

## NRC DISTRIBUTION FOR PART 50 DOCKET MATERIAL

FILE NUMBER

TO: ROBERT W. REID

FROM: H.B. ROBINSON  
E.E.UTLEYDATE OF DOCUMENT  
3/3/77

DATE RECEIVED 3/14/77

☒ LETTER  
☐ ORIGINAL  
COPY  
☐ NOTORIZED  
☒ UNCLASSIFIED

PROP

INPUT FORM

NUMBER OF COPIES RECEIVED

1 signed

DESCRIPTION Ltr. re ltr from D.F. Ross to  
W.S. Nachodom dtd 11/23/76, and rpt (XN-76-54),  
dtd December '76 trans the following:ENCLOSURE Consisting of table 1, furnishing  
HB Robinson increase Fission Gas LOCA results.

(40 cys rec'd)

PLANT NAME: H. B. Robinson

## SAFETY

## FOR ACTION/INFORMATION

## ENVIRO

ASSIGNED AD:

BRANCH CHIEF:

PROJECT MANAGER:

LIC. ASST. :

ASSIGNED AD:

BRANCH CHIEF:

PROJECT MANAGER:

LIC. ASST. :

Reid  
Zwetzig  
Ingram

## INTERNAL DISTRIBUTION

REG FILE

NRC PDR

I &amp; E (2)

OELD

GOSSICK &amp; STAFF

MIPC

CASE

HANAUER

HARLESS

SYSTEMS SAFETY

HEINEMAN

SCHROEDER

ENGINEERING

MACARRY

BOSNAK

SIHWEIL

PAWLICKI

PLANT SYSTEMS

TEDESCO

BENAROYA

LAINAS

IPPOLITO

KIRKWOOD

OPERATING REACTORS

STELLO

SITE SAFETY &amp;

ENVIRO ANALYSIS

DENTON &amp; MULLER

ENVIRO TECH.

ERNST

BALLARD

YOUNGBLOOD

SITE TECH.

GAMMILL

STEPP

HULMAN

SITE ANALYSIS

VOLLMER

BUNCH

J. COLLINS

KREGER

PROJECT MANAGEMENT

BOYD

P. COLLINS

HOUSTON

PETERSON

MELTZ

HELTEMES

SKOVHOLT

REACTOR SAFETY

ROSS

NOVAK

ROSZTOCZY

CHECK

AT &amp; I

SALTZMAN

RUTBERG

OPERATING TECH.

EISENHUT

SHAO

BAER

BUTLER

GRIMES

## EXTERNAL DISTRIBUTION

LPDR: Hartselle, SC

TIC:

NSIC:

ASLB:

ACRS 16 CYS HOLDING/SENT

NAT. LAB:

REG V. IE

IA PDR

CONSULTANTS:

AS CAB B

BROOKHAVEN NAT. LAB.  
ULRIKSON (ORNL)

CONTROL NUMBER

770750216

770750302



Carolina Power & Light Company

March 3, 1977

FILE: NG-3514(R)

REGULATORY DOCKET FILE COPY

SERIAL: NG-77-237

Director of Nuclear Reactor Regulation  
ATTN: Robert W. Reid, Chief  
Operating Reactors Branch 4  
U. S. Nuclear Regulatory Commission  
Washington, D. C. 20555

H. B. ROBINSON STEAM ELECTRIC PLANT UNIT NO. 2  
DOCKET NO. 50-261  
FACILITY OPERATING LICENSE NO. DPR-23  
EFFECTS OF INCREASED FISSION GAS RELEASES



- Reference: (1) Letter from D. F. Ross (NRC) to W. S. Nachodom (ENC)  
dated November 23, 1976
- (2) "LOCA Analysis for H. B. Robinson Unit No. 2 Using WREM  
Based PWR ECCS Evaluation Model with Reduced LPSI Flow,  
Steam Generator Plugging, and Increased Upper Head  
Temperature," XN-76-54, December, 1976

Dear Mr. Reid:

Your letter of November 29, 1976, requested information on the impact of a new fission gas release model on fuel design limits. Our response of December 31, 1976, provided information for the fuel supplied by the Westinghouse Electric Corporation, which is the only fuel in the unit which will have achieved a burnup of more than 20,000 MWD/MTU by June 1, 1977. The fuel supplied by the Exxon Nuclear Corporation has not yet achieved 20,000 MWD/MTU but will reach this burnup by the end of the current cycle. This letter provides the requested data for the Exxon Nuclear supplied fuel.

The impact of additional fission gas release after 20,000 MWD/MTU burnup has been investigated. This investigation was conducted for the H. B. Robinson Unit 2 15x15 fuel supplied by Exxon Nuclear using the NRC approved PWR fuel densification model with modifications to incorporate the fission gas release formula specified in Reference 1. The revised analysis uses a history which envelopes the power limits given in Reference 2. With the revised release formula, a peak pin pressure of 1855 psia is calculated, compared to 1445 psia with the present model. The maximum fission gas release fraction is calculated to be 0.24 with the revised model, compared to .05 with the present model.

336 Fayetteville Street • P. O. Box 1551 • Raleigh, N. C. 27602

2647

770750216

March 3, 1977

In both analyses, the fuel pellet-to-clad gap is closed for the power levels and exposures ( $>20,000$  MWD/MTU); hence, fuel average temperatures were found to be very nearly the same for the same LHGR and exposure (less than  $70^{\circ}\text{F}$  increase due to the fission gas release model revision was calculated). It is also observed that pin pressure at end-of-life (EOL) did not exceed the system operating pressure.

To determine the LOCA impact of the increased fission gas release, a heatup calculation was performed. The blowdown and reflood boundary conditions were obtained from the limiting break (0.8 DECLG) as reported in Reference 2. RELAP4/HOTCHANNEL and TOODEE2/HOT ROD calculations were performed using the calculated exposed fuel geometry, fission gas inventory and stored energy. The limiting LOCA conditions were found to be those corresponding to beginning of life (BOL). Table 1 shows the BOL LOCA results as compared to the EOL results where the effect of the fission gas release model has maximum impact. Since the BOL LOCA results are still controlling, the new fission gas model has no impact on any of the plant safety analyses for this fuel.

Yours very truly,



E. E. Utley  
Senior Vice President  
Power Supply

CSB/MFP/dkm  
Attachment

TABLE 1

H. B. ROBINSON INCREASE FISSION GAS LOCA RESULTS

	<u>BOL</u>	<u>EOL</u>
Peak Cladding Temperature, °F	2152	1885
Peak Temperature Location, ft	6.375	7.125
Time of PCT (sec)	123.5	129.5
Local Zr/H <sub>w</sub> O Reaction (Max.), %	7.89	1.52
Local Zr/H <sub>2</sub> O Location, ft	6.125	6.125
Total Zr/H <sub>2</sub> O	<1%	<1%
Hot Rod Burst Time, sec	46.66	44.44
Hot Rod Burst Location, ft	6.125	6.125