

# **EXTENDED DRY STORAGE AND TRANSPORTATION: MODEL FOR EVALUATING VACUUM DRYING ADEQUACY**

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## **DISCLAIMER**

The NRC staff views expressed herein are preliminary and do not constitute a final judgment or determination of the matters addressed or of the acceptability of any licensing action that may be under consideration at the NRC.

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# Introduction

- **Potential excessive residual moisture following incomplete drying of spent nuclear fuel (SNF)**
- **A time-dependent integration model, to assess potential radiolysis, producing oxygen and hydrogen, and potential effects on the integrity of SNF, cladding, internals, and flammability**
- **Interim progress made for the process of model abstraction, model integration, and uncertainty assessments. Quantitative results will be presented in the future.**

# Outline

- **Quantity of Water Remaining after Drying: water reacts with SNF, cladding and internals**
- **Temperature: affects reactions**
- **Radiolysis: produces oxygen and hydrogen; affects reactions; poses flammability potential**
- **Relative Humidity (RH): affects reaction**
- **Oxidation and Hydration of SNF: affect SNF integrity**
- **Cladding Oxidation: affects cladding integrity**

## **Outline (continued)**

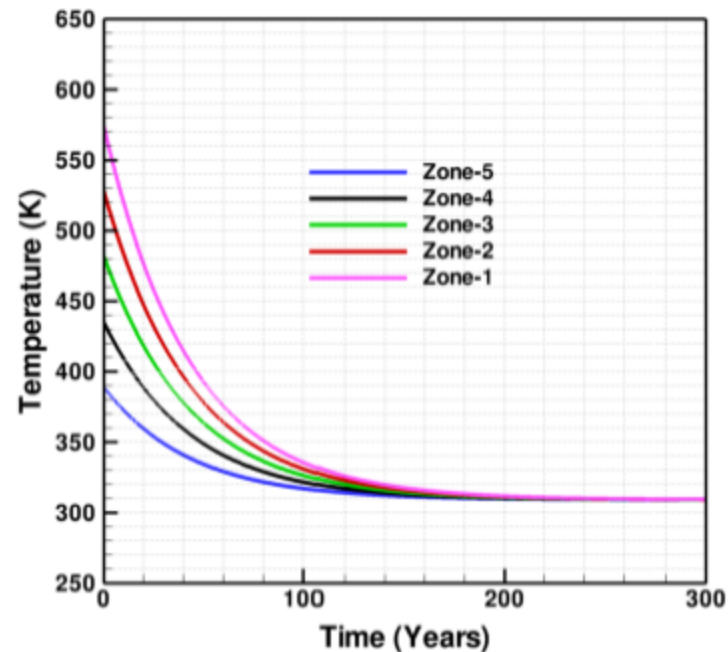
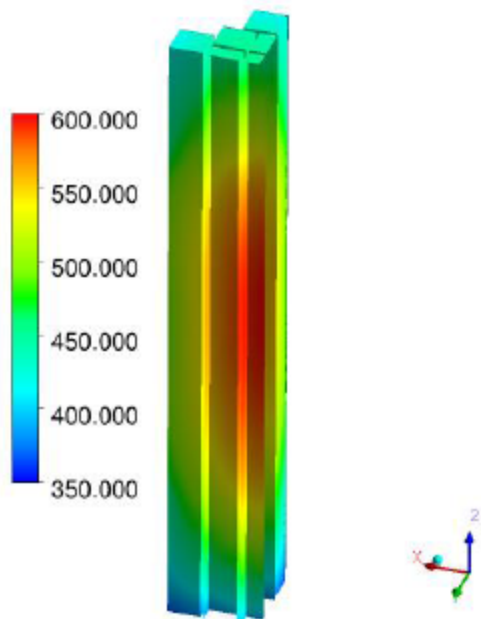
- **Cladding Splitting - Strain Estimate due to SNF Swelling: affects integrity of SNF and cladding**
- **Flammability**
- **Hydrogen-Absorption-Induced Damage**
- **Aqueous Corrosion: affects reactions**
- **Integration and Benchmarking**

## **Quantity of Water Remaining after Drying and Temperature**

- **Quantity of Water Remaining after Drying**
  - **Unbound residual liquid water, unbound water vapor, and water chemically bound to hydroxide and hydrate species**
  - **Properly executed vacuum drying procedure result in:  
1 to 5 moles (0.02 to 0.1 L [0.7 to 3.5 oz]) water inventory**
  - **up to 55 moles (~ 1 L [35 oz]) are conservatively assumed**
- **Temperature**
  - **Spatially distributed and decreases over time**

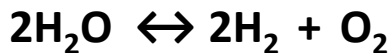
## Temperature (continued)

- **Temperature distribution in the SNF basket assembly (left). The scales for temperature are in K (  $F = 1.8 \text{ K} - 459.4$ ); SNF and cladding in the five zones calculated using mean values of low-end SNF and cladding initial temperatures (right)**



## **Radiolysis and Relative Humidity (RH)**

- **Radiolysis: Global Approximation  
for Various Intermediate Species**



- **Decomposition rate of water by  
radiolysis:  
exponential time function**
- **Recombination – additional  
steps for molecular collision  
needed, compared with  
decomposition**

- **Relative Humidity (RH)**

- **The radiolysis removes water molecules  
by dissociating them into oxygen and  
hydrogen**
- **RH is modified by radiolysis**

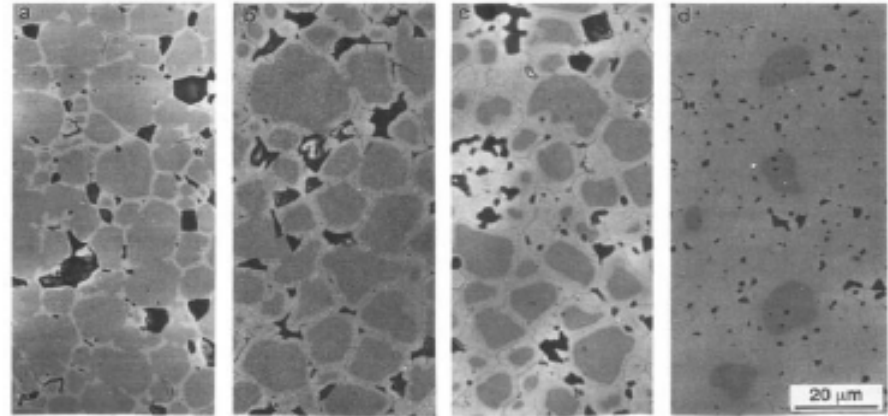


## Oxidation and Hydration of SNF

- Upon cladding breach, the  $\text{UO}_2$  could be oxidized to form:

- $\text{U}_4\text{O}_9$ ,  $\text{U}_3\text{O}_7$ , and  $\text{U}_3\text{O}_8$  in dry air (less than 40 percent RH)

- Hydrated uranium oxides, such as schoepite ( $\text{UO}_3 \cdot x\text{H}_2\text{O}$ ,  $x = 0.5$  to 2), in humid air (greater than 40 percent RH) or in an aqueous environment



Grain boundary oxidation of AM-105 spent nuclear SNF to  $\text{U}_4\text{O}_9$ . Optical ceramographs, as polished: (a) 95 hrs, Bulk O/M = 2.05; (b) 420 hrs, bulk O/M = 2.17; (c) 775.5 hrs, bulk O/M = 2.24; and (d) 1,677 hrs, bulk O/M = 2.31 (Einziger, et al., 1992)

- Chemical Arrhenius-type Kinetics
- Actual Rates are Controlled by Radiolysis Kinetics or Chemical Kinetics

## **Cladding Oxidation, and Cladding Splitting: Strain Estimate due to SNF Swelling**

- **Cladding Oxidation**
  - $\text{Zr} + \text{O}_2 = \text{ZrO}_2$  for dry air and
  - $\text{Zr} + 2\text{H}_2\text{O} = \text{ZrO}_2 + 2\text{H}_2$  for water or humid air (e.g., steam)
  - Model by Hillner, et al (1994) and 8 other similar kinetics
  - Large surface area of cladding
  - Actual Rates Controlled by Radiolysis Kinetics or Chemical Kinetics
- **Cladding Splitting: Strain Estimate due to SNF Swelling**
  - Oxidation of  $\text{UO}_2$  to  $\text{U}_3\text{O}_8$  can generate stress on cladding as  $\text{U}_3\text{O}_8$  swells (36 percent when there is 100 percent conversion to  $\text{U}_3\text{O}_8$ ).
  - Various threshold values of strain are assessed to determine the cladding splitting condition.
  - Observed threshold values:
    - 6.5% strain (100% conversion);
    - 5.1% volume expansion correlation (25 % conversion);
    - 2% strain (50% conversion)

## **Flammability and Hydrogen-Absorption-Induced Damage**

- **Flammability**
  - **The cladding will not absorb radiolysis-generated hydrogen.**
  - **The flammability criterion requires the volume fraction of any flammable gas to be more than 5 percent, with oxygen and ignition.**
- **Hydrogen-Absorption-Induced Damage**
  - **Cladding: Zirconium oxide is expected to limit the absorption of molecular hydrogen:**

**Total possible amount of hydrogen from 55 mole water is assessed.**
  - **Canister Internals: the mechanical properties may or may not be degraded with hydrogen concentration exceeding a threshold value.**

# **Aqueous Corrosion, and Integration and Benchmarking**

- **Aqueous Corrosion**
  - **Aqueous corrosion could occur in vapor when RH is greater than a threshold value: At above the threshold RH**
    - (i) **SCC of the canister's internal structural components could occur in carbon and stainless steels; no relevant data available**
    - (ii) **Shadow corrosion (a form of galvanic corrosion) between cladding and spacer-grid material could occur.**
- **Integration and Benchmarking**
  - **In each time step, all reactions and gas generations are assessed**
  - **Bench marking with long-term demonstration data (e.g., hydrogen amount)**

# Summary

**Program is under development that evaluates:**

- **Time-dependent integrated models for temperature, relative humidity, and radiolysis kinetics to decompose water into oxygen and hydrogen.**
- **Various abstracted models for temperature, radiolysis, relative humidity, and chemical reactions of SNF, cladding and internals.**
- **Time integrated model: in each time step, all reactions and gas generations are assessed.**
- **Assess degradation of SNF, cladding and internals.**
- **Possibility of flammability conditions.**