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 MECREDY, R.C. Rochester Gas & Electric Corp.
 RECIP. NAME RECIPIENT AFFILIATION
 VISSING, G.

SUBJECT: Transmits response to 960913 RAI.

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ROBERT C. MECREDY
Vice President
Nuclear Operations

December 11, 1996

U.S. Nuclear Regulatory Commission
Document Control Desk
Attn: Guy Vissing
Project Directorate I-1
Washington, D.C. 20555

Subject: Letter from Guy S. Vissing, NRC, to Robert C. Mecredy,
RGE, Subject: "Request for Additional Information
Relating to Rochester Gas and Electric Corporation
(RG&E)", dated September 13, 1996 (TAC No. M96529)
R.E. Ginna Nuclear Power Plant
Docket No. 50-244

Dear Mr. Vissing:

The purpose of this letter is to transmit the Rochester Gas and Electric (RG&E) response to the subject Request for Additional Information (RAI). Attachment A to this letter provides that response.

Very truly yours,


Robert C. Mecredy

Attachment
REJ\442

xc: Mr. Guy Vissing (Mail Stop 14C7)
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Washington, D.C. 20555

U.S. Nuclear Regulatory Commission
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Ginna Senior Resident Inspector

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Question 1:

Describe the basis for the copper and nickel values used (i.e., 0.25 and 0.56 respectively) for the reactor vessel circumferential weld seam SA-847. In addition, describe how the coil-to-coil variability in the amount of copper in the filler wire is accounted for.

Response:

- (a) .25 Cu & .56 Ni came from PTS SER (3/22/96) p. 3, Sect. 2.2, 1st paragraph. When the new sample data from WCAP-14684 Table 5-4A p. 55 were factored in, the new values would be \approx .248 Cu & \approx .55 Ni. Since .25 Cu & .56 Ni were conservative we elected to not challenge the SER. In effect an additional penalty was added into the chemistry factor (CF). The Cu & Ni in Table 5-4A p. 55 represent actual surveillance capsule chemistry data. The values from Reference 54 of that table weren't available until after our PTS submittal.
- (b) As described in the PTS SER (3/22/96) Ginna does not have coil-to-coil variability information. Any discussion would be speculative and would not be in accordance with 10CFR50.61.

Question 2:

It appears from Table 5-4A of WCAP-14684 that the copper and nickel values used for the Ginna surveillance program weld metal are 0.236 and 0.517 respectively. In the staff's pressurized thermal shock evaluation forwarded by letter dated March 22, 1996, the staff concluded that the best estimate of the copper and nickel content in the surveillance weld was 0.225% and 0.53%, respectively. In addition, it was reported that the licensee's best estimate for copper and nickel in the surveillance weld were 0.214% and 0.50%. Discuss the basis for the values of copper and nickel in the surveillance weld reported in Table 5-4A. Furthermore, discuss how the chemistry factor for the surveillance weld reported on page 56 of WCAP-14684 was determined (i.e., provide the interpolation).

Response:

- (a) The PTS SER (3/22/96) did not have the benefit of additional chemistry sampling results of surveillance capsules as provided in WCAP-14684 Table 5-4A. This information was added per GL 92-01, which indicated that we should provide the latest available information. As stated in the PTS SER p. 4, Section 2.3, there were only 2 points for the surveillance chemistry available. The additional 8 points changed the mean chemistry values and, therefore, the Chemistry Factor.

- (b) CF = 159.4°F used Cu = .236 and Ni = .517 in its determination as follows:

From 10CFR50.61, Table 1:

$$(1) \quad \text{For Ni} = .4: \begin{array}{l} \text{Cu @ .23} = 140 \\ \text{Cu @ .24} = 144 \end{array} \left. \vphantom{\begin{array}{l} \text{Cu @ .23} = 140 \\ \text{Cu @ .24} = 144 \end{array}} \right\} \Rightarrow \frac{(\underline{144-140})(6)}{10} + 140 = 142.4$$

$$(2) \quad \text{For Ni} = .6: \begin{array}{l} \text{Cu @ .23} = 169 \\ \text{Cu @ .24} = 173 \end{array} \left. \vphantom{\begin{array}{l} \text{Cu @ .23} = 169 \\ \text{Cu @ .24} = 173 \end{array}} \right\} \Rightarrow \frac{(\underline{173-169})(6)}{10} + 169 = 171.4$$

$$(3) \quad \text{For Ni} = .517 \Rightarrow \left[\frac{(\underline{171.4 - 142.4})(11.7)}{20} \right] + 142.4 \approx 159.4^\circ\text{F CF}$$

$$\Rightarrow \text{CF} = 159.4$$

Question 3:

Clarify the thickness of the reactor vessel. On page 22 of WCAP-14684, it indicates that the vessel thickness is 16.83 cm (6.6 inches). On page 52, however, the thickness reported as 6.5 inches. Discuss the reason for the apparent discrepancy.

Response:

The RG&E value used is the nominal 6.5" thickness value versus the specific 6.6" thickness. RG&E considers that using the 6.5" nominal value is conservative with respect to fluence.