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SUBJECT: Forwards flux maps from last half of Cycle 12 to supplement data provided in 890512 ltr re 10 W/O gadolinia program.

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H. B. ROBINSON STEAM ELECTRIC PLANT, UNIT NO. 2
DOCKET NO. 50-261/LICENSE NO. DPR-23
USE OF 10-WEIGHT PERCENT GADOLINIA DURING CYCLE 12

Gentlemen:

By letter dated January 19, 1987, Carolina Power & Light Company committed to provide data to the NRC regarding the 10 W/O Gadolinia Program. Enclosed are flux maps from the last half of Cycle 12 to supplement data provided you by letter dated May 12, 1988.

Questions regarding this matter may be referred to Mr. R. W. Prunty at (919) 546-7318.

Yours very truly,

L. I. Loflin
Manager
Nuclear Licensing Section

JSK/crs (394CRS)

Enclosure

*cc: Mr. S. D. Ebneter
Mr. L. Garner (NRC - HBR)
Mr. R. Lo

A001
1/1

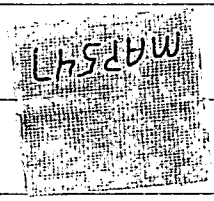
411 Fayetteville Street • P. O. Box 1551 • Raleigh, N. C. 27602

C12 MAP547 04/04/88 D-155 7214MWD/MTU 58.89%HFP 54P 1 B-529 FCFM

SUMMARY OF INCORE RESULTS	MEASURED			WITH UNCERTAINTY FACTOR	TECH. SPEC. LIMIT
FZ (MAX. ASSEMBLY)	= 1.716 LOC J15				
FZ (MAX. AVERAGE)	= 1.202				
KW/FT (MAX. AVERAGE)	= 4.782 LOC C 8			5.172	
KW/FT (MAX. PEAK)	= 6.913 LOC C 8			7.477	
F-DELTA-H (MAX. ASSEMBLY)	= 1.393 LOC C 8	REGION 15			
F-DELTA-H (MAX. ASSEMBLY)	= 1.315 LOC L12	REGION 14			
F-DELTA-H (MAX. ASSEMBLY)	= 1.064 LOC E11	REGION 12R			
F-DELTA-H (MAX. ASSEMBLY)	= 1.077 LOC N 7	REGION 13A			
F-DELTA-H (MAX. ASSEMBLY)	= 0.261 LOC R 8	REGION 13			
F-DELTA-H (PEAK PIN)	= 1.578 LOC L 3	REGION 15		1.641	1.786
F-DELTA-H (PEAK PIN)	= 1.451 LOC K13	REGION 14		1.509	1.786
F-DELTA-H (PEAK PIN)	= 1.119 LOC E11	REGION 12R		1.163	1.786
F-DELTA-H (PEAK PIN)	= 1.143 LOC N 7	REGION 13A		1.188	1.786
F-DELTA-H (PEAK PIN)	= 0.418 LOC R 7	REGION 13		0.434	1.786
FQT (PENALIZED)	= 1.995 LOC E 3	REGION 15		2.095	3.838
FQT (PENALIZED)	= 1.841 LOC K13	REGION 14		1.933	3.838
FQT (PENALIZED)	= 1.385 LOC L11	REGION 12R		1.455	3.838
FQT (PENALIZED)	= 1.445 LOC N 7	REGION 13A		1.518	3.838
FQT (PENALIZED)	= 0.740 LOC R 7	REGION 13		0.777	3.838
FQN (WITH LOCAL PEAKING)	= 1.955 LOC C 8	REGION 15			
FQN (WITH LOCAL PEAKING)	= 1.722 LOC K13	REGION 14			
FQN (WITH LOCAL PEAKING)	= 1.313 LOC E11	REGION 12R			
FQN (WITH LOCAL PEAKING)	= 1.381 LOC N 7	REGION 13A			
FQN (WITH LOCAL PEAKING)	= 0.702 LOC R 7	REGION 13			
CALCULATED POWER TILTS(NORMALIZED TO 1.000)					
			(-,+) QUADRANT =	1.0010	1.02
			(+,+) QUADRANT =	0.9965	1.02
			(-,-) QUADRANT =	1.0046	1.02
			(+,-) QUADRANT =	0.9978	1.02
AXIAL OFFSET	= -2.401				
FXY (NEGLECTING GRIDS)	= 1.663 LOC E 3 NODE 12				
FQZ BASED APL FOR 3% TARGET BAND = 99.88%					
FQZ BASED APL FOR 5% TARGET BAND = 97.18%					

FORM 0113 (02/83)

R'CVD.....DATE.....
INCORE - CP&L VERSION PNR16021 - 04/22/88



FORM 2113 (02/83)

C12 MAP547 04/04/88 D-155 7214MWD/MTU 58.89%HFP 54P 1 B-529 FCFM

FINAL COMPARISON OF SATURATION ACTIVITY AND PDQ ACTIVATION

THIMBLE		STATUS	MEASURED AXIAL FACTOR	REGION PERCENTAGE DIFFERENCE 1- 4	4-20	20-43	43-58	58-61	F*S(Z)
1	M 3	GOOD	1.1651	-11.6578	-8.6935	2.6948	-0.0479	11.0337	1.1950
2	J15	NONE							
3	F 4	GOOD	1.1526	8.1834	-2.9779	-0.4854	-2.8342	-3.2856	1.1685
4	L 8	GOOD	1.1958	19.7678	10.7707	-2.1926	-0.7433	15.9157	1.1958
5	F 8	GOOD	1.1653	8.6267	14.1331	-0.0678	0.1163	-4.6117	1.1653
6	D12	GOOD	1.1319	-19.7068	-10.8557	-2.1556	-1.9034	3.1211	1.1694
7	B 5	GOOD	1.1713	-21.3039	-10.2972	2.7653	0.8539	0.0188	1.1867
8	H 6	GOOD	1.1648	10.7655	13.5344	0.0962	1.4454	0.1970	1.1648
9	J 3	GOOD	1.1816	14.4405	-1.4015	-2.6872	-3.4468	-6.2384	1.1996
10	D 3	GOOD	1.1791	-15.1678	-9.5872	1.4796	-2.3856	6.5512	1.2032
11	L 9	GOOD	1.1567	12.7648	5.7181	-1.5456	0.1173	4.3671	1.1567
12	B10	GOOD	1.1764	-24.6711	-5.6232	2.1257	-0.1489	-12.0178	1.1996
13	L 4	GOOD	1.1380	-12.6168	-7.0382	2.2723	2.1768	2.0856	1.1608
14	F13	GOOD	1.1833	-5.7111	-7.4159	0.4313	0.1572	-1.6290	1.1833
15	F 6	GOOD	1.1726	15.1207	3.3702	-0.4484	-0.9104	4.3530	1.1726
16	J12	GOOD	1.1650	8.1943	8.0445	-0.0501	0.8074	-3.4965	1.1688
17	B 7	GOOD	1.2035	-4.2244	-1.7987	0.0155	-2.9350	-15.8829	1.2280
18	H 1	NONE							
19	G 9	GOOD	1.1824	26.6066	11.5374	-6.3492	-4.1259	-6.2878	1.1824
20	G 7	GOOD	1.1760	16.9338	9.8141	-5.3135	-3.0227	4.1983	1.1760
21	F11	GOOD	1.1303	-15.8420	-3.8206	-0.6196	2.6802	5.2787	1.1303
22	N 5	GOOD	1.1411	-20.1653	-9.5108	1.8899	3.4477	1.4092	1.1610
23	J10	GOOD	1.1575	15.7702	7.3985	-2.3452	-0.3598	8.3570	1.1575
24	J 5	GOOD	1.1474	10.3757	5.7479	-2.1314	0.9163	7.9345	1.1474
25	B 8	GOOD	1.2399	8.8153	-2.4748	-0.6254	-2.9557	-8.9354	1.2423
26	N10	GOOD	1.1486	1.3944	-5.7220	-0.6571	-2.1504	-12.1584	1.1685
27	C12	NONE							
28	J 7	GOOD	1.1770	28.7637	15.7310	-2.2395	-2.5420	-5.5399	1.1770
29	D 7	GOOD	1.1736	18.8710	5.9450	-1.9312	-2.2382	-9.0320	1.1736
30	L14	GOOD	1.1611	-17.1032	-9.5883	3.2845	2.1428	0.5473	1.1763
31	F 2	GOOD	1.1679	-21.1339	-6.3245	2.8039	3.6594	-1.3882	1.1887
32	F 9	GOOD	1.1623	23.4803	9.8736	-2.0900	-2.2063	-2.6060	1.1623
33	N 7	NONE							
34	A 9	NONE							
35	N12	GOOD	1.1786	-5.9910	-7.7104	2.3518	-3.0687	0.6474	1.2089
36	R 8	NONE							
37	H 4	NONE							
38	H11	GOOD	1.1985	35.5843	13.1783	-0.9690	1.0389	4.6288	1.1985
39	D 5	GOOD	1.1397	-19.6853	-6.4491	1.6257	0.5122	-6.1880	1.1621
40	L 6	GOOD	1.1214	-13.8049	-1.2189	0.3637	2.2421	3.4552	1.1225
41	D10	GOOD	1.1612	-9.5186	-5.1495	0.0693	0.6926	15.6575	1.1849
42	G14	GOOD	1.2059	-20.8185	-1.8639	0.5511	-0.8581	-10.9522	1.2227
43	H13	GOOD	1.1958	9.1693	1.8744	-2.2301	-1.1403	-7.8733	1.2109
44	C 8	GOOD	1.2088	11.0332	6.8679	3.0069	2.3525	-11.7323	1.2088
45	H 3	NONE							
46	N 8	GOOD	1.1986	8.5544	4.5547	0.9787	1.0484	-7.3815	1.2001
47	E11	GOOD	1.1557	3.8896	0.8121	6.9520	7.6199	31.6792	1.1748
48	L11	GOOD	1.1625	13.8943	-0.6088	3.2652	1.7643	11.7699	1.1862
49	E 5	GOOD	1.1522	5.8978	-3.2869	1.0709	0.6651	19.8394	1.1714
50	L 5	NONE							
AVG. OF ABSOLUTE VALUES OF GOOD THIMBLES ONLY			1.1694	14.54	6.79	1.88	1.87	7.32	

FORM 0113 (02/83)

MEASURED AXIAL PEAKING FACTORS C12 MAP547 04/04/88 D-155 7214MWD/MTU 58.89%HFP 54P 1 B-529 FCFM

					H 1									
							1.168							
							F 2							
		1.165		1.182					1.179					
		M 3		J 3	H 3				D 3					
			1.138				1.153							
			L 4		H 4		F 4							
	1.141			1.147				1.152	1.140			1.171		
	N 5		L 5	J 5				E 5	D 5			B 5		
			1.121		1.165		1.173							
			L 6		H 6		F 6							
				1.177		1.176			1.174			1.203		
	N 7			J 7		G 7			D 7			B 7		
	1.199		1.196				1.165				1.209	1.240		
R 8	N 8		L 8				F 8				C 8	B 8		
			1.157			1.182	1.162							
			L 9			G 9	F 9						A 9	
	1.149			1.158					1.161			1.176		
	N10			J10					D10			B10		
			1.162		1.199		1.130	1.156						
			L11		H11		F11	E11						
	1.179			1.165					1.132					
	N12			J12					D12		C12			
					1.196		1.183							
					H13		F13							
			1.161			1.206								
			L14			G14								
				J15										

FORM 0113 (02/83)

C12 MAP547 04/04/88 D-155 7214MWD/MTU 58.89%HFP 54P 1 B-529 FCFM

MAX FQT INCLUDES LOCA AXIAL PENALTY FACTOR

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.731	0.711	0.731							1
2					1.770	2.049	1.973	1.619	1.987	2.026	1.779					2
3				1.159	2.088	1.880	1.443	1.969	1.468	1.872	2.095	1.149				3
4			1.098	1.639	1.813	1.387	1.584	1.252	1.590	1.366	1.820	1.637	1.099			4
5		1.735	2.046	1.802	1.404	1.868	1.566	1.228	1.585	1.848	1.412	1.793	2.060	1.750		5
6		1.981	1.827	1.324	1.838	1.220	1.264	1.840	1.237	1.196	1.858	1.357	1.883	2.011		6
7	0.777	2.093	1.518	1.631	1.579	1.238	1.475	1.511	1.449	1.232	1.576	1.617	1.483	1.995	0.733	7
8	0.756	1.714	2.052	1.288	1.234	1.816	1.511	1.207	1.490	1.839	1.240	1.303	2.077	1.641	0.713	8
9	0.711	1.999	1.467	1.624	1.574	1.242	1.467	1.476	1.441	1.242	1.581	1.650	1.483	2.004	0.727	9
10		1.970	1.824	1.353	1.894	1.213	1.228	1.799	1.223	1.205	1.870	1.339	1.866	2.012		10
11		1.751	2.065	1.835	1.455	1.933	1.610	1.240	1.589	1.828	1.452	1.820	2.055	1.782		11
12			1.111	1.676	1.894	1.459	1.623	1.278	1.610	1.360	1.818	1.581	1.052			12
13				1.153	2.068	1.933	1.503	2.015	1.461	1.841	2.014	1.099				13
14					1.751	2.000	2.061	1.654	1.977	2.002	1.741					14
15							0.731	0.713	0.732							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

112	D10	1.23027	1.79902	1.81420	1.42751	6.27099	0.9845	1.1674	1.2379	-3.3874
113	C10	1.59841	2.35557	2.36358	1.76288	8.08045	1.2686	1.5155	1.7258	-2.1347
114	B10	1.47404	2.19252	2.18878	1.49074	7.34607	1.1533	1.4041	1.8607	-0.1765
115	P11	1.12783	1.61788	1.58741	1.12156	5.45468	0.8563	1.0372	1.6189	0.6734
116	N11	1.70483	2.42905	2.38755	1.70438	8.22581	1.2914	1.5571	1.9095	0.5100
117	M11	1.70793	2.36962	2.33267	1.72651	8.13672	1.2774	1.5227	1.6963	0.2259
118	L11	1.54937	1.90663	1.82108	1.41164	6.68873	1.0501	1.2445	1.3451	3.3380
119	K11	1.72359	2.40292	2.38795	1.80299	8.31745	1.3058	1.5452	1.7869	-0.7747
120	J11	1.36186	2.01095	2.06650	1.60336	7.04266	1.1057	1.3176	1.4886	-4.2180
121	H11	0.99832	1.57061	1.67837	1.34335	5.59065	0.8777	1.0928	1.1464	-8.0991
122	G11	1.29661	1.97128	2.07819	1.63097	6.97705	1.0953	1.3306	1.4689	-6.3244
123	F11	1.58295	2.31341	2.39980	1.86748	8.16365	1.2816	1.5240	1.6901	-4.5435
124	E11	1.51070	1.91885	1.85556	1.49079	6.77590	1.0638	1.2485	1.3430	1.2281
125	D11	1.67549	2.35854	2.33296	1.80516	8.17216	1.2830	1.5138	1.6827	-1.2736
126	C11	1.68106	2.41621	2.37989	1.75409	8.23125	1.2923	1.5447	1.8997	-0.4460
127	B11	1.12666	1.64323	1.62260	1.13241	5.52490	0.8674	1.0532	1.6478	0.2694
128	N12	0.65316	0.91959	0.89793	0.64822	3.11890	0.4896	0.5898	1.0269	0.8527
129	M12	1.37159	1.90329	1.85421	1.35844	6.48752	1.0185	1.2254	1.5496	0.9591
130	L12	1.78981	2.42817	2.37414	1.78149	8.37360	1.3146	1.5669	1.7508	0.7446
131	K12	1.36470	1.86873	1.84000	1.40541	6.47885	1.0171	1.2042	1.3489	-0.1849
132	J12	1.33311	2.06019	2.15687	1.69026	7.24043	1.1367	1.3831	1.5005	-6.2680
133	H12	0.61650	1.42214	1.75025	1.38116	5.17005	0.8117	1.1291	1.1814	-21.1365
134	G12	1.24659	1.99486	2.14648	1.68956	7.07750	1.1111	1.3742	1.4882	-8.4013
135	F12	1.24383	1.79488	1.85193	1.44023	6.33088	0.9939	1.1854	1.2580	-4.0034
136	E12	1.67944	2.35018	2.34600	1.81063	8.18625	1.2852	1.4967	1.6812	-1.5516
137	D12	1.29209	1.80767	1.79450	1.37986	6.27412	0.9850	1.1519	1.4615	-1.1891
138	C12	0.62803	0.87336	0.86688	0.66647	3.03474	0.4764	0.5573	0.9724	-1.0529
139	M13	0.66229	0.94832	0.94315	0.70334	3.25709	0.5113	0.6051	1.0665	-1.1018
140	L13	1.64241	2.46257	2.48972	1.79395	8.38865	1.3170	1.5834	1.9119	-2.1302
141	K13	1.68565	2.41254	2.39679	1.78598	8.28096	1.3001	1.5428	1.7872	-1.0214
142	J13	1.35689	1.98817	1.97640	1.46490	6.78636	1.0654	1.2872	1.3896	-1.4182
143	H13	1.57173	2.54549	2.62021	1.87677	8.61420	1.3524	1.6807	1.8636	-4.4085
144	G13	1.26019	1.92907	1.98101	1.44163	6.61190	1.0380	1.2768	1.3508	-3.5298
145	F13	1.59110	2.31773	2.36035	1.76507	8.03424	1.2613	1.5350	1.7023	-2.6959
146	E13	1.67314	2.39051	2.38661	1.77192	8.22217	1.2908	1.5371	1.8623	-1.1540
147	D13	0.64790	0.90141	0.89808	0.70485	3.15224	0.4949	0.5776	1.0159	-1.7006
148	L14	1.08466	1.63632	1.65120	1.17626	5.54844	0.8711	1.0515	1.6187	-1.9190
149	K14	1.41680	2.17800	2.22002	1.54042	7.35523	1.1547	1.4206	1.8497	-2.2521
150	J14	1.63713	2.38583	2.26128	1.52472	7.80896	1.2260	1.5560	1.9055	3.0344
151	H14	1.32350	1.97322	1.92275	1.25236	6.47183	1.0160	1.2710	1.5290	1.8789
152	G14	1.57940	2.34910	2.30332	1.50171	7.73353	1.2141	1.5078	1.8282	1.5966
153	F14	1.50190	2.17996	2.14921	1.49648	7.32755	1.1504	1.3989	1.8514	0.4936
154	E14	1.12035	1.60901	1.60350	1.17019	5.50304	0.8639	1.0482	1.6094	-0.8056
155	J15	0.37913	0.58329	0.47218	0.0	1.43460	0.2252	0.3865	0.6757	34.1727
156	H15	0.44709	0.64940	0.50355	0.0	1.60004	0.2512	0.4168	0.6592	37.0575
157	G15	0.41123	0.59395	0.45791	0.0	1.46309	0.2297	0.3793	0.6770	37.4052

REGION 15 LIMITING FQT = 2.0952 IN ASSEMBLY E 3
REGION 14 LIMITING FQT = 1.9328 IN ASSEMBLY K13
REGION 12R LIMITING FQT = 1.4548 IN ASSEMBLY L11
REGION 13A LIMITING FQT = 1.5178 IN ASSEMBLY N 7
REGION 13 LIMITING FQT = 0.7774 IN ASSEMBLY R 7

196

ASM"Y RELATIVE POWER EXPECTED / MEASURED/ % DIFF SUMS: 156.9923 / 156.9933 / -13.0764

						0.232.	0.254.	0.232.						
						0.228.	0.249.	0.228.						
						-1.88.	-1.96.	-1.76.						
					0.882.	1.169.	1.227.	1.022.	1.227.	1.169.	0.882.			
					0.867.	1.144.	1.202.	1.001.	1.226.	1.167.	0.870.			
					-1.72.	-2.11.	-2.07.	-2.09.	-0.05.	-0.13.	-1.34.			
				0.522.	1.335.	1.287.	1.051.	1.353.	1.051.	1.287.	1.335.	0.522.		
				0.513.	1.317.	1.266.	1.027.	1.323.	1.041.	1.275.	1.309.	0.505.		
				-1.79.	-1.31.	-1.67.	-2.28.	-2.25.	-0.94.	-0.99.	-1.95.	-3.35.		
			0.503.	1.027.	1.291.	0.991.	1.106.	0.799.	1.106.	0.991.	1.291.	1.027.	0.503.	
			0.494.	1.012.	1.278.	0.986.	1.101.	0.792.	1.086.	0.975.	1.271.	1.007.	0.490.	
			-1.80.	-1.47.	-1.02.	-0.57.	-0.45.	-0.91.	-1.79.	-1.66.	-1.56.	-1.93.	-2.47.	
		0.879.	1.326.	1.287.	1.033.	1.278.	1.074.	0.846.	1.074.	1.278.	1.033.	1.287.	1.326.	0.879.
		0.866.	1.305.	1.276.	1.024.	1.286.	1.093.	0.870.	1.087.	1.274.	1.027.	1.268.	1.302.	0.861.
		-1.49.	-1.54.	-0.85.	-0.80.	0.64.	1.82.	2.82.	1.23.	-0.31.	-0.60.	-1.42.	-1.82.	-2.04.
		1.168.	1.285.	0.989.	1.280.	0.872.	0.857.	1.221.	0.857.	0.872.	1.280.	0.989.	1.285.	1.168.
		1.151.	1.266.	0.985.	1.286.	0.883.	0.884.	1.269.	0.873.	0.877.	1.282.	0.986.	1.271.	1.146.
		-1.45.	-1.48.	-0.40.	0.46.	1.27.	3.07.	3.87.	1.85.	0.53.	0.16.	-0.29.	-1.10.	-1.86.
	0.232.	1.228.	1.052.	1.108.	1.078.	0.866.	1.015.	1.019.	1.015.	0.866.	1.078.	1.108.	1.052.	1.228.	0.232.
	0.239.	1.262.	1.077.	1.130.	1.097.	0.886.	1.046.	1.042.	1.023.	0.881.	1.098.	1.120.	1.057.	1.214.	0.229.
	2.90.	2.73.	2.45.	1.94.	1.75.	2.30.	3.07.	2.27.	0.80.	1.71.	1.80.	1.09.	0.48.	-1.17.	-1.08.
	0.254.	1.023.	1.355.	0.802.	0.852.	1.229.	1.021.	0.768.	1.021.	1.229.	0.852.	0.802.	1.355.	1.023.	0.254.
	0.261.	1.051.	1.389.	0.816.	0.873.	1.261.	1.048.	0.763.	1.032.	1.270.	0.871.	0.817.	1.393.	1.011.	0.251.
	2.80.	2.69.	2.53.	1.70.	2.48.	2.58.	2.65.	-0.67.	1.09.	3.30.	2.27.	1.85.	2.80.	-1.18.	-1.19.
	0.232.	1.228.	1.052.	1.108.	1.078.	0.866.	1.015.	1.019.	1.015.	0.866.	1.078.	1.108.	1.052.	1.228.	0.232.
	0.224.	1.229.	1.050.	1.120.	1.098.	0.882.	1.028.	1.019.	1.017.	0.881.	1.097.	1.120.	1.056.	1.227.	0.228.
	-3.26.	0.08.	-0.13.	1.10.	1.79.	1.89.	1.33.	0.05.	0.20.	1.70.	1.70.	1.11.	0.42.	-0.08.	-1.57.
		1.168.	1.285.	0.989.	1.280.	0.872.	0.857.	1.221.	0.857.	0.872.	1.280.	0.989.	1.285.	1.168.	
		1.137.	1.250.	0.987.	1.303.	0.885.	0.872.	1.248.	0.867.	0.883.	1.301.	0.985.	1.269.	1.153.	
		-2.64.	-2.73.	-0.23.	1.80.	1.48.	1.75.	2.15.	1.16.	1.22.	1.64.	-0.48.	-1.26.	-1.26.	
		0.879.	1.326.	1.287.	1.033.	1.278.	1.074.	0.846.	1.074.	1.278.	1.033.	1.287.	1.326.	0.879.	
		0.856.	1.291.	1.277.	1.050.	1.306.	1.106.	0.878.	1.095.	1.282.	1.064.	1.283.	1.292.	0.867.	
		-2.55.	-2.59.	-0.72.	1.68.	2.18.	2.99.	3.77.	2.03.	0.29.	3.01.	-0.28.	-2.53.	-1.29.	
			0.503.	1.027.	1.291.	0.991.	1.106.	0.799.	1.106.	0.991.	1.291.	1.027.	0.503.		
			0.490.	1.018.	1.315.	1.017.	1.137.	0.812.	1.111.	0.994.	1.285.	0.985.	0.476.		
			-2.61.	-0.85.	1.80.	2.60.	2.76.	1.54.	0.45.	0.26.	-0.48.	-4.12.	-5.24.		
				0.522.	1.335.	1.287.	1.051.	1.353.	1.051.	1.287.	1.335.	0.522.			
				0.511.	1.317.	1.300.	1.065.	1.352.	1.038.	1.261.	1.291.	0.495.			
				-2.06.	-1.33.	0.99.	1.37.	-0.06.	-1.23.	-2.02.	-3.29.	-5.21.			
					0.882.	1.169.	1.227.	1.022.	1.227.	1.169.	0.882.				
					0.871.	1.155.	1.226.	1.016.	1.214.	1.150.	0.864.				
					-1.27.	-1.22.	-0.09.	-0.62.	-1.06.	-1.59.	-2.08.				
							0.232.	0.254.	0.232.						
							0.225.	0.251.	0.230.						

FORM 0113 (02/83)

. -2.92. -1.10. -0.99.

ASSEMBLY RELATIVE POWER C12 MAP547 04/04/88 D-155 7214MWD/MTU 58.89%HFP 54P 1 B-529 FCFM

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.228	0.249	0.228							1
2					0.867	1.144	1.202	1.001	1.226	1.167	0.870					2
3				0.513	1.317	1.266	1.027	1.323	1.041	1.275	1.309	0.505				3
4			0.494	1.012	1.278	0.986	1.101	0.792	1.086	0.975	1.271	1.007	0.490			4
5		0.866	1.305	1.276	1.024	1.286	1.093	0.870	1.087	1.274	1.027	1.268	1.302	0.861		5
6		1.151	1.266	0.985	1.286	0.883	0.884	1.269	0.873	0.877	1.282	0.986	1.271	1.146		6
7	0.239	1.262	1.077	1.130	1.097	0.886	1.046	1.042	1.023	0.881	1.098	1.120	1.057	1.214	0.229	7
8	0.261	1.051	1.389	0.816	0.873	1.261	1.048	0.763	1.032	1.270	0.871	0.817	1.393	1.011	0.251	8
9	0.224	1.229	1.050	1.120	1.098	0.882	1.028	1.019	1.017	0.881	1.097	1.120	1.056	1.227	0.228	9
10		1.137	1.250	0.987	1.303	0.885	0.872	1.248	0.867	0.883	1.301	0.985	1.269	1.153		10
11		0.856	1.291	1.277	1.050	1.306	1.106	0.878	1.095	1.282	1.064	1.283	1.292	0.867		11
12			0.490	1.018	1.315	1.017	1.137	0.812	1.111	0.994	1.285	0.985	0.476			12
13				0.511	1.317	1.300	1.065	1.352	1.038	1.261	1.291	0.495				13
14					0.871	1.155	1.226	1.016	1.214	1.150	0.864					14
15							0.225	0.251	0.230							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

194

FORM 0113 (02/83)

198

A QUARTER CORE AVERAGED ASSEMBLY RELATIVE POWER C12 MAP547 04/04/88 D-155 7214MWD/MTU 58.89%HFP 54P 1 B-529 FCFM

	H	G	F	E	D	C	B	A	
	0.768	1.021	1.229	0.852	0.802	1.355	1.023	0.254	
1	0.763	1.040	1.266	0.872	0.817	1.391	1.031	0.256	1
	-0.669	1.866	2.941	2.370	1.775	2.663	0.756	0.805	
	1.019	1.015	0.866	1.078	1.108	1.052	1.228	0.232	
2	1.031	1.028	0.883	1.097	1.123	1.060	1.233	0.230	2
	1.157	1.349	1.900	1.760	1.310	0.803	0.391	-0.752	
	1.221	0.857	0.872	1.280	0.989	1.285	1.168		
3	1.258	0.874	0.882	1.293	0.986	1.264	1.147		3
	3.011	1.955	1.124	1.014	-0.352	-1.644	-1.803		
	0.846	1.074	1.278	1.033	1.287	1.326	0.879		
4	0.874	1.095	1.287	1.041	1.276	1.298	0.863		4
	3.296	2.018	0.701	0.821	-0.818	-2.120	-1.843		
	0.799	1.106	0.991	1.291	1.027	0.503			
5	0.802	1.109	0.993	1.287	1.006	0.488			5
	0.315	0.244	0.156	-0.314	-2.091	-3.030			
	1.353	1.051	1.287	1.335	0.522				
6	1.338	1.043	1.275	1.308	0.506				6
	-1.155	-0.770	-0.920	-1.969	-3.103				
	1.022	1.227	1.169	0.882					
7	1.009	1.217	1.154	0.868					7
	-1.355	-0.817	-1.265	-1.606					
	0.254	0.232							
8	0.250	0.228							8
	-1.530	-1.890							

	PRED
	MES
	DIF

H	G	F	E	D	C	B	A

FORM 0113 (02/83)

FORM 0113 (02/83)

200

FQN C12 MAP547 04/04/88 D-155 7214MWD/MTU 58.89%HFP 54P 1 B-529 FCFM

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.661.	0.644.	0.668.							1
2					1.604.	1.841.	1.804.	1.483.	1.838.	1.835.	1.607.					2
3				1.040.	1.893.	1.689.	1.318.	1.850.	1.359.	1.688.	1.891.	1.036.				3
4			0.990.	1.480.	1.647.	1.225.	1.491.	1.256.	1.495.	1.222.	1.642.	1.480.	0.993.			4
5		1.577.	1.862.	1.629.	1.270.	1.684.	1.468.	1.142.	1.487.	1.694.	1.275.	1.629.	1.872.	1.600.		5
6		1.804.	1.698.	1.229.	1.702.	1.079.	1.137.	1.696.	1.136.	1.090.	1.692.	1.218.	1.691.	1.820.		6
7	0.702.	1.910.	1.381.	1.536.	1.490.	1.145.	1.362.	1.423.	1.339.	1.140.	1.486.	1.523.	1.358.	1.825.	0.664.	7
8	0.683.	1.566.	1.930.	1.295.	1.152.	1.673.	1.427.	1.181.	1.405.	1.693.	1.157.	1.309.	1.955.	1.520.	0.648.	8
9	0.648.	1.830.	1.349.	1.529.	1.486.	1.149.	1.355.	1.394.	1.332.	1.149.	1.493.	1.553.	1.368.	1.837.	0.664.	9
10		1.780.	1.654.	1.221.	1.723.	1.085.	1.125.	1.661.	1.126.	1.090.	1.712.	1.230.	1.693.	1.822.		10
11		1.584.	1.870.	1.660.	1.308.	1.732.	1.481.	1.153.	1.494.	1.707.	1.313.	1.650.	1.855.	1.609.		11
12			1.001.	1.511.	1.709.	1.279.	1.525.	1.283.	1.514.	1.258.	1.632.	1.421.	0.946.			12
13				1.035.	1.897.	1.722.	1.365.	1.873.	1.354.	1.713.	1.841.	0.988.				13
14					1.605.	1.844.	1.877.	1.514.	1.818.	1.815.	1.600.					14
15							0.676.	0.650.	0.663.							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

CALCULATED LOCAL PEAKING FACTORS C12 MAP547 04/04/88 D-155 7214MWD/MTU 58.89%HFP 54P 1 B-529 FCFM

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							1.749	1.561	1.750							1
2					1.526	1.298	1.206	1.191	1.207	1.298	1.526					2
3				1.711	1.198	1.116	1.061	1.115	1.061	1.116	1.198	1.711				3
4			1.697	1.234	1.090	1.061	1.102	1.135	1.102	1.062	1.090	1.234	1.697			4
5		1.528	1.201	1.090	1.051	1.121	1.123	1.055	1.123	1.121	1.051	1.090	1.201	1.528		5
6		1.298	1.117	1.054	1.121	1.068	1.086	1.100	1.086	1.068	1.121	1.054	1.117	1.298		6
7	1.750	1.206	1.061	1.102	1.123	1.079	1.071	1.088	1.071	1.079	1.124	1.102	1.061	1.206	1.750	7
8	1.561	1.191	1.115	1.135	1.054	1.101	1.090	1.101	1.090	1.101	1.054	1.134	1.115	1.191	1.561	8
9	1.750	1.206	1.061	1.102	1.123	1.079	1.071	1.088	1.071	1.079	1.123	1.101	1.061	1.206	1.750	9
10		1.298	1.117	1.054	1.121	1.068	1.086	1.100	1.086	1.068	1.121	1.054	1.117	1.298		10
11		1.528	1.201	1.090	1.051	1.121	1.124	1.055	1.123	1.120	1.052	1.090	1.201	1.527		11
12			1.697	1.234	1.090	1.062	1.103	1.137	1.102	1.061	1.090	1.234	1.697			12
13				1.711	1.198	1.116	1.061	1.115	1.061	1.116	1.198	1.711				13
14					1.526	1.298	1.206	1.191	1.206	1.298	1.526					14
15							1.750	1.561	1.749							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

PEAK ROD ENTHALPY RISE C12 MAP547 04/04/88 D-155 7214MWD/MTU 58.89%HFP 54P 1 B-529 FCFM

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.398	0.389	0.399							1
2					1.324	1.485	1.449	1.192	1.480	1.515	1.329					2
3				0.877	1.578	1.413	1.089	1.474	1.104	1.423	1.568	0.863				3
4			0.838	1.249	1.394	1.046	1.214	0.899	1.197	1.035	1.386	1.243	0.832			4
5		1.323	1.568	1.391	1.077	1.441	1.228	0.918	1.221	1.428	1.079	1.383	1.563	1.315		5
6		1.494	1.413	1.038	1.442	0.943	0.960	1.396	0.948	0.936	1.438	1.040	1.419	1.488		6
7	0.418	1.521	1.143	1.245	1.232	0.956	1.120	1.134	1.095	0.951	1.233	1.235	1.121	1.463	0.402	7
8	0.407	1.252	1.549	0.926	0.920	1.389	1.143	0.840	1.125	1.398	0.918	0.927	1.553	1.204	0.392	8
9	0.393	1.482	1.114	1.235	1.233	0.952	1.101	1.109	1.088	0.951	1.232	1.234	1.120	1.480	0.400	9
10		1.476	1.396	1.041	1.462	0.945	0.947	1.373	0.942	0.942	1.459	1.038	1.417	1.497		10
11		1.308	1.551	1.393	1.104	1.464	1.242	0.926	1.230	1.436	1.119	1.399	1.552	1.325		11
12			0.831	1.256	1.433	1.080	1.253	0.923	1.224	1.054	1.401	1.215	0.809			12
13				0.875	1.578	1.451	1.130	1.507	1.101	1.408	1.546	0.847				13
14					1.330	1.499	1.479	1.210	1.464	1.493	1.319					14
15							0.394	0.392	0.402							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

PERCENT AXIAL OFFSET TOWARD TOP OF ASSEMBLY C12 MAP547 04/04/88 D-155 7214MWD/MTU 58.89%HFP 54P 1 B-529 FCFM

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							38.8	38.5	35.5							1
2					-0.8	2.9	2.6	2.1	-1.4	-1.1	-0.6					2
3				-1.3	-1.1	-0.6	-2.0	-4.7	-4.7	-1.6	0.0	-0.7				3
4			-1.5	-1.3	-1.8	-1.9	-7.3	-22.3	-8.4	-1.4	-0.1	-0.1	-0.6			4
5		-2.3	-2.5	-2.1	1.1	-2.6	-5.6	-9.3	-5.4	-1.9	2.5	-1.2	-1.3	-1.8		5
6		-2.7	-4.7	-4.3	-3.8	-2.6	-3.6	-5.1	-4.2	-2.4	-2.2	-1.8	-1.0	0.3		6
7	38.9	2.5	-2.2	-7.9	-6.7	-5.2	-5.1	-8.8	-6.9	-5.3	-5.1	-6.5	-1.9	2.4	37.8	7
8	38.5	2.0	-5.0	-21.9	-9.3	-5.8	-7.8	-23.0	-9.3	-5.5	-9.0	-21.8	-4.6	1.9	37.4	8
9	36.7	1.3	-3.4	-7.6	-5.8	-5.9	-7.9	-9.1	-5.9	-4.5	-5.5	-9.1	-3.4	1.4	36.7	9
10		0.4	-1.5	-1.7	-1.6	-2.4	-4.5	-5.1	-4.3	-3.0	-3.2	-3.4	-2.1	-0.2		10
11		0.7	0.5	0.2	3.3	-0.8	-4.2	-8.1	-6.3	-4.5	1.2	-1.3	-0.4	0.3		11
12			0.9	1.0	0.7	-0.2	-6.3	-21.1	-8.4	-4.0	-1.6	-1.2	-1.1			12
13				-1.1	-2.1	-1.0	-1.4	-4.4	-3.5	-2.7	-1.2	-1.7				13
14					-1.9	-2.3	3.0	1.9	1.6	0.5	-0.8					14
15							34.2	37.1	37.4							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

FQT*V(Z)*FQE*FQM 3%TARGET BAND C12 MAP547 04/04/88 D-155 7214MWD/MTU 58.89%HFP 54P 1 B-529 FCFM
FULL CORE SEARCH

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.789.	0.768.	0.790.							1
2					1.912.	2.213.	2.130.	1.749.	2.146.	2.188.	1.921.					2
3				1.251.	2.255.	2.031.	1.558.	2.126.	1.585.	2.022.	2.263.	1.241.				3
4			1.186.	1.770.	1.958.	1.498.	1.711.	1.352.	1.717.	1.475.	1.966.	1.768.	1.187.			4
5		1.873.	2.210.	1.947.	1.516.	2.017.	1.692.	1.326.	1.712.	1.995.	1.525.	1.937.	2.225.	1.890.		5
6		2.140.	1.973.	1.430.	1.985.	1.318.	1.365.	1.987.	1.336.	1.292.	2.007.	1.466.	2.034.	2.172.		6
7	0.840.	2.261.	1.639.	1.761.	1.705.	1.337.	1.593.	1.632.	1.565.	1.331.	1.702.	1.747.	1.602.	2.155.	0.791.	7
8	0.816.	1.851.	2.216.	1.391.	1.333.	1.962.	1.632.	1.304.	1.609.	1.986.	1.339.	1.407.	2.244.	1.772.	0.770.	8
9	0.767.	2.159.	1.584.	1.754.	1.699.	1.342.	1.584.	1.594.	1.557.	1.342.	1.707.	1.782.	1.602.	2.164.	0.785.	9
10		2.128.	1.970.	1.461.	2.046.	1.310.	1.326.	1.942.	1.321.	1.301.	2.020.	1.446.	2.016.	2.173.		10
11		1.891.	2.230.	1.981.	1.571.	2.087.	1.739.	1.339.	1.716.	1.974.	1.569.	1.965.	2.219.	1.925.		11
12			1.199.	1.810.	2.045.	1.575.	1.753.	1.380.	1.738.	1.469.	1.964.	1.707.	1.136.			12
13				1.246.	2.233.	2.087.	1.623.	2.177.	1.578.	1.988.	2.175.	1.187.				13
14					1.891.	2.160.	2.226.	1.786.	2.135.	2.162.	1.880.					14
15							0.789.	0.770.	0.791.							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

FQT*V(Z)*FQE*FQM 5%TARGET BAND C12 MAP547 04/04/88 D-155 7214MWD/MTU 58.89%HFP 54P 1 B-529 FCFM
FULL CORE SEARCH

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.811	0.789	0.812							1
2					1.965	2.274	2.190	1.797	2.206	2.249	1.974					2
3				1.286	2.318	2.087	1.602	2.185	1.629	2.078	2.326	1.275				3
4			1.219	1.820	2.012	1.540	1.758	1.390	1.765	1.516	2.021	1.817	1.220			4
5		1.925	2.271	2.001	1.558	2.073	1.739	1.363	1.759	2.051	1.568	1.990	2.286	1.943		5
6		2.199	2.028	1.470	2.040	1.354	1.403	2.043	1.373	1.328	2.063	1.506	2.090	2.233		6
7	0.863	2.324	1.685	1.810	1.752	1.374	1.637	1.677	1.609	1.368	1.749	1.795	1.646	2.214	0.813	7
8	0.839	1.902	2.278	1.430	1.370	2.016	1.678	1.340	1.654	2.042	1.376	1.446	2.306	1.822	0.792	8
9	0.789	2.219	1.628	1.802	1.747	1.379	1.628	1.639	1.600	1.379	1.755	1.832	1.646	2.225	0.807	9
10		2.187	2.024	1.501	2.103	1.347	1.363	1.996	1.357	1.337	2.076	1.486	2.072	2.234		10
11		1.943	2.292	2.036	1.615	2.145	1.787	1.376	1.763	2.029	1.612	2.020	2.281	1.978		11
12			1.233	1.860	2.102	1.619	1.801	1.418	1.787	1.510	2.018	1.754	1.167			12
13				1.280	2.295	2.145	1.668	2.237	1.622	2.044	2.236	1.220				13
14					1.943	2.220	2.287	1.836	2.195	2.223	1.932					14
15							0.811	0.791	0.813							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

MAXIMUM FQT*V(Z)*FQE*FQM C12 MAP547 04/04/88 D-155 7214MWD/MTU 58.89%HFP 54P 1 B-529 FCFM

AXIAL NODE	3%TARGET	ASSEMBLY#	5%TARGET	ASSEMBLY#
1	.71395	40	.73307	40
2	.91527	118	.93979	118
3	1.0056	118	1.0325	118
4	1.1300	118	1.1603	118
5	1.5891	58	1.6317	58
6	1.6634	5	1.7081	5
7	1.7812	116	1.8293	116
8	1.9184	116	1.9704	116
9	2.0145	18	2.0692	18
10	2.0916	18	2.1487	18
11	2.1521	18	2.2111	18
12	2.1860	18	2.2461	18
13	2.2066	18	2.2675	18
14	2.2111	18	2.2724	18
15	2.2186	18	2.2802	18
16	2.2060	140	2.2673	140
17	2.1431	18	2.2026	18
18	2.1982	58	2.2592	58
19	2.2341	58	2.2961	58
20	2.2534	58	2.3160	58
21	2.2628	18	2.3257	18
22	2.2602	58	2.3230	58
23	2.2540	18	2.3166	18
24	2.2501	12	2.3126	12
25	2.2413	12	2.3036	12
26	2.2261	12	2.2880	12
27	2.2207	140	2.2823	140
28	2.1548	84	2.2146	84
29	2.2131	84	2.2745	84
30	2.2327	84	2.2948	84
31	2.2359	84	2.2980	84
32	2.2436	84	2.3060	84
33	2.2409	84	2.3032	84
34	2.2411	84	2.3034	84
35	2.2330	84	2.2950	84
36	2.2274	84	2.2893	84
37	2.2118	84	2.2732	84
38	2.1830	140	2.2436	140
39	2.1187	84	2.1776	84
40	2.1628	84	2.2228	84
41	2.1766	74	2.2370	74
42	2.1888	140	2.2496	140
43	2.1879	140	2.2487	140
44	2.2036	140	2.2648	140
45	2.2055	140	2.2668	140
46	2.2074	140	2.2688	140
47	2.1928	140	2.2537	140
48	2.1616	140	2.2216	140
49	2.1220	140	2.1810	140
50	2.0303	32	2.0867	32
51	2.0380	32	2.0947	32
52	2.0380	32	2.0947	32
53	1.9887	32	2.0439	32
54	1.9111	32	1.9642	32
55	1.7948	32	1.8446	32
56	1.6431	32	1.6888	32

57	1.4968	47	1.5383	47	
58	1.3809	47	1.4192	47	
59	.68258	124	.70154	124	
60	.51202	124	.52624	124	
61	.39948	124	.41058	124	

C12 MAP552 05/23/88 D-163 8042MWD/MTU 59.50%HFP 49P 1 B-457 FCFM

SUMMARY OF INCORE RESULTS	MEASURED			WITH UNCERTAINTY FACTOR	TECH. SPEC. LIMIT
FZ (MAX. ASSEMBLY)	= 1.676 LOC R 8				
FZ (MAX. AVERAGE)	= 1.187				
KW/FT (MAX. AVERAGE)	= 4.822 LOC C 8			5.215	
KW/FT (MAX. PEAK)	= 6.701 LOC L 3			7.247	
F-DELTA-H (MAX. ASSEMBLY)	= 1.390 LOC C 8	REGION 15			
F-DELTA-H (MAX. ASSEMBLY)	= 1.310 LOC L12	REGION 14			
F-DELTA-H (MAX. ASSEMBLY)	= 1.038 LOC E11	REGION 12R			
F-DELTA-H (MAX. ASSEMBLY)	= 1.056 LOC J13	REGION 13A			
F-DELTA-H (MAX. ASSEMBLY)	= 0.261 LOC R 8	REGION 13			
F-DELTA-H (PEAK PIN)	= 1.574 LOC L 3	REGION 15		1.637	1.784
F-DELTA-H (PEAK PIN)	= 1.429 LOC L12	REGION 14		1.486	1.784
F-DELTA-H (PEAK PIN)	= 1.101 LOC E11	REGION 12R		1.145	1.784
F-DELTA-H (PEAK PIN)	= 1.120 LOC J13	REGION 13A		1.165	1.784
F-DELTA-H (PEAK PIN)	= 0.407 LOC R 7	REGION 13		0.423	1.784
FQT (PENALIZED)	= 1.982 LOC L 3	REGION 15		2.081	3.798
FQT (PENALIZED)	= 1.833 LOC K13	REGION 14		1.925	3.798
FQT (PENALIZED)	= 1.336 LOC E11	REGION 12R		1.402	3.798
FQT (PENALIZED)	= 1.416 LOC J13	REGION 13A		1.487	3.798
FQT (PENALIZED)	= 0.720 LOC R 8	REGION 13		0.756	3.798
FQN (WITH LOCAL PEAKING)	= 1.876 LOC L 3	REGION 15			
FQN (WITH LOCAL PEAKING)	= 1.693 LOC L12	REGION 14			
FQN (WITH LOCAL PEAKING)	= 1.262 LOC E11	REGION 12R			
FQN (WITH LOCAL PEAKING)	= 1.341 LOC J13	REGION 13A			
FQN (WITH LOCAL PEAKING)	= 0.679 LOC R 8	REGION 13			

CALCULATED POWER TILTS(NORMALIZED TO 1.000)

(-,+) QUADRANT =	1.0019	1.02
(+,+) QUADRANT =	0.9977	1.02
(-,-) QUADRANT =	1.0020	1.02
(+,-) QUADRANT =	0.9984	1.02

AXIAL OFFSET = -1.281

FXY (NEGLECTING GRIDS) = 1.657 LOC L 3 NODE 11

FQZ BASED APL FOR 3% TARGET BAND = 100.55%

FQZ BASED APL FOR 5% TARGET BAND = 97.83%

[redacted]R/CVD.....DATE.....
INCORE - CP&L VERSION PNR16021 - 05/24/88

FORM 0113 (02/83)

C12 MAP552 05/23/88 D-163 8042MWD/MTU 59.50%HFP 49P 1 B-457 FCFM

FINAL COMPARISON OF SATURATION ACTIVITY AND PDQ ACTIVATION

THIMBLE		STATUS	MEASURED AXIAL FACTOR	REGION PERCENTAGE DIFFERENCE 1- 4	4-18	18-43	F*S(Z) 43-58	58-61	
1	M 3	GOOD	1.1562	-3.0809	-8.3587	2.0777	-2.3785	1.7576	1.1963
2	J15	NONE							
3	F 4	GOOD	1.1407	-1.2886	-3.5072	-0.2547	-1.8152	4.6232	1.1700
4	L 8	GOOD	1.1748	27.5424	13.4450	-1.2476	0.4344	11.1106	1.1748
5	F 8	GOOD	1.1378	4.0281	13.2096	1.6727	4.4395	10.2177	1.1378
6	D12	GOOD	1.1402	-10.3386	-8.5899	-1.7712	-3.6100	-7.2381	1.1908
7	B 5	GOOD	1.1535	-19.6476	-11.1004	1.1593	-1.6549	-5.6513	1.1894
8	H 6	GOOD	1.1343	17.0752	16.2261	1.9071	2.9559	-3.5793	1.1545
9	J 3	GOOD	1.1672	2.6939	-3.5941	-2.7030	-2.0049	7.2206	1.1922
10	D 3	GOOD	1.1647	-17.1090	-11.1416	0.7258	-3.2466	8.6702	1.1976
11	L 9	NONE							
12	B10	GOOD	1.1637	-26.0501	-8.4412	0.0081	-1.8624	-11.1280	1.1956
13	L 4	GOOD	1.1319	-9.5371	-5.9595	2.4620	1.5640	1.2433	1.1609
14	F13	GOOD	1.1531	-7.2474	-8.3867	-0.4994	-1.2287	-1.8734	1.1537
15	F 6	GOOD	1.1511	19.1255	6.3474	1.1115	0.7787	2.7492	1.1511
16	J12	GOOD	1.1427	7.1125	9.0170	0.3750	0.7751	-2.7919	1.1569
17	B 7	GOOD	1.1958	-6.1414	-3.5788	-1.2900	-4.2221	-15.2585	1.2233
18	H 1	NONE							
19	G 9	GOOD	1.1566	27.9561	14.4750	-4.3001	-1.6068	-3.3770	1.1566
20	G 7	GOOD	1.1454	20.4344	12.4784	-3.8895	-2.1158	0.7847	1.1515
21	F11	GOOD	1.1144	-11.6224	0.1186	1.5166	4.5263	7.1897	1.1144
22	N 5	GOOD	1.1259	-21.0994	-11.6560	-0.7082	1.1362	1.9251	1.1709
23	J10	GOOD	1.1323	17.8306	9.3947	-1.1352	0.8004	8.6792	1.1505
24	J 5	GOOD	1.1310	19.8029	10.8925	-0.8963	-0.8942	-7.1025	1.1359
25	B 8	GOOD	1.2075	5.2036	-4.2820	-2.1597	-3.9526	-8.3094	1.2353
26	N10	GOOD	1.1357	-0.7393	-7.2623	-2.2417	-3.6583	-12.8999	1.1604
27	C12	NONE							
28	J 7	GOOD	1.1468	30.3391	17.8712	-0.2827	0.1663	-1.6078	1.1638
29	D 7	GOOD	1.1503	18.4128	7.8219	-1.0521	-0.4360	-7.2705	1.1587
30	L14	GOOD	1.1428	-19.6425	-11.8710	1.5435	0.0918	-0.4550	1.1845
31	F 2	GOOD	1.1546	-21.2416	-7.5877	1.6550	1.4449	-3.2688	1.1890
32	F 9	GOOD	1.1461	24.5484	12.0049	-0.4455	0.3008	0.0500	1.1461
33	N 7	GOOD	1.1696	9.8140	-0.5441	-0.6958	-2.6848	-2.5756	1.1937
34	A 9	NONE							
35	N12	GOOD	1.1734	-8.4101	-10.2216	0.6353	-4.1795	1.8040	1.2066
36	R 8	NONE							
37	H 4	NONE							
38	H11	GOOD	1.1739	35.2048	13.5491	-0.8375	1.2962	6.3711	1.1739
39	D 5	GOOD	1.1338	-20.9175	-6.4778	0.7153	-0.2338	-7.2619	1.1629
40	L 6	GOOD	1.1068	-10.5234	1.2584	1.5846	3.9437	5.0763	1.1282
41	D10	GOOD	1.1584	-9.9409	-5.3036	-0.5809	0.2382	10.7902	1.1831
42	G14	GOOD	1.1908	-23.3115	-4.0544	-0.9793	-2.8123	-11.5479	1.2213
43	H13	GOOD	1.1756	6.8039	0.4067	-3.6672	-2.4269	-6.6804	1.1965
44	C 8	GOOD	1.1747	8.0269	5.7984	1.4503	1.5920	-12.5024	1.1970
45	H 3	NONE							
46	N 8	GOOD	1.1693	5.4632	3.3135	-0.6983	0.3245	-7.3011	1.1875
47	E11	GOOD	1.1525	0.6395	0.0242	7.4930	8.4985	35.3160	1.1760
48	L11	GOOD	1.1585	13.5721	-0.6880	4.3466	2.8418	11.7932	1.1882
49	E 5	GOOD	1.1461	4.5106	-4.1389	1.1057	0.7657	20.0985	1.1731
50	L 5	NONE							
AVG. OF ABSOLUTE VALUES OF GOOD THIMBLES ONLY			1.1532	14.00	7.67	1.61	2.10	7.25	

FORM 0113 (02/83)

SYMMETRIC THIMBLE COMPARISON C12 MAP552 05/23/88 D-163 8042MWD/MTU 59.50%HFP 49P 1 B-457 FCFM

THMBL	LOC	INTEGRAL	THMBL	LOC	INTEGRAL	RATIO
1	M 3	0.35849E+02	10	D 3	0.35206E+02	1.0183
10	D 3	0.35206E+02	1	M 3	0.35849E+02	.98206
19	G 9	0.60218E+02	20	G 7	0.60000E+02	1.0036
19	G 9	0.60218E+02	28	J 7	0.62127E+02	.96927
20	G 7	0.60000E+02	19	G 9	0.60218E+02	.99638
20	G 7	0.60000E+02	28	J 7	0.62127E+02	.96576
28	J 7	0.62127E+02	19	G 9	0.60218E+02	1.0317
28	J 7	0.62127E+02	20	G 7	0.60000E+02	1.0354
44	C 8	0.71568E+02	46	N 8	0.70320E+02	1.0177
46	N 8	0.70320E+02	44	C 8	0.71568E+02	.98257
47	E11	0.77668E+02	48	L11	0.75309E+02	1.0313
47	E11	0.77668E+02	49	E 5	0.73188E+02	1.0612
48	L11	0.75309E+02	47	E11	0.77668E+02	.96963
48	L11	0.75309E+02	49	E 5	0.73188E+02	1.0290
49	E 5	0.73188E+02	47	E11	0.77668E+02	.94232
49	E 5	0.73188E+02	48	L11	0.75309E+02	.97184

C12 MAP552 05/23/88 D-163 8042MWD/MTU 59.50%HFP 49P 1 B-457 FCFM

MAX FQT INCLUDES LOCA AXIAL PENALTY FACTOR

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.732	0.715	0.724							1
2					1.743	2.030	1.940	1.602	1.935	1.997	1.746					2
3				1.153	2.081	1.863	1.431	1.961	1.451	1.852	2.072	1.139				3
4			1.088	1.610	1.801	1.398	1.563	1.249	1.570	1.363	1.808	1.609	1.093			4
5		1.697	2.004	1.810	1.373	1.889	1.585	1.233	1.575	1.838	1.355	1.783	2.043	1.720		5
6		1.992	1.854	1.355	1.875	1.242	1.285	1.880	1.255	1.215	1.857	1.363	1.873	1.983		6
7	0.748	2.007	1.458	1.591	1.577	1.250	1.489	1.517	1.441	1.245	1.586	1.596	1.464	1.943	0.726	7
8	0.756	1.658	2.007	1.269	1.233	1.875	1.520	1.211	1.495	1.859	1.245	1.285	2.031	1.601	0.708	8
9	0.700	1.948	1.431	1.585	1.653	1.246	1.465	1.483	1.445	1.257	1.577	1.604	1.456	1.951	0.717	9
10		1.933	1.780	1.308	1.909	1.211	1.240	1.832	1.247	1.227	1.874	1.332	1.818	1.969		10
11		1.715	2.030	1.805	1.384	1.917	1.599	1.233	1.581	1.861	1.402	1.829	2.047	1.739		11
12			1.095	1.641	1.882	1.463	1.597	1.262	1.586	1.379	1.840	1.592	1.084			12
13				1.138	2.034	1.925	1.487	1.972	1.420	1.801	2.038	1.129				13
14					1.716	1.949	2.000	1.614	1.926	1.974	1.739					14
15							0.715	0.709	0.726							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

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ASSEMBLY RELATIVE POWER C12 MAP552 05/23/88 D-163 8042MWD/MTU 59.50%HFP 49P 1 B-457 FCFM

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.228	0.250	0.229							1
2					0.862	1.136	1.191	0.997	1.204	1.148	0.861					2
3				0.516	1.326	1.254	1.024	1.337	1.035	1.256	1.310	0.506				3
4			0.492	1.000	1.269	0.986	1.105	0.809	1.091	0.973	1.255	0.996	0.491			4
5		0.848	1.289	1.260	1.005	1.305	1.107	0.891	1.104	1.288	0.995	1.251	1.301	0.850		5
6		1.139	1.246	0.983	1.315	0.903	0.907	1.318	0.897	0.898	1.297	0.986	1.253	1.127		6
7	0.234	1.220	1.041	1.120	1.116	0.910	1.073	1.069	1.044	0.904	1.117	1.128	1.046	1.188	0.229	7
8	0.261	1.024	1.379	0.823	0.893	1.311	1.077	0.791	1.059	1.319	0.895	0.830	1.390	0.993	0.251	8
9	0.224	1.202	1.032	1.109	1.124	0.904	1.049	1.047	1.045	0.906	1.112	1.110	1.039	1.198	0.227	9
10		1.116	1.221	0.971	1.321	0.901	0.892	1.289	0.892	0.905	1.319	0.979	1.243	1.126		10
11		0.844	1.283	1.259	1.025	1.320	1.114	0.889	1.113	1.317	1.038	1.273	1.295	0.850		11
12			0.487	1.006	1.310	1.016	1.136	0.822	1.111	0.997	1.279	0.984	0.484			12
13				0.508	1.305	1.278	1.056	1.348	1.021	1.237	1.296	0.503				13
14					0.856	1.131	1.199	0.997	1.186	1.129	0.856					14
15							0.225	0.251	0.228							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

ASM"Y RELATIVE POWER EXPECTED / MEASURED/ % DIFF SUMS: 156.9927 / 156.9932 / -23.8531

					0.235	0.258	0.235						
					0.228	0.250	0.229						
					-2.73	-2.80	-2.47						
				0.880	1.162	1.217	1.019	1.217	1.162	0.880			
				0.862	1.136	1.191	0.997	1.204	1.148	0.861			
				-2.08	-2.22	-2.19	-2.20	-1.10	-1.19	-2.18			
			0.527	1.342	1.273	1.048	1.367	1.048	1.273	1.342	0.527		
			0.516	1.326	1.254	1.024	1.337	1.035	1.256	1.310	0.506		
			-2.03	-1.14	-1.44	-2.29	-2.21	-1.24	-1.29	-2.34	-3.85		
		0.507	1.019	1.275	0.985	1.104	0.813	1.104	0.985	1.275	1.019	0.507	
		0.492	1.000	1.269	0.986	1.105	0.809	1.091	0.973	1.255	0.996	0.491	
		-3.08	-1.79	-0.43	0.01	0.04	-0.48	-1.25	-1.23	-1.56	-2.20	-3.11	
	0.878	1.335	1.272	0.999	1.282	1.077	0.856	1.077	1.282	0.999	1.272	1.335	0.878
	0.848	1.289	1.260	1.005	1.305	1.107	0.891	1.104	1.288	0.995	1.251	1.301	0.850
	-3.41	-3.45	-0.95	0.58	1.82	2.82	4.00	2.55	0.51	-0.37	-1.65	-2.53	-3.19
	1.163	1.272	0.985	1.285	0.878	0.868	1.251	0.868	0.878	1.285	0.985	1.272	1.163
	1.139	1.246	0.983	1.315	0.903	0.907	1.318	0.897	0.898	1.297	0.986	1.253	1.127
	-2.03	-2.09	-0.26	2.31	2.85	4.50	5.37	3.37	2.19	0.93	0.06	-1.49	-3.09
0.235	1.218	1.047	1.106	1.081	0.876	1.023	1.030	1.023	0.876	1.081	1.106	1.047	1.218	0.235
0.234	1.220	1.041	1.120	1.116	0.910	1.073	1.069	1.044	0.904	1.117	1.128	1.046	1.188	0.229
-0.27	0.13	-0.56	1.29	3.16	3.88	4.85	3.76	2.05	3.27	3.31	2.02	-0.14	-2.48	-2.44
0.258	1.019	1.367	0.815	0.862	1.257	1.031	0.784	1.031	1.257	0.862	0.815	1.367	1.019	0.258
0.261	1.024	1.379	0.823	0.893	1.311	1.077	0.791	1.059	1.319	0.895	0.830	1.390	0.993	0.251
1.25	0.51	0.85	0.99	3.66	4.29	4.48	0.98	2.71	4.94	3.87	1.79	1.68	-2.52	-2.57
0.235	1.218	1.047	1.106	1.081	0.876	1.023	1.030	1.023	0.876	1.081	1.106	1.047	1.218	0.235
0.224	1.202	1.032	1.109	1.124	0.904	1.049	1.047	1.045	0.906	1.112	1.110	1.039	1.198	0.227
-4.48	-1.29	-1.49	0.31	3.97	3.26	2.49	1.67	2.08	3.45	2.82	0.42	-0.78	-1.63	-3.26
	1.163	1.272	0.985	1.285	0.878	0.868	1.251	0.868	0.878	1.285	0.985	1.272	1.163	
	1.116	1.221	0.971	1.321	0.901	0.892	1.289	0.892	0.905	1.319	0.979	1.243	1.126	
	-3.97	-4.05	-1.41	2.83	2.59	2.78	3.02	2.76	3.06	2.63	-0.67	-2.32	-3.13	
	0.878	1.335	1.272	0.999	1.282	1.077	0.856	1.077	1.282	0.999	1.272	1.335	0.878	
	0.844	1.283	1.259	1.025	1.320	1.114	0.889	1.113	1.317	1.038	1.273	1.295	0.850	
	-3.88	-3.92	-1.03	2.65	3.01	3.43	3.84	3.33	2.76	3.89	0.06	-3.00	-3.15	
		0.507	1.019	1.275	0.985	1.104	0.813	1.104	0.985	1.275	1.019	0.507	
		0.487	1.006	1.310	1.016	1.136	0.822	1.111	0.997	1.279	0.984	0.484	
		-3.94	-1.28	2.78	3.15	2.83	1.15	0.56	1.19	0.33	-3.43	-4.53	
			0.527	1.342	1.273	1.048	1.367	1.048	1.273	1.342	0.527		
			0.508	1.305	1.278	1.056	1.348	1.021	1.237	1.296	0.503		
			-3.44	-2.76	0.41	0.79	-1.36	-2.49	-2.81	-3.43	-4.52		
				0.880	1.162	1.217	1.019	1.217	1.162	0.880			
				0.856	1.131	1.199	0.997	1.186	1.129	0.856			
				-2.71	-2.66	-1.55	-2.18	-2.60	-2.77	-2.78			
						0.235	0.258	0.235					
						0.225	0.251	0.228					

A QUARTER CORE AVERAGED ASSEMBLY RELATIVE POWER C12 MAP552 05/23/88 D-163 8042MWD/MTU 59.50%HFP 49P 1 B-457 FCFM

	H	G	F	E	D	C	B	A	
	0.784	1.031	1.257	0.862	0.815	1.367	1.019	0.258	
1	0.791	1.068	1.315	0.894	0.827	1.385	1.009	0.256	1
	0.976	3.594	4.614	3.765	1.390	1.265	-1.002	-0.657	
	1.030	1.023	0.876	1.081	1.106	1.047	1.218	0.235	
2	1.058	1.053	0.906	1.117	1.117	1.039	1.202	0.228	2
	2.717	2.868	3.463	3.316	1.008	-0.744	-1.318	-2.613	
	1.251	0.868	0.878	1.285	0.985	1.272	1.163		
3	1.303	0.897	0.902	1.313	0.979	1.241	1.127		3
	4.196	3.352	2.674	2.176	-0.572	-2.488	-3.053		
	0.856	1.077	1.282	0.999	1.272	1.335	0.878		
4	0.890	1.109	1.307	1.016	1.261	1.292	0.848		4
	3.920	3.031	2.024	1.689	-0.894	-3.223	-3.410		
	0.813	1.104	0.985	1.275	1.019	0.507			
5	0.816	1.110	0.993	1.278	0.996	0.489			5
	0.333	0.548	0.780	0.280	-2.175	-3.665			
	1.367	1.048	1.273	1.342	0.527				
6	1.342	1.034	1.257	1.309	0.508				6
	-1.784	-1.307	-1.284	-2.418	-3.459				
	1.019	1.217	1.162	0.880					
7	0.997	1.195	1.136	0.859					7
	-2.188	-1.862	-2.210	-2.439					
	0.258	0.235							
8	0.251	0.227							8
	-2.732	-2.998							
	H	G	F	E	D	C	B	A	

PRED
MES
DIF

FORM 0113 (02/83)

196

. -4.22. -2.67. -2.58.

FORM 0113 (02/83)

FQN C12 MAP552 05/23/88 D-163 8042MWD/MTU 59.50%HFP 49P 1 B-457 FCFM

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.659	0.646	0.660							1
2					1.576	1.820	1.773	1.466	1.789	1.795	1.571					2
3				1.032	1.876	1.659	1.298	1.818	1.327	1.648	1.864	1.020				3
4			0.973	1.446	1.628	1.217	1.467	1.238	1.471	1.202	1.612	1.445	0.981			4
5		1.520	1.799	1.605	1.221	1.684	1.459	1.152	1.467	1.672	1.207	1.599	1.841	1.549		5
6		1.791	1.636	1.200	1.702	1.087	1.137	1.704	1.131	1.090	1.680	1.208	1.656	1.784		6
7	0.672	1.825	1.322	1.493	1.481	1.154	1.358	1.416	1.327	1.149	1.480	1.498	1.325	1.776	0.655	7
8	0.679	1.509	1.857	1.264	1.157	1.690	1.426	1.178	1.404	1.712	1.167	1.280	1.876	1.464	0.641	8
9	0.636	1.772	1.303	1.488	1.477	1.151	1.343	1.396	1.338	1.161	1.484	1.504	1.323	1.780	0.649	9
10		1.738	1.597	1.203	1.757	1.090	1.120	1.671	1.130	1.100	1.712	1.220	1.646	1.772		10
11		1.544	1.827	1.626	1.258	1.725	1.463	1.152	1.483	1.713	1.262	1.626	1.834	1.561		11
12			0.984	1.474	1.693	1.271	1.499	1.257	1.487	1.233	1.625	1.422	0.966			12
13				1.018	1.831	1.689	1.341	1.821	1.296	1.636	1.819	1.003				13
14					1.545	1.768	1.820	1.472	1.757	1.774	1.552					14
15							0.653	0.640	0.654							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

198

FORM 0113 (02/83)

PEAK ROD ENTHALPY RISE C12 MAP552 05/23/88 D-163 8042MWD/MTU 59.50%HFP 49P 1 B-457 FCFM

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.397	0.389	0.398							1
2					1.308	1.482	1.437	1.187	1.453	1.498	1.307					2
3				0.875	1.574	1.397	1.086	1.477	1.097	1.399	1.555	0.859				3
4			0.827	1.226	1.384	1.044	1.212	0.911	1.195	1.031	1.368	1.220	0.827			4
5		1.289	1.533	1.373	1.066	1.449	1.238	0.940	1.235	1.430	1.056	1.364	1.548	1.292		5
6		1.487	1.389	1.035	1.460	0.960	0.979	1.442	0.968	0.954	1.441	1.039	1.397	1.470		6
7	0.407	1.471	1.105	1.228	1.247	0.978	1.145	1.162	1.114	0.973	1.249	1.237	1.109	1.432	0.398	7
8	0.405	1.218	1.524	0.927	0.942	1.434	1.173	0.865	1.153	1.443	0.943	0.934	1.536	1.181	0.390	8
9	0.390	1.450	1.094	1.216	1.258	0.973	1.119	1.139	1.115	0.974	1.243	1.216	1.102	1.445	0.394	9
10		1.457	1.361	1.023	1.467	0.957	0.962	1.410	0.962	0.962	1.465	1.031	1.385	1.470		10
11		1.283	1.526	1.372	1.088	1.466	1.246	0.939	1.244	1.462	1.101	1.387	1.540	1.292		11
12			0.820	1.232	1.429	1.077	1.246	0.927	1.217	1.056	1.395	1.205	0.815			12
13				0.862	1.549	1.423	1.120	1.490	1.084	1.377	1.538	0.853				13
14					1.300	1.475	1.446	1.186	1.430	1.474	1.299					14
15							0.391	0.389	0.397							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

200

CALCULATED LOCAL PEAKING FACTORS C12 MAP552 05/23/88 D-163 8042MWD/MTU 59.50%HFP 49P 1 B-457 FCFM

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							1.740	1.553	1.740							1
2					1.518	1.305	1.206	1.191	1.207	1.305	1.518					2
3				1.696	1.187	1.114	1.061	1.105	1.061	1.113	1.187	1.696				3
4			1.683	1.225	1.090	1.059	1.097	1.126	1.096	1.059	1.090	1.225	1.683			4
5		1.520	1.190	1.090	1.061	1.111	1.119	1.056	1.118	1.111	1.061	1.090	1.190	1.520		5
6		1.305	1.115	1.054	1.111	1.062	1.080	1.094	1.079	1.062	1.111	1.054	1.115	1.305		6
7	1.739	1.206	1.061	1.096	1.118	1.075	1.067	1.088	1.067	1.075	1.118	1.097	1.061	1.206	1.739	7
8	1.553	1.190	1.105	1.126	1.055	1.094	1.089	1.093	1.089	1.094	1.054	1.125	1.105	1.189	1.553	8
9	1.739	1.206	1.061	1.096	1.119	1.076	1.067	1.088	1.067	1.076	1.118	1.095	1.061	1.206	1.739	9
10		1.305	1.115	1.054	1.111	1.062	1.079	1.094	1.079	1.062	1.111	1.053	1.115	1.305		10
11		1.520	1.190	1.090	1.061	1.111	1.118	1.056	1.118	1.110	1.061	1.090	1.190	1.520		11
12			1.683	1.225	1.091	1.060	1.097	1.127	1.096	1.059	1.090	1.225	1.683			12
13				1.696	1.187	1.114	1.061	1.105	1.061	1.113	1.187	1.696				13
14					1.518	1.305	1.206	1.190	1.206	1.305	1.518					14
15							1.740	1.553	1.739							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

FQT*V(Z)*FQE*FQM 3%TARGET BAND C12 MAP552 05/23/88 D-163 8042MWD/MTU 59.50%HFP 49P 1 B-457 FCFM
FULL CORE SEARCH

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.790	0.772	0.782							1
2					1.883	2.197	2.096	1.730	2.090	2.156	1.886					2
3				1.245	2.248	2.012	1.545	2.117	1.567	2.000	2.238	1.230				3
4			1.176	1.739	1.947	1.511	1.688	1.349	1.695	1.472	1.954	1.738	1.180			4
5		1.832	2.165	1.955	1.482	2.042	1.711	1.331	1.701	1.985	1.463	1.925	2.206	1.858		5
6		2.152	2.002	1.463	2.025	1.343	1.388	2.030	1.355	1.315	2.005	1.472	2.023	2.142		6
7	0.808	2.171	1.575	1.718	1.703	1.349	1.608	1.638	1.557	1.344	1.713	1.723	1.581	2.098	0.784	7
8	0.816	1.791	2.167	1.371	1.332	2.025	1.641	1.308	1.614	2.007	1.344	1.388	2.194	1.729	0.765	8
9	0.756	2.104	1.546	1.712	1.786	1.345	1.582	1.602	1.561	1.358	1.703	1.732	1.572	2.107	0.775	9
10		2.087	1.926	1.413	2.062	1.308	1.340	1.979	1.346	1.327	2.024	1.438	1.964	2.126		10
11		1.853	2.192	1.953	1.495	2.074	1.727	1.331	1.707	2.010	1.515	1.978	2.217	1.878		11
12			1.183	1.773	2.038	1.584	1.725	1.363	1.713	1.490	1.993	1.724	1.174			12
13				1.229	2.197	2.085	1.605	2.129	1.533	1.951	2.208	1.223				13
14					1.857	2.105	2.160	1.743	2.080	2.132	1.883					14
15							0.772	0.766	0.784							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

57	1.0800	1.1100
58	1.0800	1.1100
59	1.0800	1.1100
60	1.0800	1.1100
61	1.0800	1.1100

FQT*V(Z)*FQE*FQM 5%TARGET BAND C12 MAP552 05/23/88 D-163 8042MWD/MTU 59.50%HFP 49P 1 B-457 FCFM
FULL CORE SEARCH

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.812	0.793	0.803							1
2					1.935	2.258	2.154	1.778	2.148	2.216	1.939					2
3				1.279	2.310	2.068	1.588	2.176	1.611	2.056	2.300	1.264				3
4			1.209	1.787	2.001	1.553	1.735	1.387	1.742	1.513	2.008	1.786	1.213			4
5		1.883	2.225	2.009	1.524	2.098	1.759	1.368	1.749	2.040	1.504	1.979	2.268	1.910		5
6		2.212	2.057	1.504	2.081	1.380	1.426	2.086	1.393	1.351	2.061	1.512	2.079	2.201		6
7	0.830	2.232	1.619	1.766	1.751	1.387	1.653	1.684	1.600	1.382	1.761	1.771	1.625	2.156	0.806	7
8	0.839	1.841	2.228	1.409	1.369	2.081	1.687	1.345	1.659	2.063	1.382	1.427	2.255	1.777	0.786	8
9	0.777	2.162	1.589	1.759	1.835	1.383	1.626	1.646	1.604	1.396	1.751	1.780	1.616	2.165	0.796	9
10		2.145	1.979	1.452	2.120	1.344	1.377	2.034	1.384	1.364	2.080	1.478	2.018	2.185		10
11		1.904	2.253	2.007	1.537	2.132	1.775	1.368	1.755	2.066	1.557	2.033	2.278	1.930		11
12			1.216	1.822	2.094	1.628	1.773	1.401	1.760	1.531	2.048	1.772	1.206			12
13				1.263	2.258	2.143	1.650	2.188	1.576	2.005	2.269	1.257				13
14					1.909	2.163	2.220	1.791	2.138	2.191	1.936					14
15							0.793	0.787	0.806							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

FQT*V(Z)*FQE*FQM 3%TARGET BAND C12 MAP552 05/23/88 D-163 8042MWD/MTU 59.50%HFP 49P 1 B-457 FCFM
SEARCH BETWEEN NODES 6 AND 56

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.790	0.772	0.782							1
2					1.883	2.197	2.096	1.730	2.090	2.156	1.886					2
3				1.245	2.248	2.012	1.545	2.117	1.567	2.000	2.238	1.230				3
4			1.176	1.739	1.947	1.511	1.688	1.349	1.695	1.472	1.954	1.738	1.180			4
5		1.832	2.165	1.955	1.482	2.042	1.711	1.331	1.701	1.985	1.463	1.925	2.206	1.858		5
6		2.152	2.002	1.463	2.025	1.343	1.388	2.030	1.355	1.315	2.005	1.472	2.023	2.142		6
7	0.808	2.171	1.575	1.718	1.703	1.349	1.608	1.638	1.557	1.344	1.713	1.723	1.581	2.098	0.784	7
8	0.816	1.791	2.167	1.371	1.332	2.025	1.641	1.308	1.614	2.007	1.344	1.388	2.194	1.729	0.765	8
9	0.756	2.104	1.546	1.712	1.786	1.345	1.582	1.602	1.561	1.358	1.703	1.732	1.572	2.107	0.775	9
10		2.087	1.926	1.413	2.062	1.308	1.340	1.979	1.346	1.327	2.024	1.438	1.964	2.126		10
11		1.853	2.192	1.953	1.495	2.074	1.727	1.331	1.707	2.010	1.515	1.978	2.217	1.878		11
12			1.183	1.773	2.038	1.584	1.725	1.363	1.713	1.490	1.993	1.724	1.174			12
13				1.229	2.197	2.085	1.605	2.129	1.533	1.951	2.208	1.223				13
14					1.857	2.105	2.160	1.743	2.080	2.132	1.883					14
15							0.772	0.766	0.784							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

MAXIMUM FQT*V(Z)*FQE*FQM C12 MAP552 05/23/88 D-163 8042MWD/MTU 59.50%HFP 49P 1 B-457 FCFM

AXIAL NODE	3%TARGET	ASSEMBLY#	5%TARGET	ASSEMBLY#
1	.72069	52	.74000	52
2	.90032	118	.92444	118
3	.99690	118	1.0236	118
4	1.1225	118	1.1526	118
5	1.6500	12	1.6942	12
6	1.7143	12	1.7604	12
7	1.8341	126	1.8836	126
8	1.9917	126	2.0457	126
9	2.0949	12	2.1518	12
10	2.1674	12	2.2266	12
11	2.2025	12	2.2628	12
12	2.2222	18	2.2834	18
13	2.2336	18	2.2952	18
14	2.2379	18	2.2999	18
15	2.2332	18	2.2952	18
16	2.2185	18	2.2801	18
17	2.1395	18	2.1990	18
18	2.1890	12	2.2498	12
19	2.2394	12	2.3016	12
20	2.2476	12	2.3100	12
21	2.2458	12	2.3082	12
22	2.2373	12	2.2995	12
23	2.2325	12	2.2945	12
24	2.2225	12	2.2842	12
25	2.2008	12	2.2620	12
26	2.1811	12	2.2417	12
27	2.1414	140	2.2008	140
28	2.0882	84	2.1463	84
29	2.1336	84	2.1928	84
30	2.1497	84	2.2094	84
31	2.1534	84	2.2132	84
32	2.1520	84	2.2118	84
33	2.1503	84	2.2101	84
34	2.1502	84	2.2100	84
35	2.1412	84	2.2007	84
36	2.1344	84	2.1937	84
37	2.1182	84	2.1771	84
38	2.0872	140	2.1452	140
39	2.0342	84	2.0907	84
40	2.0803	84	2.1380	84
41	2.0893	84	2.1473	84
42	2.1020	140	2.1604	140
43	2.1177	140	2.1766	140
44	2.1335	140	2.1928	140
45	2.1357	140	2.1950	140
46	2.1462	140	2.2058	140
47	2.1318	140	2.1910	140
48	2.1174	140	2.1762	140
49	2.0946	140	2.1528	140
50	2.0052	140	2.0609	140
51	2.0018	12	2.0574	12
52	2.0032	32	2.0588	32
53	1.9752	32	2.0300	32
54	1.9086	32	1.9616	32
55	1.8071	32	1.8572	32
56	1.6670	32	1.7133	32

FQT*V(Z)*FQE*FQM 5%TARGET BAND C12 MAP552 05/23/88 D-163 8042MWD/MTU 59.50%HFP 49P 1 B-457 FCFM
SEARCH BETWEEN NODES 6 AND 56

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.812	0.793	0.803							1
2					1.935	2.258	2.154	1.778	2.148	2.216	1.939					2
3				1.279	2.310	2.068	1.588	2.176	1.611	2.056	2.300	1.264				3
4			1.209	1.787	2.001	1.553	1.735	1.387	1.742	1.513	2.008	1.786	1.213			4
5		1.883	2.225	2.009	1.524	2.098	1.759	1.368	1.749	2.040	1.504	1.979	2.268	1.910		5
6		2.212	2.057	1.504	2.081	1.380	1.426	2.086	1.393	1.351	2.061	1.512	2.079	2.201		6
7	0.830	2.232	1.619	1.766	1.751	1.387	1.653	1.684	1.600	1.382	1.761	1.771	1.625	2.156	0.806	7
8	0.839	1.841	2.228	1.409	1.369	2.081	1.687	1.345	1.659	2.063	1.382	1.427	2.255	1.777	0.786	8
9	0.777	2.162	1.589	1.759	1.835	1.383	1.626	1.646	1.604	1.396	1.751	1.780	1.616	2.165	0.796	9
10		2.145	1.979	1.452	2.120	1.344	1.377	2.034	1.384	1.364	2.080	1.478	2.018	2.185		10
11		1.904	2.253	2.007	1.537	2.132	1.775	1.368	1.755	2.066	1.557	2.033	2.278	1.930		11
12			1.216	1.822	2.094	1.628	1.773	1.401	1.760	1.531	2.048	1.772	1.206			12
13				1.263	2.258	2.143	1.650	2.188	1.576	2.005	2.269	1.257				13
14					1.909	2.163	2.220	1.791	2.138	2.191	1.936					14
15							0.793	0.787	0.806							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

57	1.5314	123	1.5740	123	
58	1.4010	47	1.4399	47	
59	.71212	124	.73190	124	
60	.53205	124	.54683	124	
61	.40650	124	.41779	124	

PDQ ACTIVATIONS FOR EACH THIMBLE

THIMBLE	(X-ORD, Y-ORD)	REGION 1	REGION 2	REGION 3	REGION 4	REGION 5	REGION 6	REGION 7	REGION 8
1 M 3	(-60., 75.)	0.251E+17	0.103E+17	0.870E+16	0.903E+16	0.208E+17	0.0	0.0	0.0
2 J15	(-15., -105.)	0.164E+17	0.924E+16	0.851E+16	0.434E+16	0.469E+16	0.0	0.0	0.0
3 F 4	(30., 60.)	0.454E+17	0.182E+17	0.173E+17	0.179E+17	0.432E+17	0.0	0.0	0.0
4 L 8	(-45., 0.)	0.285E+17	0.127E+17	0.159E+17	0.168E+17	0.413E+17	0.0	0.0	0.0
5 F 8	(30., 0.)	0.434E+17	0.140E+17	0.164E+17	0.170E+17	0.542E+17	0.0	0.0	0.0
6 D12	(60., -60.)	0.471E+17	0.162E+17	0.138E+17	0.143E+17	0.387E+17	0.0	0.0	0.0
7 B 5	(90., 45.)	0.358E+17	0.128E+17	0.109E+17	0.111E+17	0.300E+17	0.0	0.0	0.0
8 H 6	(0., 30.)	0.432E+17	0.139E+17	0.163E+17	0.166E+17	0.529E+17	0.0	0.0	0.0
9 J 3	(-15., 75.)	0.406E+17	0.177E+17	0.181E+17	0.181E+17	0.425E+17	0.0	0.0	0.0
10 D 3	(60., 75.)	0.251E+17	0.103E+17	0.870E+16	0.903E+16	0.208E+17	0.0	0.0	0.0
11 L 9	(-45., -15.)	0.407E+17	0.144E+17	0.159E+17	0.167E+17	0.480E+17	0.0	0.0	0.0
12 B10	(90., -30.)	0.471E+17	0.165E+17	0.146E+17	0.144E+17	0.399E+17	0.0	0.0	0.0
13 L 4	(-45., 60.)	0.594E+17	0.191E+17	0.167E+17	0.173E+17	0.510E+17	0.0	0.0	0.0
14 F13	(30., -75.)	0.538E+17	0.194E+17	0.176E+17	0.180E+17	0.489E+17	0.0	0.0	0.0
15 F 6	(30., 30.)	0.331E+17	0.159E+17	0.164E+17	0.168E+17	0.341E+17	0.0	0.0	0.0
16 J12	(-15., -60.)	0.382E+17	0.142E+17	0.162E+17	0.170E+17	0.492E+17	0.0	0.0	0.0
17 B 7	(90., 15.)	0.475E+17	0.164E+17	0.155E+17	0.140E+17	0.389E+17	0.0	0.0	0.0
18 H 1	(0., 105.)	0.178E+17	0.979E+16	0.915E+16	0.392E+16	0.436E+16	0.0	0.0	0.0
19 G 9	(15., -15.)	0.331E+17	0.126E+17	0.156E+17	0.160E+17	0.436E+17	0.0	0.0	0.0
20 G 7	(15., 15.)	0.331E+17	0.126E+17	0.156E+17	0.160E+17	0.436E+17	0.0	0.0	0.0
21 F11	(30., -45.)	0.603E+17	0.163E+17	0.160E+17	0.164E+17	0.581E+17	0.0	0.0	0.0
22 N 5	(-75., 45.)	0.589E+17	0.192E+17	0.165E+17	0.169E+17	0.493E+17	0.0	0.0	0.0
23 J10	(-15., -30.)	0.348E+17	0.140E+17	0.157E+17	0.161E+17	0.400E+17	0.0	0.0	0.0
24 J 5	(-15., 45.)	0.405E+17	0.143E+17	0.159E+17	0.165E+17	0.473E+17	0.0	0.0	0.0
25 B 8	(90., 0.)	0.388E+17	0.157E+17	0.152E+17	0.132E+17	0.318E+17	0.0	0.0	0.0
26 N10	(-75., -30.)	0.538E+17	0.194E+17	0.176E+17	0.180E+17	0.488E+17	0.0	0.0	0.0
27 C12	(75., -60.)	0.245E+17	0.102E+17	0.863E+16	0.884E+16	0.197E+17	0.0	0.0	0.0
28 J 7	(-15., 15.)	0.331E+17	0.126E+17	0.156E+17	0.160E+17	0.436E+17	0.0	0.0	0.0
29 D 7	(60., 15.)	0.382E+17	0.142E+17	0.162E+17	0.170E+17	0.491E+17	0.0	0.0	0.0
30 L14	(-45., -90.)	0.359E+17	0.128E+17	0.109E+17	0.111E+17	0.302E+17	0.0	0.0	0.0
31 F 2	(30., 90.)	0.471E+17	0.165E+17	0.146E+17	0.144E+17	0.398E+17	0.0	0.0	0.0
32 F 9	(30., -15.)	0.352E+17	0.141E+17	0.158E+17	0.164E+17	0.417E+17	0.0	0.0	0.0
33 N 7	(-75., 15.)	0.405E+17	0.177E+17	0.181E+17	0.181E+17	0.424E+17	0.0	0.0	0.0
34 A 9	(105., -15.)	0.163E+17	0.924E+16	0.851E+16	0.435E+16	0.471E+16	0.0	0.0	0.0
35 N12	(-75., -60.)	0.245E+17	0.102E+17	0.863E+16	0.884E+16	0.197E+17	0.0	0.0	0.0
36 R 8	(-105., 0.)	0.178E+17	0.979E+16	0.915E+16	0.393E+16	0.437E+16	0.0	0.0	0.0
37 H 4	(0., 60.)	0.102E+17	0.833E+16	0.165E+17	0.173E+17	0.422E+17	0.0	0.0	0.0
38 H11	(0., -45.)	0.284E+17	0.127E+17	0.158E+17	0.166E+17	0.407E+17	0.0	0.0	0.0
39 D 5	(60., 45.)	0.594E+17	0.191E+17	0.167E+17	0.172E+17	0.507E+17	0.0	0.0	0.0
40 L 6	(-45., 30.)	0.605E+17	0.164E+17	0.160E+17	0.165E+17	0.583E+17	0.0	0.0	0.0
41 D10	(60., -30.)	0.454E+17	0.183E+17	0.173E+17	0.178E+17	0.430E+17	0.0	0.0	0.0
42 G14	(15., -90.)	0.476E+17	0.165E+17	0.155E+17	0.140E+17	0.388E+17	0.0	0.0	0.0
43 H13	(0., -75.)	0.454E+17	0.161E+17	0.180E+17	0.177E+17	0.540E+17	0.0	0.0	0.0
44 C 8	(75., 0.)	0.453E+17	0.161E+17	0.180E+17	0.177E+17	0.540E+17	0.0	0.0	0.0
45 H 3	(0., 75.)	0.454E+17	0.161E+17	0.180E+17	0.177E+17	0.540E+17	0.0	0.0	0.0
46 N 8	(-75., 0.)	0.453E+17	0.161E+17	0.180E+17	0.177E+17	0.540E+17	0.0	0.0	0.0
47 E11	(45., -45.)	0.395E+17	0.198E+17	0.180E+17	0.184E+17	0.352E+17	0.0	0.0	0.0
48 L11	(-45., -45.)	0.395E+17	0.198E+17	0.180E+17	0.184E+17	0.352E+17	0.0	0.0	0.0
49 E 5	(45., 45.)	0.395E+17	0.198E+17	0.180E+17	0.184E+17	0.352E+17	0.0	0.0	0.0
50 L 5	(-45., 45.)	0.395E+17	0.198E+17	0.180E+17	0.184E+17	0.352E+17	0.0	0.0	0.0

C12 MAP553 06/22/88 D-205 8666MWD/MTU 89.92%HFP 5OP 1 B-347 FCFM

FINAL COMPARISON OF SATURATION ACTIVITY AND PDQ ACTIVATION

THIMBLE		STATUS	MEASURED AXIAL FACTOR	REGION PERCENTAGE DIFFERENCE 1- 4	4-43	43-58	58-61	F*S(Z)
1	M 3	GOOD	1.1286	13.2452	0.3848	-2.6315	1.7386	1.1818
2	J15	NONE						
3	F 4	NONE						
4	L 8	GOOD	1.1381	3.1520	2.2706	1.5128	9.9073	1.1816
5	F 8	GOOD	1.1169	-7.1146	3.4901	5.0704	10.4411	1.1552
6	D12	GOOD	1.1280	8.4991	-2.2992	-3.8862	-8.3793	1.1763
7	B 5	GOOD	1.1496	-6.2231	-2.3987	-3.2283	-8.0748	1.1756
8	H 6	GOOD	1.1043	1.7395	4.0119	3.4643	-3.4509	1.1533
9	J 3	GOOD	1.1420	-0.9765	-3.1153	-3.5893	3.0954	1.1896
10	D 3	GOOD	1.1341	3.0070	-1.9004	-4.8264	4.6560	1.1876
11	L 9	GOOD	1.1273	3.0423	1.1331	2.7136	7.4513	1.1628
12	B10	GOOD	1.1360	-19.7018	-3.9410	-4.5734	-14.4451	1.1736
13	L 4	GOOD	1.1323	1.9047	-0.7151	0.5844	-0.9033	1.1347
14	F13	GOOD	1.1215	-0.1181	-3.8307	-2.5068	-2.6986	1.1476
15	F 6	GOOD	1.1316	19.5647	3.3063	2.2241	3.5009	1.1818
16	J12	GOOD	1.1241	-9.7412	1.2382	0.1682	-4.2969	1.1735
17	B 7	GOOD	1.1599	-7.2386	-3.1760	-2.4206	0.8178	1.2073
18	H 1	NONE						
19	G 9	GOOD	1.1299	6.5525	-0.3153	-0.7795	-3.0423	1.1832
20	G 7	GOOD	1.1140	0.0399	-0.3341	-0.9198	0.3692	1.1604
21	F11	GOOD	1.1159	-6.4677	2.1733	5.7471	8.3111	1.1281
22	N 5	GOOD	1.1400	-2.5611	-4.0923	-2.5039	-11.4255	1.1507
23	J10	GOOD	1.1171	6.4520	2.4503	2.7398	12.5503	1.1667
24	J 5	GOOD	1.1131	2.4172	1.6027	2.8182	10.9136	1.1655
25	B 8	GOOD	1.1906	9.2400	-2.0258	-4.7327	-11.4752	1.2402
26	N10	GOOD	1.1330	7.7725	-4.0222	-4.6176	-12.6818	1.1532
27	C12	NONE						
28	J 7	GOOD	1.1196	8.0592	3.1640	1.1064	-2.4289	1.1693
29	D 7	GOOD	1.1277	1.1759	0.2720	-0.9742	-8.6831	1.1748
30	L14	GOOD	1.1431	-7.3094	-2.8656	-2.6842	-2.2571	1.1687
31	F 2	GOOD	1.1325	-10.0695	-2.4107	-1.9633	-8.7289	1.1827
32	F 9	GOOD	1.1318	15.7083	3.5814	1.6441	0.3123	1.1823
33	N 7	GOOD	1.1479	5.0135	-1.3215	-3.0749	-0.9356	1.1988
34	A 9	NONE						
35	N12	GOOD	1.1356	12.4376	-0.8912	-5.0638	-0.7351	1.1891
36	R 8	NONE						
37	H 4	NONE						
38	H11	GOOD	1.1376	7.7306	2.3486	1.9382	4.5931	1.1731
39	D 5	GOOD	1.1387	-9.6028	-1.0184	-1.1347	-9.8463	1.1458
40	L 6	GOOD	1.1064	-6.1882	2.5100	5.5016	7.7915	1.1362
41	D10	GOOD	1.1319	0.4230	-1.0982	0.2667	15.1956	1.1524
42	G14	GOOD	1.1677	-33.2590	-2.6780	-1.5160	3.8678	1.2164
43	H13	GOOD	1.1316	-8.4869	-4.3337	-3.9359	-8.7629	1.1818
44	C 8	GOOD	1.1298	-8.4541	-0.3651	-0.1309	-13.6745	1.1799
45	H 3	NONE						
46	N 8	GOOD	1.1436	-8.9311	-1.1555	-0.8544	-10.5806	1.1975
47	E11	GOOD	1.1329	14.4095	6.4796	8.6141	30.8823	1.1559
48	L11	GOOD	1.1387	24.5962	4.3287	3.7255	10.8521	1.1628
49	E 5	GOOD	1.1350	18.7806	1.5031	1.4908	13.0641	1.1715
50	L 5	NONE						
AVG. OF ABSOLUTE VALUES OF GOOD THIMBLES ONLY			1.1332	8.47	2.35	2.78	7.51	

FORM 0113 (02/83)

SYMMETRIC THIMBLE COMPARISON C12 MAP553 06/22/88 D-205 8666MWD/MTU 89.92%HFP 5OP 1 B-347 FCFM

THMBL	LOC	INTEGRAL	THMBL	LOC	INTEGRAL	RATIO
1	M 3	0.32993E+02	10	D 3	0.32224E+02	1.0239
10	D 3	0.32224E+02	1	M 3	0.32993E+02	.97670
19	G 9	0.60089E+02	20	G 7	0.60000E+02	1.0015
19	G 9	0.60089E+02	28	J 7	0.61852E+02	.97151
20	G 7	0.60000E+02	19	G 9	0.60089E+02	.99851
20	G 7	0.60000E+02	28	J 7	0.61852E+02	.97006
28	J 7	0.61852E+02	19	G 9	0.60089E+02	1.0293
28	J 7	0.61852E+02	20	G 7	0.60000E+02	1.0309
44	C 8	0.67127E+02	46	N 8	0.66692E+02	1.0065
46	N 8	0.66692E+02	44	C 8	0.67127E+02	.99352
47	E11	0.72919E+02	48	L11	0.70899E+02	1.0285
47	E11	0.72919E+02	49	E 5	0.69120E+02	1.0550
48	L11	0.70899E+02	47	E11	0.72919E+02	.97230
48	L11	0.70899E+02	49	E 5	0.69120E+02	1.0257
49	E 5	0.69120E+02	47	E11	0.72919E+02	.94790
49	E 5	0.69120E+02	48	L11	0.70899E+02	.97490

C12 MAP553 06/22/88 D-205 8666MWD/MTU 89.92%HFP 50P 1 B-347 FCFM

MAX FQT INCLUDES LOCA AXIAL PENALTY FACTOR

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.704	0.693	0.704							1
2					1.687	1.883	1.859	1.559	1.861	1.885	1.643					2
3				1.112	1.972	1.729	1.419	1.970	1.420	1.731	1.957	1.095				3
4			1.033	1.524	1.702	1.308	1.578	1.292	1.652	1.329	1.714	1.531	1.039			4
5		1.592	1.892	1.692	1.321	1.876	1.649	1.268	1.654	1.889	1.326	1.689	1.936	1.632		5
6		1.877	1.724	1.312	1.900	1.227	1.289	1.971	1.274	1.228	1.872	1.311	1.740	1.877		6
7	0.717	1.902	1.448	1.597	1.655	1.290	1.575	1.606	1.531	1.284	1.648	1.595	1.439	1.857	0.702	7
8	0.714	1.597	2.027	1.314	1.279	1.978	1.625	1.277	1.609	1.985	1.277	1.299	2.007	1.568	0.694	8
9	0.681	1.859	1.417	1.593	1.649	1.286	1.567	1.606	1.558	1.302	1.646	1.591	1.419	1.850	0.693	9
10		1.825	1.677	1.306	1.902	1.225	1.282	1.961	1.281	1.231	1.892	1.301	1.702	1.825		10
11		1.621	1.926	1.717	1.355	1.898	1.642	1.267	1.637	1.889	1.363	1.734	1.925	1.584		11
12			1.054	1.561	1.775	1.350	1.603	1.298	1.592	1.317	1.734	1.540	1.046			12
13				1.088	1.935	1.765	1.444	1.961	1.402	1.689	1.919	1.091				13
14					1.628	1.873	1.840	1.552	1.857	1.861	1.592					14
15							0.700	0.696	0.706							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

ASSEMBLY RELATIVE POWER C12 MAP553 06/22/88 D-205 8666MWD/MTU 89.92%HFP 50P 1 B-347 FCFM

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.219	0.242	0.220							1
2					0.838	1.080	1.150	0.975	1.158	1.088	0.819					2
3				0.503	1.282	1.205	1.016	1.365	1.023	1.199	1.253	0.492				3
4			0.474	0.962	1.222	0.969	1.140	0.943	1.189	0.992	1.222	0.963	0.475			4
5		0.806	1.232	1.214	0.992	1.315	1.144	0.947	1.158	1.325	0.994	1.213	1.254	0.814		5
6		1.084	1.194	0.970	1.338	0.923	0.936	1.378	0.930	0.924	1.311	0.971	1.205	1.080		6
7	0.223	1.167	1.028	1.149	1.153	0.943	1.128	1.152	1.105	0.938	1.144	1.144	1.028	1.148	0.220	7
8	0.246	0.989	1.388	0.950	0.943	1.368	1.159	0.954	1.146	1.381	0.947	0.944	1.392	0.974	0.244	8
9	0.217	1.154	1.017	1.144	1.142	0.938	1.128	1.139	1.104	0.944	1.148	1.139	1.025	1.150	0.219	9
10		1.068	1.177	0.971	1.334	0.926	0.935	1.359	0.927	0.928	1.338	0.975	1.197	1.065		10
11		0.811	1.240	1.225	1.023	1.330	1.141	0.941	1.150	1.341	1.033	1.240	1.246	0.800		11
12			0.476	0.978	1.279	0.996	1.152	0.944	1.140	0.991	1.242	0.956	0.473			12
13				0.492	1.250	1.219	1.031	1.357	1.011	1.189	1.246	0.491				13
14					0.817	1.085	1.136	0.969	1.150	1.080	0.811					14
15							0.219	0.242	0.219							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

1	ASM"Y· RELATIVE POWER													SUMS: 156.9928 / 156.9968 / -34.3862
2														
3							0.227.	0.251.	0.227.					
4							0.219.	0.242.	0.220.					
5							-3.62.	-3.60.	-3.11.					
6														
7						0.837.	1.111.	1.183.	1.003.	1.183.	1.111.	0.837.		
8						0.838.	1.080.	1.150.	0.975.	1.158.	1.088.	0.819.		
9						0.15.	-2.80.	-2.78.	-2.80.	-2.07.	-2.08.	-2.09.		
10														
11					0.503.	1.281.	1.227.	1.047.	1.405.	1.047.	1.227.	1.281.	0.503.	
12					0.503.	1.282.	1.205.	1.016.	1.365.	1.023.	1.199.	1.253.	0.492.	
13					0.05.	0.11.	-1.73.	-2.91.	-2.83.	-2.29.	-2.22.	-2.14.	-2.23.	
14														
15				0.484.	0.969.	1.221.	0.971.	1.143.	0.946.	1.143.	0.971.	1.221.	0.969.	0.484.
16				0.474.	0.962.	1.222.	0.969.	1.140.	0.943.	1.189.	0.992.	1.222.	0.963.	0.475.
17				-2.05.	-0.78.	0.04.	-0.18.	-0.23.	-0.28.	4.07.	2.12.	0.05.	-0.65.	-1.87.
18														
19		0.833.	1.274.	1.219.	0.978.	1.288.	1.116.	0.918.	1.116.	1.288.	0.978.	1.219.	1.274.	0.833.
20		0.806.	1.232.	1.214.	0.992.	1.315.	1.144.	0.947.	1.158.	1.325.	0.994.	1.213.	1.254.	0.814.
21		-3.24.	-3.29.	-0.42.	1.44.	2.11.	2.59.	3.19.	3.77.	2.82.	1.68.	-0.46.	-1.55.	-2.25.
22														
23		1.109.	1.224.	0.969.	1.290.	0.899.	0.909.	1.330.	0.909.	0.899.	1.290.	0.969.	1.224.	1.109.
24		1.084.	1.194.	0.970.	1.338.	0.923.	0.936.	1.378.	0.930.	0.924.	1.311.	0.971.	1.205.	1.080.
25		-2.32.	-2.42.	0.14.	3.67.	2.67.	3.04.	3.55.	2.38.	2.81.	1.58.	0.18.	-1.53.	-2.63.
26														
27	0.227.	1.181.	1.043.	1.142.	1.118.	0.916.	1.096.	1.127.	1.096.	0.916.	1.118.	1.142.	1.043.	1.181. 0.227.
28	0.223.	1.167.	1.028.	1.149.	1.153.	0.943.	1.128.	1.152.	1.105.	0.938.	1.144.	1.144.	1.028.	1.148. 0.220.
29	-1.75.	-1.14.	-1.44.	0.64.	3.12.	2.94.	2.99.	2.25.	0.83.	2.45.	2.27.	0.16.	-1.46.	-2.72. -3.10.
30														
31	0.250.	1.000.	1.402.	0.945.	0.921.	1.334.	1.127.	0.946.	1.127.	1.334.	0.921.	0.945.	1.402.	1.000. 0.250.
32	0.246.	0.989.	1.388.	0.950.	0.943.	1.368.	1.159.	0.954.	1.146.	1.381.	0.947.	0.944.	1.392.	0.974. 0.244.
33	-1.91.	-1.08.	-0.99.	0.52.	2.47.	2.58.	2.87.	0.79.	1.70.	3.52.	2.84.	-0.14.	-0.72.	-2.57. -2.75.
34														
35	0.227.	1.181.	1.043.	1.142.	1.118.	0.916.	1.096.	1.127.	1.096.	0.916.	1.118.	1.142.	1.043.	1.181. 0.227.
36	0.217.	1.154.	1.017.	1.144.	1.142.	0.938.	1.128.	1.139.	1.104.	0.944.	1.148.	1.139.	1.025.	1.150. 0.219.
37	-4.47.	-2.29.	-2.48.	0.19.	2.13.	2.42.	2.98.	1.10.	0.74.	3.06.	2.67.	-0.21.	-1.79.	-2.63. -3.49.
38														
39		1.109.	1.224.	0.969.	1.290.	0.899.	0.909.	1.330.	0.909.	0.899.	1.290.	0.969.	1.224.	1.109.
40		1.068.	1.177.	0.971.	1.334.	0.926.	0.935.	1.359.	0.927.	0.928.	1.338.	0.975.	1.197.	1.065.
41		-3.77.	-3.86.	0.19.	3.42.	2.98.	2.91.	2.17.	2.02.	3.28.	3.69.	0.60.	-2.17.	-4.02.
42														
43		0.833.	1.274.	1.219.	0.978.	1.288.	1.116.	0.918.	1.116.	1.288.	0.978.	1.219.	1.274.	0.833.
44		0.811.	1.240.	1.225.	1.023.	1.330.	1.141.	0.941.	1.150.	1.341.	1.033.	1.240.	1.246.	0.800.
45		-2.64.	-2.67.	0.53.	4.66.	3.26.	2.28.	2.55.	3.09.	4.11.	5.61.	1.76.	-2.16.	-4.00.
46														
47			0.484.	0.969.	1.221.	0.971.	1.143.	0.946.	1.143.	0.971.	1.221.	0.969.	0.484.	
48			0.476.	0.978.	1.279.	0.996.	1.152.	0.944.	1.140.	0.991.	1.242.	0.956.	0.473.	
49			-1.60.	0.91.	4.75.	2.51.	0.82.	-0.15.	-0.24.	1.99.	1.73.	-1.34.	-2.38.	
50														
51				0.503.	1.281.	1.227.	1.047.	1.405.	1.047.	1.227.	1.281.	0.503.		
52				0.492.	1.250.	1.219.	1.031.	1.357.	1.011.	1.189.	1.246.	0.491.		
53				-2.09.	-2.44.	-0.65.	-1.50.	-3.40.	-3.36.	-3.04.	-2.74.	-2.39.		
54														
55					0.837.	1.111.	1.183.	1.003.	1.183.	1.111.	0.837.			
56					0.817.	1.085.	1.136.	0.969.	1.150.	1.080.	0.811.			
57					-2.39.	-2.40.	-3.94.	-3.32.	-2.73.	-2.79.	-2.99.			
58														
59							0.227.	0.251.	0.227.					
60							0.219.	0.242.	0.219.					

C12 MAP553 06/22/88 D-205 8666MWD/MTU 89.92%HFP 50P 1 B-347 FCFM

SUMMARY OF INCORE RESULTS	MEASURED			WITH UNCERTAINTY FACTOR	TECH. SPEC. LIMIT
FZ (MAX. ASSEMBLY)	= 1.660 LOC R 8				
FZ (MAX. AVERAGE)	= 1.166				
KW/FT (MAX. AVERAGE)	= 7.286 LOC C 8			7.880	
KW/FT (MAX. PEAK)	= 9.670 LOC N 8			10.458	
F-DELTA-H (MAX. ASSEMBLY)	= 1.392 LOC C 8	REGION 15			
F-DELTA-H (MAX. ASSEMBLY)	= 1.279 LOC L12	REGION 14			
F-DELTA-H (MAX. ASSEMBLY)	= 1.033 LOC E11	REGION 12R			
F-DELTA-H (MAX. ASSEMBLY)	= 1.031 LOC J13	REGION 13A			
F-DELTA-H (MAX. ASSEMBLY)	= 0.246 LOC R 8	REGION 13			
F-DELTA-H (PEAK PIN)	= 1.516 LOC L 3	REGION 15	1.576	1.684	
F-DELTA-H (PEAK PIN)	= 1.389 LOC L12	REGION 14	1.444	1.684	
F-DELTA-H (PEAK PIN)	= 1.092 LOC E11	REGION 12R	1.135	1.684	
F-DELTA-H (PEAK PIN)	= 1.094 LOC J13	REGION 13A	1.138	1.684	
F-DELTA-H (PEAK PIN)	= 0.387 LOC R 7	REGION 13	0.402	1.684	
FQT (PENALIZED)	= 1.930 LOC N 8	REGION 15	2.027	2.583	
FQT (PENALIZED)	= 1.691 LOC L12	REGION 14	1.775	2.583	
FQT (PENALIZED)	= 1.299 LOC E11	REGION 12R	1.363	2.583	
FQT (PENALIZED)	= 1.379 LOC N 7	REGION 13A	1.448	2.583	
FQT (PENALIZED)	= 0.683 LOC R 7	REGION 13	0.717	2.583	
FQN (WITH LOCAL PEAKING)	= 1.793 LOC N 8	REGION 15			
FQN (WITH LOCAL PEAKING)	= 1.633 LOC L12	REGION 14			
FQN (WITH LOCAL PEAKING)	= 1.246 LOC E11	REGION 12R			
FQN (WITH LOCAL PEAKING)	= 1.285 LOC N 7	REGION 13A			
FQN (WITH LOCAL PEAKING)	= 0.637 LOC R 7	REGION 13			

CALCULATED POWER TILTS(NORMALIZED TO 1.000)

(-,+) QUADRANT =	1.0003	1.02
(+,+) QUADRANT =	1.0001	1.02
(-,-) QUADRANT =	1.0010	1.02
(+,-) QUADRANT =	0.9987	1.02

AXIAL OFFSET = -0.580
FXY (NEGLECTING GRIDS) = 1.557 LOC C 5 NODE 44

FQZ BASED APL FOR 3% TARGET BAND = 105.30%
FQZ BASED APL FOR 5% TARGET BAND = 102.47%

R'CVD [redacted] ....DATE.....


MAP553

A QUARTER CORE AVERAGED ASSEMBLY RELATIVE POWER. C12 MAP553 06/22/88 D-205 8666MWD/MTU 89.92%HFP 5OP 1 B-347 FCFM

	H	G	F	E	D	C	B	A	
								0.250	
1	0.946	1.127	1.334	0.921	0.945	1.402	1.000	0.250	1
	0.954	1.152	1.374	0.945	0.947	1.390	0.981	0.245	
	0.792	2.285	3.050	2.654	0.189	-0.859	-1.828	-2.332	
	1.127	1.096	0.916	1.118	1.142	1.043	1.181	0.227	
2	1.145	1.116	0.941	1.147	1.144	1.024	1.155	0.219	2
	1.672	1.884	2.716	2.549	0.195	-1.794	-2.196	-3.200	
	1.330	0.909	0.899	1.290	0.969	1.224	1.109		
3	1.368	0.932	0.925	1.330	0.972	1.193	1.074		3
	2.862	2.590	2.935	3.090	0.276	-2.494	-3.188		
	0.918	1.116	1.288	0.978	1.219	1.274	0.833		
4	0.944	1.148	1.328	1.011	1.223	1.243	0.808		4
	2.869	2.933	3.075	3.349	0.354	-2.418	-3.033		
	0.946	1.143	0.971	1.221	0.969	0.484			
5	0.944	1.156	0.987	1.241	0.965	0.475			5
	-0.212	1.104	1.607	1.642	-0.463	-1.976			
	1.405	1.047	1.227	1.281	0.503				
6	1.361	1.020	1.203	1.258	0.495				6
	-3.114	-2.513	-1.909	-1.802	-1.665				
	1.003	1.183	1.111	0.837					
7	0.972	1.149	1.083	0.821					7
	-3.064	-2.879	-2.518	-1.829					
	0.251	0.227							
8	0.242	0.219							8
	-3.640	-3.483							
	H	G	F	E	D	C	B	A	

PRED
MES
DIF

FORM 0113 (02/83)

159

. -3.54. -3.68. -3.67.

FORM 0113 (02/83)

FQN C12 MAP553 06/22/88 D-205 8666MWD/MTU 89.92%HFP 50P 1 B-347 FCFM

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.627	0.618	0.626							1
2					1.493	1.678	1.673	1.411	1.670	1.675	1.459					2
3				1.007	1.786	1.566	1.263	1.751	1.274	1.574	1.737	0.976				3
4			0.941	1.393	1.574	1.186	1.445	1.178	1.515	1.211	1.555	1.382	0.941			4
5		1.459	1.744	1.564	1.206	1.684	1.472	1.169	1.495	1.692	1.200	1.559	1.775	1.483		5
6		1.668	1.560	1.189	1.719	1.104	1.143	1.749	1.137	1.105	1.680	1.190	1.567	1.668		6
7	0.637	1.707	1.285	1.462	1.495	1.181	1.396	1.427	1.363	1.176	1.483	1.457	1.277	1.668	0.625	7
8	0.633	1.440	1.793	1.195	1.171	1.752	1.441	1.153	1.427	1.771	1.178	1.194	1.779	1.418	0.618	8
9	0.605	1.666	1.263	1.464	1.485	1.177	1.391	1.422	1.379	1.190	1.495	1.462	1.262	1.661	0.617	9
10		1.629	1.546	1.191	1.710	1.107	1.141	1.737	1.142	1.119	1.721	1.195	1.570	1.643		10
11		1.443	1.724	1.562	1.236	1.695	1.471	1.167	1.499	1.735	1.246	1.579	1.742	1.447		11
12			0.931	1.399	1.633	1.210	1.469	1.188	1.461	1.215	1.586	1.378	0.932			12
13				0.996	1.769	1.593	1.279	1.739	1.247	1.552	1.727	0.988				13
14					1.478	1.671	1.651	1.402	1.671	1.658	1.443					14
15							0.620	0.620	0.629							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

PEAK ROD ENTHALPY RISE C12 MAP553 06/22/88 D-205 8666MWD/MTU 89.92%HFP 50P 1 B-347 FCEM

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.380.	0.375.	0.382.							1
2					1.269.	1.410.	1.386.	1.166.	1.396.	1.421.	1.241.					2
3				0.851.	1.516.	1.331.	1.079.	1.481.	1.085.	1.324.	1.481.	0.832.				3
4			0.796.	1.178.	1.326.	1.014.	1.220.	0.996.	1.272.	1.038.	1.326.	1.180.	0.798.			4
5		1.223.	1.459.	1.317.	1.048.	1.446.	1.261.	0.988.	1.276.	1.456.	1.051.	1.316.	1.485.	1.235.		5
6		1.415.	1.320.	1.016.	1.471.	0.967.	0.991.	1.508.	0.985.	0.969.	1.441.	1.016.	1.332.	1.410.		6
7	0.387.	1.406.	1.091.	1.229.	1.271.	1.003.	1.204.	1.232.	1.178.	0.999.	1.261.	1.223.	1.091.	1.383.	0.382.	7
8	0.381.	1.183.	1.505.	1.004.	0.983.	1.498.	1.241.	0.987.	1.227.	1.511.	0.986.	0.997.	1.509.	1.164.	0.378.	8
9	0.376.	1.390.	1.080.	1.223.	1.259.	0.998.	1.204.	1.219.	1.177.	1.005.	1.266.	1.218.	1.087.	1.385.	0.380.	9
10		1.394.	1.301.	1.016.	1.467.	0.970.	0.990.	1.488.	0.981.	0.973.	1.471.	1.020.	1.323.	1.390.		10
11		1.231.	1.469.	1.330.	1.082.	1.462.	1.257.	0.982.	1.267.	1.475.	1.092.	1.346.	1.476.	1.213.		11
12			0.800.	1.198.	1.389.	1.041.	1.233.	0.998.	1.220.	1.036.	1.349.	1.171.	0.794.			12
13				0.833.	1.477.	1.346.	1.094.	1.472.	1.074.	1.313.	1.472.	0.830.				13
14					1.237.	1.416.	1.369.	1.160.	1.386.	1.410.	1.230.					14
15							0.381.	0.375.	0.380.							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

CALCULATED LOCAL PEAKING FACTORS C12 MAP553 06/22/88 D-205 8666MWD/MTU 89.92%HFP 50P 1 B-347 FCFM

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							1.738	1.552	1.738							1
2					1.515	1.306	1.205	1.196	1.205	1.306	1.515					2
3				1.691	1.182	1.104	1.062	1.085	1.061	1.104	1.182	1.691				3
4			1.679	1.225	1.086	1.046	1.070	1.057	1.070	1.046	1.086	1.225	1.679			4
5		1.517	1.184	1.085	1.057	1.099	1.102	1.043	1.102	1.099	1.057	1.085	1.184	1.517		5
6		1.306	1.105	1.047	1.100	1.048	1.059	1.094	1.059	1.048	1.100	1.047	1.105	1.306		6
7	1.737	1.205	1.061	1.069	1.103	1.064	1.067	1.070	1.067	1.064	1.103	1.069	1.061	1.205	1.737	7
8	1.552	1.196	1.085	1.056	1.042	1.095	1.070	1.035	1.070	1.095	1.042	1.056	1.085	1.195	1.552	8
9	1.738	1.205	1.061	1.069	1.103	1.065	1.067	1.070	1.067	1.064	1.103	1.069	1.061	1.205	1.737	9
10		1.306	1.105	1.047	1.100	1.048	1.059	1.094	1.059	1.048	1.100	1.047	1.105	1.306		10
11		1.517	1.184	1.085	1.057	1.099	1.102	1.043	1.102	1.099	1.057	1.085	1.184	1.517		11
12			1.679	1.225	1.086	1.046	1.070	1.057	1.070	1.046	1.086	1.225	1.679			12
13				1.691	1.182	1.104	1.061	1.085	1.061	1.104	1.182	1.691				13
14					1.515	1.306	1.205	1.196	1.205	1.306	1.515					14
15							1.738	1.551	1.737							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

FQT*V(Z)*FQE*FQM 3%TARGET BAND C12 MAP553 06/22/88 D-205 8666MWD/MTU 89.92%HFP 50P 1 B-347 FCFM
FULL CORE SEARCH

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.762	0.750	0.763							1
2					1.833	2.038	2.012	1.687	2.016	2.042	1.784					2
3				1.209	2.146	1.872	1.536	2.133	1.539	1.876	2.128	1.191				3
4			1.123	1.657	1.843	1.419	1.714	1.404	1.784	1.439	1.862	1.663	1.127			4
5		1.729	2.054	1.832	1.431	2.038	1.797	1.380	1.795	2.052	1.438	1.829	2.097	1.769		5
6		2.038	1.873	1.421	2.057	1.331	1.403	2.137	1.380	1.334	2.034	1.424	1.884	2.033		6
7	0.779	2.067	1.573	1.733	1.793	1.398	1.717	1.743	1.656	1.387	1.791	1.737	1.558	2.011	0.760	7
8	0.776	1.736	2.203	1.429	1.390	2.152	1.773	1.391	1.746	2.150	1.386	1.413	2.174	1.694	0.750	8
9	0.740	2.020	1.541	1.724	1.793	1.399	1.707	1.751	1.698	1.419	1.788	1.719	1.538	2.003	0.750	9
10		1.982	1.821	1.419	2.068	1.332	1.397	2.135	1.392	1.336	2.054	1.412	1.848	1.980		10
11		1.762	2.094	1.865	1.470	2.063	1.788	1.377	1.773	2.045	1.480	1.885	2.092	1.719		11
12			1.145	1.696	1.926	1.467	1.747	1.411	1.719	1.427	1.883	1.674	1.137			12
13				1.182	2.103	1.920	1.570	2.131	1.521	1.833	2.086	1.186				13
14					1.769	2.036	1.999	1.683	2.010	2.016	1.730					14
15							0.761	0.752	0.764							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

57	1.0800	1.1100
58	1.0800	1.1100
59	1.0800	1.1100
60	1.0800	1.1100
61	1.0800	1.1100

FQT*V(Z)*FQE*FQM 5%TARGET BAND C12 MAP553 06/22/88 D-205 8666MWD/MTU 89.92%HFP 5OP 1 B-347 FCFM
FULL CORE SEARCH

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.783	0.771	0.784							1
2					1.884	2.094	2.068	1.734	2.071	2.098	1.833					2
3				1.242	2.205	1.924	1.578	2.192	1.581	1.927	2.186	1.223				3
4			1.154	1.703	1.893	1.459	1.762	1.442	1.833	1.479	1.913	1.708	1.159			4
5		1.776	2.111	1.883	1.470	2.094	1.847	1.418	1.844	2.109	1.478	1.880	2.154	1.818		5
6		2.094	1.924	1.461	2.114	1.368	1.442	2.195	1.419	1.370	2.090	1.464	1.937	2.089		6
7	0.800	2.124	1.616	1.780	1.842	1.436	1.764	1.791	1.702	1.425	1.840	1.785	1.602	2.067	0.781	7
8	0.797	1.784	2.264	1.468	1.428	2.212	1.822	1.429	1.794	2.210	1.424	1.451	2.234	1.741	0.771	8
9	0.760	2.076	1.583	1.772	1.842	1.438	1.754	1.799	1.745	1.458	1.837	1.767	1.580	2.059	0.771	9
10		2.037	1.871	1.458	2.125	1.368	1.435	2.193	1.430	1.373	2.110	1.451	1.899	2.034		10
11		1.811	2.151	1.917	1.511	2.120	1.837	1.415	1.822	2.102	1.521	1.937	2.150	1.766		11
12			1.177	1.743	1.979	1.508	1.795	1.449	1.767	1.466	1.935	1.720	1.168			12
13				1.215	2.161	1.973	1.613	2.190	1.563	1.884	2.144	1.219				13
14					1.818	2.092	2.054	1.729	2.066	2.071	1.777					14
15							0.782	0.773	0.785							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FQT*V(Z)*FQE*FQM 3%TARGET BAND C12 MAP553 06/22/88 D-205 8666MWD/MTU 89.92%HFP 5OP 1 B-347 FCFM
SEARCH BETWEEN NODES 6 AND 56

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.762.	0.750.	0.763.							1
2					1.833.	2.038.	2.012.	1.687.	2.016.	2.042.	1.784.					2
3				1.209.	2.146.	1.872.	1.536.	2.133.	1.539.	1.876.	2.128.	1.191.				3
4			1.123.	1.657.	1.843.	1.419.	1.714.	1.404.	1.784.	1.439.	1.862.	1.663.	1.127.			4
5		1.729.	2.054.	1.832.	1.431.	2.038.	1.797.	1.380.	1.795.	2.052.	1.438.	1.829.	2.097.	1.769.		5
6		2.038.	1.873.	1.421.	2.057.	1.331.	1.403.	2.137.	1.380.	1.334.	2.034.	1.424.	1.884.	2.033.		6
7	0.779.	2.067.	1.573.	1.733.	1.793.	1.398.	1.717.	1.743.	1.656.	1.387.	1.791.	1.737.	1.558.	2.011.	0.760.	7
8	0.776.	1.736.	2.203.	1.429.	1.390.	2.152.	1.773.	1.391.	1.746.	2.150.	1.386.	1.413.	2.174.	1.694.	0.750.	8
9	0.740.	2.020.	1.541.	1.724.	1.793.	1.399.	1.707.	1.751.	1.698.	1.419.	1.788.	1.719.	1.538.	2.003.	0.750.	9
10		1.982.	1.821.	1.419.	2.068.	1.332.	1.397.	2.135.	1.392.	1.336.	2.054.	1.412.	1.848.	1.980.		10
11		1.762.	2.094.	1.865.	1.470.	2.063.	1.788.	1.377.	1.773.	2.045.	1.480.	1.885.	2.092.	1.719.		11
12			1.145.	1.696.	1.926.	1.467.	1.747.	1.411.	1.719.	1.427.	1.883.	1.674.	1.137.			12
13				1.182.	2.103.	1.920.	1.570.	2.131.	1.521.	1.833.	2.086.	1.186.				13
14					1.769.	2.036.	1.999.	1.683.	2.010.	2.016.	1.730.					14
15							0.761.	0.752.	0.764.							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

MAXIMUM FQT*V(Z)*FQE*FQM C12 MAP553 06/22/88 D-205 8666MWD/MTU 89.92%HFP 50P 1 B-347 FCFM

AXIAL NODE	3%TARGET	ASSEMBLY#	5%TARGET	ASSEMBLY#
1	.76806	52	.78863	52
2	.91720	118	.94176	118
3	1.0247	118	1.0522	118
4	1.1605	118	1.1916	118
5	1.7495	50	1.7964	50
6	1.7705	50	1.8182	50
7	1.8688	50	1.9193	50
8	1.9930	50	2.0470	50
9	2.0781	84	2.1347	84
10	2.1407	74	2.1992	74
11	2.1800	74	2.2397	74
12	2.1978	74	2.2582	74
13	2.2033	74	2.2641	74
14	2.1910	74	2.2516	74
15	2.1792	74	2.2397	74
16	2.1325	74	2.1917	74
17	2.0510	84	2.1079	84
18	2.1054	84	2.1639	84
19	2.1093	84	2.1679	84
20	2.0982	84	2.1565	84
21	2.0840	12	2.1418	12
22	2.0755	12	2.1331	12
23	2.0572	12	2.1144	12
24	2.0390	12	2.0957	12
25	2.0308	12	2.0872	12
26	2.0127	12	2.0687	12
27	1.9656	12	2.0202	12
28	1.9078	84	1.9608	84
29	1.9631	84	2.0177	84
30	1.9791	84	2.0341	84
31	1.9789	84	2.0339	84
32	1.9813	84	2.0363	84
33	1.9874	84	2.0426	84
34	1.9878	84	2.0430	84
35	1.9901	84	2.0454	84
36	1.9895	84	2.0448	84
37	1.9841	12	2.0392	12
38	1.9485	12	2.0027	12
39	1.9158	84	1.9690	84
40	1.9779	84	2.0328	84
41	1.9890	84	2.0443	84
42	1.9971	84	2.0526	84
43	2.0178	42	2.0739	42
44	2.0481	42	2.1049	42
45	2.0613	42	2.1185	42
46	2.0799	42	2.1376	42
47	2.0835	12	2.1413	12
48	2.0899	12	2.1480	12
49	2.0515	12	2.1085	12
50	1.9794	81	2.0343	81
51	2.0350	12	2.0915	12
52	2.0416	12	2.0983	12
53	2.0019	81	2.0575	81
54	1.9438	81	1.9978	81
55	1.8472	81	1.8985	81
56	1.7380	47	1.7862	47

171

FQT*V(Z)*FQE*FQM 5%TARGET BAND C12 MAP553 06/22/88 D-205 8666MWD/MTU 89.92%HFP 5OP 1 B-347 FCFM
SEARCH BETWEEN NODES 6 AND 56

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.783	0.771	0.784							1
2					1.884	2.094	2.068	1.734	2.071	2.098	1.833					2
3				1.242	2.205	1.924	1.578	2.192	1.581	1.927	2.186	1.223				3
4			1.154	1.703	1.893	1.459	1.762	1.442	1.833	1.479	1.913	1.708	1.159			4
5		1.776	2.111	1.883	1.470	2.094	1.847	1.418	1.844	2.109	1.478	1.880	2.154	1.818		5
6		2.094	1.924	1.461	2.114	1.368	1.442	2.195	1.419	1.370	2.090	1.464	1.937	2.089		6
7	0.800	2.124	1.616	1.780	1.842	1.436	1.764	1.791	1.702	1.425	1.840	1.785	1.602	2.067	0.781	7
8	0.797	1.784	2.264	1.468	1.428	2.212	1.822	1.429	1.794	2.210	1.424	1.451	2.234	1.741	0.771	8
9	0.760	2.076	1.583	1.772	1.842	1.438	1.754	1.799	1.745	1.458	1.837	1.767	1.580	2.059	0.771	9
10		2.037	1.871	1.458	2.125	1.368	1.435	2.193	1.430	1.373	2.110	1.451	1.899	2.034		10
11		1.811	2.151	1.917	1.511	2.120	1.837	1.415	1.822	2.102	1.521	1.937	2.150	1.766		11
12			1.177	1.743	1.979	1.508	1.795	1.449	1.767	1.466	1.935	1.720	1.168			12
13				1.215	2.161	1.973	1.613	2.190	1.563	1.884	2.144	1.219				13
14					1.818	2.092	2.054	1.729	2.066	2.071	1.777					14
15							0.782	0.773	0.785							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

1	57	1.6167	47	1.6616	47
2	58	1.4776	47	1.5186	47
3	59	.74224	124	.76285	124
4	60	.54268	124	.55776	124
5	61	.45143	118	.46397	118
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PDQ ACTIVATIONS FOR EACH THIMBLE

THIMBLE		(X-ORD, Y-ORD)	REGION 1	REGION 2	REGION 3	REGION 4	REGION 5	REGION 6	REGION 7	REGION 8
1	M 3	(-60., 75.)	0.195E+17	0.880E+16	0.912E+16	0.208E+17	0.0	0.0	0.0	0.0
2	J15	(-15., -105.)	0.146E+17	0.854E+16	0.439E+16	0.469E+16	0.0	0.0	0.0	0.0
3	F 4	(30., 60.)	0.414E+17	0.174E+17	0.180E+17	0.429E+17	0.0	0.0	0.0	0.0
4	L 8	(-45., 0.)	0.393E+17	0.162E+17	0.170E+17	0.413E+17	0.0	0.0	0.0	0.0
5	F 8	(30., 0.)	0.532E+17	0.168E+17	0.173E+17	0.543E+17	0.0	0.0	0.0	0.0
6	D12	(60., -60.)	0.368E+17	0.139E+17	0.143E+17	0.384E+17	0.0	0.0	0.0	0.0
7	B 5	(90., 45.)	0.283E+17	0.109E+17	0.111E+17	0.299E+17	0.0	0.0	0.0	0.0
8	H 6	(0., 30.)	0.530E+17	0.168E+17	0.170E+17	0.534E+17	0.0	0.0	0.0	0.0
9	J 3	(-15., 75.)	0.415E+17	0.181E+17	0.182E+17	0.424E+17	0.0	0.0	0.0	0.0
10	D 3	(60., 75.)	0.195E+17	0.880E+16	0.912E+16	0.208E+17	0.0	0.0	0.0	0.0
11	L 9	(-45., -15.)	0.463E+17	0.162E+17	0.169E+17	0.478E+17	0.0	0.0	0.0	0.0
12	B10	(90., -30.)	0.391E+17	0.145E+17	0.143E+17	0.395E+17	0.0	0.0	0.0	0.0
13	L 4	(-45., 60.)	0.481E+17	0.168E+17	0.174E+17	0.505E+17	0.0	0.0	0.0	0.0
14	F13	(30., -75.)	0.462E+17	0.176E+17	0.180E+17	0.486E+17	0.0	0.0	0.0	0.0
15	F 6	(30., 30.)	0.336E+17	0.167E+17	0.171E+17	0.342E+17	0.0	0.0	0.0	0.0
16	J12	(-15., -60.)	0.462E+17	0.163E+17	0.171E+17	0.489E+17	0.0	0.0	0.0	0.0
17	B 7	(90., 15.)	0.429E+17	0.153E+17	0.139E+17	0.384E+17	0.0	0.0	0.0	0.0
18	H 1	(0., 105.)	0.162E+17	0.920E+16	0.397E+16	0.436E+16	0.0	0.0	0.0	0.0
19	G 9	(15., -15.)	0.436E+17	0.160E+17	0.163E+17	0.440E+17	0.0	0.0	0.0	0.0
20	G 7	(15., 15.)	0.436E+17	0.160E+17	0.163E+17	0.440E+17	0.0	0.0	0.0	0.0
21	F11	(30., -45.)	0.566E+17	0.162E+17	0.166E+17	0.575E+17	0.0	0.0	0.0	0.0
22	N 5	(-75., 45.)	0.466E+17	0.166E+17	0.170E+17	0.491E+17	0.0	0.0	0.0	0.0
23	J10	(-15., -30.)	0.400E+17	0.161E+17	0.164E+17	0.402E+17	0.0	0.0	0.0	0.0
24	J 5	(-15., 45.)	0.462E+17	0.161E+17	0.167E+17	0.472E+17	0.0	0.0	0.0	0.0
25	B 8	(90., 0.)	0.371E+17	0.152E+17	0.132E+17	0.315E+17	0.0	0.0	0.0	0.0
26	N10	(-75., -30.)	0.461E+17	0.176E+17	0.180E+17	0.484E+17	0.0	0.0	0.0	0.0
27	C12	(75., -60.)	0.190E+17	0.872E+16	0.893E+16	0.198E+17	0.0	0.0	0.0	0.0
28	J 7	(-15., 15.)	0.436E+17	0.160E+17	0.163E+17	0.440E+17	0.0	0.0	0.0	0.0
29	D 7	(60., 15.)	0.461E+17	0.163E+17	0.170E+17	0.487E+17	0.0	0.0	0.0	0.0
30	L14	(-45., -90.)	0.284E+17	0.109E+17	0.112E+17	0.302E+17	0.0	0.0	0.0	0.0
31	F 2	(30., 90.)	0.392E+17	0.145E+17	0.144E+17	0.397E+17	0.0	0.0	0.0	0.0
32	F 9	(30., -15.)	0.404E+17	0.162E+17	0.167E+17	0.418E+17	0.0	0.0	0.0	0.0
33	N 7	(-75., 15.)	0.413E+17	0.181E+17	0.181E+17	0.421E+17	0.0	0.0	0.0	0.0
34	A 9	(105., -15.)	0.145E+17	0.854E+16	0.436E+16	0.466E+16	0.0	0.0	0.0	0.0
35	N12	(-75., -60.)	0.190E+17	0.872E+16	0.893E+16	0.198E+17	0.0	0.0	0.0	0.0
36	R 8	(-105., 0.)	0.161E+17	0.920E+16	0.394E+16	0.433E+16	0.0	0.0	0.0	0.0
37	H 4	(0., 60.)	0.399E+17	0.167E+17	0.175E+17	0.422E+17	0.0	0.0	0.0	0.0
38	H11	(0., -45.)	0.391E+17	0.161E+17	0.169E+17	0.409E+17	0.0	0.0	0.0	0.0
39	D 5	(60., 45.)	0.481E+17	0.168E+17	0.173E+17	0.504E+17	0.0	0.0	0.0	0.0
40	L 6	(-45., 30.)	0.567E+17	0.163E+17	0.167E+17	0.577E+17	0.0	0.0	0.0	0.0
41	D10	(60., -30.)	0.413E+17	0.174E+17	0.179E+17	0.428E+17	0.0	0.0	0.0	0.0
42	G14	(15., -90.)	0.430E+17	0.153E+17	0.140E+17	0.387E+17	0.0	0.0	0.0	0.0
43	H13	(0., -75.)	0.540E+17	0.180E+17	0.179E+17	0.540E+17	0.0	0.0	0.0	0.0
44	C 8	(75., 0.)	0.539E+17	0.180E+17	0.178E+17	0.536E+17	0.0	0.0	0.0	0.0
45	H 3	(0., 75.)	0.540E+17	0.180E+17	0.179E+17	0.540E+17	0.0	0.0	0.0	0.0
46	N 8	(-75., 0.)	0.539E+17	0.180E+17	0.178E+17	0.536E+17	0.0	0.0	0.0	0.0
47	E11	(45., -45.)	0.339E+17	0.183E+17	0.187E+17	0.352E+17	0.0	0.0	0.0	0.0
48	L11	(-45., -45.)	0.339E+17	0.183E+17	0.187E+17	0.352E+17	0.0	0.0	0.0	0.0
49	E 5	(45., 45.)	0.339E+17	0.183E+17	0.187E+17	0.352E+17	0.0	0.0	0.0	0.0
50	L 5	(-45., 45.)	0.339E+17	0.183E+17	0.187E+17	0.352E+17	0.0	0.0	0.0	0.0

244

C12 MAP554 07/05/88 D-228 9126MWD/MTU 99.65%HFP 5OP 1 B-262 FCFM

SUMMARY OF INCORE RESULTS	MEASURED			WITH UNCERTAINTY FACTOR	TECH. SPEC. LIMIT
FZ (MAX. ASSEMBLY)	= 1.634 LOC J15				
FZ (MAX. AVERAGE)	= 1.175				
KW/FT (MAX. AVERAGE)	= 8.093 LOC F 8			8.752	
KW/FT (MAX. PEAK)	= 10.957 LOC F 8			11.850	
F-DELTA-H (MAX. ASSEMBLY)	= 1.393 LOC F 8	REGION 15			
F-DELTA-H (MAX. ASSEMBLY)	= 1.278 LOC L12	REGION 14			
F-DELTA-H (MAX. ASSEMBLY)	= 1.033 LOC E11	REGION 12R			
F-DELTA-H (MAX. ASSEMBLY)	= 1.024 LOC N 7	REGION 13A			
F-DELTA-H (MAX. ASSEMBLY)	= 0.242 LOC R 8	REGION 13			
F-DELTA-H (PEAK PIN)	= 1.522 LOC F 8	REGION 15		1.583	1.651
F-DELTA-H (PEAK PIN)	= 1.384 LOC L12	REGION 14		1.439	1.651
F-DELTA-H (PEAK PIN)	= 1.094 LOC E11	REGION 12R		1.137	1.651
F-DELTA-H (PEAK PIN)	= 1.087 LOC N 7	REGION 13A		1.130	1.651
F-DELTA-H (PEAK PIN)	= 0.382 LOC R 7	REGION 13		0.397	1.651
FQT (PENALIZED)	= 1.878 LOC F 8	REGION 15		1.972	2.328
FQT (PENALIZED)	= 1.722 LOC L12	REGION 14		1.808	2.328
FQT (PENALIZED)	= 1.315 LOC E11	REGION 12R		1.381	2.328
FQT (PENALIZED)	= 1.339 LOC G 3	REGION 13A		1.406	2.328
FQT (PENALIZED)	= 0.662 LOC R 7	REGION 13		0.695	2.328
FQN (WITH LOCAL PEAKING)	= 1.831 LOC F 8	REGION 15			
FQN (WITH LOCAL PEAKING)	= 1.672 LOC L12	REGION 14			
FQN (WITH LOCAL PEAKING)	= 1.282 LOC E11	REGION 12R			
FQN (WITH LOCAL PEAKING)	= 1.296 LOC G 3	REGION 13A			
FQN (WITH LOCAL PEAKING)	= 0.618 LOC R 7	REGION 13			
CALCULATED POWER TILTS(NORMALIZED TO 1.000)					
			(-,+) QUADRANT =	1.0001	1.02
			(+,+) QUADRANT =	0.9996	1.02
			(-,-) QUADRANT =	1.0019	1.02
			(+,-) QUADRANT =	0.9984	1.02
AXIAL OFFSET	= -2.792				
FXY (NEGLECTING GRIDS)	= 1.558 LOC C 5 NODE 44				

FQZ BASED APL FOR 3% TARGET BAND = 108.95%
FQZ BASED APL FOR 5% TARGET BAND = 106.01%

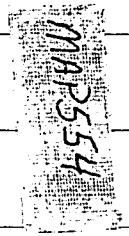
FORM 0113 (02/83)

245

[redacted]

R'CVD.....DATE.....

INCORE - CP&L VERSION PNR16021 - 07/05/88



FORM 0113 (02/83)

C12 MAP554 07/05/88 D-228 9126MWD/MTU 99.65%HFP 50P 1 B-262 FCFM

FINAL COMPARISON OF SATURATION ACTIVITY AND PDQ ACTIVATION

	THIMBLE		STATUS	MEASURED AXIAL FACTOR	REGION PERCENTAGE DIFFERENCE 1- 4	4-43	43-58	58-61	F*S(Z)
1	M 3		GOOD	1.1570	11.1023	1.1679	-3.0398	-3.0103	1.1570
2	J15		NONE						
3	F 4		NONE						
4	L 8		GOOD	1.1597	13.4495	3.6791	2.2613	8.3310	1.1597
5	F 8		GOOD	1.1458	-4.3972	3.0425	4.7274	7.5233	1.1458
6	D12		GOOD	1.1572	-8.0830	-3.0050	-2.0388	4.5411	1.1572
7	B 5		GOOD	1.1772	-8.3041	-2.3330	-3.6685	-9.7582	1.1772
8	H 6		GOOD	1.1316	3.3832	3.9413	3.5105	-5.3429	1.1379
9	J 3		GOOD	1.1330	1.6837	-2.2573	-3.4295	2.9649	1.1462
10	D 3		GOOD	1.1550	-0.7374	-3.0170	-7.0607	-3.2858	1.1570
11	L 9		GOOD	1.1537	4.6772	1.0404	2.5465	5.5315	1.1537
12	B10		GOOD	1.1595	-23.0854	-4.8097	-5.2524	-15.2658	1.1595
13	L 4		GOOD	1.1594	-1.3042	-1.8357	-0.1647	-0.9943	1.1595
14	F13		GOOD	1.1631	-4.4520	-4.7695	-3.5846	-6.4299	1.1631
15	F 6		GOOD	1.1614	18.0093	2.7123	1.5706	-0.9422	1.1614
16	J12		GOOD	1.1589	-5.4826	0.6835	-1.1495	-8.4044	1.1589
17	B 7		GOOD	1.1233	-4.3412	-3.3943	-5.5478	-16.1817	1.1725
18	H 1		NONE						
19	G 9		GOOD	1.1426	8.9617	-0.1509	-0.4282	-3.4296	1.1432
20	G 7		GOOD	1.1327	0.0447	-0.5443	-0.5310	2.4690	1.1327
21	F11		GOOD	1.1452	-7.7276	1.9683	5.9725	8.3531	1.1452
22	N 5		GOOD	1.1722	-15.8475	-6.1341	-1.6781	1.4758	1.1722
23	J10		GOOD	1.1397	7.9448	2.9721	3.0836	11.6322	1.1397
24	J 5		GOOD	1.1358	4.6397	1.7192	2.1572	6.6095	1.1358
25	B 8		GOOD	1.1467	7.6991	-1.9648	-4.0750	-7.1506	1.1945
26	N10		GOOD	1.1618	5.8506	-3.7631	-4.3583	-12.7791	1.1618
27	C12		NONE						
28	J 7		GOOD	1.1285	11.3024	3.2097	0.3928	-6.7841	1.1307
29	D 7		GOOD	1.1523	9.7586	1.5473	0.0607	-8.1244	1.1523
30	L14		GOOD	1.1712	-10.9088	-3.3762	-3.0073	-3.4760	1.1712
31	F 2		GOOD	1.1383	-10.6692	-2.3077	-2.0639	-7.3603	1.1440
32	F 9		GOOD	1.1544	2.5197	3.2981	4.2773	19.0424	1.1544
33	N 7		GOOD	1.1343	8.1513	-0.8787	-3.2731	-4.1368	1.1592
34	A 9		NONE						
35	N12		GOOD	1.1466	11.0048	-0.1560	-5.6367	-8.3316	1.1557
36	R 8		NONE						
37	H 4		NONE						
38	H11		GOOD	1.1636	18.6140	4.2072	3.0657	3.7398	1.1636
39	D 5		GOOD	1.1615	-13.7615	-0.5217	-0.3613	-8.7471	1.1615
40	L 6		GOOD	1.1359	-6.9986	2.6646	5.7837	5.2632	1.1359
41	D10		GOOD	1.1662	1.9088	0.3062	0.9019	11.9721	1.1663
42	G14		GOOD	1.1339	-34.1286	-2.2724	-2.5661	-0.5676	1.1831
43	H13		GOOD	1.1217	-1.6313	-4.0626	-4.3881	-8.7520	1.1379
44	C 8		GOOD	1.1340	-6.1640	-2.0038	0.3266	2.9055	1.1340
45	H 3		NONE						
46	N 8		GOOD	1.1291	-1.4908	-1.2424	-1.1073	-8.1638	1.1520
47	E11		GOOD	1.1632	11.5884	5.6905	7.8132	27.8759	1.1632
48	L11		GOOD	1.1678	20.4298	4.4980	3.9808	8.5957	1.1678
49	E 5		GOOD	1.1625	14.5463	1.7098	2.2360	15.6666	1.1625
50	L 5		NONE						
51									
52	AVG. OF ABSOLUTE VALUES OF GOOD THIMBLES ONLY			1.1497	8.95	2.56	3.00	7.61	

FORM 0113 (02/83)

SYMMETRIC THIMBLE COMPARISON C12 MAP554 07/05/88 D-228 9126MWD/MTU 99.65%HFP 5OP 1 B-262 FCFM

THMBL	LOC	INTEGRAL	THMBL	LOC	INTEGRAL	RATIO
1	M 3	0.32797E+02	10	D 3	0.31411E+02	1.0441
10	D 3	0.31411E+02	1	M 3	0.32797E+02	.95776
19	G 9	0.60232E+02	20	G 7	0.60000E+02	1.0039
19	G 9	0.60232E+02	28	J 7	0.61701E+02	.97619
20	G 7	0.60000E+02	19	G 9	0.60232E+02	.99615
20	G 7	0.60000E+02	28	J 7	0.61701E+02	.97243
28	J 7	0.61701E+02	19	G 9	0.60232E+02	1.0244
28	J 7	0.61701E+02	20	G 7	0.60000E+02	1.0284
44	C 8	0.65948E+02	46	N 8	0.65892E+02	1.0009
46	N 8	0.65892E+02	44	C 8	0.65948E+02	.99914
47	E11	0.71929E+02	48	L11	0.70513E+02	1.0201
47	E11	0.71929E+02	49	E 5	0.68933E+02	1.0435
48	L11	0.70513E+02	47	E11	0.71929E+02	.98032
48	L11	0.70513E+02	49	E 5	0.68933E+02	1.0229
49	E 5	0.68933E+02	47	E11	0.71929E+02	.95836
49	E 5	0.68933E+02	48	L11	0.70513E+02	.97759

ASM"Y RELATIVE POWER EXPECTED / MEASURED/ % DIFF SUMS: 156.9915 / 156.9966 / -35.8553

					0.224	0.248	0.224							
					0.218	0.241	0.217							
					-2.77	-2.75	-3.07							
				0.833	1.103	1.172	0.996	1.172	1.103	0.833				
				0.837	1.079	1.148	0.974	1.149	1.080	0.811				
				0.50	-2.12	-2.10	-2.12	-2.01	-2.02	-2.65				
			0.505	1.278	1.219	1.042	1.400	1.042	1.219	1.278	0.505			
			0.506	1.275	1.198	1.018	1.370	1.018	1.192	1.239	0.485			
			0.22	-0.22	-1.71	-2.23	-2.15	-2.23	-2.16	-3.06	-3.82			
		0.486	0.968	1.218	0.972	1.142	0.947	1.142	0.972	1.218	0.968	0.486		
		0.473	0.955	1.208	0.968	1.142	0.947	1.187	0.996	1.217	0.959	0.475		
		-2.62	-1.32	-0.84	-0.48	0.04	-0.01	4.01	2.47	-0.09	-0.95	-2.27		
	0.829	1.271	1.216	0.983	1.299	1.121	0.924	1.121	1.299	0.983	1.216	1.271	0.829	
	0.793	1.215	1.202	0.993	1.322	1.148	0.953	1.159	1.334	1.002	1.217	1.254	0.810	
	-4.40	-4.44	-1.16	0.98	1.81	2.46	3.09	3.39	2.66	1.92	0.04	-1.34	-2.36	
	1.100	1.215	0.969	1.301	0.909	0.918	1.346	0.918	0.909	1.301	0.969	1.215	1.100	
	1.069	1.180	0.969	1.351	0.933	0.945	1.393	0.937	0.929	1.324	0.978	1.198	1.064	
	-2.80	-2.88	-0.05	3.85	2.60	2.90	3.48	2.12	2.22	1.83	0.93	-1.42	-3.25	
0.223	1.169	1.037	1.140	1.123	0.925	1.105	1.136	1.105	0.925	1.123	1.140	1.037	1.169	0.223
0.221	1.157	1.024	1.152	1.166	0.955	1.136	1.160	1.113	0.944	1.151	1.154	1.020	1.127	0.216
-1.30	-1.03	-1.25	1.03	3.84	3.24	2.77	2.14	0.71	2.07	2.50	1.21	-1.63	-3.62	-3.23
0.247	0.992	1.395	0.945	0.926	1.349	1.136	0.955	1.136	1.349	0.926	0.945	1.395	0.992	0.247
0.242	0.981	1.381	0.954	0.959	1.389	1.166	0.963	1.155	1.393	0.956	0.947	1.377	0.965	0.240
-1.93	-1.03	-1.02	0.92	3.54	3.02	2.64	0.78	1.74	3.32	3.20	0.12	-1.31	-2.68	-2.83
0.223	1.169	1.037	1.140	1.123	0.925	1.105	1.136	1.105	0.925	1.123	1.140	1.037	1.169	0.223
0.214	1.143	1.012	1.145	1.148	0.952	1.143	1.152	1.116	0.958	1.158	1.142	1.017	1.133	0.215
-4.27	-2.21	-2.39	0.47	2.22	2.86	3.45	1.41	0.95	3.52	3.16	0.18	-1.95	-3.11	-3.96
	1.100	1.215	0.969	1.301	0.909	0.918	1.346	0.918	0.909	1.301	0.969	1.215	1.100	
	1.061	1.171	0.972	1.345	0.938	0.950	1.387	0.942	0.940	1.352	0.984	1.191	1.046	
	-3.53	-3.63	0.28	3.42	3.15	3.50	3.04	2.59	3.32	3.91	1.55	-2.01	-4.87	
	0.829	1.271	1.216	0.983	1.299	1.121	0.924	1.121	1.299	0.983	1.216	1.271	0.829	
	0.809	1.240	1.225	1.029	1.341	1.152	0.961	1.165	1.350	1.033	1.239	1.245	0.789	
	-2.39	-2.44	0.71	4.69	3.22	2.74	3.92	3.91	3.94	5.08	1.89	-2.04	-4.84	
		0.486	0.968	1.218	0.972	1.142	0.947	1.142	0.972	1.218	0.968	0.486		
		0.479	0.979	1.278	0.992	1.145	0.949	1.141	0.986	1.234	0.955	0.474		
		-1.40	1.08	4.88	2.06	0.34	0.21	-0.05	1.37	1.28	-1.40	-2.37		
			0.505	1.278	1.219	1.042	1.400	1.042	1.219	1.278	0.505			
			0.493	1.241	1.203	1.023	1.353	1.003	1.170	1.236	0.493			
			-2.23	-2.90	-1.29	-1.83	-3.37	-3.68	-3.97	-3.34	-2.35			
				0.833	1.103	1.172	0.996	1.172	1.103	0.833				
				0.809	1.071	1.128	0.963	1.139	1.066	0.800				
				-2.85	-2.87	-3.82	-3.28	-2.85	-3.32	-3.99				
					0.224	0.248	0.224							
					0.215	0.240	0.216							

ASSEMBLY RELATIVE POWER C12 MAP554 07/05/88 D-228 9126MWD/MTU 99.65%HFP 50P 1 B-262 FCFM

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.218	0.241	0.217							1
2					0.837	1.079	1.148	0.974	1.149	1.080	0.811					2
3				0.506	1.275	1.198	1.018	1.370	1.018	1.192	1.239	0.485				3
4			0.473	0.955	1.208	0.968	1.142	0.947	1.187	0.996	1.217	0.959	0.475			4
5		0.793	1.215	1.202	0.993	1.322	1.148	0.953	1.159	1.334	1.002	1.217	1.254	0.810		5
6		1.069	1.180	0.969	1.351	0.933	0.945	1.393	0.937	0.929	1.324	0.978	1.198	1.064		6
7	0.221	1.157	1.024	1.152	1.166	0.955	1.136	1.160	1.113	0.944	1.151	1.154	1.020	1.127	0.216	7
8	0.242	0.981	1.381	0.954	0.959	1.389	1.166	0.963	1.155	1.393	0.956	0.947	1.377	0.965	0.240	8
9	0.214	1.143	1.012	1.145	1.148	0.952	1.143	1.152	1.116	0.958	1.158	1.142	1.017	1.133	0.215	9
10		1.061	1.171	0.972	1.345	0.938	0.950	1.387	0.942	0.940	1.352	0.984	1.191	1.046		10
11		0.809	1.240	1.225	1.029	1.341	1.152	0.961	1.165	1.350	1.033	1.239	1.245	0.789		11
12			0.479	0.979	1.278	0.992	1.145	0.949	1.141	0.986	1.234	0.955	0.474			12
13				0.493	1.241	1.203	1.023	1.353	1.003	1.170	1.236	0.493				13
14					0.809	1.071	1.128	0.963	1.139	1.066	0.800					14
15							0.215	0.240	0.216							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

A QUARTER CORE AVERAGED ASSEMBLY RELATIVE POWER C12 MAP554 07/05/88 D-228 9126MWD/MTU 99.65%HFP 50P 1 B-262 FCFM

	H	G	F	E	D	C	B	A	
	0.955	1.136	1.349	0.926	0.945	1.395	0.992	0.247	
1	0.963	1.161	1.391	0.957	0.950	1.379	0.973	0.241	1
	0.776	2.189	3.170	3.370	0.520	-1.161	-1.858	-2.381	
	1.136	1.105	0.925	1.123	1.140	1.037	1.169	0.223	
2	1.156	1.127	0.952	1.156	1.148	1.018	1.140	0.216	2
	1.772	1.969	2.921	2.929	0.723	-1.805	-2.493	-3.189	
	1.346	0.918	0.909	1.301	0.969	1.215	1.100		
3	1.390	0.944	0.935	1.343	0.976	1.185	1.060		3
	3.259	2.776	2.821	3.253	0.678	-2.484	-3.612		
	0.924	1.121	1.299	0.983	1.216	1.271	0.829		
4	0.957	1.156	1.337	1.014	1.221	1.239	0.800		4
	3.504	3.126	2.908	3.166	0.371	-2.565	-3.498		
	0.947	1.142	0.972	1.218	0.968	0.486			
5	0.948	1.154	0.985	1.234	0.962	0.475			5
	0.098	1.083	1.357	1.308	-0.646	-2.168			
	1.400	1.042	1.219	1.278	0.505				
6	1.361	1.016	1.191	1.248	0.494				6
	-2.762	-2.494	-2.283	-2.381	-2.045				
	0.996	1.172	1.103	0.833					
7	0.969	1.141	1.074	0.814					7
	-2.701	-2.693	-2.582	-2.248					
	0.248	0.224							
8	0.240	0.217							8
	-3.067	-3.337							
	H	G	F	E	D	C	B	A	

	PRED
1	MES
	DIF

FORM 0113 (02/83)

184

. -4.14. -3.38. -3.37.

FORM 0113 (02/83)

180

C12 MAP554 07/05/88 D-228 9126MWD/MTU 99.65%HFP 50P 1 B-262 FCFM

MAX FQT INCLUDES LOCA AXIAL PENALTY FACTOR

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.684	0.675	0.683							1
2					1.643	1.812	1.789	1.503	1.811	1.830	1.599					2
3				1.104	1.968	1.725	1.383	1.903	1.406	1.727	1.897	1.052				3
4			1.037	1.530	1.723	1.308	1.629	1.311	1.701	1.346	1.715	1.521	1.038			4
5		1.601	1.915	1.721	1.339	1.875	1.628	1.304	1.654	1.887	1.336	1.730	1.964	1.638		5
6		1.810	1.710	1.322	1.928	1.233	1.272	1.954	1.268	1.229	1.882	1.330	1.728	1.787		6
7	0.695	1.824	1.395	1.634	1.668	1.335	1.539	1.582	1.515	1.328	1.645	1.639	1.378	1.761	0.674	7
8	0.690	1.533	1.945	1.316	1.314	1.953	1.586	1.289	1.588	1.972	1.318	1.312	1.909	1.497	0.669	8
9	0.662	1.787	1.395	1.633	1.646	1.338	1.556	1.579	1.530	1.347	1.662	1.632	1.388	1.756	0.666	9
10		1.812	1.707	1.326	1.912	1.239	1.282	1.950	1.283	1.252	1.930	1.344	1.739	1.798		10
11		1.599	1.912	1.731	1.376	1.895	1.637	1.315	1.678	1.939	1.381	1.755	1.939	1.588		11
12			1.027	1.546	1.808	1.338	1.641	1.317	1.645	1.346	1.749	1.523	1.034			12
13				1.086	1.944	1.741	1.396	1.887	1.374	1.710	1.913	1.089				13
14					1.627	1.842	1.764	1.496	1.786	1.782	1.599					14
15							0.675	0.678	0.687							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

181

FORM 0113 (02/83)

FQN C12 MAP554 07/05/88 D-228 9126MWD/MTU 99.65%HFP 50P 1 B-262 FCFM

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.609	0.602	0.607							1
2					1.514	1.646	1.611	1.362	1.620	1.679	1.473					2
3				1.035	1.816	1.597	1.275	1.743	1.296	1.598	1.751	0.986				3
4			0.962	1.417	1.593	1.213	1.494	1.224	1.560	1.248	1.585	1.409	0.962			4
5		1.475	1.765	1.591	1.243	1.731	1.510	1.212	1.534	1.742	1.241	1.599	1.811	1.508		5
6		1.660	1.582	1.225	1.779	1.142	1.177	1.811	1.173	1.139	1.737	1.233	1.599	1.638		6
7	0.618	1.638	1.281	1.501	1.549	1.223	1.427	1.464	1.405	1.216	1.528	1.505	1.270	1.585	0.601	7
8	0.612	1.384	1.776	1.230	1.224	1.814	1.467	1.189	1.469	1.831	1.228	1.226	1.764	1.356	0.596	8
9	0.594	1.599	1.286	1.500	1.529	1.226	1.443	1.462	1.419	1.234	1.544	1.499	1.280	1.580	0.595	9
10		1.661	1.580	1.229	1.765	1.149	1.186	1.808	1.188	1.160	1.781	1.246	1.609	1.649		10
11		1.472	1.762	1.599	1.277	1.749	1.519	1.222	1.556	1.790	1.282	1.622	1.788	1.462		11
12			0.952	1.433	1.672	1.241	1.505	1.229	1.508	1.248	1.617	1.411	0.959			12
13				1.018	1.794	1.610	1.287	1.732	1.266	1.582	1.766	1.020				13
14					1.500	1.689	1.581	1.348	1.604	1.634	1.474					14
15							0.608	0.603	0.611							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

PEAK ROD ENTHALPY RISE C12 MAP554 07/05/88 D-228 9126MWD/MTU 99.65%HFP 50P 1 B-262 FCFM

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.377	0.373	0.376							1
2					1.265	1.407	1.382	1.165	1.383	1.408	1.225					2
3				0.852	1.501	1.320	1.081	1.482	1.081	1.314	1.458	0.818				3
4			0.792	1.168	1.309	1.014	1.219	0.998	1.267	1.044	1.319	1.173	0.795			4
5		1.199	1.433	1.302	1.051	1.450	1.264	0.995	1.275	1.462	1.061	1.317	1.479	1.225		5
6		1.394	1.302	1.016	1.481	0.977	0.998	1.521	0.991	0.974	1.452	1.026	1.321	1.387		6
7	0.382	1.393	1.087	1.228	1.284	1.016	1.210	1.241	1.186	1.004	1.267	1.230	1.083	1.356	0.375	7
8	0.375	1.173	1.494	1.006	1.000	1.518	1.247	0.996	1.236	1.522	0.997	0.998	1.490	1.153	0.372	8
9	0.371	1.376	1.074	1.221	1.264	1.012	1.218	1.232	1.189	1.019	1.275	1.218	1.079	1.363	0.372	9
10		1.383	1.292	1.019	1.474	0.983	1.004	1.515	0.996	0.984	1.482	1.032	1.313	1.364		10
11		1.224	1.462	1.326	1.090	1.469	1.267	1.003	1.282	1.480	1.094	1.342	1.468	1.193		11
12			0.802	1.197	1.384	1.040	1.223	1.000	1.218	1.033	1.337	1.167	0.794			12
13				0.831	1.460	1.326	1.086	1.464	1.065	1.290	1.454	0.830				13
14					1.223	1.396	1.358	1.151	1.371	1.389	1.208					14
15							0.372	0.371	0.375							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

CALCULATED LOCAL PEAKING FACTORS C12 MAP554 07/05/88 D-228 9126MWD/MTU 99.65%HFP 5OP 1 B-262 FCFM

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							1.733	1.548	1.733							1
2					1.511	1.303	1.204	1.196	1.204	1.303	1.511					2
3				1.686	1.177	1.102	1.062	1.082	1.062	1.102	1.177	1.686				3
4			1.674	1.223	1.083	1.048	1.068	1.055	1.067	1.048	1.083	1.223	1.674			4
5		1.513	1.179	1.083	1.058	1.096	1.100	1.044	1.100	1.096	1.058	1.083	1.179	1.512		5
6		1.303	1.103	1.049	1.096	1.048	1.057	1.092	1.057	1.048	1.096	1.049	1.103	1.303		6
7	1.733	1.204	1.061	1.067	1.101	1.064	1.066	1.070	1.066	1.064	1.101	1.067	1.061	1.203	1.733	7
8	1.548	1.196	1.082	1.054	1.043	1.092	1.070	1.034	1.070	1.092	1.043	1.054	1.082	1.195	1.548	8
9	1.733	1.204	1.061	1.067	1.101	1.064	1.066	1.070	1.066	1.064	1.101	1.067	1.061	1.204	1.733	9
10		1.303	1.103	1.049	1.096	1.048	1.057	1.092	1.057	1.048	1.096	1.049	1.103	1.303		10
11		1.512	1.179	1.083	1.058	1.096	1.100	1.044	1.100	1.096	1.058	1.083	1.179	1.512		11
12			1.674	1.223	1.083	1.048	1.067	1.055	1.068	1.048	1.083	1.223	1.674			12
13				1.685	1.177	1.102	1.062	1.082	1.062	1.102	1.177	1.685				13
14					1.511	1.303	1.204	1.196	1.204	1.303	1.511					14
15							1.733	1.548	1.732							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

FQT*V(Z)*FQE*FQM 3%TARGET BAND C12 MAP554 07/05/88 D-228 9126MWD/MTU 99.65%HFP 50P 1 B-262 FCFM
FULL CORE SEARCH

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.741	0.731	0.741							1
2					1.780	1.963	1.938	1.628	1.956	1.977	1.726					2
3				1.192	2.125	1.864	1.493	2.061	1.519	1.865	2.049	1.145				3
4			1.120	1.652	1.861	1.412	1.759	1.416	1.838	1.453	1.852	1.642	1.121			4
5		1.729	2.068	1.859	1.446	2.025	1.758	1.408	1.786	2.038	1.443	1.869	2.121	1.769		5
6		1.955	1.847	1.427	2.082	1.331	1.373	2.110	1.369	1.327	2.032	1.436	1.866	1.944		6
7	0.756	1.983	1.517	1.765	1.801	1.441	1.675	1.708	1.637	1.434	1.776	1.770	1.501	1.915	0.730	7
8	0.750	1.667	2.115	1.421	1.419	2.117	1.729	1.392	1.716	2.129	1.423	1.417	2.077	1.618	0.722	8
9	0.719	1.938	1.506	1.763	1.778	1.445	1.681	1.717	1.662	1.454	1.795	1.762	1.499	1.904	0.720	9
10		1.957	1.844	1.432	2.065	1.339	1.384	2.110	1.386	1.352	2.084	1.452	1.878	1.942		10
11		1.727	2.065	1.869	1.486	2.046	1.768	1.420	1.812	2.095	1.491	1.895	2.095	1.715		11
12			1.113	1.670	1.953	1.445	1.772	1.422	1.776	1.454	1.889	1.645	1.117			12
13				1.173	2.099	1.880	1.513	2.053	1.484	1.847	2.066	1.176				13
14					1.757	1.990	1.919	1.626	1.941	1.932	1.727					14
15							0.734	0.737	0.746							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

57	1.0800	1.1100
58	1.0800	1.1100
59	1.0800	1.1100
60	1.0800	1.1100
61	1.0800	1.1100

FQT*V(Z)*FQE*FQM 5%TARGET BAND C12 MAP554 07/05/88 D-228 9126MWD/MTU 99.65%HFP 5OP 1 B-262 FCFM
FULL CORE SEARCH

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.761	0.751	0.761							1
2					1.829	2.017	1.991	1.673	2.010	2.032	1.774					2
3				1.225	2.184	1.915	1.535	2.118	1.561	1.917	2.106	1.177				3
4			1.152	1.698	1.912	1.452	1.808	1.455	1.889	1.494	1.903	1.688	1.152			4
5		1.777	2.125	1.911	1.486	2.082	1.807	1.448	1.835	2.095	1.483	1.920	2.180	1.818		5
6		2.009	1.898	1.467	2.140	1.368	1.412	2.168	1.407	1.364	2.089	1.476	1.918	1.997		6
7	0.776	2.037	1.558	1.814	1.851	1.481	1.721	1.756	1.682	1.474	1.826	1.819	1.542	1.967	0.751	7
8	0.771	1.713	2.173	1.461	1.458	2.175	1.777	1.431	1.763	2.189	1.463	1.456	2.134	1.663	0.742	8
9	0.739	1.992	1.548	1.812	1.827	1.485	1.727	1.764	1.708	1.495	1.845	1.811	1.541	1.957	0.740	9
10		2.011	1.895	1.472	2.123	1.376	1.423	2.168	1.425	1.389	2.142	1.492	1.930	1.996		10
11		1.775	2.122	1.921	1.527	2.103	1.818	1.460	1.862	2.153	1.533	1.948	2.153	1.762		11
12			1.144	1.716	2.007	1.486	1.821	1.462	1.826	1.494	1.942	1.691	1.148			12
13				1.205	2.158	1.932	1.554	2.110	1.525	1.898	2.124	1.209				13
14					1.806	2.045	1.971	1.671	1.995	1.985	1.775					14
15							0.754	0.757	0.767							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FQT*V(Z)*FQE*FQM 3%TARGET BAND C12 MAP554 07/05/88 D-228 9126MWD/MTU 99.65%HFP 5OP 1 B-262 FCFM
SEARCH BETWEEN NODES 6 AND 56

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.741	0.731	0.741							1
2					1.780	1.963	1.938	1.628	1.956	1.977	1.726					2
3				1.192	2.125	1.864	1.493	2.061	1.519	1.865	2.049	1.145				3
4			1.120	1.652	1.861	1.412	1.759	1.416	1.838	1.453	1.852	1.642	1.121			4
5		1.729	2.068	1.859	1.446	2.025	1.758	1.408	1.786	2.038	1.443	1.869	2.121	1.769		5
6		1.955	1.847	1.427	2.082	1.331	1.373	2.110	1.369	1.327	2.032	1.436	1.866	1.944		6
7	0.756	1.983	1.517	1.765	1.801	1.441	1.675	1.708	1.637	1.434	1.776	1.770	1.501	1.915	0.730	7
8	0.750	1.667	2.115	1.421	1.419	2.117	1.729	1.392	1.716	2.129	1.423	1.417	2.077	1.618	0.722	8
9	0.719	1.938	1.506	1.763	1.778	1.445	1.681	1.717	1.662	1.454	1.795	1.762	1.499	1.904	0.720	9
10		1.957	1.844	1.432	2.065	1.339	1.384	2.110	1.386	1.352	2.084	1.452	1.878	1.942		10
11		1.727	2.065	1.869	1.486	2.046	1.768	1.420	1.812	2.095	1.491	1.895	2.095	1.715		11
12			1.113	1.670	1.953	1.445	1.772	1.422	1.776	1.454	1.889	1.645	1.117			12
13				1.173	2.099	1.880	1.513	2.053	1.484	1.847	2.066	1.176				13
14					1.757	1.990	1.919	1.626	1.941	1.932	1.727					14
15							0.734	0.737	0.746							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

MAXIMUM FQT*V(Z)*FQE*FQM C12 MAP554 07/05/88 D-228 9126MWD/MTU 99.65%HFP 5OP 1 B-262 FCFM

AXIAL NODE	3%TARGET	ASSEMBLY#	5%TARGET	ASSEMBLY#
1	.78391	52	.80491	52
2	.92158	118	.94626	118
3	1.0367	118	1.0645	118
4	1.1565	118	1.1874	118
5	1.8019	50	1.8503	50
6	1.8116	50	1.8604	50
7	1.8987	108	1.9500	108
8	2.0167	77	2.0714	77
9	2.0731	77	2.1294	77
10	2.1058	77	2.1633	77
11	2.1169	77	2.1749	77
12	2.1159	77	2.1741	77
13	2.1145	74	2.1729	74
14	2.1026	74	2.1608	74
15	2.0821	74	2.1400	74
16	2.0475	81	2.1043	81
17	1.9643	81	2.0188	81
18	2.0217	50	2.0778	50
19	2.0316	50	2.0880	50
20	2.0262	50	2.0825	50
21	2.0137	50	2.0696	50
22	2.0105	50	2.0664	50
23	1.9990	50	2.0546	50
24	1.9839	50	2.0390	50
25	1.9692	12	2.0239	12
26	1.9593	50	2.0137	50
27	1.9230	81	1.9765	81
28	1.8559	50	1.9075	50
29	1.9222	50	1.9756	50
30	1.9384	50	1.9923	50
31	1.9399	81	1.9938	81
32	1.9461	81	2.0001	81
33	1.9521	81	2.0063	81
34	1.9584	81	2.0127	81
35	1.9568	50	2.0112	50
36	1.9650	12	2.0196	12
37	1.9677	50	2.0224	50
38	1.9592	81	2.0136	81
39	1.9053	50	1.9583	50
40	1.9749	50	2.0297	50
41	2.0079	50	2.0637	50
42	2.0306	50	2.0870	50
43	2.0470	50	2.1039	50
44	2.0806	42	2.1384	42
45	2.0978	42	2.1561	42
46	2.1151	42	2.1738	42
47	2.1212	42	2.1801	42
48	2.1265	81	2.1856	81
49	2.1200	81	2.1789	81
50	2.0538	81	2.1109	81
51	2.1002	81	2.1586	81
52	2.1294	81	2.1886	81
53	2.1091	81	2.1677	81
54	2.0590	81	2.1162	81
55	1.9710	81	2.0257	81
56	1.8506	81	1.9020	81

FQT*V(Z)*FQE*FQM 5%TARGET BAND C12 MAP554 07/05/88 D-228 9126MWD/MTU 99.65%HFP 5OP 1 B-262 FCFM
SEARCH BETWEEN NODES 6 AND 56

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.761.	0.751.	0.761.							1
2					1.829.	2.017.	1.991.	1.673.	2.010.	2.032.	1.774.					2
3				1.225.	2.184.	1.915.	1.535.	2.118.	1.561.	1.917.	2.106.	1.177.				3
4			1.152.	1.698.	1.912.	1.452.	1.808.	1.455.	1.889.	1.494.	1.903.	1.688.	1.152.			4
5		1.777.	2.125.	1.911.	1.486.	2.082.	1.807.	1.448.	1.835.	2.095.	1.483.	1.920.	2.180.	1.818.		5
6		2.009.	1.898.	1.467.	2.140.	1.368.	1.412.	2.168.	1.407.	1.364.	2.089.	1.476.	1.918.	1.997.		6
7	0.776.	2.037.	1.558.	1.814.	1.851.	1.481.	1.721.	1.756.	1.682.	1.474.	1.826.	1.819.	1.542.	1.967.	0.751.	7
8	0.771.	1.713.	2.173.	1.461.	1.458.	2.175.	1.777.	1.431.	1.763.	2.189.	1.463.	1.456.	2.134.	1.663.	0.742.	8
9	0.739.	1.992.	1.548.	1.812.	1.827.	1.485.	1.727.	1.764.	1.708.	1.495.	1.845.	1.811.	1.541.	1.957.	0.740.	9
10		2.011.	1.895.	1.472.	2.123.	1.376.	1.423.	2.168.	1.425.	1.389.	2.142.	1.492.	1.930.	1.996.		10
11		1.775.	2.122.	1.921.	1.527.	2.103.	1.818.	1.460.	1.862.	2.153.	1.533.	1.948.	2.153.	1.762.		11
12			1.144.	1.716.	2.007.	1.486.	1.821.	1.462.	1.826.	1.494.	1.942.	1.691.	1.148.			12
13				1.205.	2.158.	1.932.	1.554.	2.110.	1.525.	1.898.	2.124.	1.209.				13
14					1.806.	2.045.	1.971.	1.671.	1.995.	1.985.	1.775.					14
15							0.754.	0.757.	0.767.							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

1	57	1.7238	123	1.7717	123
2	58	1.5834	47	1.6273	47
3	59	.79471	124	.81678	124
4	60	.59772	124	.61433	124
5	61	.49502	118	.50877	118
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PDQ ACTIVATIONS FOR EACH THIMBLE

THIMBLE		(X-ORD, Y-ORD)	REGION 1	REGION 2	REGION 3	REGION 4	REGION 5	REGION 6	REGION 7	REGION 8
1	M 3	(-60., 75.)	0.196E+17	0.886E+16	0.919E+16	0.209E+17	0.0	0.0	0.0	0.0
2	J15	(-15., -105.)	0.146E+17	0.857E+16	0.441E+16	0.468E+16	0.0	0.0	0.0	0.0
3	F 4	(30., 60.)	0.413E+17	0.176E+17	0.181E+17	0.427E+17	0.0	0.0	0.0	0.0
4	L 8	(-45., 0.)	0.393E+17	0.164E+17	0.172E+17	0.412E+17	0.0	0.0	0.0	0.0
5	F 8	(30., 0.)	0.534E+17	0.171E+17	0.175E+17	0.544E+17	0.0	0.0	0.0	0.0
6	D12	(60., -60.)	0.367E+17	0.139E+17	0.144E+17	0.383E+17	0.0	0.0	0.0	0.0
7	B 5	(90., 45.)	0.283E+17	0.109E+17	0.111E+17	0.299E+17	0.0	0.0	0.0	0.0
8	H 6	(0., 30.)	0.532E+17	0.171E+17	0.173E+17	0.536E+17	0.0	0.0	0.0	0.0
9	J 3	(-15., 75.)	0.413E+17	0.181E+17	0.183E+17	0.423E+17	0.0	0.0	0.0	0.0
10	D 3	(60., 75.)	0.196E+17	0.886E+16	0.919E+16	0.209E+17	0.0	0.0	0.0	0.0
11	L 9	(-45., -15.)	0.463E+17	0.164E+17	0.170E+17	0.477E+17	0.0	0.0	0.0	0.0
12	B10	(90., -30.)	0.388E+17	0.145E+17	0.143E+17	0.392E+17	0.0	0.0	0.0	0.0
13	L 4	(-45., 60.)	0.479E+17	0.169E+17	0.174E+17	0.502E+17	0.0	0.0	0.0	0.0
14	F13	(30., -75.)	0.460E+17	0.176E+17	0.181E+17	0.483E+17	0.0	0.0	0.0	0.0
15	F 6	(30., 30.)	0.337E+17	0.170E+17	0.174E+17	0.343E+17	0.0	0.0	0.0	0.0
16	J12	(-15., -60.)	0.460E+17	0.164E+17	0.172E+17	0.487E+17	0.0	0.0	0.0	0.0
17	B 7	(90., 15.)	0.425E+17	0.153E+17	0.139E+17	0.381E+17	0.0	0.0	0.0	0.0
18	H 1	(0., 105.)	0.162E+17	0.924E+16	0.400E+16	0.435E+16	0.0	0.0	0.0	0.0
19	G 9	(15., -15.)	0.438E+17	0.162E+17	0.165E+17	0.442E+17	0.0	0.0	0.0	0.0
20	G 7	(15., 15.)	0.438E+17	0.162E+17	0.165E+17	0.442E+17	0.0	0.0	0.0	0.0
21	F11	(30., -45.)	0.562E+17	0.164E+17	0.167E+17	0.571E+17	0.0	0.0	0.0	0.0
22	N 5	(-75., 45.)	0.464E+17	0.166E+17	0.170E+17	0.489E+17	0.0	0.0	0.0	0.0
23	J10	(-15., -30.)	0.401E+17	0.164E+17	0.166E+17	0.404E+17	0.0	0.0	0.0	0.0
24	J 5	(-15., 45.)	0.462E+17	0.163E+17	0.169E+17	0.472E+17	0.0	0.0	0.0	0.0
25	B 8	(90., 0.)	0.369E+17	0.152E+17	0.132E+17	0.314E+17	0.0	0.0	0.0	0.0
26	N10	(-75., -30.)	0.458E+17	0.176E+17	0.180E+17	0.481E+17	0.0	0.0	0.0	0.0
27	C12	(75., -60.)	0.190E+17	0.878E+16	0.901E+16	0.198E+17	0.0	0.0	0.0	0.0
28	J 7	(-15., 15.)	0.438E+17	0.162E+17	0.165E+17	0.442E+17	0.0	0.0	0.0	0.0
29	D 7	(60., 15.)	0.459E+17	0.164E+17	0.171E+17	0.484E+17	0.0	0.0	0.0	0.0
30	L14	(-45., -90.)	0.284E+17	0.109E+17	0.112E+17	0.302E+17	0.0	0.0	0.0	0.0
31	F 2	(30., 90.)	0.389E+17	0.145E+17	0.144E+17	0.395E+17	0.0	0.0	0.0	0.0
32	F 9	(30., -15.)	0.406E+17	0.164E+17	0.169E+17	0.419E+17	0.0	0.0	0.0	0.0
33	N 7	(-75., 15.)	0.411E+17	0.181E+17	0.182E+17	0.418E+17	0.0	0.0	0.0	0.0
34	A 9	(105., -15.)	0.146E+17	0.856E+16	0.437E+16	0.463E+16	0.0	0.0	0.0	0.0
35	N12	(-75., -60.)	0.190E+17	0.878E+16	0.901E+16	0.198E+17	0.0	0.0	0.0	0.0
36	R 8	(-105., 0.)	0.162E+17	0.924E+16	0.396E+16	0.430E+16	0.0	0.0	0.0	0.0
37	H 4	(0., 60.)	0.398E+17	0.168E+17	0.176E+17	0.421E+17	0.0	0.0	0.0	0.0
38	H11	(0., -45.)	0.392E+17	0.164E+17	0.171E+17	0.409E+17	0.0	0.0	0.0	0.0
39	D 5	(60., 45.)	0.478E+17	0.169E+17	0.174E+17	0.501E+17	0.0	0.0	0.0	0.0
40	L 6	(-45., 30.)	0.563E+17	0.164E+17	0.168E+17	0.573E+17	0.0	0.0	0.0	0.0
41	D10	(60., -30.)	0.412E+17	0.176E+17	0.181E+17	0.427E+17	0.0	0.0	0.0	0.0
42	G14	(15., -90.)	0.426E+17	0.153E+17	0.140E+17	0.385E+17	0.0	0.0	0.0	0.0
43	H13	(0., -75.)	0.535E+17	0.180E+17	0.181E+17	0.539E+17	0.0	0.0	0.0	0.0
44	C 8	(75., 0.)	0.534E+17	0.180E+17	0.179E+17	0.533E+17	0.0	0.0	0.0	0.0
45	H 3	(0., 75.)	0.535E+17	0.180E+17	0.181E+17	0.539E+17	0.0	0.0	0.0	0.0
46	N 8	(-75., 0.)	0.534E+17	0.180E+17	0.179E+17	0.533E+17	0.0	0.0	0.0	0.0
47	E11	(45., -45.)	0.339E+17	0.185E+17	0.188E+17	0.352E+17	0.0	0.0	0.0	0.0
48	L11	(-45., -45.)	0.339E+17	0.185E+17	0.188E+17	0.352E+17	0.0	0.0	0.0	0.0
49	E 5	(45., 45.)	0.339E+17	0.185E+17	0.188E+17	0.352E+17	0.0	0.0	0.0	0.0
50	L 5	(-45., 45.)	0.339E+17	0.185E+17	0.188E+17	0.352E+17	0.0	0.0	0.0	0.0

C12 MAP560 09/12/88 D-215 10437MWD/MTU 99.79%HFP 5OP 1 B-149 FCFM

RECEIVED BY.....
RECEIVED DATE.....

VERSION PNR16022
RUN DATE 08/15/88

SUMMARY OF INCORE RESULTS

	MEASURED			MEASURED /W UNCERTAINTY FACTOR	TECH. SPEC. LIMIT
F-DELTA-H (MAX. ASSEMBLY) =	1.408	LOC K 8	REGION 15		
F-DELTA-H (MAX. ASSEMBLY) =	1.256	LOC L12	REGION 14		
F-DELTA-H (MAX. ASSEMBLY) =	1.062	LOC E11	REGION 12R		
F-DELTA-H (MAX. ASSEMBLY) =	1.022	LOC G 3	REGION 13A		
F-DELTA-H (MAX. ASSEMBLY) =	0.246	LOC A 8	REGION 13		
F-DELTA-H (PEAK PIN) =	1.534	LOC K 8	REGION 15	1.595	1.651
F-DELTA-H (PEAK PIN) =	1.351	LOC L12	REGION 14	1.405	1.651
F-DELTA-H (PEAK PIN) =	1.129	LOC E11	REGION 12R	1.175	1.651
F-DELTA-H (PEAK PIN) =	1.085	LOC G 3	REGION 13A	1.128	1.651
F-DELTA-H (PEAK PIN) =	0.380	LOC R 7	REGION 13	0.395	1.651
FQT/K(Z) =		LOC F11	REGION 15	1.983	2.325
FQT/K(Z) =		LOC L12	REGION 14	1.764	2.325
FQT/K(Z) =		LOC E11	REGION 12R	1.433	2.325
FQT/K(Z) =		LOC G 3	REGION 13A	1.396	2.325
FQT/K(Z) =		LOC R 7	REGION 13	0.693	2.325
FQN (WITH LOCAL PEAKING) =	1.835	LOC K 8	REGION 15		
FQN (WITH LOCAL PEAKING) =	1.629	LOC L12	REGION 14		
FQN (WITH LOCAL PEAKING) =	1.331	LOC E11	REGION 12R		
FQN (WITH LOCAL PEAKING) =	1.287	LOC G 3	REGION 13A		
FQN (WITH LOCAL PEAKING) =	0.614	LOC R 7	REGION 13		

CALCULATED POWER TILTS(NORMALIZED TO 1.000)

(-,+) QUADRANT =	1.000	1.02
(+,+) QUADRANT =	0.998	1.02
(-,-) QUADRANT =	0.999	1.02
(+,-) QUADRANT =	1.002	1.02

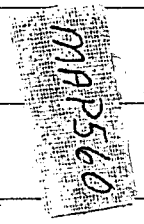
REGION 15 AVERAGE POWER FRACTION	1.159	REGION 15 STD % DIF		2.466
REGION 14 AVERAGE POWER FRACTION	1.135	REGION 14 STD % DIF		1.679
REGION 12R AVERAGE POWER FRACTION	0.995	REGION 12R STD % DIF		3.593
REGION 13A AVERAGE POWER FRACTION	0.882	REGION 13A STD % DIF		1.707
REGION 13 AVERAGE POWER FRACTION	0.228	REGION 13 STD % DIF		2.752

AXIAL OFFSET = -2.933
FXY (NEGLECTING GRIDS) = 1.567 LOC L 6 NODE 44

MAX FQT*V(Z)/K(Z) FOR 3% BANDS = 2.142
MAX FQT*V(Z)/K(Z) FOR 5% BANDS = 2.202

243

FQZ BASED APL FOR 3% BANDS = 108.31%
FQZ BASED APL FOR 5% BANDS = 105.38%



FORM 0113 (02/83)

C12 MAP560 09/12/88 D-215 10437MWD/MTU 99.79%HFP 5OP 1 B-149 FCFM

FINAL COMPARISON OF SATURATION ACTIVITY AND PDQ ACTIVATION

DRIVE	THIMBLE		STATUS	MEASURED AXIAL FACTOR	REGION % DIFF 1- 4	4-43	43-58	58-61	FZ/KZ
5	1	M 3	GOOD	1.1491	13.4829	2.4055	-2.5541	-3.8184	1.1534
0	2	J15	NONE						
5	3	F 4	GOOD	1.1632	-14.7179	0.4062	1.7578	17.3082	1.1632
5	4	L 8	GOOD	1.1694	9.6592	2.7444	2.5291	8.6717	1.1694
5	5	F 8	GOOD	1.1498	-5.3506	0.3821	2.6978	6.2606	1.1498
5	6	D12	GOOD	1.1553	7.5480	-1.4555	-3.2952	-8.5899	1.1553
5	7	B 5	GOOD	1.1697	-7.5870	-1.3311	-3.0758	-10.6729	1.1697
5	8	H 6	GOOD	1.1340	0.9983	1.0036	2.1772	-4.8689	1.1531
5	9	J 3	GOOD	1.1415	0.3117	-1.5698	-1.8519	3.3340	1.1415
2	10	D 3	GOOD	1.1406	0.9653	-1.8987	-6.7424	-1.0537	1.1553
2	11	L 9	GOOD	1.1626	2.8039	0.8047	3.1527	6.1316	1.1626
2	12	B10	GOOD	1.1461	-22.6453	-2.9820	-4.5537	-15.1761	1.1461
2	13	L 4	GOOD	1.1503	0.6450	-0.2279	1.0344	0.1264	1.1503
2	14	F13	GOOD	1.1672	-2.6463	-2.7450	-1.7049	-2.4963	1.1672
2	15	F 6	GOOD	1.1658	15.9950	2.0917	2.5211	0.3311	1.1658
2	16	J12	GOOD	1.1617	-6.6400	1.3204	0.4686	-5.4534	1.1617
2	17	B 7	GOOD	1.1100	-7.0972	-2.4178	-2.1636	1.3101	1.1562
0	18	H 1	NONE						
3	19	G 9	GOOD	1.1399	7.7576	-1.6135	-1.4620	-4.1645	1.1399
2	20	G 7	GOOD	1.1305	-0.0589	-1.9875	-2.0549	-1.4970	1.1305
3	21	F11	GOOD	1.1431	-5.2095	2.7385	6.9146	9.7887	1.1431
3	22	N 5	GOOD	1.1643	-3.4002	-3.6753	-3.1699	-12.4355	1.1643
3	23	J10	GOOD	1.1407	5.1742	1.7213	2.4542	10.4571	1.1407
3	24	J 5	GOOD	1.1404	3.3397	0.8968	2.1941	8.0803	1.1404
3	25	B 8	GOOD	1.1441	9.4215	-0.9281	-3.8710	-9.1118	1.1878
3	26	N10	GOOD	1.1546	7.1053	-2.7919	-3.6358	-12.4525	1.1546
0	27	C12	NONE						
4	28	J 7	GOOD	1.1275	8.4944	0.4076	-1.3247	-5.5104	1.1275
4	29	D 7	GOOD	1.1486	5.9793	0.7052	-0.8719	-7.7877	1.1486
4	30	L14	GOOD	1.1533	-10.6764	-3.2157	-4.5682	-5.3479	1.1533
4	31	F 2	GOOD	1.1246	-10.5698	-2.1899	-2.5680	-5.8812	1.1398
4	32	F 9	GOOD	1.1528	14.7031	1.6499	0.4874	-0.3833	1.1528
4	33	N 7	GOOD	1.1289	5.5288	-1.4713	-3.8199	-1.9738	1.1571
0	34	A 9	NONE						
5	35	N12	GOOD	1.1366	11.5169	0.4021	-5.2281	-4.4539	1.1522
0	36	R 8	NONE						
0	37	H 4	NONE						
5	38	H11	GOOD	1.1579	13.9814	2.9313	2.3468	3.2382	1.1579
5	39	D 5	GOOD	1.1588	-13.2055	-0.0650	-0.3368	-8.5915	1.1588
5	40	L 6	GOOD	1.1383	-5.7830	2.6474	6.4281	7.8850	1.1383
5	41	D10	GOOD	1.1567	1.7415	0.2298	1.0578	12.3190	1.1567
5	42	G14	GOOD	1.1279	-34.0281	-1.1871	-1.7469	1.1522	1.1769
3	43	H13	GOOD	1.1203	-3.9941	-4.2178	-4.4884	-9.2017	1.1332
2	44	C 8	GOOD	1.1277	-9.3985	-1.4458	0.4836	3.6747	1.1277
0	45	H 3	NONE						
4	46	N 8	GOOD	1.1271	-5.2095	-2.7463	-3.2703	-10.4223	1.1450
2	47	E11	GOOD	1.1758	14.2807	7.5597	9.7535	27.2119	1.1758
4	48	L11	GOOD	1.1635	20.8530	3.4921	3.0324	8.2055	1.1635
5	49	E 5	GOOD	1.1590	17.1127	1.9343	2.1553	12.8484	1.1590
0	50	L 5	NONE						
AVG. OF ABSOLUTE VALUES OF GOOD THIMBLES ONLY				1.1471	8.75	1.92	2.90	7.14	

FORM 0113 (02/83)

99

SYMMETRIC THIMBLE COMPARISON C12 MAP560 09/12/88 D-215 10437MWD/MTU 99.79%HFP 5OP 1 B-149 FCFM

THMBL	LOC	INTEGRAL	THMBL	LOC	INTEGRAL	RATIO
1	M 3	0.32798E+02	10	D 3	0.31407E+02	1.0443
10	D 3	0.31407E+02	1	M 3	0.32798E+02	.95760
19	G 9	0.60349E+02	20	G 7	0.60000E+02	1.0058
19	G 9	0.60349E+02	28	J 7	0.61186E+02	.98632
20	G 7	0.60000E+02	19	G 9	0.60349E+02	.99421
20	G 7	0.60000E+02	28	J 7	0.61186E+02	.98062
28	J 7	0.61186E+02	19	G 9	0.60349E+02	1.0139
28	J 7	0.61186E+02	20	G 7	0.60000E+02	1.0198
44	C 8	0.64967E+02	46	N 8	0.63518E+02	1.0228
46	N 8	0.63518E+02	44	C 8	0.64967E+02	.97769
47	E11	0.73489E+02	48	L11	0.70172E+02	1.0473
47	E11	0.73489E+02	49	E 5	0.69311E+02	1.0603
48	L11	0.70172E+02	47	E11	0.73489E+02	.95487
48	L11	0.70172E+02	49	E 5	0.69311E+02	1.0124
49	E 5	0.69311E+02	47	E11	0.73489E+02	.94315
49	E 5	0.69311E+02	48	L11	0.70172E+02	.98773

177

MAX FQT/K(Z) C12 MAP560 09/12/88 D-215 10437MWD/MTU 99.79%HFP 5OP 1 B-149 FCFM

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.683.	0.678.	0.681.							1
2					1.617.	1.767.	1.737.	1.484.	1.741.	1.755.	1.548.					2
3				1.104.	1.929.	1.708.	1.387.	1.888.	1.396.	1.707.	1.865.	1.053.				3
4			1.036.	1.523.	1.711.	1.330.	1.623.	1.313.	1.648.	1.349.	1.700.	1.506.	1.034.			4
5		1.567.	1.879.	1.705.	1.370.	1.903.	1.640.	1.312.	1.651.	1.903.	1.358.	1.708.	1.922.	1.603.		5
6		1.750.	1.665.	1.337.	1.969.	1.262.	1.280.	1.948.	1.282.	1.266.	1.907.	1.337.	1.686.	1.746.		6
7	0.693.	1.752.	1.366.	1.620.	1.697.	1.354.	1.529.	1.572.	1.520.	1.346.	1.652.	1.617.	1.375.	1.725.	0.681.	7
8	0.680.	1.481.	1.877.	1.309.	1.343.	1.975.	1.575.	1.290.	1.581.	1.973.	1.315.	1.306.	1.888.	1.475.	0.677.	8
9	0.664.	1.722.	1.369.	1.624.	1.676.	1.370.	1.571.	1.579.	1.528.	1.342.	1.647.	1.625.	1.373.	1.720.	0.673.	9
10		1.766.	1.669.	1.335.	1.933.	1.269.	1.302.	1.954.	1.296.	1.283.	1.963.	1.351.	1.685.	1.753.		10
11		1.561.	1.866.	1.693.	1.381.	1.908.	1.654.	1.325.	1.683.	1.983.	1.433.	1.737.	1.886.	1.552.		11
12			1.027.	1.522.	1.764.	1.357.	1.640.	1.314.	1.638.	1.383.	1.754.	1.519.	1.035.			12
13				1.071.	1.864.	1.694.	1.388.	1.848.	1.370.	1.706.	1.898.	1.091.				13
14					1.560.	1.753.	1.704.	1.466.	1.744.	1.760.	1.602.					14
15							0.674.	0.685.	0.689.							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

ASSEMBLY RELATIVE POWER C12 MAP560 09/12/88 D-215 10437MWD/MTU 99.79%HFP 50P 1 B-149 FCFM

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.220	0.245	0.218							1
2					0.832	1.063	1.133	0.968	1.123	1.053	0.800					2
3				0.512	1.272	1.188	1.014	1.366	1.022	1.189	1.240	0.491				3
4			0.481	0.962	1.216	0.976	1.141	0.950	1.153	0.986	1.216	0.958	0.480			4
5		0.791	1.213	1.204	1.015	1.357	1.155	0.953	1.155	1.358	1.016	1.209	1.243	0.804		5
6		1.048	1.161	0.975	1.387	0.955	0.952	1.394	0.949	0.955	1.355	0.980	1.181	1.053		6
7	0.221	1.121	1.005	1.144	1.180	0.968	1.132	1.157	1.119	0.955	1.154	1.145	1.013	1.120	0.220	7
8	0.242	0.956	1.346	0.950	0.970	1.408	1.159	0.967	1.155	1.394	0.953	0.947	1.369	0.960	0.246	8
9	0.218	1.115	0.996	1.141	1.163	0.971	1.155	1.159	1.122	0.961	1.155	1.144	1.011	1.120	0.220	9
10		1.046	1.159	0.976	1.372	0.959	0.964	1.402	0.956	0.965	1.388	0.989	1.176	1.038		10
11		0.803	1.231	1.214	1.034	1.366	1.161	0.966	1.178	1.395	1.062	1.239	1.236	0.789		11
12			0.484	0.972	1.256	0.995	1.150	0.949	1.143	1.002	1.240	0.957	0.480			12
13				0.495	1.218	1.182	1.013	1.337	0.999	1.170	1.236	0.497				13
14					0.793	1.041	1.101	0.952	1.125	1.056	0.803					14
15							0.216	0.244	0.220							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

ASM'Y RELATIVE POWER: PRED/MEAS/DIFF C12 MAP560 09/12/88 D-215 10437MWD/MTU 99.79%HFP 5OP 1 B-149 FCFM

					0.225	0.250	0.225							
					0.220	0.245	0.218							
					-2.16	-2.14	-3.01							
				0.820	1.076	1.147	0.980	1.147	1.076	0.820				
				0.832	1.063	1.133	0.968	1.123	1.053	0.800				
				1.49	-1.24	-1.22	-1.26	-2.09	-2.11	-2.36				
			0.506	1.259	1.195	1.028	1.383	1.028	1.195	1.259	0.506			
			0.512	1.272	1.188	1.014	1.366	1.022	1.189	1.240	0.491			
			1.26	1.02	-0.59	-1.35	-1.27	-0.59	-0.52	-1.48	-2.92			
		0.488	0.962	1.209	0.974	1.139	0.949	1.139	0.974	1.209	0.962	0.488		
		0.481	0.962	1.216	0.976	1.141	0.950	1.153	0.986	1.216	0.958	0.480		
		-1.47	-0.08	0.59	0.26	0.20	0.15	1.18	1.24	0.57	-0.48	-1.59		
	0.816	1.253	1.206	0.996	1.330	1.136	0.939	1.136	1.330	0.996	1.206	1.253	0.816	
	0.791	1.213	1.204	1.015	1.357	1.155	0.953	1.155	1.358	1.016	1.209	1.243	0.804	
	-3.13	-3.18	-0.15	1.84	2.03	1.68	1.57	1.75	2.13	1.94	0.31	-0.77	-1.52	
	1.074	1.192	0.972	1.333	0.937	0.942	1.377	0.942	0.937	1.333	0.972	1.192	1.074	
	1.048	1.161	0.975	1.387	0.955	0.952	1.394	0.949	0.955	1.355	0.980	1.181	1.053	
	-2.45	-2.55	0.22	4.04	1.86	1.05	1.22	0.71	1.93	1.68	0.72	-0.93	-1.98	
0.225	1.145	1.025	1.140	1.139	0.949	1.129	1.157	1.129	0.949	1.139	1.140	1.025	1.145	0.225
0.221	1.121	1.005	1.144	1.180	0.968	1.132	1.157	1.119	0.955	1.154	1.145	1.013	1.120	0.220
-1.95	-2.08	-2.01	0.34	3.61	2.04	0.28	-0.04	-0.88	0.67	1.34	0.41	-1.16	-2.19	-2.29
0.250	0.979	1.381	0.949	0.942	1.380	1.157	0.977	1.157	1.380	0.942	0.949	1.381	0.979	0.250
0.242	0.956	1.346	0.950	0.970	1.408	1.159	0.967	1.155	1.394	0.953	0.947	1.369	0.960	0.246
-3.50	-2.32	-2.59	0.07	2.99	2.02	0.15	-1.01	-0.17	1.00	1.18	-0.15	-0.87	-1.86	-1.87
0.225	1.145	1.025	1.140	1.139	0.949	1.129	1.157	1.129	0.949	1.139	1.140	1.025	1.145	0.225
0.218	1.115	0.996	1.141	1.163	0.971	1.155	1.159	1.122	0.961	1.155	1.144	1.011	1.120	0.220
-3.33	-2.65	-2.83	0.13	2.09	2.34	2.31	0.13	-0.66	1.24	1.40	0.32	-1.35	-2.18	-2.59
	1.074	1.192	0.972	1.333	0.937	0.942	1.377	0.942	0.937	1.333	0.972	1.192	1.074	
	1.046	1.159	0.976	1.372	0.959	0.964	1.402	0.956	0.965	1.388	0.989	1.176	1.038	
	-2.67	-2.76	0.37	2.91	2.38	2.36	1.83	1.52	2.97	4.16	1.71	-1.32	-3.43	
	0.816	1.253	1.206	0.996	1.330	1.136	0.939	1.136	1.330	0.996	1.206	1.253	0.816	
	0.803	1.231	1.214	1.034	1.366	1.161	0.966	1.178	1.395	1.062	1.239	1.236	0.789	
	-1.70	-1.74	0.67	3.75	2.72	2.25	2.92	3.72	4.92	6.57	2.73	-1.35	-3.40	
		0.488	0.962	1.209	0.974	1.139	0.949	1.139	0.974	1.209	0.962	0.488		
		0.484	0.972	1.256	0.995	1.150	0.949	1.143	1.002	1.240	0.957	0.480		
		-0.86	1.02	3.89	2.21	0.93	0.04	0.30	2.89	2.61	-0.59	-1.67		
			0.506	1.259	1.195	1.028	1.383	1.028	1.195	1.259	0.506			
			0.495	1.218	1.182	1.013	1.337	0.999	1.170	1.236	0.497			
			-2.16	-3.30	-1.06	-1.49	-3.36	-2.77	-2.09	-1.86	-1.67			
				0.820	1.076	1.147	0.980	1.147	1.076	0.820				
				0.793	1.041	1.101	0.952	1.125	1.056	0.803				
				-3.25	-3.26	-4.01	-2.90	-1.91	-1.85	-2.00				
					0.225	0.250	0.225							
					0.216	0.244	0.220							

180

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FORM 0113 (02/83)

181

A QUARTER CORE AVERAGED ASSEMBLY RELATIVE POWER C12 MAP560 09/12/88 D-215 10437MWD/MTU 99.79%HFP 5OP 1 B-149 FCFM

	H	G	F	E	D	C	B	A	
	0.977	1.157	1.380	0.942	0.949	1.381	0.979	0.250	
1	0.967	1.157	1.401	0.962	0.949	1.357	0.958	0.244	1
	-1.015	-0.010	1.509	2.082	-0.040	-1.729	-2.090	-2.687	
	1.157	1.129	0.949	1.139	1.140	1.025	1.145	0.225	
2	1.158	1.132	0.964	1.163	1.143	1.006	1.119	0.220	2
	0.047	0.265	1.570	2.110	0.299	-1.839	-2.272	-2.542	
	1.377	0.942	0.937	1.333	0.972	1.192	1.074		
3	1.398	0.955	0.959	1.376	0.980	1.169	1.046		3
	1.522	1.410	2.285	3.196	0.756	-1.890	-2.631		
	0.939	1.136	1.330	0.996	1.206	1.253	0.816		
4	0.960	1.162	1.369	1.031	1.216	1.231	0.797		4
	2.246	2.352	2.948	3.526	0.892	-1.761	-2.435		
	0.949	1.139	0.974	1.209	0.962	0.488			
5	0.950	1.147	0.990	1.232	0.962	0.481			5
	0.094	0.652	1.650	1.915	-0.029	-1.400			
	1.383	1.028	1.195	1.259	0.506				
6	1.351	1.012	1.182	1.241	0.499				6
	-2.316	-1.552	-1.064	-1.408	-1.373				
	0.980	1.147	1.076	0.820					
7	0.960	1.120	1.053	0.807					7
	-2.080	-2.309	-2.116	-1.529					
	0.250	0.225							
8	0.245	0.219							8
	-2.266	-2.898							
	H	G	F	E	D	C	B	A	

PRED	
MES	
DIF	

FORM 0113 (02/83)

FORM 0113 (02/83)

183

FQN C12 MAP560 09/12/88 D-215 10437MWD/MTU 99.79%HFP 50P 1 B-149 FCFM

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.608	0.605	0.607							1
2					1.482	1.619	1.565	1.335	1.562	1.608	1.426					2
3				1.034	1.783	1.580	1.278	1.746	1.287	1.579	1.724	0.979				3
4			0.961	1.412	1.580	1.235	1.490	1.225	1.513	1.252	1.570	1.397	0.959			4
5		1.443	1.734	1.576	1.273	1.757	1.520	1.224	1.529	1.757	1.262	1.579	1.774	1.477		5
6		1.603	1.540	1.239	1.818	1.169	1.184	1.808	1.186	1.172	1.760	1.239	1.559	1.599		6
7	0.614	1.570	1.252	1.488	1.575	1.241	1.418	1.455	1.409	1.234	1.533	1.485	1.267	1.554	0.607	7
8	0.603	1.336	1.721	1.222	1.253	1.835	1.456	1.191	1.462	1.833	1.227	1.219	1.746	1.337	0.604	8
9	0.598	1.539	1.262	1.492	1.556	1.256	1.456	1.462	1.416	1.231	1.529	1.493	1.266	1.551	0.604	9
10		1.618	1.544	1.238	1.784	1.175	1.204	1.813	1.200	1.189	1.812	1.253	1.558	1.605		10
11		1.438	1.723	1.565	1.284	1.762	1.532	1.236	1.559	1.831	1.331	1.606	1.740	1.429		11
12			0.946	1.411	1.629	1.260	1.505	1.226	1.503	1.284	1.620	1.408	0.960			12
13				1.003	1.722	1.567	1.279	1.709	1.263	1.578	1.753	1.022				13
14					1.437	1.606	1.527	1.322	1.567	1.612	1.476					14
15							0.602	0.609	0.613							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

CALCULATED LOCAL PEAKING FACTORS C12 MAP560 09/12/88 D-215 10437MWD/MTU 99.79%HFP 50P 1 B-149 FCFM

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							1.720.	1.538.	1.720.							1
2					1.497.	1.293.	1.196.	1.191.	1.196.	1.292.	1.497.					2
3				1.672.	1.165.	1.094.	1.062.	1.078.	1.062.	1.094.	1.165.	1.672.				3
4			1.660.	1.219.	1.075.	1.054.	1.060.	1.049.	1.060.	1.054.	1.075.	1.219.	1.660.			4
5		1.498.	1.167.	1.075.	1.064.	1.086.	1.097.	1.046.	1.097.	1.086.	1.064.	1.075.	1.167.	1.498.		5
6		1.293.	1.095.	1.055.	1.087.	1.047.	1.056.	1.088.	1.056.	1.047.	1.087.	1.055.	1.095.	1.293.		6
7	1.720.	1.196.	1.062.	1.059.	1.097.	1.060.	1.062.	1.067.	1.062.	1.060.	1.097.	1.059.	1.062.	1.196.	1.720.	7
8	1.538.	1.191.	1.078.	1.048.	1.046.	1.089.	1.068.	1.033.	1.068.	1.089.	1.046.	1.048.	1.078.	1.190.	1.538.	8
9	1.720.	1.196.	1.062.	1.059.	1.097.	1.060.	1.062.	1.067.	1.062.	1.060.	1.097.	1.059.	1.062.	1.196.	1.719.	9
10		1.293.	1.095.	1.055.	1.087.	1.047.	1.056.	1.088.	1.056.	1.047.	1.087.	1.056.	1.095.	1.293.		10
11		1.498.	1.167.	1.075.	1.064.	1.086.	1.097.	1.046.	1.097.	1.086.	1.064.	1.075.	1.167.	1.498.		11
12			1.660.	1.219.	1.075.	1.054.	1.060.	1.049.	1.060.	1.054.	1.075.	1.219.	1.660.			12
13				1.672.	1.165.	1.094.	1.062.	1.078.	1.062.	1.094.	1.165.	1.672.				13
14					1.497.	1.292.	1.196.	1.191.	1.196.	1.292.	1.497.					14
15							1.720.	1.537.	1.719.							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

185

NUCLEAR F-DELTA-H (FDHN) C12 MAP560 09/12/88 D-215 10437MWD/MTU 99.79%HFP 50P 1 B-149 FCFM

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.379	0.377	0.375							1
2					1.245	1.374	1.355	1.153	1.343	1.361	1.198					2
3				0.857	1.481	1.300	1.077	1.472	1.085	1.301	1.445	0.821				3
4			0.798	1.172	1.308	1.029	1.210	0.997	1.222	1.039	1.307	1.168	0.797			4
5		1.185	1.415	1.294	1.079	1.473	1.266	0.997	1.267	1.475	1.080	1.300	1.450	1.205		5
6		1.355	1.272	1.029	1.507	0.999	1.005	1.517	1.002	1.000	1.473	1.034	1.293	1.362		6
7	0.380	1.341	1.067	1.212	1.295	1.027	1.202	1.234	1.189	1.013	1.266	1.212	1.076	1.340	0.379	7
8	0.372	1.138	1.451	0.995	1.014	1.534	1.238	0.999	1.234	1.518	0.997	0.993	1.476	1.143	0.378	8
9	0.375	1.334	1.058	1.209	1.276	1.030	1.227	1.236	1.191	1.019	1.267	1.211	1.074	1.340	0.378	9
10		1.352	1.269	1.030	1.491	1.005	1.018	1.526	1.010	1.010	1.509	1.044	1.288	1.342		10
11		1.203	1.436	1.305	1.100	1.483	1.273	1.010	1.292	1.515	1.129	1.331	1.442	1.182		11
12			0.803	1.185	1.351	1.049	1.219	0.996	1.212	1.056	1.334	1.166	0.797			12
13				0.828	1.418	1.294	1.075	1.441	1.061	1.280	1.439	0.832				13
14					1.187	1.345	1.317	1.133	1.345	1.365	1.203					14
15							0.371	0.376	0.378							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

PERCENT AXIAL OFFSET TOWARD TOP OF ASSEMBLY C12 MAP560 09/12/88 D-215 10437MWD/MTU 99.79%HFP 5OP 1 B-149 FCFM

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							38.9	39.0	38.2							1
2					-2.2	-2.9	-1.2	-0.5	-1.6	-3.3	-3.3					2
3				-3.3	-3.7	-4.5	-3.3	-3.1	-4.2	-5.0	-3.8	-3.1				3
4			-3.7	-3.9	-4.8	-4.4	-4.8	-4.8	-6.0	-5.1	-4.3	-3.7	-3.6			4
5		-4.4	-4.7	-5.2	-4.9	-4.6	-4.4	-5.0	-4.5	-4.1	-3.4	-4.4	-4.3	-3.9		5
6		-2.9	-3.9	-4.7	-5.6	-4.1	-3.3	-3.6	-3.4	-3.1	-3.7	-3.7	-4.0	-3.0		6
7	39.0	-0.5	-2.5	-4.6	-4.9	-4.3	-2.5	-3.0	-3.4	-4.6	-4.1	-4.1	-3.0	-0.9	38.6	7
8	39.1	0.1	-2.7	-4.4	-4.6	-3.6	-2.4	-3.3	-3.3	-4.3	-4.7	-4.7	-3.6	0.8	38.8	8
9	38.6	-1.0	-3.0	-4.8	-4.8	-4.6	-3.5	-3.0	-3.0	-3.7	-4.1	-5.2	-3.3	-0.7	38.5	9
10		-2.8	-3.9	-3.8	-3.9	-3.4	-3.4	-3.1	-3.4	-3.9	-4.4	-4.3	-4.3	-2.9		10
11		-2.6	-2.8	-3.2	-2.6	-3.3	-3.6	-4.0	-4.8	-5.7	-4.3	-4.3	-3.9	-3.7		11
12			-1.8	-2.6	-3.7	-3.6	-4.4	-4.2	-5.4	-5.6	-4.9	-3.5	-3.2			12
13				-3.9	-4.6	-4.4	-3.1	-2.8	-3.7	-5.5	-4.7	-4.0				13
14					-4.4	-3.6	-0.8	-0.3	-1.3	-3.7	-5.3					14
15							37.5	38.2	38.2							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

189

FQT*V(Z)/K(Z) FOR 3% BANDS C12 MAP560 09/12/88 D-215 10437MWD/MTU 99.79%HFP 50P 1 B-149 FCFM
FULL CORE SEARCH

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.744	0.739	0.740							1
2					1.764	1.908	1.893	1.605	1.883	1.896	1.673					2
3				1.192	2.084	1.844	1.497	2.039	1.508	1.843	2.015	1.149				3
4			1.119	1.645	1.847	1.436	1.753	1.418	1.780	1.457	1.836	1.627	1.117			4
5		1.692	2.030	1.841	1.480	2.056	1.772	1.417	1.783	2.055	1.467	1.845	2.076	1.731		5
6		1.890	1.798	1.444	2.127	1.363	1.382	2.104	1.384	1.367	2.059	1.443	1.821	1.891		6
7	0.754	1.908	1.488	1.750	1.833	1.462	1.656	1.697	1.641	1.454	1.784	1.746	1.485	1.873	0.737	7
8	0.742	1.613	2.046	1.414	1.450	2.133	1.707	1.393	1.708	2.130	1.421	1.411	2.051	1.594	0.732	8
9	0.725	1.870	1.478	1.754	1.810	1.480	1.696	1.718	1.659	1.450	1.779	1.755	1.483	1.869	0.732	9
10		1.907	1.803	1.442	2.088	1.370	1.406	2.121	1.400	1.386	2.120	1.459	1.819	1.893		10
11		1.686	2.016	1.828	1.492	2.061	1.786	1.431	1.817	2.142	1.547	1.876	2.037	1.676		11
12			1.121	1.644	1.905	1.466	1.772	1.419	1.769	1.494	1.895	1.640	1.118			12
13				1.157	2.013	1.829	1.499	2.016	1.480	1.842	2.049	1.178				13
14					1.684	1.893	1.858	1.595	1.895	1.901	1.730					14
15							0.732	0.744	0.749							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

FQT*V(Z)/K(Z) FOR 5% BANDS C12 MAP560 09/12/88 D-215 10437MWD/MTU 99.79%HFP 50P 1 B-149 FCFM
FULL CORE SEARCH

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.764	0.759	0.760							1
2					1.812	1.961	1.945	1.649	1.935	1.948	1.719					2
3				1.225	2.142	1.895	1.539	2.096	1.550	1.895	2.070	1.181				3
4			1.150	1.690	1.899	1.476	1.802	1.457	1.830	1.497	1.887	1.672	1.148			4
5		1.739	2.086	1.892	1.521	2.113	1.821	1.456	1.832	2.112	1.508	1.896	2.133	1.780		5
6		1.942	1.848	1.484	2.186	1.401	1.420	2.162	1.423	1.405	2.117	1.484	1.872	1.943		6
7	0.775	1.960	1.529	1.799	1.884	1.502	1.702	1.744	1.687	1.494	1.833	1.795	1.526	1.924	0.758	7
8	0.762	1.658	2.102	1.453	1.490	2.193	1.754	1.432	1.755	2.190	1.460	1.450	2.108	1.638	0.752	8
9	0.745	1.921	1.519	1.803	1.861	1.521	1.743	1.766	1.704	1.490	1.829	1.804	1.524	1.921	0.752	9
10		1.960	1.853	1.482	2.146	1.408	1.445	2.180	1.439	1.424	2.179	1.499	1.870	1.946		10
11		1.733	2.072	1.879	1.533	2.118	1.836	1.470	1.868	2.202	1.590	1.928	2.093	1.723		11
12			1.151	1.690	1.958	1.506	1.821	1.459	1.818	1.535	1.947	1.686	1.149			12
13				1.189	2.069	1.880	1.540	2.072	1.521	1.893	2.106	1.211				13
14					1.731	1.946	1.909	1.639	1.948	1.954	1.778					14
15							0.752	0.765	0.770							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

191

FQT*V(Z)/K(Z) FOR 3% BANDS C12 MAP560 09/12/88 D-215 10437MWD/MTU 99.79%HFP 50P 1 B-149 FCFM
SEARCH BETWEEN NODES 6 AND 56

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.744.	0.739.	0.740.							1
2					1.764.	1.908.	1.893.	1.605.	1.883.	1.896.	1.673.					2
3				1.192.	2.084.	1.844.	1.497.	2.039.	1.508.	1.843.	2.015.	1.149.				3
4			1.119.	1.645.	1.847.	1.436.	1.753.	1.418.	1.780.	1.457.	1.836.	1.627.	1.117.			4
5		1.692.	2.030.	1.841.	1.480.	2.056.	1.772.	1.417.	1.783.	2.055.	1.467.	1.845.	2.076.	1.731.		5
6		1.890.	1.798.	1.444.	2.127.	1.363.	1.382.	2.104.	1.384.	1.367.	2.059.	1.443.	1.821.	1.891.		6
7	0.754.	1.908.	1.488.	1.750.	1.833.	1.462.	1.656.	1.697.	1.641.	1.454.	1.784.	1.746.	1.485.	1.873.	0.737.	7
8	0.742.	1.613.	2.046.	1.414.	1.450.	2.133.	1.707.	1.393.	1.708.	2.130.	1.421.	1.411.	2.051.	1.594.	0.732.	8
9	0.725.	1.870.	1.478.	1.754.	1.810.	1.480.	1.696.	1.718.	1.659.	1.450.	1.779.	1.755.	1.483.	1.869.	0.732.	9
10		1.907.	1.803.	1.442.	2.088.	1.370.	1.406.	2.121.	1.400.	1.386.	2.120.	1.459.	1.819.	1.893.		10
11		1.686.	2.016.	1.828.	1.492.	2.061.	1.786.	1.431.	1.817.	2.142.	1.547.	1.876.	2.037.	1.676.		11
12			1.121.	1.644.	1.905.	1.466.	1.772.	1.419.	1.769.	1.494.	1.895.	1.640.	1.118.			12
13				1.157.	2.013.	1.829.	1.499.	2.016.	1.480.	1.842.	2.049.	1.178.				13
14					1.684.	1.893.	1.858.	1.595.	1.895.	1.901.	1.730.					14
15							0.732.	0.744.	0.749.							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

FQT*V(Z)/K(Z) FOR 5% BANDS C12 MAP560 09/12/88 D-215 10437MWD/MTU 99.79%HFP 50P 1 B-149 FCFM
SEARCH BETWEEN NODES 6 AND 56

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.764	0.759	0.760							1
2					1.812	1.961	1.945	1.649	1.935	1.948	1.719					2
3				1.225	2.142	1.895	1.539	2.096	1.550	1.895	2.070	1.181				3
4			1.150	1.690	1.899	1.476	1.802	1.457	1.830	1.497	1.887	1.672	1.148			4
5		1.739	2.086	1.892	1.521	2.113	1.821	1.456	1.832	2.112	1.508	1.896	2.133	1.780		5
6		1.942	1.848	1.484	2.186	1.401	1.420	2.162	1.423	1.405	2.117	1.484	1.872	1.943		6
7	0.775	1.960	1.529	1.799	1.884	1.502	1.702	1.744	1.687	1.494	1.833	1.795	1.526	1.924	0.758	7
8	0.762	1.658	2.102	1.453	1.490	2.193	1.754	1.432	1.755	2.190	1.460	1.450	2.108	1.638	0.752	8
9	0.745	1.921	1.519	1.803	1.861	1.521	1.743	1.766	1.704	1.490	1.829	1.804	1.524	1.921	0.752	9
10		1.960	1.853	1.482	2.146	1.408	1.445	2.180	1.439	1.424	2.179	1.499	1.870	1.946		10
11		1.733	2.072	1.879	1.533	2.118	1.836	1.470	1.868	2.202	1.590	1.928	2.093	1.723		11
12			1.151	1.690	1.958	1.506	1.821	1.459	1.818	1.535	1.947	1.686	1.149			12
13				1.189	2.069	1.880	1.540	2.072	1.521	1.893	2.106	1.211				13
14					1.731	1.946	1.909	1.639	1.948	1.954	1.778					14
15							0.752	0.765	0.770							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

MAXIMUM FQT*V(Z)/K(Z) C12 MAP560 09/12/88 D-215 10437MWD/MTU 99.79%HFP 50P 1 B-149 FCFM

AXIAL NODE	3%	SOURCE	5%	SOURCE
1	.85031	F 6	.87308	F 6
2	.96526	L11	.99111	L11
3	1.0726	L11	1.1013	L11
4	1.1911	L11	1.2230	L11
5	1.8047	H 6	1.8531	H 6
6	1.8212	H 6	1.8703	H 6
7	1.9175	H10	1.9692	H10
8	2.0265	H10	2.0815	H10
9	2.0833	K 8	2.1400	K 8
10	2.1094	K 8	2.1669	K 8
11	2.1245	K 8	2.1827	K 8
12	2.1272	K 8	2.1857	K 8
13	2.1211	K 8	2.1796	K 8
14	2.1021	K 8	2.1604	K 8
15	2.0794	K 8	2.1372	K 8
16	2.0320	K 8	2.0884	K 8
17	1.9449	K 8	1.9989	K 8
18	2.0008	H10	2.0564	H10
19	2.0160	K 8	2.0720	K 8
20	2.0067	H10	2.0624	H10
21	1.9991	H10	2.0546	H10
22	1.9938	K 8	2.0492	K 8
23	1.9834	K 8	2.0385	K 8
24	1.9799	K 8	2.0349	K 8
25	1.9669	K 8	2.0215	K 8
26	1.9566	K 8	2.0109	K 8
27	1.9162	K 8	1.9695	K 8
28	1.8419	H 6	1.8930	H 6
29	1.9090	H10	1.9620	H10
30	1.9308	K 8	1.9844	K 8
31	1.9342	K 8	1.9880	K 8
32	1.9425	K 8	1.9965	K 8
33	1.9478	K 8	2.0019	K 8
34	1.9534	K 8	2.0077	K 8
35	1.9603	K 8	2.0148	K 8
36	1.9656	K 8	2.0202	K 8
37	1.9714	K 8	2.0262	K 8
38	1.9672	F11	2.0219	F11
39	1.9029	F11	1.9557	F11
40	1.9740	K 8	2.0288	K 8
41	2.0175	H10	2.0735	H10
42	2.0340	H10	2.0905	H10
43	2.0510	L 6	2.1080	L 6
44	2.0802	L 6	2.1380	L 6
45	2.0923	F11	2.1505	F11
46	2.1054	F11	2.1639	F11
47	2.1234	F11	2.1824	F11
48	2.1421	F11	2.2016	F11
49	2.1344	F11	2.1937	F11
50	2.0548	F11	2.1118	F11
51	2.1149	K 8	2.1737	K 8
52	2.1334	K 8	2.1926	K 8
53	2.1112	F 8	2.1698	F 8
54	2.0686	F 8	2.1261	F 8
55	1.9868	F11	2.0420	F11
56	1.9058	L 6	1.9588	L 6
57	1.7803	F11	1.8297	F11

58	1.6352	L 6	1.6806	L 6	
59	.82970	E11	.85275	E11	
60	.61513	E11	.63222	E11	
61	.53296	L11	.54776	L11	

ASM'Y RELATIVE POWER: PRED/MEAS/DIFF C12 MAP566 09/27/88 D-194 11220MWD/MTU 87.89%HFP 52P 1 B-115 FCFM

					0.228.	0.254.	0.228.							
					0.222.	0.247.	0.226.							
					-2.77.	-2.76.	-0.69.							
				0.813.	1.063.	1.135.	0.974.	1.135.	1.063.	0.813.				
				0.827.	1.046.	1.118.	0.959.	1.131.	1.059.	0.808.				
				1.74.	-1.54.	-1.54.	-1.59.	-0.35.	-0.39.	-0.61.				
			0.507.	1.247.	1.182.	1.021.	1.374.	1.021.	1.182.	1.247.	0.507.			
			0.515.	1.269.	1.179.	1.004.	1.352.	1.024.	1.186.	1.244.	0.501.			
			1.62.	1.77.	-0.29.	-1.69.	-1.58.	0.22.	0.27.	-0.24.	-1.10.			
		0.488.	0.959.	1.204.	0.976.	1.140.	0.951.	1.140.	0.976.	1.204.	0.959.	0.488.		
		0.485.	0.966.	1.225.	0.979.	1.132.	0.943.	1.152.	0.988.	1.217.	0.964.	0.486.		
		-0.77.	0.73.	1.75.	0.28.	-0.73.	-0.78.	1.07.	1.17.	1.05.	0.49.	-0.53.		
	0.809.	1.239.	1.199.	1.004.	1.350.	1.146.	0.947.	1.146.	1.350.	1.004.	1.199.	1.239.	0.809.	
	0.791.	1.211.	1.208.	1.030.	1.375.	1.147.	0.946.	1.158.	1.379.	1.025.	1.210.	1.238.	0.802.	
	-2.20.	-2.24.	0.73.	2.66.	1.82.	0.12.	-0.18.	1.03.	2.10.	2.15.	0.89.	-0.10.	-0.82.	
	1.059.	1.177.	0.973.	1.352.	0.952.	0.956.	1.393.	0.956.	0.952.	1.352.	0.973.	1.177.	1.059.	
	1.043.	1.158.	0.982.	1.411.	0.964.	0.950.	1.385.	0.952.	0.970.	1.374.	0.981.	1.173.	1.051.	
	-1.56.	-1.64.	0.89.	4.37.	1.22.	-0.58.	-0.58.	-0.37.	1.85.	1.67.	0.76.	-0.34.	-0.76.	
0.228.	1.132.	1.017.	1.138.	1.147.	0.962.	1.142.	1.168.	1.142.	0.962.	1.147.	1.138.	1.017.	1.132.	0.228.
0.224.	1.114.	1.004.	1.142.	1.180.	0.971.	1.128.	1.150.	1.118.	0.959.	1.154.	1.136.	1.008.	1.123.	0.226.
-1.51.	-1.53.	-1.27.	0.31.	2.84.	1.01.	-1.17.	-1.55.	-2.07.	-0.26.	0.59.	-0.16.	-0.83.	-0.78.	-0.71.
0.253.	0.971.	1.370.	0.949.	0.950.	1.395.	1.167.	0.988.	1.167.	1.395.	0.950.	0.949.	1.370.	0.971.	0.253.
0.245.	0.952.	1.337.	0.944.	0.961.	1.402.	1.153.	0.961.	1.147.	1.388.	0.950.	0.945.	1.361.	0.955.	0.251.
-3.46.	-1.94.	-2.39.	-0.53.	1.22.	0.51.	-1.25.	-2.72.	-1.77.	-0.52.	0.07.	-0.39.	-0.60.	-1.58.	-0.88.
0.228.	1.132.	1.017.	1.138.	1.147.	0.962.	1.142.	1.168.	1.142.	0.962.	1.147.	1.138.	1.017.	1.132.	0.228.
0.220.	1.106.	0.992.	1.133.	1.157.	0.968.	1.143.	1.141.	1.109.	0.962.	1.154.	1.143.	1.009.	1.117.	0.224.
-3.47.	-2.25.	-2.40.	-0.47.	0.85.	0.68.	0.09.	-2.28.	-2.89.	0.03.	0.58.	0.44.	-0.76.	-1.25.	-1.58.
	1.059.	1.177.	0.973.	1.352.	0.952.	0.956.	1.393.	0.956.	0.952.	1.352.	0.973.	1.177.	1.059.	
	1.039.	1.154.	0.978.	1.387.	0.964.	0.957.	1.389.	0.955.	0.974.	1.408.	0.991.	1.175.	1.046.	
	-1.93.	-1.97.	0.53.	2.58.	1.20.	0.17.	-0.35.	-0.05.	2.27.	4.17.	1.87.	-0.16.	-1.20.	
	0.809.	1.239.	1.199.	1.004.	1.350.	1.146.	0.947.	1.146.	1.350.	1.004.	1.199.	1.239.	0.809.	
	0.802.	1.228.	1.216.	1.045.	1.381.	1.155.	0.958.	1.175.	1.414.	1.076.	1.239.	1.236.	0.799.	
	-0.82.	-0.85.	1.39.	4.18.	2.24.	0.83.	1.17.	2.58.	4.70.	7.27.	3.33.	-0.28.	-1.17.	
		0.488.	0.959.	1.204.	0.976.	1.140.	0.951.	1.140.	0.976.	1.204.	0.959.	0.488.		
		0.489.	0.977.	1.257.	0.999.	1.146.	0.941.	1.136.	1.009.	1.244.	0.962.	0.485.		
		0.18.	1.83.	4.36.	2.29.	0.52.	-1.06.	-0.32.	3.35.	3.26.	0.32.	-0.75.		
			0.507.	1.247.	1.182.	1.021.	1.374.	1.021.	1.182.	1.247.	0.507.			
			0.503.	1.228.	1.180.	0.999.	1.314.	0.996.	1.170.	1.237.	0.503.			
			-0.74.	-1.50.	-0.22.	-2.22.	-4.33.	-2.51.	-1.00.	-0.83.	-0.75.			
				0.813.	1.063.	1.135.	0.974.	1.135.	1.063.	0.813.				
				0.801.	1.047.	1.075.	0.944.	1.122.	1.054.	0.806.				
				-1.44.	-1.44.	-5.29.	-3.07.	-1.15.	-0.81.	-0.86.				
					0.228.	0.254.	0.228.							
					0.224.	0.250.	0.225.							

. -1.66. -1.38. -1.37.

98

C12 MAP566 09/27/88 D-194 11220MWD/MTU 87.89%HFP 52P 1 B-115 FCFM

FINAL COMPARISON OF SATURATION ACTIVITY AND PDQ ACTIVATION

DRIVE	THIMBLE		STATUS	MEASURED AXIAL FACTOR	REGION % DIFF 1- 4	4-43	43-58	58-61	FZ/KZ
1	1	M 3	GOOD	1.1331	15.0594	2.9595	-2.7061	-2.4165	1.1570
0	2	J15	NONE						
1	3	F 4	GOOD	1.1455	-8.0374	0.7314	0.8897	13.0106	1.1455
1	4	L 8	GOOD	1.1699	-2.2746	0.6953	1.6230	9.4725	1.1699
1	5	F 8	GOOD	1.1410	-1.9672	-1.0859	1.0341	4.9274	1.1410
1	6	D12	GOOD	1.1313	14.5213	-0.3879	-2.7768	-3.3245	1.1370
1	7	B 5	GOOD	1.1495	-12.8607	-0.1070	-3.0590	-9.1864	1.1495
1	8	H 6	GOOD	1.1307	-14.3676	-0.5289	-0.0436	-5.7634	1.1307
1	9	J 3	GOOD	1.1337	-14.3307	-1.8445	-1.5903	6.7020	1.1434
2	10	D 3	GOOD	1.1190	21.5514	0.8055	-6.6983	-12.4294	1.1659
2	11	L 9	GOOD	1.1571	3.3421	0.4771	0.8031	-4.6213	1.1571
2	12	B10	GOOD	1.1367	-27.3867	-0.6615	-2.0953	-7.8113	1.1405
2	13	L 4	GOOD	1.1347	12.2980	2.0693	0.3398	-9.3715	1.1347
2	14	F13	GOOD	1.1383	0.7889	-0.2767	-2.8876	-15.7167	1.1383
2	15	F 6	GOOD	1.1515	16.5598	1.7119	2.5558	15.4058	1.1515
2	16	J12	GOOD	1.1628	-24.5120	0.7350	1.8194	3.1747	1.1628
2	17	B 7	GOOD	1.1379	-7.9789	0.4228	-2.4348	-8.0979	1.1798
0	18	H 1	NONE						
3	19	G 9	GOOD	1.1491	4.1818	-4.4037	-3.1160	-6.1851	1.1491
1	20	G 7	GOOD	1.1343	-4.0706	-3.4125	-2.4440	-1.2108	1.1343
3	21	F11	GOOD	1.1386	-0.2054	2.4532	6.4108	7.2452	1.1386
3	22	N 5	GOOD	1.1482	-0.1557	-3.0114	-1.5439	-1.5023	1.1482
3	23	J10	GOOD	1.1431	7.5627	-0.5707	0.5424	6.4926	1.1431
3	24	J 5	GOOD	1.1403	2.8630	-0.7874	1.3225	6.0179	1.1403
3	25	B 8	GOOD	1.1568	13.0064	-1.0164	-3.3485	-7.8659	1.1914
3	26	N10	GOOD	1.1429	5.9515	-2.8100	-1.1237	1.7369	1.1429
0	27	C12	NONE						
4	28	J 7	GOOD	1.1299	0.0791	-1.8458	-0.7008	4.6301	1.1299
4	29	D 7	GOOD	1.1512	-3.3731	-0.9048	0.7618	2.6458	1.1512
4	30	L14	GOOD	1.1425	0.2406	-0.8933	-3.6961	-9.7517	1.1425
4	31	F 2	GOOD	1.1150	1.0129	0.0560	-1.8739	-11.2446	1.1442
4	32	F 9	GOOD	1.1507	7.9666	0.0631	0.9652	11.3390	1.1507
4	33	N 7	GOOD	1.1268	4.2771	-0.9218	-1.9855	2.2223	1.1540
0	34	A 9	NONE						
5	35	N12	GOOD	1.1208	23.0223	1.6690	-4.6503	-6.4782	1.1508
0	36	R 8	NONE						
0	37	H 4	NONE						
5	38	H11	GOOD	1.1686	7.6062	0.6371	1.8497	2.3839	1.1686
5	39	D 5	GOOD	1.1474	-4.3734	0.8264	-0.0927	-9.7318	1.1474
5	40	L 6	GOOD	1.1336	0.6809	3.2152	6.3962	4.9459	1.1336
5	41	D10	GOOD	1.1542	7.6385	0.5000	0.9128	9.7000	1.1542
5	42	G14	GOOD	1.1310	-28.7725	-0.2298	-0.6696	1.5429	1.1781
3	43	H13	GOOD	1.1270	-8.8342	-5.6792	-4.9568	-10.4458	1.1288
2	44	C 8	GOOD	1.1310	-15.2511	-0.5248	0.0180	-8.4683	1.1327
0	45	H 3	NONE						
4	46	N 8	GOOD	1.1276	-5.9480	-2.6406	-2.8679	-13.9458	1.1452
2	47	E11	GOOD	1.1523	36.9988	9.5675	8.2459	10.7488	1.1523
4	48	L11	GOOD	1.1547	7.4553	3.3365	4.9377	25.6882	1.1547
5	49	E 5	GOOD	1.1496	26.5733	2.1697	2.0333	11.7768	1.1496
0	50	L 5	NONE						
AVG. OF ABSOLUTE VALUES OF GOOD THIMBLES ONLY				1.1414	10.14	1.66	2.40	7.79	

FORM 0113 (02/83)

SYMMETRIC THIMBLE COMPARISON C12 MAP566 09/27/88 D-194 11220MWD/MTU 87.89%HFP 52P 1 B-115 FCFM

THMBL	LOC	INTEGRAL	THMBL	LOC	INTEGRAL	RATIO
1	M 3	0.32857E+02	10	D 3	0.31991E+02	1.0270
10	D 3	0.31991E+02	1	M 3	0.32857E+02	.97367
19	G 9	0.59522E+02	20	G 7	0.60000E+02	.99204
19	G 9	0.59522E+02	28	J 7	0.61132E+02	.97367
20	G 7	0.60000E+02	19	G 9	0.59522E+02	1.0080
20	G 7	0.60000E+02	28	J 7	0.61132E+02	.98148
28	J 7	0.61132E+02	19	G 9	0.59522E+02	1.0270
28	J 7	0.61132E+02	20	G 7	0.60000E+02	1.0189
44	C 8	0.64263E+02	46	N 8	0.62916E+02	1.0214
46	N 8	0.62916E+02	44	C 8	0.64263E+02	.97903
47	E11	0.74842E+02	48	L11	0.71158E+02	1.0518
47	E11	0.74842E+02	49	E 5	0.70113E+02	1.0675
48	L11	0.71158E+02	47	E11	0.74842E+02	.95078
48	L11	0.71158E+02	49	E 5	0.70113E+02	1.0149
49	E 5	0.70113E+02	47	E11	0.74842E+02	.93681
49	E 5	0.70113E+02	48	L11	0.71158E+02	.98531

221

C12 MAP566 09/27/88 D-194 11220MWD/MTU 87.89%HFP 52P 1 B-115 FCFM

RECEIVED BY.....
RECEIVED DATE.....

VERSION PNR16022
RUN DATE 09/28/88

SUMMARY OF INCORE RESULTS	MEASURED			MEASURED /W UNCERTAINTY FACTOR	TECH. SPEC. LIMIT
F-DELTA-H (MAX. ASSEMBLY) =	1.414	LOC F11	REGION 15		
F-DELTA-H (MAX. ASSEMBLY) =	1.257	LOC L12	REGION 14		
F-DELTA-H (MAX. ASSEMBLY) =	1.076	LOC E11	REGION 12R		
F-DELTA-H (MAX. ASSEMBLY) =	1.024	LOC G 3	REGION 13A		
F-DELTA-H (MAX. ASSEMBLY) =	0.251	LOC A 8	REGION 13		
F-DELTA-H (PEAK PIN) =	1.527	LOC F11	REGION 15	1.588	1.690
F-DELTA-H (PEAK PIN) =	1.345	LOC L12	REGION 14	1.399	1.690
F-DELTA-H (PEAK PIN) =	1.148	LOC E11	REGION 12R	1.194	1.690
F-DELTA-H (PEAK PIN) =	1.086	LOC G 3	REGION 13A	1.130	1.690
F-DELTA-H (PEAK PIN) =	0.387	LOC G 1	REGION 13	0.403	1.690
FQT/K(Z) =		LOC F11	REGION 15	1.984	2.640
FQT/K(Z) =		LOC L12	REGION 14	1.735	2.640
FQT/K(Z) =		LOC E11	REGION 12R	1.435	2.640
FQT/K(Z) =		LOC G 3	REGION 13A	1.380	2.640
FQT/K(Z) =		LOC G15	REGION 13	0.699	2.640
FQN (WITH LOCAL PEAKING) =	1.832	LOC F11	REGION 15		
FQN (WITH LOCAL PEAKING) =	1.603	LOC L12	REGION 14		
FQN (WITH LOCAL PEAKING) =	1.332	LOC E11	REGION 12R		
FQN (WITH LOCAL PEAKING) =	1.274	LOC F12	REGION 13A		
FQN (WITH LOCAL PEAKING) =	0.623	LOC G15	REGION 13		

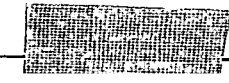
CALCULATED POWER TILTS(NORMALIZED TO 1.000)

(-,+) QUADRANT =	0.999	1.02
(+,+) QUADRANT =	1.000	1.02
(-,-) QUADRANT =	0.998	1.02
(+,-) QUADRANT =	1.003	1.02

REGION 15	AVERAGE POWER FRACTION	1.160	REGION 15	STD % DIF	1.992
REGION 14	AVERAGE POWER FRACTION	1.132	REGION 14	STD % DIF	1.642
REGION 12R	AVERAGE POWER FRACTION	1.006	REGION 12R	STD % DIF	3.739
REGION 13A	AVERAGE POWER FRACTION	0.881	REGION 13A	STD % DIF	1.286
REGION 13	AVERAGE POWER FRACTION	0.232	REGION 13	STD % DIF	2.101

AXIAL OFFSET = -3.061
FXY (NEGLECTING GRIDS) = 1.589 LOC L 6 NODE 44

MAX FQT*V(Z)/K(Z) FOR 3% BANDS = 2.142
MAX FQT*V(Z)/K(Z) FOR 5% BANDS = 2.202



FORM 0113 (02/83)

FQZ BASED APL FOR 3% BANDS = 108.29%
FQZ BASED APL FOR 5% BANDS = 105.37%

A QUARTER CORE AVERAGED ASSEMBLY RELATIVE POWER C12 MAP566 09/27/88 D-194 11220MWD/MTU 87.89%HFP 52P 1 B-115 FCFM

	H	G	F	E	D	C	B	A	
1	0.988 0.961 -2.715	1.167 1.150 -1.510	1.395 1.395 -0.005	0.950 0.956 0.647	0.949 0.945 -0.463	1.370 1.349 -1.491	0.971 0.954 -1.758	0.253 0.248 -2.174	1
2	1.168 1.146 -1.918	1.142 1.125 -1.510	0.962 0.965 0.366	1.147 1.161 1.217	1.138 1.139 0.030	1.017 1.003 -1.316	1.132 1.115 -1.452	0.228 0.223 -1.815	2
3	1.393 1.387 -0.463	0.956 0.954 -0.208	0.952 0.968 1.636	1.352 1.395 3.197	0.973 0.983 1.014	1.177 1.165 -1.028	1.059 1.045 -1.364		3
4	0.947 0.952 0.493	1.146 1.159 1.140	1.350 1.387 2.714	1.004 1.044 4.065	1.199 1.218 1.586	1.239 1.228 -0.869	0.809 0.798 -1.251		4
5	0.951 0.942 -0.923	1.140 1.142 0.136	0.976 0.994 1.772	1.204 1.236 2.607	0.959 0.967 0.844	0.488 0.486 -0.467			5
6	1.374 1.333 -2.957	1.021 1.006 -1.550	1.182 1.179 -0.313	1.247 1.244 -0.203	0.507 0.505 -0.242				6
7	0.974 0.951 -2.332	1.135 1.111 -2.081	1.063 1.052 -1.045	0.813 0.810 -0.292					7
8	0.254 0.249 -2.072	0.228 0.224 -1.623							8
	H	G	F	E	D	C	B	A	

PRED
MES
DIF

FORM 0113 (02/83)

181

FQN C12 MAP566 09/27/88 D-194 1122OMWD/MTU 87.89%HFP 52P 1 B-115 FCFM

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.616.	0.614.	0.619.							1
2					1.441.	1.572.	1.555.	1.334.	1.562.	1.589.	1.410.					2
3				1.019.	1.744.	1.537.	1.253.	1.711.	1.271.	1.539.	1.697.	0.978.				3
4			0.950.	1.394.	1.559.	1.226.	1.459.	1.203.	1.481.	1.239.	1.541.	1.384.	0.951.			4
5		1.416.	1.702.	1.554.	1.283.	1.764.	1.503.	1.208.	1.513.	1.756.	1.266.	1.551.	1.730.	1.436.		5
6		1.570.	1.517.	1.245.	1.827.	1.180.	1.181.	1.787.	1.184.	1.179.	1.760.	1.236.	1.520.	1.560.		6
7	0.619.	1.551.	1.247.	1.472.	1.564.	1.241.	1.408.	1.442.	1.401.	1.228.	1.522.	1.468.	1.250.	1.575.	0.621.	7
8	0.606.	1.325.	1.702.	1.204.	1.238.	1.828.	1.447.	1.184.	1.447.	1.810.	1.220.	1.208.	1.719.	1.341.	0.616.	8
9	0.608.	1.529.	1.248.	1.463.	1.532.	1.243.	1.435.	1.444.	1.400.	1.226.	1.516.	1.469.	1.251.	1.561.	0.618.	9
10		1.579.	1.517.	1.236.	1.784.	1.178.	1.195.	1.806.	1.201.	1.195.	1.814.	1.252.	1.535.	1.595.		10
11		1.410.	1.690.	1.543.	1.292.	1.762.	1.523.	1.233.	1.555.	1.832.	1.332.	1.579.	1.713.	1.426.		11
12			0.939.	1.397.	1.603.	1.258.	1.490.	1.212.	1.477.	1.274.	1.585.	1.388.	0.947.			12
13				0.999.	1.710.	1.535.	1.260.	1.678.	1.241.	1.528.	1.702.	1.004.				13
14					1.428.	1.591.	1.482.	1.310.	1.561.	1.572.	1.429.					14
15							0.621.	0.621.	0.623.							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

CALCULATED LOCAL PEAKING FACTORS C12 MAP566 09/27/88 D-194 11220MWD/MTU 87.89%HFP 52P 1 B-115 FCFM

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							1.711	1.531	1.712							1
2					1.489	1.286	1.192	1.188	1.191	1.286	1.489					2
3				1.665	1.160	1.090	1.061	1.077	1.061	1.090	1.160	1.665				3
4			1.653	1.217	1.070	1.058	1.056	1.045	1.056	1.058	1.070	1.217	1.652			4
5		1.490	1.161	1.069	1.067	1.080	1.095	1.046	1.095	1.080	1.067	1.069	1.161	1.490		5
6		1.287	1.090	1.059	1.081	1.047	1.056	1.087	1.056	1.047	1.081	1.059	1.090	1.286		6
7	1.711	1.191	1.062	1.055	1.095	1.058	1.059	1.065	1.059	1.058	1.095	1.055	1.062	1.191	1.711	7
8	1.531	1.187	1.077	1.044	1.047	1.088	1.066	1.032	1.066	1.088	1.047	1.044	1.077	1.186	1.531	8
9	1.712	1.192	1.062	1.055	1.095	1.058	1.059	1.066	1.059	1.058	1.095	1.055	1.062	1.191	1.711	9
10		1.287	1.090	1.059	1.081	1.047	1.056	1.087	1.056	1.047	1.081	1.059	1.090	1.286		10
11		1.490	1.161	1.069	1.067	1.080	1.095	1.046	1.095	1.080	1.067	1.069	1.161	1.490		11
12			1.653	1.217	1.070	1.057	1.056	1.045	1.056	1.058	1.070	1.217	1.653			12
13				1.665	1.160	1.089	1.061	1.077	1.061	1.089	1.160	1.665				13
14					1.489	1.286	1.192	1.187	1.191	1.286	1.489					14
15							1.712	1.531	1.711							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

NUCLEAR F-DELTA-H (FDHN) C12 MAP566 09/27/88 D-194 11220MWD/MTU 87.89%HFP 52P 1 B-115 FCFM

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.379	0.378	0.387							1
2					1.231	1.346	1.332	1.139	1.348	1.362	1.203					2
3				0.857	1.472	1.284	1.066	1.456	1.086	1.292	1.443	0.834				3
4			0.801	1.176	1.311	1.035	1.195	0.986	1.217	1.045	1.302	1.173	0.803			4
5		1.179	1.407	1.292	1.099	1.485	1.256	0.989	1.267	1.489	1.094	1.294	1.437	1.195		5
6		1.342	1.262	1.040	1.524	1.009	1.003	1.506	1.005	1.016	1.485	1.038	1.279	1.352		6
7	0.384	1.328	1.066	1.205	1.292	1.027	1.195	1.225	1.185	1.015	1.264	1.199	1.070	1.337	0.387	7
8	0.375	1.130	1.439	0.986	1.006	1.525	1.229	0.992	1.223	1.509	0.995	0.987	1.466	1.134	0.385	8
9	0.376	1.318	1.054	1.195	1.267	1.024	1.211	1.216	1.175	1.017	1.263	1.206	1.071	1.331	0.383	9
10		1.337	1.258	1.036	1.498	1.009	1.011	1.510	1.009	1.020	1.522	1.050	1.281	1.346		10
11		1.195	1.427	1.301	1.115	1.492	1.265	1.003	1.287	1.527	1.148	1.325	1.435	1.191		11
12			0.808	1.189	1.345	1.056	1.210	0.983	1.200	1.067	1.331	1.171	0.801			12
13				0.837	1.424	1.285	1.060	1.415	1.057	1.275	1.434	0.837				13
14					1.193	1.347	1.281	1.121	1.337	1.356	1.200					14
15							0.383	0.383	0.385							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

PERCENT AXIAL OFFSET TOWARD TOP OF ASSEMBLY C12 MAP566 09/27/88 D-194 11220MWD/MTU 87.89%HFP 52P 1 B-115 FCFM

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							38.1	38.2	38.2							1
2					-1.5	-3.3	-1.6	-0.9	-0.7	-2.4	-2.2					2
3				-2.5	-2.6	-4.0	-3.8	-3.7	-3.4	-4.1	-2.7	-1.4				3
4			-3.6	-3.1	-3.2	-4.0	-5.4	-5.5	-5.3	-4.5	-3.5	-2.7	-2.6			4
5		-4.5	-4.8	-4.7	-3.9	-4.4	-5.0	-5.4	-4.5	-4.0	-3.2	-3.8	-3.5	-2.9		5
6		-3.2	-4.4	-4.9	-5.5	-4.9	-4.3	-4.1	-4.1	-3.9	-4.0	-4.2	-3.7	-1.7		6
7	38.1	-1.1	-3.2	-5.2	-5.4	-5.5	-4.3	-4.0	-4.3	-5.2	-5.1	-5.7	-3.1	0.3	38.6	7
8	38.0	-0.5	-3.3	-5.0	-5.5	-4.5	-4.4	-4.6	-4.2	-4.8	-5.8	-5.6	-3.4	0.9	38.6	8
9	37.9	-1.7	-3.9	-5.1	-4.5	-4.8	-4.0	-3.8	-4.0	-4.9	-4.8	-5.0	-3.2	-0.7	38.1	9
10		-3.9	-5.0	-4.5	-4.1	-4.0	-4.0	-4.2	-4.4	-4.2	-4.1	-3.9	-4.1	-2.8		10
11		-2.8	-3.1	-3.8	-4.1	-4.4	-4.8	-5.4	-5.5	-5.5	-2.9	-3.4	-3.5	-3.5		11
12			-1.2	-2.6	-4.7	-4.9	-5.8	-5.5	-5.4	-4.4	-3.8	-2.8	-2.7			12
13				-3.1	-3.7	-4.5	-4.2	-3.7	-3.4	-3.7	-3.3	-3.3				13
14					-3.4	-2.6	-1.6	-0.7	-1.2	-2.7	-3.4					14
15							37.7	37.7	37.7							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

FQT*V(Z)/K(Z) FOR 3% BANDS C12 MAP566 09/27/88 D-194 11220MWD/MTU 87.89%HFP 52P 1 B-115 FCFM
FULL CORE SEARCH

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.741	0.738	0.759							1
2					1.746	1.857	1.850	1.587	1.894	1.901	1.687					2
3				1.196	2.037	1.794	1.470	2.002	1.491	1.797	2.003	1.178				3
4			1.106	1.624	1.822	1.428	1.717	1.394	1.742	1.443	1.801	1.613	1.107			4
5		1.660	1.990	1.816	1.492	2.062	1.750	1.396	1.763	2.054	1.472	1.813	2.023	1.683		5
6		1.858	1.772	1.451	2.137	1.375	1.377	2.079	1.381	1.374	2.059	1.441	1.776	1.889		6
7	0.754	1.869	1.472	1.730	1.819	1.462	1.641	1.683	1.633	1.446	1.770	1.724	1.468	1.884	0.752	7
8	0.738	1.586	2.007	1.393	1.433	2.124	1.691	1.385	1.691	2.104	1.412	1.397	2.025	1.585	0.746	8
9	0.726	1.829	1.463	1.718	1.782	1.463	1.672	1.685	1.631	1.443	1.763	1.726	1.467	1.852	0.741	9
10		1.862	1.772	1.441	2.087	1.372	1.394	2.102	1.400	1.393	2.122	1.460	1.793	1.882		10
11		1.653	1.976	1.803	1.503	2.061	1.774	1.425	1.811	2.142	1.549	1.846	2.004	1.672		11
12			1.122	1.628	1.873	1.465	1.753	1.404	1.737	1.484	1.853	1.626	1.114			12
13				1.154	1.998	1.792	1.478	1.962	1.456	1.784	1.989	1.162				13
14					1.674	1.880	1.780	1.560	1.871	1.876	1.675					14
15							0.750	0.752	0.755							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

FQT*V(Z)/K(Z) FOR 5% BANDS C12 MAP566 09/27/88 D-194 11220MWD/MTU 87.89%HFP 52P 1 B-115 FCFM
FULL CORE SEARCH

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.762	0.758	0.780							1
2					1.794	1.908	1.901	1.631	1.946	1.954	1.733					2
3				1.229	2.093	1.844	1.511	2.058	1.532	1.847	2.058	1.210				3
4			1.137	1.669	1.873	1.468	1.764	1.432	1.790	1.483	1.851	1.658	1.138			4
5		1.706	2.045	1.866	1.534	2.120	1.799	1.435	1.812	2.111	1.513	1.863	2.079	1.730		5
6		1.910	1.821	1.492	2.196	1.413	1.416	2.137	1.419	1.412	2.116	1.481	1.825	1.941		6
7	0.775	1.921	1.512	1.778	1.869	1.502	1.687	1.730	1.678	1.486	1.819	1.772	1.509	1.936	0.773	7
8	0.758	1.630	2.063	1.431	1.473	2.183	1.738	1.424	1.738	2.162	1.451	1.436	2.080	1.629	0.766	8
9	0.746	1.880	1.504	1.766	1.832	1.504	1.719	1.732	1.676	1.483	1.811	1.773	1.508	1.904	0.762	9
10		1.914	1.821	1.481	2.145	1.411	1.433	2.160	1.439	1.431	2.181	1.500	1.842	1.934		10
11		1.699	2.031	1.853	1.545	2.118	1.823	1.465	1.862	2.202	1.592	1.897	2.059	1.719		11
12			1.152	1.673	1.925	1.505	1.802	1.443	1.785	1.525	1.905	1.671	1.145			12
13				1.186	2.053	1.842	1.519	2.017	1.496	1.834	2.044	1.193				13
14					1.720	1.932	1.830	1.603	1.923	1.928	1.721					14
15							0.771	0.773	0.776							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

MAXIMUM FQT*V(Z)/K(Z) C12 MAP566 09/27/88 D-194 11220MWD/MTU 87.89%HFP 52P 1 B-115 FCFM

AXIAL NODE	3%	SOURCE	5%	SOURCE
1	.92268	F 6	.94740	F 6
2	.89122	E11	.91509	E11
3	1.0421	E11	1.0700	E11
4	1.1009	E11	1.1304	E11
5	1.6796	L 6	1.7246	L 6
6	1.6864	L 3	1.7318	L 3
7	1.8039	L 3	1.8526	L 3
8	1.9158	L 3	1.9677	L 3
9	1.9788	L 3	2.0326	L 3
10	2.0169	L 3	2.0719	L 3
11	2.0411	K 8	2.0971	K 8
12	2.0680	K 8	2.1249	K 8
13	2.0812	K 8	2.1387	K 8
14	2.0824	K 8	2.1401	K 8
15	2.0796	K 8	2.1373	K 8
16	2.0485	K 8	2.1054	K 8
17	1.9612	K 8	2.0157	K 8
18	2.0081	H 6	2.0639	H 6
19	2.0477	K 8	2.1046	K 8
20	2.0414	K 8	2.0981	K 8
21	2.0328	K 8	2.0893	K 8
22	2.0347	K 8	2.0912	K 8
23	2.0295	K 8	2.0858	K 8
24	2.0266	K 8	2.0829	K 8
25	2.0167	K 8	2.0728	K 8
26	2.0013	K 8	2.0569	K 8
27	1.9632	K 8	2.0178	K 8
28	1.8820	F11	1.9343	F11
29	1.9339	H10	1.9876	H10
30	1.9643	K 8	2.0188	K 8
31	1.9706	K 8	2.0253	K 8
32	1.9838	F11	2.0389	F11
33	1.9892	F11	2.0444	F11
34	2.0010	F11	2.0566	F11
35	2.0010	F11	2.0566	F11
36	1.9976	F11	2.0531	F11
37	2.0041	F11	2.0597	F11
38	1.9939	F11	2.0493	F11
39	1.9313	F11	1.9849	F11
40	1.9818	H10	2.0368	H10
41	2.0398	L 6	2.0965	L 6
42	2.0606	L 6	2.1178	L 6
43	2.0791	L 6	2.1369	L 6
44	2.1044	L 6	2.1629	L 6
45	2.1119	L 6	2.1706	L 6
46	2.1194	L 6	2.1783	L 6
47	2.1362	F11	2.1955	F11
48	2.1423	F11	2.2018	F11
49	2.1285	L 6	2.1876	L 6
50	2.0505	F11	2.1075	F11
51	2.1032	L 6	2.1616	L 6
52	2.1368	L 6	2.1962	L 6
53	2.1109	F11	2.1695	F11
54	2.0570	F11	2.1141	F11
55	1.9794	F 8	2.0344	F 8
56	1.8882	L 6	1.9406	L 6
57	1.7410	F11	1.7893	F11

1	58	1.6185	L 6	1.6634	L 6
2	59	.87882	L11	.90323	L11
3	60	.63232	L11	.64989	L11
4	61	.53197	E11	.54675	E11
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243

C12 MAP567 10/24/88 D-202 11949MWD/MTU 91.03%HFP 51P 1 B-45 FCFM

RECEIVED BY.....
RECEIVED DATE.....

VERSION PNR16023
RUN DATE 10/25/88

SUMMARY OF INCORE RESULTS	MEASURED				MEASURED /W UNCERTAINTY FACTOR	TECH. SPEC. LIMIT
F-DELTA-H (MAX. ASSEMBLY) =	1.427	LOC F11	REGION 15			
F-DELTA-H (MAX. ASSEMBLY) =	1.257	LOC L12	REGION 14			
F-DELTA-H (MAX. ASSEMBLY) =	1.075	LOC E11	REGION 12R			
F-DELTA-H (MAX. ASSEMBLY) =	1.020	LOC G 3	REGION 13A			
F-DELTA-H (MAX. ASSEMBLY) =	0.255	LOC H15	REGION 13			
F-DELTA-H (PEAK PIN) =	1.534	LOC F11	REGION 15		1.596	1.680
F-DELTA-H (PEAK PIN) =	1.340	LOC L12	REGION 14		1.393	1.680
F-DELTA-H (PEAK PIN) =	1.147	LOC E11	REGION 12R		1.193	1.680
F-DELTA-H (PEAK PIN) =	1.083	LOC G 3	REGION 13A		1.126	1.680
F-DELTA-H (PEAK PIN) =	0.393	LOC G 1	REGION 13		0.409	1.680
FQT/K(Z) =		LOC F11	REGION 15		1.974	2.549
FQT/K(Z) =		LOC L12	REGION 14		1.725	2.549
FQT/K(Z) =		LOC E11	REGION 12R		1.422	2.549
FQT/K(Z) =		LOC N 7	REGION 13A		1.382	2.549
FQT/K(Z) =		LOC R 7	REGION 13		0.716	2.549
FQN (WITH LOCAL PEAKING) =	1.822	LOC F11	REGION 15			
FQN (WITH LOCAL PEAKING) =	1.594	LOC L12	REGION 14			
FQN (WITH LOCAL PEAKING) =	1.321	LOC E11	REGION 12R			
FQN (WITH LOCAL PEAKING) =	1.269	LOC F12	REGION 13A			
FQN (WITH LOCAL PEAKING) =	0.637	LOC R 7	REGION 13			

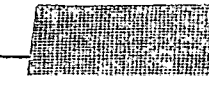
CALCULATED POWER TILTS(NORMALIZED TO 1.000)

(-,+) QUADRANT =	1.001	1.02
(+,+) QUADRANT =	0.999	1.02
(-,-) QUADRANT =	0.999	1.02
(+,-) QUADRANT =	1.001	1.02

REGION 15 AVERAGE POWER FRACTION	1.157	REGION 15 STD % DIF	1.937	
REGION 14 AVERAGE POWER FRACTION	1.131	REGION 14 STD % DIF	1.455	
REGION 12R AVERAGE POWER FRACTION	1.012	REGION 12R STD % DIF	3.383	
REGION 13A AVERAGE POWER FRACTION	0.884	REGION 13A STD % DIF	1.258	
REGION 13 AVERAGE POWER FRACTION	0.236	REGION 13 STD % DIF	1.974	

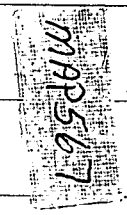
AXIAL OFFSET = -2.009
FXY (NEGLECTING GRIDS) = 1.592 LOC L 6 NODE 44

MAX FQT*V(Z)/K(Z) FOR 3% BANDS = 2.136
MAX FQT*V(Z)/K(Z) FOR 5% BANDS = 2.195



FORM 0113 (02/83)

FQZ BASED APL FOR 3% BANDS = 108.62%
FQZ BASED APL FOR 5% BANDS = 105.71%



C12 MAP567 10/24/88 D-202 11949MWD/MTU 91.03%HFP 51P 1 B-45 FCFM

FINAL COMPARISON OF SATURATION ACTIVITY AND PDQ ACTIVATION

DRIVE	THIMBLE		STATUS	MEASURED AXIAL FACTOR	REGION % DIFF 1- 4	4-43	43-58	58-61	FZ/KZ
1	1	M 3	GOOD	1.1238	11.8482	2.7321	-2.0036	-0.1689	1.1643
0	2	J15	NONE						
1	3	F 4	GOOD	1.1381	-10.6264	0.2050	0.2965	12.4176	1.1381
1	4	L 8	GOOD	1.1523	-0.1633	1.3336	1.9443	9.9593	1.1523
1	5	F 8	GOOD	1.1236	-1.0882	-0.3899	1.5434	4.8821	1.1236
1	6	D12	GOOD	1.1171	10.1024	-1.3052	-2.7634	-1.7422	1.1505
1	7	B 5	GOOD	1.1429	-11.7788	-0.5632	-2.6498	-8.2760	1.1454
1	8	H 6	GOOD	1.1160	-11.1169	-0.8182	-0.6616	-6.8041	1.1170
1	9	J 3	GOOD	1.1272	-14.4151	-1.9077	-1.3791	8.9638	1.1523
2	10	D 3	GOOD	1.1185	15.9420	0.4482	-5.9686	-10.0148	1.1743
2	11	L 9	GOOD	1.1428	5.7684	0.0831	0.7021	-3.4926	1.1435
2	12	B10	GOOD	1.1250	-29.3504	-1.1462	-2.3753	-7.5791	1.1532
2	13	L 4	GOOD	1.1290	8.0536	0.8159	-0.2564	-9.4364	1.1290
2	14	F13	GOOD	1.1410	-2.3688	-1.1991	-3.2878	-15.0857	1.1410
2	15	F 6	GOOD	1.1360	14.7044	0.5809	1.8068	15.9959	1.1488
2	16	J12	GOOD	1.1496	-23.8217	0.5332	1.1228	3.4723	1.1508
2	17	B 7	GOOD	1.1371	-7.1777	-0.1133	-2.8227	-8.1304	1.1845
0	18	H 1	NONE						
3	19	G 9	GOOD	1.1229	6.2551	-3.3735	-2.4029	-4.0907	1.1497
1	20	G 7	GOOD	1.1173	-1.9881	-2.4610	-1.7507	0.8215	1.1219
3	21	F11	GOOD	1.1235	-0.0691	2.5972	6.6462	7.1748	1.1235
3	22	N 5	GOOD	1.1405	-2.1828	-3.1601	-1.1823	-0.6527	1.1405
3	23	J10	GOOD	1.1300	7.9323	-0.1929	0.9184	8.3926	1.1307
3	24	J 5	GOOD	1.1319	3.2308	-0.5956	1.3261	6.9558	1.1319
3	25	B 8	GOOD	1.1514	11.9608	-0.6531	-3.1100	-8.0643	1.1994
3	26	N10	GOOD	1.1327	11.9034	-1.8119	-2.7214	-12.2377	1.1327
0	27	C12	NONE						
4	28	J 7	GOOD	1.1081	10.3104	0.0470	-1.6503	-7.7091	1.1357
4	29	D 7	GOOD	1.1417	-1.0495	0.7315	-0.3851	-7.8462	1.1475
4	30	L14	GOOD	1.1273	-1.0162	-0.7850	-2.6303	-8.1511	1.1431
4	31	F 2	GOOD	1.1007	-0.0911	0.0347	-1.5092	-12.6714	1.1526
4	32	F 9	GOOD	1.1305	8.5614	0.9078	2.0624	13.5644	1.1529
4	33	N 7	GOOD	1.1169	4.9299	-0.0629	-1.2589	4.7741	1.1664
0	34	A 9	NONE						
5	35	N12	GOOD	1.1180	18.5138	1.2243	-4.4746	-4.3055	1.1593
0	36	R 8	NONE						
0	37	H 4	NONE						
5	38	H11	GOOD	1.1533	10.0374	1.2378	1.7209	1.2334	1.1533
5	39	D 5	GOOD	1.1396	-7.8898	0.4558	0.0390	-10.0427	1.1396
5	40	L 6	GOOD	1.1246	0.5383	3.0308	6.6715	4.6105	1.1246
5	41	D10	GOOD	1.1386	7.1776	0.1281	0.7643	10.9596	1.1386
5	42	G14	GOOD	1.1376	-31.0517	-0.4071	-0.3482	2.7353	1.1868
3	43	H13	GOOD	1.1103	-6.3771	-5.5216	-5.3248	-10.7591	1.1408
2	44	C 8	GOOD	1.1110	-13.4534	-0.9751	-1.0940	-8.2320	1.1536
0	45	H 3	NONE						
4	46	N 8	GOOD	1.1112	-9.0825	-2.5030	-0.8074	0.8091	1.1517
2	47	E11	GOOD	1.1497	33.1652	8.1079	7.2162	9.6690	1.1497
4	48	L11	GOOD	1.1453	4.3693	3.2084	5.7055	28.2356	1.1453
5	49	E 5	GOOD	1.1457	24.7318	1.2148	1.6049	10.2697	1.1457
0	50	L 5	NONE						
AVG. OF ABSOLUTE VALUES OF GOOD THIMBLES ONLY				1.1305	9.91	1.42	2.31	7.89	

FORM 0113 (02/83)

SYMMETRIC THIMBLE COMPARISON C12 MAP567 10/24/88 D-202 11949MWD/MTU 91.03%HFP 51P 1 B-45 FCFM

THMBL	LOC	INTEGRAL	THMBL	LOC	INTEGRAL	RATIO
1	M 3	0.32729E+02	10	D 3	0.31829E+02	1.0283
10	D 3	0.31829E+02	1	M 3	0.32729E+02	.97251
19	G 9	0.59574E+02	20	G 7	0.60000E+02	.99290
19	G 9	0.59574E+02	28	J 7	0.61111E+02	.97485
20	G 7	0.60000E+02	19	G 9	0.59574E+02	1.0071
20	G 7	0.60000E+02	28	J 7	0.61111E+02	.98182
28	J 7	0.61111E+02	19	G 9	0.59574E+02	1.0258
28	J 7	0.61111E+02	20	G 7	0.60000E+02	1.0185
44	C 8	0.63167E+02	46	N 8	0.62863E+02	1.0048
46	N 8	0.62863E+02	44	C 8	0.63167E+02	.99518
47	E11	0.73963E+02	48	L11	0.71274E+02	1.0377
47	E11	0.73963E+02	49	E 5	0.69596E+02	1.0627
48	L11	0.71274E+02	47	E11	0.73963E+02	.96365
48	L11	0.71274E+02	49	E 5	0.69596E+02	1.0241
49	E 5	0.69596E+02	47	E11	0.73963E+02	.94096
49	E 5	0.69596E+02	48	L11	0.71274E+02	.97645

177

MAX FQT/K(Z) C12 MAP567 10/24/88 D-202 11949MWD/MTU 91.03%HFP 51P 1 B-45 FCFM

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.701	0.699	0.712							1
2					1.600	1.719	1.719	1.469	1.748	1.748	1.552					2
3				1.105	1.861	1.634	1.356	1.863	1.375	1.641	1.842	1.089				3
4			1.022	1.491	1.658	1.316	1.582	1.285	1.593	1.326	1.648	1.486	1.025			4
5		1.518	1.816	1.658	1.374	1.900	1.617	1.282	1.612	1.887	1.360	1.661	1.838	1.539		5
6		1.717	1.624	1.342	1.971	1.277	1.278	1.893	1.271	1.260	1.890	1.333	1.625	1.729		6
7	0.716	1.744	1.382	1.593	1.672	1.339	1.521	1.540	1.489	1.320	1.622	1.585	1.367	1.732	0.705	7
8	0.700	1.484	1.874	1.284	1.316	1.958	1.567	1.266	1.557	1.926	1.301	1.276	1.877	1.472	0.701	8
9	0.687	1.703	1.343	1.579	1.633	1.340	1.524	1.555	1.516	1.329	1.625	1.576	1.352	1.711	0.696	9
10		1.692	1.614	1.328	1.921	1.277	1.293	1.928	1.296	1.290	1.941	1.338	1.620	1.710		10
11		1.524	1.810	1.646	1.397	1.914	1.635	1.311	1.672	1.974	1.422	1.676	1.809	1.516		11
12			1.040	1.508	1.725	1.353	1.601	1.285	1.596	1.368	1.694	1.499	1.031			12
13				1.072	1.823	1.637	1.358	1.818	1.345	1.631	1.822	1.073				13
14					1.534	1.737	1.657	1.455	1.736	1.730	1.530					14
15							0.708	0.711	0.712							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

ASSEMBLY RELATIVE POWER C12 MAP567 10/24/88 D-202 11949MWD/MTU 91.03%HFP 51P 1 B-45 FCFM

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.226	0.252	0.231							1
2					0.825	1.041	1.114	0.959	1.129	1.053	0.806					2
3				0.518	1.255	1.169	1.004	1.350	1.020	1.177	1.234	0.504				3
4			0.488	0.964	1.212	0.979	1.134	0.947	1.147	0.986	1.209	0.962	0.489			4
5		0.789	1.205	1.203	1.032	1.385	1.152	0.948	1.154	1.381	1.026	1.205	1.229	0.799		5
6		1.040	1.157	0.987	1.422	0.975	0.955	1.380	0.953	0.971	1.380	0.983	1.166	1.041		6
7	0.229	1.117	1.010	1.147	1.184	0.979	1.132	1.147	1.120	0.963	1.158	1.141	1.005	1.112	0.229	7
8	0.249	0.957	1.340	0.949	0.967	1.403	1.155	0.965	1.147	1.393	0.959	0.946	1.348	0.954	0.255	8
9	0.225	1.105	0.994	1.134	1.157	0.972	1.142	1.142	1.114	0.973	1.161	1.137	1.003	1.109	0.227	9
10		1.034	1.149	0.982	1.398	0.974	0.964	1.393	0.964	0.985	1.417	0.991	1.165	1.035		10
11		0.800	1.221	1.215	1.055	1.395	1.161	0.965	1.182	1.427	1.075	1.229	1.224	0.794		11
12			0.492	0.977	1.257	1.001	1.144	0.944	1.137	1.007	1.233	0.957	0.485			12
13				0.506	1.226	1.174	0.996	1.311	0.992	1.157	1.220	0.503				13
14					0.802	1.045	1.072	0.944	1.117	1.044	0.797					14
15							0.229	0.255	0.228							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

ASM'Y RELATIVE POWER: PRED/MEAS/DIFF C12 MAP567 10/24/88 D-202 11949MWD/MTU 91.03%HFP 51P 1 B-45 FCFM

					0.232.	0.259.	0.232.							
					0.226.	0.252.	0.231.							
					-2.85.	-2.84.	-0.72.							
				0.810.	1.057.	1.132.	0.974.	1.132.	1.057.	0.810.				
				0.825.	1.041.	1.114.	0.959.	1.129.	1.053.	0.806.				
				1.79.	-1.52.	-1.53.	-1.58.	-0.29.	-0.33.	-0.58.				
			0.510.	1.239.	1.177.	1.021.	1.371.	1.021.	1.177.	1.239.	0.510.			
			0.518.	1.255.	1.169.	1.004.	1.350.	1.020.	1.177.	1.234.	0.504.			
			1.57.	1.25.	-0.70.	-1.66.	-1.57.	-0.04.	0.01.	-0.41.	-1.13.			
		0.492.	0.961.	1.203.	0.980.	1.141.	0.954.	1.141.	0.980.	1.203.	0.961.	0.492.		
		0.488.	0.964.	1.212.	0.979.	1.134.	0.947.	1.147.	0.986.	1.209.	0.962.	0.489.		
		-0.76.	0.34.	0.78.	-0.14.	-0.64.	-0.69.	0.48.	0.56.	0.56.	0.18.	-0.69.		
	0.807.	1.233.	1.198.	1.011.	1.364.	1.150.	0.951.	1.150.	1.364.	1.011.	1.198.	1.233.	0.807.	
	0.789.	1.205.	1.203.	1.032.	1.385.	1.152.	0.948.	1.154.	1.381.	1.026.	1.205.	1.229.	0.799.	
	-2.23.	-2.26.	0.39.	2.09.	1.55.	0.20.	-0.30.	0.38.	1.29.	1.42.	0.54.	-0.33.	-1.01.	
	1.052.	1.171.	0.976.	1.364.	0.961.	0.958.	1.390.	0.958.	0.961.	1.364.	0.976.	1.171.	1.052.	
	1.040.	1.157.	0.987.	1.422.	0.975.	0.955.	1.380.	0.953.	0.971.	1.380.	0.983.	1.166.	1.041.	
	-1.15.	-1.22.	1.09.	4.27.	1.50.	-0.33.	-0.71.	-0.53.	1.08.	1.20.	0.70.	-0.41.	-1.10.	
0.231.	1.125.	1.014.	1.137.	1.149.	0.964.	1.136.	1.160.	1.136.	0.964.	1.149.	1.137.	1.014.	1.125.	0.231.
0.229.	1.117.	1.010.	1.147.	1.184.	0.979.	1.132.	1.147.	1.120.	0.963.	1.158.	1.141.	1.005.	1.112.	0.229.
-0.65.	-0.74.	-0.42.	0.88.	3.06.	1.54.	-0.34.	-1.06.	-1.48.	-0.10.	0.76.	0.35.	-0.89.	-1.16.	-0.89.
0.257.	0.968.	1.362.	0.949.	0.951.	1.391.	1.158.	0.982.	1.158.	1.391.	0.951.	0.949.	1.362.	0.968.	0.257.
0.249.	0.957.	1.340.	0.949.	0.967.	1.403.	1.155.	0.965.	1.147.	1.393.	0.959.	0.946.	1.348.	0.954.	0.255.
-3.43.	-1.18.	-1.62.	-0.00.	1.63.	0.92.	-0.28.	-1.79.	-0.95.	0.16.	0.77.	-0.39.	-0.99.	-1.48.	-0.88.
0.231.	1.125.	1.014.	1.137.	1.149.	0.964.	1.136.	1.160.	1.136.	0.964.	1.149.	1.137.	1.014.	1.125.	0.231.
0.225.	1.105.	0.994.	1.134.	1.157.	0.972.	1.142.	1.142.	1.114.	0.973.	1.161.	1.137.	1.003.	1.109.	0.227.
-2.37.	-1.80.	-1.94.	-0.26.	0.68.	0.82.	0.48.	-1.56.	-1.98.	0.91.	1.07.	0.02.	-1.06.	-1.46.	-1.68.
	1.052.	1.171.	0.976.	1.364.	0.961.	0.958.	1.390.	0.958.	0.961.	1.364.	0.976.	1.171.	1.052.	
	1.034.	1.149.	0.982.	1.398.	0.974.	0.964.	1.393.	0.964.	0.985.	1.417.	0.991.	1.165.	1.035.	
	-1.77.	-1.86.	0.53.	2.50.	1.37.	0.57.	0.17.	0.59.	2.54.	3.88.	1.49.	-0.53.	-1.66.	
	0.807.	1.233.	1.198.	1.011.	1.364.	1.150.	0.951.	1.150.	1.364.	1.011.	1.198.	1.233.	0.807.	
	0.800.	1.221.	1.215.	1.055.	1.395.	1.161.	0.965.	1.182.	1.427.	1.075.	1.229.	1.224.	0.794.	
	-0.88.	-0.92.	1.41.	4.32.	2.31.	0.97.	1.48.	2.83.	4.61.	6.27.	2.57.	-0.75.	-1.62.	
		0.492.	0.961.	1.203.	0.980.	1.141.	0.954.	1.141.	0.980.	1.203.	0.961.	0.492.		
		0.492.	0.977.	1.257.	1.001.	1.144.	0.944.	1.137.	1.007.	1.233.	0.957.	0.485.		
		-0.08.	1.73.	4.49.	2.12.	0.25.	-1.06.	-0.38.	2.78.	2.53.	-0.40.	-1.40.		
			0.510.	1.239.	1.177.	1.021.	1.371.	1.021.	1.177.	1.239.	0.510.			
			0.506.	1.226.	1.174.	0.996.	1.311.	0.992.	1.157.	1.220.	0.503.			
			-0.67.	-1.13.	-0.22.	-2.39.	-4.37.	-2.79.	-1.71.	-1.56.	-1.39.			
				0.810.	1.057.	1.132.	0.974.	1.132.	1.057.	0.810.				
				0.802.	1.045.	1.072.	0.944.	1.117.	1.044.	0.797.				
				-1.06.	-1.08.	-5.28.	-3.11.	-1.30.	-1.24.	-1.64.				
					0.232.	0.259.	0.232.							
					0.229.	0.255.	0.228.							

-1.57. -1.63. -1.62.

181

A QUARTER CORE AVERAGED ASSEMBLY RELATIVE POWER C12 MAP567 10/24/88 D-202 11949MWD/MTU 91.03%HFP 51P 1 B-45 FCFM

	H	G	F	E	D	C	B	A	
1	0.982 0.965 -1.787	1.158 1.151 -0.616	1.391 1.398 0.540	0.951 0.963 1.200	0.949 0.947 -0.195	1.362 1.344 -1.309	0.968 0.955 -1.328	0.257 0.252 -2.153	1
2	1.160 1.144 -1.310	1.136 1.127 -0.828	0.964 0.972 0.795	1.149 1.165 1.392	1.137 1.140 0.249	1.014 1.003 -1.079	1.125 1.110 -1.293	0.231 0.228 -1.398	2
3	1.390 1.387 -0.269	0.958 0.959 0.074	0.961 0.977 1.623	1.364 1.404 2.961	0.976 0.986 0.955	1.171 1.159 -1.006	1.052 1.037 -1.422		3
4	0.951 0.956 0.592	1.150 1.162 1.096	1.364 1.397 2.440	1.011 1.047 3.525	1.198 1.213 1.225	1.233 1.220 -1.066	0.807 0.795 -1.435		4
5	0.954 0.945 -0.874	1.141 1.140 -0.073	0.980 0.993 1.331	1.203 1.228 2.094	0.961 0.965 0.461	0.492 0.488 -0.732			5
6	1.371 1.331 -2.968	1.021 1.003 -1.723	1.177 1.169 -0.657	1.239 1.234 -0.461	0.510 0.508 -0.407				6
7	0.974 0.952 -2.348	1.132 1.108 -2.100	1.057 1.046 -1.044	0.810 0.807 -0.374					7
8	0.259 0.254 -2.236	0.232 0.228 -1.690							8
	H	G	F	E	D	C	B	A	

PRED
MES
DIF

FORM 0113 (02/83)

FQN C12 MAP567 10/24/88 D-202 11949MWD/MTU 91.03%HFP 51P 1 B-45 FCFM

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.623	0.622	0.632							1
2					1.420	1.545	1.546	1.331	1.566	1.556	1.386					2
3				1.014	1.708	1.511	1.247	1.699	1.258	1.518	1.666	0.973				3
4			0.948	1.375	1.532	1.221	1.452	1.198	1.463	1.230	1.522	1.369	0.944			4
5		1.398	1.678	1.532	1.276	1.754	1.499	1.198	1.494	1.741	1.263	1.535	1.698	1.417		5
6		1.546	1.502	1.245	1.821	1.183	1.176	1.755	1.176	1.168	1.746	1.237	1.503	1.541		6
7	0.637	1.567	1.242	1.464	1.551	1.229	1.386	1.412	1.381	1.212	1.505	1.456	1.235	1.559	0.628	7
8	0.623	1.343	1.684	1.197	1.228	1.795	1.423	1.169	1.427	1.788	1.214	1.190	1.680	1.334	0.625	8
9	0.609	1.527	1.235	1.451	1.515	1.230	1.414	1.418	1.376	1.220	1.508	1.448	1.231	1.539	0.620	9
10		1.550	1.492	1.232	1.775	1.183	1.197	1.782	1.197	1.195	1.794	1.241	1.498	1.557		10
11		1.390	1.662	1.521	1.297	1.767	1.515	1.225	1.550	1.822	1.321	1.549	1.672	1.396		11
12			0.937	1.385	1.594	1.255	1.470	1.198	1.465	1.269	1.565	1.364	0.935			12
13				0.995	1.686	1.512	1.241	1.652	1.230	1.508	1.685	0.998				13
14					1.406	1.567	1.485	1.314	1.559	1.541	1.410					14
15							0.628	0.633	0.634							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

CALCULATED LOCAL PEAKING FACTORS C12 MAP567 10/24/88 D-202 11949MWD/MTU 91.03%HFP 51P 1 B-45 FCFM

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							1.704	1.524	1.704							1
2					1.481	1.281	1.188	1.184	1.187	1.281	1.481					2
3				1.657	1.156	1.085	1.061	1.075	1.061	1.085	1.156	1.657				3
4			1.645	1.214	1.066	1.059	1.054	1.043	1.054	1.059	1.066	1.214	1.645			4
5		1.483	1.158	1.066	1.068	1.075	1.095	1.045	1.094	1.075	1.068	1.066	1.158	1.482		5
6		1.281	1.086	1.060	1.076	1.049	1.060	1.084	1.060	1.049	1.076	1.060	1.086	1.281		6
7	1.703	1.188	1.061	1.053	1.095	1.055	1.056	1.064	1.056	1.055	1.095	1.052	1.061	1.187	1.703	7
8	1.524	1.184	1.075	1.042	1.047	1.085	1.066	1.030	1.066	1.085	1.047	1.042	1.075	1.183	1.524	8
9	1.704	1.188	1.061	1.052	1.095	1.055	1.056	1.064	1.056	1.055	1.095	1.052	1.061	1.187	1.703	9
10		1.281	1.086	1.060	1.076	1.049	1.060	1.084	1.060	1.049	1.076	1.060	1.086	1.281		10
11		1.482	1.158	1.066	1.068	1.075	1.094	1.045	1.094	1.075	1.068	1.066	1.158	1.482		11
12			1.645	1.214	1.066	1.059	1.054	1.043	1.054	1.059	1.066	1.214	1.645			12
13				1.657	1.156	1.085	1.061	1.075	1.061	1.085	1.156	1.657				13
14					1.481	1.281	1.188	1.184	1.187	1.281	1.481					14
15							1.704	1.524	1.704							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

185

NUCLEAR F-DELTA-H (FDHN) C12 MAP567 10/24/88 D-202 11949MWD/MTU 91.03%HFP 51P 1 B-45 FCFM

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.384	0.384	0.393							1
2					1.222	1.334	1.324	1.136	1.340	1.350	1.193					2
3				0.858	1.451	1.268	1.065	1.451	1.083	1.277	1.427	0.835				3
4			0.803	1.171	1.292	1.036	1.195	0.988	1.208	1.044	1.289	1.169	0.803			4
5		1.170	1.395	1.282	1.102	1.489	1.261	0.991	1.263	1.486	1.095	1.284	1.422	1.184		5
6		1.333	1.257	1.046	1.530	1.023	1.012	1.496	1.010	1.019	1.485	1.042	1.267	1.333		6
7	0.391	1.326	1.071	1.207	1.297	1.033	1.196	1.221	1.183	1.016	1.268	1.201	1.066	1.320	0.390	7
8	0.379	1.133	1.440	0.989	1.012	1.522	1.231	0.994	1.223	1.511	1.003	0.985	1.449	1.128	0.389	8
9	0.384	1.312	1.055	1.193	1.267	1.026	1.206	1.215	1.177	1.027	1.272	1.197	1.064	1.316	0.387	9
10		1.325	1.248	1.041	1.504	1.022	1.022	1.509	1.022	1.034	1.524	1.051	1.265	1.326		10
11		1.185	1.414	1.295	1.126	1.500	1.270	1.008	1.294	1.534	1.147	1.310	1.416	1.176		11
12			0.808	1.187	1.340	1.060	1.205	0.984	1.198	1.067	1.314	1.162	0.798			12
13				0.839	1.417	1.274	1.057	1.410	1.053	1.255	1.411	0.833				13
14					1.187	1.339	1.273	1.118	1.326	1.337	1.180					14
15							0.390	0.389	0.389							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

PERCENT AXIAL OFFSET TOWARD TOP OF ASSEMBLY C12 MAP567 10/24/88 D-202 11949MWD/MTU 91.03%HFP 51P 1 B-45 FCFM

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							39.2	39.2	39.1							1
2					-1.0	-2.4	-0.6	0.1	0.2	-1.6	-1.5					2
3				-2.0	-2.1	-3.3	-2.9	-2.8	-2.5	-3.2	-2.0	-1.0				3
4			-3.0	-2.4	-2.6	-3.1	-4.4	-4.4	-4.4	-3.5	-2.8	-2.1	-2.1			4
5		-4.0	-4.2	-4.0	-3.2	-3.5	-3.9	-4.2	-3.5	-3.1	-2.4	-3.2	-2.9	-2.4		5
6		-2.5	-3.6	-4.0	-4.6	-3.3	-2.6	-2.7	-2.8	-2.9	-2.9	-2.9	-2.7	-1.1		6
7	39.2	-0.5	-2.3	-4.3	-4.1	-3.5	-1.7	-2.2	-2.8	-3.8	-3.3	-3.4	-1.7	1.1	39.6	7
8	38.8	0.0	-3.1	-4.0	-3.9	-2.7	-1.6	-2.6	-2.7	-3.5	-4.1	-3.6	-2.1	1.9	39.6	8
9	39.2	-0.7	-2.8	-3.9	-3.1	-3.4	-2.9	-2.4	-2.5	-3.6	-3.5	-3.9	-2.2	0.3	39.0	9
10		-1.9	-3.0	-3.1	-3.3	-2.9	-2.9	-2.8	-3.1	-3.1	-3.2	-3.1	-3.4	-2.1		10
11		-1.5	-1.8	-2.8	-3.6	-3.5	-3.4	-3.8	-4.2	-4.6	-2.1	-2.7	-2.9	-2.8		11
12			-0.6	-2.0	-4.2	-3.9	-4.4	-4.0	-4.3	-3.6	-3.2	-2.2	-2.2			12
13				-2.6	-3.2	-3.6	-2.8	-2.4	-2.4	-3.0	-2.7	-2.9				13
14					-2.9	-2.1	-0.2	0.4	-0.3	-2.0	-2.7					14
15							38.4	38.5	38.5							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

FQT*V(Z)/K(Z) FOR 3% BANDS C12 MAP567 10/24/88 D-202 11949MWD/MTU 91.03%HFP 51P 1 B-45 FCFM
FULL CORE SEARCH

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.761	0.760	0.775							1
2					1.746	1.869	1.869	1.597	1.903	1.903	1.693					2
3				1.206	2.030	1.765	1.474	2.025	1.495	1.772	2.008	1.188				3
4			1.112	1.627	1.791	1.424	1.708	1.387	1.720	1.432	1.780	1.622	1.119			4
5		1.640	1.961	1.790	1.484	2.053	1.747	1.385	1.741	2.039	1.469	1.794	1.985	1.667		5
6		1.867	1.754	1.449	2.128	1.379	1.395	2.064	1.377	1.363	2.045	1.440	1.759	1.886		6
7	0.777	1.891	1.499	1.720	1.806	1.446	1.660	1.680	1.616	1.426	1.756	1.712	1.492	1.879	0.762	7
8	0.760	1.609	2.033	1.386	1.421	2.136	1.709	1.368	1.693	2.094	1.405	1.378	2.048	1.593	0.759	8
9	0.749	1.853	1.461	1.705	1.774	1.447	1.660	1.695	1.651	1.436	1.755	1.702	1.475	1.863	0.755	9
10		1.842	1.743	1.434	2.078	1.379	1.398	2.099	1.409	1.393	2.096	1.446	1.750	1.865		10
11		1.663	1.975	1.777	1.508	2.067	1.766	1.416	1.806	2.132	1.536	1.810	1.974	1.650		11
12			1.135	1.645	1.863	1.462	1.729	1.387	1.723	1.477	1.830	1.642	1.128			12
13				1.169	1.981	1.781	1.480	1.981	1.464	1.761	1.973	1.175				13
14					1.667	1.888	1.807	1.583	1.887	1.881	1.653					14
15							0.770	0.773	0.774							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

FQT*V(Z)/K(Z) FOR 5% BANDS C12 MAP567 10/24/88 D-202 11949MWD/MTU 91.03%HFP 51P 1 B-45 FCFM
FULL CORE SEARCH

	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	
1							0.782	0.781	0.797							1
2					1.794	1.920	1.920	1.641	1.955	1.955	1.739					2
3				1.239	2.086	1.814	1.514	2.081	1.536	1.822	2.063	1.221				3
4			1.143	1.671	1.841	1.463	1.756	1.426	1.768	1.472	1.830	1.666	1.150			4
5		1.685	2.016	1.840	1.525	2.110	1.795	1.423	1.789	2.095	1.509	1.844	2.040	1.713		5
6		1.919	1.803	1.490	2.188	1.418	1.433	2.121	1.415	1.401	2.101	1.480	1.807	1.938		6
7	0.798	1.943	1.540	1.768	1.856	1.487	1.705	1.726	1.660	1.465	1.805	1.759	1.533	1.930	0.784	7
8	0.781	1.653	2.089	1.425	1.461	2.195	1.756	1.406	1.740	2.151	1.444	1.417	2.104	1.637	0.780	8
9	0.770	1.904	1.501	1.753	1.823	1.488	1.706	1.742	1.696	1.476	1.804	1.750	1.516	1.914	0.776	9
10		1.892	1.791	1.474	2.136	1.417	1.436	2.157	1.448	1.431	2.155	1.486	1.799	1.917		10
11		1.709	2.029	1.827	1.550	2.125	1.815	1.456	1.856	2.191	1.579	1.860	2.028	1.695		11
12			1.166	1.690	1.915	1.502	1.777	1.426	1.771	1.518	1.880	1.687	1.159			12
13				1.201	2.035	1.830	1.521	2.036	1.504	1.810	2.028	1.207				13
14					1.713	1.940	1.857	1.626	1.939	1.933	1.699					14
15							0.791	0.794	0.795							15
	R	P	N	M	L	K	J	H	G	F	E	D	C	B	A	

FORM 0113 (02/83)

193

MAXIMUM FQT*V(Z)/K(Z) C12 MAP567 10/24/88 D-202 11949MWD/MTU 91.03%HFP 51P 1 B-45 FCFM

AXIAL NODE	3%	SOURCE	5%	SOURCE
1	.99293	F 6	1.0195	F 6
2	.94446	E11	.96976	E11
3	1.0938	E11	1.1231	E11
4	1.1480	E11	1.1787	E11
5	1.7756	H 6	1.8233	H 6
6	1.7941	H 6	1.8424	H 6
7	1.8750	H 6	1.9257	H 6
8	1.9989	K 8	2.0531	K 8
9	2.0698	K 8	2.1261	K 8
10	2.1064	K 8	2.1639	K 8
11	2.1286	K 8	2.1869	K 8
12	2.1360	K 8	2.1947	K 8
13	2.1269	K 8	2.1856	K 8
14	2.1135	K 8	2.1721	K 8
15	2.0977	K 8	2.1560	K 8
16	2.0415	F 8	2.0982	F 8
17	1.9637	F 8	2.0182	F 8
18	2.0211	K 8	2.0772	K 8
19	2.0355	K 8	2.0921	K 8
20	2.0271	K 8	2.0834	K 8
21	2.0270	E10	2.0833	E10
22	2.0172	E10	2.0732	E10
23	2.0109	E10	2.0667	E10
24	1.9975	E10	2.0530	E10
25	1.9827	K 8	2.0377	K 8
26	1.9684	E10	2.0231	E10
27	1.9399	F11	1.9938	F11
28	1.8675	F11	1.9193	F11
29	1.9101	K 8	1.9632	K 8
30	1.9525	F11	2.0067	F11
31	1.9684	F11	2.0230	F11
32	1.9745	F11	2.0294	F11
33	1.9745	F11	2.0294	F11
34	1.9816	F11	2.0367	F11
35	1.9858	F11	2.0410	F11
36	1.9868	F11	2.0420	F11
37	1.9920	F11	2.0473	F11
38	1.9762	F11	2.0311	F11
39	1.9069	F11	1.9598	F11
40	1.9682	L 6	2.0229	L 6
41	2.0195	L 6	2.0756	L 6
42	2.0519	L 6	2.1089	L 6
43	2.0620	L 6	2.1192	L 6
44	2.0784	L 6	2.1361	L 6
45	2.0982	L 6	2.1565	L 6
46	2.1117	L 6	2.1704	L 6
47	2.1216	F11	2.1805	F11
48	2.1286	F11	2.1878	F11
49	2.1169	F11	2.1757	F11
50	2.0473	F11	2.1042	F11
51	2.1094	L 6	2.1680	L 6
52	2.1321	F11	2.1914	F11
53	2.1094	L 6	2.1680	L 6
54	2.0557	F11	2.1128	F11
55	1.9764	F11	2.0313	F11
56	1.8870	L 6	1.9394	L 6
57	1.7463	F11	1.7948	F11

FORM 0113 (02/83)

58	1.6217	L 6	1.6668	L 6
59	.90868	L11	.93393	L11
60	.65944	L11	.67776	L11
61	.55187	E11	.56720	E11