

**AEC DISTRIBUTION FOR PART 50 DOCKET MATERIAL**  
(TEMPORARY FORM)

CONTROL NO: 5396

FILE

FROM: Niagara Mohawk Power Corp. Syracuse, N. Y. 13202 T. J. Brosnan	DATE OF DOC: 9-29-72	DATE REC'D 10-2-72	LTR X	MEMO	RPT	OTHER
TO: Mr. Skovholt	ORIG 1	CC	OTHER	SENT AEC PDR X SENT LOCAL PDR X		
CLASS: <u>U</u> /PROP INFO	INPUT	NO CYS REC'D 40	DOCKET NO: 50-220			

**DESCRIPTION:**

Ltr re our 8-3-72 ltr.....furnishing info regarding flooding potential & the HPCI System.....W/Attachment Figure 1

\* NOTE: "PLEASE CIRCULATE - INSUFFICIENT COPIES RECEIVED FOR FULL DISTRIBUTION"

PLANT NAMES: Nine Mile Point Unit No. 1

**ENCLOSURES:**

**DO NOT REMOVE  
ACKNOWLEDGED**

*39 add'l cys rec'd 10-5-72 of LTR*

FOR ACTION/INFORMATION

10-3-72

AB

Y.M.S.

BUTLER(L) W/ Copies	KNIEL(L) W/ Copies	VASSALLO(L) W/ Copies	✓ ZIEMANN(L) W/9 Copies	KNIGHTON(ENVIRO) W/ Copies
CLARK(L) W/ Copies	SCHWENCER(L) W/ Copies	H. DENTON W/ Copies	CHITWOOD(FM) W/ Copies	YOUNGBLOOD(ENVIRO) W/ Copies
GOLLER W/ Copies	STOLZ(L) W/ Copies	SCHEMEL(L) W/ Copies	DICKER(ENVIRO) W/ Copies	

**INTERNAL DISTRIBUTION**

✓ REG FILE	TECH REVIEW	VOLLMER	HARLESS	WADE	E
✓ AEC PDR	BENDRIE	DENTON		SHAFAER	F & M
✓ OGC, ROOM P-506A	SCHROEDER	GRIMES	F & M	BROWN	E
✓ MUNTZING/STAFF	✓ MACCARY *	GAMMILL	SMILEY	G. WILLIAMS	E
✓ CASE	LANGE	KASTNER	NUSSBAUMER		
✓ GIAMBUSSO	PAWLICKI	BALLARD		A/T IND	
✓ BOYD-L(BWR)	SHAO	FINE	LIC ASST.	BRATTMAN	
✓ DEYOUNG-L(PWR)	✓ KNUTH *	ENVIRO	SERVICE L	SALTZMAN	
✓ SKOVHOLT-L	STELLO	MULLER	MASON L		
P. COLLINS	MOORE	DICKER	WILSON L	PLANS	
✓ REG OPR	✓ THOMPSON	KNIGHTON	KARI L	MCDONALD	
✓ FILE & REGION (2)	✓ TEDESCO *	YOUNGBLOOD	SMITH L	DUBE	
MORRIS	LONG	PROJECT LEADER	GEARIN L	INFO	
STELLE	LAINAS		DIGGS L	C. MILES	
	BENAROYA		TEETS L		

**EXTERNAL DISTRIBUTION**

✓ 1-LOCAL PDR Oswego, N. Y.	(1)(5)(9)-NATIONAL LAB'S	1-PDR-SAN/LA/NY
✓ 1-DTIE(ABERNATHY)	1-R. CARROLL-OC, GT-B227	1-GERALD LELLOUCHE
✓ 1-NSIC(BUCHANAN)	1-R. CATLIN, A-170-GT	BROOKHAVEN NAT. LAB
1-ASLB-YORE/SAYRE	1-CONSULANT'S	1-BOLAND, IDAHO FALLS,
WOODWARD/H. ST.	NEWARK/BLUME/AGABIAN	IDAHO(50-331 Only)
✓ 16-CYS ACRS HOLDING SENT TO LIC ASST.	R. DIGGS FOR DIST ON 10-3-72	1-RD...MULLER...F-309GT

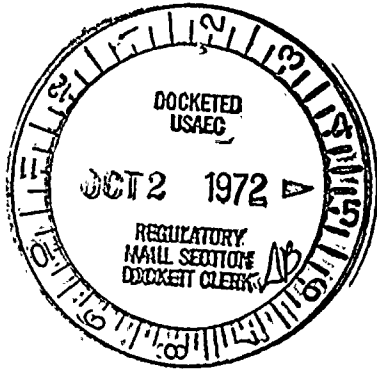
100-44111-2-1

63

100-443887-100

1. *Chlorophyll a* and *Chlorophyll b* were determined by the method of Lichtenthaler and Whistler (1972). The total chlorophyll content was determined by the method of Arar and Cook (1980). The carotenoid content was determined by the method of Lichtenthaler and Whistler (1972). The total carotenoid content was determined by the method of Arar and Cook (1980). The total protein content was determined by the method of Lowry et al. (1951). The total lipid content was determined by the method of Bligh and Dyer (1959). The total carbohydrate content was determined by the method of Dubois and Gilles (1950). The total nucleic acid content was determined by the method of Burton (1956). The total ash content was determined by the method of AOAC (1990). The total moisture content was determined by the method of AOAC (1990). The total dry matter content was determined by the method of AOAC (1990). The total organic acid content was determined by the method of AOAC (1990). The total alkaloid content was determined by the method of AOAC (1990). The total saponin content was determined by the method of AOAC (1990). The total tannin content was determined by the method of AOAC (1990). The total flavonoid content was determined by the method of AOAC (1990). The total phenol content was determined by the method of AOAC (1990). The total terpenoid content was determined by the method of AOAC (1990). The total steroid content was determined by the method of AOAC (1990). The total glycoside content was determined by the method of AOAC (1990). The total alkaloid content was determined by the method of AOAC (1990). The total saponin content was determined by the method of AOAC (1990). The total tannin content was determined by the method of AOAC (1990). The total flavonoid content was determined by the method of AOAC (1990). The total phenol content was determined by the method of AOAC (1990). The total terpenoid content was determined by the method of AOAC (1990). The total steroid content was determined by the method of AOAC (1990). The total glycoside content was determined by the method of AOAC (1990).

31-3-



## NIAGARA MOHAWK POWER CORPORATION

NIAGARA  MOHAWK300 ERIE BOULEVARD, WEST  
SYRACUSE, N. Y. 13202

September 29, 1972



Mr. Donald J. Skovholt  
Assistant Director for Operating Reactors  
Directorate of Licensing  
United States Atomic Energy Commission  
Washington, D. C. 20545

Dear Mr. Skovholt:

Re: Nine Mile Point Unit No. 1  
Docket 50-220

Your letter of August 3, 1972, requested a review of our Nine Mile Point Unit No. 1 facility to determine (1) whether failure of any equipment which does not meet the criteria of Class I seismic construction, particularly the circulating water system, could cause flooding sufficient to adversely affect the performance of engineered safety systems, and (2) whether failure of any equipment could cause flooding such that common mode failure of redundant safety related equipment would result. The requested studies have been completed with the result that there is no flooding potential for existing engineered safety systems. For the case of the HPCI system, which is scheduled to be in service by the end of the Spring 1973 refueling outage, flood protection is being incorporated as described below.

Reactor Building

The reactor building houses a large number of engineered safety systems at various elevations throughout the structure. These include the core spray system pumps and discharge valves at the corners of the building at elevation 198 feet, the pumps and valves of the containment spray system - also at elevation 198 feet, the pumps and explosive valves for the liquid poison system at elevation 298 feet, the control rod drive pump motors at elevation 237 feet, the auto depressurization system valves located on the main steam lines inside the drywell, the containment isolation valving and inerting system components at various locations in the building, sensors of the reactor protection system located in the north, east and west instrument rooms, power boards 16, 17, 167 at elevation 281 feet and power boards 161 and 171 at elevation 261 feet.

27

September 29, 1972

Investigation of piping routed within the reactor building reveals that there are no non-Class I systems of sufficient size whose failure could cause flooding anywhere in the building. Most of these non-Class I lines are associated with drain and sump systems.

#### Turbine Building

Engineered safety systems housed within the turbine building include the following:

- a. The isolation valves for the normal reactor building ventilation system and the fans, valves and filters associated with the reactor building emergency ventilation system are located in the turbine building above elevation 290 feet.
- b. The High Pressure Coolant Injection (HPCI) system was previously committed to be in service by the end of the Spring 1973 refueling outage. It consists of the condensate, booster and feedwater pumps, and associated piping and valving. The condensate pumps are located at elevation 243 feet with their motors at elevation 252 feet, as shown in Figure 1. Both the booster and feedwater pumps are located at elevation 261 feet. (The 115KV reserve bus and reserve transformers which serve this system are located outside the turbine building at, or above, grade elevation in an area not subject to flooding.)
- c. The diesel generator and Station battery systems are both located at elevation 261 feet.
- d. All power boards serving engineered safety systems are located at, or above, elevation 261 feet. These include power boards 11, 12, 102 and 103 at elevation 261 feet, power board 101 at elevation 277 feet, and power board 1671 at elevation 300 feet.

Analysis shows that there are several non-Class I piping systems within the turbine building, the largest of which are the circulating water and service water piping systems. Failure of these lines would drain to the turbine building subfloors below elevation 261 feet and would eventually fill this area, assuming the inrush of water exceeds the 200 gpm capacity of the turbine building sump pumps. High level alarm from the turbine building sump pump pit at elevation 243 feet would alert the control room operator to an abnormally high water condition. If flooding continues, the water level would rise above the condensate pumps with a second high level alarm being given in the control room from the sump pump at elevation 250 feet. In the event of total failure of the largest pipe (one 72-inch circulating water line), it would take approximately 40 minutes after the operator receives the first high water alarm



September 29, 1972

for flooding to reach elevation 261 feet. Therefore, ample time is available for the operator to manually shut off the pump responsible for the flooding condition.

Portions of the HPCI system are the only safety-related equipment located below the 261 foot elevation. Before the HPCI is placed in service, the cavity housing this system's equipment below elevation 261 feet will be suitably protected against flooding to that elevation by structures meeting Class I requirements.

#### Screenhouse

The only engineered safety equipment located in the screenhouse are four containment spray raw water pumps and two diesel engine cooling water pumps. All of these are located at or above elevation 256 feet, as indicated in Figure 1. There are a number of non-Class I piping systems located in the screenhouse such as the circulating water system and the service water system.

Investigation shows that failure of these lines would first fill the cavity below elevation 256 feet which houses the circulating water and service water pumps before spilling over to the inlet forebay. There is no way for the water level to rise sufficiently above the 256 foot elevation so as to adversely affect the six pumps mentioned above.

Very truly yours,



T. J. Brosnan  
Vice President and Chief Engineer

TJB/vk





