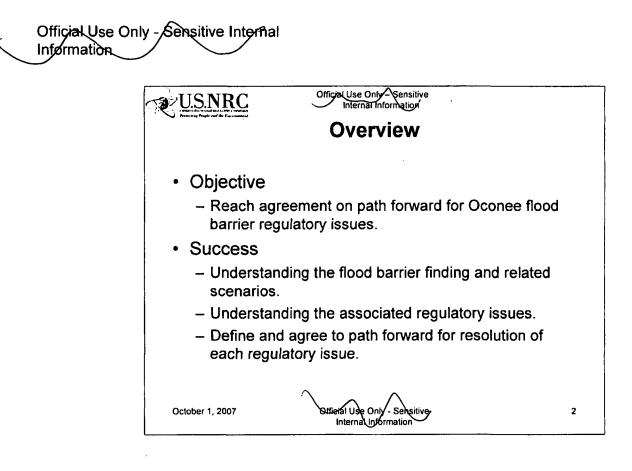


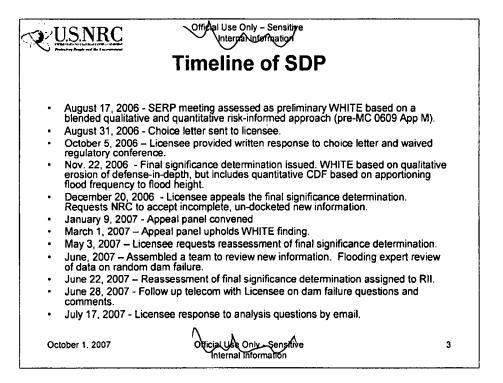
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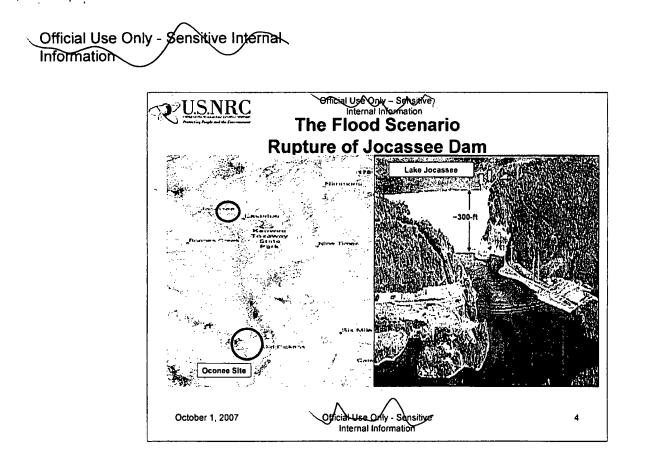
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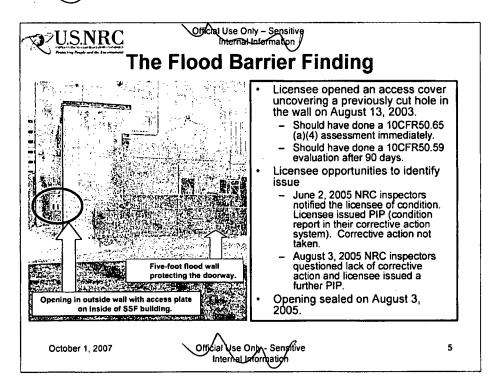


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River miles are approximately 14 miles.

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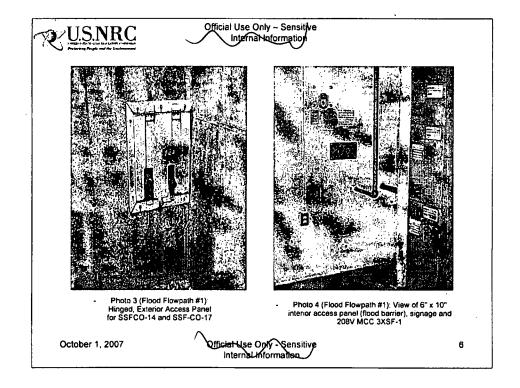


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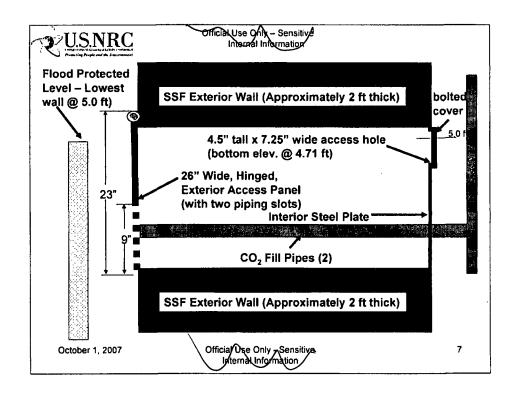


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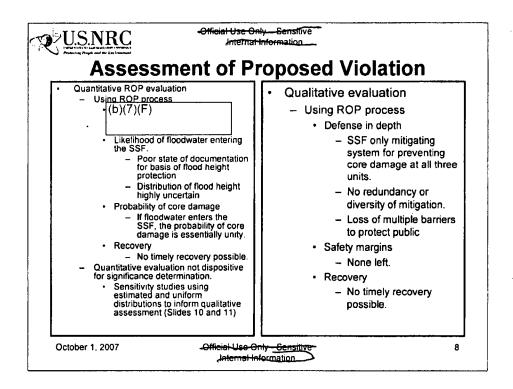
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Note: The licensee surveyed the SSF and associated flood walls and provided an estimate that the lowest level of protection was at 801.0' msl. There was some initial discrepancies on the dimensions when NRC sent the preliminary white finding to the licensee in 2006. In order to resolve these differences, the licensee removed the interior bolted cover last October, and the resident inspectors verified the elevations and dimensions noted above.

Reference points	Elevation (feet msl)
Oconee Yard Grade	796.00
Ground floor of SSF	797.00
Bottom of breached flood barrier	800.71
Top of SSF North flood wall	801.00
Top of SSF South flood wall	801.75

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- Qualitative decision-making attributes are in accordance with numerous NRC guidance documents on risk-informed integrated decision-making (e.g., Regulatory Guide 1.174, SDP Appendix M, SDP IMC 308 (SDP basis document), LIC504, etc...).

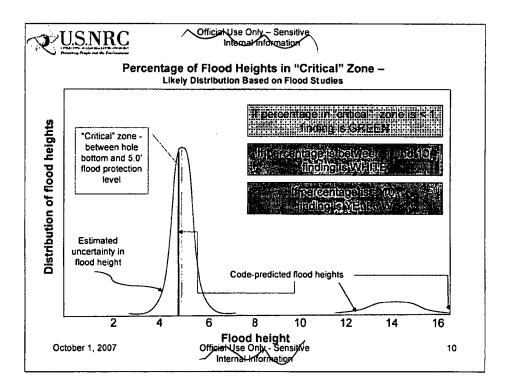
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Review of Data of Random Jocassee Dam Failure	
• Lic	ensee
-	Assumed 3 failures in 220,080 dam-years which yielded a frequency of \sim 1.4 x 10 ^{.5} per year.
• NF	RC .
-	Reviewed the licensee dam failure data.
-	Licensee inappropriately used data for all rockfill, composite rockfill-earthen, and earthen dams over 50-ft matching Jocassee in the denominator with failures of rockfill only dams in the numerator.
-	(b)(7)(F)
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- Correcting Duke's calculation results in a point-estimate of 1.92e-4/yr frequency when properly matching the numerator definition to what Duke used in the denominator of all Dams over 50 ft.

- The staff's best estimate is the Bayesian mean (state of the art approach). The 90 percent credible interval is the [5th, 95th] values. Assessment assumes rockfilled dams only.

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Note: The 1983 study estimated flood level at 4.7 fl. Using the DAMBRK code, the Duke/FERC study in 1992 cited values for the sunny day dam break at 12.51 ft and for the probable maximum flood at 16.82 ft.

Total area under both curves = 1.0. Area under the curve for the 5' flood height approximately 0.8. Area under the curve for the 12' to 16' flood height approximately 0.2.

Change in CDF in terms of Pr $_{\rm flood \, critical \, zone}$, probability of floods occurring in the "critical zone" using simplified risk calc:

ΔCDF = CDF non-conforming - CDF baseline = (IEF Jocasee Break * Pr flood critical zone * CCDP SSF flood unprotected) -(IEF Jocasee Break * Pr flood critical zone * CCDP SSF flood protected) = IEF Jocasee Break * Pr flood critical zone * (CCDP SSF flood unprotected - CCDP SSF flood protected)

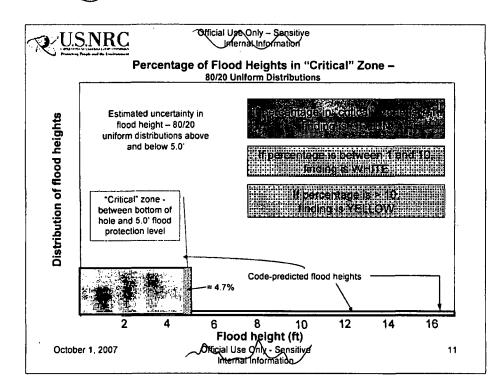
= 1.8E-4/yr * Pr flood critical zone * (1.0 - 0.3)

△CDF = 1.26E-4/yr * Pr flood critical zone

SDP color thresholds in terms of Pr flood critical zone :

White: 1e-6/1.26e-4 = 0.0079 or ≈ 1 percent Yellow 1e-5/1.26e-4 = 0.079 or ≈ 10 percent

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80 percent of flood distributed below 5.0' mark. The 80/20 split is based on the Duke PRA assessment (1990s). The assumption of uniform distributions is provided here only for a relative non-conservative perspective to the previous slide that has a bimodal distribution.

Likelihood of flood between 4.71' and 5.0' is:

0.8 * (3.5"/60") = 0.0466

Using 1.8e-4/yr for Jocassee Dam break frequency and a 0.047 probability of floods in the critical zone, and a nominal SSF unavailability of the SSF (test& maintenance, system unreliability, or human error) yields an estimated delta CDF (full calc not shown) of:

<u>1.26e-4/yr * 0.047 = 5.9e-6/yr</u> White finding

Likely distribution of flood height expected to be greater than 4.7% in the "critical zone."

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NUREG-1742 identified only two IPEEEs that addressed dam failure floods quantitatively – Ft. Calhoun and Diablo Canyon. Everyone else only addressed probable maximum precipitation and screened out dam failure as low probability. Unfortunately, there were few dam failure data sources around back then, so many plants used the estimate published in NUREG/CR-5042. The data source for the estimate in NUREG/CR-5042 was the Oconee PRA - NSAC/60. The calculation in NSAC/60 was done in error and it propagated throughout the industry.

References:

NUREG/CR-5042, "Evaluation of External Hazards to Nuclear Power Plants in the United States.

NUREG-1742, "Perspectives Gained From the Individual Plant Examination of External Events (IPEEE) Program

NSAC/60, "Oconee PRA"