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SUBJECT: Provides updated Table 1 re GL 92-01, rev1, "Reactor Structural Integrity."

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ROBERT C. MECREDY
Vice President
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October 25, 1994

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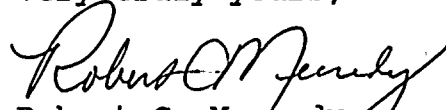
Subject: Generic Letter 92-01, Revision 1, "Reactor Structural Integrity," Data Table Update
R.E. Ginna Nuclear Power Plant
Docket No. 50-244

Ref.(a): Letter from R. C. Mecredy (RG&E), to A. R. Johnson (NRC),
"Response to Generic Letter 92-01, Request for Closure Information," dated June 30, 1994.

Dear Mr. Johnson:

The referenced letter provided data for the R.E. Ginna reactor vessel. Table 1 of the letter listed IRT_{NDT} for "SA-847 IS to LS Circ. Weld" and "SA-848 LS to Dutch Circ. Weld" as -5°F ($\sigma_t=19.7^{\circ}\text{F}$). Further evaluation with the B&W Owner's Group has shown that this value should be -19.5°F ($\sigma_t=18.5^{\circ}\text{F}$) as reflected by previous B&W reports 1801 R1, 1543 Rev. 4, and 1920P, April 1991. Please replace the Table 1 submitted in the referenced letter with the enclosed updated Table 1.

Very truly yours,


Robert C. Mecredy

REJ/350

xc: Mr. Allen R. Johnson (Mail Stop 14D1)
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Washington, D.C. 20555

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Table 1. R. E. Ginna - - Data Summary for Pressurized Thermal Shock Calculation

Beltline Material	Heat No.	IS Neut. Fluence at EOL/EFPY	IRT_{NDT} °F	Method of Determin. IRT_{NDT}	Chemistry Factor	Method of Determin. CF	%Cu	%Ni
Upper Shell Forging	123P118VA1	$3.69E+18^1$	$+30^3$ ($\sigma_t=0$)	Plant Specific	223.6	RG1.99 Table 2	0.35^9	0.68^3
Interm. Shell Forging	125S255VA1	$3.68E+19^2$	$+20^3$ ($\sigma_t=0$)	Plant Specific	16.2^6	Calculated	0.07^{10}	0.68^{10}
Lower Shell Forging	125P666VA1	$3.68E+19^2$	$+40^3$ ($\sigma_t=0$)	Plant Specific	27.80^6	Calculated	0.05^{10}	0.68^{10}
SA-1101 US to IS Circ. Weld	71249	$3.72E+18^1$	$+10^4$ ($\sigma_t=0$)	Plant Specific	173.56^7	Calculated	0.26^{11}	0.60^{11}
SA-847 IS to LS Circ. Weld	61782	$3.68E+19^2$	-19.5^5 ($\sigma_t=18.5$)	Generic	147.19^8	Calculated	0.25^{11}	0.54^{11}
SA-848 LS to Dutch. Circ. Weld	61782	N/A ¹	-19.5^5 ($\sigma_t=18.5$)	Generic	147.19^8	Calculated	0.25^{12}	0.54^{12}

Table 1. (cont.) R. E. Ginna - - Data Summary for Pressurized Thermal Shock Calculations

NOTES:

1. Values from July 2, 1992 letter from R. C. Mecredy (RG&E) to A. R. Johnson (USNRC) Subject: Reactor Vessel Structural Integrity, 10CFR50.54(f), Response to Generic Letter 92-01, Revision 1, R. E. Ginna Nuclear Power Plant.
2. Values determined from WCAP-13902 and WCAP-13893.
3. Values determined from data in Material Test Report.
4. Value determined from data in EPRI NP-373.
5. Mean values from data in BAW-1803, Revision 1; BAW-1543, Revision 4; BAW-1920P, April 1991.
6. Chemistry Factors for forging 125S255VA1 and forging 125P666VA1 were determined using REG surveillance data as reported in WCAP-13902 and WCAP 13893.
7. Chemistry Factor for weld metal SA-1101 was determined using TP3 surveillance data for weld metal SA-1101. The TP3 30 ft-lb transition temperature shift data were obtained from BAW-1803, Revision 1, while the fluence data for the capsules were obtained from BAW-1803, Revision 1 and NUREG CR-3319, Revision 1.
8. Chemistry Factor for weld metal SA-847 and weld metal SA-848 was determined using B&WOG surveillance data for weld metal SA-1135 and REG surveillance data for weld metal SA-1036. These surveillance welds were fabricated with the same wire heat as weld metal SA-847 and weld metal SA-848. The B&WOG surveillance data were obtained from BAW-1803, Revision 1. The REG surveillance data were obtained from WCAP-13902.
9. No data available for this material, therefore, 0.35% is specified as defined in Regulatory Guide 1.99, Revision 2.
10. Values obtained from BAW-2150.
11. Values obtained from BAW-2121P.
12. Values obtained from BAW-1500.

