, \text{Prob})$$

$$x := 0 \quad z_{\text{cRowOR}} := \text{root}(\text{normal}(0, 1, x) - \text{Prob}_{\text{cRowOR}}, x)$$

$$m := 1 \quad \text{intercept} := 0 \quad \text{line}_{\text{cRowOR}} := m \cdot \text{OrdRes}_{\text{cRowOR}, 1} + \text{intercept}$$



PAS

By: WLL Date: 4/14/97
 CHECKED PAS 4/15/97

MS-PS 23A,B,C,D and MS-LIS-24A,B,C,D LOGIC
One sided upper tolerance bounds

(Data in msec)

$$D_1 := \begin{bmatrix} 33 \\ 30 \\ 35 \\ 30 \\ 21 \\ 32 \end{bmatrix} \quad D_2 := \begin{bmatrix} 30 \\ 25 \\ 30 \\ 40 \\ 15 \\ 25 \\ 30 \\ 30 \end{bmatrix} \quad Data := stack(D_1, D_2)$$

Establish mean and standard deviation using standard MathCad functions:

Notation as follows:

n = number of data points
 Mean = mean of the data
 s = standard deviation

$n := rows(Data) \quad n = 14$

$Mean := mean(Data) \quad Mean = 29 \quad s := stdev(Data) \cdot \sqrt{\frac{n}{n-1}} \quad s = 6.0764$

The following analysis establishes the 95%/ 95% one sided upper tolerance interval. The tolerance interval is obtained from the matrix Tol₉₅ using MathCad's linterp function.

$$Tol_{95} := \begin{bmatrix} 4 & 5.14 \\ 5 & 4.2 \\ 6 & 3.71 \\ 7 & 3.4 \\ 8 & 3.19 \\ 9 & 3.03 \\ 10 & 2.91 \\ 12 & 2.74 \\ 15 & 2.57 \\ 20 & 2.4 \\ 25 & 2.29 \end{bmatrix} \quad TF := linterp(Tol_{95}^{<1>}, Tol_{95}^{<2>}, n) \quad TF = 2.6267$$

PAS 4/15/97

One-sided upper tolerance bound

$$T_{upper} := \text{Mean} + s \cdot TF$$

$$T_{upper} = 44.9608$$

Establish normality plot:

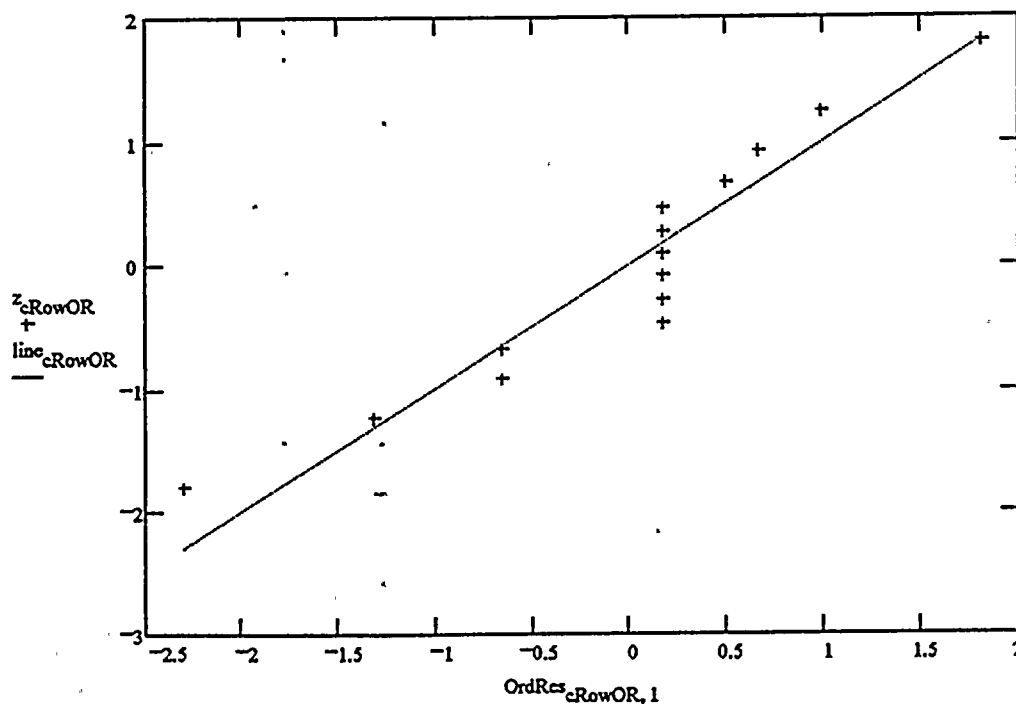
$$\text{Residuals} := \text{Data} - \text{Mean} \quad \text{Standard Residuals} := \frac{\text{Residuals}}{s}$$

$$\text{OrdRes} := \text{csort}(\text{Standard Residuals}, 1) \quad \text{cRowOR} := 1 \dots \text{rows}(\text{OrdRes})$$

$$\text{Prob}_{\text{cRowOR}} := \frac{\text{cRowOR} - \frac{1}{2}}{\text{rows}(\text{OrdRes})} \quad \text{OrdRes} := \text{augment}(\text{OrdRes}, \text{Prob})$$

$$x := 0 \quad z_{\text{cRowOR}} := \text{root}(\text{normal}(0, 1, x) - \text{Prob}_{\text{cRowOR}}, x)$$

$$m := 1 \quad \text{intercept} := 0 \quad \text{line}_{\text{cRowOR}} := m \cdot \text{OrdRes}_{\text{cRowOR}, 1} + \text{intercept}$$





General Electric Company
175 Curtner Avenue, San Jose, CA 95125

OG97-121-964
February 12, 1997

TO: BWR Owners' Group Response Time Testing (RTT) Committee

SUBJECT: ***Response Time Testing Committee Meeting Notice for March 12, 1997***

Attachments: (1) Draft NEDO-32291 Supplement 1, "BWR Owners' Group Licensing Topical Report -- System Analyses for the Simplification of Selected Response Time Testing Requirements", dated February 1997
(2) Washington, DC subway map
(3) Driving directions to meeting location

A BWR Owners' Group Response Time Testing (RTT) Committee meeting will be held on Wednesday, March 12, 1997 in Washington, DC. The purpose of this meeting is to discuss the draft NEDO-32291 Supplement 1 (see Attachment 1). Appropriate comments will be incorporated and the Committee will be asked to approve the revised document. This document supplements NEDO-32291-A, "System Analyses for the Elimination of Selected Response Time Testing Requirements" by providing technical justification for the further simplification of response time testing requirements of selected Reactor Protection System (RPS) and (2) Isolation Actuation System (IAS) instrumentation loops. The technical justification methods utilized include Failure Modes and Effects Analysis (FMEA), failure experience reviews, and identification of functional surveillance testing other than response time testing that adequately confirms the ability of the selected instrumentation loops to meet response time requirements.

RTT Committee members are requested to carefully review the attached draft Licensing Topical Report and provide your comments to the undersigned no later than Wednesday, March 5, 1997. The report is complete except for the FMEA information for the GE CR120A relays. That is expected to be available before the meeting. As we discussed in conference calls last fall, the fast response RTTs are not included. In addition, main steam line radiation loop for MSIV closure is not included because it has been addressed by other BWROG action. Four radiation monitoring loops, each applying to a single plant, are not included because it appeared unlikely that the FMEA could provide adequate justification (due to complexity). Finally, one Drywell High Pressure (RPS) loop for a single plant is not included because there are other ways to address that one with greater likelihood of success.

The Response Time Testing Committee will meet in the morning at the Embassy Suites Hotel at Friendship Heights, and then will travel to NRC headquarters in Rockville to discuss the report conclusions, the schedule for Licensing Topical Report submittal, and the review/approval cycle. Following the meeting with the NRC we will return to the Embassy Suites Hotel to closeout open issues if required.

