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 50-287 Oconee Nuclear Station, Unit 3, Duke Power Co.  
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DOCKET #  
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SUBJECT: Forwards response to NRC 791121 ltr requesting addl info re small break LOCA. Loads imposed on tubes of once-through steam generator during postulated slug flow evaluated & found acceptable.

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DUKE POWER COMPANY

POWER BUILDING

422 SOUTH CHURCH STREET, CHARLOTTE, N. C. 28242

WILLIAM O. PARKER, JR.  
VICE PRESIDENT  
STEAM PRODUCTION

January 24, 1980

TELEPHONE: AREA 704  
373-4083

Mr. Harold R. Denton, Director  
Office of Nuclear Reactor Regulation  
U. S. Nuclear Regulatory Commission  
Washington, D. C. 20555

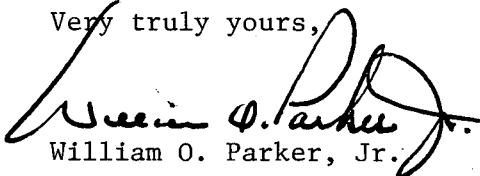
Attention: Mr. R. W. Reid, Chief  
Operating Reactors Branch No. 4

Re: Oconee Nuclear Station  
Docket Nos. 50-269, -270, -287

Dear Sir:

With regard to my letters of December 3 and 28, 1979 and in response to the Staff's letter of November 21, 1979, please find attached a response to the request for additional information concerning small break loss of coolant accidents.

Very truly yours,

  
William O. Parker, Jr.

RLG:scs

Attachment

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S.I.  
357

DUKE POWER COMPANY  
Response to Request for Additional Information  
Small Break Loss-of-Coolant Accident

Oconee Nuclear Station

1. Transitions from solid natural circulation to reflux boiling and back to solid natural circulation may cause slug flow in the hot leg piping. By use of analysis and/or experiment address the mechanical effects of the induced slug flow on steam generator tubes.

RESPONSE

The loads imposed on the tubes of the OTSG during the postulated "slug flow" have been conservatively evaluated and found to be acceptable. Based on very conservative assumptions, the end loading on each tube will be 21.5 lb<sub>f</sub> compared to a theoretical buckling load of about 700 lb<sub>f</sub>.

It was assumed for this analysis that a water level has been established in the hot leg piping and inside the tubes of OTSG. The transient consists of a "front" of solid water impinging on the primary face of the upper tubesheet. The flow was assumed to be equal to full 100% power flow (about 70,000,000 lb/hr). The load is assumed to be a suddenly - applied load. The upper tubesheet is conservatively assumed to offer no resistance to the load and the lower tubesheet is assumed to be fixed so that the entire load is absorbed by tubes directly under the primary inlet nozzle. The flow is assumed to not follow the diffuser so that the velocity impinging on the tubesheet is the same as the velocity in the 36-inch nozzle. Hot leg temperature is assumed to be 605°F.

The velocity in the 36-inch pipe would be 64.4 ft/sec. By use of the momentum equation, the steady-state force on the upper tubesheet due to the velocity would be 16,080 lb<sub>f</sub>. There are about 1500 tubes in a 36-inch diameter circle. Thus the 32,160 lb<sub>f</sub> will result in 21.5 lb<sub>f</sub> per tube. Since the cross-sectional area of each tube is 0.070 in, the momentary axial compressive stress in these tubes would be 307 psi.