



Pre-submission Meeting, July 31, 2012
NAC-LWT Amendment for NRU/NRX



Agenda

- Introductions
- NRU/NRX package overview
 - Structural
 - Thermal
 - Shielding
 - Criticality
- Licensing and schedule considerations
- Q&A session

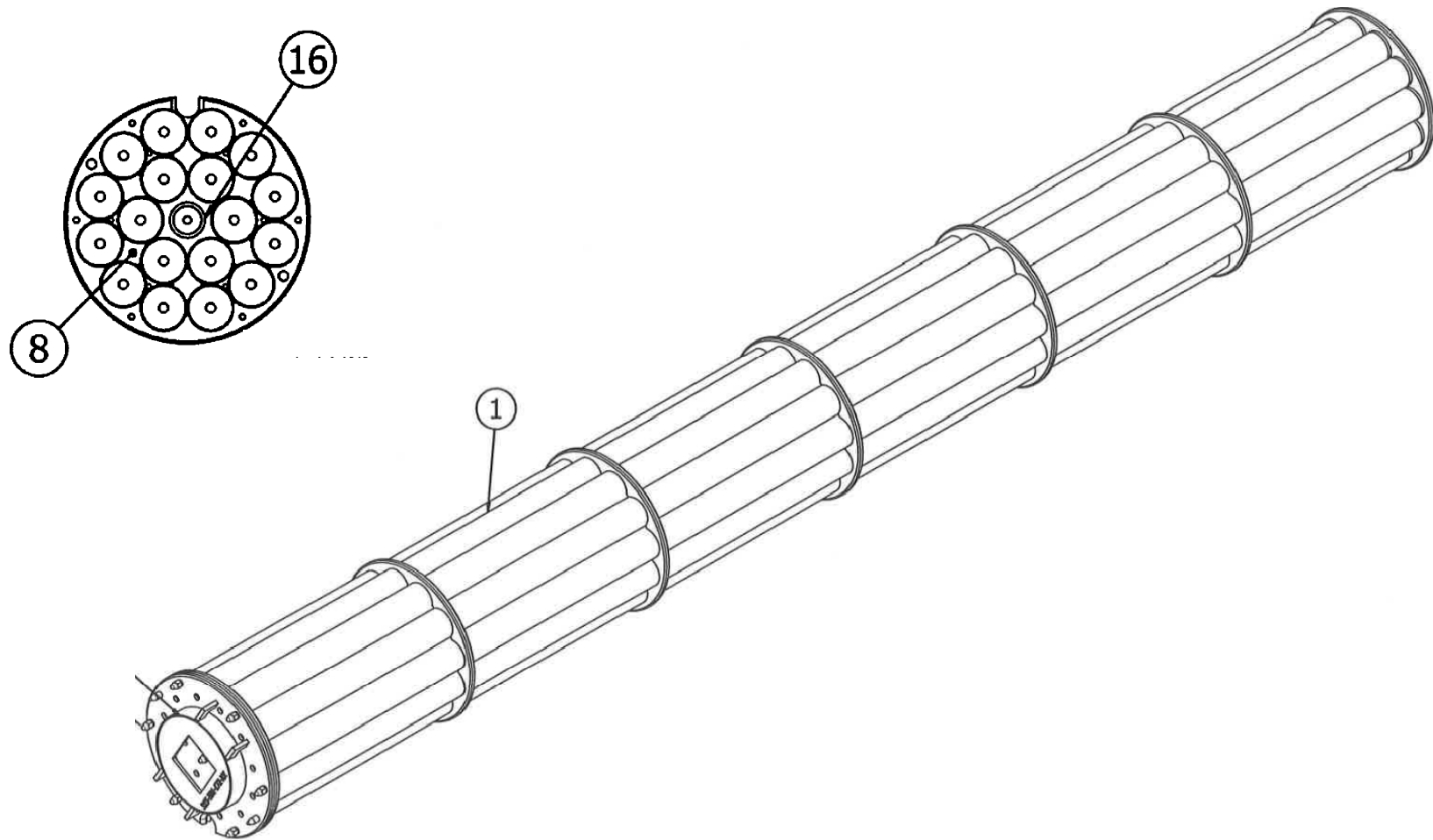
Package Overview

NRU/NRX

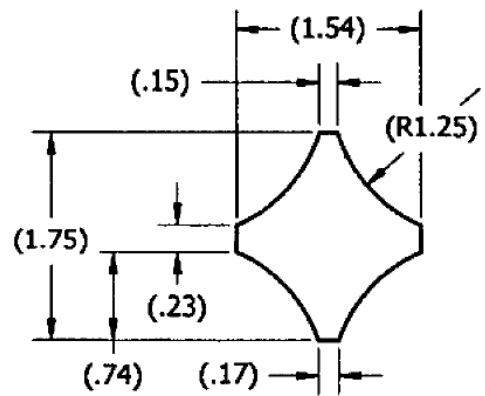
NRU/NRX Package Overview

- Fuel basket is designed to accommodate both the National Research Universal (NRU) and National Research Experimental (NRX) fuel
- Basket is designed to retain any gross particulate from damaged fuel
- Basket accommodates up to 18 NRU or NRX fuel rod bundles
 - NRU bundle consists of 12 fuel rods
 - NRX bundle consists of 7 fuel rods
- Lower spacer used to limit axial movement of the fuel basket

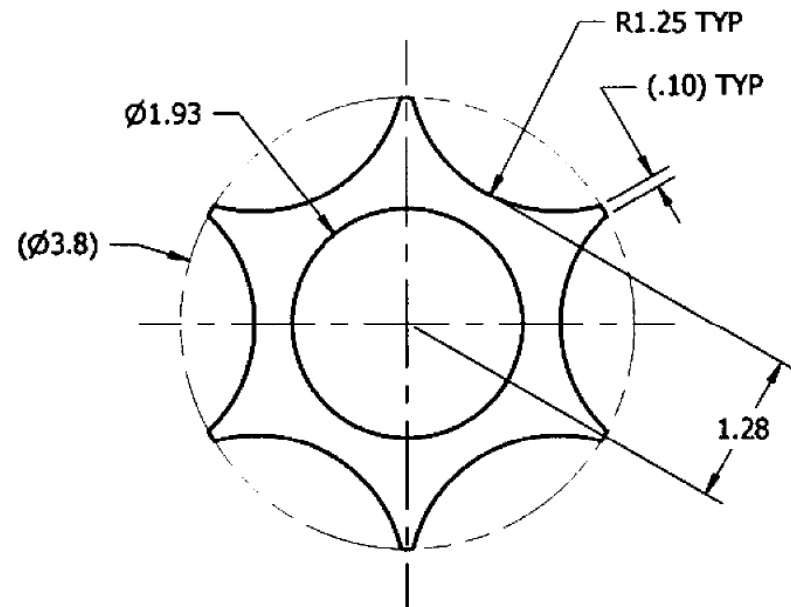
NRU/NRX Package Overview (cont'd)



NRU/NRX Package Overview (cont'd)

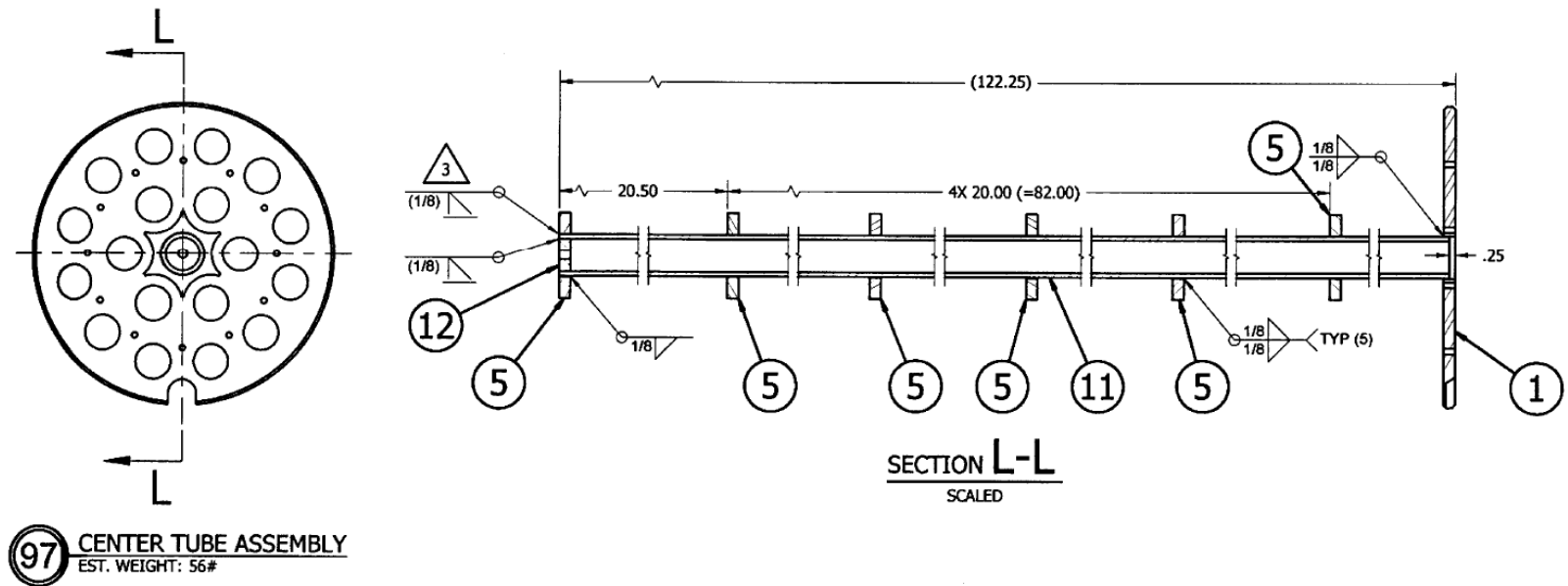


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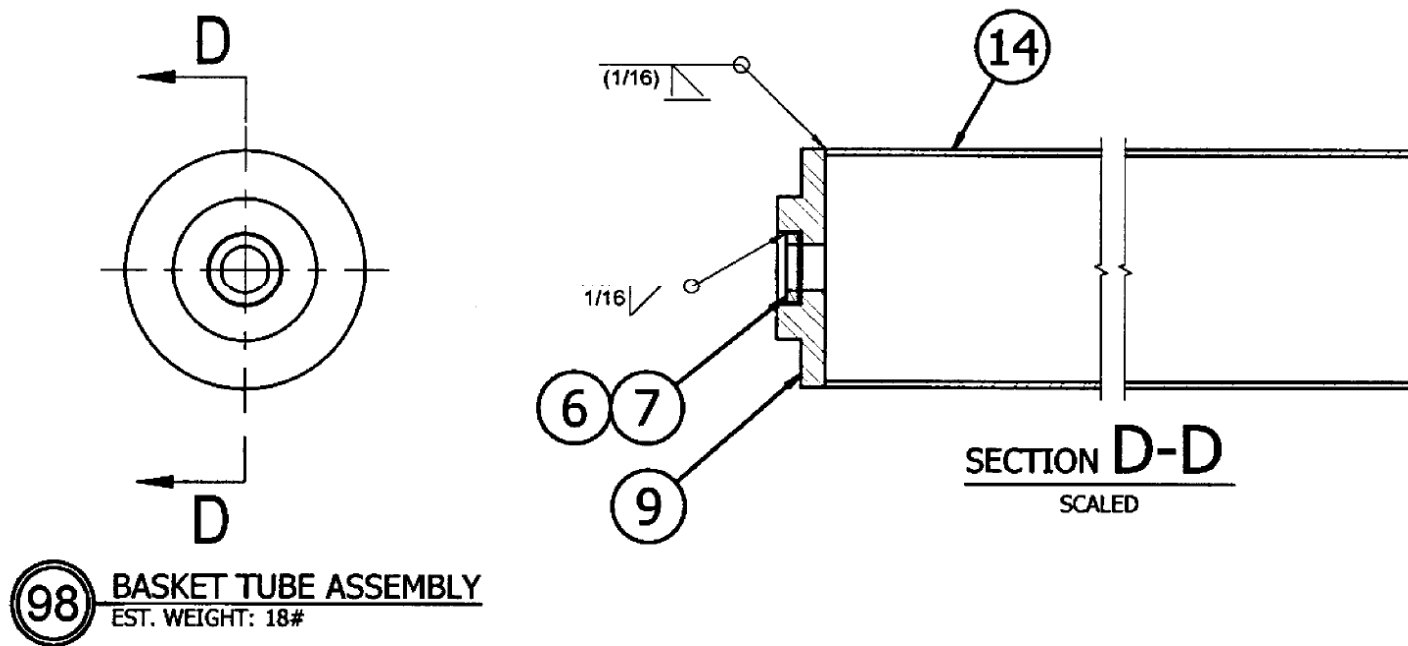


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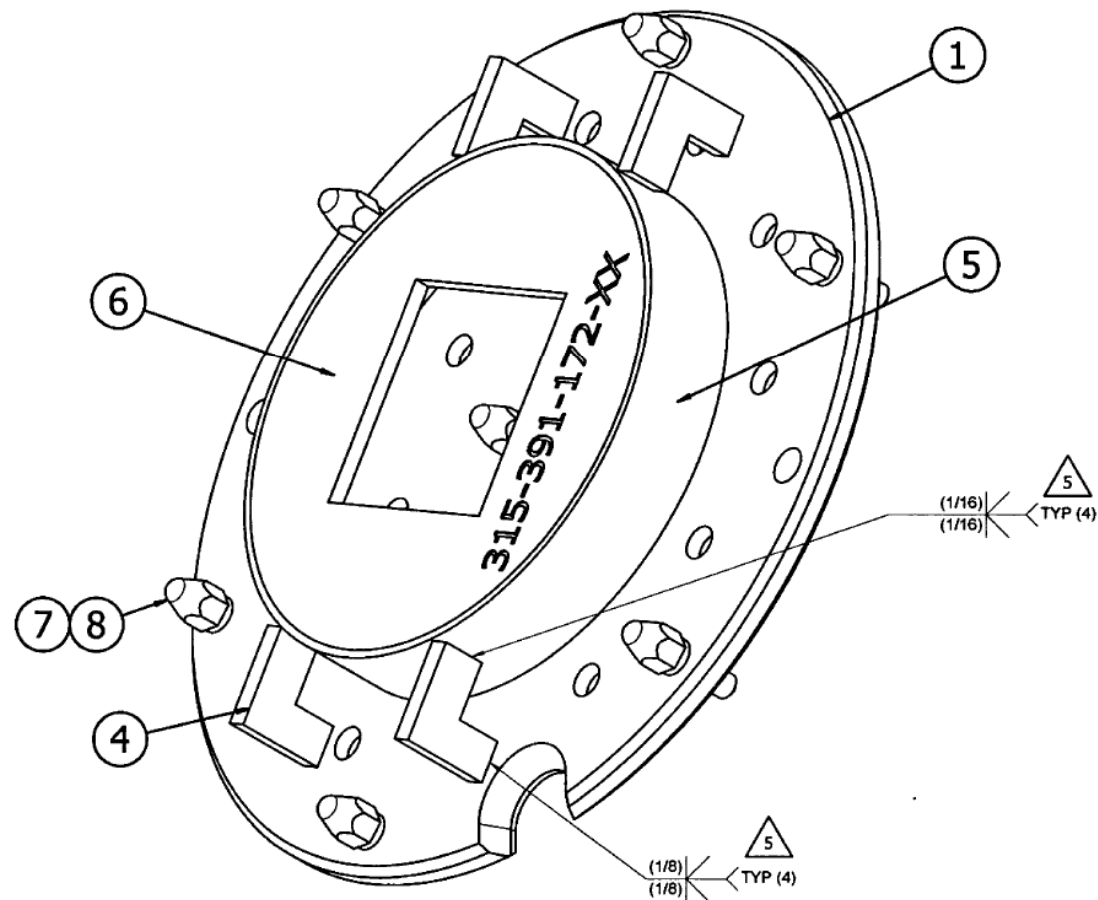
Age Group	Percentage
18-24	100%
25-34	100%
35-44	100%
45-54	100%
55-64	100%
65-74	100%
75-84	100%
85+	100%



NRU/NRX Package Overview (cont'd)



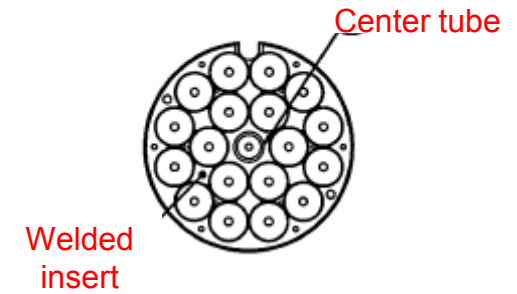
NRU/NRX Package Overview (cont'd)



NRU/NRX Structural Overview

- Maximum of 18 NRU/NRX fuel elements
 - NRU/NRX weight: 11 pounds each
- Each fuel element is contained in a separate basket tube (2.5" OD, 0.06" wall thickness)
- Tubes are joined along their length, and constrained around a structural center tube by 7 disks at a 20.5 inch pitch
- All structural components are comprised of stainless steel type 304
- Total basket assembly weight is 450 lbs.
- Spacer is inserted in cavity to minimize contents motion (115 pounds)
- Total transport contents weight is enveloped by 4000-pound licensed weight
- Cask body evaluation is not required
- Basket is qualified under Subsection NG
 - Weld quality factors are included in the stress evaluation

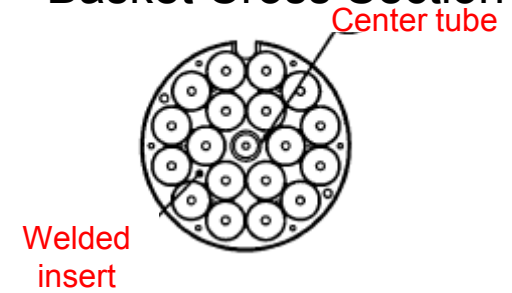
Basket Cross Section



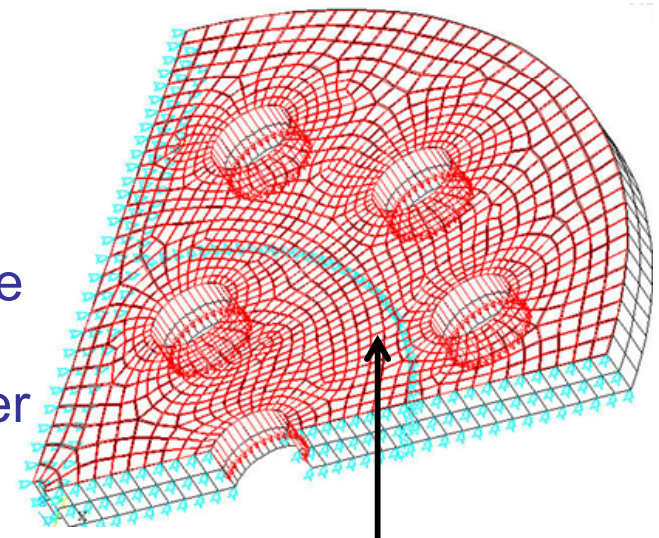
NRU/NRX Structural Overview (cont'd)

- Normal and accident drop conditions for the basket are evaluated using hand calculations
 - Tubes are treated as simply supported beams
 - Buckling evaluated as cylinders using Blake
 - Disk-cavity bearing stress evaluated using Roark
- Bottom end plate for the bottom end drops are evaluated using quarter symmetry FEA model
 - Simulates the effect of load transfer from the tubes to the end supports bearing against the cask cavity
- Top end plate is evaluated using a similar quarter symmetry model for the top end drop

Basket Cross Section



End Plate Model

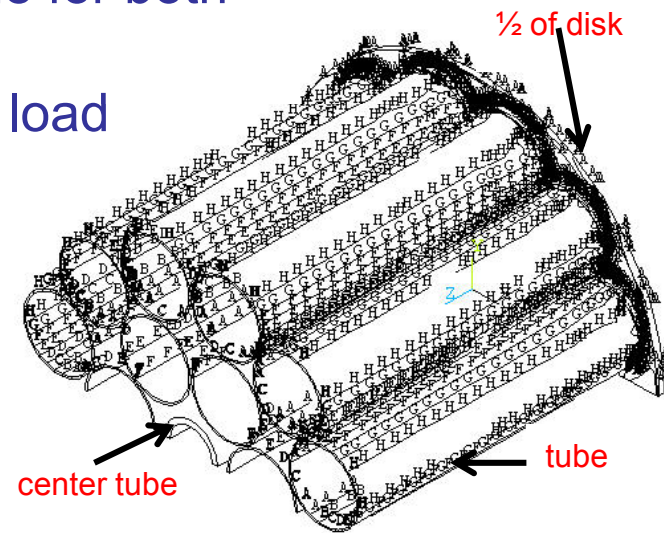


Restraint represents support ring

NRU/NRX Structural Overview (cont'd)

- Thermal stresses are evaluated using quarter symmetry periodic 3D ANSYS model
 - Captures stresses due to radial gradient and the welded components
 - Temperatures are imported from the thermal model
 - Element/node models are the same for both
 - Thermal stress < 2ksi
 - Minimum stress is due to low heat load
- Minimum Safety Factors

Component	Normal Condition	Accident Condition
Basket Assembly	9.71	1.94
Basket Lid	1.85	1.79
Spacer Assembly	6.21	6.32



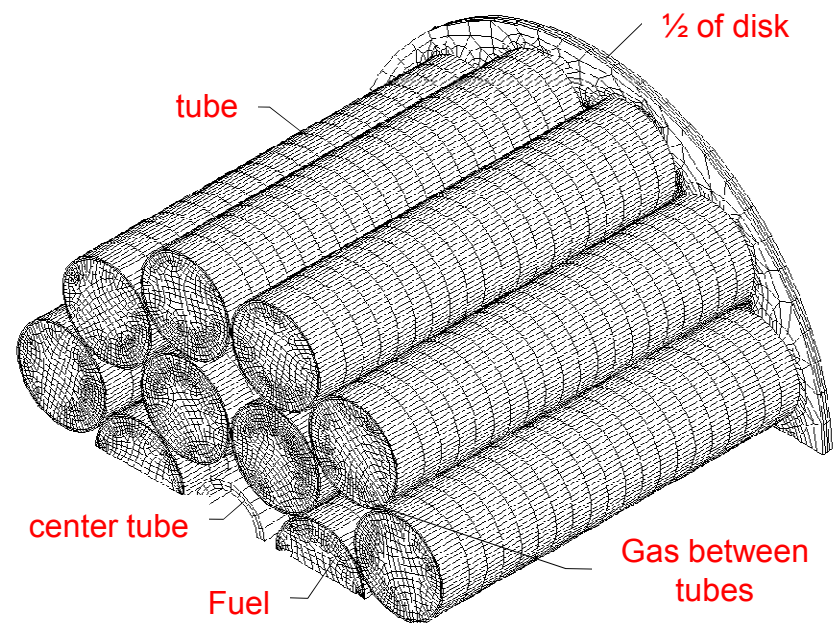
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 B=250.948 D=584.785 F=918.621 H=1252

NRU/NRX Thermal Overview

- LWT is transported in an ISO container used in the current LWT SAR
- LWT cask is backfilled with helium
- Total heat load in the cask cavity is 200 W (bounds actual 171 W)
 - 108 inch active fuel length
 - No peaking factor is required
- The current ANSYS model in the SAR for the LWT cask body and ISO container is used to determine the inner shell surface temperature for the NRU/NRX contents
 - Model was previously used for MTR and SLOWPOKE fuel contents
 - Heat load (200 W) is applied to the cask inner shell surface of the model
 - Insulance is applied to ISO container surface

NRU/NRX Thermal Overview (cont'd)

- Quarter symmetry 3D periodic model used to determine maximum temperatures
- Fuel region is conservatively modeled as helium conduction
- All voids in the basket are modeled as helium conduction
- Radiation matrix models radiation from tube outer surface to cask inner shell
- 0.05 inch radial gap between disks and cask inner shell is modeled with helium
- Cask inner shell temperature is applied to outer layer of nodes of the model
- Maximum normal condition fuel temperature is 182°F
- Fire accident condition is bounded by the 1.26 kW MTR evaluation (385°F)



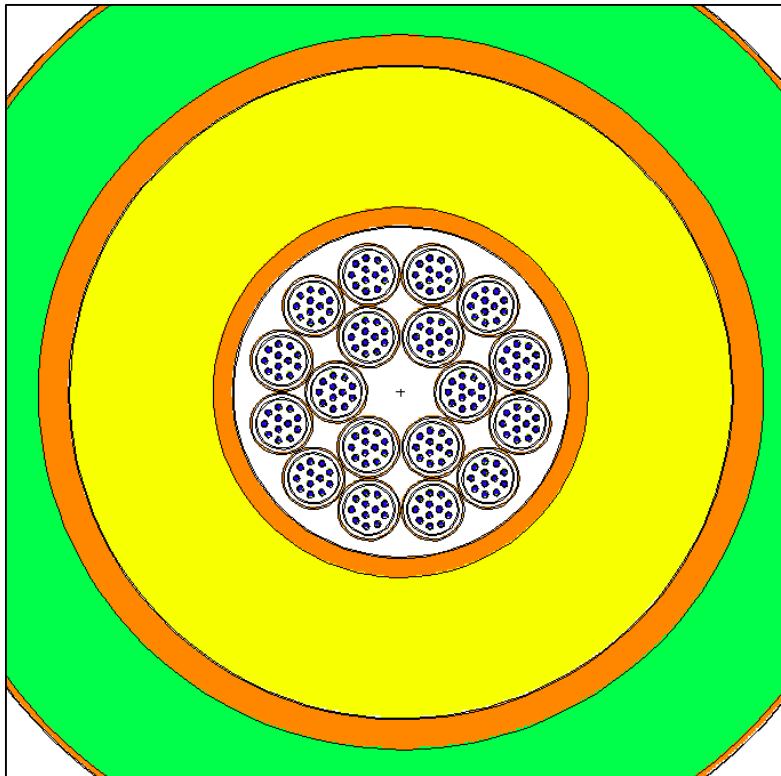
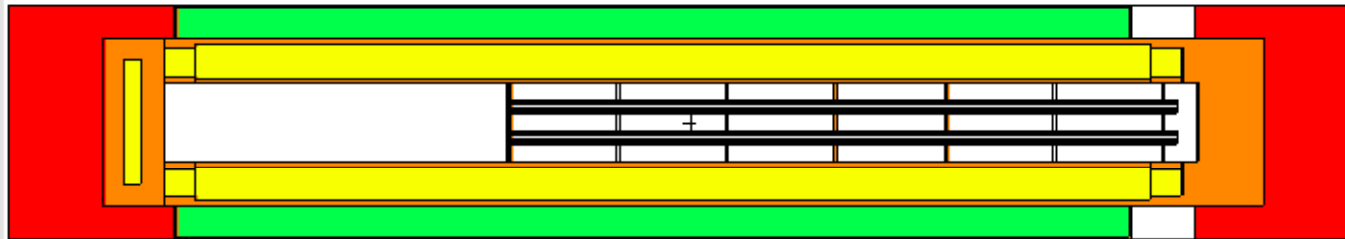
NRU/NRX Shielding Overview

- Source term calculated using SCALE/TRITON
 - Single cell modeled for NRU and NRX cores
 - Compared against “Supercell” model that is representative of the reactor lattice configuration
 - Single cell model shown to be more conservative for the source term evaluation
 - Conservatively adjusted fuel parameters (lower enrichment and higher ^{235}U mass) to maximize source
 - Source terms based on 238-group library calculation to minimize cross-section collapse effects

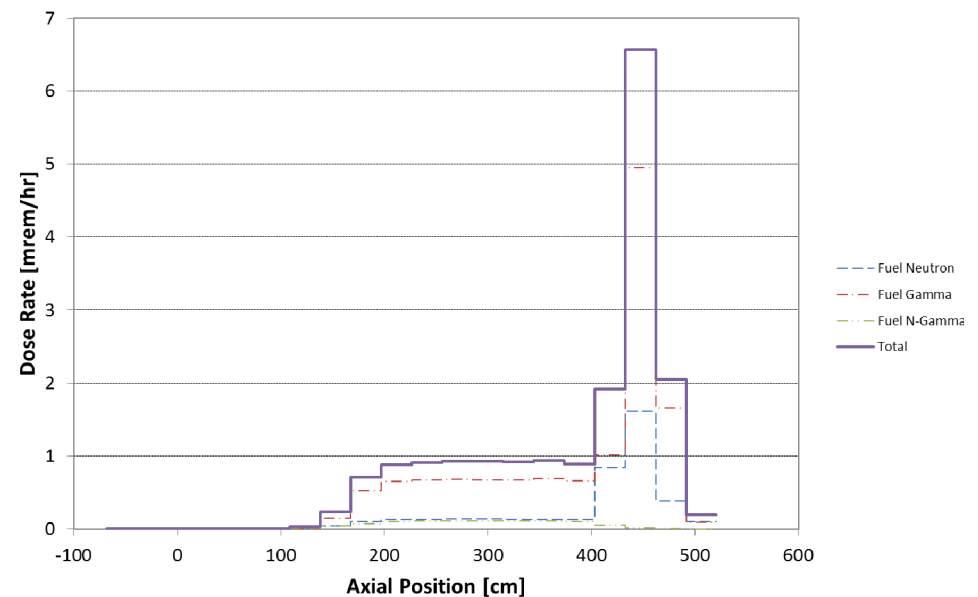
NRU/NRX Shielding Overview (cont'd)

- Source applied in 3-D detailed MCNP model to determine dose rates for normal and accident conditions
 - Includes detailed “as cut” fuel assembly model
 - Basket spacer conservatively not modeled
 - Normal conditions with neutron shield and impact limiter intact
 - Accident condition – lead slump, removal of neutron shield and impact limiter
 - Fuel is uranium-aluminum metal alloy not subject to fuel debris formation observed in oxide fuels
 - Expected transport index (TI) < 1.0

NRU/NRX Shielding Overview (cont'd)



NAC-LWT Cask - NRU Payload v1.0 - NRU Fuel -
Normal Conditions - Rad Detector DRA (Surface)



NRU/NRX Criticality Overview

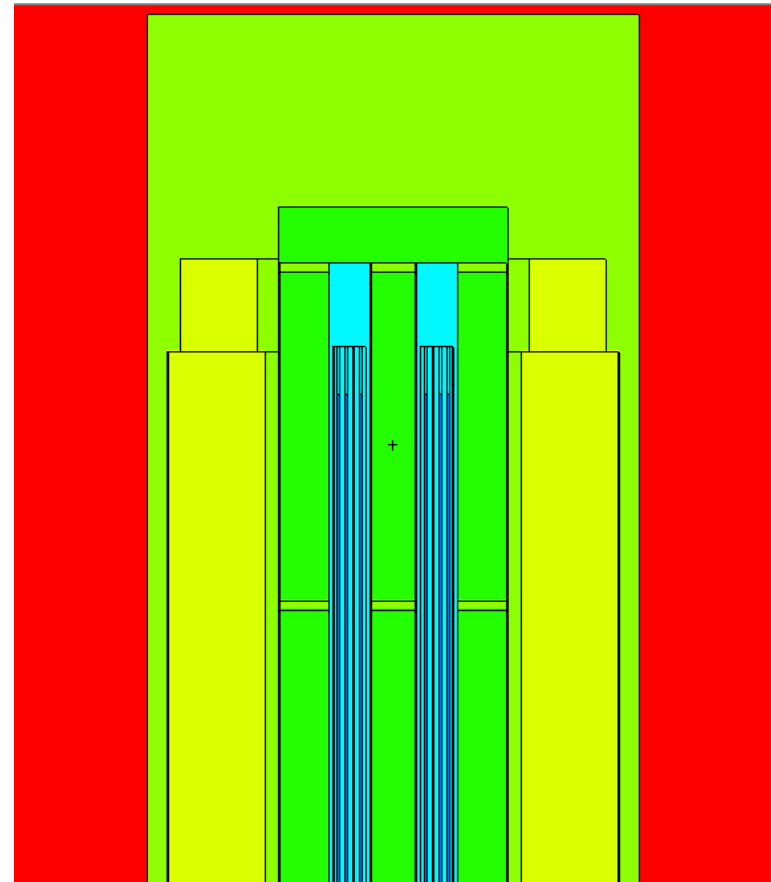
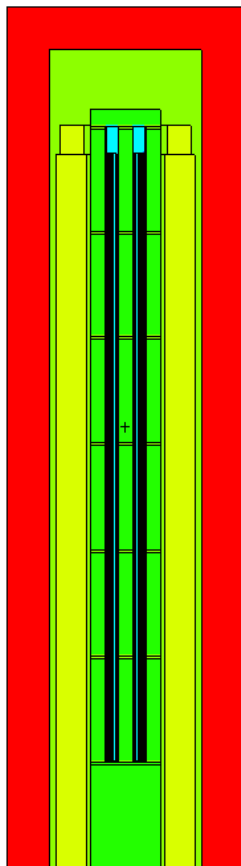
- MCNP5 v1.30 evaluation using primarily ENDF/B-VI cross section
- Code validated for use with highly enriched fuel
- Detailed geometry modeled using tube/basket configuration designed for NRU/NRX fuel in the NAC-LWT
- Evaluated both undamaged fuel and fuel debris
 - Fuel debris evaluated as fuel/water mixtures occupying all void spaces inside tube
 - Uranium/aluminum fuel matrix not expected to produce significant debris

NRU/NRX Criticality Overview (cont'd)

- Evaluated
 - Tube/basket manufacturing tolerances
 - Geometric perturbations
 - Interior and exterior moderator densities to arrive at maximum reactivity conditions as specified in 10 CFR 71.55 and 59
 - Included in moderator density studies is an evaluation of preferential flooding (i.e., moderator density different in tube and cask cavity)
 - 71.59 analysis based on single cask (CSI = 100)

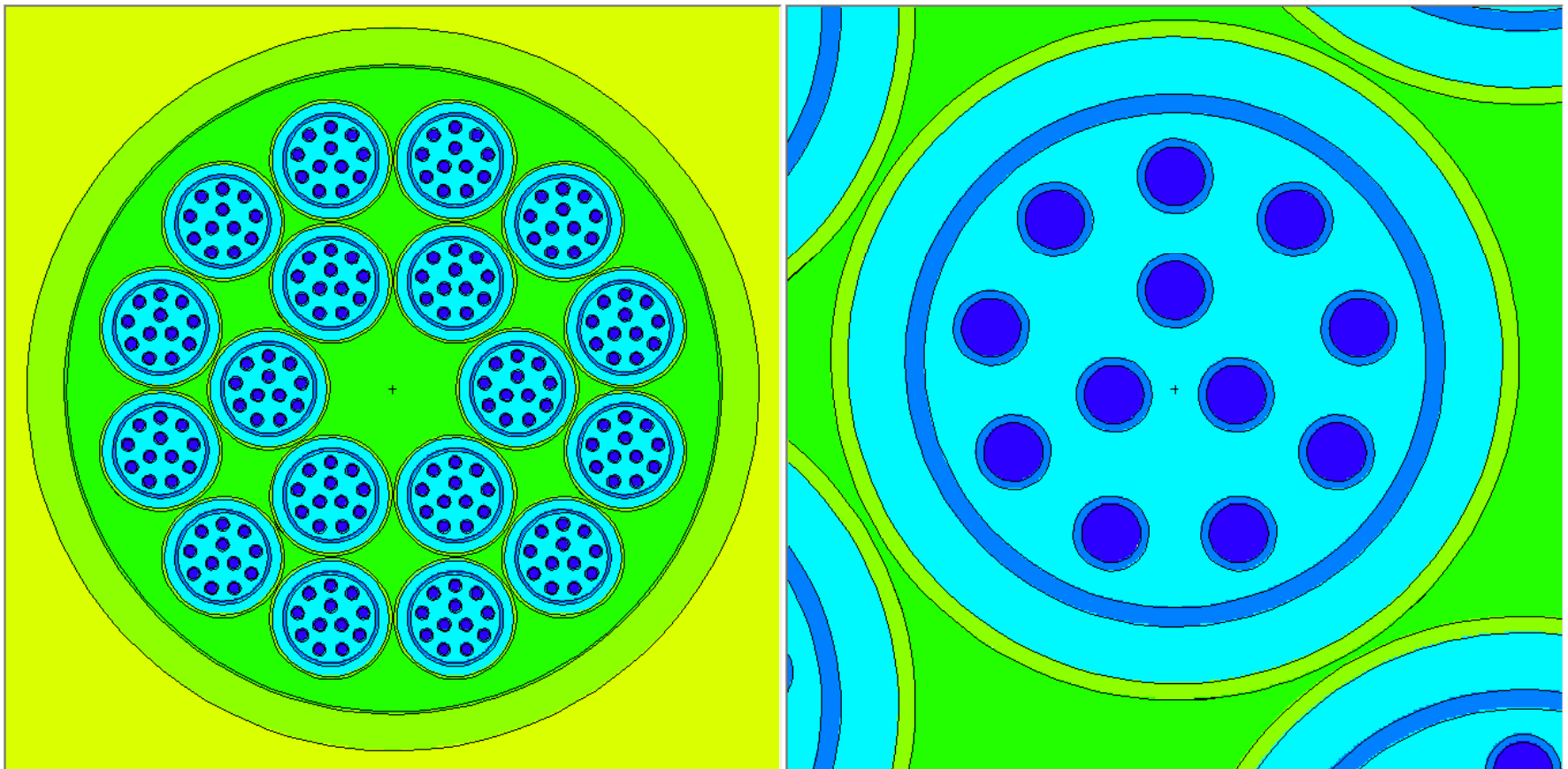
NRU/NRX Criticality Overview (cont'd)

- Model Images



NRU/NRX Criticality Overview (cont'd)

- Model images cont'd



NRU/NRX Criticality Overview (cont'd)

- Maximum reactivity ($k_{\text{eff}} + 2\sigma$) of 0.9275
 - Maximum reactivity due to preferential flood condition

Licensing and Schedule

CONSIDERATIONS

Licensing and Schedule Considerations

- Intend to submit application early September
- Conduct post-submittal meeting late September
- To support NRU/NRX clients, NAC is requesting revised CoC to be issued by March 2013

Q&A Session

