

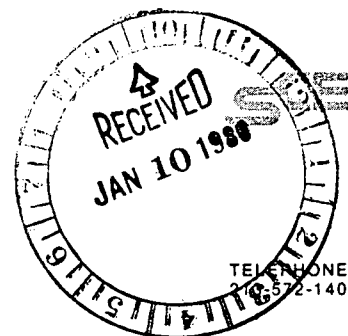
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K. P. BASKIN
MANAGER, GENERATION ENGINEERING

January 3, 1980



U. S. Nuclear Regulatory Commission
Region V
Suite 202, Walnut Creek Plaza
1990 N. California Boulevard
Walnut Creek, California 95696

Attention: R. H. Engelken

Gentlemen:

Subject: IE Bulletin No. 79-02, Revision 2
Docket Nos. 50-361 and 50-362
San Onofre Nuclear Generating Station
Units 2 and 3

Reference: Letter, K. P. Baskin to R. H. Engelken
dated July 8, 1979; re: IE Bulletin 79-02 and
79-02, Revision 1

Your letter of November 8, 1979 forwards IE Bulletin 79-02, Revision 2, "Pipe Support Base Plate Designs Using Concrete Expansion Anchor Bolts" and requests information pertaining to use of the subject bolts in concrete block walls to attach Seismic Category I piping supports.

Attached, in response, is a report from the San Onofre Units 2 and 3 A/E (Bechtel) which addresses the new specific concerns of the subject document and should be considered in conjunction with the referenced previous response.

Should you have any questions or require additional clarification, please contact me.

Very truly yours,

K P Baskin

cc: U. S. Nuclear Regulatory Commission
Office of Inspection & Enforcement
Division of Reactor Construction Inspection
Washington, D. C. 20555

R. Pate, U.S.N.R.C.
Site Inspector
San Onofre Units 2 and 3

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Supplemental Input on Report on Pipe Support Base
Plate Design Using Concrete Expansion Anchor Bolts

(Response to: NRC IE Bulletin No. 79-02, Revision 2, November 8, 1979)

The following text provides supplemental input in response to IE Bulletin 79-02 and addresses new issues identified in Revision 2 of the bulletin dated November 8, 1979. The referenced item numbers are related directly to item numbers in that document. No response is provided herein to items in the revised IE Bulletin which were already addressed in our previous response. However it should be noted that the method for determining the bolt ultimate capacity when considering shear-tension interaction has been revised to reflect the most liberal case per our current practice.

2.The bolt ultimate capacity should account for the effects of shear-tension interaction, minimum edge distance and proper bolt spacing

Response:

Shear-tension interaction is calculated by the square-root-sum of squares of the individual shear and tension and must be equal to or less than the specified allowable design value for the selected expansion anchor.

5. Determine the extent that expansion anchor bolts were used in concrete block (masonry) walls to attach piping supports in Seismic Category I systems (or safety related systems as defined in Revision 1 of IE Bulletin No. 79-02). If expansion anchor bolts were used in concrete block walls:

Response:

Concrete block (masonry) walls are not used as structural elements in Seismic Category I structures in the San Onofre Units 2 and 3 project and therefore no expansion anchor bolts are used to attach Seismic Category I piping supports to concrete block (masonry) walls.

6. Determine the extent that pipe supports with expansion anchor bolts used structural steel shapes instead of base plates. The systems and lines reviewed must be consistent with the criteria of IE Bulletin No. 79-02, Revision 1. If expansion anchor bolts were used as described above, verify

Response:

The design of all Seismic Category I pipe supports which utilize expansion anchor bolts incorporate the use of a base plate at the interface point between the pipe support structural elements and the concrete surface. Therefore, no further investigation is necessary.